

BK. 42 Dr. 11A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan.....Survey

Ramsey County Prop. (New)

From S.E. Cor. of N.E. $\frac{1}{4}$ Co.....

Sec. 36-30-23

Road Acc't. No.

Date Filed 8-3-48

File.....

Soo Line R.R. Ditch, No. of New Shop,
E Onassso Blvd. No. to Co. Rd. E"
East side of tracks.

W. Line of Co. Prop. in SW $\frac{1}{4}$ of SE $\frac{1}{4}$
Sec. 15-24-23

X Sections

500 Line RR Ditch
North of New Shop.

From & Dwasso Blvd. No.
to Co Rd. "E" East side of tracks

Sta	+	π	-	Elev
BM	5.71	930.11		924.40
			6.2	923.9
			5.8	924.3
			4.0	26.1

Stationing North

0+00 2 Track @ 2 Owasso Blvd N 28.3

-27

28.3

-44

28.3

+14

28.3

+19

28.3

+25

28.3

+15

28.3

Lt

2

R+

2

Top Mont. & Rice @ New Shop

NW Cor. Graded Area N of Shop

Ditch Line @ E Driveway, N Side Prev. on Owaro.

Shoulder Between Above Drive & RR. Track

		w.R.			E Rail		
2.8	<u>2.3</u>	1.91	1.8	<u>1.76</u>	<u>2.1</u>	<u>2.7</u>	
50	26				33	50	

[illegible]

		W Rail		E Rail									
4.4	5.1	5.0	3.1	1.95	1.81	2.6	3.3	4.2	7.4	6.7	4.9	3.3	
50	45	19	8			7	9	18	21	34	47	50	

T/ERRA!

1.75	2.2	2.6	2.3	2.9
1	6	14	27	50

1.8					
1.79	2.2	2.8	5.7	28	30
1	7	20	26	36	50

1							
1	1.8					2.8	
78	2.2	30	7.3			3.1	3.1
1	<u>7</u>	20	31-36			46	50

1.84	2.5	4.5	4.6	6.3	5.2	3.9	3.9
8	21	30	36	42	45	50	

Sta	+	T	-	Elev.
		930.11		
1+00				28.3
	+50			28.3
2				28.2
	+50			28.0
3				27.8
	+50			27.7
4				27.6
	+50			27.5

2

1.8
1/1 Rail

1.84	3.2	4.5	5.7	4.2
2.35	13	30	43	47 & 50

Shoulder ent drive

1.8

1.83

3.1	6.0	9.8	4.7	5.8	4.8
12	25	31	39	44	50

1.9

1.91	2.3	4.2	6.9	6.8	5.4	4.9
8	18	28	37	42	50	

Shoulder Graded Area

2.10

3.5	4.4	7.9	5.7	5.3
10	19	30	38	50

2.3

2.26	3.3	4.9	7.5	5.8	5.7
9	22	31	41	50	

2.4

2.39

3.9	7.2	7.6	5.8
18	26	38	50

2.5

2.45	3.7	4.9	6.5	7.0	5.9
8	21	26	37	50	

2.6

2.59

4.0	9.0	6.3
13	32	50

Sta	+	π	-	Elev
-----	---	-------	---	------

930.11

5				27.4
---	--	--	--	------

+50				27.3
-----	--	--	--	------

6				27.2
---	--	--	--	------

+36 = N Property Line

+50				27.1
-----	--	--	--	------

5.46	929.39	6.18	923.93
------	--------	------	--------

		5.62	924.91
--	--	------	--------

		4.88	
--	--	------	--

→ 929.37³⁹

7

+50

8

+50

Sta

+

π

-

Elu

929.39

9

+50

10

+50

2

Top E Rail

ditch 25'

3.18

4.7 24.7

3.35

5.2 24.2

4.53

5.6 23.8

Sta

+

π

-

Elev

Additional X Sections
Soo Line ROW Ditch
North of New Shop.

10-14-49

GB
BC
MB

Sta	+	π	-	Elev
BM	2.56	929.76		927.2
BM	2.69			927.1
			5.9	23.9
7 + 00				27.0
+ 50				26.8
8				26.6
+ 50				26.4
9				26.3
+ 50				26.1
10				25.9

£

Top of East Rail @ Sta 6+00

" " " " " " 6+50

NW cor. Graded Shop Area.

Stop of East Rail ^{24.3}2.81 4.2 5.5 5.3 5.0

15 23 34 50

3.00

3.8 4.5 4.8

8 24 50

3.17

4.1

^{25.0}

4.8

4.8 4.5

13

17

30 50

3.35

4.1

4.9

^{24.7}

5.1

4.9

9

16

30

50

3.54

4.2

^{24.8}

5.0

4.9

12

32

50

3.72

4.7

5.4

^{24.4}

5.2

4.9

10

19

28

50

3.92

4.9

^{23.9}

5.9

5.3

^{23.0}

4.7

13

22

31

50

Sta	+	π	-	Elev
-----	---	-------	---	------

929.76

10 + 50

25.7

11

25.5

+ 50

25.2

12

24.9

+ 50

24.6

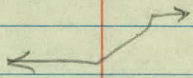
13

24.3

+ 50

24.0

2



TOP E Rail

4.13	5.1	5.6	5.3	4.7
1	9	16	28	50

24.2

4.34	5.2	5.5	4.8	4.5
1	11	17	29	50

24.3

4.56	5.7	6.0	4.6	4.5
1	10	16	22	50

23.8

4.87	6.0	5.9	4.7	4.3
1	9	18	24	50

23.8

5.18	5.9	6.4	4.7	4.8
1	8	16	22	50

23.4

5.50	6.7	6.5	4.6	5.0
1	9	17	23	50

23.1

5.80	7.0	6.9	4.6	4.6
1	9	16	23	50

22.8

Sta	+ π	-	Elev
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*Profile**S Ditch Line N. Owasso Blvd*

Sta + π - Elev

930.11

0+00 100'S $\frac{1}{2}$ track, $\frac{1}{2}$ Nowasso Blvd.

0-100

+25

+43
~~-50~~

+59

+70

+81

1 $\frac{1}{2}$ track $\frac{1}{2}$ Nowasso Blvd

+15
+50

+35

+50

2

3.0

$\begin{array}{r} 1.9 \\ \times 2 \\ \hline 4.2 \\ 23' \end{array}$
 4.3

$\begin{array}{r} 1.8 \\ \times 2 \\ \hline 5.3 \end{array}$

23.5
 6.6

25.6
 4.5

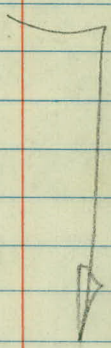
27.2
 3.9

26.9
 3.2

25.3
 4.8

25.5
 4.6

25.9
 4.2



Sta	+	π	-	Elev
-----	---	-------	---	------

		930.11		
--	--	--------	--	--

2 + 00				
--------	--	--	--	--

+50				
-----	--	--	--	--

+90				
-----	--	--	--	--

		Entrance	Prev.	
--	--	----------	-------	--

3				
---	--	--	--	--

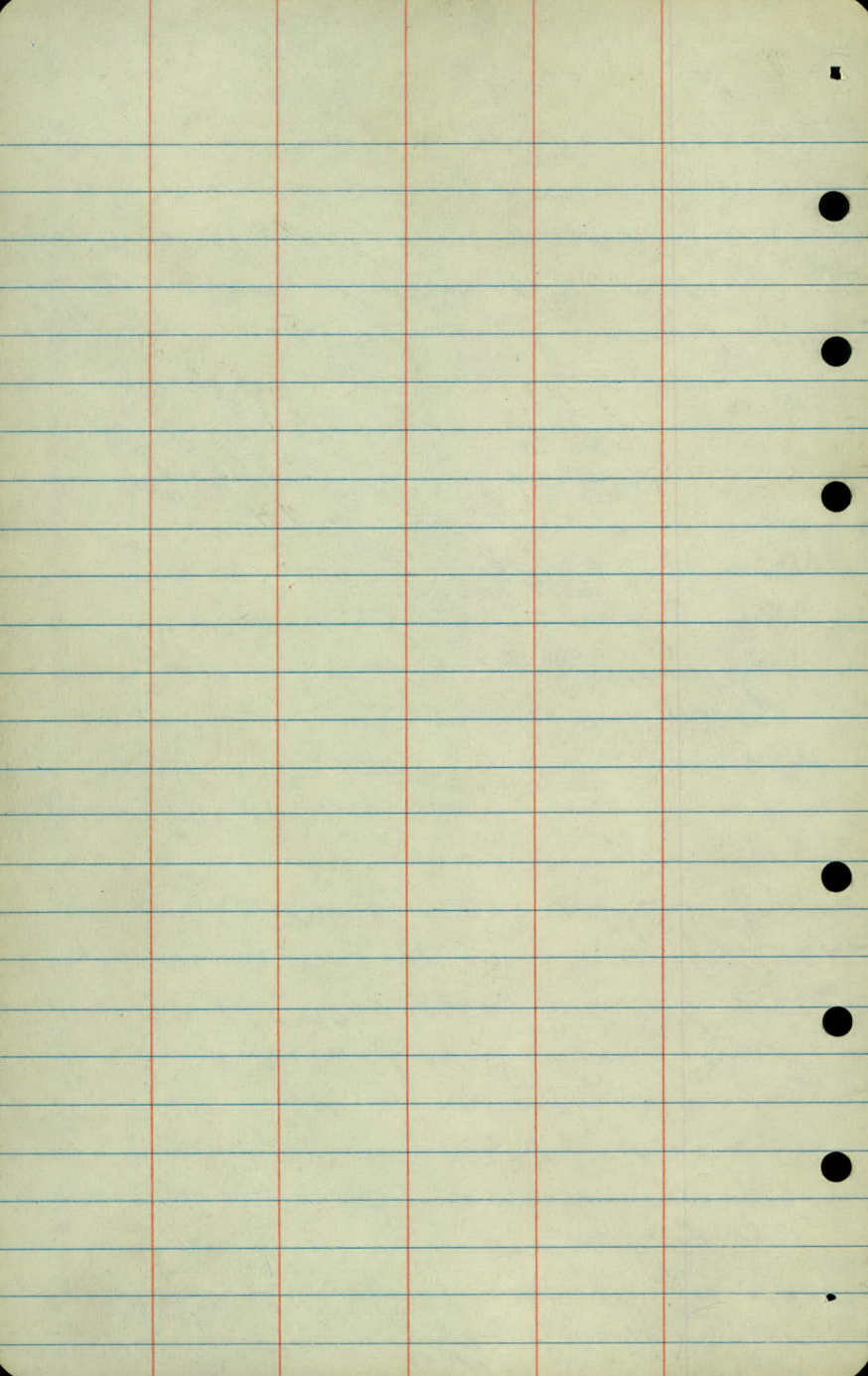
+28				
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44 257

56 24.5

6.1 24.0

7.4 22.7



500 Line R.R. ROW.
Ditch @ New Shop.

X Sections Cont
to Co. Rd "E"

Sta	+	π	-	Elev
BM	2.04	928.99		926.95
"	2.40	(928.99)		926.59
"	3.12	928.96		925.84
		926.83		924.88
T.P.	1.95	926.86	4.08	924.91

14 23.67

+50 23.41

15 23.02

+58 22.49

16 22.01

+50 21.53

17 21.20

Q = Q track

top F Rail

13

= Sta 7+00

= Sta 8+00

= Sta 10+00

3.2	23.0	22.5	22.7	25.3	25.5
3.16	3.8	4.3	4.1	1.5	1.3
	5	7	16	23	50

✓

3.4	22.7	22.3	22.8	25.3	25.5	25.8
3.42	4.1	4.5	4.0	1.5	1.3	1.0
	4	8	11	23	34	50

✓

2.8	22.2	21.8	21.9	24.4	25.3	25.8
3.81	4.1	5.0	4.9	2.4	1.5	1.0
	4	8	16	23	35	50

✓

4.3	21.7	21.5	21.3	23.0	23.7	25.3
4.34	5.1	5.3	5.5	3.8	3.1	1.5
	10	12	18	25	33	50

✓

4.4	21.2	20.2	21.6	23.6
4.82	5.6	6.6	5.2	3.2
	9	17	31	50

✓

5.3	20.9	20.4	19.8	18.4	19.7	20.7
5.30	5.9	6.4	6.9	8.4	7.1	6.1
	8	10	21	26	38	50

✓

5.6	20.4	19.7	19.2	16.8	18.1
5.63	6.4	7.1	7.6	10.0	8.7
	8	11	18	25	50

✓

Sta	+	Σ	-	Elev
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926.83
~~926.86~~

17+50

20.96

18

20.69

+36

20.50

Bm - Sta 10

Top E
Rail5.9
5.87

20.2	13.8	15.5
6.6	13.0	11.3
8	26	50

6.1	19.8	11.8	11.8	13.3	14.9	15.7
6.14	7.0	15.0	15.0	13.3	11.9	11.1
6.0	21	26	31	44	50	50

6.33 6.3

19.8	19.0	9.2	N	0.9
7.0	7.8	17.6	0	0.9
4	8	35	41	50

NS Ditch
Co Rd E

E R.O.W. ditch runs into S ditch
of Co. Rd E Thence under RR
To Catch Basin at toe of RR
fill and S ditch of Co. Rd. E.

Sta

+

π

-

Elev

Typical X Sections
on W. Line of
County Property
in
SW $\frac{1}{4}$ of SE $\frac{1}{4}$ Sec 15 - 29 - 23

7-15-49

GB

AM

MB

BC

Sta.	+	π	-	Elev.
0+00	3.8	103.8		100.00
1+00			9.8	94.0
2+00				94.5
BM	0.2	94.2		94.0 Sta 1+00
3+00				94.2
TP	10.2	104.4		94.2
TP	1.0	99.8 100.8	4.6	98.8 99.8
5+00				99.8

L+

C

R+

$$\begin{array}{r}
 +16.4 \\
 \hline
 80
 \end{array}
 + \frac{+11.0}{62}
 + \frac{+7.6}{51}
 + \frac{0.0}{30}
 + 9.8
 + \frac{16.2}{27}
 + \frac{23.6}{81}
 + \frac{27.2}{125} \checkmark$$

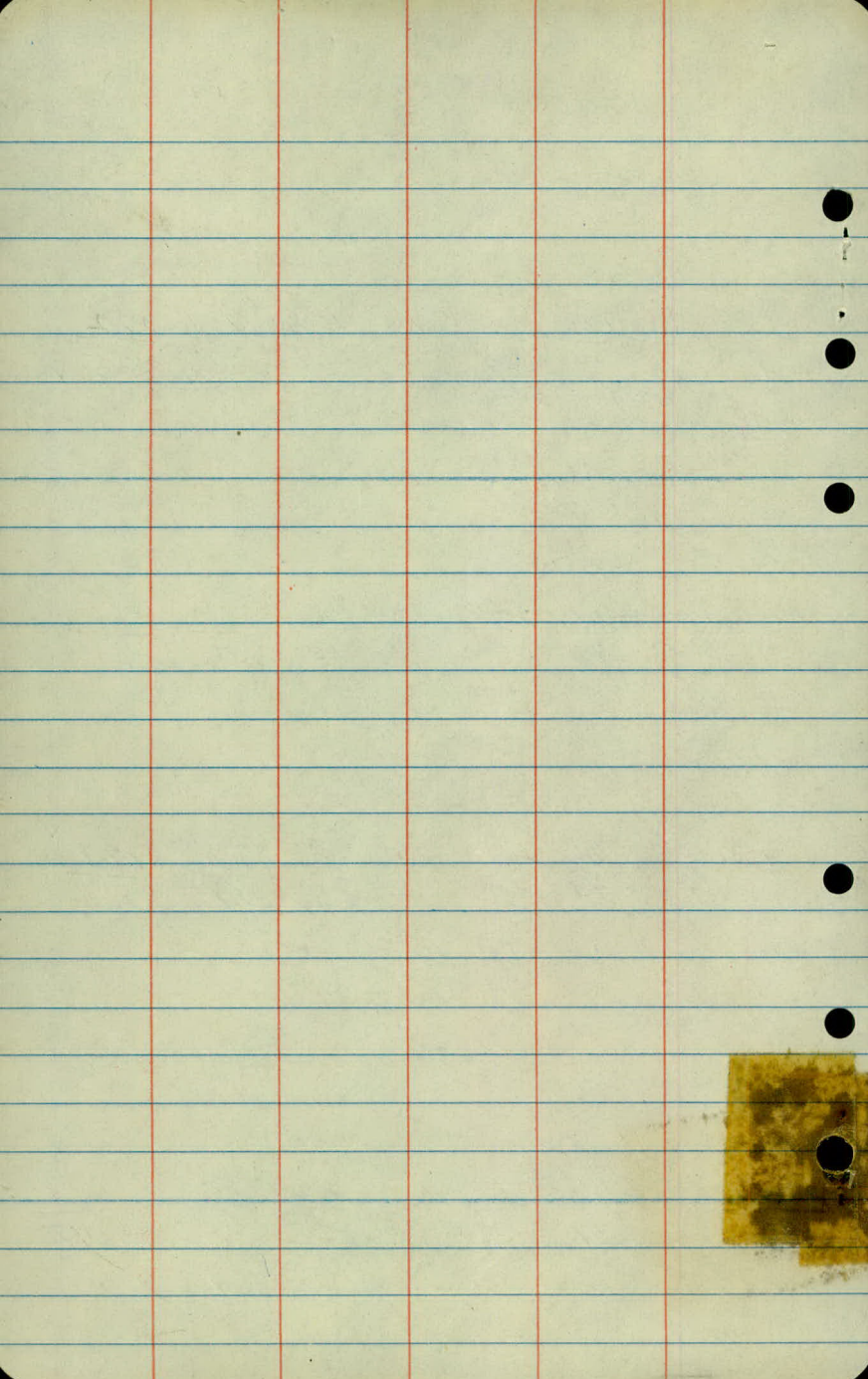
Top of B. Slope.

$$\begin{array}{r}
 25.0 \\
 \hline
 134
 \end{array}$$

$$\begin{array}{r}
 +22.9 \\
 \hline
 120
 \end{array}
 + \frac{+7.7}{46}
 + \frac{+2.3}{30}
 + 9.3
 + \frac{14.8}{13}
 + \frac{23.8}{56}
 + \frac{27.6}{100} \checkmark$$

$$\begin{array}{r}
 +31.6 \\
 \hline
 125
 \end{array}
 + \frac{+17.2}{44}
 + \frac{+11.8}{26}
 + 0.0
 + \frac{7.8}{24}
 + \frac{16.6}{77}
 + \frac{19.1}{100} \checkmark$$

$$\begin{array}{r}
 +22.9 \\
 \hline
 140
 \end{array}
 + \frac{+21.9}{100}
 + \frac{+16.6}{77}
 + \frac{+10.6}{50}
 + 1.0
 + \frac{9.2}{45}
 + \frac{10.8}{95}
 + \frac{12.3}{115} \checkmark$$



FK
KP
JT

May 15, 1957
Cold Cloudy 74°

1

Ramsey Co Property

R/R Ditch X-sections

Sta	+	π	-	Elev
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B.M	6.00	930.40		924.40
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TP	5.82	931.51	4.71	925.69
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0+00 $\nsubseteq$ Owasso Blvd N

+19 Shoulder Line

+25

✓

+50

4

May 15, 1957

2

RT

Top Mont E 1/4 Cor Sec 36-30-22

	28.28	28.2	27.9	27.7			
3.23	3.3	3.6	3.8				
	10	36	50				
E Rail							
28.32	27.9	27.4	26.7	26.4	27.7	27.2	27.49
3.19	3.6	4.1	4.8	5.1	3.8	4.3	4.02
E Rail	5	13	21	27	33	36	46
							BT
28.29	27.9	27.0	25.8	23.1	21.8	21.0	
3.22	3.6	4.5	5.7	8.4	9.7	10.51	
Rail	6	8	18	24	38	32	
						FL 15 CM	
				27.36			
				4.15	4.4	5.2	
				45	40	38	
				BT			
28.21	27.6	27.5	26.2	23.9	21.7	22.1	
3.30	3.9	4.0	5.3	7.6	9.8	9.4	
Rail	3	7	18	21	27	31	
				26.91			
				4.40	5.2	5.2	
				45	41	38	
					26.3		
						26.3	

Sta + π - Elev

931.51

1

✓

+50

✓

2

#

May 15, 1957

RT

3

28.22	27.7	27.3	26.6	23.5	22.2	21.1
3.29	3.8	4.2	4.9	8.0	9.3	9.4
Rail	2	5	16	21	26	28

26.05	25.4	23.1
5.46	6.1	8.4
44	40	33
BT		

28.19	27.5	27.1	27.1	26.3	25.9	23.5
3.32	4.0	4.4	4.4	5.2	5.6	8.0
Rail	2	5	8	10	15	20

25.83	25.4	23.0	22.2
5.68	6.1	8.5	9.3
43	39	32	26
BT			

28.12	27.4	26.8	25.8	23.6	22.2	22.4	24.8
3.39	4.1	4.7	5.7	7.9	9.3	9.1	6.7
Rail	2	5	15	19	25	28	40

25.27
6.24
43
BT

Sta	+	π	-	Elev
-----	---	-------	---	------

		931.51		
--	--	--------	--	--

2+50				
------	--	--	--	--

✓				
---	--	--	--	--

3				
---	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

4				
---	--	--	--	--

TP	1.07	928.16	4.42	927.09
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May 15, 1957 4

27.96	27.2	26.6	26.3	25.6	23.6	22.8
3.55	4.3	4.9	5.2	5.9	7.9	8.7
Rail	2	5	11	16	20	24

24.96	24.4	22.6
6.55	7.1	8.9
43	39	27
BT		

27.79	27.1	26.6	26.0	25.4	23.8	23.2
3.72	4.4	4.9	5.5	6.1	7.7	8.3
Rail	2	5	11	16	20	24

24.2	23.6	22.6
7.3	7.9	8.9
43	37	27
Broken BT		

27.64	26.9	26.6	25.7	23.4	22.7	23.6	24.3
3.87	4.6	4.9	5.8	8.1	8.8	7.9	7.2
Rail	2	4	13	20	25	40	47
						Fe	

27.56	26.9	26.5	25.4	23.5	22.7	22.3	22.8
3.95	4.6	5.0	6.1	8.0	8.8	9.2	8.7
Rail	2	6	17	21	25	28	34

24.0	23.7
7.5	7.8
48	41
Fe	

Sta + π - Elev

928.16

4+50

5

+50

6

27.2 ✓

+50

✓

2

May 15, 1957

Rt

5

27.44

0.72	1.4	1.8	2.6	5.0	5.4	4.5	✓
E Rail	2	5	12	25	34	47	
						Fe	

27.35

0.81	1.5	1.8	1.9	3.5	5.0	5.2	4.8	4.3	✓
Rail	3	5	18	22	27	31	36	47	
								Fe	

27.26

0.90	1.6	2.0	3.5	5.5	5.7	5.1	4.5	✓
Rail	2	7	17	23	27	39	47	
							Fe	

27.14

1.02	1.7	2.1	2.4	3.2	4.6	4.5	4.5	✓
Rail	3	5	12	17	26	37	47	
							Fe	

26.97

1.19	1.8	2.3	2.6	3.4	3.8	4.5	4.3	3.7
Rail	2	7	11	14	18	23	29	32

36 ✓
36
P.P. Line

Sta + π - Elev

928.16

7

+50

8

BM 3.81 929.77 2.20 925.96

+50

9

+50

£

May 15, 1957

6

RT

26.85

✓
1.31 2.0 2.2 2.5 2.9 3.5 4.4 4.4 3.7
E Rail 3 5 10 12 18 26 30 36
PP₁₁

26.71

1.45 2.0 2.3 2.5 3.2 3.1 3.1 3.2
Rail 2 6 11 16 23 30 36

26.50

1.66 2.3 2.5 2.6 3.2 3.4 3.5 3.5
Rail 3 6 10 13 22 32 36
Spike in PP 820' at sta 2+?

26.30

3.47 4.1 4.3 4.5 4.8 5.1 5.1 5.3
Rail 3 8 11 14 22 30 36

26.12

3.65 4.2 4.4 4.5 4.7 5.3 5.4
Rail 2 6 11 15 22 36

25.93

3.84 4.5 4.7 5.1 5.8 5.7 5.5 5.4
Rail 3 6 11 20 24 29 36

Sta + π - Elev

929.77

10

10 + 50

11

+ 50

12

+ 50

TP 4.06 927.75 6.08 923.69

2

May 15, 1957

Rt

7

25.76

4.01	4.6	5.0	5.3	6.0	5.8	5.5	5.2
E. Rail	3	7	11	16	23	29	36

P.P. Line

25.53

4.24	4.9	5.2	5.4	5.8	5.3	5.2	5.3
Rail	2	7	11	14	21	31	36

25.32

4.45	5.2	5.5	5.6	5.8	5.2	5.0	5.0
Rail	3	6	11	14	20	28	36

25.08

4.69	5.4	5.7	5.7	5.7	4.7	4.7	4.7
Rail	2	6	10	15	19	29	36

24.79

4.98	5.7	6.0	6.2	4.8	4.6	4.5
Rail	2	6	14	19	30	36

24.49

5.28	6.0	6.2	6.3	4.7	4.7	4.9
Rail	2	6	13	21	30	35

Sta

+

π

-

Elev

927.75

13

+50

14

+50

15

+50

2

May 15, 1957

BT

8

24.10

3.65	4.3	4.5	4.4	2.8	3.0
E. Rail	2	6	14	20	35

PP Line

23.83

3.92	4.7	4.9	4.9	2.6	2.6
Rail	3	6	14	21	35

PP Line

23.58

4.17	5.0	5.2	5.1	2.5	2.4
Rail	2	5	14	21	35

23.30

4.45	5.1	5.2	5.2	2.6	2.3
Rail	3	6	14	20	35

22.85

4.90	5.6	5.8	5.8	3.7	2.6	2.4
Rail	3	6	13	20	28	34

PP Line

22.33

5.42	6.0	6.5	5.0	4.0	3.7
Rail	2	14	20	29	32

sta

927.75

16+00

16+29.3 Intersection of E. Rail & N. P. L. Extended

+50

17

BM

1.84 925.91

2

RT

9

21.79

5.96	6.6	7.6	6.3	5.5
ERail	5	15	29	39

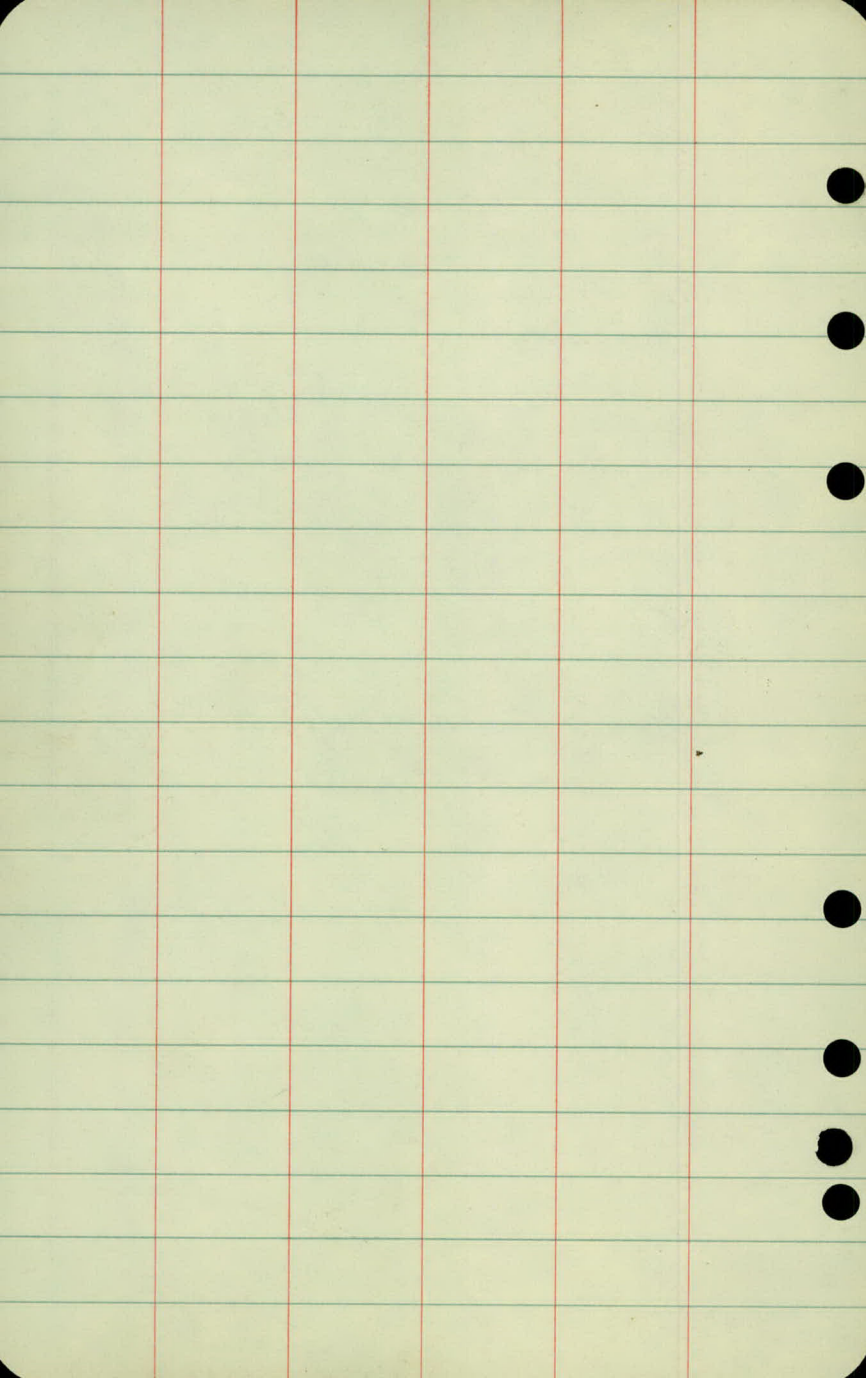
21.35

6.40	7.0	7.2	7.9	8.4	9.6	8.9	8.1
ERail	3	7	15	20	24	35	42

21.03

6.72	7.2	7.5	8.5	11.3	11.1	10.4
	2	6	12	22	31	42

Spike in PP 820' Lt sta 21 P'



Ramsey Co Property

Survey of 1957

at Rice St +

No Onasso Blvd

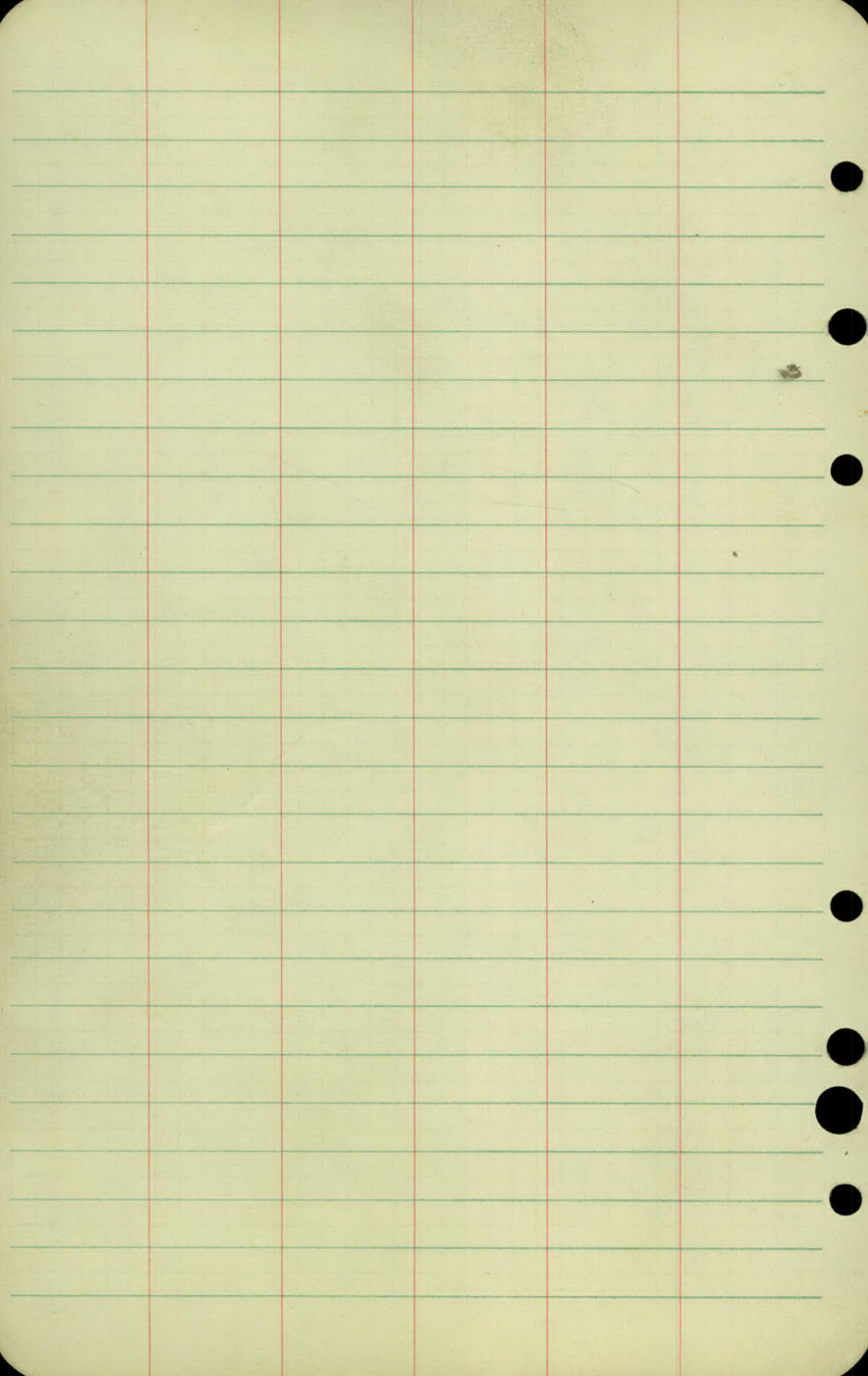
22
19
18 Pages

Recd.

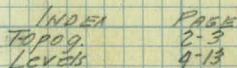
4/22/57

3:55 PM.

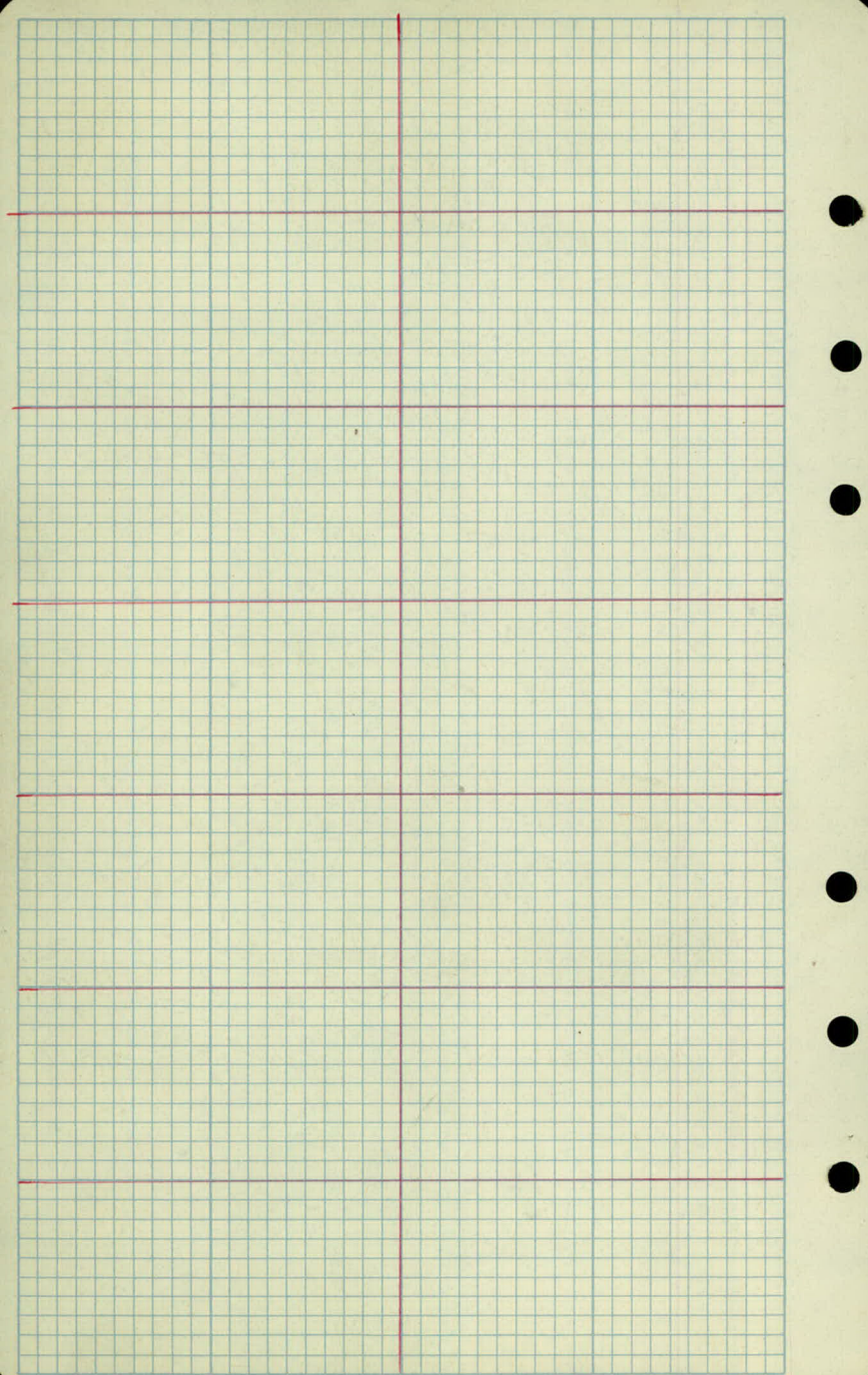
L.C.



5-11-48 - K. Antler.



Power



Topography

+46-S.E. Cor. Ho-111
+31-30°0'-34'
+16-30°0'-50
+11-30°0'-131

4

+95-30°0'-140
+69-30°0'-123
+60-30°0'-43

+44-PP-20 PP-30'

3 36°0'-41'

+67-24°0'-62'
+44-24°0'-61'
+41-30°0'-103'
+41-24°0'-72'
+33-30°0'-40
+26-18°0'-22'
+13-24°0'-54'-137

2

+89-30°0'-35' +92-30°0'-117
+79-PP-19- PP-25'
+53-30°0'-157'
+34-18°0'-68'
+27-18°0'-20
+24-36°0'-45
+75-24°0'-37' s/p-123'
+14-30°0'-40
+13-30°0'-108'

1

+79-30°0'-68'

0

+15-PP-19'

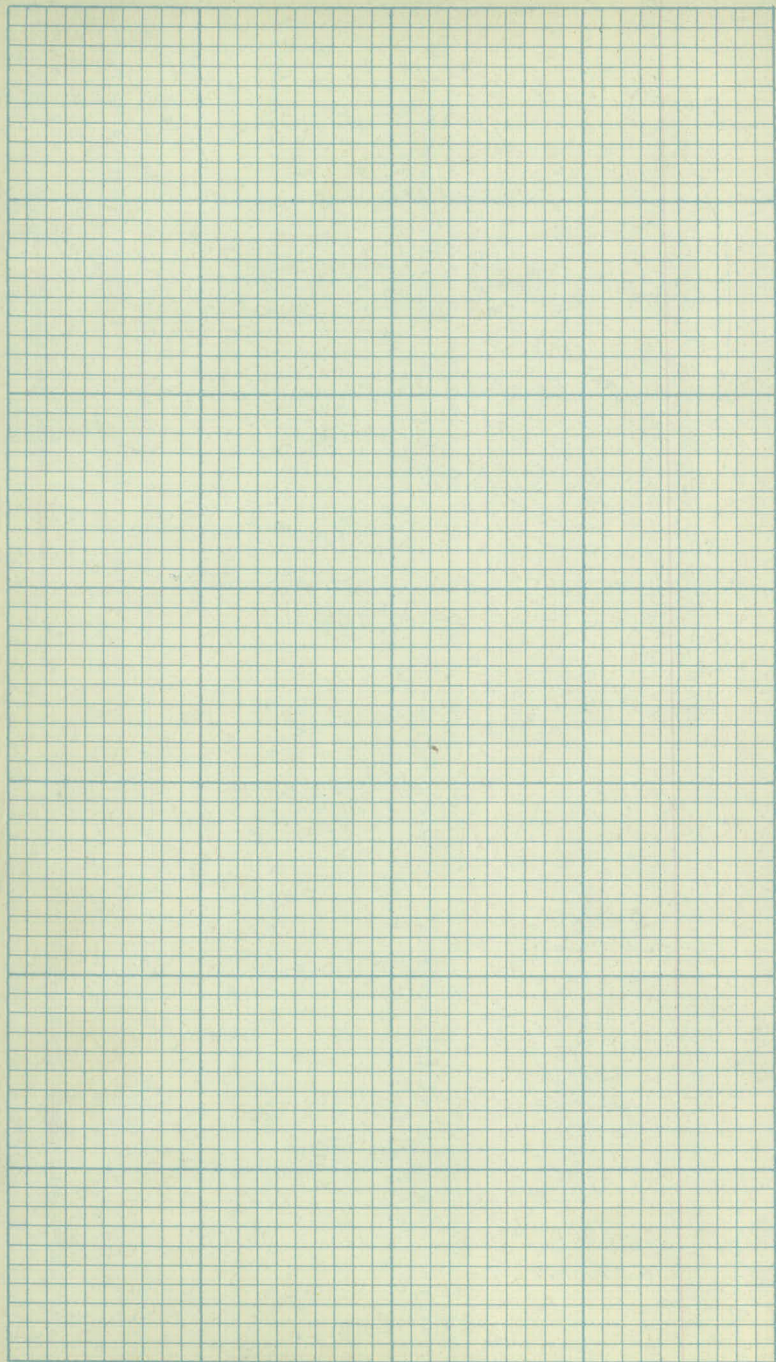
-07-18°E Int-33- Low 1° Pp.
-22-N.E. Cor. Ho-60'

-01-PP-25' = New.

317.45
305
406.45

24' 20'
15'

20' 14' 55"
34'

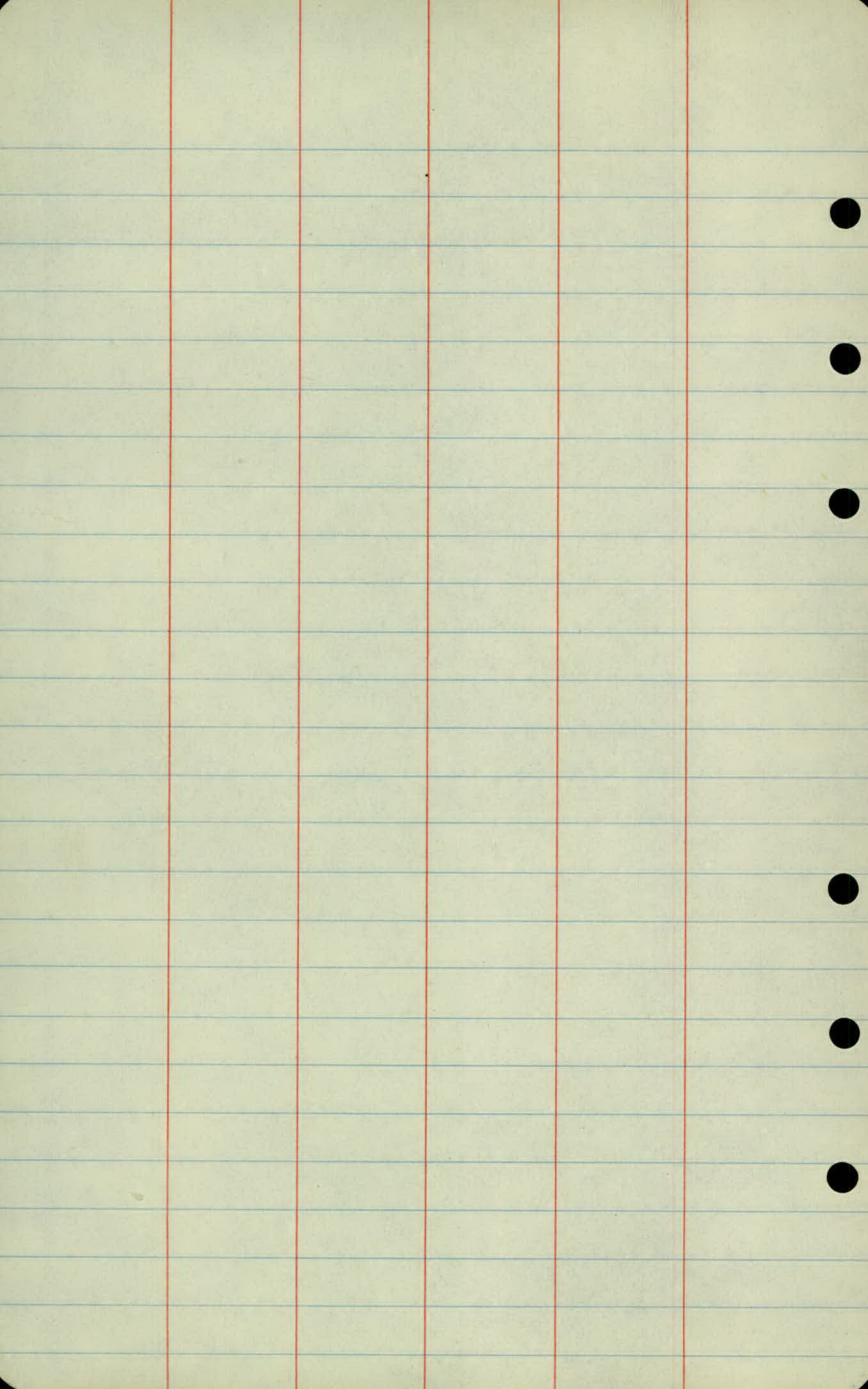


Bench Levels

Sta	+	-	Elev	
B.M.	6.38	898.66		(892.28)
	9.54	903.11	5.09	893.57
	12.77	915.77	0.11	903.00
	11.88	927.42	0.23	915.54
	5.01	932.06	0.37	927.05
B.M			7.66	924.40
	1.49	927.97	5.58	926.48
	0.32	915.86	12.43	915.54
	0.60	903.61	12.85	903.01
	4.97	898.55	10.03	893.58
			6.27	892.28

Spt. in 20" Oct. SW. of Pump Ho. of Lake Owasso
(Lake Imp. Data.)

Top. MONT. E. $\frac{1}{4}$ Cor. Sec. 36-30-23



Levels

Rice = Base Line

stationing runs north.

Distances to west = left.

Xsections are parallel to Rice St
and E-W sec. line.

Sta.	+	π	-	Elev
B.M.	553	929.93		(924.40)

0 +100

+25

+50

+75

+25

+50

+75

1. H.
A.M.
M.B.
P.G.

5-11-48

7

Top Mont E 1/4 Cor. Sec. 36

Edge Pay

25.9	24.8	24.5	24.5	24.3	24.1	24.37	24.40
40	51	54	54	56	58	556	553
100	75	50	33	29	18	12.2	

25.6	24.9	24.2	24.0	24.0		24.45	24.52
43	50	57	59	59		548	541
100	75	50	33	21		12.3	

25.9	24.7	24.2	24.2	24.0	24.3	24.52	24.62
40	52	57	57	59	56	541	531
100	75	50	33	22	13	12.4	

25.5	24.9	24.3	23.9	24.4		24.62	24.75
44	50	56	60	55		531	518
100	75	50	33	19		12.5	

25.8	25.0	24.3	23.9	24.6		24.82	24.85
41	49	56	60	53		511	508
100	75	50	33	20		12.5	

26.1	25.3	24.7	24.3	24.0	24.8	24.91	24.90
38	46	52	56	59	51	502	503
100	75	50	33	29	18	12.6	

26.2	25.7	25.1	24.3	24.2	25.0	25.03	25.00
37	42	48	56	57	49	490	493
100	75	50	33	29	18	12.7	

26.5	26.1	25.3	24.9	24.9	23.4	25.1	25.15
34	38	46	50	50	65	48	476
100	75	50	33	31	26	24	20

Sta.	+	π	-	Elev.
		929.93		

2

+25

+50

+75

3

+25

+50

+75

L

4

Edge

Par

26.6	26.3	25.5	25.1	23.6	25.1	25.32	25.30
33	36	44	48	63	48	461	463
100	75	50	33	30	27	23	20

26.7	26.4	25.6	25.1	23.3	25.2	25.44	25.45
32	35	43	48	66	47	449	448
100	75	50	33	32	26	24	19

26.6	26.4	25.8	25.2	25.0	23.6	25.4	25.56
33	35	41	47	49	63	45	437
100	75	50	33	31	27	24	19

26.4	26.5	26.0	25.4	25.2	23.6	25.6	25.67
35	34	39	45	47	63	43	426
100	75	50	33	31	27	24	20

26.3	26.6	26.3	25.8	25.7	23.9	25.7	25.80
36	33	36	41	42	60	42	413
100	75	50	33	32	27	24	19

26.5	26.8	26.6	25.9	25.9	23.9	25.9	25.95
34	31	33	40	40	60	40	398
100	75	50	33	31	27	24	19

26.5	26.9	26.8	26.0	26.0	24.2	26.1	26.07
34	30	31	39	39	57	38	386
100	75	50	33	32	27	24	19

26.3	26.7	26.6	26.1	25.7	24.3	26.0	26.12
36	32	33	38	42	56	39	381
100	75	50	33	30	27	24	19

Sta	+	π	-	Elev.
		929.93		

4

+25

B.M.	602	930.42	5.53	924.40
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0 +00

+25

+50

25.8 26.1 26.1 25.7 25.3 24.0 26.0
 41 3.8 3.8 4.2 4.6 5.9 3.9 3.73 3.71
 100 75 50 39 30 27-24 18 13

Edge
 Pav
 26.20
 26.22

25.4 25.6 25.8 25.5 25.4 24.0 26.0
 4.5 4.3 4.1 4.4 4.5 5.9 3.9
 100 75 50 33 31 27-24 19

26.28
 26.28
 26.33
 365 360
 13

25.1 25.0 25.3 25.4 25.4 25.6 26.1 26.4 26.3 26.3
 53 54 51 50 50 48 43 40 41 41 37
 375 350 325 300 275 250 225 200 175 150 125

25.1 24.9 25.3 25.2 24.2 25.1 25.0 23.4 26.6 27.6 28.20
 5.9 5.5 5.1 5.2 6.2 5.3 5.4 7.0 3.8 2.8 2.2 = Top Rail
 400 425 450 475 500 508 521 529 552 559 558
 Fe.

25.0 25.0 25.0 25.4 25.6 25.8 26.2 26.3 26.4 26.8 26.7
 54 54 54 50 48 46 42 41 40 3.6 3.7
 375 350 325 300 275 250 225 200 175 150 125

25.1 25.0 25.1 25.8 25.1 25.4 25.1 23.5 23.1 25.8 26.7 27.5 28.12
 5.3 5.4 5.3 4.6 5.3 5.0 5.3 6.9 7.3 4.6 3.7 2.9 2.30 = Top Rail
 400 475 450 475 500 518 526 533 542 552 565 568 570
 Fe.

25.4 25.4 25.1 24.8 25.0 25.4 25.4 25.6 25.9 26.2 26.4 26.6 26.3
 5.0 5.0 5.3 5.6 5.4 5.0 5.0 4.8 4.5 4.2 4.0 3.8 4.1
 425 400 375 350 325 300 275 250 225 200 175 150 125

25.5 24.9 24.9 25.8 24.9 22.7 25.7 26.7 27.3 28.02
 4.9 5.5 5.5 4.6 5.5 7.7 4.7 3.7 3.1 2.40 = Top Rail
 450 475 500 529 543 553 557 565 577 581 583
 Fe.

Sta

+

π

-

Elev.

930.42

0 +75

1 +00

+25

+50

K.H.
A.M.
M.B.
R.C.

5-11-48

10

25.6 25.2 24.9 25.1 25.2 25.4 25.7 25.9 25.9 26.3 26.6 26.8

48 52 53 53 52 50 47 45 45 41 38 36
400 375 350 325 300 275 250 225 200 175 150 125

25.3 25.3 25.0 24.8 25.2 25.1 24.9 22.0 25.3 26.4 27.3 27.94

51 51 54 56 52 53 55 84 51 40 31 248 = Top Rail
425 450 475 500 525 541 551 561 565 573 586 590 592
Fe.

25.5 25.4 25.4 24.8 24.5 25.0 25.1 25.1 25.3 25.5 26.0 26.5 26.2

49 50 50 56 59 54 53 53 51 49 44 39 42
425 400 375 350 325 300 275 250 225 200 175 150 125

25.3 25.1 24.6 25.2 25.1 24.9 24.0 26.3 26.6 27.3 27.85

51 53 58 52 53 55 64 41 38 31 257 = Top Rail
450 475 500 525 552 569 578 573 598 601 604
Fe.

25.5 25.6 25.4 25.0 25.1 25.1 25.1 24.9 25.1 25.2 25.8 26.4 26.5

49 48 50 54 53 53 53 55 53 52 46 40 39
425 400 375 350 325 300 275 250 225 200 175 150 125

25.4 25.0 24.9 25.1 24.9 25.0 24.3 21.6 22.7 25.1 26.6 27.1 27.79

50 54 55 53 55 54 61 88 77 53 38 33 263 = Top Rail
450 475 500 525 550 563 569 580 587 594 609 613 615
Fe.

25.1 25.3 25.4 25.4 25.2 25.4 25.3 25.3 25.2 25.1 25.4 25.5 26.1 26.5

53 51 50 50 52 50 51 51 52 53 50 49 43 39
450 425 400 375 350 325 300 275 250 225 200 175 150 125

25.1 24.7 25.0 24.6 24.8 22.8 24.1 26.3 26.5 27.2 27.71

53 57 54 58 56 76 63 41 39 32 271 = Top Rail
475 500 525 550 575 584 601 615 620 624 626
Fe.

Elev.	+	π	-	Elev.
		930.42		

1	+75			
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2	+00			
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B.M.	5.82	930.22	6.02	929.40
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	+25			
--	-----	--	--	--

	+50			
--	-----	--	--	--

L

R

25.5 25.4 25.2 25.2 25.4 25.5 25.2 25.0 25.2 25.4 25.6 26.3 26.6
49 50 52 52 50 49 52 54 52 50 49 41 38
425 400 375 350 325 300 275 250 225 200 175 150 125

25.1 25.1 24.8 24.8 25.0 24.9 24.8 23.3 23.4 25.7 26.3 27.1 27.64
5.3 5.3 5.6 5.6 5.4 5.5 5.6 7.1 7.0 4.1 4.1 9.3 27.8 = Top Rail
450 475 500 525 550 575 596 599 613 621 631 635 637.5
Fe.

25.2 25.5 25.7 25.6 25.6 25.6 25.6 25.3 25.2 25.4 25.6 25.9 26.6 26.7
5.2 4.9 4.7 4.8 4.8 4.8 4.8 5.1 5.2 5.0 4.8 4.5 3.8 3.7
450 425 400 375 350 325 300 275 250 225 200 175 150 125

25.0 24.8 25.2 25.1 24.6 24.9 23.4 22.9 25.4 26.3 26.9 27.61
5.4 5.6 5.2 5.3 5.8 5.5 7.0 7.5 5.0 4.1 3.5 2.81 = Top Rail
475 500 525 550 575 599 609 621 631 643 647 649
Fe.

25.7 25.7 25.8 26.0 25.8 25.6 25.6 25.6 25.5 25.7 25.9 26.3 26.7
46 45 44 42 44 46 46 46 47 45 43 39 35
425 400 375 350 325 300 275 250 225 200 175 150 125

25.1 25.0 24.8 25.1 24.9 24.6 24.8 24.5 21.8 25.0 26.2 26.8 27.56
5.1 5.2 5.4 5.1 5.3 5.6 5.4 5.7 5.84 5.2 4.0 3.4 2.66 = Top Rail
450 475 500 525 550 575 600 611 624 628 640 654 659 660
Fe.

25.3 25.6 25.8 25.7 25.8 25.7 25.7 25.6 25.7 25.6 25.7 26.1 26.4
49 4.6 4.4 4.5 4.4 4.5 4.5 4.6 4.5 4.6 4.5 4.5 4.1 3.8
450 425 400 375 350 325 300 275 250 225 200 175 150 125

25.2 25.1 25.2 25.0 24.5 24.6 24.4 21.3 25.7 26.3 26.8 27.51
5.0 5.1 5.0 5.2 5.7 5.6 5.8 8.9 4.5 3.9 3.4 2.71 = Top Rail
475 500 525 550 575 600 620 633 642 657 666 670 672
Fe.

Sta.	+	π	-	Elev.
		950.22		

2	+75			
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3				
---	--	--	--	--

	+25			
--	-----	--	--	--

	+50			
--	-----	--	--	--

25.3

25.6

25.9

25.8

25.8

25.8

25.9

25.7

25.9

25.8

25.5

25.5

25.5

25.9

26.3

4.9 4.6 4.3 4.4 4.4 4.4 4.3 4.5 4.3 4.4 4.7 4.7 4.3 3.9
 450 475 400 375 350 325 300 275 250 225 200 175 150 125

25.0

24.6

25.1

25.0

24.4

24.4

24.2

23.8

21.7

26.6

26.3

26.9

27.46

5.2 5.6 5.1 5.2 5.8 5.8 6.0 6.4 8.5 3.6 3.9 3.3 2.76 = Top Rail
 475 500 525 550 575 600 625 632 645 663 678 692 693
 Fe.

25.6

25.7

25.9

26.0

25.8

25.6

25.7

25.8

25.6

25.5

25.6

25.7

26.1

4.6 4.5 4.3 4.2 4.4 4.6 4.5 4.4 4.6 4.7 4.6 4.5 4.1
 425 400 375 350 325 300 275 250 225 200 175 150 125

25.4

24.8

24.8

25.1

24.6

24.5

24.2

24.3

24.5

25.0

23.2

26.1

26.1

26.8

27.40

4.8 5.4 5.4 5.1 5.6 5.7 6.0 5.9 5.7 5.2 7.0 4.1 4.1 3.4 2.92 = Top Rail
 450 475 500 525 550 575 600 625 644 655 667 675 689 692 694
 Fe.

24.9

25.5

25.6

25.9

25.6

25.5

25.4

25.4

25.6

25.6

25.1

25.5

25.7

26.1

5.3 4.7 4.6 4.3 4.6 4.7 4.8 4.3 4.6 4.6 5.1 4.7 4.5 4.1
 450 425 400 375 350 325 300 275 250 225 200 175 150 125

24.8

25.0

25.2

24.6

24.5

24.2

24.2

24.6

24.4

21.4

25.8

26.8

27.34

5.4 5.2 5.0 5.6 5.7 6.0 6.0 5.6 5.8 5.8 4.4 4.4 2.88 = Top Rail
 475 500 525 550 575 600 625 650 654 677 680 693 704 706
 Fe.

24.7

25.0

25.4

25.5

25.6

25.7

25.5

25.7

25.3

25.4

25.3

25.0

25.2

25.7

25.9

5.5 5.2 4.8 4.7 4.6 4.5 4.7 4.5 4.9 4.8 4.9 5.2 5.0 4.5 4.3
 475 450 425 400 375 350 325 300 275 250 225 200 175 150 125

24.6

25.1

24.7

24.4

24.3

24.4

24.3

24.4

24.2

22.5

22.2

24.5

26.0

26.5

27.27

4.6 5.1 5.5 5.8 5.9 5.8 5.9 5.8 6.0 7.7 8.0 5.7 4.2 3.7 2.95 = Top Rail
 500 525 550 575 600 625 650 666 670 679 688 696 712 714 717
 Fe.

Sta.	+	π	-	Elev.
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930.22

3 +75

4

+25

B.M.

583

924.39

(92440)

K.A.
A.M.
M.B.
B.C.

5-12-48

13

24.9	25.1	25.5	25.7	25.7	25.4	25.4	25.1	25.2	24.9	25.0	24.7	25.9	
53	51	47	45	45	48	48	51	50	53	52	55	46	43
450	425	400	375	350	325	300	275	250	225	200	175	150	125
25.0	24.7	25.0	24.6	24.6	24.1	24.1	24.2	24.2	24.3	24.3	24.3	23.2	23.7
52	55	52	56	56	61	61	60	60	59	59	59	70	65
475	450	425	400	375	350	325	300	275	250	225	200	175	150
25.1	25.3	25.2	25.6	25.6	25.3	25.2	24.8	24.4	24.6	24.6	25.0	25.6	
51	49	50	46	46	49	50	54	58	56	56	52	46	
425	400	375	350	325	300	275	250	225	200	175	150	125	
25.0	24.8	24.6	25.0	24.7	24.4	24.2	24.4	24.5	24.6	24.6	23.5	23.8	25.8
52	54	56	52	55	59	60	59	57	56	56	67	64	44
450	475	500	525	550	575	600	625	650	675	699	709	719	729
24.9	25.1	25.5	25.5	25.1	24.9	24.6	24.3	24.4	24.6	24.8	25.4	25.4	
53	51	47	47	51	53	56	59	59	56	54	48	48	
400	375	350	325	300	275	250	225	200	175	150	125		
24.7	24.6	24.7	24.7	24.9	24.6	24.4	24.4	24.6	24.7	24.7			
55	56	55	55	53	56	58	58	58	56	55	55		
425	450	475	500	525	550	575	600	625	650	675	701		
27.04	26.44	25.8	23.9	23.6	24.7								
318	38	44	63	66	56								
752	750	742	732	725	717								

Top Rail

= 318 38 44 63 66 56

Top Mont.

Sta.	+ -	π	-	Elev.
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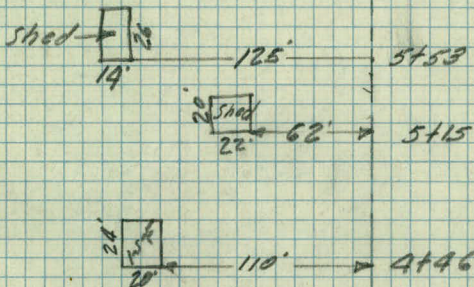
7

万

100

Elev.

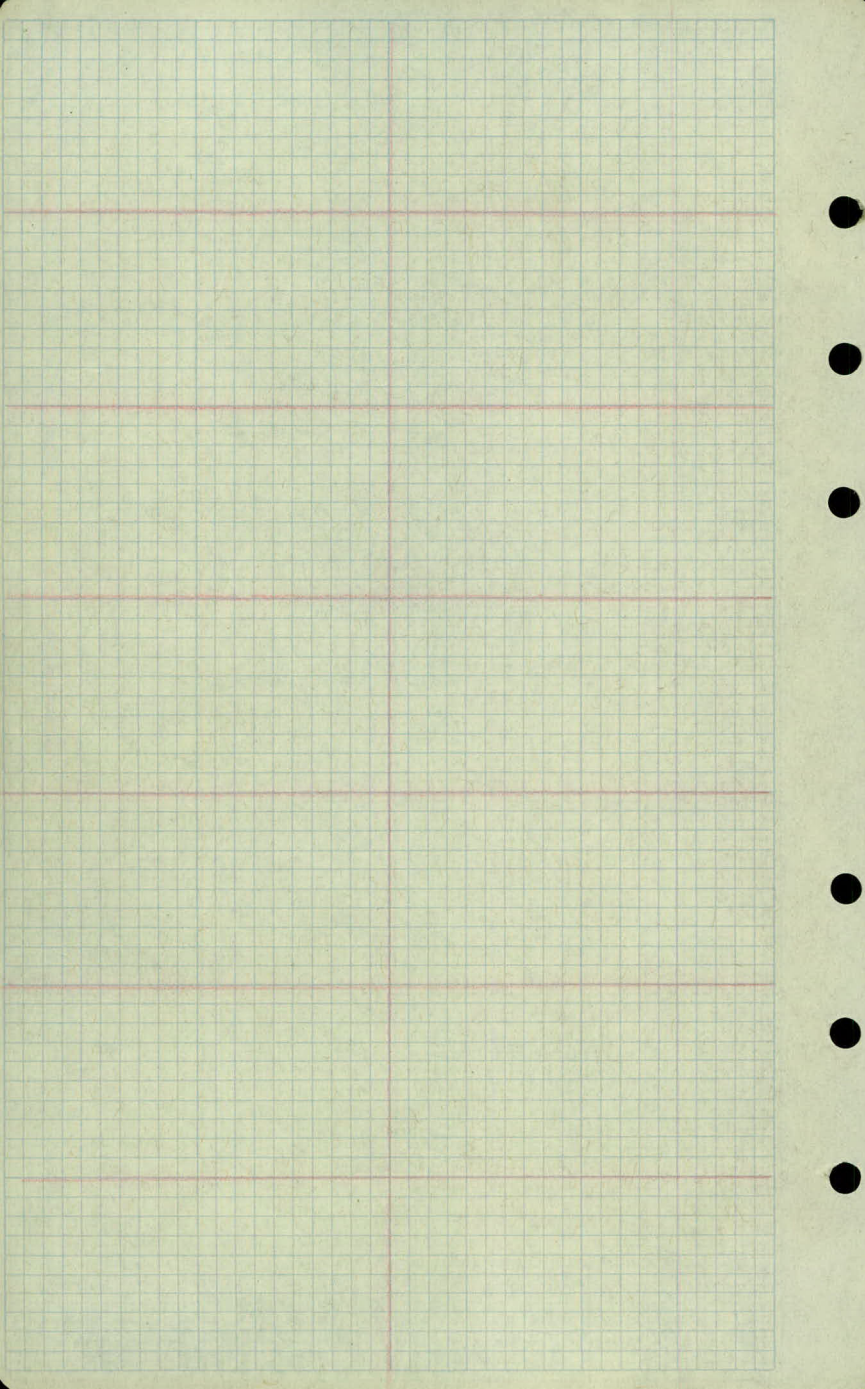
1-7-47



E 1/4 Cor. Sec. 36-30-23
0+00

Location of Bldg
Proposed Shop Location
Rice St. Near Owasso

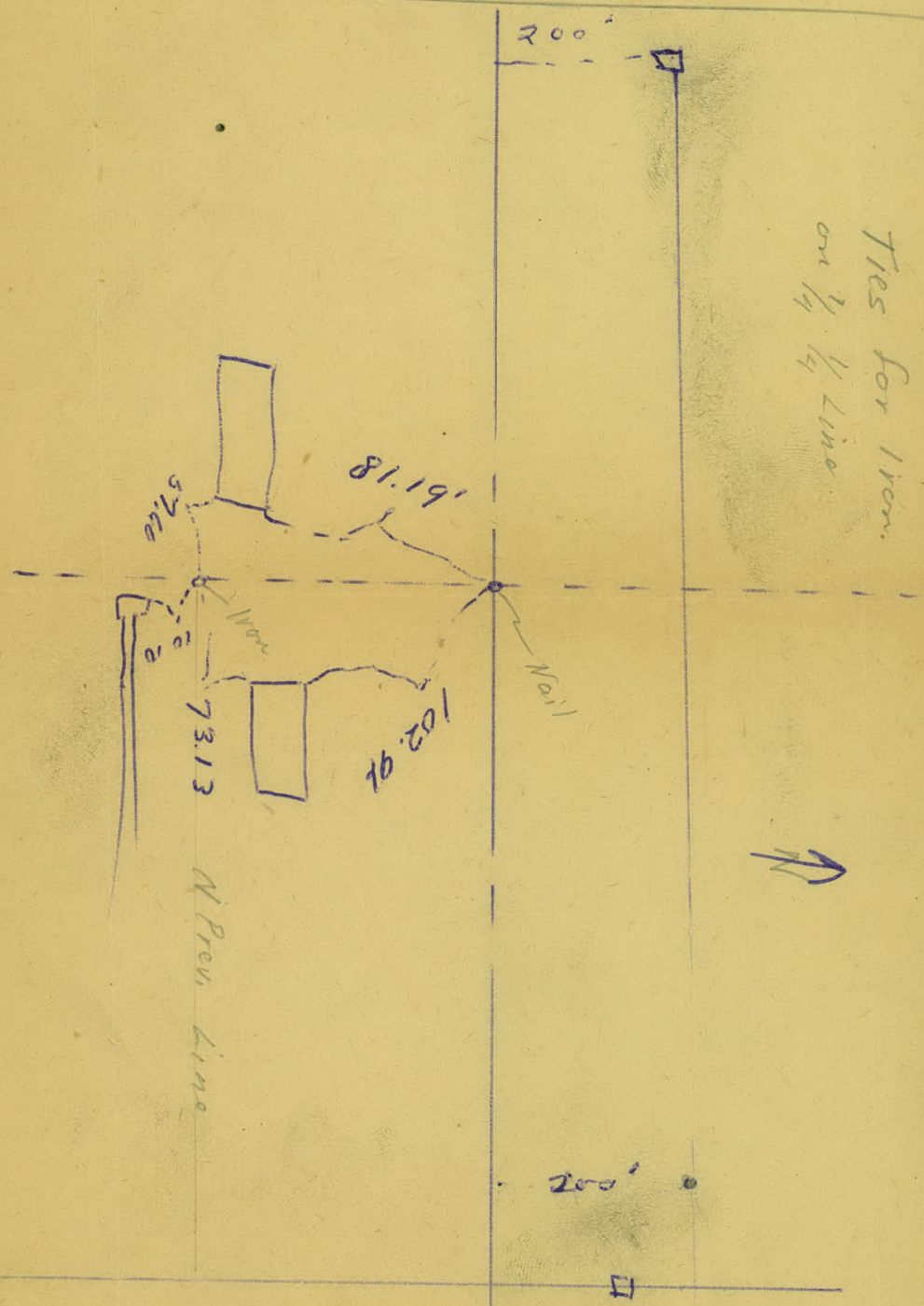
Rec
11/7/47
Dorge 1/8/48



Laneau iron on track

4 Nov. 1829

Set iron @ 90° to track

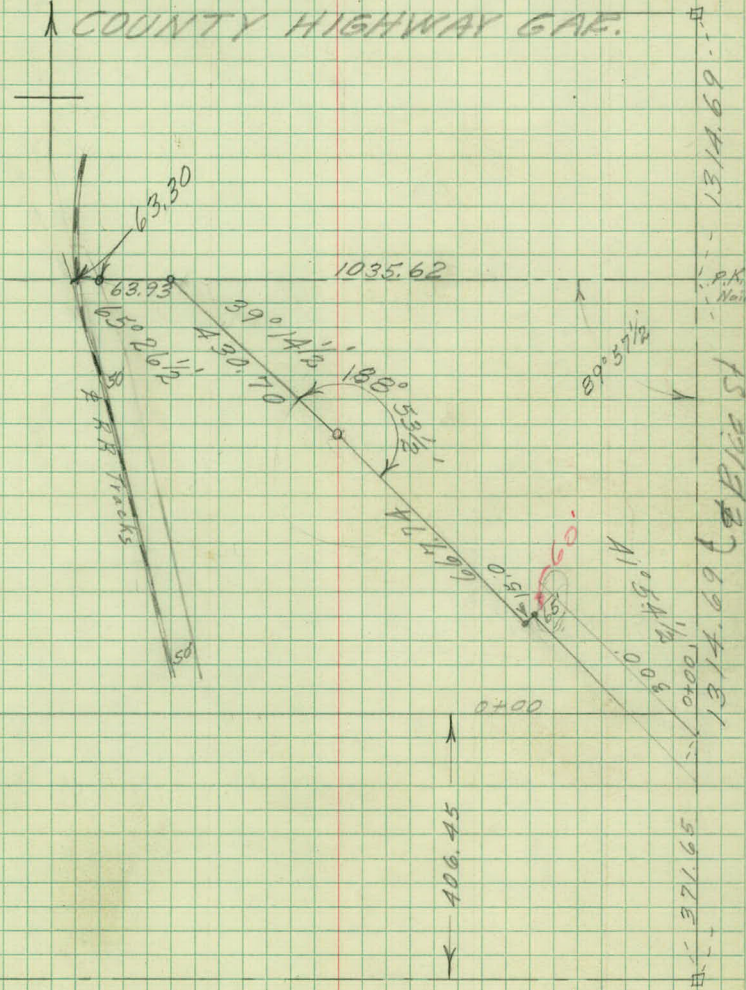


Ties for iron
on 1/4 line

SURVEY OF
 Ramsey Co. Property
 in the SE Cor. of NE 1/4 Sec. 36

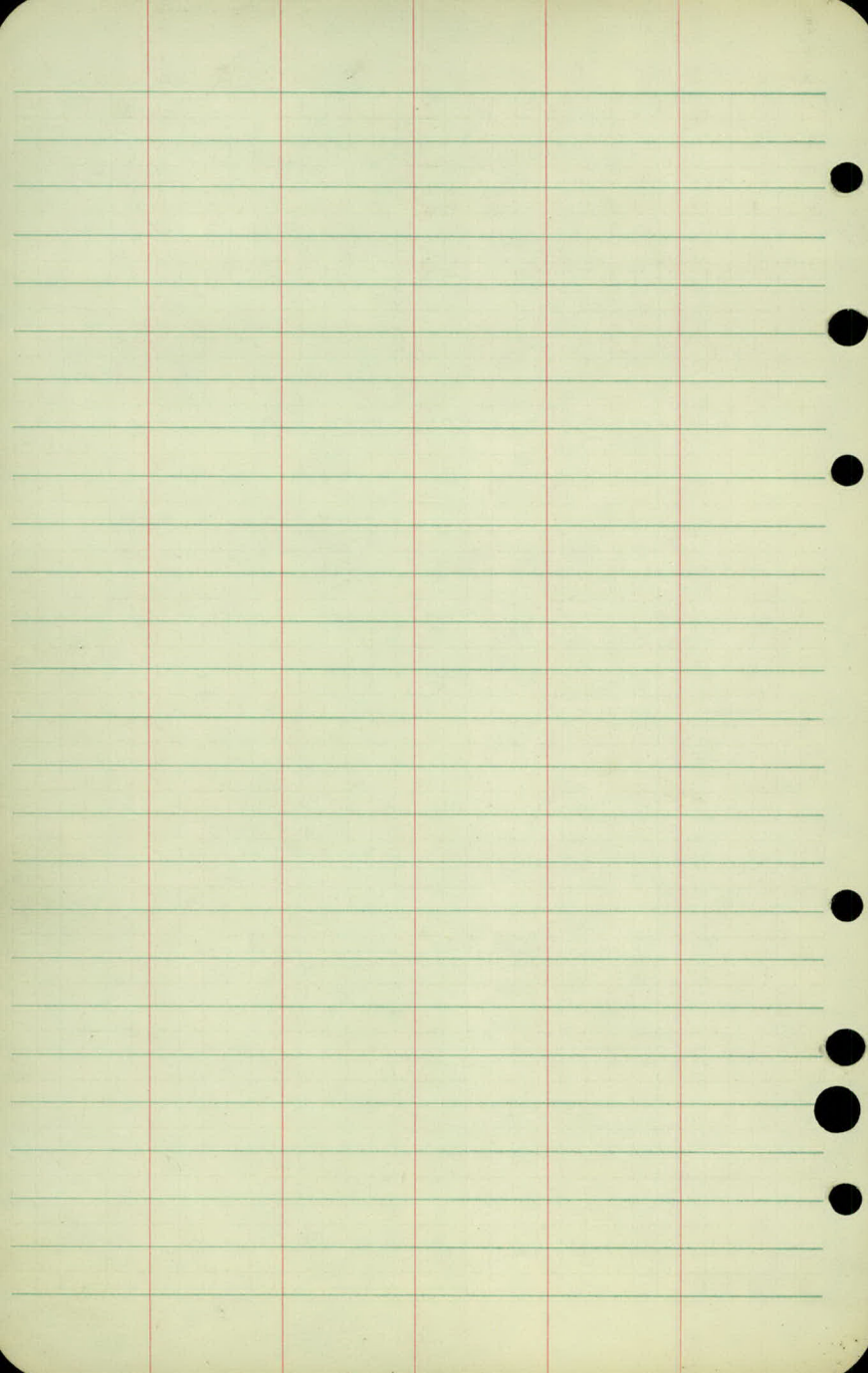
T 30 N R 23 W

COUNTY HIGHWAY GAR.



Platted

E 1/4 Cor Sec 36



FK
RG
XP
JT

March 25, 1956 1957
Clear Bright 35° 2

X-Sections

prop. No. of shop?

Sta	+	π	-	Elev
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BM	6.71	931.11		
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(924.40)

TP	2.93	930.49	3.55	927.56
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0-25 on Blacktop

✓

March 25, 1957 $\frac{1}{2}$

24

3

Top Mont E $\frac{1}{4}$ Cor Sec 36-30-23

25.8	25.9	25.9	26.0	26.0	26.1	26.4	26.4
4.7	4.6	4.6	4.5	4.5	4.4	4.1	4.1
127	100	85	61	40	20	9	

25.7	25.5	25.4	25.3	25.4	25.3
4.8	5.0	5.1	5.2	5.1	5.2
152	177	200	218	230	257

Fe

25.2	25.3	25.4	25.2	25.4	25.3	25.3
5.3	5.2	5.1	5.3	5.1	5.2	5.2
400	383	360	337	317	300	288

25.0	25.0	24.9	24.8	24.8
5.5	5.5	5.6	5.7	5.7
425	447	459	483	500

24.7	24.5	24.7	24.8
5.8	6.0	5.8	5.7
587	566	553	628

528

Sta + π - Elev

930.49

0+00 at Fe Line

✓

✓

✓

✓

TP 2.78 930.49 2.78 927.71

✓

March 25, 1957

25.5 25.7 25.6 26.0 25.9 25.9 25.9 26.5
 50 48 4.9 4.5 4.6 4.6 4.6 4.0
 141 118 100 81 59 33 17

25.3 25.2 25.3 25.4 25.2 25.1
 5.2 5.3 5.2 5.1 5.3 5.4
 167 183 200 229 255 285

Fe Cor

24.5 24.6 24.6 24.6 25.0 25.2 25.0
 6.0 5.9 5.9 5.9 5.5 5.3 5.5
 143 418 400 390 366 332 300

24.5 24.3 24.3 24.3 24.1
 6.0 6.2 6.2 6.2 6.4
 463 489 500 531 554

24.1 23.8 24.4 24.4 24.2 24.3 24.3
 6.4 6.7 6.1 6.1 6.3 6.2 6.2
 677 656 639 623 600 581 563

24.2 24.1 24.1
 6.3 6.4 6.4
 692 700 706
 Fe Cor

Sta + x - Elev

930.49

0+50

✓

✓

✓

1

✓

March 25, 1957

5

25.0	25.1	24.6	24.9	24.5	24.8	25.4
5.5	5.4	5.9	5.6	6.0	5.7	5.1
343	317	300	289	264	247	235

Bldg

24.8	25.1	24.8	25.1	24.7	25.0
5.7	5.4	5.7	5.4	5.8	5.5
367	389	400	414	429	436

24.5	24.5	24.3	24.5	24.9	24.7	24.5
6.0	6.0	6.2	6.0	5.6	5.8	6.0
600	584	574	552	525	500	480

24.3	24.5	24.5	24.4	24.4	24.8	24.8
6.2	6.0	6.0	6.1	6.1	5.7	5.7
619	641	671	687	700	715	728

24.1	24.4	24.5	24.3	24.1	24.5	24.7
6.4	6.1	6.0	6.2	6.4	6.0	5.8
308	300	285	265	246	235	200

24.5	24.4	24.5	24.7	24.6	24.8	25.3
6.0	6.1	6.0	5.8	5.9	5.7	5.2
322	338	359	383	400	418	429

Sta + π - Elev

930.49

1+00

✓

✓

1+50

✓

✓

March 25, 1951

6

✓

✓

24.8	25.3	24.8	24.7	24.9	24.8	25.2
57	52	57	5.8	5.6	5.7	5.3
545	524	500	487	466	443	436

✓

24.7	24.9	24.8	24.6	24.7	24.9
5.8	5.6	5.7	5.9	5.8	5.6
569	589	600	625	648	667

✓

24.8	24.7	24.5	24.9	24.5	24.6
5.7	5.8	6.0	5.6	6.0	5.9
752	738	722	713	700	686

✓

24.6	24.5	24.3	24.2	24.6	24.5	24.9
5.9	6.0	6.2	6.3	5.9	6.0	5.6
320	300	285	262	239	235	200

R/W

✓

24.5	24.3	24.8	24.4	25.1	25.0
6.0	6.2	5.7	6.1	5.4	5.5
348	365	379	385	394	400

✓

25.1	25.2	25.2	24.8	25.2	25.0	25.2
5.4	5.3	5.3	5.7	5.3	5.5	5.3
500	477	453	440	435	423	410

✓

Sta + π - Elev.

939.49

1450

✓

✓

2

✓

✓

March 25, 1957

7

25.0

24.8

25.0

25.1

25.4

25.2

24.9

5.5

5.7

5.5

5.4

5.1

5.3

5.6

594

569

556

545

535

523

509

24.8

24.7

24.6

24.7

24.7

24.8

5.7

5.8

5.9

5.8

5.8

5.7

600

618

639

654

674

692

24.6

25.0

24.7

24.7

24.8

5.9

5.5

5.8

5.8

5.7

775

762

742

720

700

25.2

25.1

25.1

25.2

24.8

24.7

24.6

24.4

5.3

5.4

5.4

5.3

5.7

5.8

5.9

6.1

435

420

400

398

387

362

336

313

RW

24.5

25.0

25.3

25.5

25.5

25.5

25.0

6.0

5.5

5.2

5.0

5.0

5.0

5.5

452

475

495

500

521

537

552

24.8

24.6

24.6

24.7

24.7

24.8

24.7

5.7

5.9

5.9

5.8

5.8

5.7

5.8

700

573

655

641

620

600

589

Sta + π - Elev

930.49

2

+50

✓

✓

✓

BM, 4.13 930.14 4.48 926.01 926.04

3

March 25, 1957

8

24.7 24.6 24.7 24.9 24.7 24.7
 5.8 5.9 5.8 5.6 5.8 5.8
 798 785 771 750 734 720

✓

25.3 25.1 25.4 24.9 25.0 24.9 24.9 24.5
 5.2 5.4 5.1 5.6 5.5 5.6 5.6 6.0
 471 453 436 427 415 400 381 359
 RW

✓

25.3 25.3 25.3 25.6 25.2 24.9
 5.2 5.2 5.2 4.9 5.3 5.6
 485 500 510 525 541 562

✓

25.2 25.1 24.8 24.9 24.8 24.9 24.9
 5.3 5.4 5.7 5.6 5.7 5.6 5.6
 700 683 662 640 615 600 586

✓

25.3 25.0 24.9 24.6 24.5 25.0
 5.2 5.5 5.6 5.9 6.0 5.5
 721 744 771 800 806 820
 Nail in PP 820' Lt Sta 2+50

✓

25.3 25.4 25.5 25.7 25.6 25.4
 4.8 4.7 4.6 4.4 4.5 4.7
 500 485 464 436 416 399
 RW

✓

↓

Sta

+

π

-

Elev

930.14

3

✓

✓

+40

✓

✓

PG
KP
JT

Mar 26, 1957
Clear 30°AM
45°PM

9

Lt

25.5	25.2	24.9	24.9	24.9	25.0	25.1
4.6	4.9	5.2	5.2	5.2	5.1	5.0
522	545	565	584	600	615	636

24.8	25.0	25.1	25.1	25.3	25.3	25.2
5.3	5.1	5.0	5.0	4.8	4.8	4.9
789	771	747	722	700	676	653

24.5	24.3	24.3	24.2
5.6	5.8	5.8	5.9
800	816	830	844

25.2	25.3	25.3	25.2	25.4	25.4	25.8
4.9	4.8	4.8	4.9	4.7	4.7	4.3
543	520	500	488	474	452	436
						RW

24.8	24.8	24.8	24.9	24.9	25.0
5.3	5.3	5.3	5.2	5.2	5.1
562	584	600	624	642	662

24.8	24.9	25.1	25.2	25.1	25.1	25.1
5.3	5.2	5.0	4.9	5.0	5.0	5.0
800	793	780	753	727	700	685

Sta

+

π

-

Elev

930.14

+40

4

✓

✓

✓

+50

LT.

24.5	24.4	24.4	24.2	
5.6	5.7	5.7	5.9	✓
822	838	848	861	

24.8	25.1	25.4	25.1	25.2	25.7	25.8	✓
5.3	5.0	4.7	5.0	4.9	4.4	4.3	
572	552	527	500	492	461	436	

RW

24.7	24.5	24.6	24.5	24.5	24.5	24.7	✓
5.4	5.6	5.5	5.6	5.6	5.6	5.4	
587	600	622	638	658	678	693	

24.7	25.2	25.4	25.4	25.4	25.2	24.7	✓
5.4	4.9	4.7	4.7	4.7	4.9	5.4	
857	817	800	774	752	724	700	

Sand pile

24.8	24.3	✓
5.3	5.8	
878	890	

25.0	25.4	25.4	25.2	25.5	25.7	25.9	✓
5.1	4.7	4.7	4.9	4.6	4.4	4.2	
561	535	522	500	487	466	436	

RW

Sta	+	π	-	Elev
-----	---	-------	---	------

		930.14		
--	--	--------	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

TP	3.13	930.52	2.75	927.39
----	------	--------	------	--------

5				
---	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

11

24.9	24.6	24.6	24.5	24.6	24.7
5.2	5.5	5.5	5.6	5.5	5.4
583	600	625	645	667	685

25.4	25.4	25.1	25.0
4.7	4.7	5.0	5.1
753	739	720	700

Sand Pile

Metal guard post for iron 703' LT. Sta 6+37

25.1	25.0	25.3	25.5	25.3	25.9	26.4
5.4	5.5	5.2	5.0	5.2	4.6	4.1
600	578	548	523	500	469	436

25.0	24.9	24.7	24.6	24.6
5.5	5.6	5.8	5.9	5.9
580	623	654	678	700

RW Sand Pile

24.8	25.4	25.7	25.8	25.9	25.9
5.7	5.1	4.8	4.7	4.6	4.6
500	495	482	464	457	436

24.2	25.5	25.3	25.1	25.2	25.4
6.3	5.0	5.2	5.4	5.3	5.1
505	519	540	559	580	600

Sta	+	$\bar{x}$	-	Elev
-----	---	-----------	---	------

		930.52		
--	--	--------	--	--

+50				
-----	--	--	--	--

6				
---	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

+37				
-----	--	--	--	--

L.T.

24.6

24.9

25.3

25.4

12

5.9

5.6

5.2

5.1

700

674

650

622

Sand Pile

RW

25.5

25.5

25.9

25.6

25.5

25.9

25.8

5.0

5.0

4.6

4.9

5.0

4.6

4.7

582

554

528

500

486

466

436

25.3

25.5

25.3

25.1

24.8

24.8

5.2

5.0

5.2

5.4

5.7

5.7

600

628

650

672

689

700

RW

24.8

24.3

23.8

24.1

23.8

24.5

5.7

6.2

6.7

6.4

6.7

6.0

854

823

800

782

756

724

25.0

24.8

24.6

24.9

25.3

5.5

5.7

5.9

5.6

5.2

900

926

953

968

980

25.8

26.2

25.6

25.8

26.0

25.8

25.6

4.7

4.3

4.9

4.7

4.5

4.7

4.9

556

525

511

500

488

466

436

Sta + π - Elev

930.52

+ 37

✓

✓

+ 50

✓

✓

Lt

£

13

25.6	25.5	25.4	25.2	25.1	25.2
4.9	5.0	5.1	5.3	5.4	5.3
581	600	636	657	678	700
					RW

24.3	24.1	24.2	24.4	24.2	25.0
6.2	6.4	6.3	6.1	6.3	5.5
826	800	792	772	744	717

24.3	24.9	24.5	24.8	24.5	24.7	24.8
6.2	5.6	6.0	5.7	6.0	5.8	5.7
860	880	900	929	956	982	992

25.7	26.4	25.8	25.7	25.9	25.9	25.5
4.8	4.1	4.7	4.8	4.6	4.6	5.0
554	523	570	500	484	458	436

25.6	25.5	25.3	25.2	25.0	25.2
4.9	5.0	5.2	5.3	5.5	5.3
584	600	624	648	668	686

24.2	24.2	23.9	23.9	24.6	24.9	24.9
6.3	6.3	6.5	6.5	5.9	5.6	5.6
800	786	763	739	726	718	700
					RW	

Sta + π - Elev

930.52

+50

✓

7

✓

✓

✓

LT

E

14

2A.3

2A.3

2A.6

2A.5

2A.6

2A.7

6.2

6.2

5.9

6.0

5.9

5.8

834

861

888

900

922

940

2A.9

2A.9

2A.8

2A.6

5.6

5.6

5.7

5.9

1001

991

980

962

25.4

26.0

25.7

25.5

25.7

25.5

5.1

4.5

4.8

5.0

4.8

5.0

545

528

500

4.89

456

436

25.5

25.5

25.5

25.1

24.8

24.7

5.0

5.0

5.0

5.4

5.7

5.8

583

600

623

652

680

700

23.6

23.7

23.5

23.6

23.8

24.1

6.9

6.8

7.0

6.9

6.7

6.4

812

800

779

768

750

731

RW

24.4

24.5

24.1

24.0

24.2

6.1

6.0

6.4

6.5

6.3

830

850

873

900

921

Sta + π - Elev

930.52

7

+50

✓

✓

✓

✓

LT

E

15

25.3	25.1	25.1	25.4	24.9
5.2	5.4	5.4	5.1	5.6
1025	1014	1000	983	951

25.7	26.1	25.7	25.8	26.1	26.0	25.8
4.8	4.4	4.8	4.7	4.4	4.5	4.7
561	528	500	486	472	458	436

25.5	25.5	25.3	25.3	25.1	24.8
5.0	5.0	5.2	5.2	5.4	5.7
588	600	631	652	678	692

23.4	24.5	24.4	24.4	24.5	24.6
7.1	6.0	6.1	6.1	6.0	5.9
780	776	754	738	722	700

22.9	22.9	23.5	24.0	24.4	24.4
7.6	7.6	7.0	6.5	6.1	6.1
800	818	844	864	885	900

25.6	25.3	25.4	24.9	24.2	24.3
4.9	5.2	5.1	5.6	6.3	6.2
1030	1000	993	973	940	915

sta + π - Elev

930.52

+50

A

TP 3.27 930.66 3.13 927.39

8

✓

+50

✓

9

LT

E

16

25.0
4.7
1035

25.7
4.8
1050

Guard post for iron 703' Lt. Sta 6+37

25.0
5.7
1000

25.1
5.6
995

24.3
6.4
971

23.7
7.0
947

23.6
7.1
930

23.9
6.8
901
RW

25.5
5.2
1014

26.0
4.7
1037

25.8
4.9
1059

25.4
5.3
1074

26.3
4.4
1059

26.2
4.5
1040

25.9
4.8
1021

25.4
5.3
1000

25.0
5.7
990

24.6
6.1
965
RW

25.4
5.3
1083

24.2
6.5
1094

26.3
6.4
1092

25.4
5.3
1080

26.2
4.5
1066

26.5
4.2
1052

26.5
4.2
1027
RW

Sta + π - Elev.

930.66

9

+09

BM₂ 3.07 929.91 3.82 926.84

4+50

5+00

Lt
 23.4
 7.3
 1100
 21.2
 9.5
 1118

✓

23.1
 7.6
 1100
 24.5
 6.2
 1085
 25.8
 4.9
 1072
 26.5
 4.2
 1056
 26.7
 4.0
 1036

✓

20.4
 10.3
 1121

spike in P.P. 926' LT Sta 4+82

24.7
 5.2
 911

24.8
 5.1
 900

25.0
 4.9
 881
 sand pile

✓

25.0
 4.9
 936

25.3
 4.6
 923

25.0
 4.9
 912

25.0
 4.9
 900

25.3
 4.6
 890

✓

Sta + π - Elev

929.91

5+50

TP 2.52 929.36 3.07 926.89

BM, 2.72 928.71 3.37 925.99 (926.04)

TP 5.79 931.25 3.25 925.46

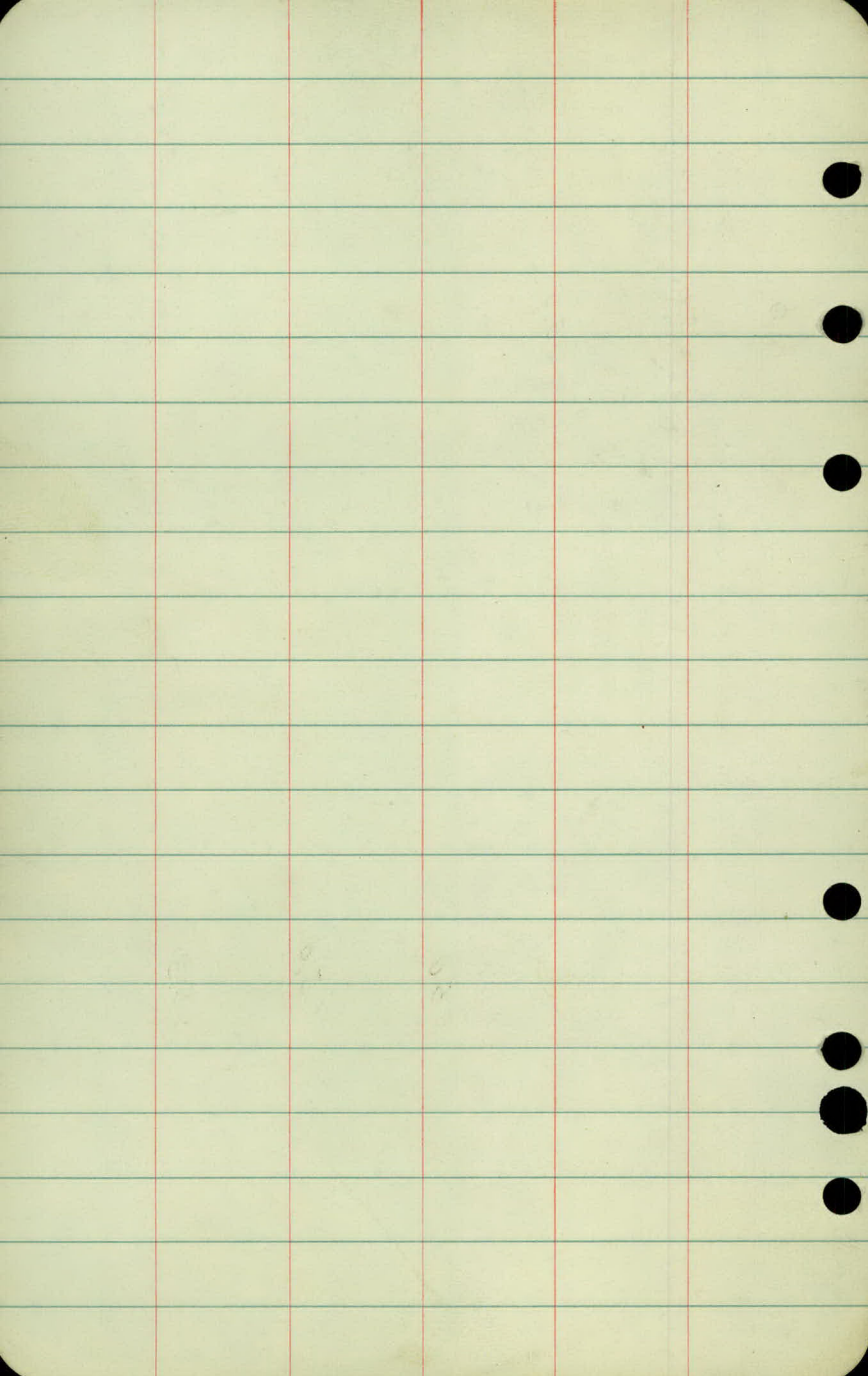
TP 4.19 930.14 5.30 925.95

BM 5.81 924.33 (924.40)

L2					18
25.0	25.2	25.3	25.1	25.5	
4.9	4.7	4.6	4.8	4.4 ✓	
931	914	900	884	868	
25.0	25.0				
4.9	4.9 ✓				
950	962				

Spike in P.P. 926' LT. Sta 4+82 (BM₂)
 Spike in P.P. 820' Lt. Sta 2+50

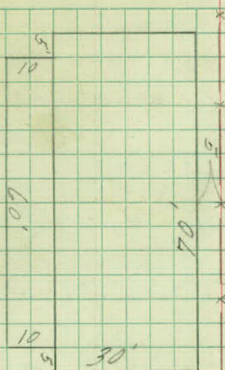
Top Mont E 1/4 Cw Sec 36-30-23



FK
KT
JT

May 8, 1957
Partly cloudy 75°

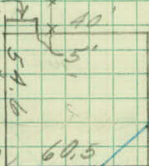
19



58.6

34.2

6' Conc Walk.

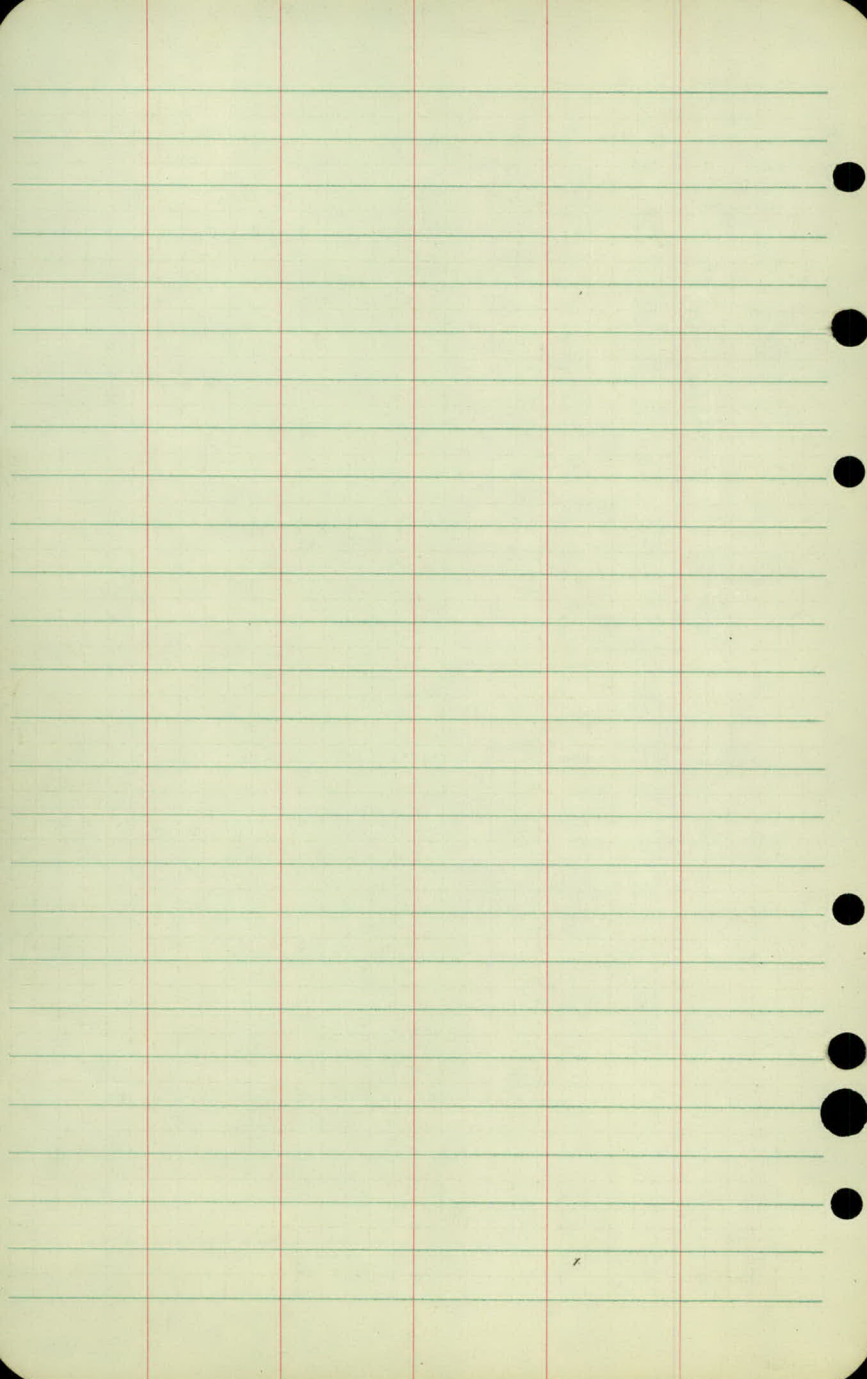


23.5'

18'

Rice St

191
340
2361



May 8, 1931

20

Bldg Elev

Sta	+	π	-	Elev
BM	3.11	929.15		926.04
Co Shed Floor	1.22			24.93
N.W. Cor. Co. Shed	5.3			23.85
S.W. Cor. Co. Shed	4.8			24.35
S.W. Cor. Apron of shed	4.75			24.40
S.E. Cor. shed Apron	4.66			24.49
N.E. Cor. shed Apron	4.27			24.88
N.W. Cor. shed Apron	4.33			24.82
S.E. Cor. Co. Shed	4.4			24.75
N.E. Cor. Co. shed	5.1			24.05
T.P.	5.54	931.14	3.55	925.60
Soccco Bldg Floor	5.26			<u>25.88</u>
"	"	S.W. Cor.	5.8	25.34
"	"	S.E. Cor	5.5	25.64
"	"	N.E. Cor	5.8	25.34
"	"	N.W. Cor	6.3	24.84
"	"	S.W. Cor 6' Walk	5.40	25.74
BM			6.68	924.46 924.40

May 8, 1957

21

Nail in PP 820' Lt Sta 2+50

47.05

47.15

47.25

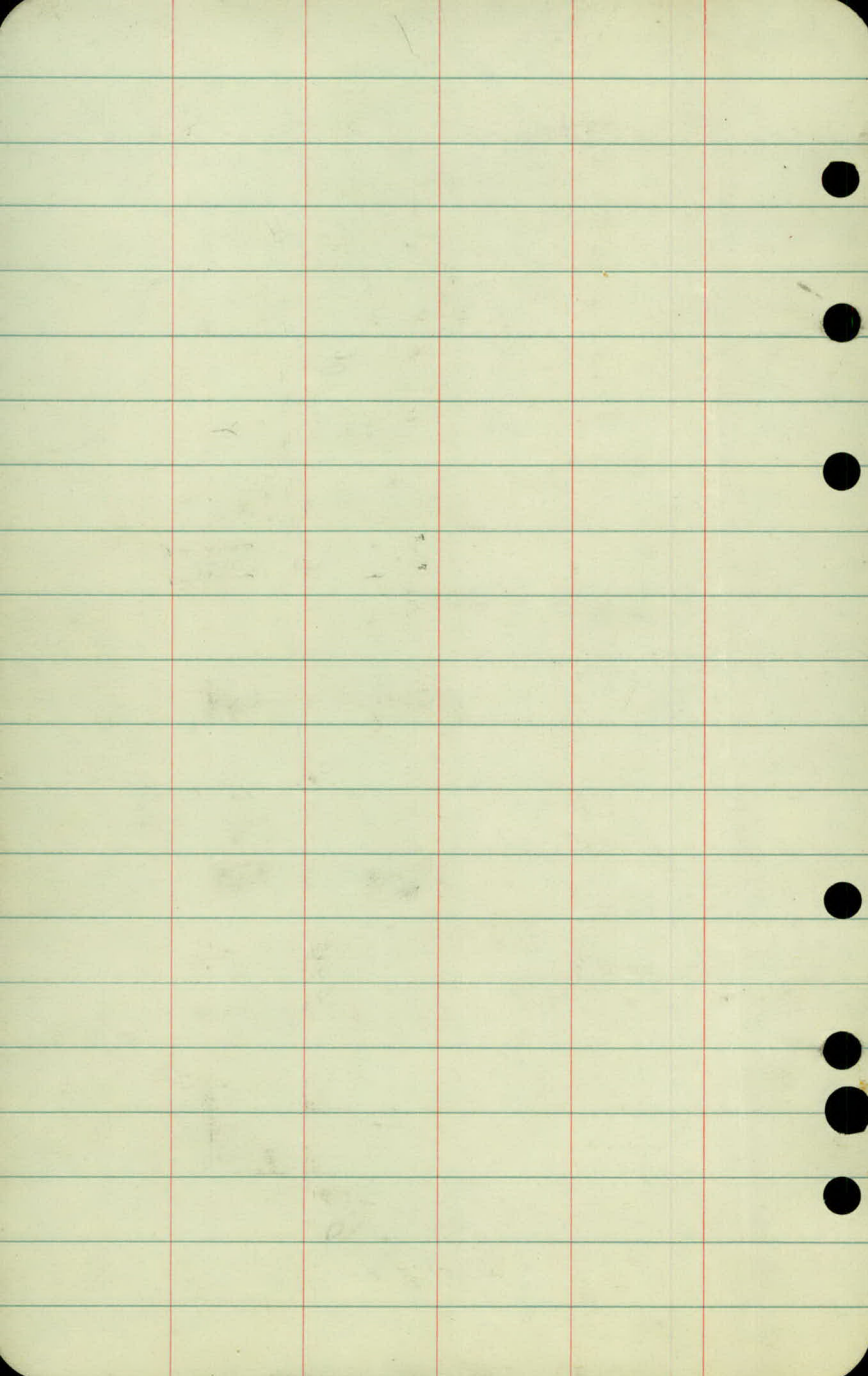
47.35

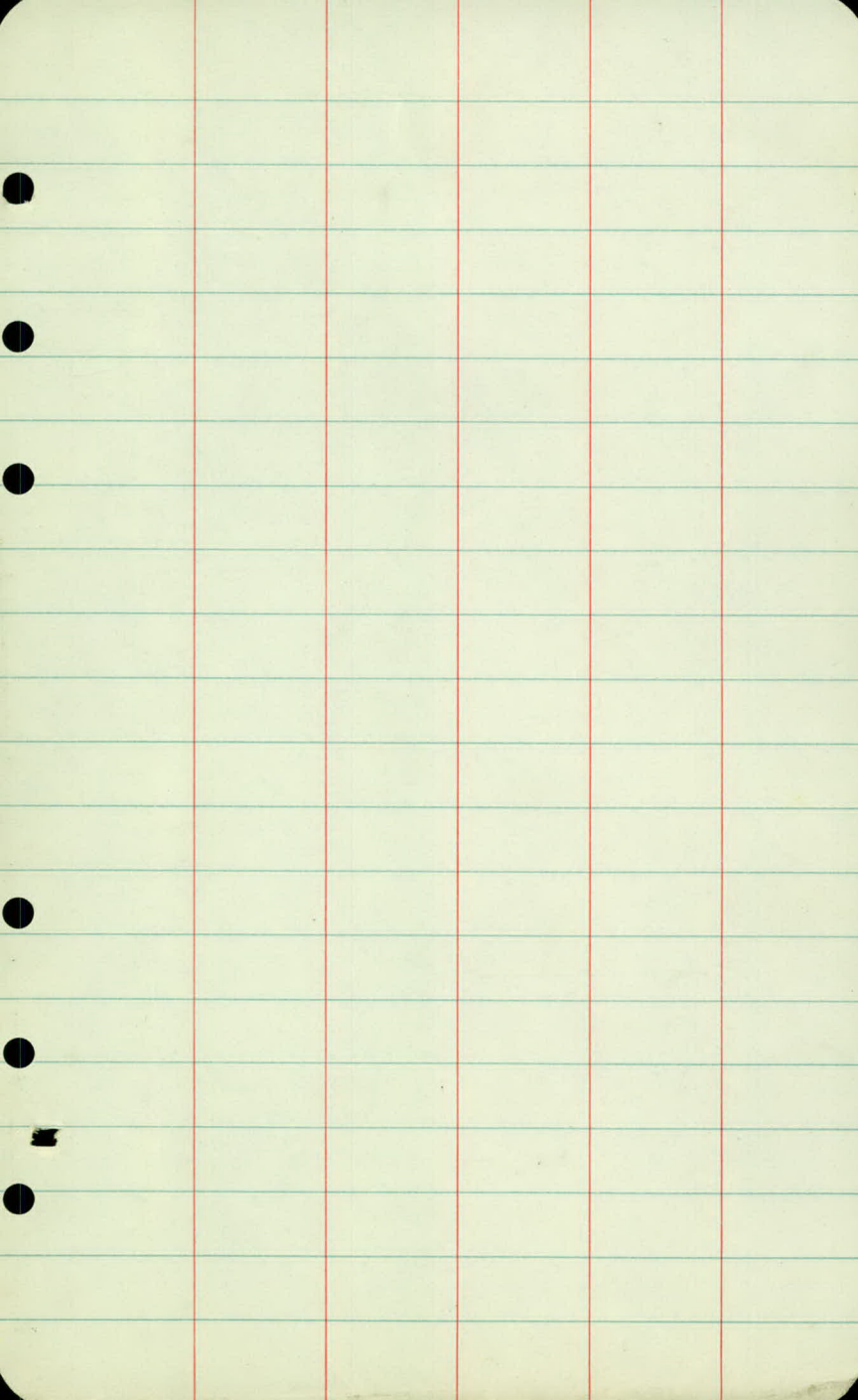
47.45

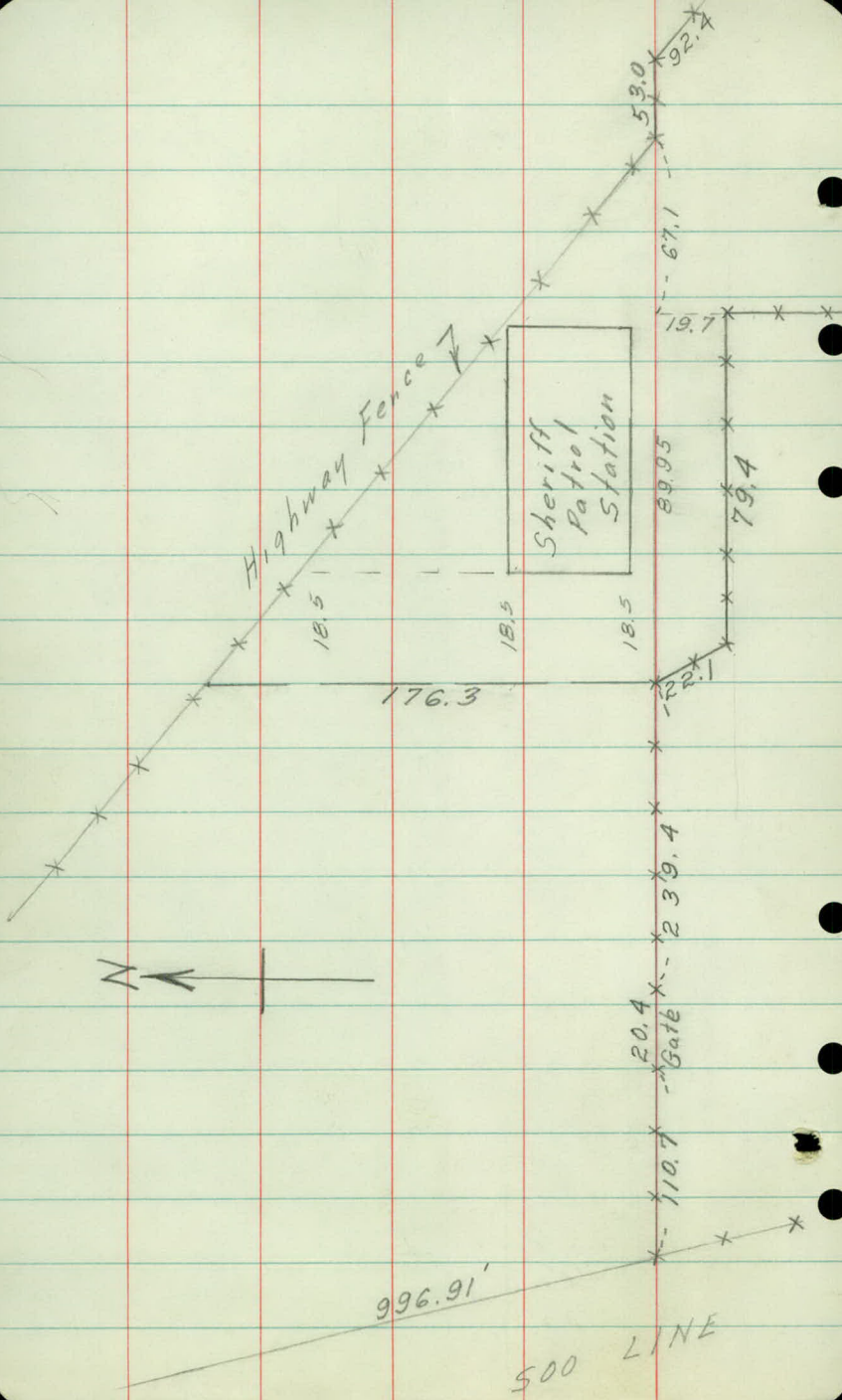
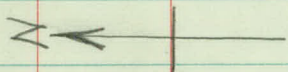
47.55

Top Mont E $\frac{1}{4}$ Cor Sec 36-30-23

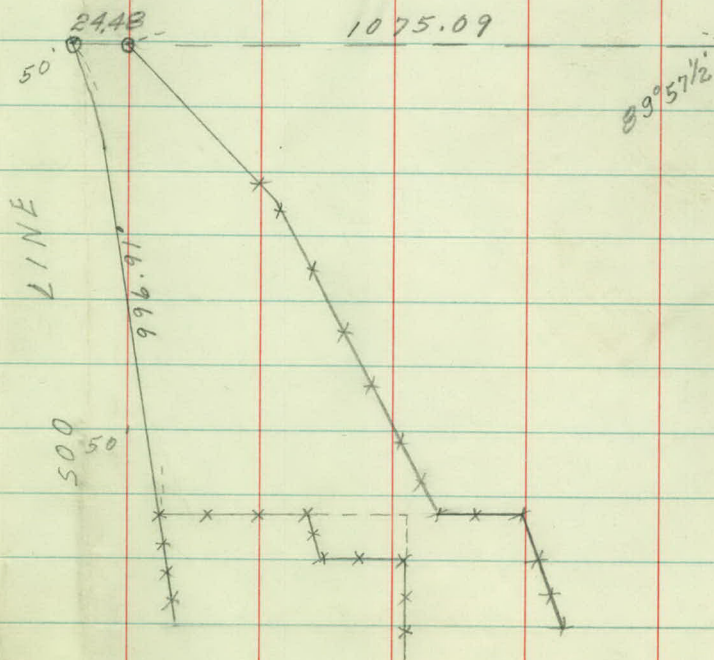
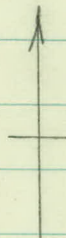
Sta	+	π	-	Elev
BM	7.74	932.14		924.40
A MH	F.L.		11.6	20.54
A S.D.	Top		8.29	23.85
B MH	F.L.		13.7	18.44
B S.D.	Top		8.46	23.68
C S.D.	Top		6.63	25.51
C MH	F.L.		12.7	19.44
D Open End	F.L. 15" CM		11.13	21.01
BM			7.74	924.40 924.40



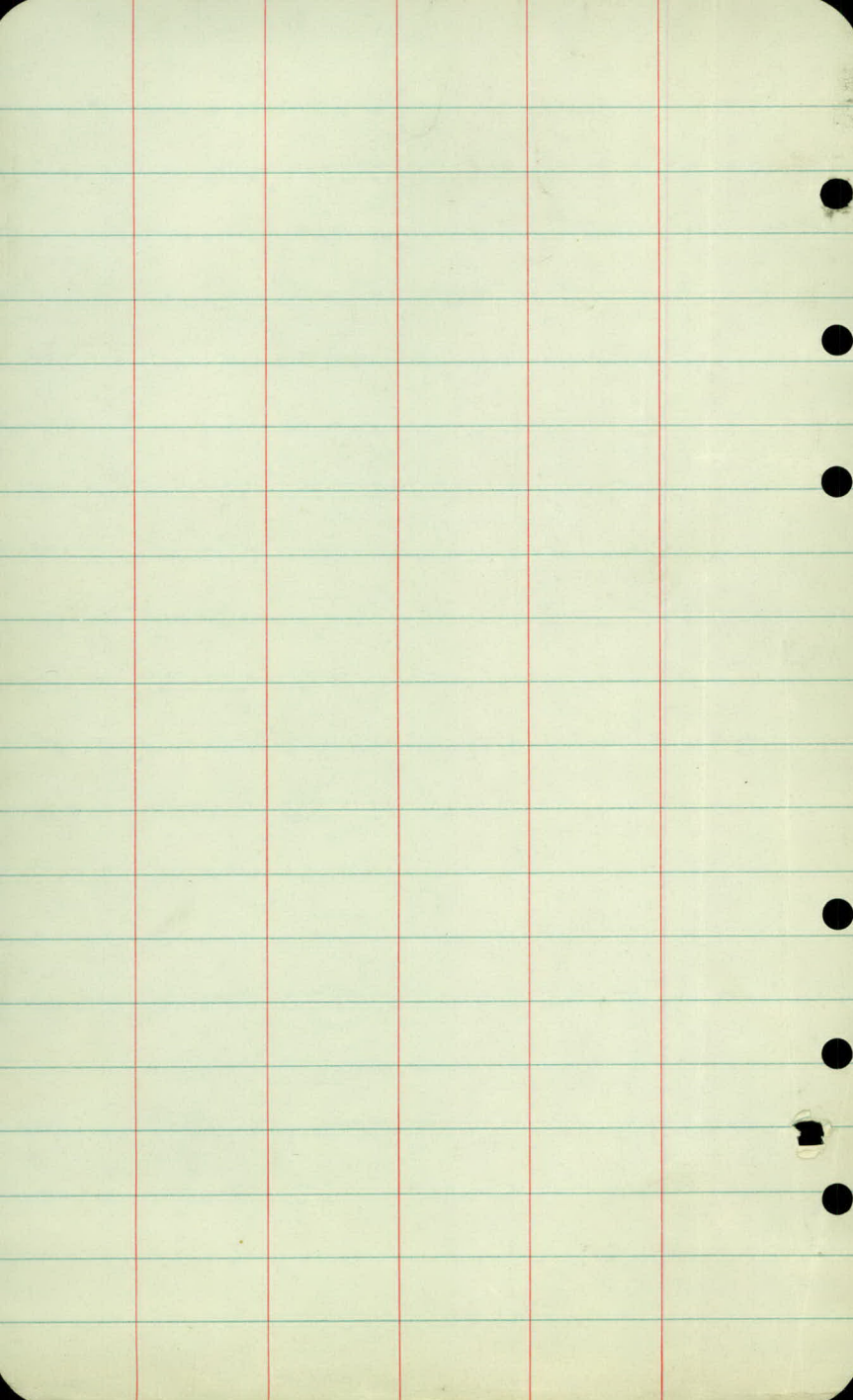




N.E. Cor. Sec. 36



E. $\frac{1}{4}$ Cor. Sec. 36

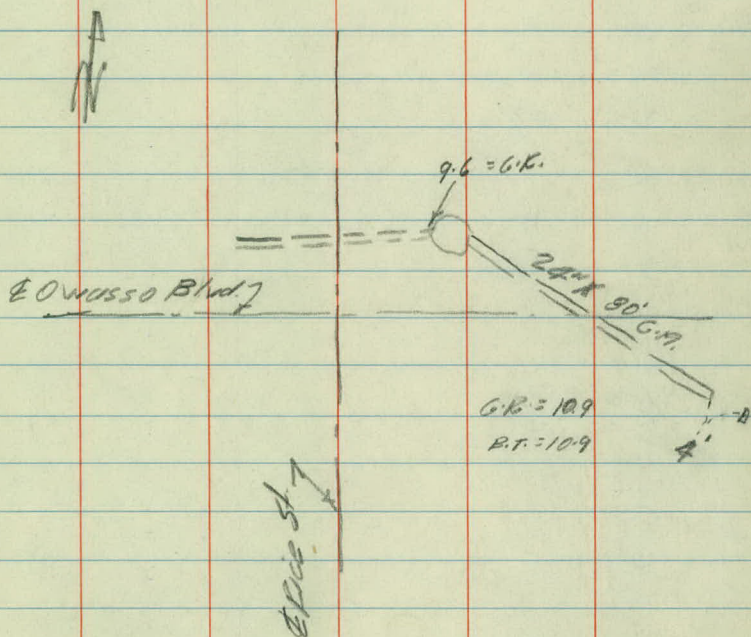


Staking Notes

County Highway Garage

Ditch along R.R. Tracks
also

Sewer along Owosso Blvd. No.



Sta G.P.

0 +00 7.7

6.2 =

+50 7.9

1 8.0

+50 8.1

2 8.3

+50 8.4

3 8.6

+50 8.7

10-11-50

Lt.

Q

Rt.

10.05.

Rt.

Low point in shop yard =

C3.8

3.4

C.21

3.3

C2.8

4.7

C27

4.9

C.3.6

4.2

C.3.8

4.1

C4.2

3.9

C.3.5

4.7

Sta.

G.P.

4

8.9

+50

9.0

+75

9.1

B.M.

1.21

Lt.

Q

Rt.

10.05.
B.T.

C.4.8
36.

C.4.7
3.8

C.4.1
4.5

Top of N.E. Bolt. at Base of R.R. Signal

Sewer staking

STA G.R.

F.L. 24 X Drain = 12.33

0+00 12.10

+ 25 11.95

+ 50 11.80

+ 75 11.65

1 11.50

+ 25 11.35

+ 50 11.20

+ 75 11.05

2 10.90

+ 25 10.75

+ 50 10.60

+ 75 10.45

4

2

K or N.

10' ⑤

B.T.

C.5.7

6.25

C.7.0

4.80

C.7.5

4.15

C.8.0

3.50

C.7.8

3.55

C.7.6

3.6

C.7.5

3.55

C.7.2

3.7

C.6.7

4.05

C.5.6

5.0

C.5.6

4.85

G.R.

3

10.30

+25

10.15

+50

10.0

+75

9.85

4

+100

9.70

+25

9.55

+50

9.40

R.R. ditch

5.04 on stake
+4.1 cut
9.14

5.04
+4.1
9.14

12.1

10' (5)

B.7

C.54

4.9

C.5.8

5.15

C.4.8

5.2

C.4.7

5.15

C.64

3.3

C.63

3.25

C.2.0

7.4

