

BK. 39 Dr. 11A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

Kieffer St.

From Owasso Blvd. N. To Harriet Ave.

Road Acc't. No.

Date Filed. 7-25-47

File

PLAN SURVEY

KIEFFER ST.

OWASSO BLVD. N. to Harriet St.

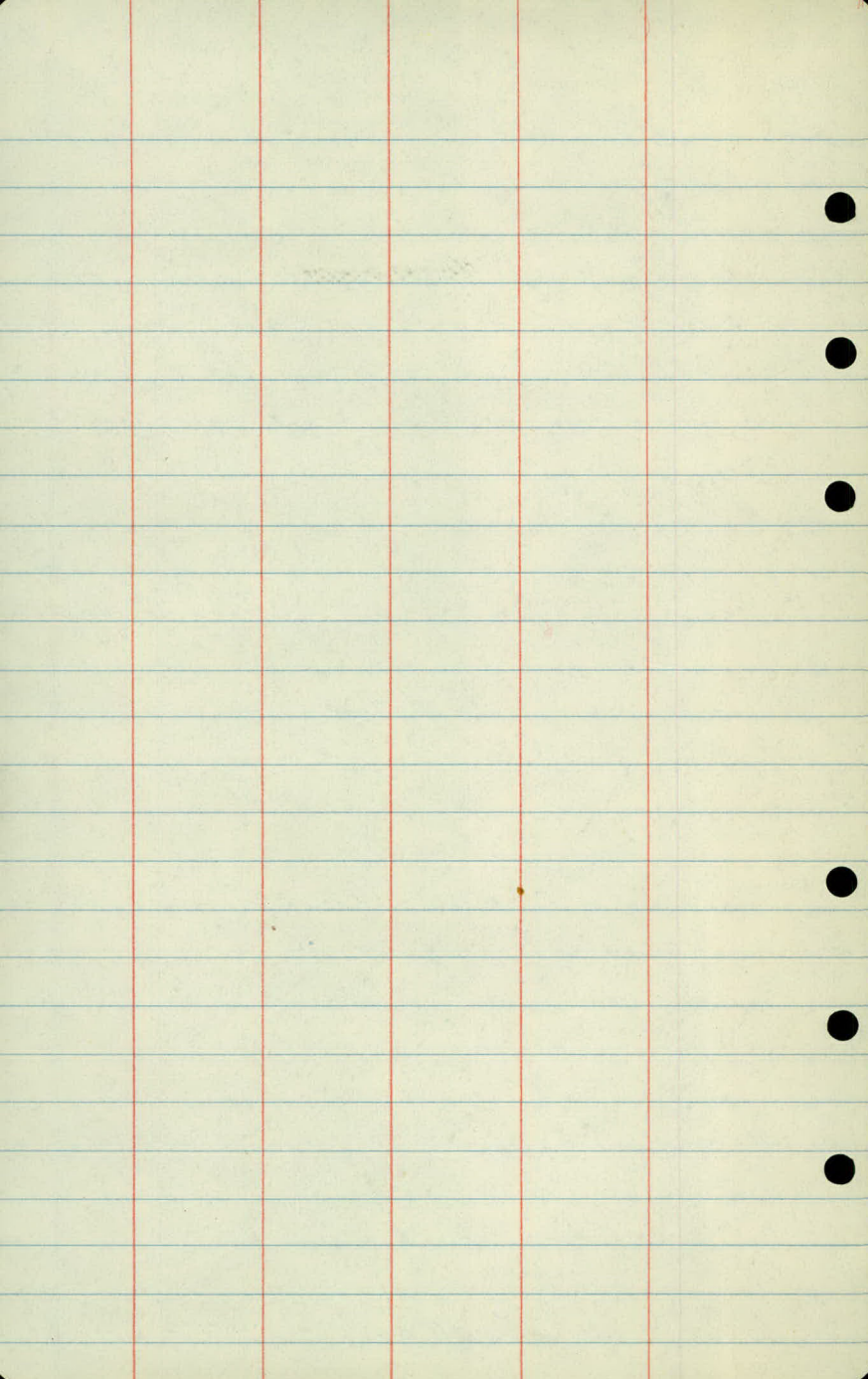
INDEX

Align P. 1-2

Topog. P. 3-5

Xsections P. 6-12

Rec 7/16/47
Drawn up 7/21/47



1

Alignment

Sta.	Point	ΔL	ΔB
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11+38.87	P.O.T. = @ Harriet St.		
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10+27.75	P.O.T.		
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8+83.84	P.O.T.		
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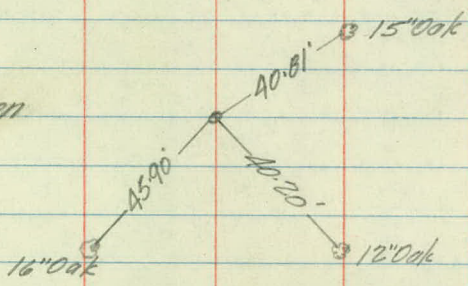
0+00	P.O.T. = @ Owasso Blvd. N.		
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K.A. 7 11-47
 AM
 M.B.
 R.F.
 R.W.

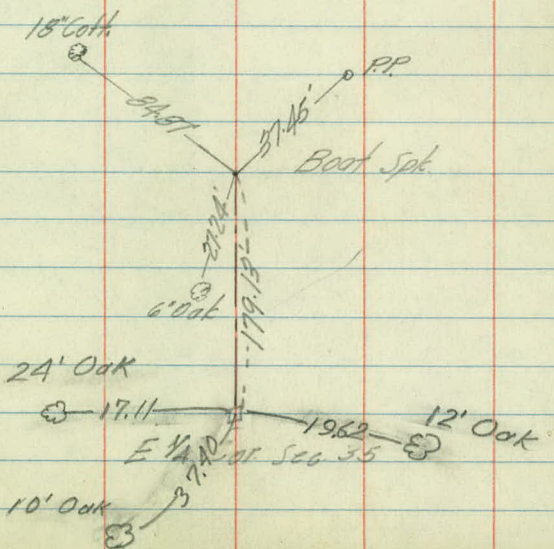
This is a true line.
 checked from
 Mont. to Mont.
 Mar. 1955

2" X 2" Hub R. H. Wolfgram

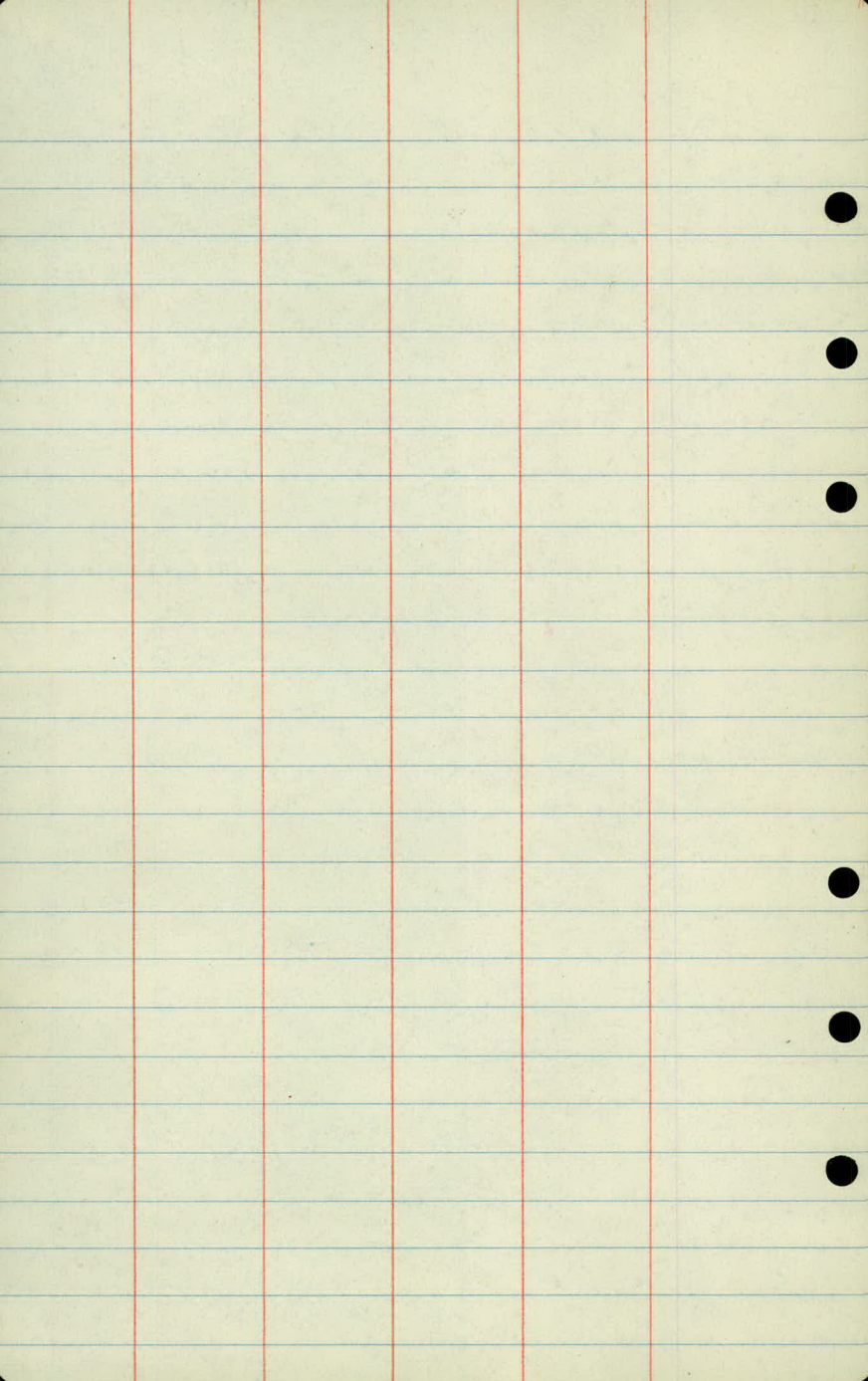
Placed Iron



1 Boot Spk. on Top Stump



E 1/4 Sec 35



Topography

Kieffer

5 FC-4' +94.5°0-00

4 FC-7'
+99.10°0-6'

+73.5°0-2'

+54.4°0-3'
+41.12°0-6'

3 FC-7'

+25.30°0-10'

2 FC-6'

+11.16°Tw. C-13'

+94.12°0-2'

1 FC-4'

+65 FC-3'
+61.15°0-10'
+58.10°0-9'

+60 FC X³ E

+61.16°0-10'

+40.16°0-29'

+39.16°19'

+15.16°35'

+13.5° Edge of Bl. Top

0
-13° Edge Bl. Top

K.A. 1-14-41
AM
M.B.
R.K.
R.W.

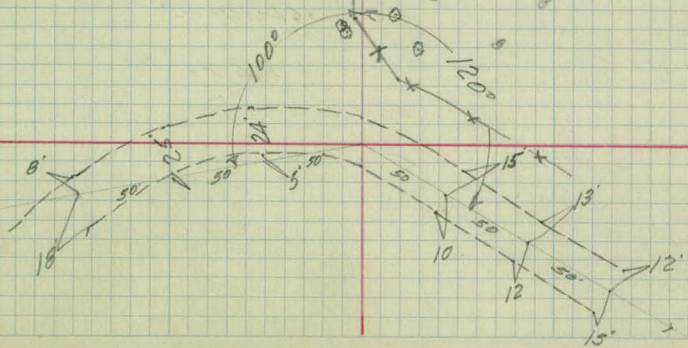
Pothole

10'

4

Dense Woods & Brush

Pasture



11

+83-Edge of Swamp

+66-24'-0"-2'

+27-18'-0"-2'
+14-15'-0"-5'

10

+95-16'-0"-3'

+43-Con. of Fe/hole-53'
20' E & W 35' N & S.

9 @ Ditch-32'

+69-End of Ditch-12'

8

+70-Fe. Cor. 1'

+66-16'-0"-28'
+58-8'-0"-16'
+30-15'-0"-6'

7

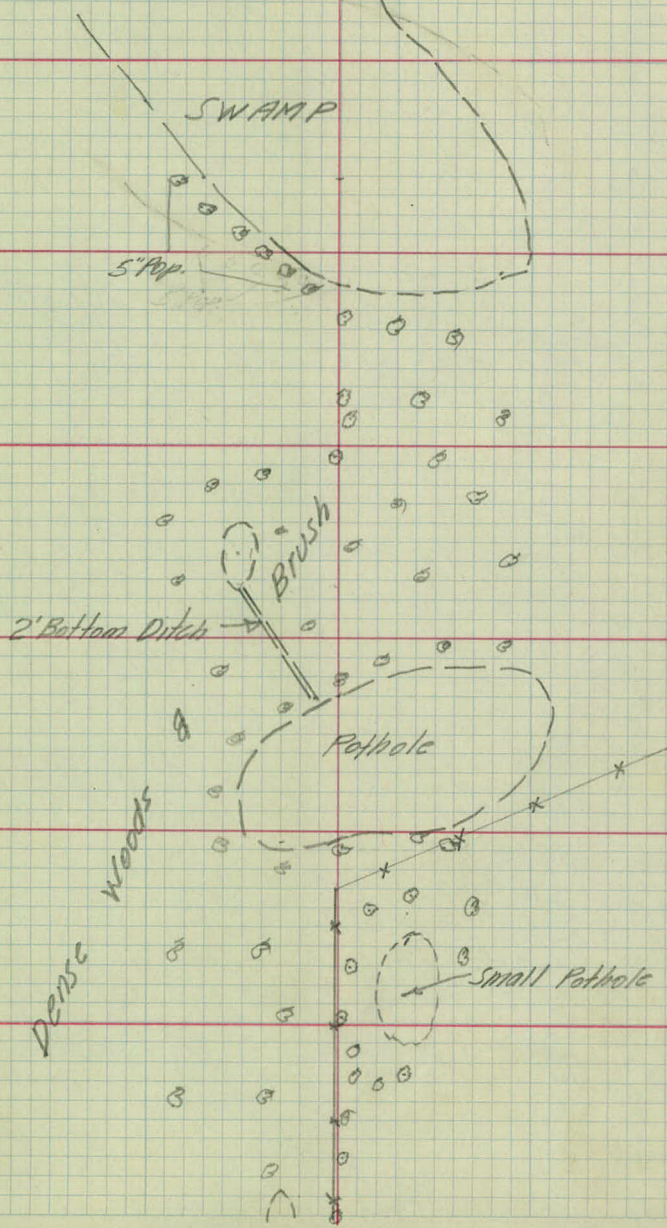
Fe-2'

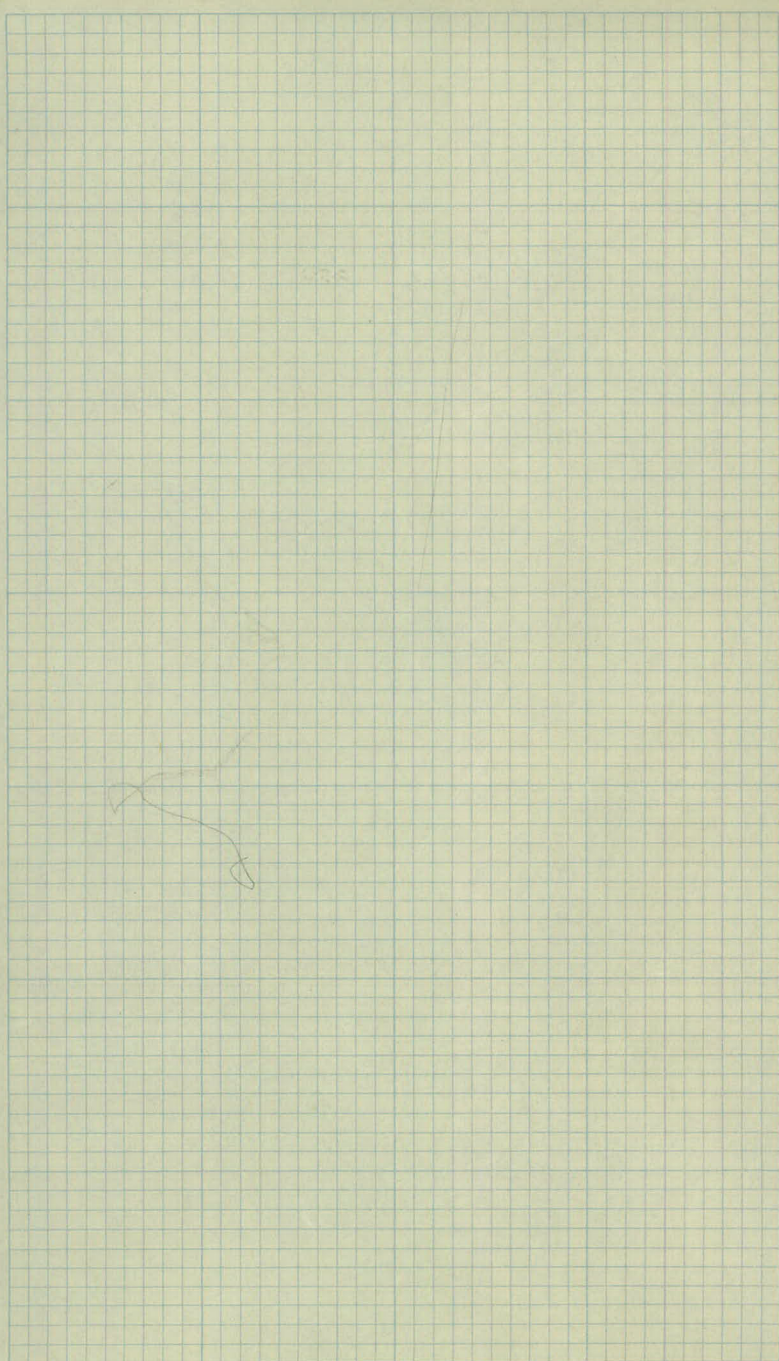
+03-15'-0"-2'

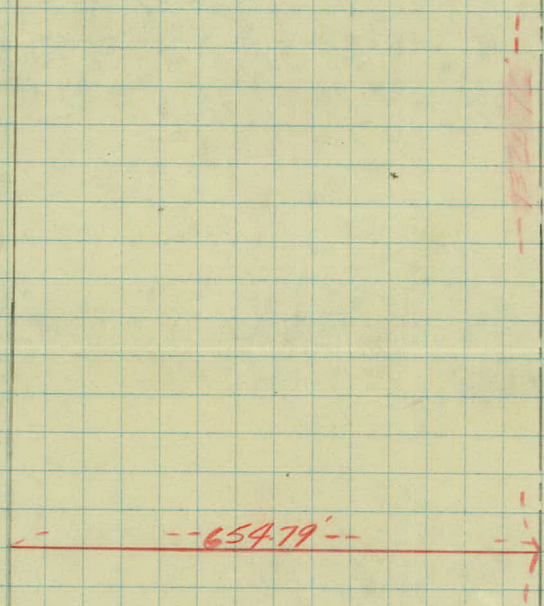
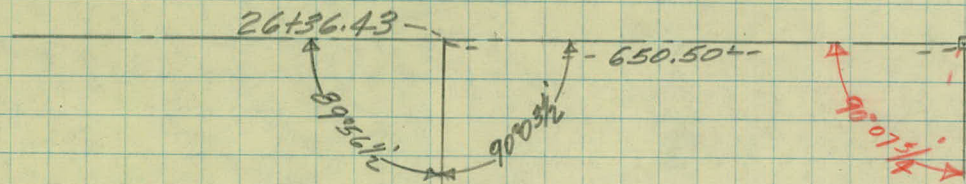
+73-15'-0"-34'

+30-8'-0"-1'

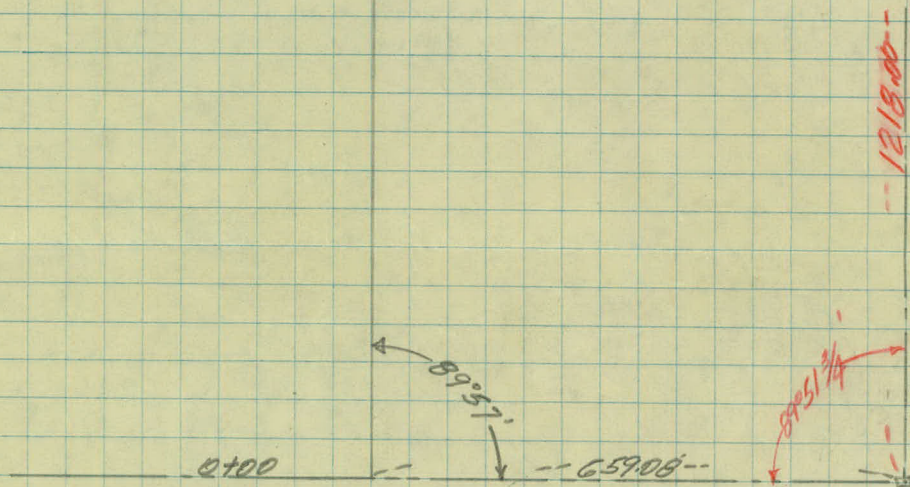
6







POT = 12+00



X Sections

Kieffer

Sta.	+	π	-	Elev.
B.M.	7.41	935.13		927.72
T.P.	1343	948.24	0.32	934.81
T.P.	1304	961.04	0.24	948.00
B.M.			5.70	955.34

0 +00 Profile of Rd. 52.7

+13 53.3

+27 52.9

+37 59.4

+44 59.3

+57 58.7

T.P.	3.84	964.76	0.12	960.92
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+60 60.3

K.A. 7-14-47
A.M.
M.B.
E.K.
E.W.

7

L E F

Spt. in 24" Oak S.W. Cor Arborescent & Owasso

R.R. Spt. in 18" Oak N.W. Cor Kieffer & B.M. N. ^{Owasso}

121 97 83 84 89 108 129 ✓
100 50 28 50 100 150

77 80 86 70 1.9 ✓
19 25 35 50

8.8 8.2 8.1 0.9 2.1 0.9 ✓
50 28 24 31 50

8.8 8.5 1.6 1.3 2.5 1.9 0.4 ✓
50 26 14 30 40 50

8.1 4.7 2.4 1.7 1.9 2.6 1.9 0.2 ✓
50 29 11 16 29 40 50

7.6 5.9 4.1 3.4 2.3 2.2 2.0 2.3 1.8 0.7 ✓
50 40 29 23 6 18 31 40 50

S.S. 13.3 9.2 7.4 4.5 3.8 4.3 5.2 5.6 5.2 ✓
50 29 18 13 24 35 41 50

Sta	+	π	-	Elev
		964.76		
1				61.5.
+35				61.7.
+70				58.7.
2				56.3.
+33				51.6.
T.P.	3.99	955.43	1332	951.44
+51				49.6.
+68				49.7.
+91				48.6.
T.P.	3.48	954.92	3.99	951.44

L

E

R

S.S. 14.1 9.0 5.8 3.3 2.6 2.9 4.2 6.3 6.6 ✓
 50 30 15 10 17 27 40 50

S.S. 16.1 8.6 5.0 3.1 2.8 3.8 7.3 8.6 ✓
 50 27 13 8 18 34 50

S.S. 15.2 13.0 8.0 5.8 4.1 8.3 10.5 11.3 11.0 ✓
 50 43 24 9 14 26 41 50

12.0 7.8 7.2 8.5 9.9 12.9 12.7 11.5 ✓
 50 26 9 7 22 35 50

13.3 11.1 11.8 13.2 13.1 13.6 14.3 ✓
 50 30 13 18 33 50

6.4 5.0 5.4 6.0 5.8 5.0 5.9 6.6 ✓
 50 37 17 5 17 33 50

7.0 7.0 6.4 5.7 6.2 7.5 9.4 ✓
 50 30 16 19 30 50

6.5 7.2 6.4 6.0 6.8 7.8 9.1 9.8 ✓
 50 38 19 12 13 30 50

Sta	+	π	-	Elev
		95492		

3				49.1.
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+23				51.7.
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+43				51.0.
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+71				48.6.
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4				46.3.
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+16				45.6.
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+36				47.5.
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+70				48.8.
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L

Z

E

53 5.2 4.8 4.8 5.8 7.3 7.6 8.4 8.4 9.4 ✓
 50 4.5 2.2 8 14 17 31 41 50

4.9 4.6 3.4 2.6 3.2 3.5 5.4 6.4 7.4 ✓
 50 4.1 2.6 9 4 20 36 50

3.8 2.7 2.2 2.5 3.9 3.9 4.2 5.2 5.9 6.1 ✓
 50 3.4 2.1 9 3 4 14 34 50

5.0 4.4 4.9 5.2 5.8 6.3 6.6 7.4 7.2 6.8 ✓
 50 3.5 1.8 9 3 12 26 44 50

5.6 5.5 6.6 7.4 8.1 8.6 8.9 9.1 8.0 ✓
 50 3.2 1.8 7 2 7 24 50

5.7 5.6 7.2 8.5 9.3 9.5 8.8 7.9 ✓
 50 3.3 1.7 7 18 36 50

5.9 6.2 6.8 7.1 7.4 7.8 7.5 7.4 ✓
 50 2.4 9 4 12 30 50

6.7 6.6 6.1 6.1 5.5 5.0 5.4 ✓
 50 3.7 1.3 17 33 50

Sta	+	π	-	Elev
		95492		
5				47.2
+36				45.2
+65				42.7
T.P.	-0.01	941.37	1354	941.38
6				40.2
		Powered out		
T.P.	6.39	942.16	560	935.77
+38				38.8
+56				37.3
7				36.2
+40				36.1

7-15-97

10

L

E

R

86 184 98 77 56 53 ✓
50 37 7 29 50

159 152 134 128 97 82 63 65 ✓
50 42 27 12 16 33 50

176 141

139 ~~148~~ ~~165~~ 122 108 105 11.2 11.7 ✓
50 26 6 15 26 41 50

43 45 40 22 12 0.5 0.2 0.8 0.1 ✓
50 35 26 8 8 28 43 50

Top Rock 14.5 to 7

27 33 33 34 33 2.1 2.0 ✓
50 28 10 23 40 50

29 28 40 49 50 43 40 38 ✓
50 31 12 12 26 40 50

40 40 ~~41~~ 49 6.0 7.2 7.5 7.1 ✓
50 26 ~~50~~ 13 18 33 50

36 5.2 5.8 6.1 6.9 7.5 7.3 7.3 ✓
50 23 4 12 25 40 50

Sta	+	π	-	Elev.
		94216		

7	172			35.5
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8				34.5
---	--	--	--	------

	+26			33.3
--	-----	--	--	------

	+60			34.8
--	-----	--	--	------

9				39.9
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T.P.	8.27	947.20	3.23	938.93
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	+27			39.5
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	+56			39.2
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	+77			37.6
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L

Q

R

58 61 66 67 69 61 59 6.3 ✓
 50 23 12 6 18 31 50

7.4 76 81 77 72 6.7 6.6 6.7 ✓
 50 34 10 12 23 33 50

58 70 79 90 89 8.4 8.7 ✓
 50 41 30 13 26 50

58 61 69 7.4 8.5 9.2 ✓
 50 ~~5~~ 26 26 50
 43

3.6 38 4.5 25 2.4 23 33 ^{4.0} 7.2 5.8 ✓
 50 38 37 35 31 10 19 29 50

11.4 10.4 8.8 7.7 8.0 8.6 9.2 ✓
 50 34 17 16 27 50

11.7 10.5 9.0 8.0 8.2 8.3 7.0 ✓
 50 31 18 15 28 50

10.7 10.4 9.7 9.6 8.7 6.9 4.5 ✓
 50 30 16 16 32 50

Sta	+	π	-	Elev
		947.20		
10				38.2
+27				42.7
+39				42.5
+67				37.0
+84				32.8
11				32.7
+38.57				33.1
B.M.		6.42	940.78	940.76

L

Q

R

90 80 85 90 72 47 29 ✓
50 26 12 20 34 50

80 64 59 45 59 76 53 ✓
50 24 9 10 29 50

77 69 ~~84~~ 59 47 65 86 74 ✓
50 32 12 13 30 50

89 95 95 102 114 116 116 117 ✓
50 33 12 8 21 36 50

104 102 134 137 144 L.O. ✓
50 33 11 3

105 107 138 144 145 L.O. ✓
50 46 33 28

141

P.R. Spt. in 15" Leaning Oak Sw. Cor. Harriet & Kieffer

