

Bk. 24 - Dr. 11A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Property Survey

SCHIFSKY

From Hodgson Rd. To $\frac{1}{4}$ Mi. West

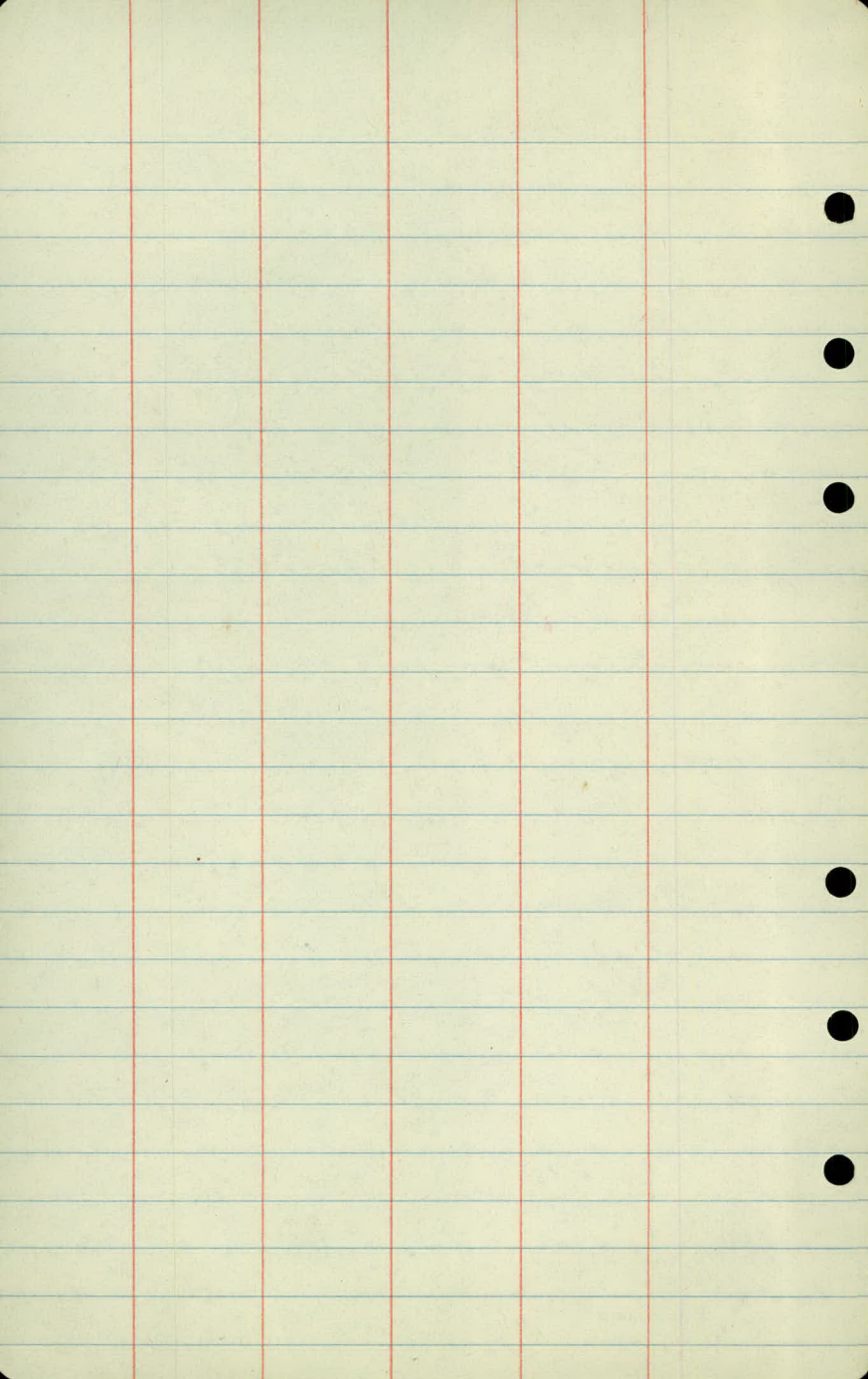
Sec 14 - Mounds View

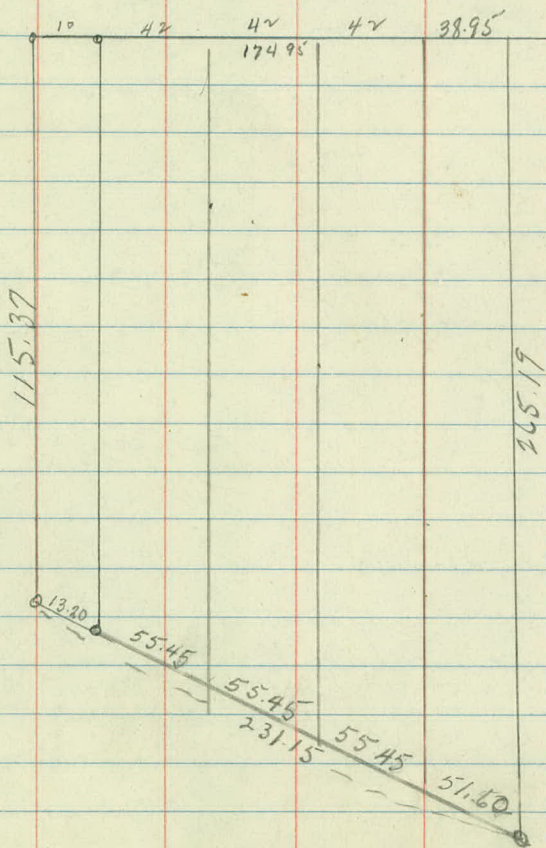
Road Acc't. No. _____

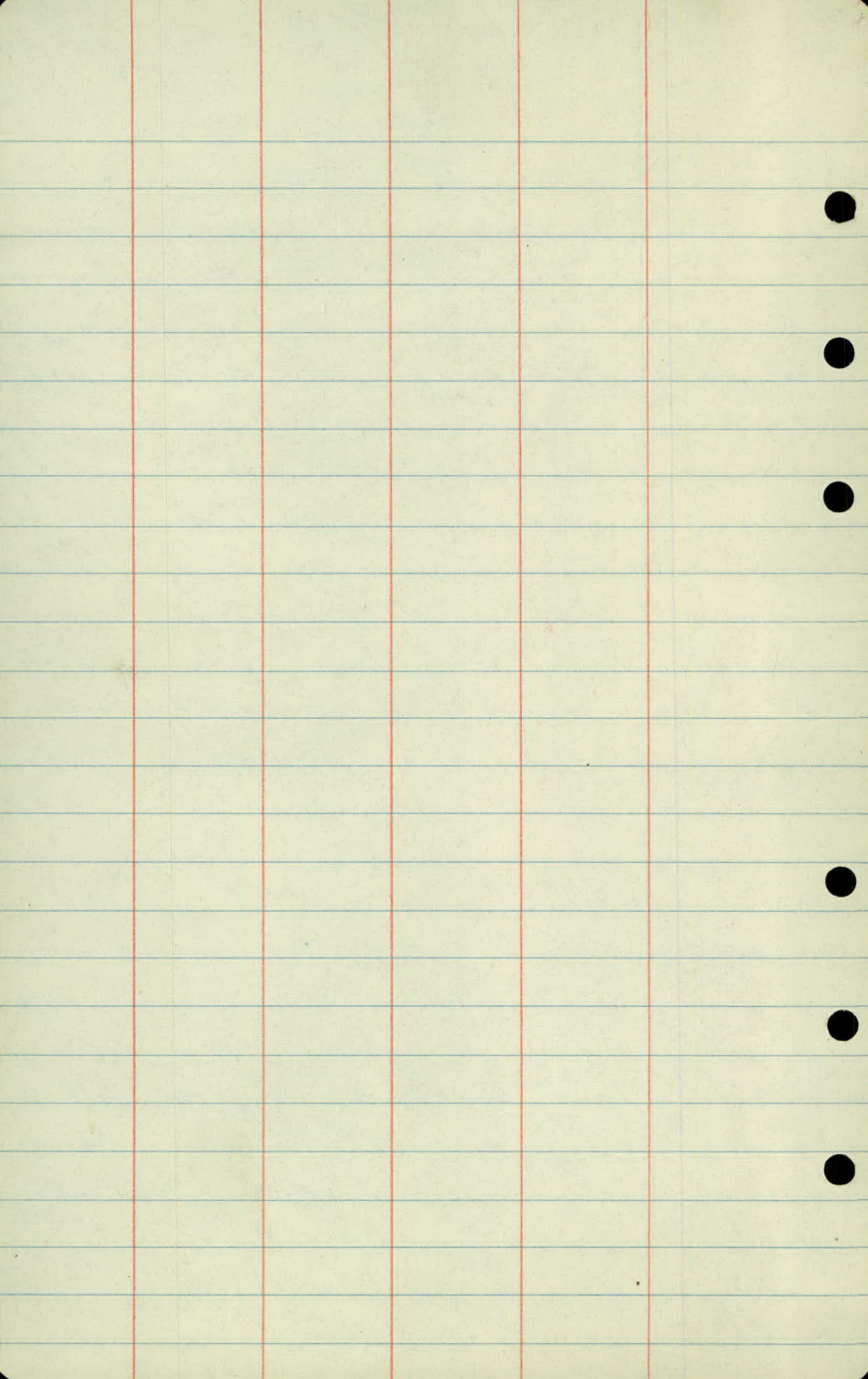
Date Filed 10-26-37

File _____

Iron Placed
on Schifsky Prop







Property Survey

Schifsky's Property

Hodgson Road N. of G. 2

NE $\frac{1}{4}$ Sec. 14 Moundsview Twp.

9/6/39

Party:

R.O.P.

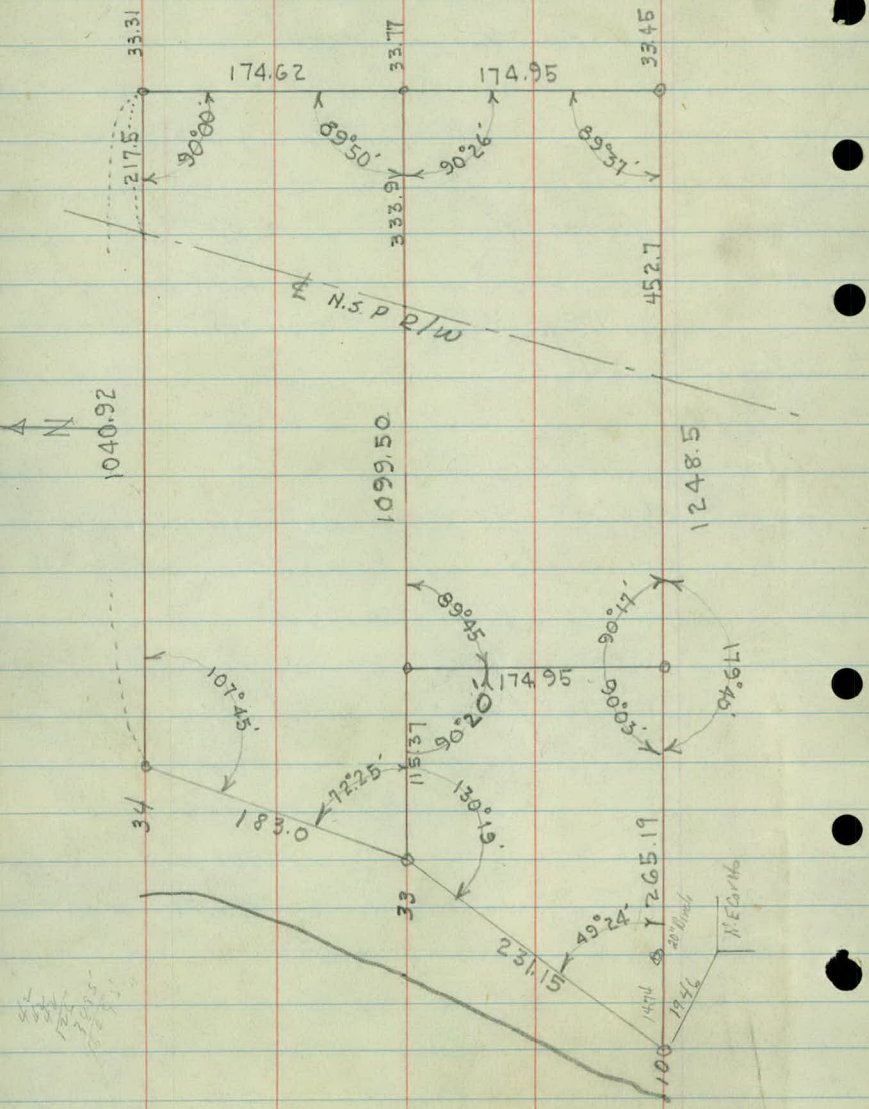
A.M.

C.F.

E.B.

E 1/4 Cor
sec. 14

1438.27



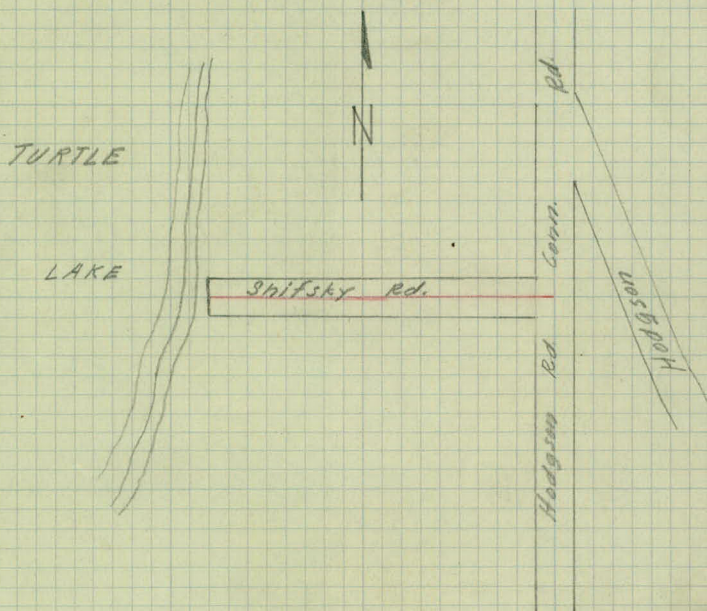
$$\begin{array}{r}
 1320.06 \\
 468.5 \\
 \hline
 1788.56 \\
 1613.23 \\
 \hline
 175.33
 \end{array}$$

$$\begin{array}{r}
 4 \\
 879.5 \\
 411 \\
 \hline
 468.5
 \end{array}$$

$$\begin{array}{r}
 1436.1 \\
 174.96 \\
 \hline
 1661.06
 \end{array}$$

Scientific Property

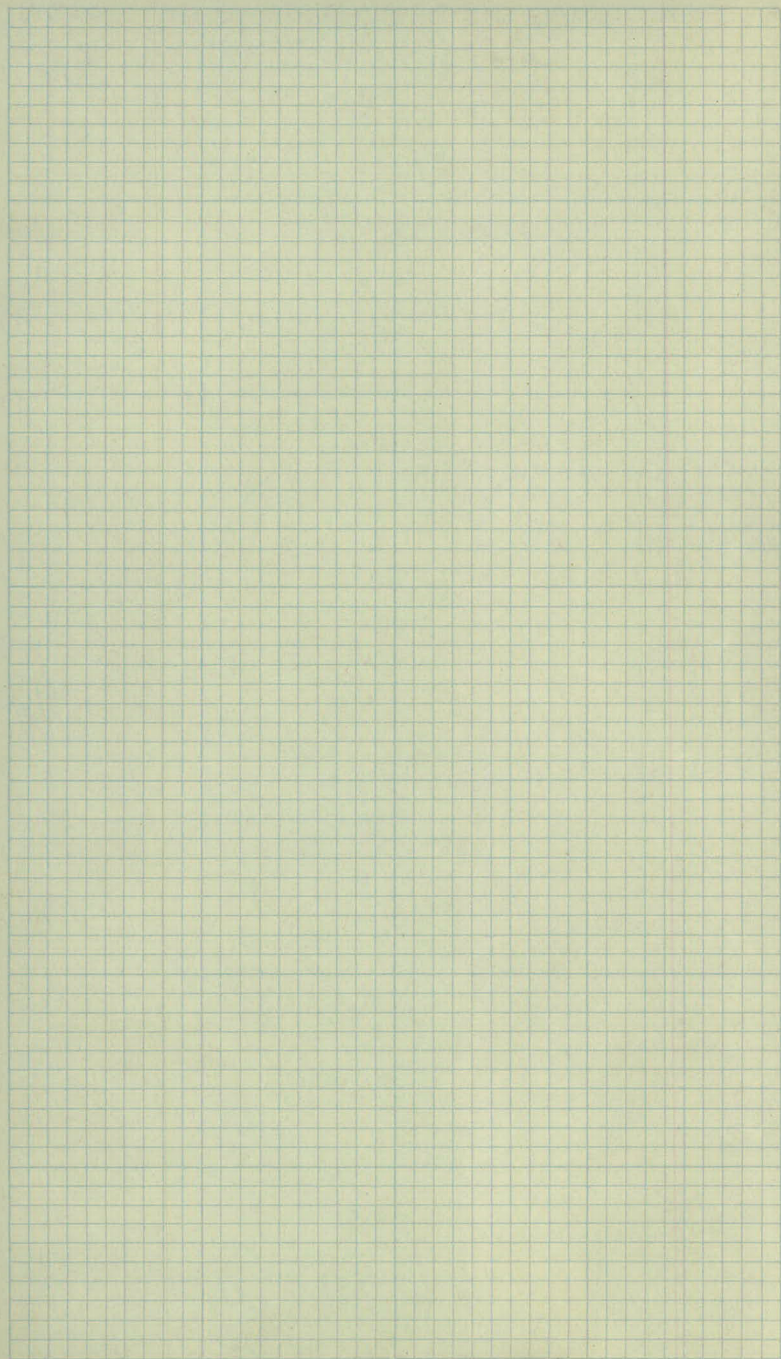
PLAN SURVEY
SHIFSKY ROAD
Hodgson Rd. West.



INDEX.

Align - 1-2
Topog - 3-5
Xsections - 6-10
Soundings - 11-12

Plans started 5/20/40
Completed 5/24/40



Alignment

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

11	+60.98		
----	--------	--	--

11	+30.79	P.O.T.	
----	--------	--------	--

12			
----	--	--	--

10	+15.40	P.O.T.	
----	--------	--------	--

3	+96.41	P.O.T.	
---	--------	--------	--

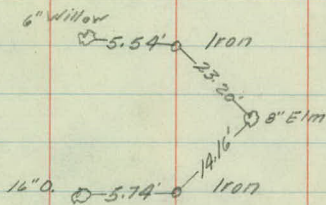
0	+33.74	P.O.T.	Iron on k
---	--------	--------	-----------

0	+33.50	P.O.T.	Iron on k
---	--------	--------	-----------

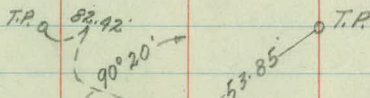
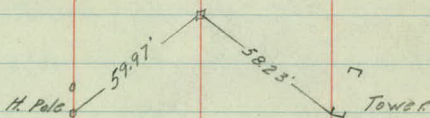
0	+00	- E Hodgson Rd. Cent.	
---	-----	-----------------------	--

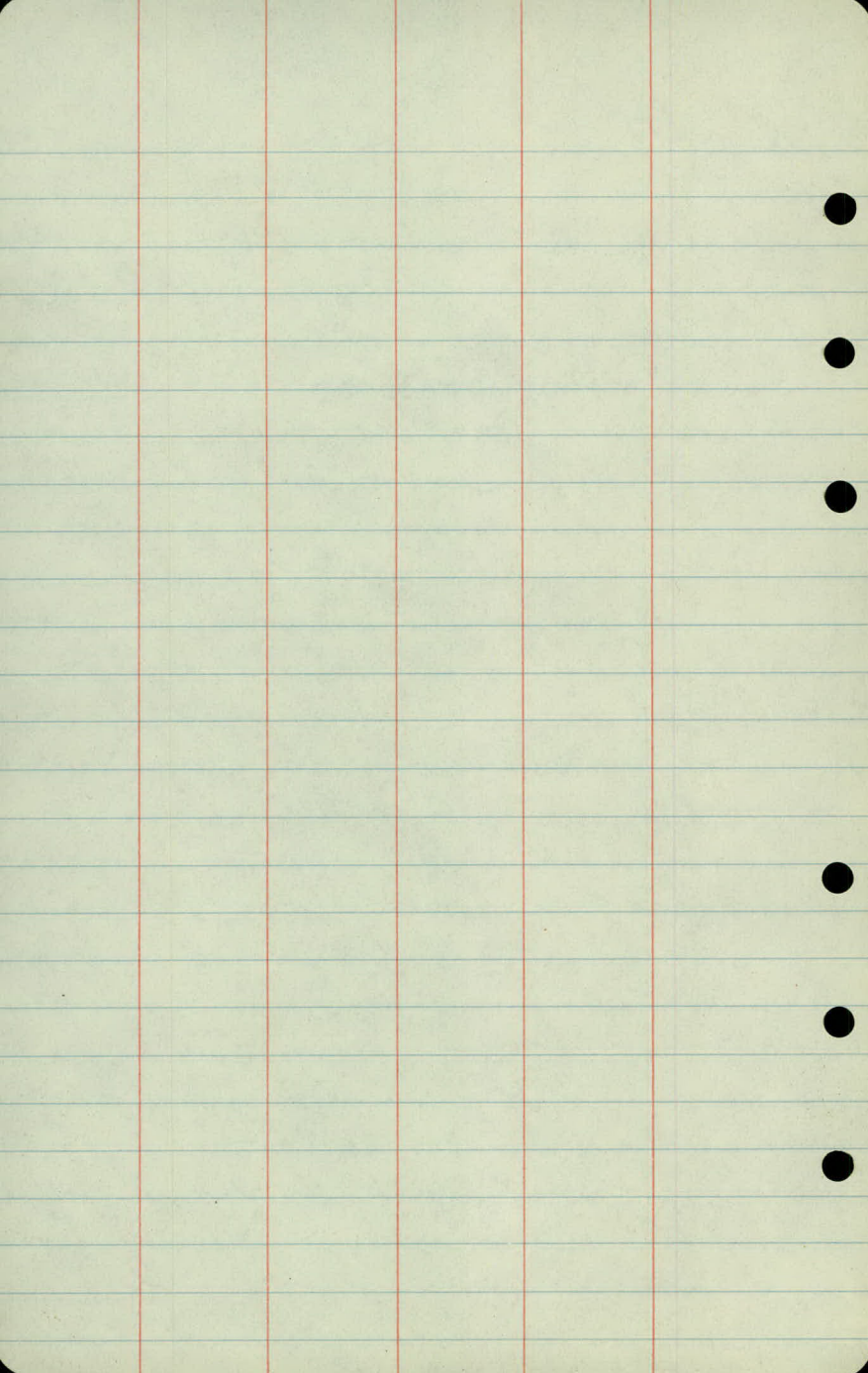
A-26-40
K.A.
L.C.
M.B.
C.N.

2



Iron





Topography

+33-24" O-27'

+14-24" O-28'

+09-86g. Fc-18'

5 +102-6" O-28'

R Trail-11'

+95-15" O-18'

+58-24" O-34'

+77-54p-1'

+98-15" O-8'

+88-Range Tigo Fc.

+63-30" O-14'

+53-15" O-24'

+50-6" O-19' 12' Birch-39'

+97-30" O-15'

+26-54p-6'

+33-12" O-6'

4

R Trail-10'

+93-15" O-52'

+82-Power Line X5%

+68-Fe. Line X5%

+66-Trail X5%

+49-Power Line X5%

+32-10" O-33'

+22-15" O-26' 10" O-33'

+11-12" O-27'

3

R Trail-17'

+98-30" O-5' 10" O-31'

+95-54p-5'

+72-15" O-25'

+60-10" O-27' +64-12" Tw. O-6'

+53-12" O-13'

+89-12" Tw. O-10'

+87-15" O-32'

+78-54p-16'

+72-54p-6' -17'

+39-12" Tw. O-27'

+34-54p-5'

+25-Fc-00

+44-54p-6'-54p-17'-12" O-26' 54p-30'

+90-10" O-11' +38-54p-35'

+25-Fc-64'

2

R Trail-16'

1

R Trail-13'

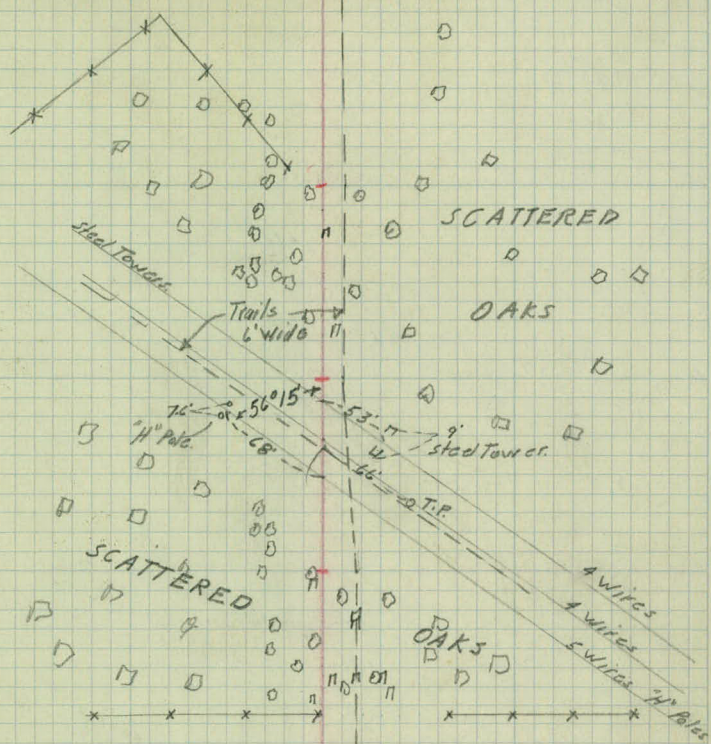
+35-R Trail-10'

+25-T.P-48'

0+00

+10-Edg c Bl. Top

-12-Edg c Bl. Top



12'

+67-Edge Water

+62-End Trees

+50-Water-29'

+40-End New Grade-1-20'

+27-Beg. Trees

11

+90 Swamp-29'

+85 Edge Swamp +80-Dike-52'

10

+21-Beg. New FH-0-20'

R Trail-10' Dike-24'

+74-Beg. 1' Wide Dike-15'

9

R Trail-9'

8

R Trail-9'

7

Swamp-17'

+09-Swamp 25'

R Trail-10'

+80-Swamp-87'

+68-Range To 8 Elders

6

+18-End Row B.Elders-35'

+06-20 0-15

R Trail-8'

TURTLE

LAKE

Scattered

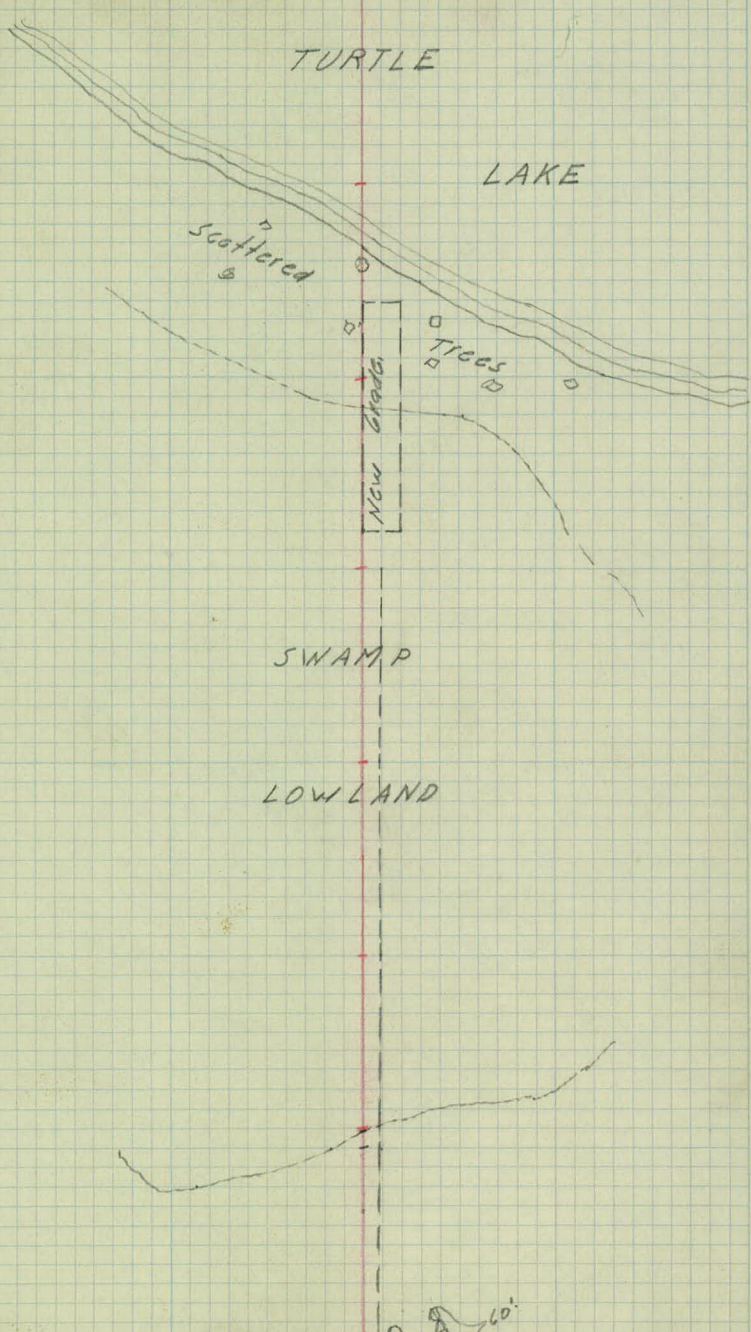
TIGES

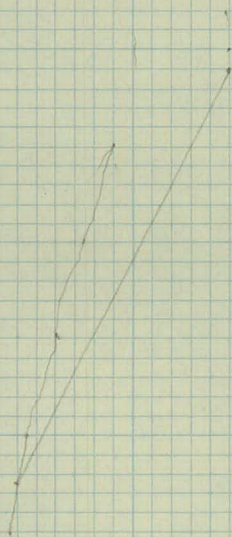
New Grads

SWAMP

LOWLAND

60'





6

X Sections

Sta	+	π	-	Elev.
B.M.	4.86	901.73		896.87
T.P.	2.55	899.23	5.05	896.68
B.M.			1.47	897.76
T.P.	11.70	908.94	1.99	897.24
T.P.	12.72	921.63	0.03	908.91
TP	4.64	924.41	1.86	919.77
B.M.			3.97	920.44

+00

21.9

+10

21.6

+23

19.8

+33

19.5

19.5

+50

19.5

19.3

+50

19.2

Lt.

C.

Rt.

Lake Imp.

Spk. in 20" Birch near Snail Lake Pipe outlet at Turtle Lake.

Spk. in 8" B. oak. 50' Right Sta 11 + 2.5

Spk. in P.R. N.W. Cor. Hodgson Rd. Conn.

$$\begin{array}{r} 21 \\ \hline 50 \end{array} \quad \begin{array}{r} 25 \\ \hline 50 \end{array} \quad \begin{array}{r} 29 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 24 \\ \hline 50 \end{array} \quad \begin{array}{r} 28 \\ \hline 50 \end{array} \quad \begin{array}{r} 30 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 43 \\ \hline 50 \end{array} \quad \begin{array}{r} 43 \\ \hline 22 \end{array} \quad \begin{array}{r} 46 \\ \hline 22 \end{array} \quad \begin{array}{r} 44 \\ \hline 22 \end{array} \quad \begin{array}{r} 47 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 47 \\ \hline 50 \end{array} \quad \begin{array}{r} 48 \\ \hline 22 \end{array} \quad \begin{array}{r} 49 \\ \hline 25 \end{array} \quad \begin{array}{r} 50 \\ \hline 25 \end{array} \quad \begin{array}{r} 49 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 46 \\ \hline 50 \end{array} \quad \begin{array}{r} 48 \\ \hline 25 \end{array} \quad \begin{array}{r} 49 \\ \hline 30 \end{array} \quad \begin{array}{r} 49 \\ \hline 30 \end{array} \quad \begin{array}{r} 49 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 47 \\ \hline 50 \end{array} \quad \begin{array}{r} 48 \\ \hline 27 \end{array} \quad \begin{array}{r} 48 \\ \hline 25 \end{array} \quad \begin{array}{r} 47 \\ \hline 25 \end{array} \quad \begin{array}{r} 44 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 48 \\ \hline 50 \end{array} \quad \begin{array}{r} 49 \\ \hline 27 \end{array} \quad \begin{array}{r} 51 \\ \hline 25 \end{array} \quad \begin{array}{r} 50 \\ \hline 25 \end{array} \quad \begin{array}{r} 47 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 48 \\ \hline 50 \end{array} \quad \begin{array}{r} 49 \\ \hline 25 \end{array} \quad \begin{array}{r} 48 \\ \hline 25 \end{array} \quad \begin{array}{r} 50 \\ \hline 25 \end{array} \quad \begin{array}{r} 50 \\ \hline 50 \end{array}$$

Sta	+	π	-	Elev
		924.41		
3				19.5
	+41			19.4
	+72			18.4
4				17.8
T.P.	0.81	918.07	7.15	917.26
	+50			15.3
5				12.8
	+42			10.10
	+67			07.9
6				05.9
T.P.	0.11	906.09	12.09	905.98
	+32			03.3
	+69			99.5
7				96.1

Lt

X

Rt

$$\begin{array}{r} 51 \\ 50 \end{array} \quad \begin{array}{r} 50 \\ 27 \end{array} \quad \begin{array}{r} 49 \\ 27 \end{array} \quad \begin{array}{r} 48 \\ 27 \end{array} \quad \begin{array}{r} 50 \\ 50 \end{array}$$

$$\begin{array}{r} 57 \\ 50 \end{array} \quad \begin{array}{r} 56 \\ 28 \end{array} \quad \begin{array}{r} 50 \\ 25 \end{array} \quad \begin{array}{r} 49 \\ 25 \end{array} \quad \begin{array}{r} 46 \\ 50 \end{array}$$

$$\begin{array}{r} 63 \\ 50 \end{array} \quad \begin{array}{r} 64 \\ 30 \end{array} \quad \begin{array}{r} 58 \\ 25 \end{array} \quad \begin{array}{r} 51 \\ 25 \end{array} \quad \begin{array}{r} 47 \\ 50 \end{array}$$

$$\begin{array}{r} 75 \\ 50 \end{array} \quad \begin{array}{r} 74 \\ 24 \end{array} \quad \begin{array}{r} 66 \\ 24 \end{array} \quad \begin{array}{r} 60 \\ 24 \end{array} \quad \begin{array}{r} 53 \\ 50 \end{array}$$

$$\begin{array}{r} 39 \\ 50 \end{array} \quad \begin{array}{r} 34 \\ 28 \end{array} \quad \begin{array}{r} 28 \\ 0 \end{array} \quad \begin{array}{r} 32 \\ 23 \end{array} \quad \begin{array}{r} 24 \\ 24 \end{array} \quad \begin{array}{r} 20 \\ 24 \end{array} \quad \begin{array}{r} 14 \\ 50 \end{array}$$

$$\begin{array}{r} 64 \\ 50 \end{array} \quad \begin{array}{r} 59 \\ 28 \end{array} \quad \begin{array}{r} 53 \\ 5 \end{array} \quad \begin{array}{r} 56 \\ 5 \end{array} \quad \begin{array}{r} 51 \\ 21 \end{array} \quad \begin{array}{r} 47 \\ 22 \end{array} \quad \begin{array}{r} 40 \\ 50 \end{array}$$

$$\begin{array}{r} 90 \\ 50 \end{array} \quad \begin{array}{r} 85 \\ 26 \end{array} \quad \begin{array}{r} 80 \\ 0 \end{array} \quad \begin{array}{r} 84 \\ 0 \end{array} \quad \begin{array}{r} 79 \\ 22 \end{array} \quad \begin{array}{r} 75 \\ 23 \end{array} \quad \begin{array}{r} 74 \\ 50 \end{array}$$

$$\begin{array}{r} 105 \\ 50 \end{array} \quad \begin{array}{r} 103 \\ 27 \end{array} \quad \begin{array}{r} 102 \\ 21 \end{array} \quad \begin{array}{r} 98 \\ 21 \end{array} \quad \begin{array}{r} 95 \\ 22 \end{array} \quad \begin{array}{r} 90 \\ 50 \end{array}$$

$$\begin{array}{r} 133 \\ 50 \end{array} \quad \begin{array}{r} 135 \\ 44 \end{array} \quad \begin{array}{r} 136 \\ 34 \end{array} \quad \begin{array}{r} 130 \\ 20 \end{array} \quad \begin{array}{r} 122 \\ 22 \end{array} \quad \begin{array}{r} 114 \\ 22 \end{array} \quad \begin{array}{r} 110 \\ 40 \end{array} \quad \begin{array}{r} 112 \\ 50 \end{array}$$

Nail in Tree.

$$\begin{array}{r} 46 \\ 50 \end{array} \quad \begin{array}{r} 43 \\ 40 \end{array} \quad \begin{array}{r} 40 \\ 16 \end{array} \quad \begin{array}{r} 28 \\ 14 \end{array} \quad \begin{array}{r} 32 \\ 14 \end{array} \quad \begin{array}{r} 24 \\ 34 \end{array} \quad \begin{array}{r} 0.9 \\ 50 \end{array}$$

4-30-40

$$\begin{array}{r} 9.1 \\ 50 \end{array} \quad \begin{array}{r} 9.1 \\ 37 \end{array} \quad \begin{array}{r} 7.5 \\ 23 \end{array} \quad \begin{array}{r} 6.6 \\ 17 \end{array} \quad \begin{array}{r} 6.0 \\ 17 \end{array} \quad \begin{array}{r} 4.6 \\ 36 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array}$$

$$\begin{array}{r} 11.6 \\ 50 \end{array} \quad \begin{array}{r} 11.4 \\ 30 \end{array} \quad \begin{array}{r} 10.8 \\ 15 \end{array} \quad \begin{array}{r} 10.0 \\ 14 \end{array} \quad \begin{array}{r} 9.2 \\ 14 \end{array} \quad \begin{array}{r} 8.5 \\ 22 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array}$$

Sta	+	π	-	Elev.
		906.09		
7+12				94.8
+34				94.9
8				95.3
+50				94.9
9				94.6
+50				94.1
10				94.0
+50				93.7
+85				93.6
+93				94.2
11				94.1
B.M.	2.63	900.39	8.34	897.75 (897.76)

LT							RT
$\frac{11.4}{50}$	$\frac{11.5}{24}$		$\frac{11.3}{5}$	$\frac{10.9}{5}$	$\frac{10.4}{7}$	$\frac{9.8}{31}$	$\frac{9.4}{50}$
$\frac{10.8}{50}$	$\frac{11.2}{24}$		$\frac{11.2}{6}$	$\frac{10.5}{14}$	$\frac{10.6}{17}$	$\frac{11.3}{39}$	$\frac{11.0}{50}$
$\frac{10.6}{50}$	$\frac{10.7}{19}$		$\frac{10.8}{31}$	$\frac{10.9}{31}$		$\frac{11.1}{50}$	
$\frac{11.5}{50}$	$\frac{11.4}{29}$		$\frac{11.2}{29}$	$\frac{11.0}{29}$		$\frac{10.6}{50}$	
$\frac{11.4}{50}$	$\frac{11.5}{22}$		$\frac{11.5}{30}$	$\frac{11.7}{30}$		$\frac{11.8}{50}$	
$\frac{11.8}{50}$	$\frac{12.0}{27}$		$\frac{12.0}{27}$	$\frac{12.1}{27}$		$\frac{12.2}{50}$	
$\frac{12.1}{50}$	$\frac{12.3}{27}$		$\frac{12.1}{25}$	$\frac{12.3}{25}$		$\frac{12.4}{50}$	
$\frac{12.1}{50}$	$\frac{12.0}{32}$		$\frac{12.4}{20}$	$\frac{11.8}{22}$	$\frac{12.4}{38}$	$\frac{12.5}{40}$	$\frac{13.5}{50}$
$\frac{12.6}{50}$	$\frac{12.6}{27}$	$\frac{12.7}{4}$	$\frac{12.5}{20}$	$\frac{11.9}{22}$	$\frac{12.6}{32}$	$\frac{12.5}{50}$	$\frac{13.5}{54}$
$\frac{12.3}{50}$	$\frac{11.2}{36}$	$\frac{11.5}{17}$	$\frac{11.9}{19}$	$\frac{11.8}{22}$	$\frac{12.3}{33}$	$\frac{12.0}{40}$	$\frac{12.7}{50}$
$\frac{10.6}{50}$	$\frac{11.3}{23}$	$\frac{12.3}{3}$	$\frac{12.0}{21}$	$\frac{11.7}{21}$	$\frac{12.1}{50}$		

Spike 8" B. Oak 50' RT Sta 11 + 25

Sta	+	π	-	Elev.
		900.39		
11	+25		5.0	95.4
	+29		3.4	97.0
	+31		3.4	97.0
	+43		5.3	95.1
	+46		7.5	92.9
	+63		8.0	92.4
	+66		8.77	91.62
B.M.			3.49	896.90 (896.87)

5-6-40
K.A.
L.G.
M.B.
C.H.

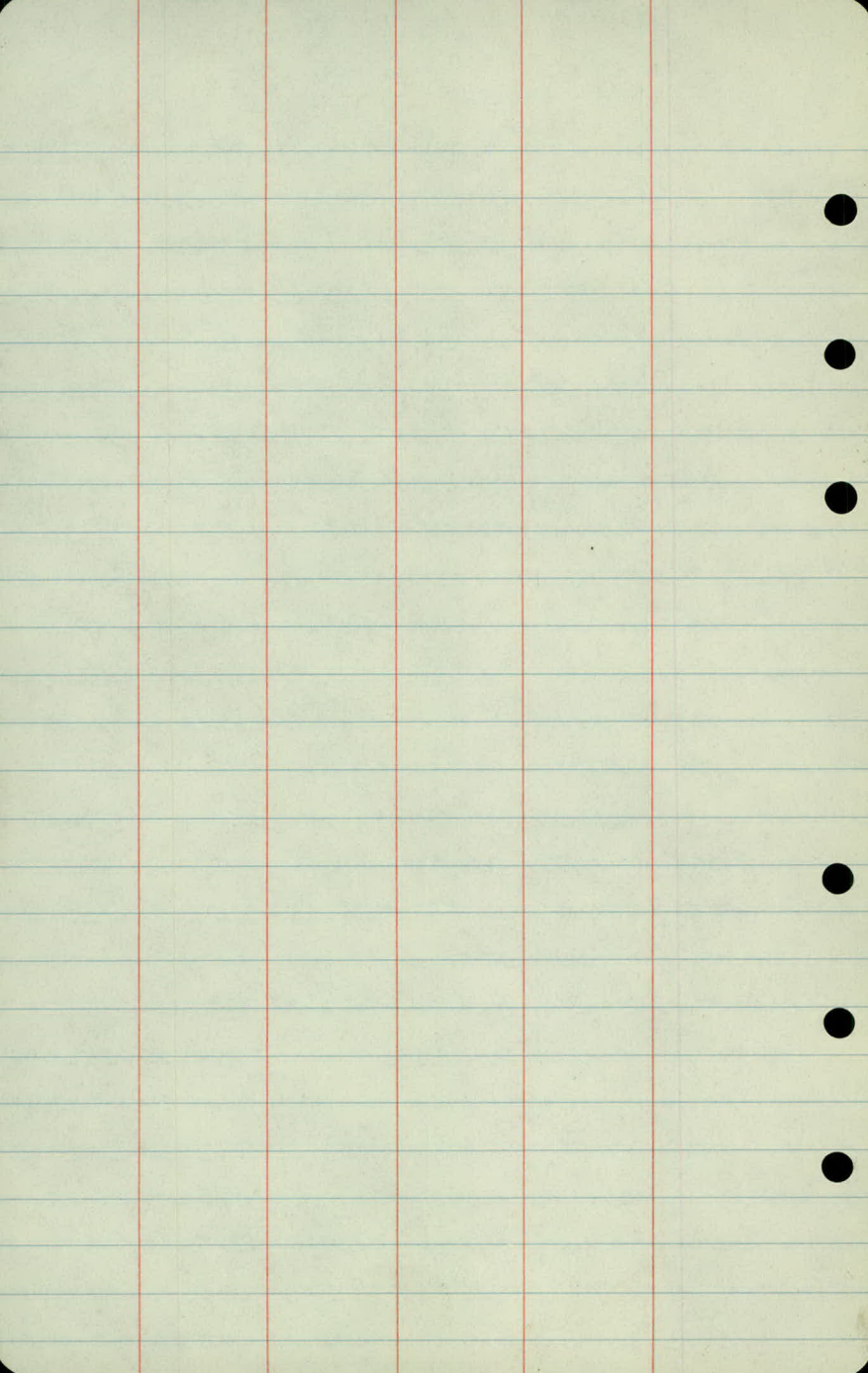
10

Lt

4

Rt

Elev. Turtle Lake.
Lake Imp. Bench.



Push Soundings

Sta

7 +50

P

+50

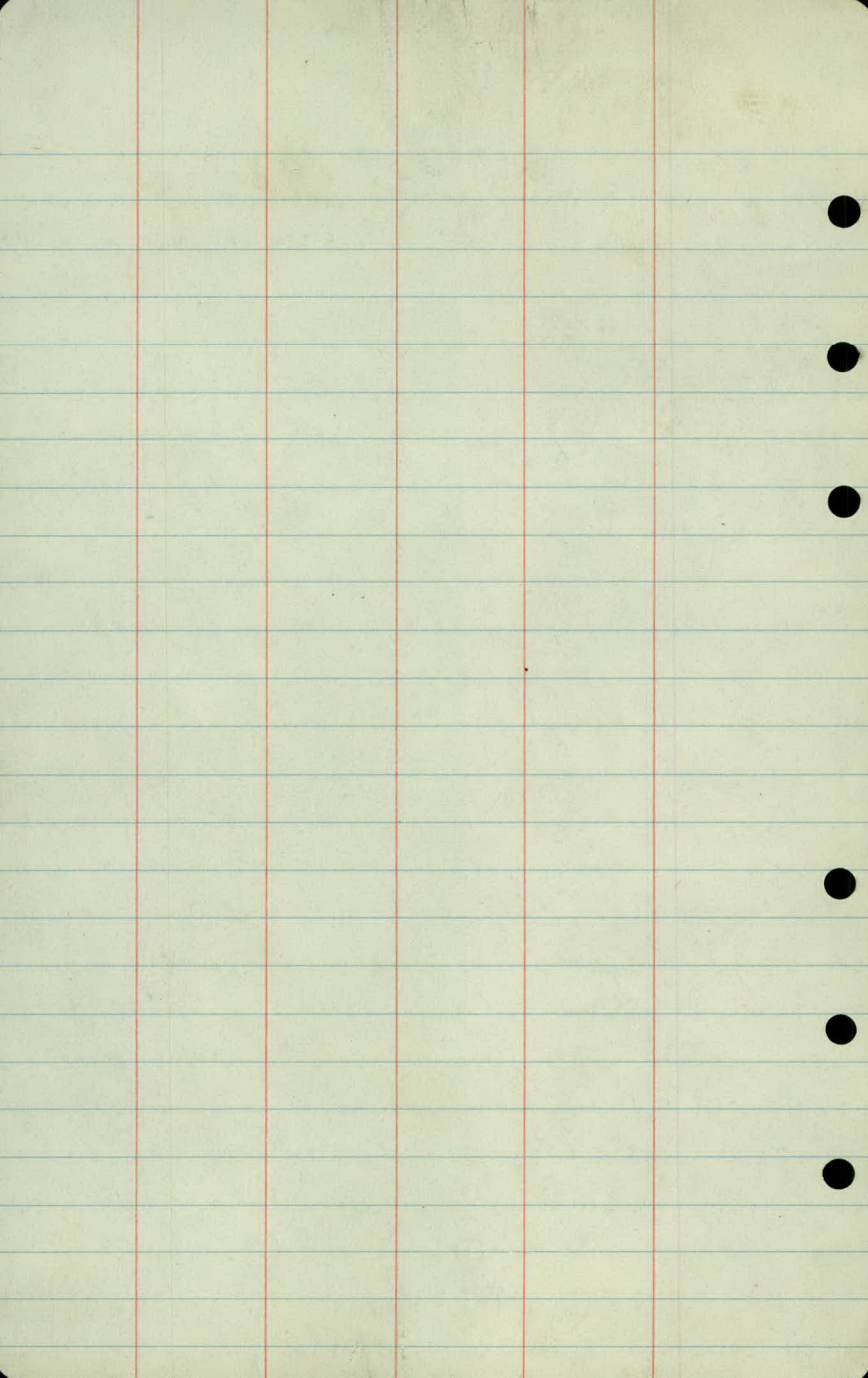
9

+50

10

+50

20' Lt.	4	20' Rt
Depth	Depth	Depth
<u>5.8</u>	46'	<u>3.9'</u>
<u>7.5'</u>	<u>69'</u>	<u>6.3'</u>
<u>9.4'</u>	<u>110'</u>	<u>7.8'</u>
<u>8.5'</u>	<u>90</u>	<u>81'</u>
<u>6.2'</u>	<u>71'</u>	<u>8.0'</u>
<u>36'</u>	<u>42'</u>	<u>45'</u>
<u>1.2'</u>	<u>15'</u>	<u>20'</u> 25'



Schifsky Road

Slope stakes

Sta	+	π	-	Grade	
B.M.	3.94	924.38			(920.44)
0	+00			21.5	
	+33			20.7	
	+65			19.5	
1				19.3	
	+50			18.9	
2				18.8	
	+50			18.8	
3				18.7	
	+41			18.4	
	+72			17.8	
4				17.0	

Gr. Rod. Lt. & Rt.

Spk. in R.P.M.W. Hodgson Rd. Conn. + Sahitsky Road.

2.9

3.7

$$14.2' / \frac{4.8}{-1.7}$$

$$\frac{4.9}{-1.2}$$

$$\frac{5.0}{-1.3} / 14.1$$

4.9

$$13.8' / \frac{4.8}{+0.1}$$

$$\frac{4.7}{+0.2}$$

$$\frac{4.9}{+0.0} / 13.6$$

5.1

$$14.2' / \frac{4.8}{+0.3}$$

$$\frac{4.8}{+0.3}$$

$$\frac{4.9}{+0.2} / 14.0$$

5.5

$$15.0' / \frac{4.8}{+0.7}$$

$$\frac{4.8}{+0.7}$$

$$\frac{4.8}{+0.7} / 15.0$$

5.6

$$15.0' / \frac{4.9}{+0.7}$$

$$\frac{5.0}{+0.6}$$

$$\frac{5.0}{+0.6} / 14.8$$

5.6

$$15.2' / \frac{4.8}{+0.8}$$

$$\frac{4.8}{+0.8}$$

$$\frac{4.9}{+0.7} / 15.0$$

5.7

$$14.8' / \frac{5.1}{+0.6}$$

$$\frac{4.9}{+0.8}$$

$$\frac{5.3}{+0.9} / 14.4$$

6.0

$$15.0' / \frac{5.3}{+0.7}$$

$$\frac{5.0}{+1.0}$$

$$\frac{4.8}{+1.2} / 16.0$$

6.6

$$13.8' / \frac{6.5}{+0.1}$$

$$\frac{5.7}{+0.9}$$

$$\frac{5.9}{+1.2} / 16.0$$

7.4

$$14.4' / \frac{7.0}{+0.4}$$

$$\frac{6.6}{+0.8}$$

$$\frac{6.1}{+1.3} / 16.2$$

Sta	+	π	-	Grade
		924.38		
4	+50			14.9
5				12.1
T.P.	1.65	914.66	11.37	913.01
	+42			09.1
	+67			07.1
6				04.5
	+32			02.1
T.P.	1.20	904.41	11.45	903.21
7	+69			99.9
7				98.4
	+12			97.9
	+34			97.2
	+65			96.4

Gr. Rod

Lt

&

Rt

9.5

$$12.8 \div \frac{94}{+0.1}$$

$$\frac{94}{+0.1}$$

$$\frac{86}{+0.9} / 5.4$$

12.3

$$14.6 \div \frac{118}{+0.5}$$

$$\frac{118}{+0.4}$$

$$\frac{117}{+0.6} / 4.8$$

5.6

$$15.6 \div \frac{46}{+1.0}$$

$$\frac{45}{+1.1}$$

$$\frac{48}{+0.8} / 5.2$$

7.6

$$15.6 \div \frac{66}{+1.0}$$

$$\frac{66}{+1.0}$$

$$\frac{63}{+1.3} / 6.2$$

10.2

$$15.2 \div \frac{94}{+0.8}$$

$$\frac{88}{+1.4}$$

$$\frac{82}{+2.0} / 7.6$$

12.6

$$14.2 \div \frac{12.3}{+0.3}$$

$$\frac{113}{+1.3}$$

$$\frac{113}{+1.3} / 6.2$$

4.5

$$12.2 \div \frac{52}{+0.1}$$

$$\frac{47}{-0.2}$$

$$\frac{45}{+0.0} / 3.6$$

6.0

$$18.2 \div \frac{91}{-3.1}$$

$$\frac{83}{-2.3}$$

$$\frac{74}{-1.4} / 4.8$$

6.5

7.2

$$16.4 \div \frac{94}{-2.2}$$

$$\frac{92}{-2.1}$$

$$\frac{95}{-2.3} / 6.6$$

8.0

$$14.2 \div \frac{91}{-1.7}$$

$$\frac{91}{-1.7}$$

$$\frac{88}{-0.8} / 3.6$$

Sta	+	π	-	Grade
		909.41		

8				96.2
---	--	--	--	------

	+50			96.1
--	-----	--	--	------

9				96.0
---	--	--	--	------

	+50			95.8
--	-----	--	--	------

10				95.7
----	--	--	--	------

	+18			95.6
--	-----	--	--	------

B.M.	2.45	900.21	6.65	897.76
------	------	--------	------	--------

(897.76)

8+45=
0+00

Alley

96.1

	+20			96.1
--	-----	--	--	------

	+50			96.1
--	-----	--	--	------

1				96.1
---	--	--	--	------

	+50			96.1
--	-----	--	--	------

+72.2 +74.62 = End.

96.1

Gr. Rod

Lt

K

Rt

8.2

$$14.0' / \frac{9.2}{-1.0}$$

$$\frac{9.0}{-0.8}$$

$$\frac{8.2}{87} / 12.0'$$

8.3

$$13.8' / \frac{9.2}{-0.9}$$

$$\frac{9.4}{-1.1}$$

$$\frac{8.1}{-98} / 12.6'$$

8.4

$$15.2' / \frac{10.0}{-1.6}$$

$$\frac{9.6}{-1.2}$$

$$\frac{9.7}{-73} / 14.6'$$

8.6

$$15.2' / \frac{10.2}{-1.6}$$

$$\frac{10.3}{-1.7}$$

$$\frac{10.1}{-15} / 15.0'$$

8.7

$$15.4' / \frac{10.4}{-1.7}$$

$$\frac{10.4}{-1.7}$$

$$\frac{10.6}{-1.9} / 15.8'$$

8.8

$$14.6' / \frac{10.1}{-1.3}$$

$$\frac{10.4}{-1.6}$$

$$\frac{10.4}{-1.6} / 15.2'$$

Spt. in 8" O. 50' Kt. 1142.5

4.1

$$10.0' / \frac{5.3}{-1.2}$$

$$\frac{5.2}{-1.1}$$

$$\frac{4.9}{-98} / 9.6'$$

4.1

$$10.0' / \frac{5.7}{-1.6}$$

$$\frac{5.6}{-1.5}$$

$$\frac{5.4}{-1.3} / 10.0'$$

4.1

$$10.0' / \frac{6.2}{-2.1}$$

$$\frac{6.1}{-2.0}$$

$$\frac{6.0}{-2.0} / 10.0'$$

4.1

$$10.0' / \frac{6.6}{-2.5}$$

$$\frac{6.5}{-2.4}$$

$$\frac{6.4}{-2.3} / 10.0'$$

4.1

$$9.7' / \frac{4.8}{-2.7}$$

$$\frac{4.1}{-2.7}$$

$$\frac{4.4}{-0.3} / 8.6'$$

