

Book-3 - Dr. 11-A

X

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan

Survey

TONER RD.

From W. Co. Line To Long Lake Rd.

Road Acc't. No. M 8

Date Filed 9-19-30 File 30-M8

PROJ. 30-M8

Office of Ramsey Co. Engineer
ST. PAUL, MINN.

Date Filed 9-19-30

File No.

Transit, Notes

Toner Road

Rd 9-M-8

Proj. 30-M-8

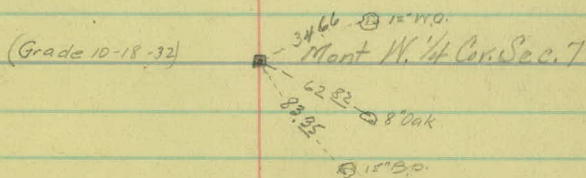
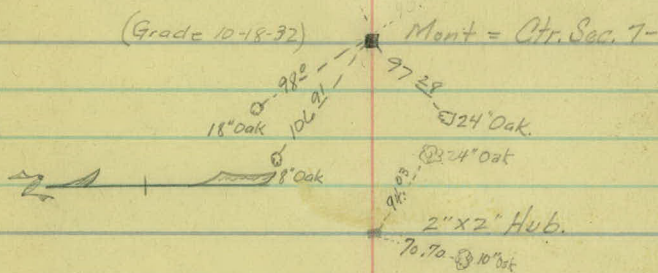
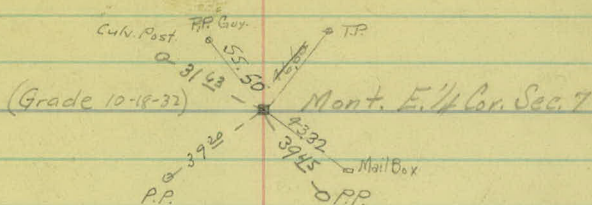
48+81.75 Mont

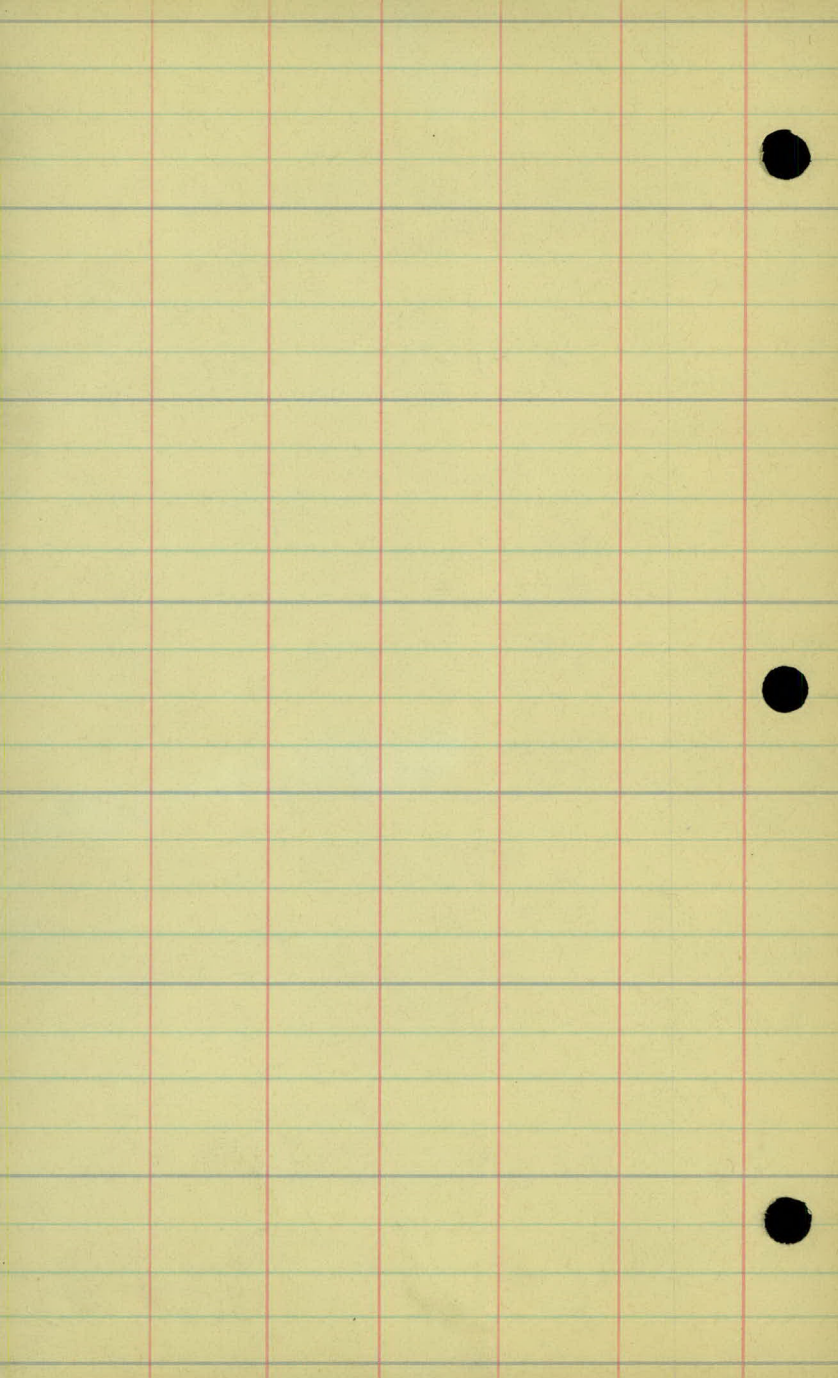
↓ 2637.10 → = M.
2633.40 = R.

22+44.65 Mont

14+00 P.O.T.

0+00 Mont





Topog.

6

5

4

3

2

1

0+00

+85 = 10" Oak 29'

+76 = 12" Oak 28'

+42 End light Clearing

F. 27'

Rd

+72 Beg. light Clearing.

+30 End light Clearing

+06 = 3-6" Oaks 12' F 27'

Rd. 2' Rd.

+55 Beg. light Clearing

+55 Beg. Heavy Brushing

+03 = 4" Oak 20' F. 28'

Rd

+67 = 6" Oak 18'

+54 = 2-6" Oaks 27'

+39 = 4" Oak 12'

F 28'

Rd

+20 End light Clearing 28'

F. 28'

+02 Beg. light Clearing 17'

Rd 2'

+17 F Oak 225'

Scattered Oaks

Rd 9'

Scattered Oaks

+93 Beg. Heavy Clearing 15'

+30 Beg. Hay. Meadow.
+30 End. Heavy j. Brg.

Scattered Oaks

+95 = 8" B.O. 14'

+54 = 18" Oak 25'

Scattered Oaks

F. 28' Rd 15'

Light Clearing 28' to 0+00

+67 = 6" W.O. 18'

+25 = Clump 3-6" Oaks 13'

+00 = 4" Oak 9'

+74 = 2-4" Oaks 9'

Scattered Oaks

+24 = 6" W.O. 23'

13

12

11

10

9

8

7

+78-2-4" W.O. 15'

F.26

F.16

F.27

LRH 15

F.17

+80 Beg. light clearing 12'
+72-4" W.O. 15'

F.27

F.17

+83-3-3" W.O. 25'

+63-3-4" W.O. 27'

F.27

2' RH 2

F.18

+53-2-10" OAKS 32'

F.28

3' RH 4

F.19

+72-2-6" OAKS 15'

F.27

2.5' RH 4

+85 End Clearing 15'
+85 F. Cor. 19'
+ To F.E.

+02-6" Oak 29' F.28

1' RH

20

19

18

17

16

15

14

Scattered
Oak trees

+15=12" B.O. 31'

F24.5

3' R.L.

+15=24" B.O. 28'
+02=12" B.O. 27'
F15.5

VII
+70 Edge of Marsh 30'

VII

F25

30'

30' E

+63=20" B.O. 24'

+14=8" W.O. 26'
F16

Dry Marsh

VII

+27 Edge Marsh 45'

F25

45'

+27= W.O. 8" - 16.5'
F16.5

F25

E X

F17

Scattered Oaks

F25

E

+66=10" W.O. 32'
+56=8" W.O. 18'

+14=15" B.O. 28'
+06=18" B.O. 27'
F17

Wooded Pasture (Scattered Oaks)

+60=12" W.O. 27'

F25

15 R.L.

F16

+50 End light Clearing 12'

+33=2=10" B.O. 29'

F25

15 R.L.

+58=18" B.O. 29'

F16.5

27

26

25

24

23

22

21

Cut 6'

Cut 10'

+64 = F Entrance

Cut 6'

E Cut 10'

+00 Cut = 6'

+00 Beg. Cut 15'

+60 = Beg. Cut 25'

+57 = End Low Boggy Land 15'

+57 Edge Low Boggy Land 10'

3'

7' 10'

+98 = 10' x 17' N. 1' X Dr.

+10 = Low Boggy Land 10'

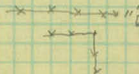
Bog.

+25' Low Boggy Land 20'

2'

+44 F 11'

+34 F Cor. 28'



+44.65 Mont

+34 F Cor 14'

F 27'

2'

F 14'

Wooded Pasture

+66-20" B.O. 22'

F 255

2'

F 15'

34

33

32

31

30

29

28

+68 E.P. 28'

Heavy
Brush
F14'

+60 = Beg. Cult. 20'
+39 E.P. 28'

+64 = 18" B.O. 24'
+33 = 15" Tw Oak 25'

F14.

+13 = 12" B.O. 19'

F15'

Scattered
Oaks.

+20 = E.P. 28'
+10 Edge of Boggy Land 10' $\frac{1}{2}$
+00 = X Dr. 10' Vit 16' $\frac{1}{2}$ 95'

+65 Boggy Land 10'

+40 Low Boggy Land 40'

+36 End X Dr. 8' = 15" x 30' C.M.

4' 10'

F14'

+13 = End X Dr. 12'

+53 Beg. Hay Meadow.
+52 E.P. 28'
+45 End Cult. 15'

+65 F Corr. 18'
+53 E Side Road.
+47 E Rd = 33'
+27 = Clump of 10-1" Birch
+09 End Cult. 10'

5'

+42 Beg Light + Clearing 11'
8'

Wooded Pasture.

41



40

39



38

37

36



35

+62 E.P. 28'

±

+89 E.P. 28'
+70 End Hay F. Beg. Cult 30'

±

±

¹⁰
+13 E.P. 28'
+10 = End Cult. Beg Hay. F ±

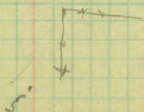
1

+40 E.P. 28'

Cult = 11'

3'

Waste Land. Scattered Timothy Hay.



+58 F cor 15'
Also End Light
C/Bar 19

48

47

46

45

44

43

42

+81.75 Mont.

+55 EP. 28'

+79 EP. 28'

+18. X Drs. 9' = 1-12" X 20 CM.
1-12" X 20" Vlt.

+08 EP. 28'

100 End Cult. Bog. Hay NW 28'±

+24 EP 28'

Low Boggy Land

Hay Meadow. Low Boggy Land
Low Boggy Land

Fair 75°F

7-2-30

Bench Levels

Towner Road

Rd. $\frac{9}{16}$ M-8

	+	M.I.	-	Elev
B.M.	1.60	917.42		915.82
T.P.	0.43	908.79	9.06	908.36
T.P.	4.09	902.30	10.58	898.21
T.P.	4.72	902.55	4.47	897.83
B.M.			1.46	901.09
T.P.	9.43	906.46	5.52	897.03
T.P.	2.47	907.40	1.53	904.93
B.M.	5.63	906.87	6.16	901.24
T.P.	4.94	908.01	3.80	903.07
B.M.	6.41	909.03	5.39	902.62
T.P.	12.47	921.20	0.30	908.73
B.M.			4.19	917.01
T.P.	0.36	909.90	11.66	909.54
T.P.	5.26	906.36	8.80	901.10
	3.40	907.18	2.58	903.78
B.M.			4.67	902.51
B.M.			2.52	904.66

{ Spike in 20" Stump 52' Rt Sta. 500+90 Anker Cutoff }
N.E. cor. Int. of Long Lake Road.

Spike in Guy Pole N.E. cor. Int. of Long Lake Road "H²"
Top Stake Sta. 46+00
" " " 41+00

Spike in So. side of 18" B.O. 46' Rt Sta. 35+20

Spike in E.P. 28' Lt Sta. 29+52

N.W. cor. Mont. Sta. 22+44.65

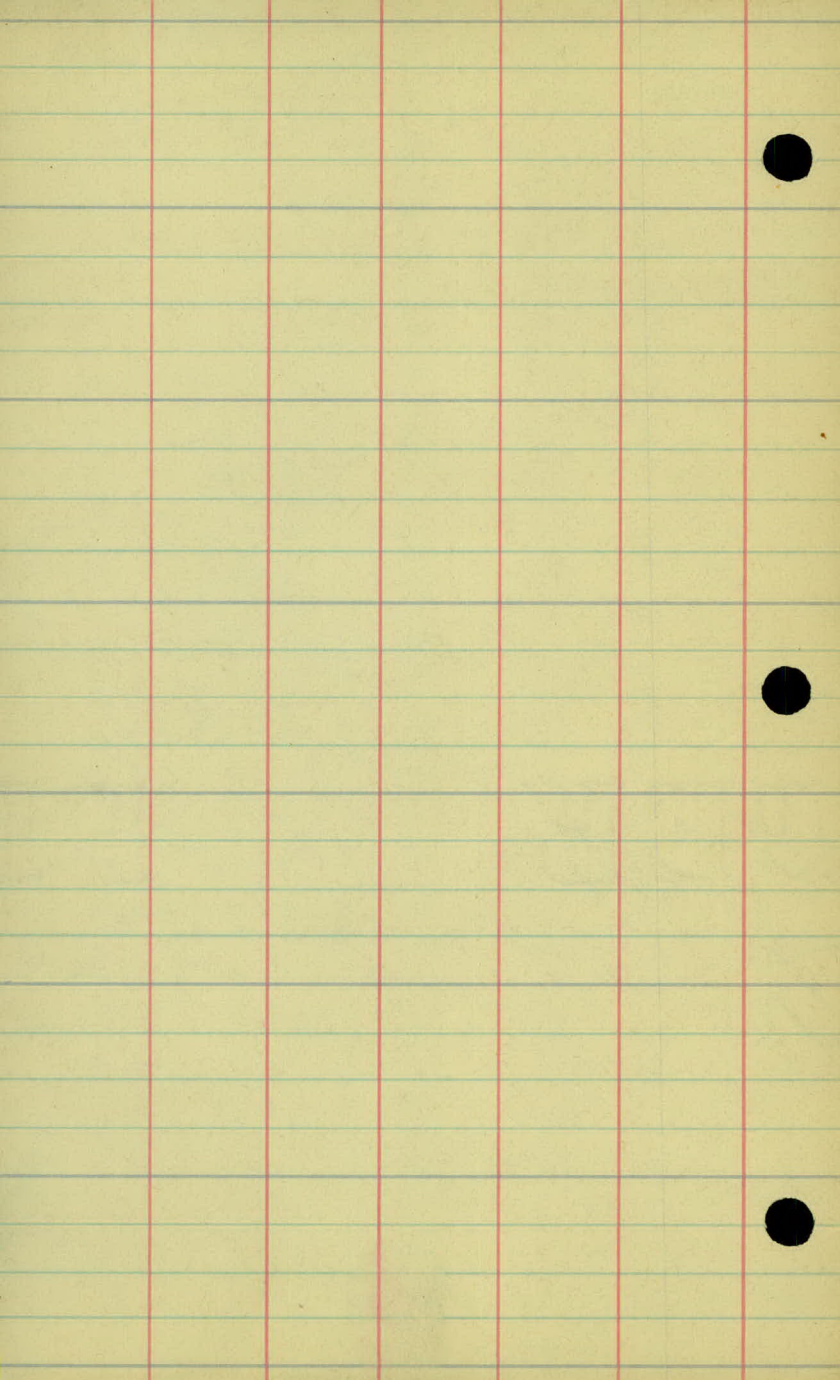
Spike in Root of 24" B.O. 45' Rt Sta 14+85

Top Stake Sta. 11+00

Sta 2

N.W. cor Mont 0+00.

Spike in 24" White Oak 78' Lt Sta. 1+45



July 3-4- -30.

X. Section Notes

Co. Road H³

West County line To Long Lake Road.

Sta.	+	H.I.	-	Elev
B.M.	2.52	907.18✓		904.66
0-100				1.9
0-50				2.2
0+00				2.5
0+50				2.7
1+00				1.8
T.P	4.13	907.91✓	3.40	903.78✓
+50				2.1
2				3.3
+50				3.6
3				3.4
+50				3.4
4				3.3
+50				2.1
5				900.1
T.P.	6.77	906.08	8.60	899.31✓

July 3-30
Fair - 80°.

Left

±

Right

Weber
Stoughton
Bell
Stevens

$\frac{4.8}{33}$ $\frac{5.5}{24}$ $\frac{5.6}{10}$ 5.3 $\frac{5.4}{6}$ $\frac{6.8}{11}$ $\frac{7.6}{14}$ $\frac{8.8}{33}$

$\frac{4.1}{33}$ $\frac{4.5}{17}$ $\frac{5.1}{16}$ 5.0 $\frac{5.0}{8}$ $\frac{6.5}{14}$ $\frac{6.0}{16}$ $\frac{6.7}{33}$

$\frac{4.0}{33}$ $\frac{4.1}{16}$ $\frac{4.6}{15}$ $\frac{4.0}{6}$ 4.7 $\frac{4.8}{11}$ $\frac{5.3}{33}$

$\frac{4.5}{33}$ $\frac{4.6}{17}$ $\frac{4.6}{9}$ 4.5 $\frac{4.2}{5}$ $\frac{4.8}{8}$ $\frac{4.6}{16}$ $\frac{5.0}{33}$

$\frac{5.7}{33}$ $\frac{5.7}{13}$ $\frac{5.4}{7}$ 5.4 $\frac{5.4}{9}$ $\frac{5.4}{23}$ $\frac{5.0}{33}$

$\frac{5.5}{33}$ $\frac{5.7}{13}$ $\frac{6.2}{11}$ $\frac{5.9}{9}$ 5.8 $\frac{5.9}{7}$ $\frac{6.3}{10}$ $\frac{6.0}{30}$ $\frac{5.8}{33}$

$\frac{4.1}{33}$ $\frac{4.3}{14}$ $\frac{5.0}{11}$ $\frac{4.7}{9}$ 4.6 $\frac{4.6}{8}$ $\frac{5.0}{11}$ $\frac{4.6}{13}$ $\frac{5.0}{33}$

$\frac{3.7}{33}$ $\frac{4.0}{15}$ $\frac{4.6}{12}$ $\frac{4.3}{8}$ 4.3 $\frac{4.4}{2}$ $\frac{4.7}{11}$ $\frac{4.3}{13}$ $\frac{4.7}{33}$

$\frac{3.8}{33}$ $\frac{4.3}{17}$ $\frac{5.2}{12}$ $\frac{4.5}{9}$ 4.5 $\frac{4.3}{4}$ $\frac{4.9}{9}$ $\frac{5.6}{14}$ $\frac{4.8}{17}$ $\frac{4.9}{33}$

$\frac{3.6}{33}$ $\frac{4.0}{19}$ $\frac{4.8}{15}$ $\frac{4.3}{9}$ 4.5 $\frac{4.5}{8}$ $\frac{5.8}{14}$ $\frac{4.8}{18}$ $\frac{5.2}{33}$

$\frac{3.3}{33}$ $\frac{3.7}{20}$ $\frac{4.8}{14}$ $\frac{4.2}{8}$ 4.6 $\frac{4.6}{7}$ $\frac{5.4}{13}$ $\frac{4.8}{17}$ $\frac{5.5}{33}$

$\frac{4.5}{33}$ $\frac{4.8}{19}$ $\frac{6.1}{13}$ $\frac{5.5}{5}$ 5.8 $\frac{5.8}{8}$ $\frac{6.8}{12}$ $\frac{6.1}{14}$ $\frac{6.4}{22}$ $\frac{7.0}{33}$

$\frac{6.5}{33}$ $\frac{7.8}{12}$ $\frac{8.2}{10}$ $\frac{7.8}{5}$ 7.9 $\frac{7.9}{9}$ $\frac{8.9}{12}$ $\frac{9.5}{22}$ $\frac{9.7}{33}$

Top Sta Sta 6+00

906.08 ✓

July 3-30

+50

Cloudy. 55°F

898.7

Prober
Stoogun
Bell
Stevens.

98.7

6

+50

899.9

7

900.3

+50

900.0

8

0.3

+50

1.0

T.F.

9.89

911.00 ✓

4.97

901.11 ✓

9

2.0

+50

3.2

10

4.4

+50

6.4

T.F.

11.30

920.84 ✓

1.46

909.54 ✓

11

9.1

+50

11.6

Left

L

Right

$\frac{7.5}{33}$	$\frac{8.3}{10}$	$\frac{7.2}{5}$	7.4	$\frac{7.4}{8}$	$\frac{9.8}{15}$	$\frac{10.4}{33}$
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$\frac{6.1}{33}$	$\frac{6.8}{16}$	$\frac{7.4}{10}$	$\frac{7.0}{8}$	7.2	$\frac{7.2}{8}$	$\frac{8.4}{18}$	$\frac{9.4}{33}$
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$\frac{4.8}{33}$	$\frac{5.4}{13}$	$\frac{6.1}{10}$	$\frac{5.9}{8}$	6.2	$\frac{6.2}{9}$	$\frac{6.3}{23}$	$\frac{6.9}{33}$
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$\frac{5.0}{33}$	$\frac{5.2}{13}$	$\frac{5.6}{11}$	$\frac{5.3}{7}$	5.8	$\frac{5.5}{8}$	$\frac{5.8}{11}$	$\frac{5.2}{15}$	$\frac{6.0}{33}$
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$\frac{6.7}{33}$	$\frac{7.5}{13}$	$\frac{6.5}{10}$	$\frac{5.8}{5}$	6.1	$\frac{5.7}{10}$	$\frac{6.1}{12}$	$\frac{5.6}{21}$	$\frac{5.0}{33}$
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$\frac{8.5}{33}$	$\frac{7.8}{13}$	$\frac{6.3}{7}$	$\frac{5.7}{4}$	5.8	$\frac{5.4}{9}$	$\frac{5.8}{13}$	$\frac{5.1}{18}$	$\frac{4.6}{33}$
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$\frac{5.5}{33}$	$\frac{5.2}{13}$	$\frac{5.8}{10}$	$\frac{4.5}{6}$	5.1	$\frac{4.6}{10}$	$\frac{5.3}{15}$	$\frac{4.3}{19}$	$\frac{4.3}{33}$
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$\frac{8.5}{33}$	$\frac{8.5}{17}$	$\frac{9.5}{13}$	$\frac{8.3}{6}$	9.0	$\frac{8.6}{10}$	$\frac{9.1}{13}$	$\frac{8.7}{18}$	$\frac{8.4}{33}$
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$\frac{7.7}{33}$	$\frac{7.8}{17}$	$\frac{8.3}{11}$	$\frac{7.4}{6}$	7.8	$\frac{7.7}{11}$	$\frac{8.5}{14}$	$\frac{7.7}{17}$	$\frac{7.8}{33}$
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$\frac{6.8}{33}$	$\frac{6.9}{15}$	$\frac{7.3}{10}$	$\frac{6.3}{6}$	6.6	$\frac{6.7}{10}$	$\frac{7.1}{12}$	$\frac{7.1}{16}$	$\frac{7.7}{33}$
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$\frac{3.3}{33}$	$\frac{3.7}{13}$	$\frac{4.1}{11}$	$\frac{4.1}{8}$	4.6	$\frac{4.1}{9}$	$\frac{4.8}{12}$	$\frac{4.6}{17}$	$\frac{5.2}{33}$
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$\frac{10.0}{33}$	$\frac{10.1}{19}$	$\frac{10.4}{9}$	$\frac{11.6}{5}$	11.8	$\frac{10.3}{9}$	$\frac{11.1}{19}$	$\frac{10.6}{23}$	$\frac{10.6}{33}$
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$\frac{9.0}{33}$	$\frac{8.8}{20}$	$\frac{8.8}{6}$	9.2	$\frac{8.7}{14}$	$\frac{8.5}{15}$	$\frac{8.5}{33}$
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920.84 ✓

12+00

12.9

+50

14.0

13

15.3

+50

16.1

14

16.6

B.M.

2.12

919.13 ✓

383

917.01 ✓

917.01

+50

15.8

15.7

15

14.6

+50

12.4

16

10.1

+50

8.2 ✓

T.P.

1.52

910.26 ✓

10.39

908.74 ✓

17

6.8

+50

5.8

18

05.1

Left $\neq$ Right

$$\begin{array}{r} 8.3 \\ 33 \end{array} \quad \begin{array}{r} 8.0 \\ 21 \end{array} \quad \begin{array}{r} 7.7 \\ 6 \end{array} \quad 7.9 \quad \begin{array}{r} 7.4 \\ 4 \end{array} \quad \begin{array}{r} 7.4 \\ 76 \end{array} \quad \begin{array}{r} 7.4 \\ 33 \end{array}$$

$$\begin{array}{r} 7.2 \\ 33 \end{array} \quad \begin{array}{r} 6.9 \\ 11 \end{array} \quad \begin{array}{r} 6.4 \\ 8 \end{array} \quad 6.8 \quad \begin{array}{r} 6.1 \\ 5 \end{array} \quad \begin{array}{r} 6.1 \\ 15 \end{array} \quad \begin{array}{r} 6.0 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 5.5 \\ 11 \end{array} \quad \begin{array}{r} 5.2 \\ 7 \end{array} \quad 5.5 \quad \begin{array}{r} 4.9 \\ 5 \end{array} \quad \begin{array}{r} 4.9 \\ 15 \end{array} \quad \begin{array}{r} 5.1 \\ 33 \end{array}$$

$$\begin{array}{r} 4.8 \\ 33 \end{array} \quad \begin{array}{r} 4.6 \\ 19 \end{array} \quad \begin{array}{r} 4.8 \\ 10 \end{array} \quad \begin{array}{r} 4.5 \\ 7 \end{array} \quad 4.7 \quad \begin{array}{r} 4.5 \\ 7 \end{array} \quad \begin{array}{r} 4.9 \\ 11 \end{array} \quad \begin{array}{r} 4.7 \\ 33 \end{array}$$

$$\begin{array}{r} 4.0 \\ 33 \end{array} \quad \begin{array}{r} 3.8 \\ 15 \end{array} \quad \begin{array}{r} 4.2 \\ 10 \end{array} \quad \begin{array}{r} 3.8 \\ 6 \end{array} \quad 4.2 \quad \begin{array}{r} 4.0 \\ 6 \end{array} \quad \begin{array}{r} 4.2 \\ 12 \end{array} \quad \begin{array}{r} 3.8 \\ 16 \end{array} \quad \begin{array}{r} 4.1 \\ 33 \end{array}$$

Spike in Root of 24° B.O. 45' RT 1/2. 14 + 85

$$\begin{array}{r} 2.3 \\ 33 \end{array} \quad \begin{array}{r} 2.4 \\ 13 \end{array} \quad \begin{array}{r} 3.0 \\ 8 \end{array} \quad 3.3 \quad \begin{array}{r} 3.0 \\ 11 \end{array} \quad \begin{array}{r} 2.3 \\ 15 \end{array} \quad \begin{array}{r} 2.1 \\ 33 \end{array}$$

$$\begin{array}{r} 3.5 \\ 33 \end{array} \quad \begin{array}{r} 3.3 \\ 13 \end{array} \quad \begin{array}{r} 4.3 \\ 9 \end{array} \quad 4.5 \quad \begin{array}{r} 4.3 \\ 11 \end{array} \quad \begin{array}{r} 3.3 \\ 14 \end{array} \quad \begin{array}{r} 3.2 \\ 33 \end{array}$$

$$\begin{array}{r} 6.6 \\ 33 \end{array} \quad \begin{array}{r} 6.3 \\ 11 \end{array} \quad \begin{array}{r} 6.6 \\ 9 \end{array} \quad 6.7 \quad \begin{array}{r} 6.4 \\ 11 \end{array} \quad \begin{array}{r} 5.4 \\ 15 \end{array} \quad \begin{array}{r} 5.1 \\ 33 \end{array}$$

$$\begin{array}{r} 8.8 \\ 33 \end{array} \quad \begin{array}{r} 8.4 \\ 13 \end{array} \quad \begin{array}{r} 9.1 \\ 10 \end{array} \quad \begin{array}{r} 8.6 \\ 8 \end{array} \quad 9.0 \quad \begin{array}{r} 8.2 \\ 12 \end{array} \quad \begin{array}{r} 7.2 \\ 15 \end{array} \quad \begin{array}{r} 6.5 \\ 33 \end{array}$$

$$\begin{array}{r} 10.7 \\ 33 \end{array} \quad \begin{array}{r} 10.5 \\ 16 \end{array} \quad \begin{array}{r} 11.1 \\ 11 \end{array} \quad \begin{array}{r} 10.7 \\ 8 \end{array} \quad 10.9 \quad \begin{array}{r} 10.6 \\ 12 \end{array} \quad \begin{array}{r} 9.6 \\ 15 \end{array} \quad \begin{array}{r} 9.0 \\ 33 \end{array}$$

$$\begin{array}{r} 4.2 \\ 33 \end{array} \quad \begin{array}{r} 5.0 \\ 13 \end{array} \quad \begin{array}{r} 3.2 \\ 8 \end{array} \quad 3.5 \quad \begin{array}{r} 3.2 \\ 6 \end{array} \quad \begin{array}{r} 5.2 \\ 10 \end{array} \quad \begin{array}{r} 5.5 \\ 18 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array}$$

$$\begin{array}{r} 5.2 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 12 \end{array} \quad \begin{array}{r} 4.2 \\ 8 \end{array} \quad 4.5 \quad \begin{array}{r} 4.2 \\ 5 \end{array} \quad \begin{array}{r} 7.0 \\ 10 \end{array} \quad \begin{array}{r} 7.4 \\ 18 \end{array} \quad \begin{array}{r} 7.9 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 5.5 \\ 15 \end{array} \quad \begin{array}{r} 6.0 \\ 12 \end{array} \quad \begin{array}{r} 5.0 \\ 8 \end{array} \quad 5.2 \quad \begin{array}{r} 5.0 \\ 5 \end{array} \quad \begin{array}{r} 6.1 \\ 9 \end{array} \quad \begin{array}{r} 6.0 \\ 15 \end{array} \quad \begin{array}{r} 6.2 \\ 33 \end{array}$$

		H.I.			
Sta.	+	91026	-	Elev.	7-3-20
+50				4.4	
19				4.0	
+50				4.0	
20				4.7	
T.P.	5.54	910.46	5.34	904.92	
+50				6.0	
21				6.6	
+50				6.0	
22				4.3	
+50				2.2	
23				90.02	
T.P.	4.84	905.29	10.01	900.45	
+50				899.1	
+98		X Drain.			
24				98.5	
+50				98.6	

Left $\frac{9.7}{33}$ $\frac{8.0}{20}$ $\frac{7.1}{10}$ $\frac{5.6}{7}$ $\frac{5.9}{6}$ $\frac{5.8}{6}$ $\frac{6.5}{11}$ $\frac{6.2}{15}$ $\frac{6.3}{33}$ Right

$\frac{9.5}{33}$ $\frac{8.3}{24}$ $\frac{7.3}{9}$ $\frac{6.0}{7}$ 6.3 $\frac{6.1}{4}$ $\frac{7.0}{11}$ $\frac{6.7}{15}$ $\frac{6.7}{33}$

$\frac{8.4}{33}$ $\frac{7.6}{23}$ $\frac{7.3}{10}$ $\frac{6.3}{7}$ 6.3 $\frac{6.3}{10}$ $\frac{6.8}{17}$ $\frac{6.2}{33}$

$\frac{7.6}{33}$ $\frac{6.6}{24}$ $\frac{6.0}{14}$ $\frac{6.4}{10}$ $\frac{5.4}{6}$ 5.6 $\frac{5.3}{9}$ $\frac{5.6}{11}$ $\frac{5.1}{15}$ $\frac{4.6}{33}$

$\frac{5.8}{33}$ $\frac{5.5}{23}$ $\frac{4.9}{8}$ $\frac{4.0}{5}$ 4.5 $\frac{4.4}{12}$ $\frac{3.3}{14}$ $\frac{3.0}{26}$ $\frac{2.5}{33}$

$\frac{3.2}{33}$ $\frac{2.8}{20}$ $\frac{4.5}{17}$ $\frac{4.0}{12}$ 3.9 $\frac{3.7}{11}$ $\frac{2.1}{15}$ $\frac{1.6}{33}$

$\frac{2.5}{33}$ $\frac{2.3}{19}$ $\frac{4.8}{15}$ $\frac{4.1}{7}$ 4.5 $\frac{3.8}{10}$ $\frac{1.7}{14}$ $\frac{1.6}{33}$

$\frac{6.6}{33}$ $\frac{6.2}{22}$ $\frac{7.3}{16}$ $\frac{5.7}{10}$ 6.2 $\frac{5.2}{9}$ $\frac{4.4}{10}$ $\frac{3.6}{33}$

$\frac{11.0}{33}$ $\frac{9.8}{22}$ $\frac{9.6}{12}$ $\frac{8.2}{6}$ 8.3 $\frac{7.7}{9}$ $\frac{6.8}{22}$ $\frac{6.4}{33}$

$\frac{12.5}{33}$ $\frac{11.7}{10}$ $\frac{9.8}{4}$ 10.3 $\frac{9.8}{9}$ $\frac{10.1}{22}$ $\frac{9.9}{33}$

Low Land { $\frac{8.8}{33}$ $\frac{8.7}{8}$ $\frac{6.0}{4}$ 6.2 $\frac{5.9}{7}$ $\frac{6.6}{12}$ $\frac{6.9}{22}$ $\frac{6.9}{33}$ }
 9.95 ← Mainline → 10.0
 { $\frac{8.7}{33}$ $\frac{8.9}{8}$ $\frac{6.4}{4}$ 6.8 $\frac{6.6}{8}$ $\frac{8.7}{12}$ $\frac{8.8}{33}$ }
 { $\frac{8.0}{33}$ $\frac{8.8}{8}$ $\frac{6.7}{4}$ 6.7 $\frac{6.7}{8}$ $\frac{8.9}{13}$ $\frac{8.9}{33}$ }

		H1			
25	+	905.29	-	Elev.	
				899.7	
	+50			901.3	
T.P.	4.50	908.43	136	903.93	
26				03.6	
	+50			05.0	
27				04.0	
	+50			02.7	
28				01.6	
	+50			01.6	
29				01.3	
	+50			01.6	
B.M.	2.22	905.29	5.36	903.07	903.07
	+65			01.3	
	+75			00.9	
30				00.2	

Left. 4 Right

$\frac{4.5}{33}$ $\frac{5.5}{8}$ 56 $\frac{5.5}{8}$ $\frac{6.8}{13}$ $\frac{7.8}{33}$

$\frac{1.7}{33}$ $\frac{3.0}{8}$ 40 $\frac{3.5}{10}$ $\frac{4.5}{12}$ $\frac{6.1}{33}$

$\frac{2.8}{33}$ $\frac{3.6}{22}$ $\frac{4.3}{8}$ 4.8 $\frac{4.6}{10}$ $\frac{6.9}{26}$ $\frac{7.7}{33}$

$\frac{2.0}{33}$ $\frac{2.5}{22}$ $\frac{2.7}{9}$ 3.4 $\frac{3.3}{5}$ $\frac{4.8}{13}$ $\frac{6.8}{33}$

$\frac{3.3}{33}$ $\frac{3.4}{18}$ $\frac{4.4}{6}$ 4.4 $\frac{4.0}{5}$ $\frac{5.0}{8}$ $\frac{7.3}{33}$

$\frac{4.3}{33}$ $\frac{4.3}{14}$ $\frac{5.5}{5}$ 5.7 $\frac{5.1}{5}$ $\frac{6.1}{9}$ $\frac{8.0}{33}$

$\frac{6.0}{33}$ $\frac{6.0}{23}$ $\frac{6.3}{11}$ 6.8 $\frac{6.5}{5}$ $\frac{7.6}{19}$ $\frac{9.0}{33}$

$\frac{5.8}{33}$ $\frac{5.8}{13}$ $\frac{6.7}{11}$ 6.8 $\frac{7.5}{9}$ $\frac{8.0}{20}$ $\frac{9.1}{33}$

$\frac{6.6}{33}$ $\frac{6.2}{15}$ $\frac{7.1}{14}$ 7.1 $\frac{7.2}{5}$ $\frac{7.8}{13}$ $\frac{9.2}{25}$ $\frac{8.6}{33}$

$\frac{6.4}{33}$ $\frac{6.8}{27}$ $\frac{6.6}{17}$ $\frac{7.0}{14}$ 6.8 $\frac{6.5}{4}$ $\frac{7.0}{10}$ $\frac{6.9}{20}$ $\frac{6.1}{22}$ $\frac{6.3}{33}$

Spike in E.P. 28 Ft. Lt. 29 + 52

$\frac{2.8}{33}$ $\frac{2.5}{23}$ $\frac{4.0}{13}$ 4.0 $\frac{4.0}{10}$ $\frac{5.0}{13}$ $\frac{6.4}{29}$ $\frac{7.4}{33}$

$\frac{4.5}{33}$ $\frac{4.8}{17}$ $\frac{3.8}{12}$ $\frac{4.4}{9}$ 4.4 $\frac{4.4}{9}$ $\frac{6.0}{14}$ $\frac{6.4}{25}$ $\frac{7.5}{28}$ $\frac{7.7}{33}$

$\frac{5.5}{33}$ $\frac{5.5}{21}$ $\frac{4.4}{21}$ $\frac{4.4}{18}$ $\frac{5.0}{9}$ 5.1 $\frac{5.3}{5}$ $\frac{6.7}{9}$ $\frac{6.7}{19}$ $\frac{8.0}{25}$ $\frac{7.5}{33}$

Sta.	+	H.I.	-		
+20		905.29 ✓		X Dr.	
+50				99.8	
31				99.4	
31 +00			X Drain		
+50				99.9	
32				01.1 ✓	
T.P.	5.93	908.14 ✓	3.08	902.21	
+50				01.7	
33				01.7	
+50				01.6	
34				01.6	
+50				01.7	
35				01.9 ✓	
B.M.	7.81	909.05 ✓	6.88	901.26	901.24
35 +00					
+50				02.6	
36				03.1	

July 7-30 Fair 80°F

(885)

Flowline

(905)

$\frac{8.0}{33}$ $\frac{7.8}{27}$ $\frac{6.6}{10}$ $\frac{5.8}{5}$ 5.5 $\frac{5.8}{6}$ $\frac{6.4}{9}$ $\frac{6.2}{22}$ $\frac{6.1}{33}$

$\frac{8.6}{33}$ $\frac{8.6}{19}$ $\frac{7.6}{9}$ $\frac{6.0}{5}$ 5.9 $\frac{5.8}{7}$ $\frac{7.3}{10}$ $\frac{7.5}{22}$ $\frac{6.3}{33}$

(87)

← Flowline →

(8.3)

$\frac{6.6}{33}$ $\frac{5.9}{13}$ $\frac{6.2}{10}$ $\frac{5.2}{8}$ 5.4 $\frac{5.2}{7}$ $\frac{6.2}{11}$ $\frac{5.2}{14}$ $\frac{5.3}{33}$

$\frac{4.4}{33}$ $\frac{4.0}{17}$ $\frac{5.4}{13}$ $\frac{4.0}{9}$ 4.2 $\frac{4.2}{7}$ $\frac{5.2}{10}$ $\frac{3.8}{13}$ $\frac{4.1}{26}$ $\frac{4.6}{33}$

$\frac{6.2}{33}$ $\frac{6.1}{17}$ $\frac{7.5}{13}$ $\frac{6.3}{9}$ 6.4 $\frac{6.4}{6}$ $\frac{7.2}{7}$ $\frac{6.2}{11}$ $\frac{6.4}{21}$ $\frac{6.9}{33}$

$\frac{5.6}{33}$ $\frac{6.0}{15}$ $\frac{7.2}{12}$ $\frac{6.4}{9}$ 6.4 $\frac{6.4}{6}$ $\frac{7.2}{9}$ $\frac{6.8}{12}$ $\frac{7.6}{33}$

$\frac{5.6}{33}$ $\frac{6.1}{18}$ $\frac{7.1}{15}$ $\frac{6.5}{12}$ 6.5 $\frac{7.0}{5}$ $\frac{7.8}{7}$ $\frac{7.2}{9}$ $\frac{7.7}{16}$ $\frac{8.5}{33}$

$\frac{5.8}{33}$ $\frac{6.1}{24}$ $\frac{7.2}{19}$ $\frac{6.3}{15}$ 6.5 $\frac{7.1}{5}$ $\frac{8.0}{8}$ $\frac{7.2}{11}$ $\frac{7.7}{16}$ $\frac{8.2}{33}$

$\frac{6.0}{33}$ $\frac{6.4}{21}$ $\frac{7.4}{18}$ $\frac{6.1}{13}$ 6.4 $\frac{6.7}{4}$ $\frac{7.8}{8}$ $\frac{7.6}{15}$ $\frac{8.3}{33}$

6.2 $\frac{5.9}{4}$ $\frac{7.2}{7}$ $\frac{6.8}{13}$ $\frac{7.8}{33}$

Spikes in S. side of 18" B.O. 40' N4 Sta. 35+20

$\frac{6.0}{33}$ $\frac{6.8}{21}$ $\frac{8.0}{18}$ $\frac{7.0}{12}$ (7.2)

$\frac{4.8}{33}$ $\frac{5.4}{21}$ $\frac{6.7}{16}$ $\frac{6.1}{12}$ 6.5 $\frac{6.2}{5}$ $\frac{7.2}{8}$ $\frac{7.0}{12}$ $\frac{8.2}{33}$

$\frac{4.1}{33}$ $\frac{5.5}{11}$ 6.0 $\frac{6.0}{6}$ $\frac{6.7}{9}$ $\frac{6.4}{12}$ $\frac{7.6}{33}$

909.05 ✓

+50

03.7

37

04.3

+50

04.0

38

03.0 ✓

T.F.

6.33

908.96 ✓

642

902.63 ✓

+50

02.0

39

01.8

+50

02.3

40

03.3

+50

04.7

41

04.7

+50

04.5 ✓

T.F.

5.79

908.27 ✓

648

902.48 ✓

42

03.8

+50

03.1

Left

&

Right

$$\begin{array}{r} 4.1 \\ 33 \end{array} \quad \begin{array}{r} 4.8 \\ 13 \end{array} \quad \begin{array}{r} 5.5 \\ 10 \end{array} \quad \begin{array}{r} 5.1 \\ 8 \end{array} \quad 5.4 \quad \begin{array}{r} 5.5 \\ 7 \end{array} \quad \begin{array}{r} 5.8 \\ 11 \end{array} \quad \begin{array}{r} 5.8 \\ 18 \end{array} \quad \begin{array}{r} 6.5 \\ 33 \end{array}$$

$$\begin{array}{r} 4.8 \\ 33 \end{array} \quad \begin{array}{r} 4.5 \\ 11 \end{array} \quad \begin{array}{r} 5.0 \\ 9 \end{array} \quad \begin{array}{r} 4.6 \\ 7 \end{array} \quad 4.8 \quad \begin{array}{r} 4.8 \\ 5 \end{array} \quad \begin{array}{r} 5.2 \\ 8 \end{array} \quad \begin{array}{r} 4.8 \\ 11 \end{array} \quad \begin{array}{r} 5.2 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \quad \begin{array}{r} 5.4 \\ 11 \end{array} \quad \begin{array}{r} 4.8 \\ 8 \end{array} \quad 5.1 \quad \begin{array}{r} 5.1 \\ 7 \end{array} \quad \begin{array}{r} 4.4 \\ 10 \end{array} \quad \begin{array}{r} 4.2 \\ 33 \end{array}$$

$$\begin{array}{r} 7.7 \\ 33 \end{array} \quad \begin{array}{r} 6.4 \\ 11 \end{array} \quad \begin{array}{r} 5.8 \\ 8 \end{array} \quad 6.1 \quad \begin{array}{r} 5.6 \\ 8 \end{array} \quad \begin{array}{r} 5.1 \\ 9 \end{array} \quad \begin{array}{r} 4.8 \\ 33 \end{array}$$

$$\begin{array}{r} 899.13 \\ 93 \\ 33 \end{array} \quad \begin{array}{r} 900.66 \\ 83 \\ 19 \end{array} \quad \begin{array}{r} 901.96 \\ 70 \\ 8 \end{array} \quad 7.0 \quad \begin{array}{r} 902.36 \\ 66 \\ 6 \end{array} \quad \begin{array}{r} 903.16 \\ 5.8 \\ 10 \end{array} \quad \begin{array}{r} 902.16 \\ 5.8 \\ 33 \end{array}$$

$$\begin{array}{r} 9.7 \\ 33 \end{array} \quad \begin{array}{r} 8.1 \\ 13 \end{array} \quad \begin{array}{r} 7.1 \\ 8 \end{array} \quad 7.2 \quad \begin{array}{r} 7.1 \\ 8 \end{array} \quad \begin{array}{r} 6.6 \\ 14 \end{array} \quad \begin{array}{r} 6.4 \\ 33 \end{array}$$

$$\begin{array}{r} 8.0 \\ 33 \end{array} \quad \begin{array}{r} 7.5 \\ 19 \end{array} \quad \begin{array}{r} 6.7 \\ 7 \end{array} \quad 6.7 \quad \begin{array}{r} 6.7 \\ 7 \end{array} \quad \begin{array}{r} 6.1 \\ 9 \end{array} \quad \begin{array}{r} 6.2 \\ 33 \end{array}$$

$$\begin{array}{r} 6.2 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 18 \end{array} \quad \begin{array}{r} 6.7 \\ 14 \end{array} \quad \begin{array}{r} 5.6 \\ 10 \end{array} \quad 5.7 \quad \begin{array}{r} 5.6 \\ 7 \end{array} \quad \begin{array}{r} 5.1 \\ 8 \end{array} \quad \begin{array}{r} 5.3 \\ 33 \end{array}$$

$$\begin{array}{r} 4.8 \\ 33 \end{array} \quad \begin{array}{r} 4.6 \\ 18 \end{array} \quad \begin{array}{r} 5.2 \\ 14 \end{array} \quad \begin{array}{r} 4.3 \\ 11 \end{array} \quad 4.3 \quad \begin{array}{r} 4.2 \\ 5 \end{array} \quad \begin{array}{r} 3.8 \\ 8 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad \begin{array}{r} 4.1 \\ 33 \end{array}$$

$$\begin{array}{r} 4.6 \\ 33 \end{array} \quad \begin{array}{r} 4.6 \\ 23 \end{array} \quad \begin{array}{r} 4.3 \\ 12 \end{array} \quad 4.3 \quad \begin{array}{r} 4.4 \\ 12 \end{array} \quad \begin{array}{r} 4.4 \\ 33 \end{array}$$

$$\begin{array}{r} 4.6 \\ 33 \end{array} \quad \begin{array}{r} 4.3 \\ 17 \end{array} \quad \begin{array}{r} 5.2 \\ 11 \end{array} \quad \begin{array}{r} 4.5 \\ 7 \end{array} \quad 4.5 \quad \begin{array}{r} 4.5 \\ 6 \end{array} \quad \begin{array}{r} 4.0 \\ 8 \end{array} \quad \begin{array}{r} 5.9 \\ 17 \end{array} \quad \begin{array}{r} 4.5 \\ 33 \end{array}$$

$$\begin{array}{r} 3.1 \\ 33 \end{array} \quad \begin{array}{r} 2.8 \\ 26 \end{array} \quad \begin{array}{r} 5.1 \\ 22 \end{array} \quad \begin{array}{r} 4.8 \\ 16 \end{array} \quad \begin{array}{r} 4.4 \\ 7 \end{array} \quad 4.5 \quad \begin{array}{r} 4.4 \\ 4 \end{array} \quad \begin{array}{r} 4.4 \\ 7 \end{array} \quad \begin{array}{r} 3.5 \\ 8 \end{array} \quad \begin{array}{r} 3.0 \\ 33 \end{array}$$

$$\begin{array}{r} 3.3 \\ 33 \end{array} \quad \begin{array}{r} 3.0 \\ 26 \end{array} \quad \begin{array}{r} 5.8 \\ 22 \end{array} \quad \begin{array}{r} 5.3 \\ 9 \end{array} \quad 5.2 \quad \begin{array}{r} 5.4 \\ 3 \end{array} \quad \begin{array}{r} 4.2 \\ 11 \end{array} \quad \begin{array}{r} 3.2 \\ 12 \end{array} \quad \begin{array}{r} 3.5 \\ 24 \end{array} \quad \begin{array}{r} 4.0 \\ 33 \end{array}$$

Sta. + H.I. - Elev
908.27 ✓

43 02.0

+20 01.5

+50 00.4

44 98.9 ✓

T.P. 2.29 901.50 9.06 899.21 ✓

+50 97.8

✓

45 96.8

+50 96.2

46 96.7

+50 96.9

47 96.8

+50 97.4

48 97.9

+40 98.0

Left $\neq$ Right

$$\frac{5.1}{33} \quad \frac{4.5}{24} \quad \frac{6.8}{21} \quad \frac{6.1}{9} \quad 6.3 \quad \frac{6.3}{5} \quad \frac{5.4}{10} \quad \frac{4.6}{11} \quad \frac{4.1}{17} \quad \frac{4.8}{33}$$

$$\frac{6.2}{33} \quad \frac{5.7}{30} \quad \frac{5.8}{20} \quad \frac{6.2}{17} \quad \frac{6.8}{9} \quad 6.8 \quad \frac{6.7}{8} \quad \frac{5.7}{9} \quad \frac{5.2}{20} \quad \frac{5.7}{33}$$

$$\frac{8.5}{33} \quad \frac{7.4}{11} \quad \frac{8.0}{9} \quad \frac{7.3}{7} \quad 7.9 \quad \frac{7.9}{12} \quad \frac{7.6}{33}$$

$$\frac{9.9}{33} \quad \frac{9.9}{13} \quad \frac{10.6}{11} \quad \frac{9.2}{8} \quad 9.4 \quad \frac{9.5}{4} \quad \frac{9.0}{7} \quad \frac{10.9}{11} \quad \frac{10.4}{13} \quad \frac{10.4}{26} \quad \frac{10.4}{33}$$

$$\frac{4.4}{33} \quad \frac{4.7}{12} \quad \frac{5.6}{11} \quad \frac{3.7}{8} \quad 3.7 \quad \frac{3.7}{4} \quad \frac{3.3}{7} \quad \frac{5.8}{10} \quad \frac{5.0}{12} \quad \frac{4.6}{33}$$

$$\frac{5.6}{33} \quad \frac{5.6}{12} \quad \frac{6.3}{11} \quad \frac{4.9}{8} \quad 4.7 \quad \frac{4.4}{9} \quad \frac{6.4}{11} \quad \frac{6.0}{13} \quad \frac{5.8}{33}$$

$$\frac{6.1}{33} \quad \frac{6.6}{11} \quad \frac{5.0}{8} \quad 5.3 \quad \frac{5.1}{8} \quad \frac{6.4}{11} \quad \frac{6.4}{33}$$

$$\frac{6.1}{33} \quad \frac{6.4}{9} \quad \frac{5.2}{7} \quad 4.8 \quad \frac{5.0}{8} \quad \frac{6.4}{10} \quad \frac{6.8}{33}$$

$$\frac{6.2}{33} \quad \frac{6.8}{11} \quad \frac{5.0}{8} \quad 4.6 \quad \frac{4.7}{4} \quad \frac{5.1}{7} \quad \frac{7.2}{10} \quad \frac{7.2}{12} \quad \frac{6.2}{13} \quad \frac{6.2}{33}$$

$$\frac{5.6}{33} \quad \frac{6.3}{11} \quad \frac{5.1}{9} \quad 4.7 \quad \frac{4.8}{8} \quad \frac{6.7}{12} \quad \frac{6.7}{14} \quad \frac{6.2}{15} \quad \frac{6.2}{33}$$

$$\frac{5.0}{33} \quad \frac{5.2}{14} \quad \frac{5.8}{13} \quad \frac{5.8}{11} \quad \frac{4.0}{9} \quad 4.1 \quad \frac{4.3}{8} \quad \frac{6.8}{11} \quad \frac{6.8}{13} \quad \frac{5.5}{14} \quad \frac{5.8}{33}$$

$$\frac{3.7}{33} \quad \frac{4.0}{14} \quad \frac{5.0}{13} \quad \frac{5.0}{11} \quad \frac{2.5}{10} \quad 3.6 \quad \frac{3.7}{9} \quad \frac{4.5}{11} \quad \frac{4.7}{12} \quad \frac{4.3}{13} \quad \frac{4.6}{33}$$

$$\frac{3.1}{33} \quad \frac{3.3}{19} \quad \frac{3.3}{9} \quad 3.5 \quad \frac{3.4}{13} \quad \frac{3.5}{21} \quad \frac{3.7}{33}$$

48

901.50 ✓

+50

98.1

+60

98.1

+81⁷⁵

Long Lake Rd. ✓ 98.9

T.P.

408

902.74

2.84

898.66 ✓

B.M.

1.67

901.07 ✓

901.09

Left

±

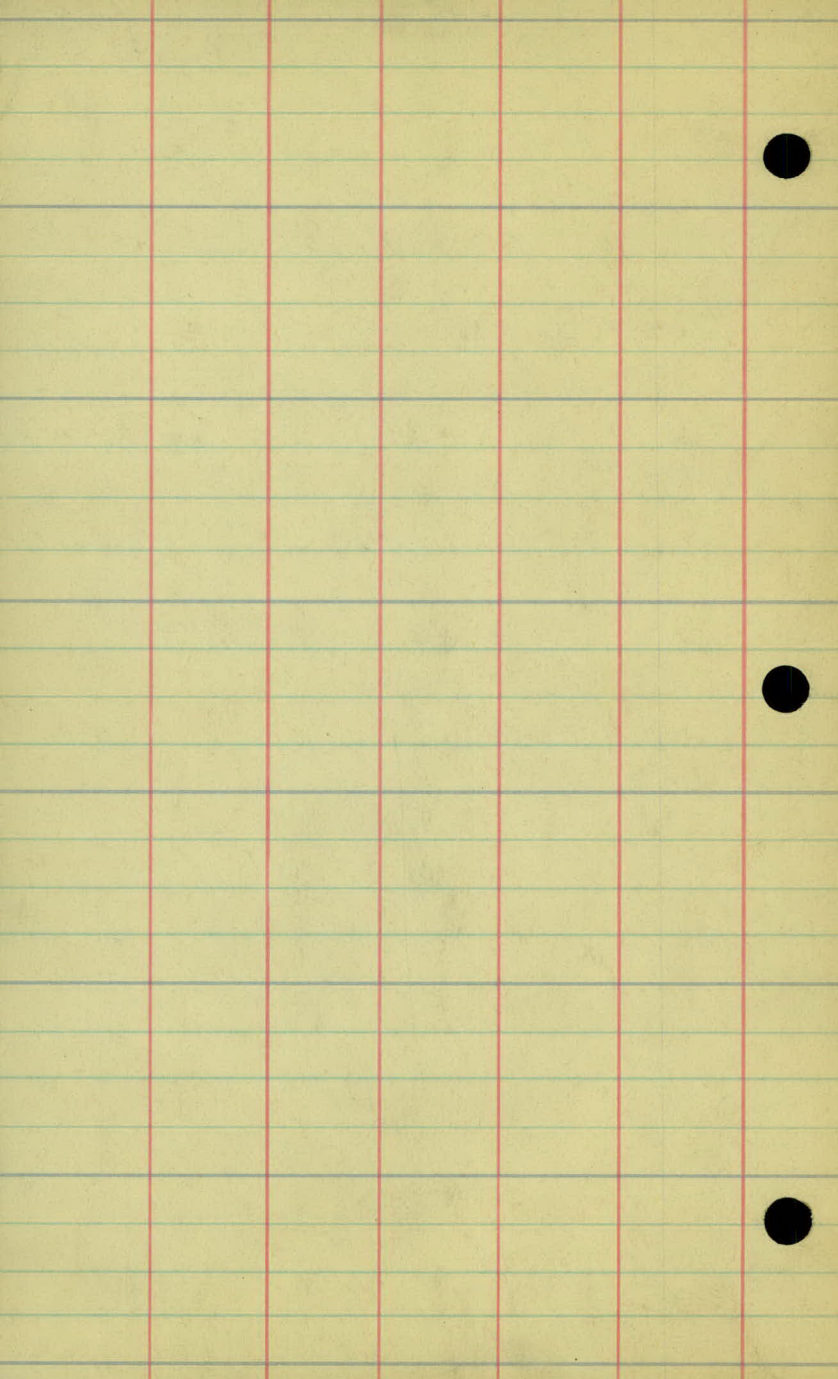
Right

$$\begin{array}{r} 5.4 \\ 33 \end{array} \quad \begin{array}{r} 4.0 \\ 14 \end{array} \quad \begin{array}{r} 3.4 \\ 8 \end{array} \quad 3.4 \quad \begin{array}{r} 3.4 \\ 9 \end{array} \quad \begin{array}{r} 3.4 \\ 23 \end{array} \quad \begin{array}{r} 3.8 \\ 33 \end{array}$$

$$\begin{array}{r} 4.4 \\ 33 \end{array} \quad \begin{array}{r} 4.4 \\ 25 \end{array} \quad \begin{array}{r} 3.8 \\ 11 \end{array} \quad 3.4 \quad \begin{array}{r} 3.8 \\ 13 \end{array} \quad \begin{array}{r} 4.0 \\ 30 \end{array} \quad \begin{array}{r} 6.1 \\ 37 \end{array}$$

$$\begin{array}{r} 3.3 \\ 50 \end{array} \quad \begin{array}{r} 3.0 \\ 25 \end{array} \quad 2.6 \quad \begin{array}{r} 2.9 \\ 25 \end{array} \quad \begin{array}{r} 3.3 \\ 50 \end{array}$$

Spike in Guy. Pole N.E. cor. Lang Lake Rd. + H. 2



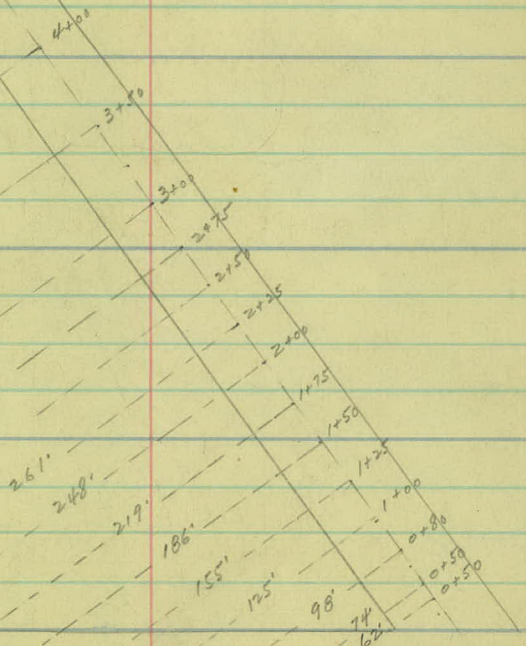
Weber
Stooglund
Bell
Stevens.

July 14-30.

Wards View St.

Prok. Cutoff.

low
hand



Co. Rd. "G"

Mont

Sta.	+	H.I.	-	Elev.	
B.M.	6.59	924.21		917.62	
0+00					19.4
+50					19.4
+60					19.4
+80					19.4
1					19.3
+25					19.3
T.P.	1.44	920.66	4.99	919.22	
+50					19.3
+75					18.6
T.P.	11.33	920.96	11.03	909.63	
2					18.9
+25					18.8
+50					18.5
+75					18.3
3					18.0

Left

L.

Spike in P.P. Lt. Sta. 28+46 Co. Rd. "G" Survey.

4.8

L"G"

(4.8)

80	7.3	7.4	6.8	6.5	5.0	4.9	
62	39	36	30	26	19	13.5	4.75

L"G"

(4.8)

85	8.2	8.2	4.0	4.2	6.8	6.6	4.9	4.9	
74	55	48	40	32	27	24	19	13.5	4.75

L"G"

(4.8)

9.6	8.3	7.9	8.2	3.2	1.7	2.5	5.2	7.1	6.5	5.0	4.85	
98	74	67	60	51	42	35	31	27	23	19	13.5	4.75

L"G"

(4.9)

10.9	10.3	3.1	2.0	2.7	3.6	5.4	6.9	6.5	5.0	4.9	
125	96	83	65	44	35	32	28	24	19	13.5	4.85

L"G"

(4.9)

12.1	11.8	3.8	2.6	3.5	4.6	4.2	4.6	6.7	6.7	5.0	5.0	
155	128	111	100	89	66	47	34	29	24	19	13.5	4.90

L"G"

(1.4)

10.1	8.8	4.4	2.3	1.7	2.5	3.3	1.9	1.4	3.4	3.2	1.6	1.54	
186	160	149	132	122	93	84	39	32	28	24	19	13.5	1.44

L"G"

(1.6)

11.7	11.9	11.3	9.0	6.6	5.2	4.6	5.2	4.7	2.0	3.7	3.2	1.8	1.66	
219	192	187	166	153	129	96	79	52	31	27	24	19	13.5	1.55

(2.1)

11.2	9.3	7.4	7.4	7.1	4.9	3.5	4.5	3.9	2.1	2.15	
150	134	115	89	65	42	30	25	24	19	13.5	2.05

(2.2)

15.0	11.5	10.3	10.3	8.5	7.3	5.8	4.3	2.3	2.35	
150	123	100	89	61	49	33	25	19	13.5	2.20

(2.5)

17.0	14.3	13.8	12.3	10.3	9.4	8.3	6.1	2.6	2.55	
150	125	100	81	68	51	43	26	19	13.5	2.45

14.8	14.1	10.4	10.4	8.2	2.8	2.30	
100	86	51	39	28	19	13.5	2.70

15.0	11.7	9.7	2.6	3.1	3.10	
100	59	34	28	19	13.5	3.00

Sta.	+	H.I.	-	Elev
		920.96		
+50				17.3
4				16.5
T. P.	4.47	913.00	12.43	908.53
2				18.9
2 + 25				18.8
T. P.	8.55	913.51	8.04	904.96
+ 50				18.5
+ 75				18.3
3				18.0
+ 50				17.3
4				16.5
T. P.	7.38	919.38	1.51	912.00
B. M			1.77	917.61 917.62

Left

2.

$$\frac{16.0}{100} \frac{10.9}{49} \frac{9.8}{35} \frac{8.0}{27} \frac{5.7}{19} \frac{3.7}{13.5} 3.7$$

$$\frac{15.0}{100} \frac{11.0}{51} \frac{6.9}{29} \frac{4.5}{19} \frac{4.6}{13.5} 4.5$$

2"G"

$$\frac{5.4}{248} \frac{5.6}{230} \frac{9.0}{220} \frac{7.2}{193} \frac{6.0}{174}$$

$$\frac{6.1}{261} \frac{6.7}{244} \frac{11.2}{235} \frac{10.6}{208} \frac{10.3}{195} \frac{9.5}{180}$$

N.E. corner monument

E MVR"

$$\frac{8.7}{304} \frac{9.0}{276} \frac{12.8}{267} \frac{11.7}{250} \frac{13.1}{227} \frac{12.5}{212} \frac{11.9}{191} \frac{10.3}{171}$$

2" MVR"

$$\frac{9.3}{284} \frac{10.0}{266} \frac{13.4}{253} \frac{13.6}{230} \frac{13.3}{200} \frac{10.9}{168} \frac{9.9}{162} \frac{9.3}{138}$$

2" MVR"

$$\frac{9.5}{263} \frac{9.7}{250} \frac{14.5}{240} \frac{13.5}{200} \frac{11.5}{163} \frac{9.8}{144}$$

2" MVR"

$$\frac{9.1}{230} \frac{9.3}{214} \frac{11.7}{208} \frac{13.0}{200} \frac{12.8}{183} \frac{11.3}{165} \frac{10.1}{128}$$

2" MVR"

$$\frac{8.4}{185} \frac{8.9}{170} \frac{11.6}{161} \frac{11.3}{148} \frac{10.0}{142} \frac{9.7}{127} \frac{8.3}{115}$$

spike in P.P. Lt & Co. Rd. "G"

Sounding #1 = 35' Lt Sta. 0+80

0+00 To 4.5 = Dry Sandy Dirt

4.5 To 6.0 = Gravel with 20% Clay.

Sounding #2 = 35' Lt Sta. 1+00

0+00 To 2.0 Dry Sandy Dirt

2.0 To 3.5 Gravel + Clay. Clay 20%

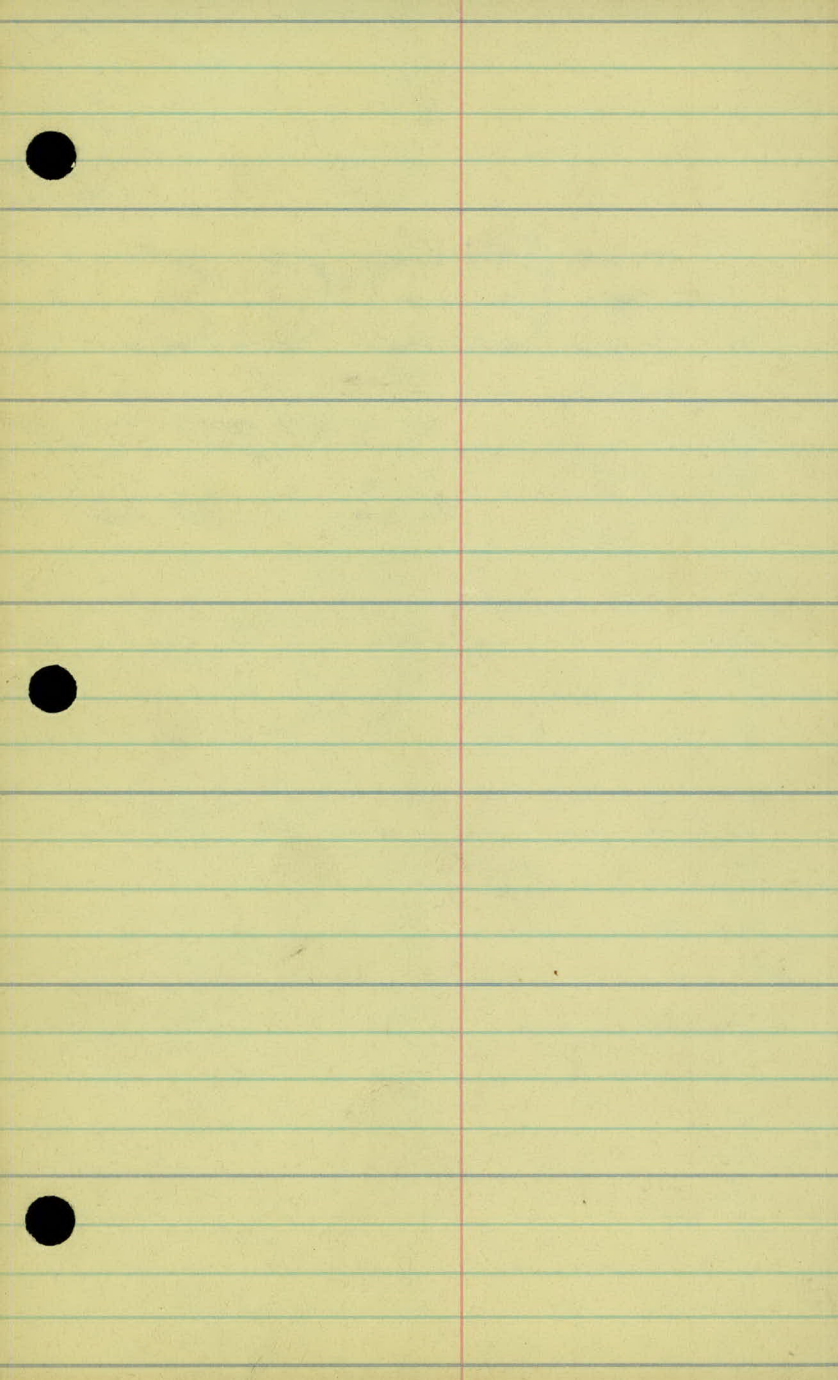
3.5 To 5.0 Clay + Gravel Clay 60%

Sounding #3 = 65' Lt Sta. 1+00

0+00 To 2.5 Dry Sandy Dirt

2.5 To 7.0 Very Fine Sand.

7.0 To 9.5 Clay + Gravel. Clay 80%



Sta.	+	H.I.	-	Elev.
B.M.	5.06	105.06		100.00 (Assumed.)
0+00				

+20

+35

+42

B.M.	8.00	108.00	5.06	100.00
------	------	--------	------	--------

+50

1+00

+50

2+00

B.M.			8.00	100.00
------	--	--	------	--------

Σ

Spike in P.P.N.E. cor. Int. Rice C.Rd. & L.H. Rd.

4.7 $\frac{6.2}{71}$ $\frac{7.2}{100}$ $\frac{8.6}{121}$ $\frac{9.5}{155}$ $\frac{11.1}{200}$

4.0 $\frac{4.3}{21}$ $\frac{5.2}{51}$ $\frac{5.3}{84}$ $\frac{5.6}{100}$ $\frac{6.5}{132}$ $\frac{7.9}{144}$ $\frac{8.4}{162}$ $\frac{7.5}{167}$ $\frac{8.4}{200}$

3.9 $\frac{4.1}{7}$ $\frac{5.6}{22}$ $\frac{6.5}{26}$ $\frac{7.0}{37}$ $\frac{6.9}{66}$ $\frac{5.8}{81}$ $\frac{6.0}{100}$ $\frac{6.0}{135}$ $\frac{7.1}{178}$ $\frac{9.1}{200}$

3.8 $\frac{4.8}{16}$ $\frac{5.9}{19}$ $\frac{6.7}{25}$ $\frac{2.2}{31}$ $\frac{1.5}{44}$ $\frac{4.4}{57}$ $\frac{6.2}{69}$ $\frac{7.2}{90}$ $\frac{6.0}{100}$ $\frac{6.5}{126}$ $\frac{6.4}{157}$ $\frac{7.4}{200}$

6.7 $\frac{7.6}{13}$ $\frac{8.0}{18}$ $\frac{9.2}{22}$ $\frac{2.0}{30}$ $\frac{4.8}{73}$ $\frac{10.0}{93}$ $\frac{10.5}{100}$ $\frac{10.5}{115}$ $\frac{9.3}{130}$ $\frac{9.8}{181}$ $\frac{10.3}{200}$

6.1 $\frac{6.6}{12}$ $\frac{8.4}{17}$ $\frac{7.3}{19}$ $\frac{2.4}{30}$ $\frac{2.7}{58}$ $\frac{4.1}{73}$ $\frac{5.4}{100}$ $\frac{8.1}{138}$ $\frac{10.0}{178}$ $\frac{9.7}{186}$ $\frac{10.5}{189}$ $\frac{11.2}{200}$

4.9 $\frac{4.7}{10}$ $\frac{8.0}{17}$ $\frac{6.8}{19}$ $\frac{3.7}{25}$ $\frac{3.9}{41}$ $\frac{4.4}{78}$ $\frac{5.6}{100}$ $\frac{6.9}{129}$ $\frac{9.3}{159}$ $\frac{11.4}{183}$ $\frac{12.2}{186}$ $\frac{13.2}{200}$

4.0 $\frac{3.8}{10}$ $\frac{7.9}{18}$ $\frac{6.0}{21}$ $\frac{5.1}{32}$ $\frac{4.1}{70}$ $\frac{4.6}{100}$ $\frac{6.9}{150}$ $\frac{9.9}{188}$ $\frac{11.2}{200}$

Base line = Rice Creek Road.

Sounding #1 = 33' Rt. Sta. 0+50

0+00 To 2.5 = Fine sand and Dirt

2.5 To 8.0 = yellow Clay and Gravel

Sounding #2 = 73' Rt. Sta. 0+50

0+00 To 2.5 = Fine Sand + Dirt

2.5 To 6.0 = yellow Clay + Gravel

Sounding #3 = 33' Rt. Sta. 1+00

0+00 To 4.0 Fine sand and Dirt

4.0 To 5 yellow Clay and Gravel.

5.0 To 6.0 Blue Clay + Gravel

6.0 To 7.5 yellow Clay + Gravel

Sounding #4 = 60' Rt. Sta. 1+00

0+00 To 3.0 Fine Sand + Dirt

3.0 To 3.5 yellow Clay + Sand

3.5 To 4.5 Course Sand

4.5 To 10.0 yellow Clay + Gravel. Clay, 80%

Sounding #5 = 130' Rt. Sta. 1+00

0+00 To 4.0 Fine Sand + Dirt

4.0 To 6.0 Blue Clay + Gravel

#6

Sounding #200 = 70' Rt. Sta. 1+00

0+00 To 1.0 Black Loam

1.0 To 4.5 Fine yellow sand wet.

4.5 To 7.0 Blue Clay + Gravel 80% Clay.

Sounding #7 = 200' Rt Sta. 2+00

0 To 2.0 Black Loam

2.0 To 3.5 Blue Clay & Gravel

3.5 To 5.5 Coarse yellow sand. (wet.)

5.5 To 7.0 Blue Clay & Gravel

Very Wet at 4.5

Sounding #8 = 150' Rt Sta. 2+00

0 To 2.5 Fine sand + Dirt (mix)

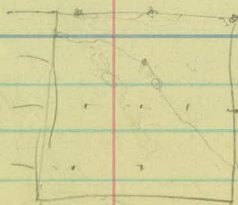
2.5 To 7.5 yellow Clay & Gravel (mix)

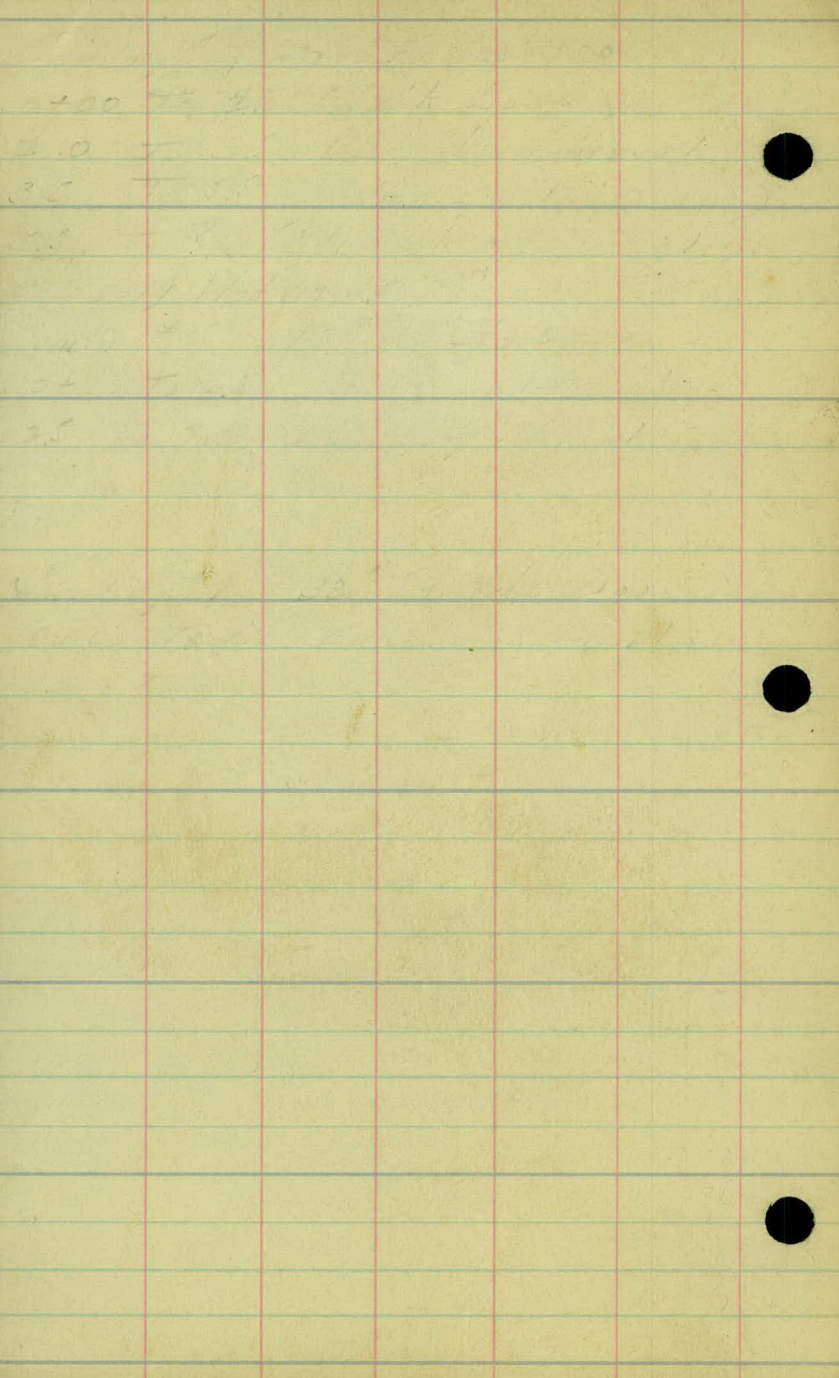
Sounding #9 = 33' Rt Sta. 2+00

0 To 1.0 = Fine sand + Dirt (mix)

1.0 To 7.5 Wet Fine sand.

7.5 To 9.5 Blue Clay & Gravel. (very wet)





- 0+00 to 3+00 - Cl. + Gr. Lt. + Rt. ✓
 3+50 to 9+00 - " " " " ✓
 5+65 - P-24" P₃ 42' - H.D. 10 C.Y. ✓
 7+70 - Rt. - 15'x20' C.M. ✓
 Special ditch on Lt. - Sta. 5+50 to 8+00. ✓
 11+50 to 15+50 Lt. - Gr. ✓
 23+98 - Remove - P 24" P₃ 42' - H.D. 10 C.Y. ✓
 16+00 to 20+50 - Rt. Cl. + Gr. ✓
 26+64 - Lt. - No culv. req. ✓
 26+64 - Rt. " " " ✓
 29+53 - Rt. " " " ✓
 Check flow lines of culv's. between 30 and 31
 and connect. H.D. Check old culv. ✓
 31+00 to 35+50 Rt. Cl. + Gr. ✓
 33+00 Lt. - P 15'x20' C.M. ✓
 33+00 Rt. - P. " " ✓
~~39 42+40~~ Rt. No culv. req. Rep. 12'x20' from ✓
 43+00 to 43+50 - Gr. minimum. ✓
 46+18 - Remove - P-24" P₃ - 42' H.D. 10 C.Y. ✓

