

BK 23 - Dr. 11A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

_____ EASTWOOD ROAD _____

From _____ Sherwood Rd. To Co. Rd. "J" _____

Road Acc't. No. _____ M-48 _____

Date Filed _____ 10-26-37 _____

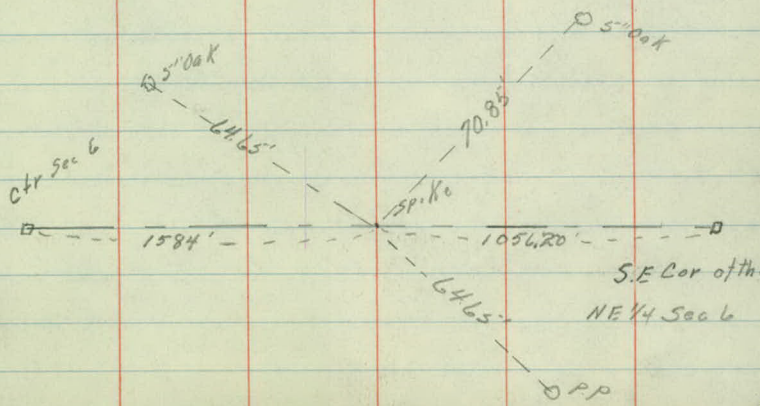
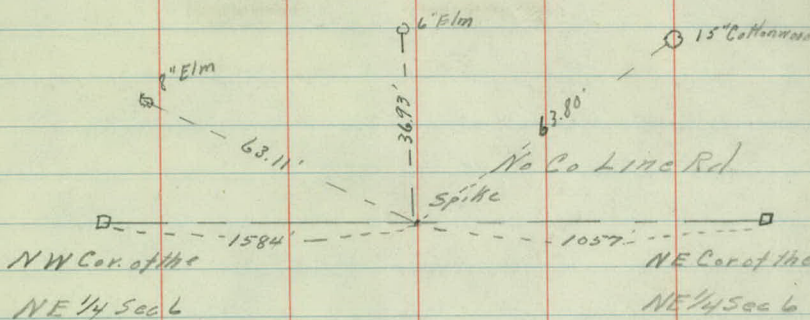
File _____

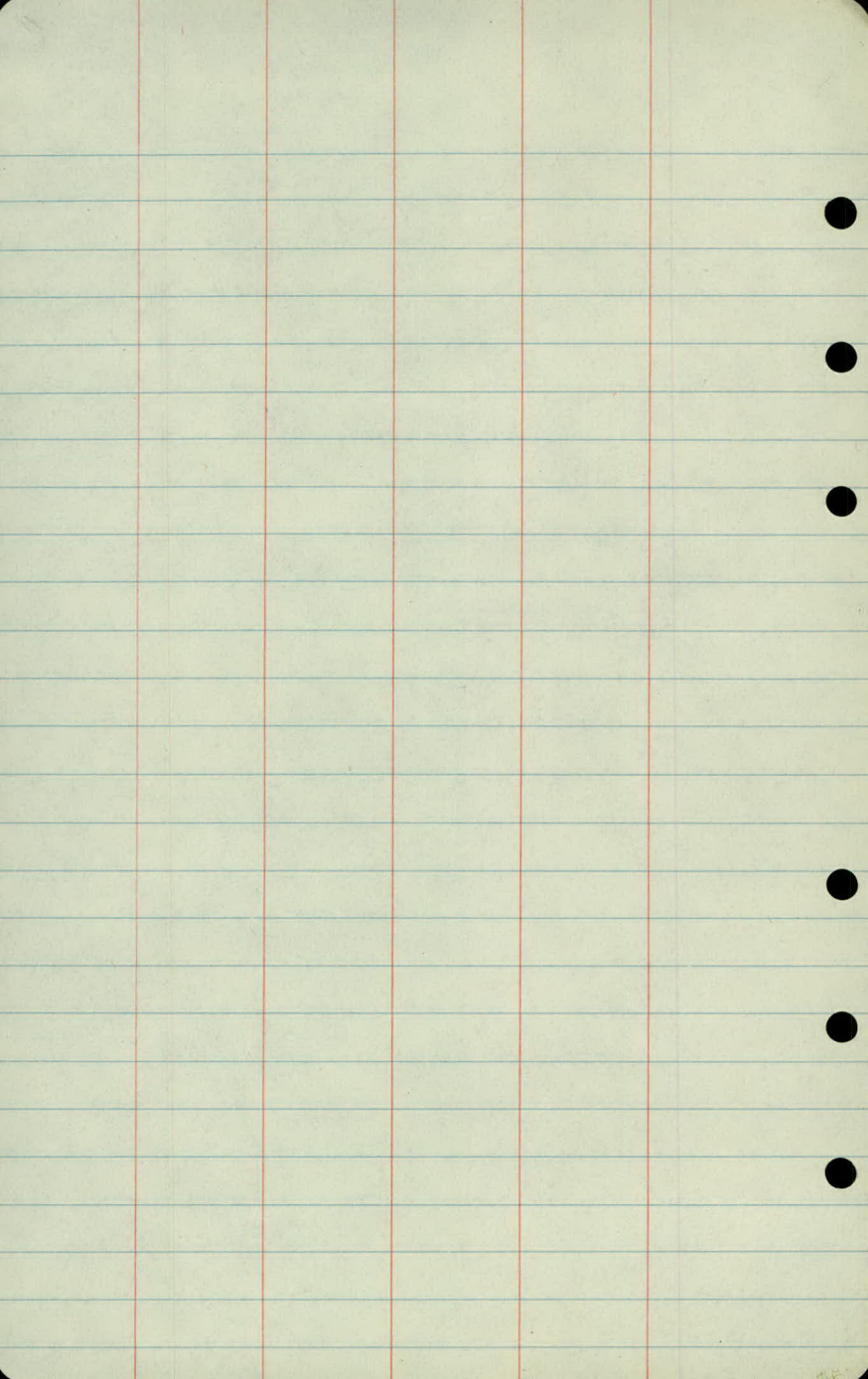
1
Alignment
Eastwood Road

Sta Pt.

33+64.00' P.O.T

0+00





Topography
Eastwood Drive

6

5

4

3

2

1

0

+50 Ent

Tree line 25'

10' Trail

Tree line 25'

+25 Ent

Small Oaks

+25 Big Oaks 25'

+25 Big Woods

Sherwood Rd

13

12

11

10

9

8

7

6

Trees 15' 5

+50 ENT

Tree line 40'

Tree line 80'

Trees 80

Tree 25' 4/100'

Meadow

Meadow

Tree line 25'
Woods

+00 End Woods 25'

Woods

Tree line 25'

20

19

18

17

16

15

14

13

+100 End Woods

Woods

Trees 100' 25'

small trees

+40 Beg Woods

+25 Ent

Meadow

Meadow

Meadow

Meadow

Trees 200'

+75 Ent

Trees 100'

27

26

25

24

23

22

21

20

Cultivated

Waste

+25 Ent

+00 End Yard

Scattered
oaks

Tree line 20'

+00 Beg Yard

+40 End Woods

+28 Beg Woods

+00 Beg Cultivation

34

33+6405
NoCo Linn Rd

33

32

31

30

29

28

No Co Line Rd

Cultivated

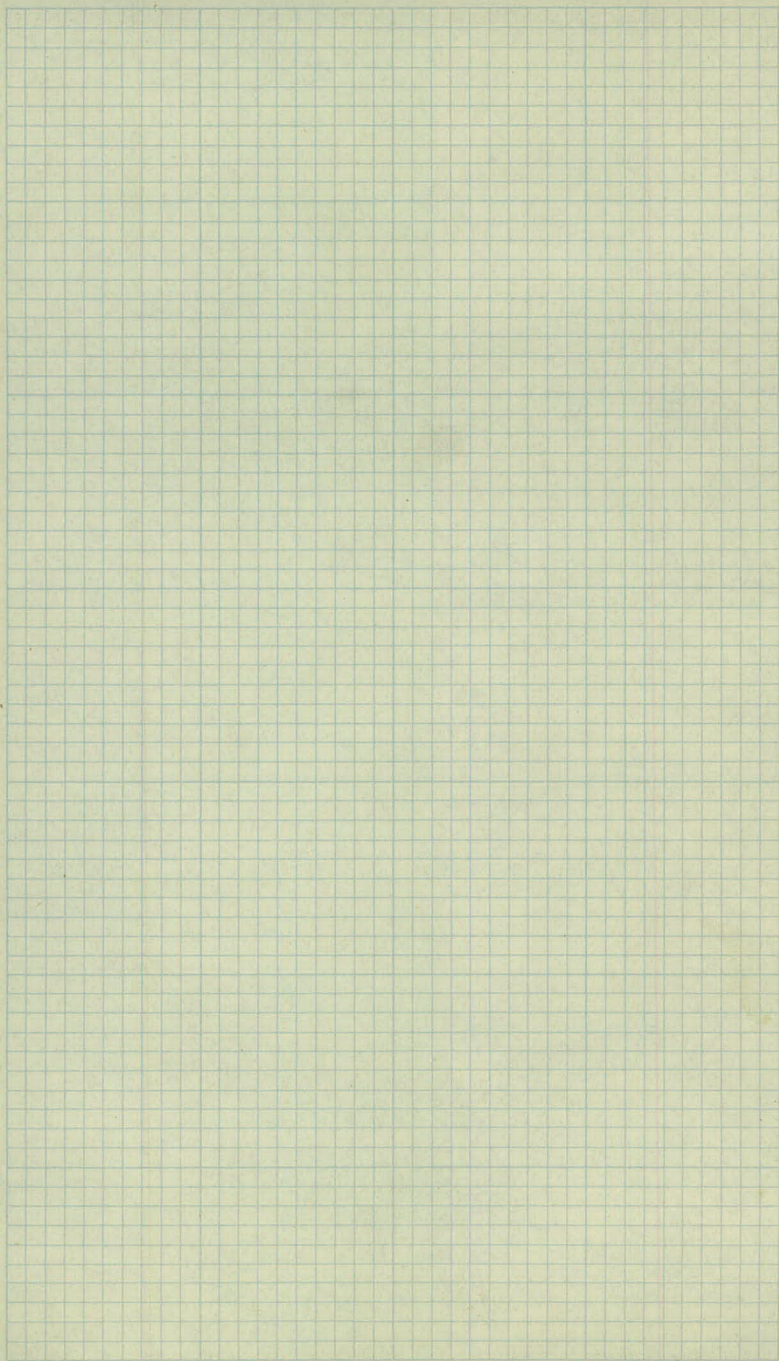
Scattered Oaks



Cultivated

Cultivated

130 Ent



X sections

Eastwood Rd

Sta	+	π	-	Elev
B.M	2.54	916.28 ✓		913.74

0			4.2	12.1'
---	--	--	-----	-------

+50			3.8	12.5'
-----	--	--	-----	-------

1+00			4.7	11.6'
------	--	--	-----	-------

+50			5.1	11.2'
-----	--	--	-----	-------

2			4.4	11.9'
---	--	--	-----	-------

+50			4.2	12.1'
-----	--	--	-----	-------

3			4.5	11.8'
---	--	--	-----	-------

+50			5.0	11.3'
-----	--	--	-----	-------

T.P.	6.59 ✓	918.76 ✓	4.11	912.17 ✓
------	--------	----------	------	----------

4			6.9	11.9'
---	--	--	-----	-------

+50			6.5	12.3'
-----	--	--	-----	-------

5			5.2	13.6'
---	--	--	-----	-------

Lt

L

Rt

Spk in 8" oad 45' Lt. Stg 0+65

$$\frac{3.7}{50}$$

$$4.2$$

$$\frac{5.0}{50}$$

$$\frac{3.6}{50} \quad \frac{3.7}{20} \quad \frac{4.0}{11} \quad \frac{4.2}{10} \quad 3.8 \quad \frac{3.9}{11} \quad \frac{4.5}{50}$$

$$\frac{5.0}{50} \quad \frac{4.7}{13} \quad \frac{5.1}{12} \quad 4.7 \quad \frac{4.9}{10} \quad \frac{5.0}{50}$$

$$\frac{4.9}{50} \quad \frac{5.0}{11} \quad \frac{5.6}{10} \quad 5.1 \quad \frac{5.4}{10} \quad \frac{5.0}{11} \quad \frac{5.5}{50}$$

$$\frac{4.1}{50} \quad \frac{4.4}{12} \quad \frac{4.8}{11} \quad 4.4 \quad \frac{4.5}{10} \quad \frac{5.1}{50}$$

$$\frac{4.1}{50} \quad \frac{4.2}{11} \quad \frac{4.5}{9} \quad 4.2 \quad \frac{4.6}{10} \quad \frac{4.2}{11} \quad \frac{4.2}{50}$$

$$\frac{5.1}{50} \quad \frac{4.5}{9} \quad \frac{4.8}{8} \quad 4.5 \quad \frac{4.7}{11} \quad \frac{4.2}{12} \quad \frac{4.4}{50}$$

$$\frac{5.1}{50} \quad \frac{5.0}{8} \quad \frac{5.4}{7} \quad 5.0 \quad \frac{5.2}{12} \quad \frac{4.9}{13} \quad \frac{4.9}{50}$$

$$\frac{6.8}{50} \quad \frac{6.7}{8} \quad \frac{7.2}{6} \quad 6.9 \quad \frac{7.2}{12} \quad \frac{6.7}{13} \quad \frac{6.7}{50}$$

$$\frac{6.4}{50} \quad \frac{6.2}{8} \quad 6.5 \quad \frac{6.0}{4} \quad \frac{6.5}{13} \quad \frac{6.1}{14} \quad \frac{5.7}{50}$$

$$\frac{5.3}{50} \quad \frac{5.0}{5} \quad 5.2 \quad \frac{4.8}{5} \quad \frac{5.2}{13} \quad \frac{4.8}{14} \quad \frac{4.7}{50}$$

Sta	+	π	-	Elev
		718.76		
5+50			4.0	14.8
6			4.9	13.9
+50			5.2	13.6
7			5.5	13.3
+50			6.8	12.0
8			8.4	10.4
+50			9.2	09.6
T.P	2.60	912.58 ✓	8.78	909.98 ✓
9			3.3	09.3
+50			4.1	08.5
10			4.8	07.8
+50			5.1	07.5
11			4.7	07.9

LT

Z

PT

$$\frac{4.8}{50} \quad \frac{4.5}{19}$$

$$4.0 \quad \frac{4.4}{12} \quad \frac{4.0}{14} \quad \frac{4.1}{50}$$

$$\frac{5.5}{50} \quad \frac{4.9}{7} \quad 4.9 \quad \frac{4.5}{3} \quad \frac{5.0}{12} \quad \frac{4.4}{13} \quad \frac{4.1}{50}$$

$$\frac{5.9}{50} \quad \frac{5.0}{7} \quad \frac{5.4}{6} \quad 5.2 \quad \frac{5.1}{12} \quad \frac{4.5}{13} \quad \frac{4.4}{50}$$

$$\frac{6.2}{50} \quad \frac{5.6}{8} \quad \frac{6.0}{7} \quad 5.5 \quad \frac{5.7}{11} \quad \frac{5.2}{12} \quad \frac{4.9}{50}$$

$$\frac{7.2}{50} \quad \frac{6.7}{9} \quad \frac{7.1}{8} \quad 6.8 \quad \frac{6.6}{7} \quad \frac{7.0}{11} \quad \frac{6.4}{12} \quad \frac{6.3}{32} \quad \frac{6.2}{50}$$

$$\frac{9.2}{50} \quad \frac{8.8}{29} \quad \frac{8.3}{9} \quad \frac{8.7}{8} \quad \frac{6.4}{5} \quad 8.4 \quad \frac{8.2}{7} \quad \frac{8.4}{11} \quad \frac{7.8}{12} \quad \frac{7.5}{33} \quad \frac{6.8}{50}$$

$$\frac{10.1}{50} \quad \frac{10.1}{32} \quad \frac{9.6}{10} \quad 9.2 \quad \frac{9.0}{7} \quad \frac{9.3}{11} \quad \frac{8.8}{12} \quad \frac{7.8}{50}$$

$$\frac{3.9}{50} \quad \frac{3.8}{26} \quad \frac{3.4}{8} \quad \frac{3.8}{7} \quad 3.3 \quad \frac{3.5}{11} \quad \frac{3.0}{12} \quad \frac{2.4}{31} \quad \frac{2.0}{50}$$

$$\frac{4.6}{50} \quad \frac{4.3}{30} \quad \frac{4.3}{8} \quad \frac{4.8}{7} \quad 4.1 \quad \frac{4.2}{7} \quad \frac{4.7}{11} \quad \frac{4.2}{12} \quad \frac{4.1}{34} \quad \frac{3.9}{50}$$

$$\frac{5.8}{50} \quad \frac{5.7}{39} \quad \frac{5.1}{9} \quad \frac{5.5}{8} \quad 4.8 \quad \frac{5.3}{11} \quad \frac{4.9}{20} \quad \frac{4.7}{35} \quad \frac{4.5}{50}$$

$$\frac{4.1}{50} \quad \frac{4.6}{32} \quad \frac{5.0}{13} \quad \frac{5.3}{11} \quad 5.1 \quad \frac{5.7}{7} \quad \frac{5.5}{8} \quad \frac{5.9}{12} \quad \frac{6.3}{39} \quad \frac{6.6}{50}$$

$$\frac{3.6}{50} \quad \frac{4.2}{28} \quad \frac{4.4}{11} \quad \frac{4.8}{11} \quad 4.7 \quad \frac{4.8}{5} \quad \frac{5.4}{7} \quad \frac{5.2}{8} \quad \frac{5.7}{34} \quad \frac{6.0}{50}$$

Sta + π - Elev

912.58[✓]

11+50 4.3 08.3.

12 4.1 08.5.

+50

+50 3.8 08.8.

13 3.4 09.2.

+50

3.5 09.1.

B.M. 119 911.39[✓]

14 4.2 08.4.

+50

4.8 07.8.

15 4.8 07.8.

T.P. (B.M.) 0.67 912.06[✓] 911.39

+50

4.0 08.1.

16 4.1 08.0.

+50

4.4 07.7.

17 4.8 07.3.

Ditch Rt. +15

Lt

K

Rt

12

$$\frac{5.4}{50} \frac{4.9}{28} \frac{4.6}{8} \frac{4.9}{7} 4.3 \frac{4.4}{11} \frac{4.0}{12} \frac{3.3}{33} \frac{2.4}{50}$$

$$\frac{5.4}{50} \frac{4.9}{29} \frac{4.4}{9} \frac{4.7}{8} 4.1 \frac{4.4}{11} \frac{3.9}{12} \frac{3.5}{22} \frac{2.2}{50}$$

$$\frac{4.8}{50} \frac{4.7}{19} \frac{3.7}{9} \frac{4.3}{8} 3.8 \frac{3.9}{11} \frac{3.4}{12} \frac{2.2}{50}$$

$$\frac{4.5}{50} \frac{4.3}{19} \frac{3.4}{9} \frac{4.1}{8} 3.4 \frac{3.5}{11} \frac{3.1}{12} \frac{2.1}{26} \frac{1.8}{50}$$

$$\frac{4.9}{50} \frac{4.3}{15} \frac{3.6}{8} \frac{4.1}{7} 3.5 \frac{3.8}{12} \frac{3.4}{13} \frac{2.4}{34} \frac{2.0}{50}$$

Spike in 24" Oak 35' Rt sta. 13 + 25

$$\frac{5.3}{50} \frac{5.0}{19} \frac{4.5}{9} \frac{4.8}{8} 4.2 \frac{4.2}{11} \frac{4.1}{13} \frac{2.9}{50}$$

$$\frac{6.0}{50} \frac{5.6}{18} \frac{5.1}{8} \frac{5.4}{7} 4.8 \frac{5.2}{11} \frac{4.7}{12} \frac{4.2}{31} \frac{3.6}{50}$$

$$\frac{5.9}{50} \frac{5.6}{18} \frac{5.1}{9} \frac{5.6}{8} 4.8 \frac{5.1}{10} \frac{4.8}{11} \frac{4.3}{28} \frac{3.7}{50}$$

$$\frac{4.9}{50} \frac{4.2}{9} \frac{4.9}{8} 4.0 \frac{4.6}{11} \frac{4.2}{12} \frac{3.3}{50}$$

$$\frac{4.6}{50} \frac{4.3}{10} \frac{4.7}{8} 4.1 \frac{4.6}{10} \frac{4.1}{11} \frac{3.7}{50}$$

$$\frac{4.7}{50} \frac{4.6}{11} \frac{5.2}{10} 4.4 \frac{4.1}{9} \frac{4.6}{10} \frac{4.2}{50}$$

$$\frac{5.5}{50} \frac{5.2}{10} \frac{5.5}{9} 4.8 \frac{4.9}{10} \frac{4.8}{50}$$

$$\frac{5.1}{25} \frac{5.3}{50} \frac{5.5}{150} \frac{5.5}{200}$$

Sta. + π - Elev

17+50 912.66 ✓ 4.6 07.5.

18 3.3 08.8.

+50 2.3 09.8.

T.P. 4.10 915.12 ✓ 1.04 911.02 ✓

19 5.0 10.1.

+50 5.1 10.0.

20 5.8 09.3.

+50 6.6 08.5.

21 6.1 09.0.

+50 5.0 10.1.

22 4.8 10.3.

+50 4.9 10.2.

23 4.9 10.2.

Lt.

L

2t

$$\frac{5.0}{50} \quad \frac{5.0}{11} \quad \frac{5.4}{10} \quad 4.6 \quad \frac{5.1}{10} \quad \frac{4.7}{11} \quad \frac{4.6}{50}$$

$$\frac{3.2}{50} \quad \frac{3.4}{12} \quad \frac{4.0}{11} \quad 3.3 \quad \frac{3.4}{8} \quad \frac{3.3}{50}$$

$$\frac{2.0}{50} \quad \frac{2.0}{13} \quad \frac{2.5}{12} \quad 2.3 \quad \frac{2.7}{8} \quad \frac{2.6}{9} \quad \frac{3.4}{50}$$

$$\frac{4.8}{50} \quad \frac{4.8}{11} \quad \frac{5.3}{10} \quad 5.0 \quad \frac{5.5}{8} \quad \frac{5.1}{9} \quad \frac{6.8}{50}$$

$$\frac{4.7}{50} \quad \frac{4.9}{10} \quad \frac{5.3}{8} \quad 5.1 \quad \frac{5.5}{10} \quad \frac{5.1}{12} \quad \frac{5.8}{50}$$

$$\frac{5.5}{50} \quad \frac{5.9}{8} \quad \frac{6.4}{7} \quad 5.8 \quad \frac{6.2}{11} \quad \frac{5.7}{12} \quad \frac{5.8}{50}$$

$$\frac{6.4}{50} \quad \frac{6.7}{35} \quad \frac{6.7}{8} \quad \frac{7.1}{6} \quad 6.6 \quad \frac{7.0}{12} \quad \frac{6.3}{13} \quad \frac{6.5}{50}$$

$$\frac{5.5}{50} \quad \frac{6.0}{8} \quad \frac{6.6}{7} \quad 6.1 \quad \frac{6.6}{12} \quad \frac{6.1}{13} \quad \frac{6.7}{50}$$

$$\frac{5.0}{50} \quad \frac{4.9}{8} \quad \frac{5.3}{6} \quad 5.0 \quad \frac{5.1}{13} \quad \frac{4.8}{14} \quad \frac{5.3}{50}$$

$$\frac{5.2}{50} \quad \frac{4.8}{8} \quad \frac{5.1}{6} \quad 4.8 \quad \frac{5.0}{14} \quad \frac{4.7}{15} \quad \frac{5.2}{50}$$

$$\frac{4.8}{50} \quad \frac{4.8}{7} \quad \frac{5.2}{6} \quad 4.9 \quad \frac{5.1}{12} \quad \frac{4.8}{13} \quad \frac{4.8}{50}$$

$$\frac{5.2}{50} \quad \frac{4.9}{6} \quad \frac{5.4}{5} \quad 4.9 \quad \frac{5.3}{12} \quad \frac{4.8}{14} \quad \frac{5.0}{50}$$

Sta	+	π	-	Elev.
		915.12 ✓		
23+50			5.9	09.2
B.M			4.38	910.74 ✓
24			6.5	08.6
+				
+50			6.2	08.9
T.P.	443	916.45 ✓	3.10	912.02 ✓
25			6.7	09.8
+				
+50			6.0	10.5
26			5.0	11.5
+				
+50			5.2	11.3
27			5.7	10.8
+				
+50			5.6	10.9
28			5.1	11.4
+				
+50			5.2	11.3
29			4.2	12.3

Lt.

C

Rt.

$$\frac{6.0}{50} \quad \frac{6.3}{6} \quad \frac{6.8}{5} \quad 5.9 \quad \frac{6.3}{12} \quad \frac{6.0}{13} \quad \frac{5.8}{50}$$

Spike in 20" Dat 33' Lt. Sta 22+98

$$\frac{6.5}{50} \quad \frac{6.6}{6} \quad \frac{7.2}{5} \quad 6.5 \quad \frac{7.2}{12} \quad \frac{6.5}{13} \quad \frac{6.4}{50}$$

$$\frac{6.2}{50} \quad \frac{6.1}{6} \quad \frac{6.5}{5} \quad 6.2 \quad \frac{6.5}{13} \quad \frac{5.8}{14} \quad \frac{5.7}{50}$$

$$\frac{5.8}{50} \quad \frac{7.6}{6} \quad \frac{7.1}{5} \quad 6.7 \quad \frac{7.0}{10} \quad \frac{7.1}{14} \quad \frac{7.2}{50}$$

$$\frac{4.5}{50} \quad \frac{4.1}{38} \quad \frac{5.2}{9} \quad \frac{6.0}{8} \quad 6.0 \quad \frac{6.3}{11} \quad \frac{6.3}{26} \quad \frac{7.3}{50}$$

$$\frac{4.2}{50} \quad \frac{4.5}{6} \quad \frac{5.0}{4} \quad 5.0 \quad \frac{5.6}{14} \quad \frac{5.4}{24} \quad \frac{6.4}{50}$$

$$\frac{4.6}{50} \quad \frac{4.8}{5} \quad \frac{5.3}{4} \quad 5.2 \quad \frac{5.4}{15} \quad \frac{5.0}{16} \quad \frac{5.6}{50}$$

$$\frac{5.8}{50} \quad \frac{5.4}{5} \quad \frac{5.8}{4} \quad 5.7 \quad \frac{5.2}{10} \quad \frac{5.7}{15} \quad \frac{5.2}{16} \quad \frac{4.8}{50}$$

$$\frac{6.2}{50} \quad \frac{5.6}{31} \quad \frac{5.3}{6} \quad 5.6 \quad \frac{5.1}{9} \quad \frac{5.7}{15} \quad \frac{5.2}{16} \quad \frac{5.3}{50}$$

$$\frac{5.8}{50} \quad \frac{5.1}{5} \quad \frac{5.6}{4} \quad 5.1 \quad \frac{5.5}{15} \quad \frac{5.3}{16} \quad \frac{5.7}{50}$$

$$\frac{5.6}{50} \quad \frac{5.4}{20} \quad \frac{5.1}{6} \quad \frac{5.4}{5} \quad 5.2 \quad \frac{5.0}{11} \quad \frac{5.5}{14} \quad \frac{5.0}{16} \quad \frac{5.7}{50}$$

$$\frac{3.7}{50} \quad \frac{4.1}{6} \quad \frac{4.7}{5} \quad 4.2 \quad \frac{4.1}{10} \quad \frac{4.8}{14} \quad \frac{4.5}{16} \quad \frac{5.1}{50}$$

Sta	+	π	-	Elev
		916.45 ✓		
29+50				13.1 .
T.P.	2.12	916.26 ✓	2.31	914.14 ✓
30			2.8	13.5 .
+50			2.7	13.6 .
31			3.2	13.1 .
+50			4.3	12.0 .
32			4.8	11.5 .
+50			3.8	12.5 .
33			3.2	13.1 .
+31			4.5	11.8 .
+35			4.7	11.6 .
+45			4.6	11.7 .
+64.05			3.9	12.4 .
B.M.			3.27	912.99 ✓
				(913.03)

Lt R 2 Rt

$\frac{2.8}{50}$ $\frac{3.0}{6}$ $\frac{3.7}{5}$ 3.4 $\frac{3.8}{14}$ $\frac{3.6}{16}$ $\frac{4.2}{50}$

$\frac{1.9}{50}$ $\frac{2.2}{5}$ $\frac{2.9}{4}$ 2.8 $\frac{2.4}{5}$ $\frac{2.7}{10}$ $\frac{3.3}{15}$ $\frac{2.6}{16}$ $\frac{3.6}{50}$

$\frac{2.2}{50}$ $\frac{2.6}{5}$ $\frac{3.0}{4}$ 2.7 $\frac{2.7}{10}$ $\frac{3.2}{13}$ $\frac{2.9}{14}$ $\frac{3.8}{50}$

$\frac{2.9}{50}$ $\frac{3.1}{5}$ $\frac{3.5}{4}$ 3.2 $\frac{3.8}{14}$ $\frac{3.4}{15}$ $\frac{4.5}{50}$

$\frac{4.1}{50}$ $\frac{4.3}{6}$ $\frac{4.7}{5}$ 4.3 $\frac{4.8}{13}$ $\frac{4.5}{14}$ $\frac{5.4}{50}$

$\frac{4.8}{50}$ $\frac{4.9}{6}$ $\frac{5.1}{5}$ 4.8 $\frac{5.2}{14}$ $\frac{4.9}{15}$ $\frac{5.1}{50}$

$\frac{3.7}{50}$ $\frac{3.7}{8}$ $\frac{4.2}{7}$ 3.8 $\frac{4.4}{13}$ $\frac{4.0}{14}$ $\frac{4.1}{50}$

$\frac{3.0}{50}$ $\frac{3.2}{9}$ $\frac{3.6}{6}$ 3.2 $\frac{3.6}{13}$ $\frac{3.2}{14}$ $\frac{3.6}{50}$

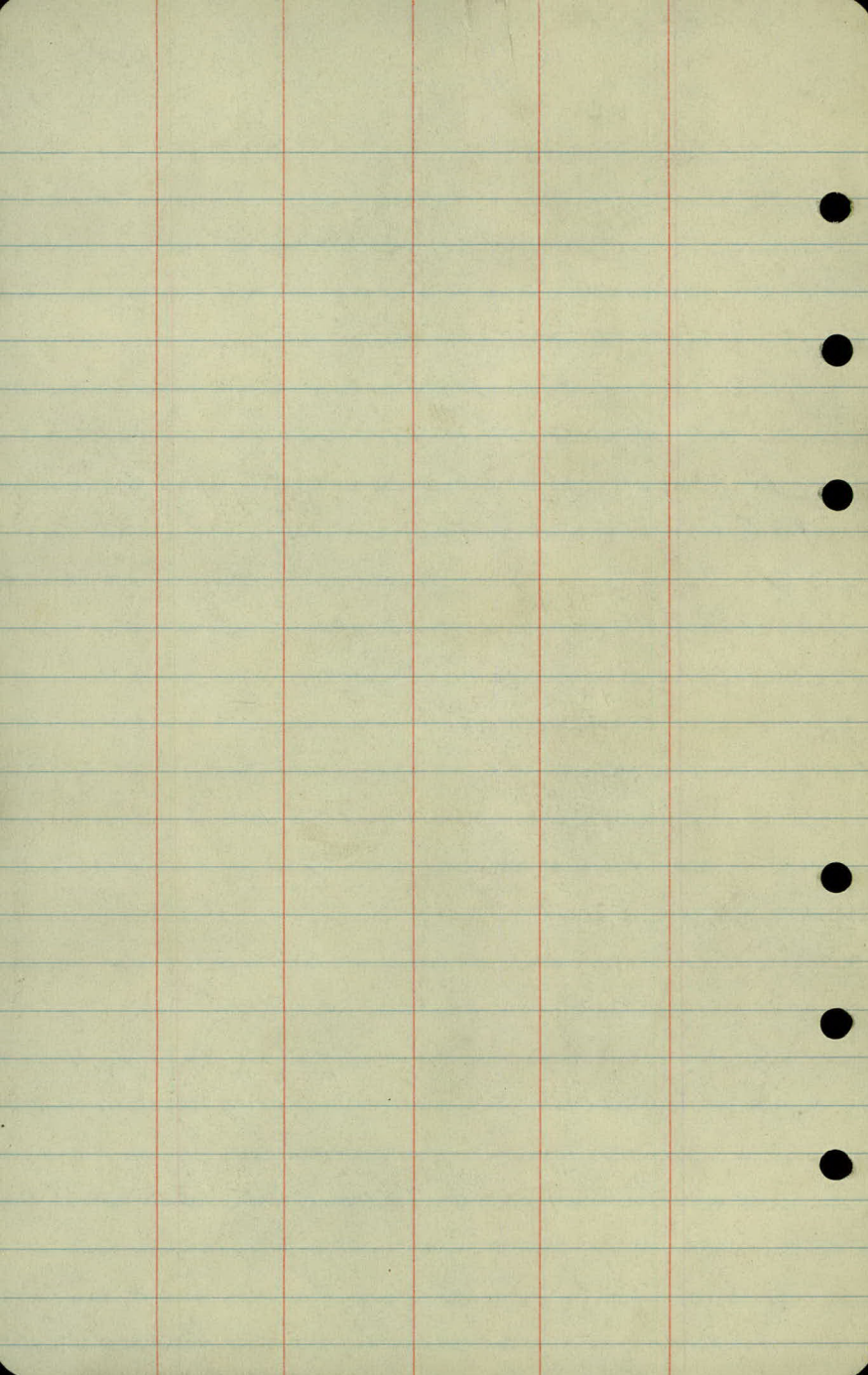
$\frac{2.8}{50}$ $\frac{3.0}{26}$ $\frac{4.1}{18}$ $\frac{4.4}{6}$ 4.5 $\frac{4.4}{10}$ $\frac{4.1}{17}$ $\frac{3.2}{24}$ $\frac{3.3}{50}$

$\frac{6.2}{50}$ $\frac{6.2}{26}$ $\frac{5.2}{15}$ $\frac{4.6}{6}$ 4.7 $\frac{4.9}{12}$ $\frac{5.5}{15}$ $\frac{6.0}{24}$ $\frac{6.2}{50}$

$\frac{4.2}{50}$ $\frac{4.3}{11}$ $\frac{4.7}{8}$ 4.6 $\frac{4.5}{10}$ $\frac{4.4}{25}$ $\frac{4.5}{50}$

$\frac{3.7}{50}$ 3.9 $\frac{3.9}{50}$

Spike in 15" Cottonwood N.E. Cor. Eastwood



Eastwood Road

Slope Stakes

Sta	+	π	-	Elev.
B.M.	3.04	916.78 ⁸		913.74
0+50				12.3
1				12.3
+50				12.4
2				12.4
+50				12.5
3				12.5
+50				12.6
4				12.6
+50				12.7
5				12.7
+50				12.6
6				12.4
T.P	3.18	916.97	2.99	913.79

G. R.

Spike in 8" Oak 45' Lt. Sta 0+65

4.5	$\begin{array}{r} 4.3 \\ C0.2 \\ \hline 2.5 \\ 5.4 \\ \hline DC1.1 \\ 23.2 \end{array}$	$\begin{array}{r} 4.4 \\ C0.1 \\ \hline 5.2 \\ \hline FO.7 \end{array}$	$\begin{array}{r} 4.6 \\ DC1.9 \\ \hline 24.8 \\ 5.3 \\ \hline DC1.2 \\ 23.4 \end{array}$
-----	---	---	---

4.5	$\begin{array}{r} 5.4 \\ \hline DC1.1 \\ 23.2 \end{array}$	$\begin{array}{r} 5.2 \\ \hline FO.7 \end{array}$	$\begin{array}{r} 5.3 \\ \hline DC1.2 \\ 23.4 \end{array}$
-----	--	---	--

4.4	$\begin{array}{r} 5.5 \\ DC0.9 \\ \hline 23.8 \end{array}$	$\begin{array}{r} 5.3 \\ \hline FO.9 \end{array}$	$\begin{array}{r} 5.8 \\ DC0.6 \\ \hline 22.2 \end{array}$
-----	--	---	--

4.4	$\begin{array}{r} 5.0 \\ DC1.4 \\ \hline 23.8 \end{array}$	$\begin{array}{r} 5.0 \\ \hline FO.6 \end{array}$	$\begin{array}{r} 5.2 \\ \hline DC1.2 \\ 23.4 \end{array}$
-----	--	---	--

4.3	$\begin{array}{r} 4.8 \\ DC1.5 \\ \hline 24.0 \end{array}$	$\begin{array}{r} 4.8 \\ \hline FO.5 \end{array}$	$\begin{array}{r} 4.8 \\ DC1.5 \\ \hline 24.0 \end{array}$
-----	--	---	--

4.3	$\begin{array}{r} 5.3 \\ DC1.0 \\ \hline 23.0 \end{array}$	$\begin{array}{r} 5.1 \\ \hline FO.8 \end{array}$	$\begin{array}{r} 4.8 \\ DC1.5 \\ \hline 24.0 \end{array}$
-----	--	---	--

4.2	$\begin{array}{r} 5.6 \\ DC0.6 \\ \hline 22.2 \end{array}$	$\begin{array}{r} 5.6 \\ \hline FO.4 \end{array}$	$\begin{array}{r} 5.2 \\ DC1.0 \\ \hline 23.0 \end{array}$
-----	--	---	--

4.2	$\begin{array}{r} 4.8 \\ DC1.4 \\ \hline 23.8 \end{array}$	$\begin{array}{r} 5.0 \\ \hline FO.8 \end{array}$	$\begin{array}{r} 5.0 \\ DC1.2 \\ \hline 23.4 \end{array}$
-----	--	---	--

4.1	$\begin{array}{r} 4.4 \\ DC1.7 \\ \hline 24.4 \end{array}$	$\begin{array}{r} 4.5 \\ \hline FO.4 \end{array}$	$\begin{array}{r} 4.0 \\ C0.1 \\ \hline 2.5 \end{array}$
-----	--	---	--

4.1	$\begin{array}{r} 3.3 \\ C0.8 \\ \hline 2.5 \end{array}$	$\begin{array}{r} 3.4 \\ \hline C0.7 \end{array}$	$\begin{array}{r} 2.7 \\ C1.4 \\ \hline 2.5 \end{array}$
-----	--	---	--

4.2	$\begin{array}{r} 2.6 \\ C1.6 \\ \hline 2.5 \end{array}$	$\begin{array}{r} 2.4 \\ \hline C1.8 \end{array}$	$\begin{array}{r} 2.1 \\ C2.1 \\ \hline 2.5 \end{array}$
-----	--	---	--

4.4	$\begin{array}{r} 3.3 \\ C1.1 \\ \hline 2.5 \end{array}$	$\begin{array}{r} 3.0 \\ C1.4 \end{array}$	$\begin{array}{r} 2.5 \\ C1.9 \\ \hline 2.5 \end{array}$
-----	--	--	--

5+0	+	$\overline{\uparrow}$ 1700	-	Elev.
		916.97		

6+50				12.1
------	--	--	--	------

7				11.7
---	--	--	--	------

+50				11.4
-----	--	--	--	------

8				11.0
---	--	--	--	------

+50				10.7
-----	--	--	--	------

9				10.3
---	--	--	--	------

+50				10.0
-----	--	--	--	------

10				9.8
----	--	--	--	-----

+50				9.6
-----	--	--	--	-----

11				9.5
----	--	--	--	-----

+50				9.5
-----	--	--	--	-----

T.P.	3.54	912.61	7.90	909.07
------	------	--------	------	--------

12				9.4
----	--	--	--	-----

G. R.

$$\begin{array}{r} 3.6 \\ C 1.3 \\ \hline 2.5 \end{array} \quad \begin{array}{r} 3.3 \\ C 1.6 \\ \hline \end{array} \quad \begin{array}{r} 2.6 \\ C 2.3 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 4.1 \\ C 1.2 \\ \hline 2.5 \end{array} \quad \begin{array}{r} 3.8 \\ C 1.5 \\ \hline \end{array} \quad \begin{array}{r} 3.5 \\ C 1.8 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 5.2 \\ C 0.4 \\ \hline 2.5 \end{array} \quad \begin{array}{r} 5.1 \\ C 0.5 \\ \hline \end{array} \quad \begin{array}{r} 4.6 \\ C 1.0 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 6.1 \\ DC 1.1 \\ \hline 23.2 \end{array} \quad \begin{array}{r} 6.7 \\ F 0.7 \\ \hline \end{array} \quad \begin{array}{r} 5.9 \\ C 0.1 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 8.2 \\ DC 0.1 \\ \hline 21.2 \end{array} \quad \begin{array}{r} 7.5 \\ F 1.2 \\ \hline \end{array} \quad \begin{array}{r} 6.6 \\ DC 1.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 8.2 \\ DC 0.5 \\ \hline 22.0 \end{array} \quad \begin{array}{r} 7.7 \\ F 1.0 \\ \hline \end{array} \quad \begin{array}{r} 7.0 \\ DC 1.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 8.7 \\ DC 0.3 \\ \hline 21.6 \end{array} \quad \begin{array}{r} 8.7 \\ F 1.7 \\ \hline \end{array} \quad \begin{array}{r} 8.7 \\ DC 0.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 9.8 \\ F 2.6 \\ \hline 18.2 \end{array} \quad \begin{array}{r} 9.4 \\ F 2.2 \\ \hline \end{array} \quad \begin{array}{r} 9.4 \\ F 2.2 \\ \hline 17.4 \end{array}$$

$$\begin{array}{r} 10.4 \\ F 3.0 \\ \hline 19.0 \end{array} \quad \begin{array}{r} 9.6 \\ F 2.2 \\ \hline \end{array} \quad \begin{array}{r} 9.4 \\ DC 0.0 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 9.7 \\ F 2.2 \\ \hline 17.4 \end{array} \quad \begin{array}{r} 9.3 \\ F 1.8 \\ \hline \end{array} \quad \begin{array}{r} 9.0 \\ DC 0.5 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 9.5 \\ DC 0.0 \\ \hline 21.8 \end{array} \quad \begin{array}{r} 8.9 \\ F 1.4 \\ \hline \end{array} \quad \begin{array}{r} 8.0 \\ DC 1.5 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ DC 0.4 \\ \hline 21.8 \end{array} \quad \begin{array}{r} 4.3 \\ F 1.1 \\ \hline \end{array} \quad \begin{array}{r} 3.4 \\ DC 1.8 \\ \hline 24.6 \end{array}$$

Sta	+	π	-	Elev	
		912.61			
12 + 50				9.4	
13				9.3	
B.M.			121	911.40	911.39
+ 50				9.3	
14				9.2	
+ 50				9.2	
15				9.1	
+ 50				9.1	
16				9.0	
+ 50				9.0	
17				09.0	
+ 50				9.1	
18				9.2	
T.P.	3.99	915.28	132	911.29	

G.R.

3.2	$\frac{4.3}{DC0.9}$ 22.8	$\frac{3.8}{FD.6}$	$\frac{3.2}{CO.0}$ 25
-----	-----------------------------	--------------------	--------------------------

3.3	$\frac{4.2}{DC1.1}$ 23.2	$\frac{3.5}{FD.2}$	$\frac{2.2}{C11.6}$ 25.0
-----	-----------------------------	--------------------	-----------------------------

Spk 24' 004 35' R1 13125

3.3	$\frac{4.2}{DC1.1}$ 23.2	$\frac{3.6}{FD.3}$	$\frac{2.8}{CO.5}$ 25
-----	-----------------------------	--------------------	--------------------------

3.4	$\frac{4.8}{DC0.6}$ 22.2	$\frac{4.3}{FD.9}$	$\frac{3.8}{DC1.6}$ 24.2
-----	-----------------------------	--------------------	-----------------------------

3.4	$\frac{5.8}{FD.4}$ 17.8	$\frac{5.2}{FI.8}$	$\frac{4.0}{DC1.0}$ 23
-----	----------------------------	--------------------	---------------------------

3.5	$\frac{5.7}{FD.2}$ 17.4	$\frac{5.0}{FI.5}$	$\frac{4.5}{DC1.0}$ 23.0
-----	----------------------------	--------------------	-----------------------------

3.5	$\frac{5.5}{DC0.0}$ 21.0	$\frac{4.9}{FI.4}$	$\frac{4.5}{DC1.0}$ 23.0
-----	-----------------------------	--------------------	-----------------------------

3.6	$\frac{5.3}{DC0.3}$ 21.6	$\frac{4.8}{FI.2}$	$\frac{4.7}{DC0.9}$ 22.8
-----	-----------------------------	--------------------	-----------------------------

3.6	$\frac{5.5}{DC0.1}$ 21.0	$\frac{5.2}{FI.6}$	$\frac{5.2}{DC0.4}$ 21.8
-----	-----------------------------	--------------------	-----------------------------

3.6	$\frac{5.9}{FD.3}$ 17.6	$\frac{5.6}{FD.0}$	$\frac{5.6}{DC0.0}$ 21.0
-----	----------------------------	--------------------	-----------------------------

3.5	$\frac{5.8}{FD.3}$ 17.6	$\frac{5.4}{FI.9}$	$\frac{5.3}{DC0.2}$ 21.4
-----	----------------------------	--------------------	-----------------------------

3.4	$\frac{4.1}{DC1.3}$ 23.6	$\frac{4.0}{FD.6}$	$\frac{3.9}{DC1.5}$ 24.0
-----	-----------------------------	--------------------	-----------------------------

Sta. + $\bar{A}$ - Elev

915.28

18+50

9.3

19

9.5

+50

9.6

20

9.7

+50

9.9

21

10.0

+50

10.2

22

10.3

+50

10.4

23

10.6

+50

10.8

24

10.9

G.R.

6.0

$$\begin{array}{r} 5.2 \\ \text{CO.8} \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.6 \\ \text{CO.4} \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ \text{DC1.8} \\ \hline 24.6 \end{array}$$

5.8

$$\begin{array}{r} 5.0 \\ \text{CO.8} \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.2 \\ \text{CO.6} \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ \text{DC1.9} \\ \hline 24.8 \end{array}$$

5.7

$$\begin{array}{r} 5.1 \\ \text{CO.6} \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.2 \\ \text{CO.5} \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ \text{CO.2} \\ \hline 25 \end{array}$$

5.6

$$\begin{array}{r} 6.0 \\ \text{DC1.6} \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 6.0 \\ \text{FO.4} \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ \text{DC1.7} \\ \hline 24.4 \end{array}$$

5.4

$$\begin{array}{r} 7.1 \\ \text{DC0.3} \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 6.8 \\ \text{F1.4} \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ \text{DC1.0} \\ \hline 23.0 \end{array}$$

5.3

$$\begin{array}{r} 6.2 \\ \text{DC1.1} \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 6.3 \\ \text{F1.0} \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ \text{DC0.8} \\ \hline 22.6 \end{array}$$

5.1

$$\begin{array}{r} 5.1 \\ \text{DC0.0} \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.2 \\ \text{FO.1} \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ \text{CO.1} \\ \hline 25 \end{array}$$

5.0

$$\begin{array}{r} 5.1 \\ \text{DC1.9} \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} 5.00 \\ \text{FO.0} \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ \text{CO.0} \\ \hline 25 \end{array}$$

4.9

$$\begin{array}{r} 5.1 \\ \text{DC1.8} \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 5.0 \\ \text{FO.1} \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ \text{DC1.8} \\ \hline 24.6 \end{array}$$

4.7

$$\begin{array}{r} 5.3 \\ \text{DC1.4} \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 5.2 \\ \text{FO.5} \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ \text{DC1.6} \\ \hline 24.2 \end{array}$$

4.5

$$\begin{array}{r} 6.6 \\ \text{F2.1} \\ \hline 17.2 \end{array}$$

$$\begin{array}{r} 6.4 \\ \text{F1.9} \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ \text{DC0.4} \\ \hline 21.8 \end{array}$$

4.4

$$\begin{array}{r} 7.1 \\ \text{F2.7} \\ \hline 18.4 \end{array}$$

$$\begin{array}{r} 6.9 \\ \text{F2.5} \\ \hline \end{array}$$

$$\begin{array}{r} 6.9 \\ \text{F2.5} \\ \hline 18.0 \end{array}$$

Sta + π - Elev.

915.28

24+50 11.1

25 11.2

T.P. 5.06 916.21 4.13 911.15

+50 11.4

26 11.5

+50 11.7

27 11.8

+50 12.0

28 12.1

+50 12.3

29 12.4

T.P. 6.38 918.51 4.08 912.13

+50 12.6

30 12.7

G.R.

1.1
4.2

6.5
F2.3
17.6

6.5
F2.2

6.1
DC0.1
21.2

4.1

5.3
DC0.8
22.6

5.7
F1.6

6.1
DC0.0
21.0

4.8

4.6
C0.2
25

5.7
F0.9

6.4
DC0.4
21.8

4.7

4.1
C0.6
25

4.8
F0.1

5.1
DC1.6
24.2

4.5

4.5
C0.0
25

5.0
F0.5

4.7
DC1.8
24.6

4.4

5.4
DC1.0
23.0

5.6
F1.2

4.8
DC1.6
24.2

4.2

5.3
DC0.9
22.8

5.4
F1.2

5.1
DC1.1
23.2

4.1

5.0
DC0.1
23.2

5.1
F1.0

5.0
DC1.1
23.2

3.9

5.3
DC0.6
22.2

5.8
F1.1

4.8
DC1.1
23.2

3.8

3.8
C0.0
25

4.1
F0.3

4.5
DC1.3
23.6

5.9

5.1
C0.8
25

5.6
C0.3

5.6
C0.3
25

5.8

4.5
C1.3
25

5.1
C0.7

5.4
C0.8
25

Sta + π - Elev

918.51

30+50

12.7

31

12.7

+50

12.7

32

12.6

+50

12.5

33

12.4

+31

12.3

B.M.

5.48

913.03

(913.03)

G R

5.8

$$\begin{array}{r} 4.7 \\ C 1.1 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.0 \\ C 0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ C 0.3 \\ \hline 25 \end{array}$$

5.8

$$\begin{array}{r} 5.3 \\ C 0.5 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.6 \\ C 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.0 \\ DC 1.8 \\ \hline 24.6 \end{array}$$

5.8

$$\begin{array}{r} 6.4 \\ DC 1.4 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 6.6 \\ F 0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 2.4 \\ DC 0.7 \\ \hline 22.4 \end{array}$$

5.9

$$\begin{array}{r} 2.1 \\ DC 0.8 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 7.2 \\ F 1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 7.2 \\ DC 0.7 \\ \hline 22.4 \end{array}$$

6.0

$$\begin{array}{r} 6.0 \\ C 0.0 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 6.2 \\ F 0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ DC 1.8 \\ \hline 24.6 \end{array}$$

6.1

$$\begin{array}{r} 5.4 \\ C 0.7 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.5 \\ C 0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ C 0.7 \\ \hline 25 \end{array}$$

6.2

$$\begin{array}{r} 5.2 \\ C 1.0 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 6.9 \\ F 0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ C 0.9 \\ \hline 25 \end{array}$$

15" Cot. NE Cor Eastwood & N.Co. Line Rd.

