

Bk. 22 Dr. 11A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

RED OAK DRIVE

From Sherwood Rd. To Co. Rd. "J"

Road Acc't. No. M-47

Date Filed 10-26-39

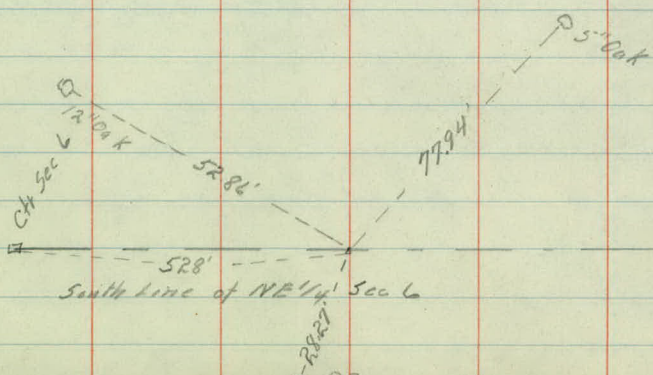
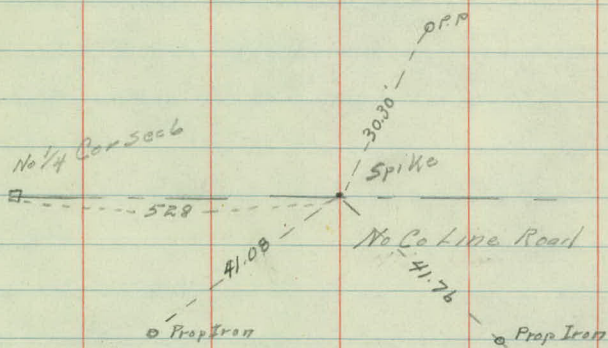
File

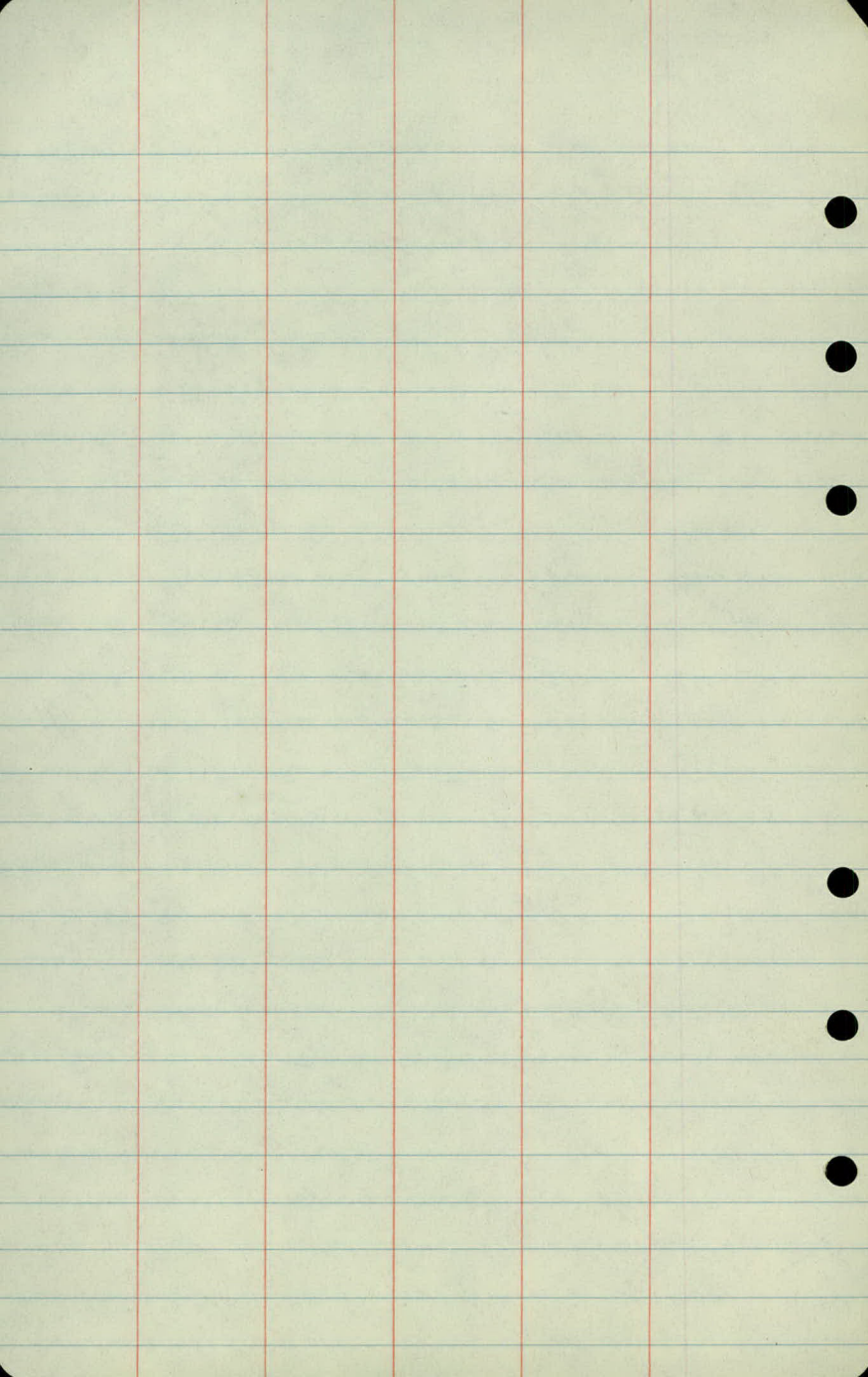
Alignment
Red Oak Drive

Sta Pt.

34+00.00 P.O.T.

0+00 P.O.T.





Topography
Red Oak Drive

6

5

4

3

2

1

0

Meadow

Mearlow

4
Trees 100'

+80 End Woods
Beg. Meadow

+100 End Woods 25'
+90 Ent

Woods

+25 Ent

Tree line 25'
10' Wagon trail

+31 Ent

+40 Beg Heavy
Woods

Woods

Scattered Oaks

School Dist #36
School

+25 Beg Woods

+25 Beg Trees

Sherwood Road

14

13

12

11

10

9

8

7

Meadow

Cultivated

+25 End Woods
Woods 25'x50'

+50 End Woods

Woods 25'x100'

Meadow

11' Wagon Trail

Trees 25'

Woods

+100 Trees 25'

+75 Trees 25'

Trees 75'

Meadow

Meadow

Trees 100'

21

20

19

18

17

16

15

14

+60 End Woods

+60 End Woods

Tree line 25'

Tree line 25'

+70 Ent

+50 Beg Woods 25'

+35 Beg Woods 25'
+30 Ent

Waste

Waste

10' Wagon Trail

+75 End Woods 25'

+100 End Woods
+90 Ent

Woods

Tree line 25'

Tree line 25'

+ Oaks

+25 Beg Oaks 25'

Meadow

+100 Beg Woods

28

27

26

25

24

23

22

21

+90 End Woods
Beg Brush

End Woods 7
+ Beg Brush

+60 Ent

Scattered Oaks

10' Wagon trail

Scattered Oaks

+50 Ent

+50 Beg Woods 25"
8 8 8 8 8

+00 Ent

Cultivated

+20 Ent
+00 Beg Woods 25"
8 8 8

Cultivated

34

34400 £ No Co Line

33

32

31

30

29

28

No Co Line Rd.

Gravel

Meadow

14' Wagon trail

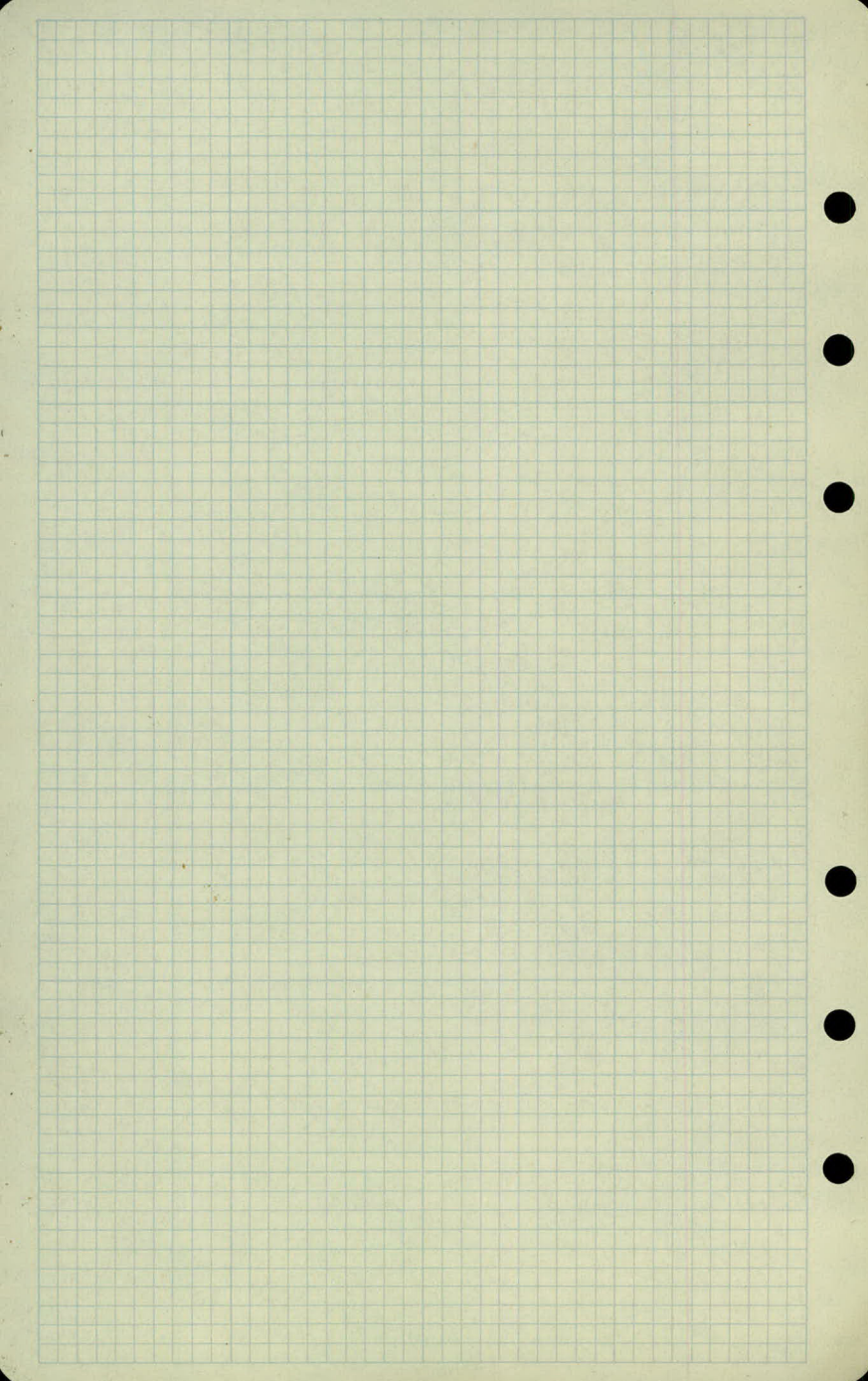
Meadow

+30 End Brush Bog Meadow

+00 End Brush

Brush

Brush



X Sections

Red Oak Drive

Sta	+	Σ	-	Elev
B.M.	3.44	921.21 ✓		917.77
0+00				16.9
0+50				17.1
1+00				16.9
+50				16.0
2				15.8
+50				15.9
3				16.1
+50				15.8
4				15.8
+50				15.1
5				13.6
T.P.	0.48	915.63 ✓	6.06	915.15 ✓
+50				11.6

Lt

L

At

Spk. in 10" oak 65' Lt Sta 0+35'

$$\frac{5.0}{50}$$

43

$$\frac{4.2}{50}$$

$$\frac{3.8}{50} \quad \frac{3.8}{5} \quad \frac{4.4}{4} \quad 4.1 \quad \frac{3.9}{6} \quad \frac{4.3}{15} \quad \frac{3.7}{16} \quad \frac{3.7}{50}$$

$$\frac{4.1}{50} \quad \frac{4.3}{7} \quad \frac{4.9}{6} \quad 4.3 \quad \frac{4.6}{14} \quad \frac{4.2}{16} \quad \frac{4.0}{50}$$

$$\frac{4.8}{50} \quad \frac{5.2}{7} \quad \frac{5.6}{7} \quad 5.2 \quad \frac{5.4}{12} \quad \frac{5.1}{14} \quad \frac{5.0}{38} \quad \frac{5.0}{50}$$

$$\frac{5.5}{50} \quad \frac{5.4}{9} \quad \frac{5.9}{8} \quad 5.4 \quad \frac{5.5}{10} \quad \frac{5.9}{11} \quad \frac{5.3}{13} \quad \frac{6.3}{25} \quad \frac{5.3}{50}$$

$$\frac{5.4}{50} \quad \frac{5.4}{10} \quad \frac{5.9}{9} \quad 5.3 \quad \frac{5.4}{9} \quad \frac{5.7}{11} \quad \frac{5.2}{12} \quad \frac{5.0}{50}$$

$$\frac{5.5}{50} \quad \frac{5.2}{11} \quad \frac{5.7}{10} \quad 5.1 \quad \frac{5.3}{8} \quad \frac{5.6}{10} \quad \frac{5.2}{11} \quad \frac{5.1}{50}$$

$$\frac{5.2}{50} \quad \frac{5.3}{12} \quad \frac{5.6}{11} \quad 5.4 \quad \frac{6.0}{9} \quad \frac{5.4}{10} \quad \frac{5.8}{50}$$

$$\frac{5.5}{50} \quad \frac{5.3}{11} \quad \frac{5.9}{10} \quad 5.4 \quad \frac{6.0}{9} \quad \frac{5.5}{10} \quad \frac{5.5}{36} \quad \frac{5.5}{50}$$

$$\frac{6.4}{50} \quad \frac{6.2}{11} \quad \frac{6.7}{10} \quad 6.1 \quad \frac{6.4}{7} \quad \frac{6.7}{10} \quad \frac{6.3}{11} \quad \frac{6.3}{37} \quad \frac{6.3}{50}$$

$$\frac{8.0}{50} \quad \frac{7.7}{11} \quad \frac{8.1}{10} \quad \frac{7.7}{6} \quad 7.6 \quad \frac{7.6}{7} \quad \frac{8.0}{9} \quad \frac{7.3}{10} \quad \frac{7.2}{30} \quad \frac{7.0}{50}$$

$$\frac{4.2}{50} \quad \frac{4.4}{39} \quad \frac{4.3}{11} \quad \frac{4.7}{10} \quad 4.0 \quad \frac{3.9}{7} \quad \frac{4.3}{10} \quad \frac{3.9}{11} \quad \frac{3.2}{26} \quad \frac{2.8}{50}$$

Sta + π - Elev

915.63

5+83

10.0

6+00

08.8

+50

08.0

7

07.7

+50

08.0

8+00

08.0

+50

08.3

9+00

09.0

+50

09.7

10

10.7

T.P.

2.21

915.40 ✓

2.44

913.19 ✓

+50

11.2 ✓

B.M.

2.62

915.40 ✓

2.62

912.78 ✓

11

10.3

LT

Z

PT

11

$$\frac{6.3}{50} \quad \frac{5.9}{11} \quad \frac{6.3}{10} \quad \frac{5.8}{5} \quad 5.6 \quad \frac{5.6}{8} \quad \frac{6.0}{11} \quad \frac{5.4}{12} \quad \frac{4.8}{19} \quad \frac{4.0}{50}$$

$$\frac{6.9}{50} \quad \frac{7.1}{26} \quad \frac{7.0}{11} \quad \frac{7.2}{10} \quad \frac{6.7}{5} \quad 6.8 \quad \frac{6.6}{8} \quad \frac{6.8}{11} \quad \frac{6.3}{13} \quad \frac{4.9}{50}$$

$$\frac{8.4}{50} \quad \frac{8.0}{11} \quad \frac{8.4}{10} \quad \frac{7.8}{5} \quad 7.6 \quad \frac{7.6}{9} \quad \frac{8.1}{11} \quad \frac{7.7}{12} \quad \frac{7.4}{50}$$

$$\frac{8.8}{50} \quad \frac{8.2}{11} \quad \frac{8.5}{10} \quad \frac{8.1}{5} \quad 7.9 \quad \frac{8.0}{9} \quad \frac{8.4}{10} \quad \frac{7.8}{11} \quad \frac{7.5}{16} \quad \frac{7.2}{50}$$

$$\frac{8.6}{50} \quad \frac{8.0}{9} \quad \frac{8.5}{8} \quad \frac{7.9}{4} \quad 7.6 \quad \frac{7.9}{11} \quad \frac{7.3}{12} \quad \frac{7.2}{15} \quad \frac{6.1}{50}$$

$$\frac{9.0}{50} \quad \frac{8.4}{26} \quad \frac{7.8}{11} \quad \frac{8.3}{10} \quad \frac{7.8}{4} \quad 7.6 \quad \frac{8.0}{9} \quad \frac{7.6}{10} \quad \frac{7.3}{24} \quad \frac{6.7}{50}$$

$$\frac{8.3}{50} \quad \frac{7.8}{25} \quad \frac{7.6}{11} \quad \frac{7.9}{10} \quad 7.3 \quad \frac{7.5}{11} \quad \frac{7.2}{12} \quad \frac{6.5}{33} \quad \frac{5.7}{50}$$

$$\frac{7.6}{50} \quad \frac{7.6}{28} \quad \frac{7.1}{10} \quad \frac{7.4}{9} \quad \frac{6.7}{4} \quad 6.6 \quad \frac{6.5}{10} \quad \frac{5.9}{27} \quad \frac{5.5}{50}$$

$$\frac{7.2}{50} \quad \frac{6.6}{27} \quad \frac{6.4}{10} \quad \frac{6.6}{9} \quad \frac{6.1}{6} \quad 5.9 \quad \frac{6.2}{10} \quad \frac{5.7}{11} \quad \frac{5.2}{27} \quad \frac{4.8}{50}$$

$$\frac{5.8}{50} \quad \frac{5.5}{32} \quad \frac{4.9}{11} \quad \frac{5.1}{10} \quad \frac{5.0}{4} \quad 4.9 \quad \frac{5.1}{11} \quad \frac{4.6}{12} \quad \frac{4.5}{30} \quad \frac{4.2}{50}$$

$$\frac{4.9}{50} \quad \frac{4.8}{24} \quad \frac{4.5}{9} \quad \frac{4.8}{8} \quad \frac{4.6}{5} \quad 4.2 \quad \frac{4.4}{9} \quad \frac{4.6}{12} \quad \frac{4.1}{13} \quad \frac{4.0}{29} \quad \frac{3.8}{50}$$

Spk in 15" Oak 75' RA Sta 10+95-

$$\frac{6.3}{50} \quad \frac{5.3}{25} \quad \frac{4.9}{8} \quad \frac{5.2}{9} \quad \frac{4.9}{4} \quad 5.1 \quad \frac{4.7}{9} \quad \frac{5.1}{13} \quad \frac{4.5}{14} \quad \frac{4.1}{33} \quad \frac{4.0}{50}$$

Sta	+	π	-	Elev
		915.40		
11	+50			10.1
12				08.9
	+50			08.7
13				07.7
	+50			09.3
14				10.2
	+50			10.4
15				11.3
T.P.	406	917.11 ✓	2.35	913.05 ✓
	+50			12.3
16				12.9
	+50			13.7
17				14.0

LT

L

PT

12

$\frac{7.7}{100} \frac{6.8}{50} \frac{5.8}{29} \frac{6.4}{8} \frac{5.8}{7} \frac{5.5}{3} \frac{5.3}{5.3} \frac{5.2}{10} \frac{5.6}{14} \frac{4.8}{15} \frac{4.7}{31} \frac{4.6}{50}$
 $\frac{8.6}{150} \frac{9.6}{200}$

$\frac{6.7}{50} \frac{6.4}{30} \frac{6.4}{8} \frac{6.8}{7} \frac{6.4}{3} \frac{6.5}{6.5} \frac{6.5}{9} \frac{7.0}{13} \frac{6.6}{14} \frac{6.9}{33} \frac{6.8}{50}$

$\frac{7.0}{50} \frac{6.8}{28} \frac{6.8}{9} \frac{7.2}{8} \frac{6.7}{6.7} \frac{6.8}{8} \frac{6.9}{15} \frac{7.1}{31} \frac{7.1}{50}$

$\frac{7.3}{50} \frac{7.4}{31} \frac{7.3}{9} \frac{7.6}{8} \frac{7.6}{3} \frac{7.7}{7.7} \frac{7.7}{11} \frac{7.4}{31} \frac{7.4}{50} \frac{7.5}{100}$

$\frac{6.4}{50} \frac{6.5}{32} \frac{6.2}{10} \frac{6.8}{9} \frac{6.3}{5} \frac{6.1}{6.1} \frac{6.5}{10} \frac{6.3}{16} \frac{6.2}{28} \frac{6.2}{50}$

$\frac{5.8}{50} \frac{5.6}{28} \frac{5.5}{10} \frac{5.8}{9} \frac{5.5}{5} \frac{5.2}{5.2} \frac{5.4}{9} \frac{5.7}{11} \frac{5.2}{12} \frac{5.2}{31} \frac{5.4}{50}$

$\frac{5.0}{50} \frac{5.0}{31} \frac{5.0}{10} \frac{5.4}{9} \frac{5.1}{5} \frac{5.0}{5.0} \frac{5.0}{5} \frac{5.5}{12} \frac{4.9}{13} \frac{5.2}{34} \frac{5.2}{50}$

$\frac{3.4}{50} \frac{3.4}{39} \frac{3.3}{20} \frac{3.7}{7} \frac{4.2}{6} \frac{4.1}{4.1} \frac{4.0}{9} \frac{4.7}{13} \frac{4.1}{15} \frac{4.5}{31} \frac{4.7}{50}$

Spk 117 8° Oak 15' LT 15' 50'
 $\frac{4.0}{50} \frac{4.3}{16} \frac{4.7}{7} \frac{5.2}{6} \frac{4.8}{4.8} \frac{5.0}{10} \frac{5.6}{14} \frac{5.3}{16} \frac{5.6}{39} \frac{6.0}{50}$

$\frac{3.4}{50} \frac{3.5}{30} \frac{3.6}{12} \frac{3.8}{6} \frac{4.3}{5} \frac{4.2}{4.2} \frac{4.2}{11} \frac{4.8}{14} \frac{4.3}{15} \frac{4.6}{31} \frac{5.0}{50}$

$\frac{2.5}{50} \frac{2.6}{30} \frac{3.1}{8} \frac{3.5}{7} \frac{3.4}{3.4} \frac{3.4}{9} \frac{3.9}{14} \frac{3.5}{15} \frac{3.9}{29} \frac{4.2}{50}$

$\frac{2.2}{50} \frac{2.3}{32} \frac{2.7}{7} \frac{3.2}{6} \frac{3.1}{3.1} \frac{3.2}{9} \frac{3.6}{14} \frac{3.3}{15} \frac{3.9}{50}$

Sta	+	T	-	Elev
		917.11		
17+50				13.3
18				11.8
+50				11.1
19				11.9
+50				12.2
20				11.4
T.P.	4.38	918.62 ✓	2.87	914.24 ✓
+50				10.6
21				09.9
+50				09.6
22				09.9
+50				11.2
23				12.3

Lt

K

Rt

$$\frac{4.2}{50} \quad \frac{4.2}{29} \quad \frac{4.0}{13} \quad \frac{4.2}{12} \quad 3.8 \quad \frac{3.8}{7} \quad \frac{3.4}{8} \quad \frac{3.1}{28} \quad \frac{2.8}{50}$$

$$\frac{4.1}{50} \quad \frac{4.4}{29} \quad \frac{5.1}{8} \quad \frac{5.5}{7} \quad 5.3 \quad \frac{5.4}{9} \quad \frac{5.9}{13} \quad \frac{5.3}{14} \quad \frac{5.3}{25} \quad \frac{5.3}{50}$$

$$\frac{5.8}{30} \quad \frac{6.0}{30} \quad \frac{6.0}{9} \quad \frac{6.3}{8} \quad 6.0 \quad \frac{6.0}{7} \quad \frac{6.4}{13} \quad \frac{5.8}{14} \quad \frac{5.9}{29} \quad \frac{5.7}{50}$$

$$\frac{5.9}{30} \quad \frac{5.4}{22} \quad \frac{5.4}{10} \quad \frac{5.8}{9} \quad \frac{5.6}{6} \quad 5.2 \quad \frac{5.0}{6} \quad \frac{5.5}{11} \quad \frac{5.0}{12} \quad \frac{5.0}{26} \quad \frac{4.9}{50}$$

$$\frac{5.2}{50} \quad \frac{5.1}{32} \quad \frac{5.2}{11} \quad \frac{5.6}{10} \quad \frac{5.1}{5} \quad 4.9 \quad \frac{5.4}{10} \quad \frac{4.9}{11} \quad \frac{5.0}{32} \quad \frac{5.0}{50}$$

$$\frac{5.3}{50} \quad \frac{5.5}{30} \quad \frac{5.6}{12} \quad \frac{6.0}{11} \quad \frac{5.7}{5} \quad 5.7 \quad \frac{5.7}{5} \quad \frac{6.2}{10} \quad \frac{5.7}{11} \quad \frac{5.8}{40} \quad \frac{5.8}{50}$$

$$\frac{7.5}{50} \quad \frac{7.9}{13} \quad \frac{8.4}{12} \quad \frac{8.3}{10} \quad 8.0 \quad \frac{8.2}{7} \quad \frac{8.2}{10} \quad \frac{8.3}{13} \quad \frac{8.1}{50}$$

$$\frac{8.4}{50} \quad \frac{8.5}{33} \quad \frac{8.6}{17} \quad \frac{9.0}{9} \quad 8.7 \quad \frac{9.0}{7} \quad \frac{9.4}{9} \quad \frac{8.7}{11} \quad \frac{9.1}{50}$$

$$\frac{8.5}{50} \quad \frac{8.8}{27} \quad \frac{9.0}{11} \quad \frac{9.3}{10} \quad 9.0 \quad \frac{9.1}{7} \quad \frac{9.4}{10} \quad \frac{9.0}{11} \quad \frac{9.1}{50}$$

$$\frac{8.5}{50} \quad \frac{8.6}{11} \quad \frac{9.1}{10} \quad \frac{9.0}{8} \quad 8.7 \quad \frac{8.8}{6} \quad \frac{9.3}{10} \quad \frac{8.7}{11} \quad \frac{8.8}{32} \quad \frac{8.8}{50}$$

$$\frac{8.0}{50} \quad \frac{7.7}{10} \quad \frac{8.1}{9} \quad \frac{7.8}{7} \quad 7.4 \quad \frac{7.6}{9} \quad \frac{8.1}{12} \quad \frac{7.3}{13} \quad \frac{7.4}{25} \quad \frac{7.1}{50}$$

$$\frac{6.7}{50} \quad \frac{6.4}{11} \quad \frac{6.6}{10} \quad \frac{6.6}{8} \quad 6.3 \quad \frac{6.4}{7} \quad \frac{6.8}{10} \quad \frac{6.3}{11} \quad \frac{6.2}{30} \quad \frac{5.9}{50}$$

Sta	+	π	-	Elev
		918.62		
23+50				13.2
24				13.4
B.M	4.44	918.62 ✓	4.44	914.18 ✓
+50				13.1
25				12.3
+50				10.4
26				08.8
T.P	2.48	915.69 ✓	5.41	913.21 ✓
+50				10.8
27				10.8
+50				10.3
28				11.1
+50				10.6
T.P	3.10	916.24	2.55	913.14
29				10.5

LX

X

Rt

$$\frac{6.1}{50} \frac{5.6}{12} \frac{5.9}{10} \frac{5.9}{8} 5.4 \frac{5.8}{8} \frac{5.2}{9} \frac{5.0}{25} \frac{5.0}{50}$$

$$\frac{6.5}{50} \frac{5.5}{27} \frac{5.2}{12} \frac{5.7}{11} \frac{5.3}{7} 5.2 \frac{5.2}{4} \frac{5.6}{9} \frac{5.2}{11} 4.8 \frac{5.0}{30} \frac{5.0}{50}$$

SpK 14' 20" 00K 70' Rt 57g 24x10-

$$\frac{6.6}{50} \frac{5.8}{12} \frac{6.2}{11} \frac{5.9}{8} 5.5 \frac{5.5}{5} \frac{5.9}{9} \frac{5.5}{10} 4.8 \frac{5.4}{33} \frac{5.0}{50}$$

$$\frac{7.0}{50} \frac{6.5}{30} \frac{6.1}{13} \frac{6.6}{12} \frac{6.3}{7} 6.3 \frac{6.4}{6} \frac{6.3}{10} \frac{5.7}{18} \frac{6.1}{50}$$

$$\frac{7.2}{50} \frac{8.0}{14} \frac{8.4}{13} \frac{8.2}{9} 8.2 \frac{8.2}{5} \frac{8.2}{9} \frac{7.7}{50}$$

$$\frac{8.6}{50} \frac{9.2}{28} \frac{9.2}{20} \frac{9.6}{11} \frac{9.6}{8} 9.8 \frac{9.2}{6} \frac{9.5}{11} \frac{9.1}{32} \frac{8.6}{50}$$

$$\frac{4.4}{50} \frac{4.8}{17} \frac{5.1}{14} \frac{4.9}{8} 4.9 \frac{5.2}{5} \frac{4.8}{8} \frac{5.1}{18} \frac{5.0}{37} \frac{5.0}{50}$$

$$\frac{3.9}{50} \frac{3.9}{33} \frac{4.4}{13} \frac{5.1}{12} \frac{4.6}{6} 4.9 \frac{5.4}{6} \frac{5.0}{8} \frac{5.2}{50}$$

$$\frac{4.2}{50} \frac{4.8}{29} \frac{5.1}{14} \frac{5.6}{12} \frac{5.3}{8} 5.4 \frac{5.2}{3} \frac{5.5}{6} \frac{5.9}{9} \frac{5.6}{10} \frac{5.9}{34} \frac{6.2}{50}$$

$$\frac{4.6}{50} \frac{4.6}{11} \frac{5.3}{10} \frac{4.8}{6} 4.6 \frac{5.0}{6} \frac{5.3}{8} \frac{4.8}{10} \frac{4.7}{37} \frac{5.1}{50}$$

$$\frac{4.8}{50} \frac{5.0}{30} \frac{5.0}{12} \frac{5.4}{10} \frac{5.2}{6} 5.1 \frac{5.3}{8} \frac{5.8}{10} \frac{5.3}{12} \frac{6.0}{50}$$

$$\frac{5.0}{50} \frac{5.5}{30} \frac{5.4}{12} \frac{5.9}{10} \frac{5.8}{7} 5.7 \frac{6.2}{6} \frac{6.4}{10} \frac{5.9}{11} \frac{6.7}{50}$$

Sta	+	π	-	Elev
		916.24		
29+50				11.3'
30				11.5'
+50				10.0'
31				08.5'
+50				07.9'
32				08.2'
+50				08.0'
33				08.5'
+50				09.5'
+65				10.0'
+70				10.0'
+78				10.4'

Lt

L

Rt

$$\frac{4.4}{20} \frac{4.6}{11} \frac{5.1}{10} \frac{4.8}{6} 4.9 \frac{5.1}{6} \frac{5.4}{8} \frac{4.9}{10} \frac{5.2}{32} \frac{5.4}{50}$$

$$\frac{5.0}{50} \frac{4.8}{35} \frac{4.8}{10} \frac{5.2}{9} \frac{4.7}{4} 4.7 \frac{4.6}{7} \frac{5.1}{10} \frac{4.4}{11} \frac{4.6}{31} \frac{4.7}{50}$$

$$\frac{6.1}{50} \frac{5.8}{27} \frac{6.0}{10} \frac{6.6}{9} \frac{6.2}{6} 6.2 \frac{6.3}{9} \frac{6.5}{11} \frac{6.0}{12} \frac{6.1}{27} \frac{5.7}{50}$$

$$\frac{7.7}{50} \frac{8.0}{29} \frac{7.8}{10} \frac{8.1}{8} \frac{7.9}{4} 7.7 \frac{7.9}{9} \frac{8.3}{12} \frac{7.9}{13} \frac{7.8}{30} \frac{7.6}{50}$$

$$\frac{8.5}{50} \frac{8.7}{29} \frac{8.8}{9} \frac{9.0}{8} \frac{8.5}{4} 8.3 \frac{8.5}{10} \frac{8.9}{13} \frac{8.7}{14} \frac{8.4}{28} \frac{8.5}{50}$$

$$\frac{8.3}{50} \frac{8.6}{32} \frac{8.7}{10} \frac{8.3}{4} 8.0 \frac{8.1}{10} \frac{8.7}{14} \frac{8.4}{12} \frac{8.9}{29} \frac{8.7}{50}$$

$$\frac{8.8}{50} \frac{8.6}{28} \frac{8.4}{8} \frac{8.8}{6} 8.2 \frac{8.4}{6} \frac{8.7}{13} \frac{8.3}{15} \frac{8.6}{28} \frac{8.4}{50}$$

$$\frac{8.2}{50} \frac{8.2}{31} \frac{7.8}{18} \frac{7.7}{8} \frac{8.3}{7} 7.7 \frac{7.5}{9} \frac{8.0}{12} \frac{7.5}{13} \frac{7.5}{27} \frac{7.3}{50}$$

$$\frac{6.7}{50} \frac{6.5}{16} \frac{6.9}{7} 6.7 \frac{6.7}{10} \frac{7.1}{12} \frac{6.6}{14} \frac{6.7}{31} \frac{6.5}{50}$$

$$\frac{5.8}{50} \frac{5.8}{32} \frac{5.9}{12} \frac{6.3}{7} 6.2 \frac{6.5}{10} \frac{6.2}{20} \frac{6.3}{35} \frac{6.3}{50}$$

$$\frac{7.2}{50} \frac{7.0}{26} \frac{6.2}{11} \frac{6.1}{7} 6.2 \frac{6.4}{9} \frac{6.7}{16} \frac{7.1}{22} \frac{7.1}{35} \frac{7.2}{50}$$

$$\frac{6.1}{50} \frac{6.4}{31} \frac{6.0}{17} \frac{5.8}{10} 5.8 \frac{6.0}{13} \frac{6.0}{29} \frac{6.2}{50}$$

Sta + π - Elev

916.24

33+85

10.9

34

11.6

B.M.

5.37 910.87 ✓

Bench Levels

B.M.

5.37

916.24 ✓

910.87 ✓

3.94

912.02 ✓

3.16

913.08 ✓

B.M.

6.31

910.71 ✓

910.70 ✓

B.M.

6.34

917.21 ✓

910.87

3.82

916.88 ✓

4.15

913.06 ✓

3.85

913.03 ✓

Lt

R

Rt

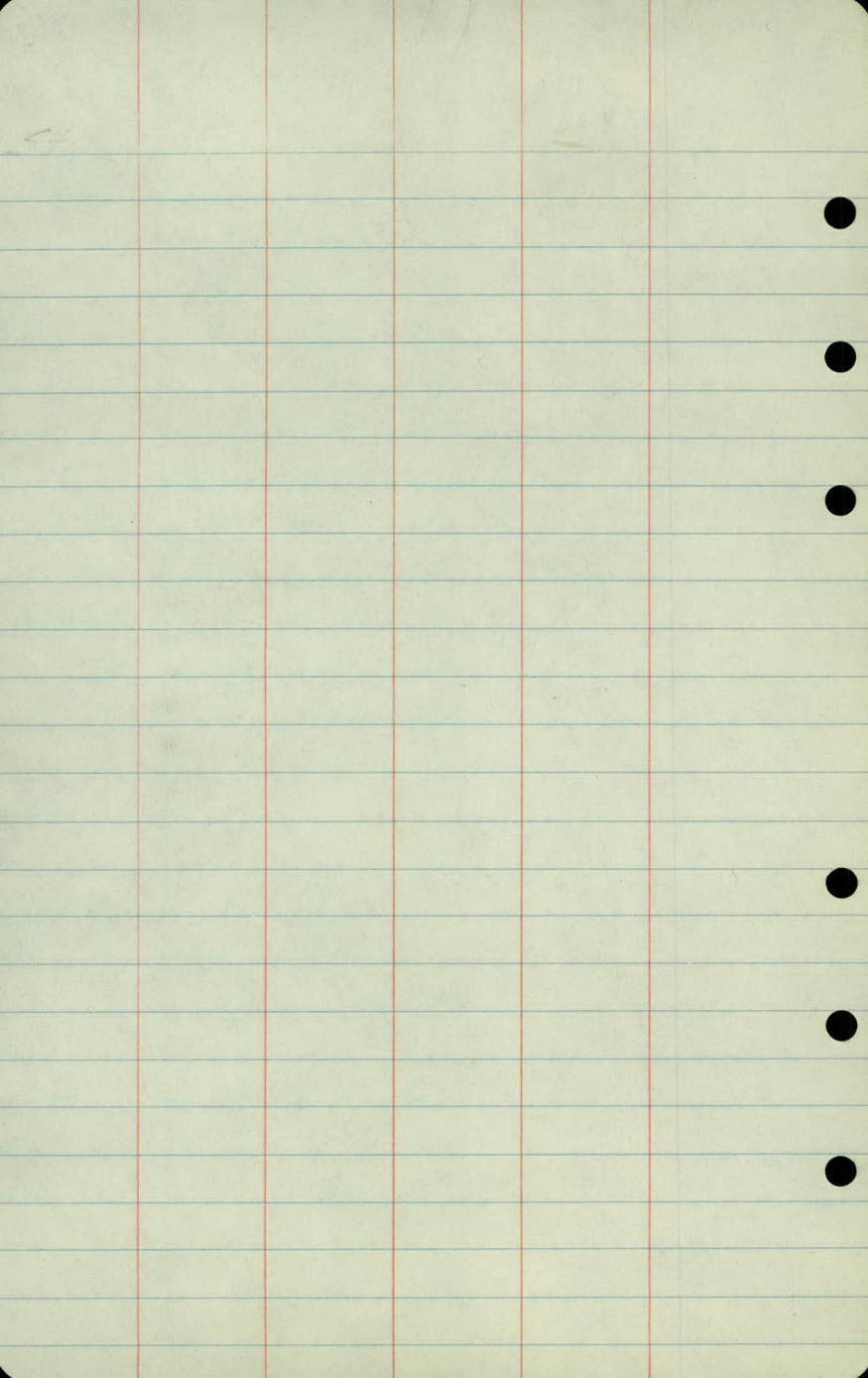
 $\frac{4.8}{30}$ $\frac{4.7}{39}$ $\frac{5.1}{18}$ 5.3 $\frac{5.3}{15}$ $\frac{5.1}{30}$ $\frac{5.0}{30}$
 $\frac{4.7}{30}$ 4.6 $\frac{4.5}{25}$ $\frac{4.5}{30}$

Spk in P.P NE Cor Red Oak Drive &
Co Rd I

Spk in P.P

Spk in P.P N.E Cor Groveland & Co Rd I

Spk in 15" Cottonwood NE Cor Eastwood &
Co Rd "I."



Red Oak Drive

Slope Stokes

Sta	+	Δ	-	Elev
B.M.	3.08	920.85		917.77

0

+50

15.7

1

15.5

+50

15.3

2

15.1

+50

14.9

3

14.7

+50

14.4

4

14.0

+50

13.5

5

12.8

T.P.

1.26

915.70

6.41

914.44

+50

12.1

Lt

R

Rt

Gr. Rod

Spike in 10" Oak 65' Lt 0+75

5.2

$$\begin{array}{r} 3.4 \\ C1.8 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 3.8 \\ C1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 3.4 \\ C1.8 \\ \hline 25 \end{array}$$

5.4

$$\begin{array}{r} 3.8 \\ C1.6 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 4.1 \\ C1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 3.9 \\ C1.5 \\ \hline 25 \end{array}$$

5.6

$$\begin{array}{r} 4.7 \\ C0.9 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 4.9 \\ C0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 4.7 \\ C0.9 \\ \hline 25 \end{array}$$

5.8

$$\begin{array}{r} 5.2 \\ C0.6 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.2 \\ C0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ C0.7 \\ \hline 25 \end{array}$$

6.0

$$\begin{array}{r} 5.1 \\ C0.9 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.0 \\ C1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ C1.2 \\ \hline 25 \end{array}$$

6.2

$$\begin{array}{r} 4.8 \\ C1.4 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 4.8 \\ C1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ C1.4 \\ \hline 25 \end{array}$$

6.5

$$\begin{array}{r} 4.9 \\ C1.6 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.1 \\ C1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ C1.1 \\ \hline 25 \end{array}$$

6.9

$$\begin{array}{r} 5.0 \\ C1.9 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.1 \\ C1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ C1.6 \\ \hline 25 \end{array}$$

7.4

$$\begin{array}{r} 6.0 \\ C1.4 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.8 \\ C1.6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.8 \\ C1.6 \\ \hline 25 \end{array}$$

8.1

$$\begin{array}{r} 7.3 \\ C0.8 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 7.3 \\ C0.8 \\ \hline \end{array}$$

$$\begin{array}{r} 7.0 \\ C1.1 \\ \hline 25 \end{array}$$

3.6

$$\begin{array}{r} 4.5 \\ C0.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 4.2 \\ F0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 3.4 \\ C0.2 \\ \hline 25 \end{array}$$

Sta	+	π	-	Elev.
		915.70		
5+83				11.7
6				11.3
+50				10.7
7				10.2
+50				10.0
8				10.0
+50				10.1
9				10.2
T.P.				
+50				10.3
10				10.4
+50				10.5
B.M.	1.70	914.48	12.95	912.75
11				10.6
				912.78

$$4.0 \quad \begin{array}{r} 6.0 \\ F2.0 \\ 17.0 \end{array} \quad \begin{array}{r} 5.8 \\ F1.8 \end{array} \quad \begin{array}{r} 4.9 \\ DC 1.1 \\ 23.2 \end{array}$$

$$4.4 \quad \begin{array}{r} 2.3 \\ F2.9 \\ 18.8 \end{array} \quad \begin{array}{r} 6.8 \\ F2.2 \end{array} \quad \begin{array}{r} 5.8 \\ DC 0.6 \\ 22.2 \end{array}$$

$$5.0 \quad \begin{array}{r} 8.4 \\ F3.4 \\ 19.8 \end{array} \quad \begin{array}{r} 7.9 \\ F2.9 \end{array} \quad \begin{array}{r} 7.7 \\ F2.7 \\ 18.4 \end{array}$$

$$5.5 \quad \begin{array}{r} 8.6 \\ F3.1 \\ 19.2 \end{array} \quad \begin{array}{r} 8.2 \\ F2.7 \end{array} \quad \begin{array}{r} 8.0 \\ F2.5 \\ 18.0 \end{array}$$

$$5.7 \quad \begin{array}{r} 8.4 \\ F2.7 \\ 18.4 \end{array} \quad \begin{array}{r} 7.9 \\ F2.2 \end{array} \quad \begin{array}{r} 7.3 \\ DC 0.4 \\ 27.8 \end{array}$$

$$5.7 \quad \begin{array}{r} 8.2 \\ F2.5 \\ 18.0 \end{array} \quad \begin{array}{r} 7.9 \\ F2.2 \end{array} \quad \begin{array}{r} 7.9 \\ F2.2 \\ 17.4 \end{array}$$

$$5.6 \quad \begin{array}{r} 7.8 \\ F2.2 \\ 17.4 \end{array} \quad \begin{array}{r} 7.4 \\ F1.8 \end{array} \quad \begin{array}{r} 7.2 \\ DC 0.4 \\ 21.8 \end{array}$$

$$5.5 \quad \begin{array}{r} 7.5 \\ F2.0 \\ 17.0 \end{array} \quad \begin{array}{r} 6.7 \\ F1.2 \end{array} \quad \begin{array}{r} 6.1 \\ DC 1.4 \\ 23.8 \end{array}$$

$$5.4 \quad \begin{array}{r} 6.7 \\ DC 0.7 \\ 22.4 \end{array} \quad \begin{array}{r} 6.0 \\ F0.6 \end{array} \quad \begin{array}{r} 5.4 \\ C 0.0 \\ 25.0 \end{array}$$

$$5.3 \quad \begin{array}{r} 5.5 \\ DC 1.8 \\ 24.0 \end{array} \quad \begin{array}{r} 5.1 \\ C 0.2 \end{array} \quad \begin{array}{r} 4.4 \\ C 0.9 \\ 25 \end{array}$$

$$5.2 \quad \begin{array}{r} 5.2 \\ C 0.0 \\ 25 \end{array} \quad \begin{array}{r} 4.7 \\ C 0.5 \end{array} \quad \begin{array}{r} 4.4 \\ C 0.8 \\ 25 \end{array}$$

Spike in 14" Oak 75' Rt 5th 10x95

$$3.9 \quad \begin{array}{r} 4.4 \\ DC 1.5 \\ 24 \end{array} \quad \begin{array}{r} 4.1 \\ F0.2 \end{array} \quad \begin{array}{r} 3.4 \\ C 0.5 \\ 25 \end{array}$$

Sta	+	π	-	Elev
-----	---	-------	---	------

914.48⁵

11+50				10.7
-------	--	--	--	------

12				10.8
----	--	--	--	------

+50				10.9
-----	--	--	--	------

13				11.0
----	--	--	--	------

+50				11.1
-----	--	--	--	------

14				11.2
----	--	--	--	------

+50				11.3
-----	--	--	--	------

15				11.4
----	--	--	--	------

T.P.	5.97	918.25 ⁷	1.80	912.68
------	------	---------------------	------	--------

+50				11.5
-----	--	--	--	------

16				11.6
----	--	--	--	------

+50				11.7
-----	--	--	--	------

17				11.8
----	--	--	--	------

G R

3.8

$$\begin{array}{r} 4.8 \\ DC 1.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 4.5 \\ FO.7 \\ \hline \end{array}$$

$$\begin{array}{r} 3.7 \\ DC 1.9 \\ \hline 24.8 \end{array}$$

3.7

$$\begin{array}{r} 5.4 \\ DC 0.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 5.5 \\ FI.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ F2.2 \\ \hline 17.4 \end{array}$$

3.6

$$\begin{array}{r} 5.9 \\ F2.3 \\ \hline 17.6 \end{array}$$

$$\begin{array}{r} 6.0 \\ F2.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ F2.6 \\ \hline 18.2 \end{array}$$

3.5

$$\begin{array}{r} 6.6 \\ F3.1 \\ \hline 19.2 \end{array}$$

$$\begin{array}{r} 7.9 \\ F4.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.7 \\ F3.2 \\ \hline 19.4 \end{array}$$

3.4

$$\begin{array}{r} 5.5 \\ F2.1 \\ \hline 17.2 \end{array}$$

$$\begin{array}{r} 5.2 \\ FI.8 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ DC 0.1 \\ \hline 21.2 \end{array}$$

3.3

$$\begin{array}{r} 4.6 \\ DC 0.7 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 4.4 \\ FI.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.3 \\ DC.10 \\ \hline 23.0 \end{array}$$

3.2

$$\begin{array}{r} 4.1 \\ DC 1.1 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 4.1 \\ FO.9 \\ \hline \end{array}$$

$$\begin{array}{r} 4.2 \\ DC.1.0 \\ \hline 23.0 \end{array}$$

3.1

$$\begin{array}{r} 2.6 \\ C 0.5 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 3.3 \\ FO.2 \\ \hline \end{array}$$

$$\begin{array}{r} 3.6 \\ DC.1.5 \\ \hline 24.0 \end{array}$$

7.2

$$\begin{array}{r} 5.8 \\ C 1.3 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 6.5 \\ C.0.7 \\ \hline \end{array}$$

$$\begin{array}{r} 7.1 \\ C.0.1 \\ \hline 2.5 \end{array}$$

7.1

$$\begin{array}{r} 5.1 \\ C 2.0 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 5.8 \\ C 1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 6.1 \\ C 1.0 \\ \hline 6.5 \end{array}$$

7.0

$$\begin{array}{r} 4.2 \\ C 2.8 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 5.1 \\ C 1.9 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ C 0.7 \\ \hline 2.5 \end{array}$$

6.9

$$\begin{array}{r} 4.0 \\ C 2.9 \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 4.7 \\ C 2.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ C 1.9 \\ \hline 2.5 \end{array}$$

Sta	t	π	-	Elev
-----	---	-------	---	------

918.65⁷

17+50

11.9

18

11.9

+50

12.0

19

12.0

+50

12.1

20

12.1

+50

12.2

T.P.

6.27

917.78⁸

7.14

911.51

stump

21

12.2

+50

12.3

22

12.3

+50

12.4

23

12.4

G 12.

6.8	$\begin{array}{r} 4.7 \\ C 2.1 \\ \hline 25 \end{array}$	$\begin{array}{r} 5.5 \\ C 1.3 \\ \hline \end{array}$	$\begin{array}{r} 5.8 \\ C 1.0 \\ \hline 25 \end{array}$
6.8	$\begin{array}{r} 4.1 \\ C 0.7 \\ \hline 25 \end{array}$	$\begin{array}{r} 6.8 \\ C 0.0 \\ \hline \end{array}$	$\begin{array}{r} 6.9 \\ DC 1.9 \\ \hline 24.8 \end{array}$
6.7	$\begin{array}{r} 7.7 \\ DC 1.0 \\ \hline 23.0 \end{array}$	$\begin{array}{r} 7.7 \\ F 1.0 \\ \hline \end{array}$	$\begin{array}{r} 7.5 \\ DC 1.2 \\ \hline 23.4 \end{array}$
6.7	$\begin{array}{r} 7.1 \\ DC 1.6 \\ \hline 24.2 \end{array}$	$\begin{array}{r} 6.8 \\ F 0.1 \\ \hline \end{array}$	$\begin{array}{r} 6.6 \\ C 0.1 \\ \hline 25 \end{array}$
6.6	$\begin{array}{r} 6.7 \\ DC 1.9 \\ \hline 24.8 \end{array}$	$\begin{array}{r} 6.6 \\ F 0.0 \\ \hline \end{array}$	$\begin{array}{r} 6.5 \\ C 0.1 \\ \hline 25 \end{array}$
6.6	$\begin{array}{r} 7.1 \\ DC 1.5 \\ \hline 24.0 \end{array}$	$\begin{array}{r} 7.3 \\ F 0.7 \\ \hline \end{array}$	$\begin{array}{r} 7.3 \\ DC 1.3 \\ \hline 23.6 \end{array}$
6.5	$\begin{array}{r} 8.0 \\ DC 0.5 \\ \hline 22.0 \end{array}$	$\begin{array}{r} 8.1 \\ F 1.6 \\ \hline \end{array}$	$\begin{array}{r} 8.3 \\ DC 0.2 \\ \hline 21.4 \end{array}$
5.6	$\begin{array}{r} 7.8 \\ F 2.2 \\ \hline 17.4 \end{array}$	$\begin{array}{r} 7.9 \\ F 2.3 \\ \hline \end{array}$	$\begin{array}{r} 8.0 \\ F 2.4 \\ \hline 17.8 \end{array}$
5.5	$\begin{array}{r} 8.1 \\ F 2.6 \\ \hline 18.2 \end{array}$	$\begin{array}{r} 8.3 \\ F 2.8 \\ \hline \end{array}$	$\begin{array}{r} 8.2 \\ F 2.7 \\ \hline 18.4 \end{array}$
5.5	$\begin{array}{r} 7.9 \\ F 2.4 \\ \hline 17.8 \end{array}$	$\begin{array}{r} 7.9 \\ F 2.4 \\ \hline \end{array}$	$\begin{array}{r} 8.0 \\ F 2.5 \\ \hline 18.0 \end{array}$
5.4	$\begin{array}{r} 7.0 \\ DC 0.4 \\ \hline 21.8 \end{array}$	$\begin{array}{r} 6.7 \\ F 1.3 \\ \hline \end{array}$	$\begin{array}{r} 6.6 \\ DC 0.8 \\ \hline 22.6 \end{array}$
5.4	$\begin{array}{r} 5.6 \\ DC 1.8 \\ \hline 24.6 \end{array}$	$\begin{array}{r} 5.4 \\ F 0.0 \\ \hline \end{array}$	$\begin{array}{r} 5.5 \\ DC 1.9 \\ \hline 24.6 \end{array}$

Sta.	+	π	-	Elev
		⁸ 917.78		
23 + 50				12.4
24				12.3
B.M.	3.61	⁸ 917.78	3.61	914.17
+50				12.2
25				12.1
+50				12.0
26				11.8
+50				11.7
T.P	4.46	⁷ 915.67	6.57	¹⁵ ¹⁷ 911.21
27				11.5
+50				11.4
28				11.2
+50				11.1
29				10.9

914.18

G. R.

$$\begin{array}{r} 5.4 \\ \begin{array}{r} 4.9 \\ \hline 60.5 \\ 25 \end{array} \end{array}$$

$$\begin{array}{r} 4.6 \\ \hline 60.8 \end{array}$$

$$\begin{array}{r} 4.2 \\ \hline 61.2 \\ 25 \end{array}$$

$$\begin{array}{r} 5.5 \\ \begin{array}{r} 4.8 \\ \hline 60.7 \\ 25 \end{array} \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 61.1 \end{array}$$

$$\begin{array}{r} 4.1 \\ \hline 61.4 \\ 25 \end{array}$$

spike in 10" Oct 70' Rt 3/4 24+14

$$\begin{array}{r} 5.6 \\ \begin{array}{r} 5.2 \\ \hline 60.4 \\ 25 \end{array} \end{array}$$

$$\begin{array}{r} 4.8 \\ \hline 60.8 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline 61.1 \\ 25 \end{array}$$

$$\begin{array}{r} 5.7 \\ \begin{array}{r} 5.7 \\ \hline 60.0 \\ 25 \end{array} \end{array}$$

$$\begin{array}{r} 5.5 \\ \hline 60.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ \hline 60.4 \\ 25 \end{array}$$

$$\begin{array}{r} 5.8 \\ \begin{array}{r} 7.1 \\ \hline DC 0.6 \\ 22.2 \end{array} \end{array}$$

$$\begin{array}{r} 7.4 \\ \hline F1.8 \end{array}$$

$$\begin{array}{r} 7.3 \\ \hline DC 0.5 \\ 22.0 \end{array}$$

$$\begin{array}{r} 6.0 \\ \begin{array}{r} 8.9 \\ \hline F2.9 \\ 18.9 \end{array} \end{array}$$

$$\begin{array}{r} 8.9 \\ \hline F2.9 \end{array}$$

$$\begin{array}{r} 8.7 \\ \hline F2.7 \\ 18.4 \end{array}$$

$$\begin{array}{r} 6.1 \\ \begin{array}{r} 6.8 \\ \hline DC 1.3 \\ 23.6 \end{array} \end{array}$$

$$\begin{array}{r} 7.0 \\ \hline F0.9 \end{array}$$

$$\begin{array}{r} 7.1 \\ \hline DC 1.0 \\ 23.0 \end{array}$$

$$\begin{array}{r} 4.2 \\ \begin{array}{r} 4.0 \\ \hline 60.2 \\ 25 \end{array} \end{array}$$

$$\begin{array}{r} 4.9 \\ \hline F0.7 \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline DC 1.0 \\ 23.0 \end{array}$$

$$\begin{array}{r} 4.3 \\ \begin{array}{r} 5.1 \\ \hline DC 1.2 \\ 23.4 \end{array} \end{array}$$

$$\begin{array}{r} 5.6 \\ \hline F0.7 \end{array}$$

$$\begin{array}{r} 5.9 \\ \hline DC 0.4 \\ 21.8 \end{array}$$

$$\begin{array}{r} 4.5 \\ \begin{array}{r} 5.0 \\ \hline DC 1.5 \\ 24.0 \end{array} \end{array}$$

$$\begin{array}{r} 4.8 \\ \hline F0.3 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline DC 1.5 \\ 24.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ \begin{array}{r} 4.8 \\ \hline DC 1.8 \\ 24.6 \end{array} \end{array}$$

$$\begin{array}{r} 5.2 \\ \hline F0.6 \end{array}$$

$$\begin{array}{r} 5.6 \\ \hline DC 1.0 \\ 23.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ \begin{array}{r} 4.8 \\ \hline 60.0 \\ 25 \end{array} \end{array}$$

$$\begin{array}{r} 6.3 \\ \hline F1.5 \end{array}$$

$$\begin{array}{r} 5.7 \\ \hline DC 1.1 \\ 23.2 \end{array}$$

319 + π - Elev

915.67

29+50

10.8

30

10.6

+50

10.5

31

10.3

+50

10.2

32

10.3

+50

10.4

33

10.7

+50

11.1

+65

X

+70

11.2

+78

X

B.M.

4.83

910.84 910.87

G.R.

4.9	$\begin{array}{r} 43 \\ 60.6 \\ \hline 25 \end{array}$	$\begin{array}{r} 44 \\ 60.5 \end{array}$	$\begin{array}{r} 43 \\ 60.6 \\ \hline 25 \end{array}$
5.1	$\begin{array}{r} 46 \\ 60.5 \\ \hline 25 \end{array}$	$\begin{array}{r} 43 \\ 60.8 \end{array}$	$\begin{array}{r} 41 \\ 61.0 \\ \hline 25 \end{array}$
5.2	$\begin{array}{r} 54 \\ 601.8 \\ \hline 24.6 \end{array}$	$\begin{array}{r} 57 \\ 60.5 \end{array}$	$\begin{array}{r} 57 \\ 601.5 \\ \hline 24.0 \end{array}$
5.4	$\begin{array}{r} 75 \\ 621 \\ \hline 17.2 \end{array}$	$\begin{array}{r} 79 \\ 62.5 \end{array}$	$\begin{array}{r} 76 \\ 62.2 \\ \hline 17.4 \end{array}$
5.5	$\begin{array}{r} 83 \\ 628 \\ \hline 18.6 \end{array}$	$\begin{array}{r} 82 \\ 62.7 \end{array}$	$\begin{array}{r} 82 \\ 62.7 \\ \hline 18.4 \end{array}$
5.4	$\begin{array}{r} 81 \\ 62.7 \\ \hline 18.4 \end{array}$	$\begin{array}{r} 79 \\ 62.5 \end{array}$	$\begin{array}{r} 81 \\ 62.7 \\ \hline 18.4 \end{array}$
5.3	$\begin{array}{r} 82 \\ 62.7 \\ \hline 18.8 \end{array}$	$\begin{array}{r} 80 \\ 62.7 \end{array}$	$\begin{array}{r} 80 \\ 62.7 \\ \hline 18.4 \end{array}$
5.0	$\begin{array}{r} 75 \\ 62.5 \\ \hline 18.0 \end{array}$	$\begin{array}{r} 73 \\ 62.3 \end{array}$	$\begin{array}{r} 71 \\ 62.1 \\ \hline 17.2 \end{array}$
4.6	$\begin{array}{r} 60 \\ 600.6 \\ \hline 22.2 \end{array}$	$\begin{array}{r} 63 \\ 61.7 \end{array}$	$\begin{array}{r} 62 \\ 600.4 \\ \hline 21.8 \end{array}$
4.5	$\begin{array}{r} 52 \\ 601.3 \\ \hline 23.6 \end{array}$	$\begin{array}{r} 59 \\ 61.4 \end{array}$	$\begin{array}{r} 57 \\ 600.8 \\ \hline 22.6 \end{array}$
4.5			

Spike in P.P. N.E. Cor. Red Oak E. N. Co. Line

