

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

_____ Co. Rd "H" _____

From Monnds View Rd To 1318' East.

Road Acc't. No. M-2 _____

Date Filed _____

File _____

BK 25 PR 11A

Plan Survey
Co Rd "H"
From Mounds View Rd To 1318' East

Survey started
6/29/40
Completed
7-1-40

Index
Alignment 1-2
Topog 3-5
Bench Levels 6-7
Cross Sections 8-11

R.O.P.
HAW "Pops"
A.L.M.
D.G.
C.F.

Worked up
July 6-1940

Sta	Pt	Angle	
		Lt	Rt

13+17.80

6+00

0+00

12" Twin Oak

17.20'

A395'

Fe Post

Iron

SE Cor of SW 1/4 of
SE 1/4 Sec 9-30-23

Fe Post

2 1/2 Hub

Mon +

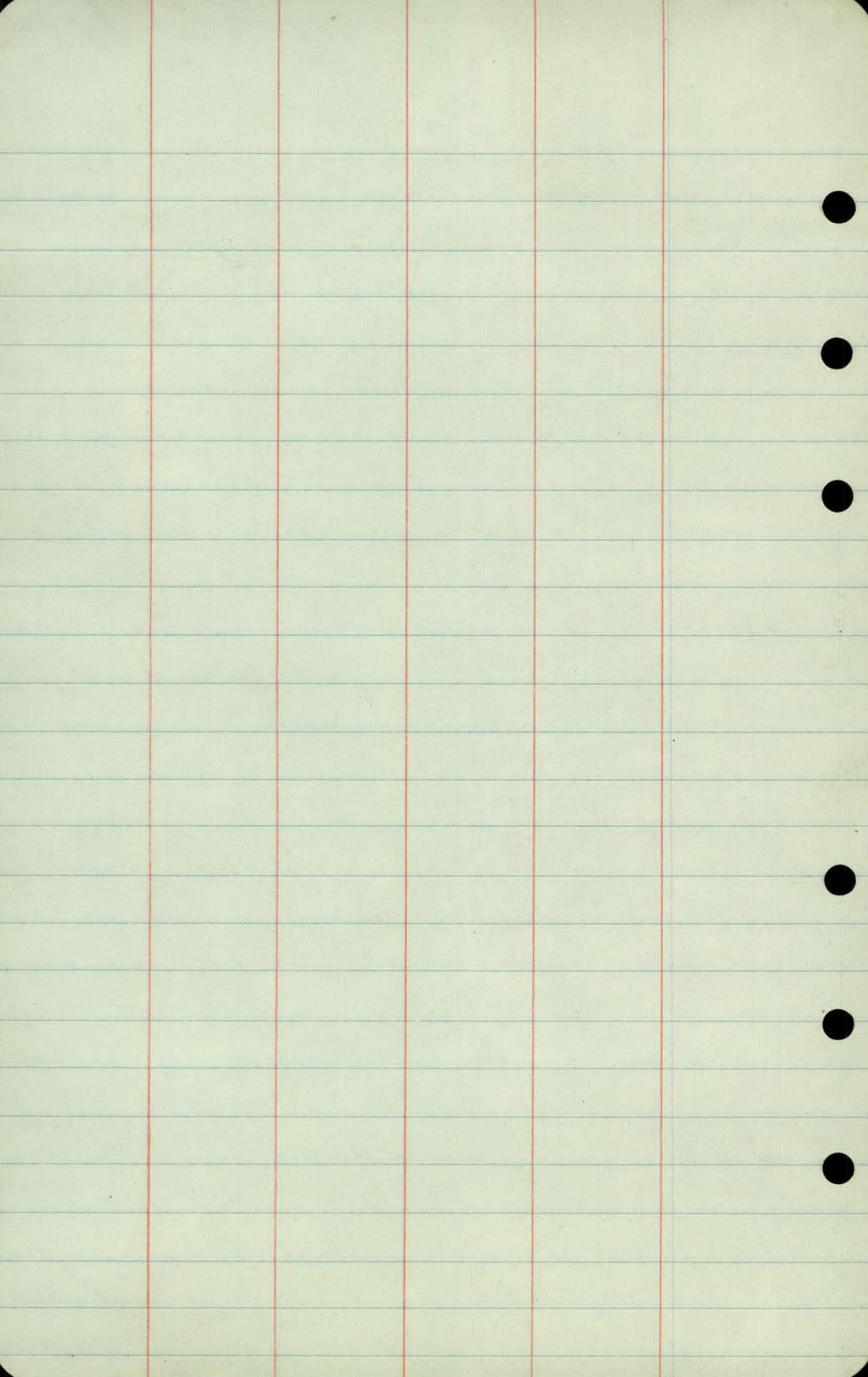
S. 1/4 Cor Sec 9-30-23

Let Iron

37.80'

15.08'

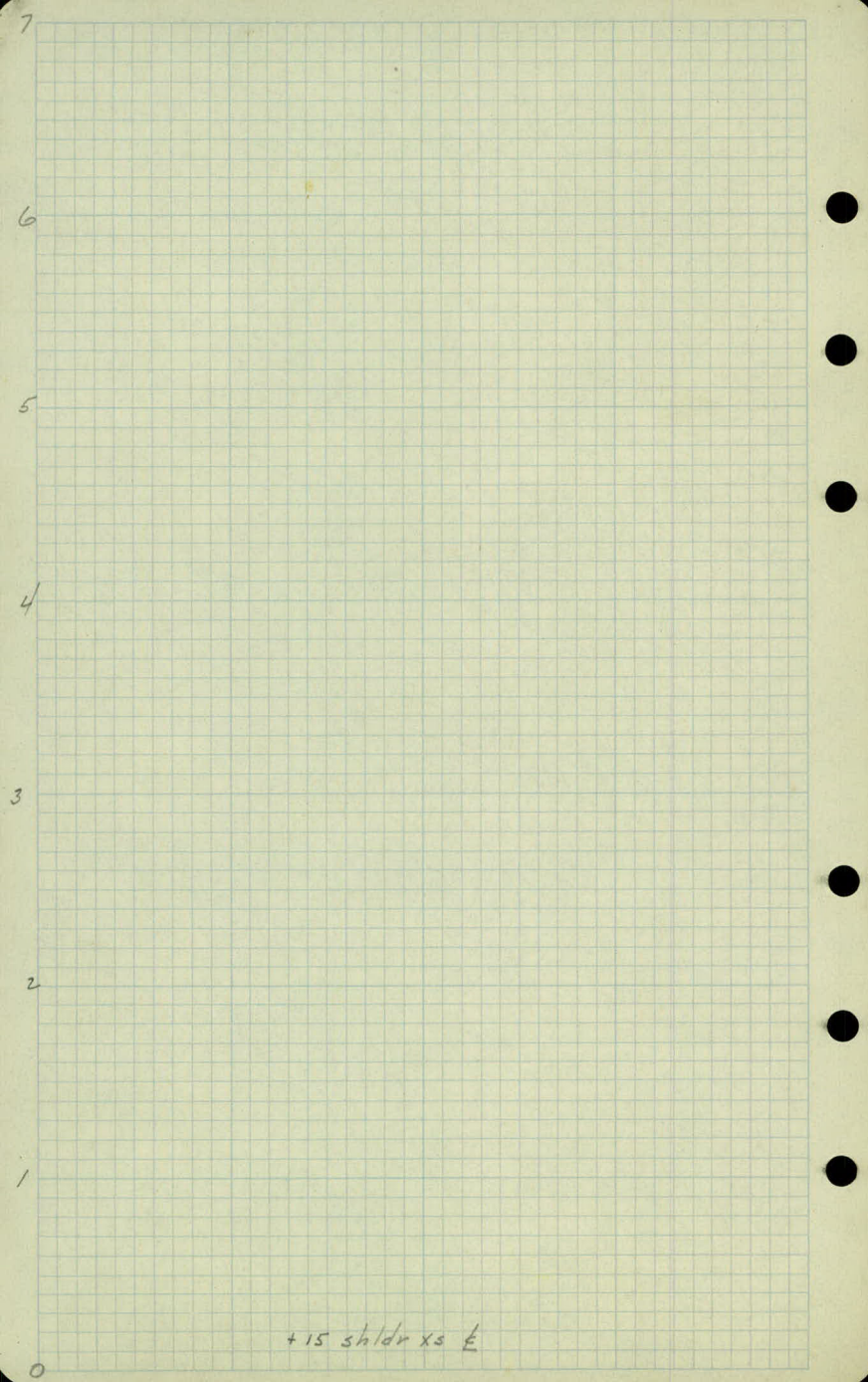
School



Topography

Co. Rd. "H"

from Mounds View Rd.
1/4 mi. East.



+ 15 shldr xs £

+50 End Cult. —————

Cultivated

Cultivated

+62 Bag Cult. —————

Hay Field

+60 Bag Cult.

Hay Field

+21 PP 02'

—————
MOUNDS VIEW ROAD.

14

3

12

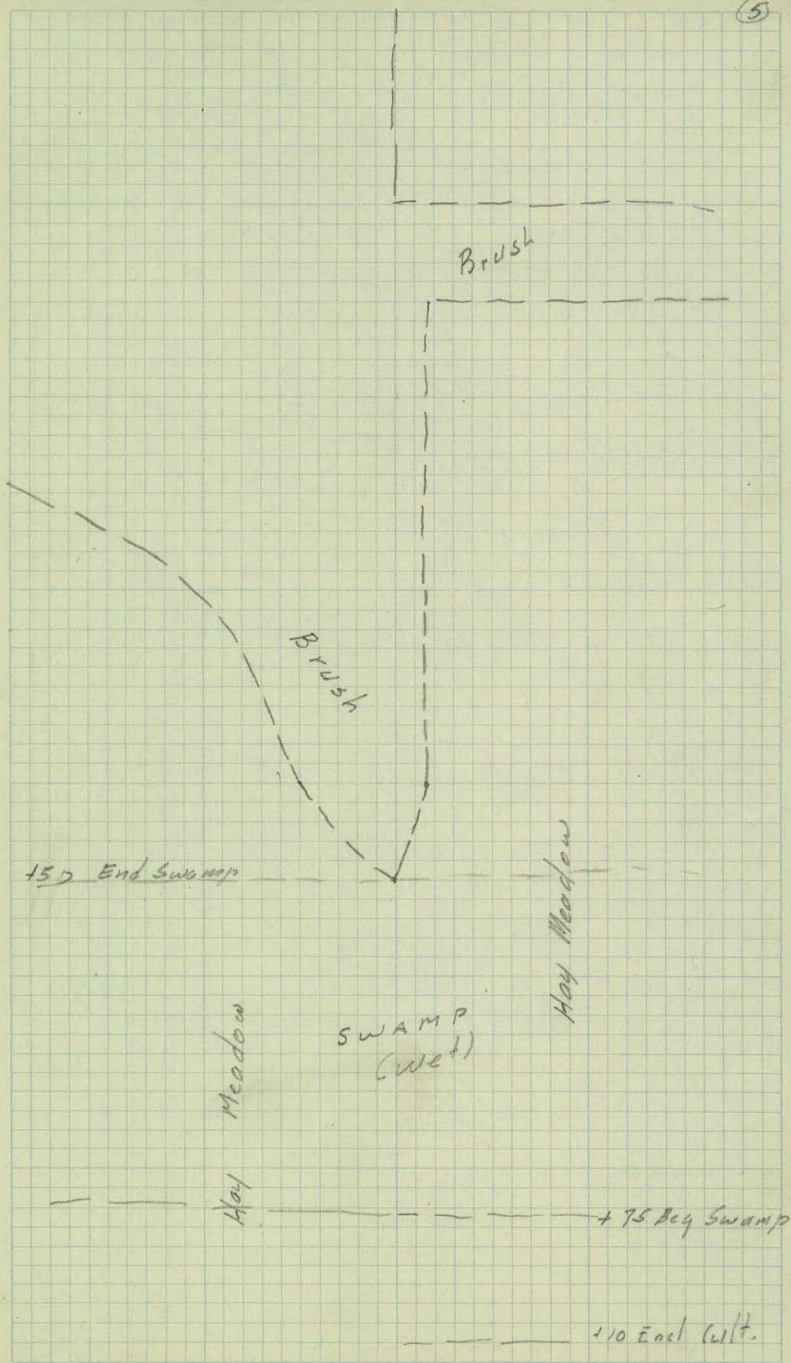
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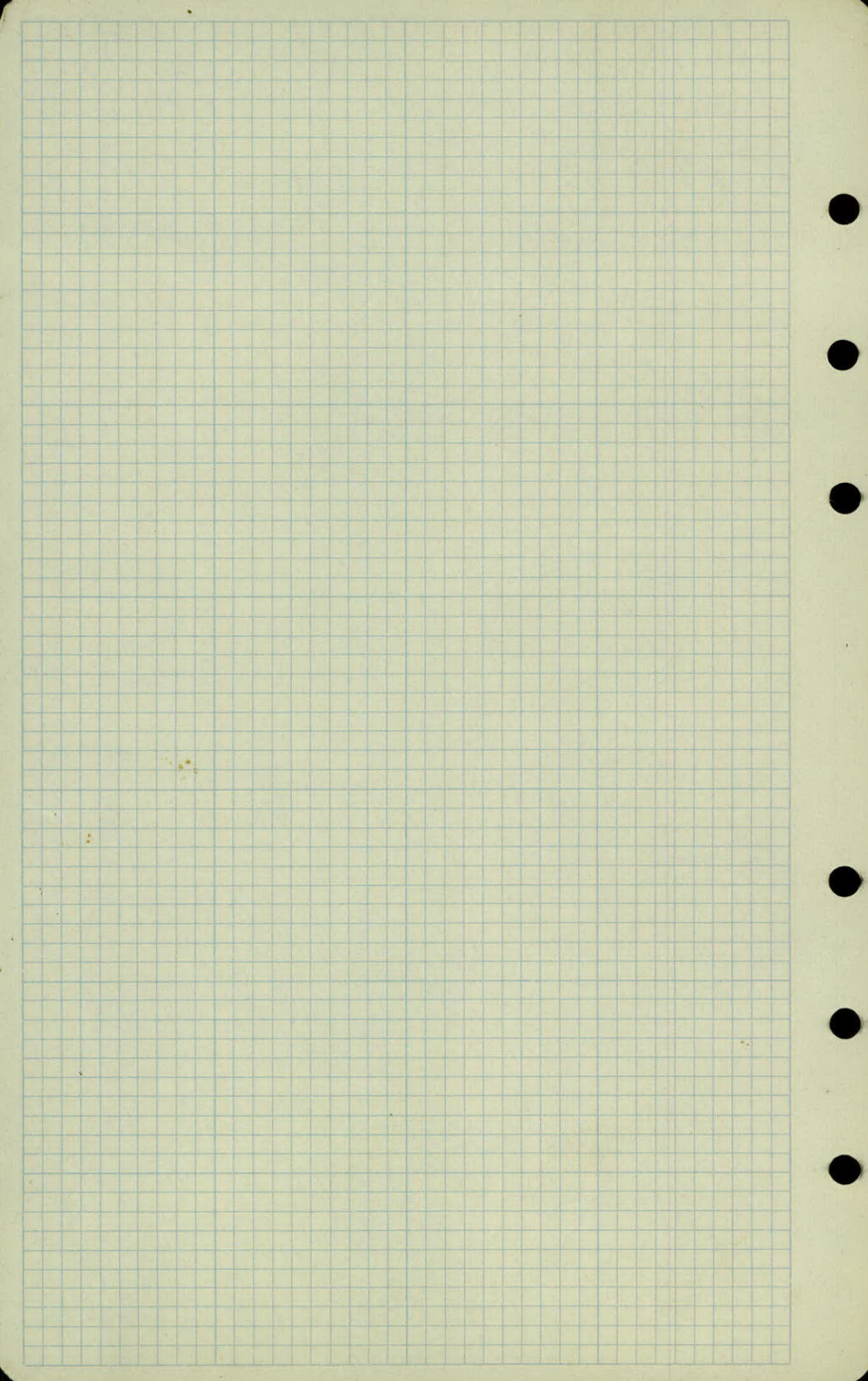
10

9

8

7





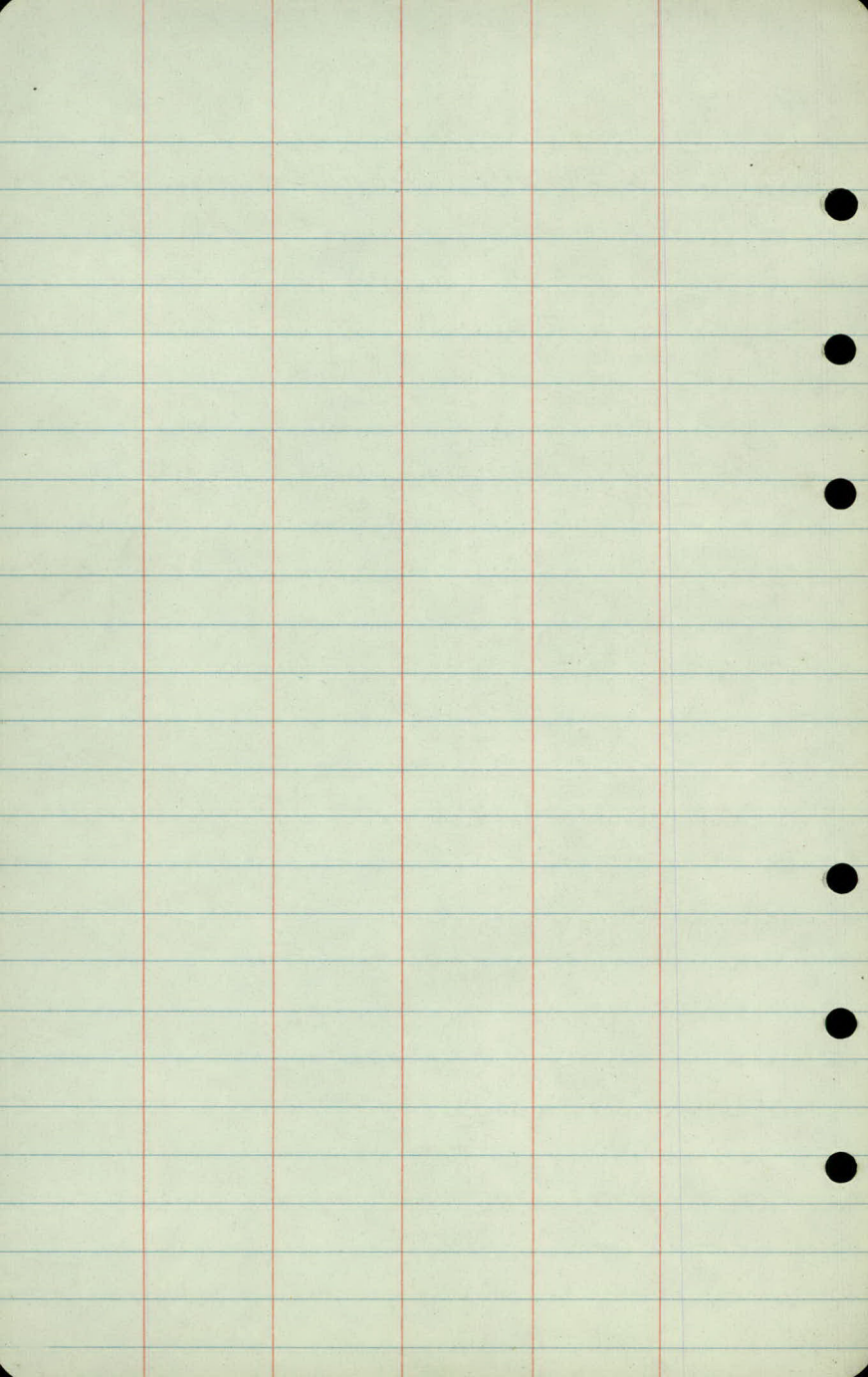
Berish Levels

Sta	+	π	-	Elev
B.M.	6.29	904.84		898.55
	12.31	915.29	1.86	902.98
	6.22	911.57	994	905.35
	13.61	924.95	0.23	911.34
	12.71	936.77	0.89	924.06
	13.10	949.53	0.34	936.43
B.M.			0.34	949.19

Description

N.E. Cor. Bottom Step School Ho. S.W. Cor. Co Rd H + M.V. Rd.

Spk in 15" Window 1' Lt Sta 13+30



CROSS SECTIONS

Co. Rd. "H"

from Mdse View Rd

1/4 Mile East

Sta	+	π	-	Elev
B.M	7.89	906.44.		898.55
0+00	1/2 Mounds View Rd. 95			96.9
+15			10.2	96.2
+20			1.4	95.0
+23			10.6	95.8
+50			10.6	95.8
1			12.3	94.1
+50			11.8	94.6
2			9.1	97.3
+50			20	99.4
3			45	01.9
+50			16	04.8
T.P	11.32	916.05	1.71	904.73
4			8.4	07.7

N.E. Cor. Bottom Step School House

$$\frac{10.5}{50} \quad 9.5 \quad \frac{9.2}{50}$$

$$\frac{10.7}{50} \quad 10.2 \quad \frac{9.3}{50}$$

$$\frac{12.0}{50} \quad 11.4 \quad \frac{11.4}{5} \quad \frac{11.5}{50}$$

$$\frac{11.0}{50} \quad 10.6 \quad \frac{10.9}{50}$$

$$\frac{11.4}{50} \quad \frac{11.3}{33} \quad \frac{10.7}{8} \quad \frac{10.2}{4} \quad \frac{10.6}{3} \quad 10.6 \quad \frac{10.4}{9} \quad \frac{10.7}{13} \quad \frac{11.1}{32} \quad \frac{11.0}{50}$$

$$\frac{13.3}{50} \quad \frac{12.9}{29} \quad \frac{12.2}{7} \quad \frac{11.8}{2} \quad 12.3 \quad \frac{11.9}{29} \quad 11.9 \quad \frac{11.6}{50}$$

$$\frac{13.5}{50} \quad \frac{12.4}{28} \quad \frac{11.5}{8} \quad 11.8 \quad \frac{10.2}{8} \quad \frac{9.0}{50}$$

$$\frac{11.6}{50} \quad \frac{10.8}{27} \quad 9.1 \quad \frac{8.8}{19} \quad \frac{8.0}{50}$$

$$\frac{8.6}{50} \quad \frac{8.5}{30} \quad \frac{7.1}{7} \quad \frac{6.6}{4} \quad 7.0 \quad \frac{7.3}{7} \quad \frac{6.4}{33} \quad \frac{5.4}{50}$$

$$\frac{6.7}{50} \quad \frac{6.5}{32} \quad \frac{5.1}{10} \quad \frac{4.1}{2} \quad 4.5 \quad \frac{4.6}{30} \quad \frac{3.9}{50}$$

$$\frac{3.8}{50} \quad \frac{3.1}{25} \quad \frac{2.2}{9} \quad \frac{1.1}{3} \quad 1.6 \quad \frac{2.3}{17} \quad \frac{0.9}{50}$$

$$\frac{11.1}{50} \quad \frac{10.4}{29} \quad \frac{8.6}{7} \quad \frac{8.0}{4} \quad 8.4 \quad \frac{8.9}{6} \quad \frac{8.9}{27} \quad \frac{8.3}{50}$$

Sta	+	π	-	Elev
		916.05		
+50			5.9	10.2
			4.7	11.4
+50			4.9	11.2
			5.4	10.7
+50			7.0	09.1
			12.0	04.1
T.P.	256	907.92	10.69	905.36
+50			9.6	98.3
+75			12.1	95.8
			12.3	95.6
+50			13.0	94.9
			11.8	96.1
+50			9.1	98.8
T.P.	12.65	916.99	3.58	904.3d

$$\begin{array}{r} 9.5 \\ 50 \end{array} \quad \begin{array}{r} 8.9 \\ 30 \end{array} \quad \begin{array}{r} 6.4 \\ 9 \end{array} \quad \begin{array}{r} 5.4 \\ 5 \end{array} \quad 5.9 \quad \begin{array}{r} 6.5 \\ 5 \end{array} \quad \begin{array}{r} 6.4 \\ 32 \end{array} \quad \begin{array}{r} 5.6 \\ 50 \end{array}$$

$$\begin{array}{r} 8.0 \\ 50 \end{array} \quad \begin{array}{r} 7.2 \\ 31 \end{array} \quad \begin{array}{r} 5.0 \\ 7 \end{array} \quad \begin{array}{r} 4.1 \\ 5 \end{array} \quad 4.7 \quad \begin{array}{r} 5.2 \\ 5 \end{array} \quad \begin{array}{r} 4.9 \\ 26 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array}$$

$$\begin{array}{r} 8.5 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 36 \end{array} \quad \begin{array}{r} 5.2 \\ 8 \end{array} \quad \begin{array}{r} 4.5 \\ 5 \end{array} \quad 4.9 \quad \begin{array}{r} 5.5 \\ 5 \end{array} \quad \begin{array}{r} 5.3 \\ 32 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array}$$

$$\begin{array}{r} 10.5 \\ 50 \end{array} \quad \begin{array}{r} 8.1 \\ 29 \end{array} \quad \begin{array}{r} 6.1 \\ 11 \end{array} \quad \begin{array}{r} 4.9 \\ 7 \end{array} \quad \begin{array}{r} 4.7 \\ 3 \end{array} \quad 5.4 \quad \begin{array}{r} 5.9 \\ 5 \end{array} \quad \begin{array}{r} 6.1 \\ 26 \end{array} \quad \begin{array}{r} 5.4 \\ 50 \end{array}$$

$$\begin{array}{r} 12.9 \\ 50 \end{array} \quad \begin{array}{r} 11.6 \\ 32 \end{array} \quad \begin{array}{r} 8.5 \\ 14 \end{array} \quad \begin{array}{r} 6.6 \\ 7 \end{array} \quad \begin{array}{r} 6.5 \\ 3 \end{array} \quad 7.0 \quad \begin{array}{r} 7.5 \\ 4 \end{array} \quad \begin{array}{r} 7.2 \\ 22 \end{array} \quad \begin{array}{r} 6.2 \\ 44 \end{array} \quad \begin{array}{r} 6.5 \\ 50 \end{array}$$

$$\begin{array}{r} 15.7 \\ 50 \end{array} \quad \begin{array}{r} 14.6 \\ 26 \end{array} \quad \begin{array}{r} 12.3 \\ 4 \end{array} \quad 12.0 \quad \begin{array}{r} 12.1 \\ 24 \end{array} \quad \begin{array}{r} 11.7 \\ 50 \end{array}$$

$$\begin{array}{r} 12.4 \\ 50 \end{array} \quad \begin{array}{r} 11.2 \\ 21 \end{array} \quad \begin{array}{r} 10.0 \\ 3 \end{array} \quad 9.6 \quad \begin{array}{r} 9.2 \\ 14 \end{array} \quad \begin{array}{r} 7.9 \\ 50 \end{array}$$

$$\begin{array}{r} 12.7 \\ 50 \end{array} \quad \begin{array}{r} 12.4 \\ 26 \end{array} \quad 12.1 \quad \begin{array}{r} 12.0 \\ 33 \end{array} \quad \begin{array}{r} 11.1 \\ 50 \end{array}$$

$$\begin{array}{r} 13.1 \\ 50 \end{array} \quad \begin{array}{r} 12.8 \\ 24 \end{array} \quad 12.3 \quad \begin{array}{r} 12.6 \\ 20 \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array}$$

Suggest E
Culvert
Drainage to North

$$\begin{array}{r} 13.3 \\ 50 \end{array} \quad \begin{array}{r} 13.3 \\ 25 \end{array} \quad 13.0 \quad \begin{array}{r} 13.0 \\ 27 \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array}$$

$$\begin{array}{r} 13.3 \\ 50 \end{array} \quad \begin{array}{r} 13.1 \\ 27 \end{array} \quad 11.8 \quad \begin{array}{r} 12.0 \\ 19 \end{array} \quad \begin{array}{r} 12.4 \\ 50 \end{array}$$

$$\begin{array}{r} 12.9 \\ 50 \end{array} \quad \begin{array}{r} 11.9 \\ 28 \end{array} \quad 9.1 \quad \begin{array}{r} 8.2 \\ 5 \end{array} \quad \begin{array}{r} 8.2 \\ 25 \end{array} \quad \begin{array}{r} 8.7 \\ 50 \end{array}$$

Sta	+	π	-	Elev.
		916.99		
10			140	03.0
+50			89	08.1
T.P.	12.74	923.10	663	910.36
11			9.7	13.4
+50			3.0	20.1
T.P.	12.66	935.33	0.43	922.67
12			7.8	27.5
+27			3.1	32.2
T.P.	13.74	947.72	1.35	933.98
+50			10.1	37.6
+80			6.8	40.9
13			43	43.4
+17			2.2	45.5
T.P.	4.93	950.92	1.73	945.99
B.M.			1.70	949.22
				949.19

$$\begin{array}{r} 18.5 \\ 50 \end{array} \quad \begin{array}{r} 16.5 \\ 27 \end{array} \quad \begin{array}{r} 15.5 \\ 18 \end{array} \quad \begin{array}{r} 14.8 \\ 10 \end{array} \quad \begin{array}{r} 14.0 \\ 14.0 \end{array} \quad \begin{array}{r} 12.5 \\ 6 \end{array} \quad \begin{array}{r} 13.0 \\ 23 \end{array} \quad \begin{array}{r} 12.0 \\ 50 \end{array}$$

$$\begin{array}{r} 13.9 \\ 50 \end{array} \quad \begin{array}{r} 12.1 \\ 25 \end{array} \quad \begin{array}{r} 9.9 \\ 10 \end{array} \quad \begin{array}{r} 8.9 \\ 8.9 \end{array} \quad \begin{array}{r} 6.9 \\ 8 \end{array} \quad \begin{array}{r} 7.2 \\ 17 \end{array} \quad \begin{array}{r} 8.4 \\ 21 \end{array} \quad \begin{array}{r} 7.4 \\ 50 \end{array}$$

$$\begin{array}{r} 14.7 \\ 50 \end{array} \quad \begin{array}{r} 14.0 \\ 43 \end{array} \quad \begin{array}{r} 11.7 \\ 21 \end{array} \quad \begin{array}{r} 10.7 \\ 6 \end{array} \quad \begin{array}{r} 9.7 \\ 9.7 \end{array} \quad \begin{array}{r} 8.8 \\ 4 \end{array} \quad \begin{array}{r} 7.2 \\ 11 \end{array} \quad \begin{array}{r} 7.2 \\ 15 \end{array} \quad \begin{array}{r} 7.2 \\ 22 \end{array} \quad \begin{array}{r} 9.9 \\ 26.29 \end{array} \quad \begin{array}{r} 8.0 \\ 31 \end{array} \quad \begin{array}{r} 8.7 \\ 50 \end{array}$$

$$\begin{array}{r} 6.5 \\ 50 \end{array} \quad \begin{array}{r} 5.5 \\ 41 \end{array} \quad \begin{array}{r} 4.5 \\ 21 \end{array} \quad \begin{array}{r} 3.5 \\ 3 \end{array} \quad \begin{array}{r} 3.0 \\ 3.0 \end{array} \quad \begin{array}{r} 2.6 \\ 4 \end{array} \quad \begin{array}{r} 2.3 \\ 13 \end{array} \quad \begin{array}{r} 2.6 \\ 23 \end{array} \quad \begin{array}{r} 3.7 \\ 25.28 \end{array} \quad \begin{array}{r} 2.8 \\ 29 \end{array} \quad \begin{array}{r} 1.5 \\ 50 \end{array}$$

$$\begin{array}{r} 8.2 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 30 \end{array} \quad \begin{array}{r} 7.7 \\ 9 \end{array} \quad \begin{array}{r} 7.8 \\ 7.8 \end{array} \quad \begin{array}{r} 8.2 \\ 8 \end{array} \quad \begin{array}{r} 9.6 \\ 14 \end{array} \quad \begin{array}{r} 9.3 \\ 27 \end{array} \quad \begin{array}{r} 8.7 \\ 28 \end{array} \quad \begin{array}{r} 7.3 \\ 50 \end{array}$$

$$\begin{array}{r} 5.1 \\ 50 \end{array} \quad \begin{array}{r} 4.1 \\ 22 \end{array} \quad \begin{array}{r} 3.0 \\ 11 \end{array} \quad \begin{array}{r} 3.1 \\ 3.1 \end{array} \quad \begin{array}{r} 3.4 \\ 11 \end{array} \quad \begin{array}{r} 4.6 \\ 22 \end{array} \quad \begin{array}{r} 3.6 \\ 36 \end{array} \quad \begin{array}{r} 1.1 \\ 50 \end{array}$$

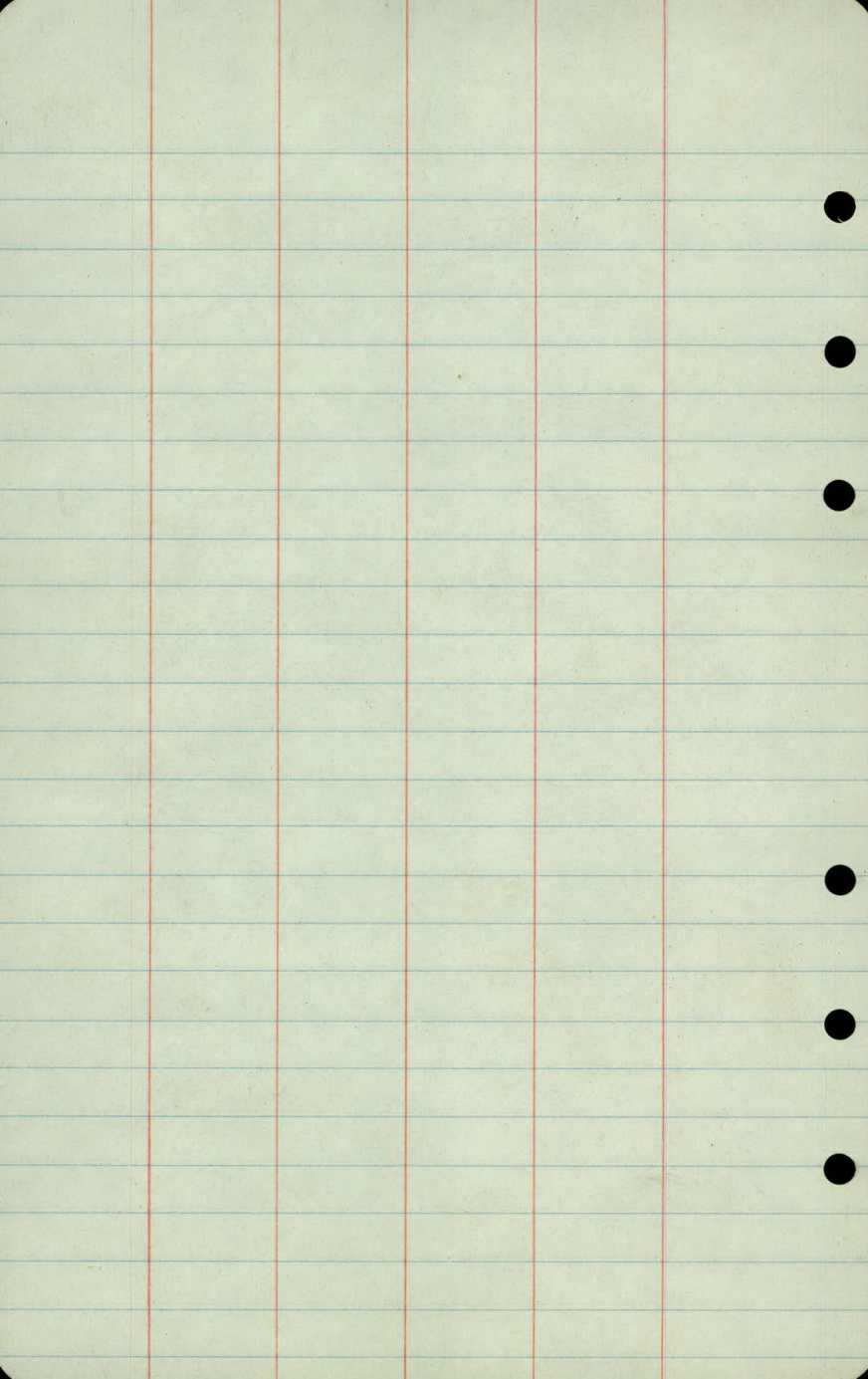
$$\begin{array}{r} 11.5 \\ 50 \end{array} \quad \begin{array}{r} 8.4 \\ 20 \end{array} \quad \begin{array}{r} 8.5 \\ 8 \end{array} \quad \begin{array}{r} 9.4 \\ 4 \end{array} \quad \begin{array}{r} 10.1 \\ 10.1 \end{array} \quad \begin{array}{r} 10.8 \\ 3 \end{array} \quad \begin{array}{r} 12.2 \\ 8 \end{array} \quad \begin{array}{r} 13.8 \\ 21 \end{array} \quad \begin{array}{r} 12.6 \\ 50 \end{array}$$

$$\begin{array}{r} 7.0 \\ 50 \end{array} \quad \begin{array}{r} 3.8 \\ 34 \end{array} \quad \begin{array}{r} 2.7 \\ 24 \end{array} \quad \begin{array}{r} 3.6 \\ 12 \end{array} \quad \begin{array}{r} 5.4 \\ 7 \end{array} \quad \begin{array}{r} 6.8 \\ 6.8 \end{array} \quad \begin{array}{r} 7.7 \\ 5 \end{array} \quad \begin{array}{r} 8.4 \\ 16 \end{array} \quad \begin{array}{r} 9.5 \\ 25 \end{array} \quad \begin{array}{r} 10.3 \\ 50 \end{array}$$

$$\begin{array}{r} +7.7 \\ 50 \end{array} \quad \begin{array}{r} 7.5 \\ 32 \end{array} \quad \begin{array}{r} +5.7 \\ 19 \end{array} \quad \begin{array}{r} 2.0 \\ 11 \end{array} \quad \begin{array}{r} 3.5 \\ 5 \end{array} \quad \begin{array}{r} 4.3 \\ 4.3 \end{array} \quad \begin{array}{r} 5.0 \\ 5 \end{array} \quad \begin{array}{r} 5.3 \\ 11 \end{array} \quad \begin{array}{r} 8.3 \\ 33 \end{array} \quad \begin{array}{r} 7.8 \\ 50 \end{array}$$

$$\begin{array}{r} +8.0 \\ 50 \end{array} \quad \begin{array}{r} +5.5 \\ 56 \end{array} \quad \begin{array}{r} +0.5 \\ 15 \end{array} \quad \begin{array}{r} 1.6 \\ 2 \end{array} \quad \begin{array}{r} 2.2 \\ 2.2 \end{array} \quad \begin{array}{r} 2.2 \\ 2.2 \end{array} \quad \begin{array}{r} 2.2 \\ 50 \end{array}$$

Sph 15" Twin Oak 1' 6" 13' 30"



Additional Topog
Co. Rd. "H"

14

17-0-03

32

13

+99 Stump 4
+97 Stump 19
+85 Stump 21
12 +98 Stumps 6-34

122 Stump 2

+96 Stump 24-20
+95 Jr 3-5
+94 Stump 22
+84 Stump 9
+73 Stump 1

+99 2 Stump 14-25
+82 Stump 4
+71 Stump 6
+67 Stump 6
+63 2 Jr 17-20
+63 Stump 10
+62 Stump 5
11 +60 Stump 6

+91 2 Stump
+78-4 Stump
+64 Stump
+51 Stump
+43 Stump
+41 Stump

+78 1/2 Stump 4 Jr.

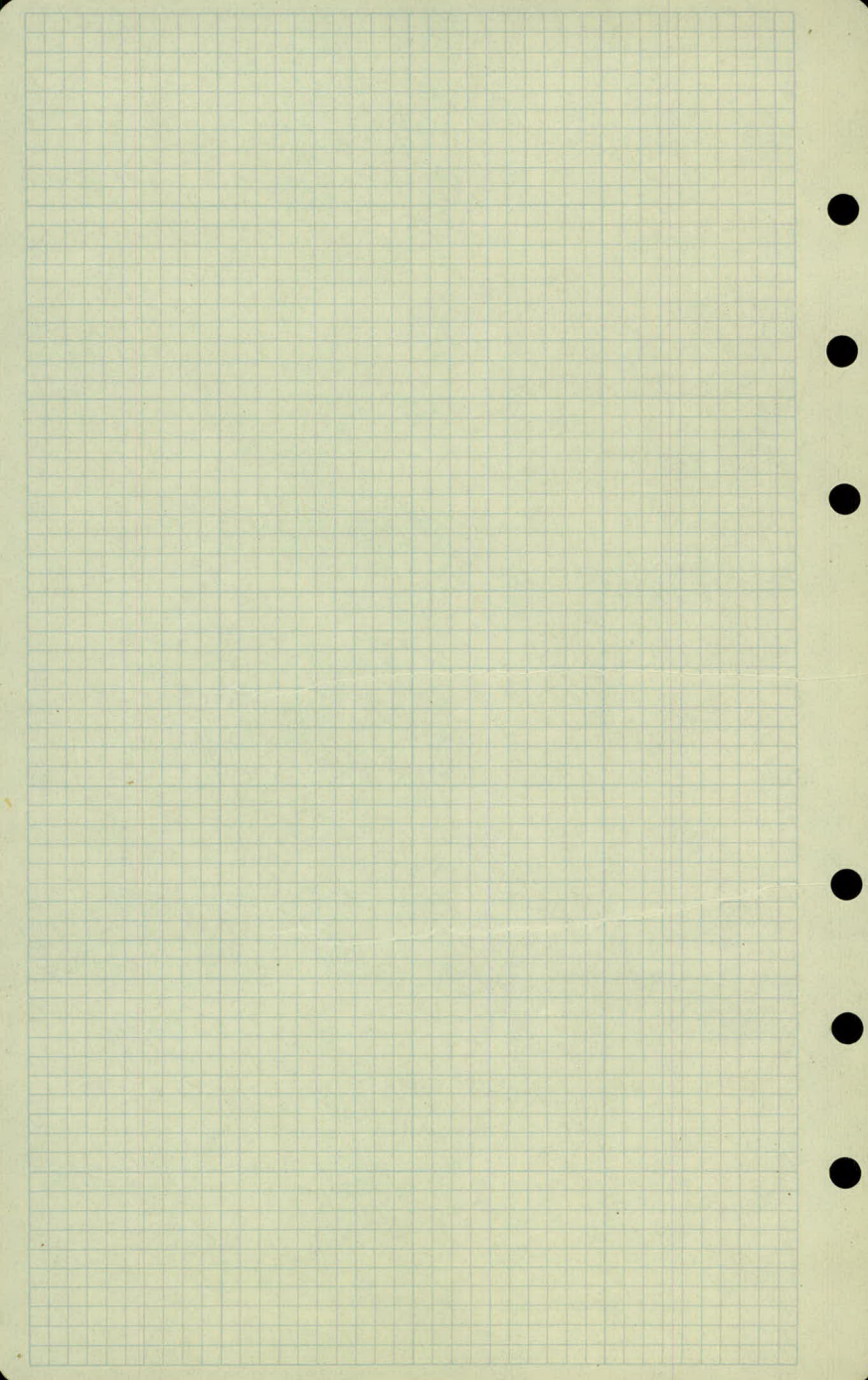
+47 Stump 1/2

+100 31
+95 4 Stump 5
10 +81 Stump 4-5

+95 3 Jr 2
+85 Stump 10
+83 Stump 8
+76 4 Jr 4
+63 2-4-8

+94 1/2
+78 1/2

9



SOUNDINGS

Co. Rd. "H"

sta.

struck
sand

$\frac{1}{2}$ " Rods - no point - Hand Push.

8+00

3'

+50

4'

+75

3'

9+00

2'

Slope Stake Notes
Co. Rd. "H"
Mdse. View Rd - 1150' East.

Staked - 8-13-40

4 Pages

Party.

ROP
AM
LG
CF

Sta	+	π	-	Elev	
B.M.	2.96	901.51		898.55	
0+15 x				96.7	
+20 x				96.7	
+23 x				96.7	
+50				96.6	4.9
1				96.4	5.1
+50				96.6	4.9
2				97.4	4.1
+50				99.0	2.5
T.P.	11.80	913.09	0.22	901.29	
3				01.2	11.9
+50				03.8	9.3
4				06.4	6.7
+50				08.5	4.6
5				09.5	3.6
T.P.	3.19	915.31	0.17	912.12	

Top Bottom Conc. Step N.E. Cor. Schl Ho.

$$\begin{array}{r} 6.0 \\ F1.1 \\ \hline 15.2 \end{array}$$

$$\begin{array}{r} 5.7 \\ F0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ F1.0 \\ \hline 15.0 \end{array}$$

$$\begin{array}{r} 7.8 \\ F2.7 \\ \hline 18.4 \end{array}$$

$$\begin{array}{r} 7.4 \\ F2.3 \\ \hline \end{array}$$

$$\begin{array}{r} 7.0 \\ F1.9 \\ \hline 16.8 \end{array}$$

$$\begin{array}{r} 6.9 \\ F2.0 \\ \hline 17.0 \end{array}$$

$$\begin{array}{r} 5.9 \\ F1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ DC0.4 \\ \hline 13.8 \end{array}$$

$$\begin{array}{r} 5.4 \\ F1.3 \\ \hline 15.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ C0.2 \\ \hline 15.0 \end{array}$$

$$\begin{array}{r} 2.9 \\ DC0.4 \\ \hline 13.8 \end{array}$$

$$\begin{array}{r} 2.0 \\ C0.5 \\ \hline \end{array}$$

$$\begin{array}{r} 1.9 \\ C0.6 \\ \hline 15.8 \end{array}$$

$$\begin{array}{r} 12.3 \\ DC0.4 \\ \hline 13.8 \end{array}$$

$$\begin{array}{r} 11.1 \\ C0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 11.5 \\ C0.4 \\ \hline 15.4 \end{array}$$

$$\begin{array}{r} 9.5 \\ DC0.6 \\ \hline 14.2 \end{array}$$

$$\begin{array}{r} 8.6 \\ C0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 8.9 \\ C0.5 \\ \hline 15.4 \end{array}$$

$$\begin{array}{r} 6.6 \\ C0.1 \\ \hline 14.8 \end{array}$$

$$\begin{array}{r} 5.3 \\ C1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.0 \\ C0.7 \\ \hline 16.0 \end{array}$$

$$\begin{array}{r} 4.2 \\ C0.4 \\ \hline 15.4 \end{array}$$

$$\begin{array}{r} 2.9 \\ C1.7 \\ \hline \end{array}$$

$$\begin{array}{r} 3.5 \\ C1.1 \\ \hline 16.8 \end{array}$$

$$\begin{array}{r} 2.8 \\ C0.8 \\ \hline 14.2 \end{array}$$

$$\begin{array}{r} 1.7 \\ C1.9 \\ \hline \end{array}$$

$$\begin{array}{r} 2.0 \\ C1.4 \\ \hline 17.8 \end{array}$$

Sta		π	-	Elev	
		915.31			
5+50				09.5	5.8
6				08.4	6.9
+50				06.3	9.0
7				03.1	12.2
T.P.	2.63	905.74	12.20	903.11	
+50				00.0	05.7
+75				99.0	06.7
8				98.3	07.4
+50				97.8	7.9
9				98.5	7.2
+50				00.6	5.1
10				03.9	1.8
T.P.	13.09	913.32	5.51	900.23	
+50				07.9	5.4
T.P.	8.59	919.86	2.05	911.27	

$$\begin{array}{r} 5.3 \\ 60.5 \\ \hline 15.6 \end{array}$$

$$\begin{array}{r} 4.2 \\ 61.6 \\ \hline \end{array}$$

$$\begin{array}{r} 4.7 \\ 61.1 \\ \hline 16.8 \end{array}$$

$$\begin{array}{r} 5.9 \\ 61.0 \\ \hline 16.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ 62.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ 61.5 \\ \hline 17.6 \end{array}$$

$$\begin{array}{r} 8.1 \\ 60.9 \\ \hline 16.4 \end{array}$$

$$\begin{array}{r} 6.2 \\ 62.8 \\ \hline \end{array}$$

$$\begin{array}{r} 6.6 \\ 62.6 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 12.8 \\ 60.2 \\ \hline 13.4 \end{array}$$

$$\begin{array}{r} 11.2 \\ 61.0 \\ \hline \end{array}$$

$$\begin{array}{r} 11.0 \\ 61.2 \\ \hline 17.0 \end{array}$$

$$\begin{array}{r} 9.0 \\ 63.3 \\ \hline 19.6 \end{array}$$

$$\begin{array}{r} 7.4 \\ 61.7 \\ \hline \end{array}$$

$$\begin{array}{r} 7.0 \\ 61.3 \\ \hline 15.6 \end{array}$$

$$\begin{array}{r} 10.1 \\ 63.4 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 9.9 \\ 63.2 \\ \hline \end{array}$$

$$\begin{array}{r} 9.9 \\ 63.2 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 10.6 \\ 63.2 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 10.1 \\ 62.7 \\ \hline \end{array}$$

$$\begin{array}{r} 10.3 \\ 62.9 \\ \hline 18.8 \end{array}$$

$$\begin{array}{r} 11.1 \\ 63.2 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 10.7 \\ 62.8 \\ \hline \end{array}$$

$$\begin{array}{r} 10.7 \\ 62.8 \\ \hline 18.6 \end{array}$$

$$\begin{array}{r} 10.6 \\ 63.4 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 9.6 \\ 62.4 \\ \hline \end{array}$$

$$\begin{array}{r} 9.7 \\ 62.5 \\ \hline 18.0 \end{array}$$

$$\begin{array}{r} 8.9 \\ 63.8 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 6.8 \\ 61.7 \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ 61.0 \\ \hline 15.0 \end{array}$$

$$\begin{array}{r} 4.5 \\ 62.7 \\ \hline 18.4 \end{array}$$

$$\begin{array}{r} 2.7 \\ 60.9 \\ \hline \end{array}$$

$$\begin{array}{r} 1.6 \\ 60.4 \\ \hline 15.4 \end{array}$$

$$\begin{array}{r} 7.3 \\ 61.9 \\ \hline 16.8 \end{array}$$

$$\begin{array}{r} 5.0 \\ 60.4 \\ \hline \end{array}$$

$$\begin{array}{r} 3.8 \\ 61.6 \\ \hline 17.8 \end{array}$$

Sta.	+	Σ	-	Elev	
		919.86			
11				12.8	7.1
T.P.	6.22	925.80	0.22	919.62	
+50				19.6	6.2
B.M.				949.19	
T.P.	11.83	936.15	1.52	924.32	
T.P.	12.45	948.37	0.23	935.92	
	5.19	951.27	2.29	946.08	
			1.96	949.31	

$$\begin{array}{r} 2.9 \\ 40.8 \\ \hline 14.6 \end{array}$$

$$\begin{array}{r} 6.6 \\ 60.5 \end{array}$$

$$\begin{array}{r} 4.7 \\ 62.1 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 6.6 \\ 40.2 \\ \hline 13.8 \end{array}$$

$$\begin{array}{r} 5.5 \\ 60.7 \end{array}$$

$$\begin{array}{r} 5.5 \\ 60.7 \\ \hline 16.2 \end{array}$$

Spike in 15" Twin Oak 1' Lt 13+30

