

Bk 21 - Dr. 11A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

----- Plan ----- Survey

----- SHERWOOD ROAD -----

From Graveland St. To Long Lake Rd.

Road Acc't. No. M-49-----

Date Filed 10-26-37-----

File-----

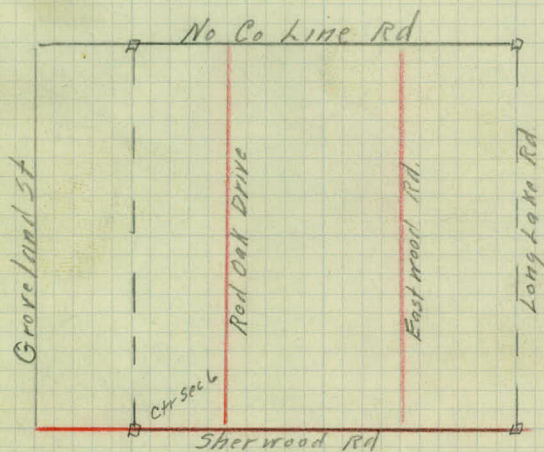
1/9/39

R.P.
H.W.
A.M.
L.G.

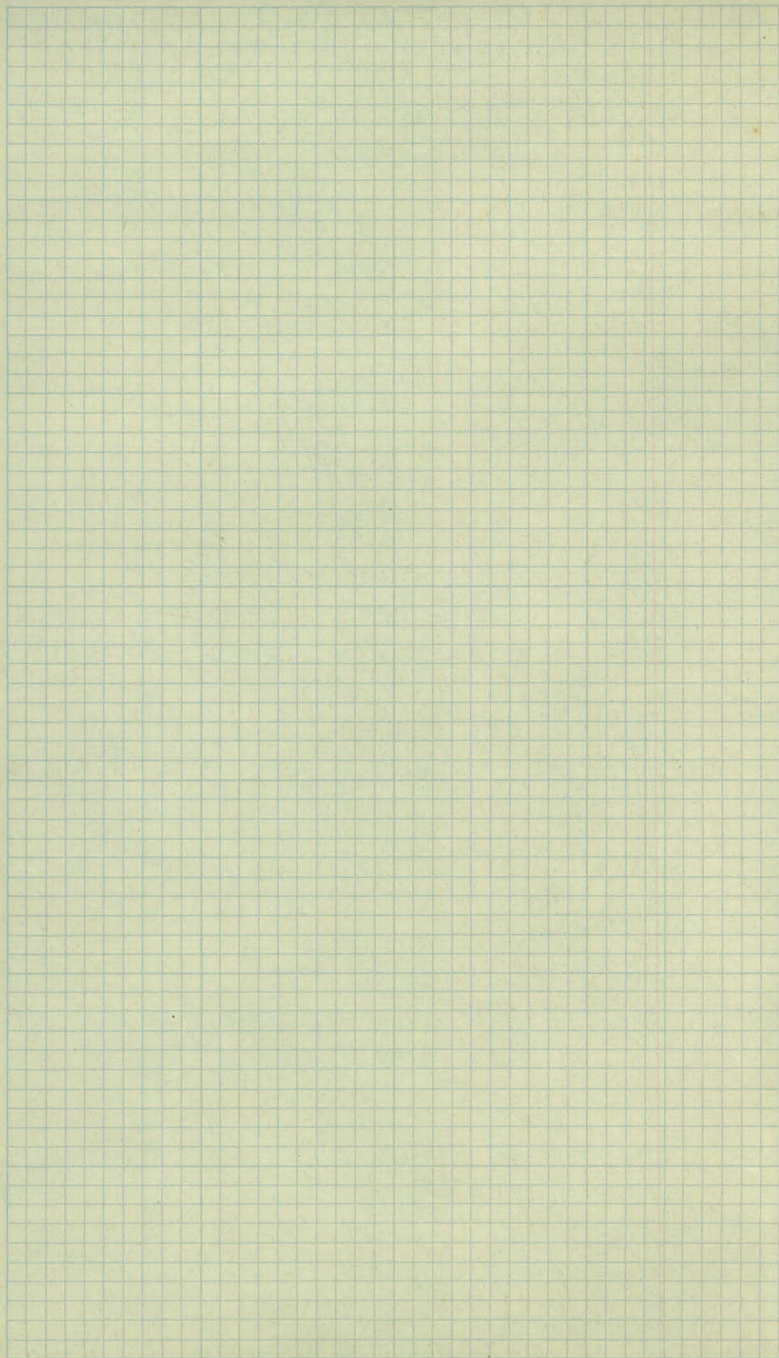
Plan Survey

Roads In Sec 6

Twp 30 N R 23 W.



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Alignment

Sherwood Rd.

Sta.

Pl.

ΔL

ΔR

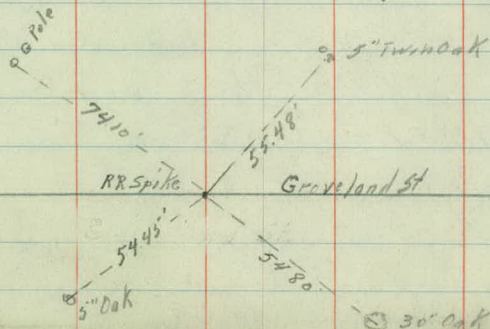
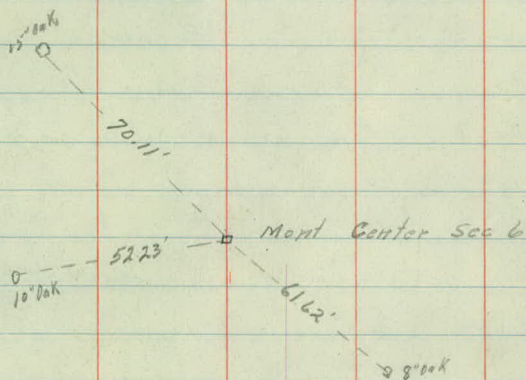
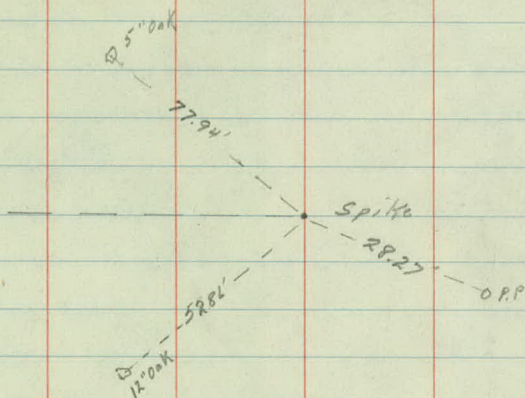
10+11.49 = P.O.T.

0+00

E Red Oak Drive

4+83.49

0+00



Sta

Pt

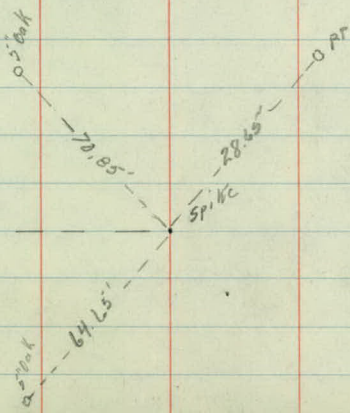
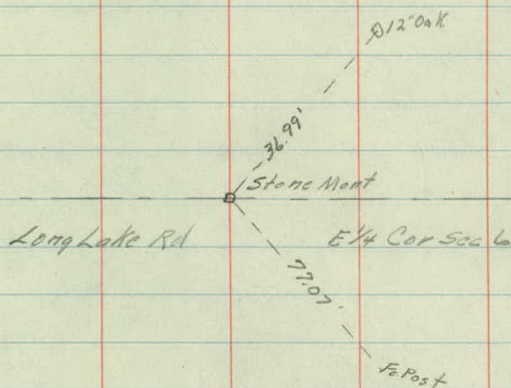
Alt

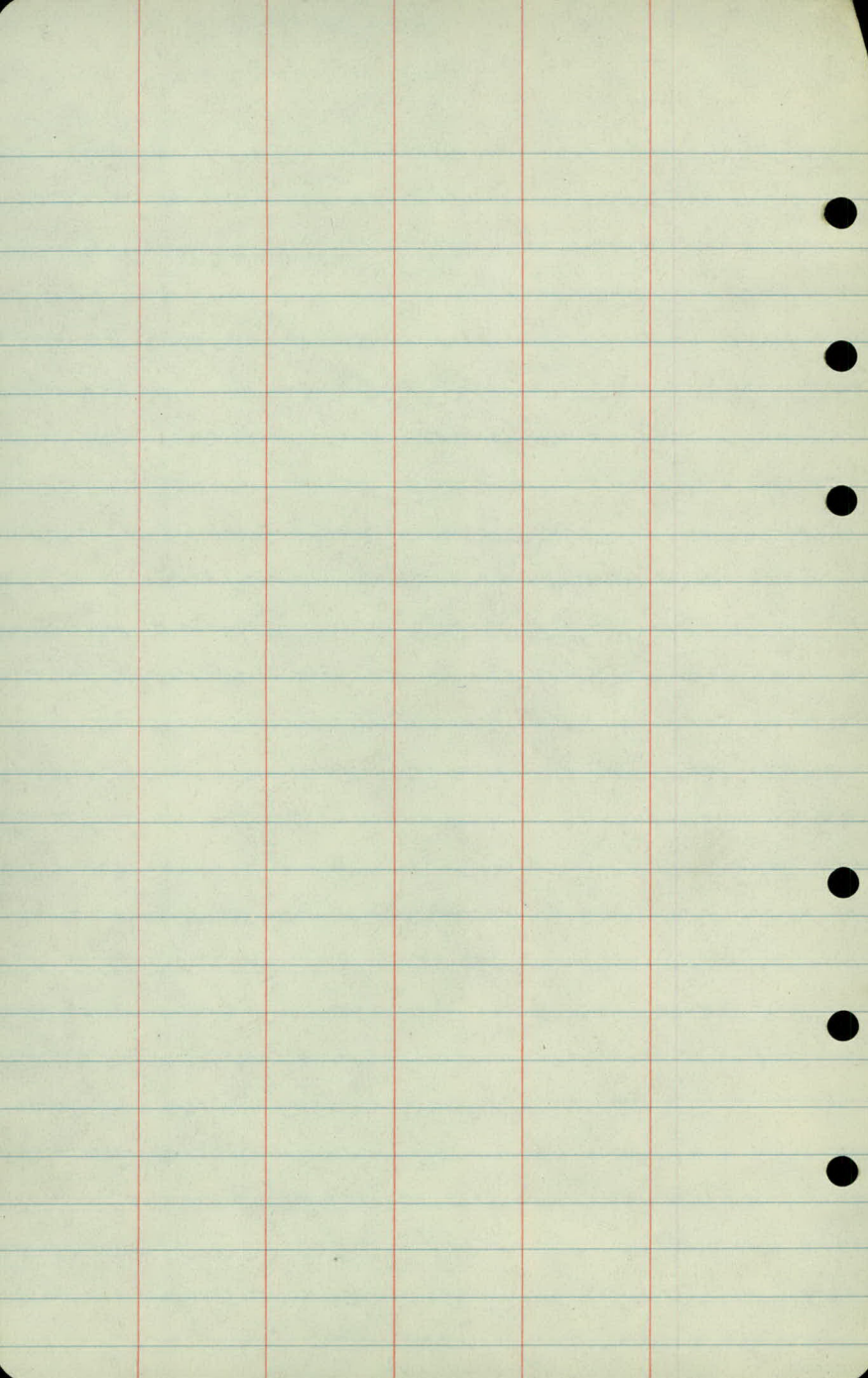
Art

31+23.49 P.I.

20+67.49 = P.O.T

0+00 E Eastwood Drive





Artificial Topography
Sherwood Rd

6

5

Rd
11-1

4

Rd
11-2

3

Rd
8-3

2

Rd
6-5

1

Rd
5-5

0+00

Rd
10-10

Pasture

Woods

+10 Ent.

+96 Fc Cor 24'
+83 P.P. 20'
+83 End Woods 25'

Tree line 25'

Tree line 25'

+27 P.P. 20'
+05 Ent

Woods

+74 P.P. 20'

+00 End Brush
Beg Heavy Woods

+30 Lt Brush 25'
+20 P.P. 20'

Groveland

St
Dirt Rd.

12

Rd/
11-0

11

Rd/
11-0

10

Rd/
11-0

9

Rd/
10-2

8

Rd/
9-2

7

Rd/
10-2

6

Rd/
12-1

+50 Beg Heavy Timber

School Dist #36
School Under Const.

+35 Beg Rt Woods R5"

Red Oak Drive 10' Trail

+85 End Woods R5"

+65 Ent

+46 Ent

Woods Tree line R5"

Waste Lt Brush

Waste

Pasture

FC R5'

+76 P.P. R20'

FC R5'
+91 P.P. R20'

+123 P.P. R20'

FC R5'

+165 P.P. R20'

FC R4'

19

Rd
9-2

18

Rd
11-0

17

Rd
11-0

16

Rd
11-0

15

Rd
11-0

14

Rd
11-0

13

Rd
11-0

Woods

+05 PPR20'

Fe 25'

80

+68-3 Oaks 4'

+R3 PPR20'

Tree line 25'

Lt Brush

Fe 25'

Woods

Waste land

+40 PPR20'

Fe 25'

+58 PP

26

Rd
5-6

25

Rd
5-6

24

Rd
7-4

23

Rd
9-2

22

Rd
10-0

21

Rd
7-3

20

Rd
6-4

Marsh

Marsh

Fc 25'
+94 PPR1'

+28 End Yard +
End Oaks

(15" Wood
Culvert N.G.)

+28 PPR21'
+08-2' Ditch
Fc 25'

Scattered
Oaks

+74 Fc Cor 25'

+57 Beg Scattered Trees

+59 PPR1'

+00 End Woods

Fc 25'

Wasteland
L + Brush

+92 Beg Scattered Oaks

+88 PPR20'

+67 Eastwood Rd

10' Front

+42 End Woods

Woods

Fc 25'

32

31

Rd
7-6

30

Rd
6-5

29

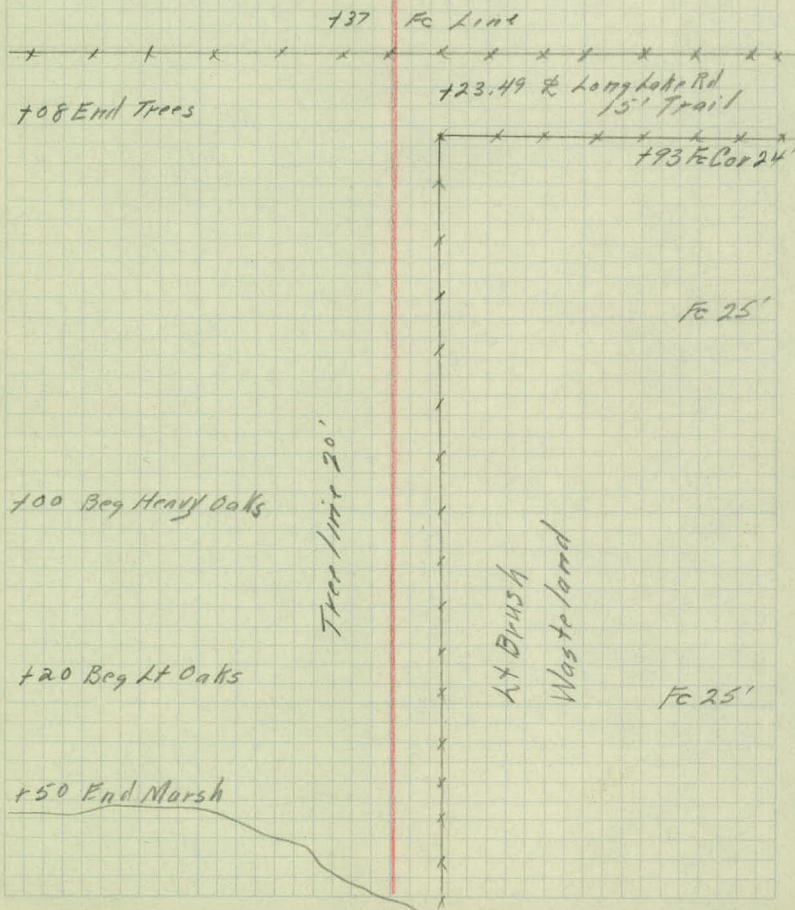
Rd
5-6

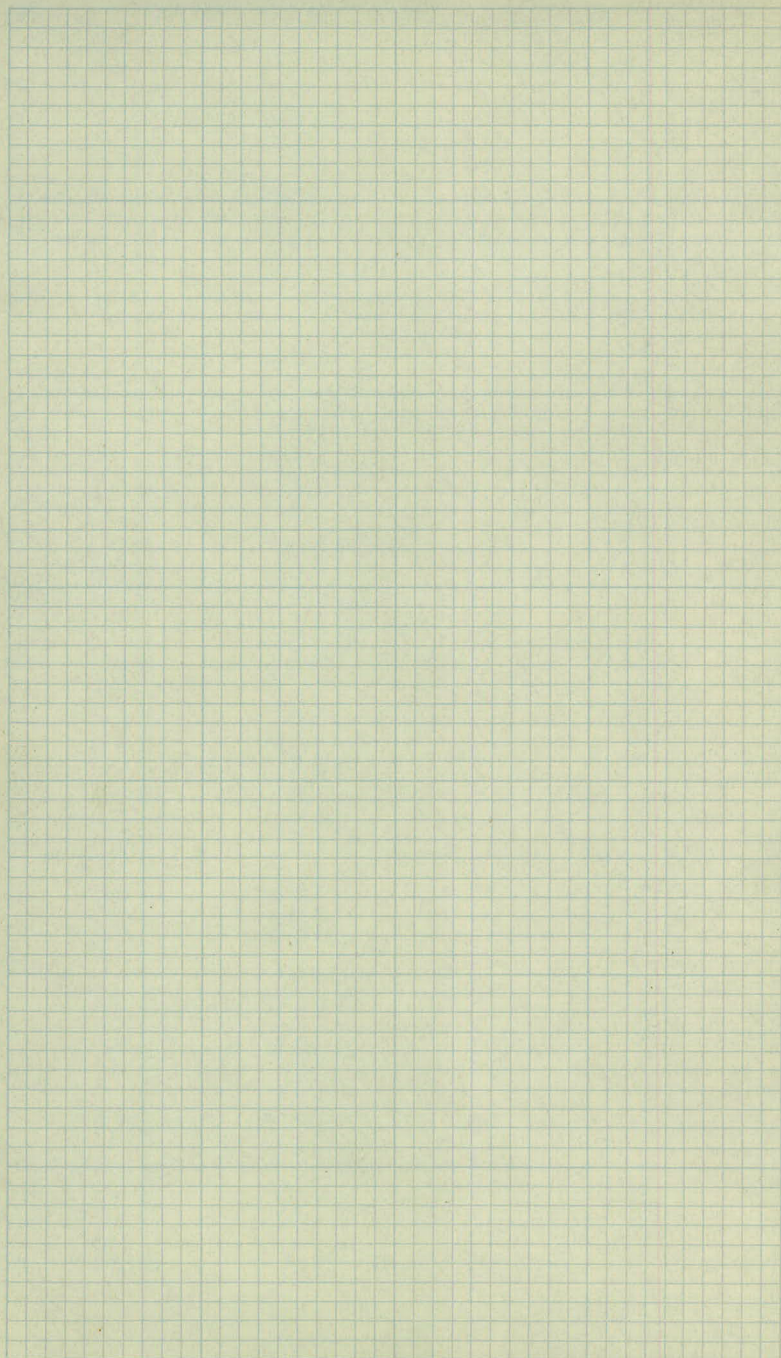
28

Rd
6-5

27

Rd
5-6





X sections

Sherwood Rd

Sta	+	π	-	Elev
B.M.	3.27	917.80		914.53
0+00				13.8
+13				13.5
+17				13.6
+21				13.4
+25				13.3
0+50				13.0
1+00				12.5
+50				12.4
2+00				13.2
+50				13.4
3+00				13.1
+50				13.0

Lt.

K

Pt

Spk 111 30" Oak 46" Pt 0-26

$$\frac{4.4}{50}$$

40

$$\frac{3.9}{50}$$

6

$$\frac{4.4}{50}$$

$$\frac{4.4}{15}$$

43

$$\frac{4.5}{8}$$

$$\frac{4.1}{20}$$

$$\frac{3.9}{50}$$

$$\frac{6.5}{50}$$

$$\frac{6.0}{28}$$

$$\frac{4.6}{25}$$

42

$$\frac{4.5}{12}$$

$$\frac{4.0}{18}$$

$$\frac{4.0}{25}$$

$$\frac{5.4}{28}$$

$$\frac{5.8}{50}$$

$$\frac{6.5}{50}$$

$$\frac{6.0}{28}$$

$$\frac{4.6}{25}$$

44

$$\frac{4.5}{12}$$

$$\frac{4.0}{18}$$

$$\frac{4.0}{25}$$

$$\frac{5.4}{28}$$

$$\frac{5.8}{50}$$

$$\frac{5.0}{50}$$

$$\frac{4.8}{25}$$

$$\frac{4.5}{7}$$

45

$$\frac{4.3}{14}$$

$$\frac{4.5}{50}$$

$$\frac{5.3}{50}$$

$$\frac{4.9}{15}$$

$$\frac{5.0}{7}$$

48

$$\frac{5.0}{7}$$

$$\frac{4.8}{14}$$

$$\frac{4.8}{50}$$

$$\frac{5.4}{50}$$

$$\frac{5.3}{11}$$

$$\frac{5.8}{6}$$

53

$$\frac{5.5}{9}$$

$$\frac{5.3}{30}$$

$$\frac{5.3}{50}$$

$$\frac{5.3}{50}$$

$$\frac{5.5}{7}$$

54

$$\frac{5.4}{7}$$

$$\frac{5.3}{23}$$

$$\frac{5.0}{50}$$

$$\frac{4.8}{50}$$

$$\frac{4.9}{7}$$

46

$$\frac{4.8}{6}$$

$$\frac{4.7}{19}$$

$$\frac{4.8}{50}$$

$$\frac{4.3}{50}$$

$$\frac{4.3}{32}$$

$$\frac{4.6}{7}$$

44

$$\frac{4.7}{7}$$

$$\frac{4.6}{22}$$

$$\frac{4.9}{50}$$

$$\frac{3.9}{50}$$

$$\frac{4.0}{25}$$

$$\frac{4.5}{7}$$

47

$$\frac{5.2}{7}$$

$$\frac{5.1}{23}$$

$$\frac{6.1}{50}$$

$$\frac{3.9}{50}$$

$$\frac{4.2}{25}$$

$$\frac{4.7}{7}$$

48

$$\frac{5.2}{5}$$

$$\frac{5.2}{25}$$

$$\frac{6.0}{50}$$

Sta.	+	π	-	Elev
		917.80		
4+00				12.5
+50				11.6
T.P.	10.00	921.16 [✓]	6.64	911.16 [✓]
5+00				10.9
+50				10.7
6+00				11.0
+50				12.1
7+00				12.9
+50				13.7
8+00				13.7
+50				14.4
9+00				14.9
+50				16.0
B.M.	3.39	921.16 [✓]	3.39	917.77 [✓]

Lt

R

Pt

$$\frac{4.8}{50} \quad \frac{48}{33} \quad \frac{5.1}{13} \quad 53 \quad \frac{5.5}{3} \quad \frac{6.6}{25} \quad \frac{6.2}{50}$$

$$\frac{5.1}{50} \quad \frac{5.5}{27} \quad \frac{5.8}{10} \quad 6.2 \quad \frac{6.1}{4} \quad \frac{6.2}{25} \quad \frac{6.9}{50}$$

$$\frac{8.6}{50} \quad \frac{96}{25} \quad \frac{98}{7} \quad 10.3 \quad \frac{10.2}{6} \quad \frac{10.5}{25} \quad \frac{11.2}{50}$$

$$\frac{8.6}{50} \quad \frac{98}{15} \quad \frac{10.5}{10} \quad 10.5 \quad \frac{10.4}{6} \quad \frac{11.1}{24} \quad \frac{11.7}{50}$$

$$\frac{8.5}{50} \quad \frac{94}{16} \quad \frac{100}{11} \quad \frac{9.7}{5} \quad 10.2 \quad \frac{10.2}{8} \quad \frac{11.0}{24} \quad \frac{11.8}{50}$$

$$\frac{7.7}{50} \quad \frac{8.0}{33} \quad \frac{8.9}{11} \quad 9.1 \quad \frac{9.1}{5} \quad \frac{10.0}{24} \quad \frac{11.5}{50}$$

$$\frac{6.9}{50} \quad \frac{7.1}{28} \quad \frac{7.5}{14} \quad \frac{8.0}{12} \quad 8.3 \quad \frac{8.4}{7} \quad \frac{9.0}{25} \quad \frac{10.5}{50}$$

$$\frac{6.5}{50} \quad \frac{6.5}{35} \quad \frac{6.8}{16} \quad \frac{7.3}{10} \quad 7.5 \quad \frac{8.2}{24} \quad \frac{10.0}{50}$$

$$\frac{6.2}{50} \quad \frac{6.5}{30} \quad \frac{6.7}{16} \quad \frac{7.2}{12} \quad 7.5 \quad \frac{7.5}{6} \quad \frac{8.1}{25} \quad \frac{9.0}{50}$$

$$\frac{5.7}{50} \quad \frac{6.0}{28} \quad \frac{6.5}{10} \quad 6.8 \quad \frac{7.0}{7} \quad \frac{7.6}{24} \quad \frac{8.5}{50}$$

$$\frac{4.5}{50} \quad \frac{5.1}{30} \quad \frac{5.5}{15} \quad \frac{5.8}{13} \quad 6.3 \quad \frac{6.2}{7} \quad \frac{6.6}{25} \quad \frac{7.1}{50}$$

$$\frac{4.0}{50} \quad \frac{4.4}{16} \quad \frac{4.7}{8} \quad 5.2 \quad \frac{5.0}{5} \quad \frac{5.4}{24} \quad \frac{6.0}{50}$$

Spk in 10" Oak 30' Lt Stg 9+50

Sta	+	π	-	Elev
		921.16 ✓		
10+00				17.0
+50				17.2
11+00				16.7
+50				15.8
12+00				15.7
+50				16.1
13+00				15.9
+50				15.2
T.P.	3.29	88	3.78	117.5
14+00				14.5
T.P.	3.29	920.67 ✓	3.78	917.38 ✓
+50				14.2
15				14.2
+50				14.2

L+

R

R+

$$\frac{3.8}{50} \quad \frac{3.8}{22} \quad \frac{4.5}{15} \quad \frac{4.0}{8} \quad 4.2 \quad \frac{4.1}{4} \quad \frac{4.4}{25} \quad \frac{5.0}{50}$$

$$\frac{3.6}{50} \quad \frac{3.7}{17} \quad \frac{3.8}{8} \quad 4.0 \quad \frac{4.2}{4} \quad \frac{3.9}{5} \quad \frac{4.1}{25} \quad \frac{4.4}{50}$$

$$\frac{3.7}{50} \quad \frac{4.1}{17} \quad \frac{4.2}{7} \quad 4.5 \quad \frac{4.8}{3} \quad \frac{4.3}{4} \quad \frac{4.5}{25} \quad \frac{4.6}{50}$$

$$\frac{3.8}{50} \quad \frac{4.6}{13} \quad \frac{5.1}{10} \quad 5.4 \quad \frac{5.3}{6} \quad \frac{5.3}{24} \quad \frac{5.2}{50}$$

$$\frac{4.0}{50} \quad \frac{4.5}{31} \quad \frac{4.8}{16} \quad \frac{5.0}{9} \quad 5.5 \quad \frac{5.3}{4} \quad \frac{5.6}{25} \quad \frac{5.1}{50}$$

$$\frac{4.2}{50} \quad \frac{4.6}{23} \quad \frac{4.7}{8} \quad 5.1 \quad \frac{4.8}{5} \quad \frac{5.1}{25} \quad \frac{5.6}{50}$$

$$\frac{4.0}{50} \quad \frac{4.3}{28} \quad \frac{4.4}{17} \quad \frac{4.8}{16} \quad \frac{4.6}{8} \quad 5.3 \quad \frac{4.9}{3} \quad \frac{5.3}{25} \quad \frac{5.9}{50}$$

$$\frac{4.6}{50} \quad \frac{5.4}{17} \quad \frac{5.4}{9} \quad 6.0 \quad \frac{5.7}{3} \quad \frac{6.1}{25} \quad \frac{6.5}{50}$$

$$\frac{5.3}{50} \quad \frac{5.4}{28} \quad \frac{5.9}{17} \quad \frac{6.3}{16} \quad \frac{6.1}{8} \quad 6.7 \quad \frac{6.4}{3} \quad \frac{6.7}{25} \quad \frac{7.2}{50}$$

$$\frac{5.1}{50} \quad \frac{5.8}{19} \quad \frac{6.0}{13} \quad \frac{5.9}{8} \quad 6.5 \quad \frac{6.2}{3} \quad \frac{6.5}{24} \quad \frac{7.0}{50}$$

$$\frac{5.6}{50} \quad \frac{6.0}{17} \quad \frac{6.0}{8} \quad 6.5 \quad \frac{6.2}{3} \quad \frac{6.4}{25} \quad \frac{7.1}{50}$$

$$\frac{6.0}{50} \quad \frac{6.2}{18} \quad \frac{6.5}{13} \quad \frac{6.2}{7} \quad 6.5 \quad \frac{6.3}{3} \quad \frac{6.6}{24} \quad \frac{7.1}{50}$$

Sta	+	π	-	Elev
		920.67		
16+00				14.0
+50				14.7
17+00				14.7
+50				13.6
18				12.7
T.P.	2.34	917.13 ✓	5.88	914.79 ✓
+50				11.5
19				12.0
+50				12.6
20				12.7
B.M.	3.39	917.13 ✓	3.39	913.74 ✓
+50				12.4
21				11.6
+50				10.6

Lt

R

Rt

14

$$\frac{6.5}{50} \quad \frac{6.4}{27} \quad \frac{6.6}{14} \quad \frac{6.9}{12} \quad \frac{6.4}{7} \quad \frac{6.7}{2} \quad \frac{6.3}{25} \quad \frac{6.4}{50}$$

$$\frac{6.4}{50} \quad \frac{5.8}{18} \quad \frac{6.1}{13} \quad \frac{5.7}{7} \quad 6.0 \quad \frac{5.5}{2} \quad \frac{5.5}{24} \quad \frac{5.6}{50}$$

$$\frac{7.1}{50} \quad \frac{6.4}{15} \quad \frac{5.8}{8} \quad 6.0 \quad \frac{5.6}{2} \quad \frac{5.4}{15} \quad \frac{5.1}{25} \quad \frac{4.7}{50}$$

$$\frac{8.0}{50} \quad \frac{7.3}{21} \quad \frac{6.9}{7} \quad 7.1 \quad \frac{6.3}{2} \quad \frac{6.0}{15} \quad \frac{5.6}{50}$$

$$\frac{8.5}{50} \quad \frac{8.1}{17} \quad \frac{7.8}{8} \quad 8.0 \quad \frac{8.0}{2} \quad \frac{7.7}{4} \quad \frac{7.1}{25} \quad \frac{6.5}{50}$$

$$\frac{5.3}{50} \quad \frac{5.3}{27} \quad \frac{5.5}{13} \quad \frac{5.1}{7} \quad 5.6 \quad \frac{5.6}{2} \quad \frac{5.1}{5} \quad \frac{4.8}{25} \quad \frac{4.3}{50}$$

$$\frac{5.6}{50} \quad \frac{5.1}{16} \quad \frac{5.4}{12} \quad \frac{4.9}{5} \quad 5.1 \quad \frac{5.4}{4} \quad \frac{4.9}{6} \quad \frac{4.7}{25} \quad \frac{4.6}{50}$$

$$\frac{4.9}{50} \quad \frac{4.3}{16} \quad \frac{4.7}{11} \quad \frac{4.3}{5} \quad 4.5 \quad \frac{4.7}{4} \quad \frac{4.3}{6} \quad \frac{4.3}{25} \quad \frac{4.4}{50}$$

$$\frac{4.5}{50} \quad \frac{4.5}{21} \quad \frac{4.5}{10} \quad \frac{4.4}{4} \quad 4.4 \quad \frac{4.8}{5} \quad \frac{4.3}{7} \quad \frac{4.5}{25} \quad \frac{4.7}{50}$$

SpK in 8" Oak 45" Lt 54" 20+20

$$\frac{4.5}{50} \quad \frac{4.6}{13} \quad \frac{5.0}{10} \quad \frac{4.8}{8} \quad 4.7 \quad \frac{5.2}{5} \quad \frac{4.9}{8} \quad \frac{5.1}{25} \quad \frac{5.3}{50}$$

$$\frac{5.1}{50} \quad \frac{5.2}{16} \quad \frac{5.6}{12} \quad \frac{5.4}{7} \quad 5.5 \quad \frac{5.8}{5} \quad \frac{5.7}{7} \quad \frac{5.9}{25} \quad \frac{6.3}{50}$$

$$\frac{5.8}{50} \quad \frac{6.3}{15} \quad \frac{6.4}{7} \quad 6.5 \quad \frac{6.8}{4} \quad \frac{6.5}{6} \quad \frac{7.1}{25} \quad \frac{7.9}{25}$$

Sta	+	π	-	Elev
		917.13		
21+82				09.7
22+00				09.6
+50				10.4
23+00				10.6
T.P	3.50	914.70 ✓	5.93	911.20 ✓
+50				10.2
24+00				09.3
+25				09.0
+38				09.0
+50				08.7
+65				08.2
25				07.7
+50				07.1

L+

X

R+

$$\frac{7.1}{50} \quad \frac{7.1}{15} \quad \frac{7.2}{9} \quad 74 \quad \frac{7.5}{5} \quad \frac{7.8}{25} \quad \frac{8.5}{20}$$

$$\frac{8.0}{50} \quad \frac{7.4}{16} \quad \frac{7.4}{9} \quad 75 \quad \frac{7.5}{5} \quad \frac{7.5}{25} \quad \frac{7.9}{20}$$

$$\frac{7.5}{50} \quad \frac{6.9}{24} \quad \frac{6.6}{8} \quad 67 \quad \frac{6.3}{6} \quad \frac{6.2}{25} \quad \frac{6.3}{33} \quad \frac{6.4}{50}$$

$$\frac{6.4}{50} \quad \frac{6.4}{14} \quad \frac{6.4}{9} \quad \frac{6.3}{4} \quad 65 \quad \frac{6.7}{2} \quad \frac{6.2}{4} \quad \frac{6.2}{7} \quad \frac{6.4}{25} \quad \frac{6.2}{60}$$

Nail in Top of Stamp 40' L of Sta 22+70

$$\frac{4.1}{50} \quad \frac{4.2}{13} \quad \frac{4.4}{9} \quad \frac{4.3}{4} \quad 45 \quad \frac{4.8}{3} \quad \frac{4.5}{3} \quad \frac{4.9}{24} \quad \frac{5.3}{50}$$

$$\frac{4.9}{50} \quad \frac{5.1}{26} \quad \frac{5.1}{13} \quad \frac{5.3}{11} \quad \frac{5.3}{7} \quad 5.4 \quad \frac{5.5}{3} \quad \frac{5.6}{17} \quad \frac{5.8}{25} \quad \frac{6.5}{50}$$

$$\frac{6.5}{50} \quad \frac{5.9}{21} \quad \frac{5.9}{5} \quad 5.7 \quad \frac{5.8}{3} \quad \frac{6.4}{15} \quad \frac{6.8}{34} \quad \frac{7.2}{50}$$

$$\frac{5.2}{50} \quad \frac{4.7}{19} \quad \frac{5.4}{10} \quad \frac{5.7}{7} \quad 5.7 \quad \frac{5.8}{4} \quad \frac{6.5}{11} \quad \frac{5.0}{13} \quad \frac{5.3}{27} \quad \frac{5.2}{50}$$

$$\frac{5.3}{50} \quad \frac{5.0}{12} \quad \frac{6.1}{11} \quad \frac{5.8}{6} \quad 6.0 \quad \frac{6.3}{5} \quad \frac{6.5}{12} \quad \frac{5.0}{13} \quad \frac{5.3}{29} \quad \frac{5.4}{50}$$

$$\frac{8.5}{100} \quad \frac{7.7}{100} \quad \frac{6.5}{50} \quad \frac{6.4}{22} \quad \frac{6.7}{7} \quad 65 \quad \frac{7.3}{8} \quad \frac{7.8}{18} \quad \frac{8.0}{28} \quad \frac{8.3}{50} \quad \frac{8.4}{100}$$

$$\frac{6.8}{50} \quad \frac{6.5}{27} \quad \frac{6.7}{14} \quad \frac{7.2}{8} \quad \frac{7.1}{4} \quad 70 \quad \frac{7.4}{6} \quad \frac{7.8}{9} \quad \frac{7.7}{11} \quad \frac{8.2}{27} \quad \frac{8.5}{50}$$

$$\frac{7.7}{50} \quad \frac{8.1}{33} \quad \frac{8.0}{10} \quad \frac{8.5}{8} \quad \frac{8.1}{4} \quad 76 \quad \frac{7.8}{5} \quad \frac{8.3}{6} \quad \frac{8.3}{27} \quad \frac{8.0}{50}$$

Sta	+	π	-	Elev
		914.70		
26+00				07.0.
+50				07.8.
27				08.1.
+50				08.6.
28				08.7.
T.P.	5.40	915.36 ✓	4.74	909.96 ✓
+50				09.1.
29+00				09.1.
+50				09.6.
30				10.0.
+50				10.5.
31				10.4.
+06				10.4.

24

2

14

16

$$\frac{7.9}{50} \quad \frac{8.0}{26} \quad \frac{8.6}{8} \quad \frac{8.3}{5} \quad 7.7 \quad \frac{8.2}{11} \quad \frac{8.1}{20} \quad \frac{8.0}{29} \quad \frac{7.4}{42} \quad \frac{6.8}{50}$$

$$\frac{7.5}{50} \quad \frac{6.7}{37} \quad \frac{7.1}{11} \quad \frac{7.3}{6} \quad 6.9 \quad \frac{7.7}{8} \quad \frac{7.4}{11} \quad \frac{7.2}{27} \quad \frac{6.3}{60}$$

$$\frac{7.8}{50} \quad \frac{6.8}{12} \quad \frac{7.2}{8} \quad 6.6 \quad \frac{6.8}{4} \quad \frac{7.2}{8} \quad \frac{6.9}{12} \quad \frac{6.8}{28} \quad \frac{5.8}{50}$$

$$\frac{6.6}{50} \quad \frac{6.4}{28} \quad \frac{6.3}{10} \quad \frac{6.7}{7} \quad 6.1 \quad \frac{6.5}{7} \quad \frac{6.6}{9} \quad \frac{6.1}{11} \quad \frac{5.9}{27} \quad \frac{5.4}{60}$$

$$\frac{6.4}{50} \quad \frac{6.0}{28} \quad \frac{6.1}{9} \quad \frac{6.5}{8} \quad 6.0 \quad \frac{6.3}{7} \quad \frac{6.2}{27} \quad \frac{5.8}{33} \quad \frac{6.1}{38} \quad \frac{5.7}{50}$$

$$\frac{6.2}{50} \quad \frac{6.5}{9} \quad \frac{6.9}{7} \quad \frac{6.7}{4} \quad 6.3 \quad \frac{6.9}{6} \quad \frac{6.9}{27} \quad \frac{7.0}{50}$$

$$\frac{6.2}{50} \quad \frac{6.3}{10} \quad \frac{6.8}{8} \quad 6.3 \quad \frac{6.8}{6} \quad \frac{6.8}{11} \quad \frac{7.3}{27} \quad \frac{7.7}{50}$$

$$\frac{5.4}{50} \quad \frac{5.7}{30} \quad \frac{5.9}{10} \quad \frac{6.3}{9} \quad 5.8 \quad \frac{6.4}{5} \quad \frac{6.3}{10} \quad \frac{6.6}{27} \quad \frac{7.1}{40} \quad \frac{6.9}{50}$$

$$\frac{4.5}{50} \quad \frac{4.9}{33} \quad \frac{5.4}{11} \quad \frac{5.5}{8} \quad 5.4 \quad \frac{6.0}{7} \quad \frac{5.7}{11} \quad \frac{6.0}{16} \quad \frac{4.8}{41} \quad \frac{6.0}{50}$$

$$\frac{4.5}{50} \quad \frac{4.5}{27} \quad \frac{4.7}{11} \quad \frac{5.0}{8} \quad 4.9 \quad \frac{5.5}{6} \quad \frac{5.1}{8} \quad \frac{5.3}{25} \quad \frac{5.4}{40} \quad \frac{5.1}{50}$$

$$\frac{4.1}{50} \quad \frac{4.4}{13} \quad \frac{4.9}{11} \quad 5.0 \quad \frac{5.1}{7} \quad \frac{4.7}{8} \quad \frac{4.9}{29} \quad \frac{5.0}{50}$$

$$\frac{4.5}{50} \quad \frac{4.4}{25} \quad \frac{4.6}{13} \quad \frac{5.1}{11} \quad 5.0 \quad \frac{5.4}{7} \quad \frac{5.1}{9} \quad \frac{4.7}{27} \quad \frac{4.9}{50}$$

Sta + π - Elev

915.36

31+10

10.1

+23

09.7

B.M

4.44

910.92 ✓

910.91 ✓

Lt

~~Rt~~

Rt

$$\frac{5.9}{50}$$

$$\frac{5.5}{29}$$

$$\frac{5.3}{13}$$

$$5.3$$

$$\frac{5.5}{16}$$

$$\frac{5.5}{30}$$

$$\frac{5.2}{50}$$

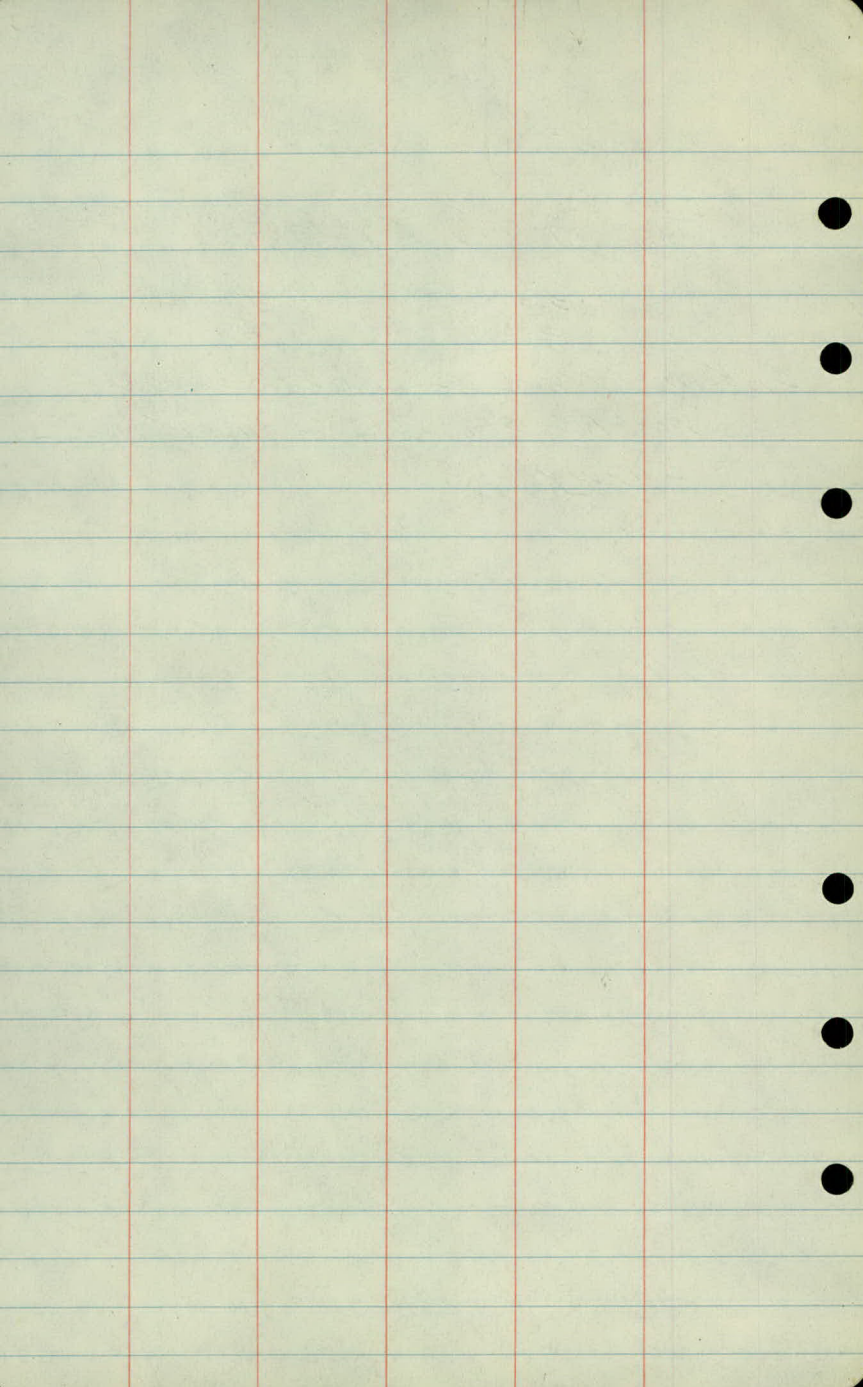
$$\frac{5.3}{50}$$

$$5.7$$

$$\frac{5.0}{50}$$

Spk. in 14" Oak 150' Rt Sta 32+00

(100' Rt Sta 36+30 Long Lake Rd)
Survey



Slope Stokes

Shexwood Road

Sta	+	π	-	Elev
-----	---	-------	---	------

B.M	3.55	918.08		914.53
-----	------	--------	--	--------

0+00				13.5	X
------	--	--	--	------	---

+13				13.5	X
-----	--	--	--	------	---

+17				13.5	X
-----	--	--	--	------	---

+21				13.5	X
-----	--	--	--	------	---

+25				13.5	
-----	--	--	--	------	--

+50				13.5	
-----	--	--	--	------	--

1				13.5	
---	--	--	--	------	--

+50				13.4	
-----	--	--	--	------	--

2				13.4	
---	--	--	--	------	--

+50				13.3	
-----	--	--	--	------	--

3				13.3	
---	--	--	--	------	--

+50				13.2	
-----	--	--	--	------	--

Gr Rod

Lt

R

Rt

Spk in 30" Oak 46' Rt Stg 0-24

X

X

X

X

4.6

$$\begin{array}{r} 5.0 \\ DC 1.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 4.8 \\ FO.2 \\ \hline \end{array}$$

$$\begin{array}{r} 4.5 \\ CO.1 \\ \hline 25.0 \end{array}$$

4.6

$$\begin{array}{r} 5.2 \\ DC 1.4 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 5.2 \\ FO.6 \\ \hline \end{array}$$

$$\begin{array}{r} 4.9 \\ DC 1.7 \\ \hline 24.4 \end{array}$$

4.6

$$\begin{array}{r} 5.7 \\ DC. 0.9 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 5.9 \\ FI.3 \\ \hline \end{array}$$

$$\begin{array}{r} 5.6 \\ DC 1.0 \\ \hline 23.0 \end{array}$$

4.7

$$\begin{array}{r} 5.9 \\ DC 0.8 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 5.9 \\ FI.2 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ DC 1.2 \\ \hline 23.4 \end{array}$$

4.7

$$\begin{array}{r} 5.1 \\ DC 1.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ FO.3 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ DC 1.7 \\ \hline 24.4 \end{array}$$

4.8

$$\begin{array}{r} 4.6 \\ CO.2 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 4.8 \\ FO.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ DC 1.8 \\ \hline 24.6 \end{array}$$

4.8

$$\begin{array}{r} 4.3 \\ CO.5 \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 4.9 \\ FO.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ DC 1.3 \\ \hline 23.6 \end{array}$$

4.9

$$\begin{array}{r} 4.5 \\ CO.4 \\ \hline 25 \end{array}$$

$$\begin{array}{r} 5.2 \\ FO.3 \\ \hline \end{array}$$

$$\begin{array}{r} 5.6 \\ DC 1.5 \\ \hline 24.0 \end{array}$$

Sta	+	π	-	Elev
		918.08		

4				13.2
---	--	--	--	------

+50				13.1
-----	--	--	--	------

T.P.	7.85	919.01	6.92	911.16
------	------	--------	------	--------

5				13.1
---	--	--	--	------

+50				13.2
-----	--	--	--	------

6				13.4
---	--	--	--	------

+50				13.7
-----	--	--	--	------

7				14.1
---	--	--	--	------

+50				14.4
-----	--	--	--	------

8				14.8
---	--	--	--	------

+50				15.1
-----	--	--	--	------

9				15.5
---	--	--	--	------

+50				15.8
-----	--	--	--	------

B.M	3.06	920.83	1.26	917.75
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917.77

Gr Rod Lt R Pt

$$\begin{array}{r} 4.9 \\ \hline \text{DC } 1.7 \\ 24.2 \end{array} \quad \begin{array}{r} 5.5 \\ \hline \text{FO.6} \end{array} \quad \begin{array}{r} 6.0 \\ \hline \text{DC } 0.9 \\ 22.8 \end{array}$$

$$\begin{array}{r} 5.0 \\ \hline \text{DC } 1.2 \\ 23.4 \end{array} \quad \begin{array}{r} 6.4 \\ \hline \text{FI.4} \end{array} \quad \begin{array}{r} 6.5 \\ \hline \text{DC } 0.5 \\ 22.0 \end{array}$$

$$\begin{array}{r} 5.9 \\ \hline \text{DC } 0.6 \\ 22.2 \end{array} \quad \begin{array}{r} 8.0 \\ \hline \text{F2.1} \end{array} \quad \begin{array}{r} 8.3 \\ \hline \text{F2.4} \\ 17.9 \end{array}$$

$$\begin{array}{r} 5.8 \\ \hline \text{DC } 0.4 \\ 21.8 \end{array} \quad \begin{array}{r} 8.2 \\ \hline \text{F2.4} \end{array} \quad \begin{array}{r} 8.7 \\ \hline \text{F2.9} \\ 18.8 \end{array}$$

$$\begin{array}{r} 5.6 \\ \hline \text{DC } 0.4 \\ 21.8 \end{array} \quad \begin{array}{r} 8.0 \\ \hline \text{F2.4} \end{array} \quad \begin{array}{r} 8.7 \\ \hline \text{F3.1} \\ 19.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ \hline \text{DC } 1.2 \\ 23.4 \end{array} \quad \begin{array}{r} 7.0 \\ \hline \text{FI.7} \end{array} \quad \begin{array}{r} 7.5 \\ \hline \text{F2.2} \\ 17.4 \end{array}$$

$$\begin{array}{r} 4.9 \\ \hline \text{DC } 1.8 \\ 24.6 \end{array} \quad \begin{array}{r} 6.0 \\ \hline \text{FI.1} \end{array} \quad \begin{array}{r} 6.7 \\ \hline \text{DC } 0.2 \\ 21.4 \end{array}$$

$$\begin{array}{r} 4.6 \\ \hline \text{DC } 1.9 \\ 24.8 \end{array} \quad \begin{array}{r} 5.4 \\ \hline \text{FO.8} \end{array} \quad \begin{array}{r} 6.1 \\ \hline \text{DC } 0.5 \\ 22.0 \end{array}$$

$$\begin{array}{r} 4.2 \\ \hline \text{DC } 1.7 \\ 24.4 \end{array} \quad \begin{array}{r} 5.1 \\ \hline \text{FO.9} \end{array} \quad \begin{array}{r} 5.9 \\ \hline \text{DC } 0.3 \\ 21.6 \end{array}$$

$$\begin{array}{r} 3.9 \\ \hline \text{DC } 1.9 \\ 24.8 \end{array} \quad \begin{array}{r} 4.7 \\ \hline \text{FO.8} \end{array} \quad \begin{array}{r} 5.5 \\ \hline \text{DC } 0.4 \\ 21.8 \end{array}$$

$$\begin{array}{r} 3.5 \\ \hline \text{CO.6} \\ 25.0 \end{array} \quad \begin{array}{r} 4.1 \\ \hline \text{FO.6} \end{array} \quad \begin{array}{r} 4.3 \\ \hline \text{DC } 1.2 \\ 23.4 \end{array}$$

$$\begin{array}{r} 3.2 \\ \hline \text{C } 1.0 \\ 25.0 \end{array} \quad \begin{array}{r} 2.8 \\ \hline \text{CO.4} \end{array} \quad \begin{array}{r} 3.3 \\ \hline \text{DC } 1.9 \\ 24.8 \end{array}$$

SpK in 10" dia 30 Lt 5tg 9t50

Sta	+	π	-	Elev
		920.83		
10+00				16.1
+50				16.2
11				16.2
+50				16.1
12				15.9
+50				15.7
13				15.5
+50				15.3
14				15.1
+50				14.9
T.P.	4.42	919.47 ⁵	5.78	915.05
15				14.7
+50				14.5

Gr Rod Lt E Rx

4.7	$\frac{3.6}{C 1.1}$	$\frac{3.8}{C 0.9}$	$\frac{4.2}{C 0.5}$
25	25		25

4.6	$\frac{3.4}{C 1.2}$	$\frac{3.8}{C 0.8}$	$\frac{3.8}{C 0.8}$
	25		25

4.6	$\frac{3.7}{C 0.9}$	$\frac{4.2}{C 0.4}$	$\frac{4.2}{C 0.4}$
	25.0		25

4.7	$\frac{4.2}{C 0.5}$	$\frac{5.2}{F 0.5}$	$\frac{4.9}{DC 1.8}$
	25		24.6

4.9	$\frac{4.4}{C 0.5}$	$\frac{5.2}{F 0.3}$	$\frac{5.3}{DC 1.6}$
	25		24.2

5.1	$\frac{4.3}{C 0.8}$	$\frac{5.0}{C 0.1}$	$\frac{4.8}{C 0.3}$
	25		25

5.3	$\frac{4.0}{C 1.3}$	$\frac{5.0}{C 0.3}$	$\frac{5.0}{C 0.3}$
	25		25

5.5	$\frac{4.4}{C 1.4}$	$\frac{5.7}{F 0.2}$	$\frac{5.8}{DC 1.7}$
	25.0		24.4

5.7	$\frac{5.4}{C 0.3}$	$\frac{6.4}{F 0.7}$	$\frac{6.4}{DC 1.3}$
	25.		23.6

5.9	$\frac{5.8}{C 0.1}$	$\frac{6.7}{F 0.8}$	$\frac{6.7}{DC 1.2}$
	25		23.4

4.8	$\frac{4.5}{C 0.3}$	$\frac{5.4}{F 0.6}$	$\frac{5.2}{DC 1.6}$
	25		24.2

5.0	$\frac{4.9}{C 0.1}$	$\frac{5.5}{F 0.5}$	$\frac{5.4}{DC 1.6}$
	25		24.2

Sta	+	π ⁵	-	Elev
		919.47		
16+00				14.3
+50				14.1
17				13.9
+50				13.7
18				13.5
+50				13.3
19				13.1
+50				12.9
20				12.7
B.M.	1.82	915.56	5.75	913.72
+50				12.5
21				12.2
+50				11.9

913.74

Gr Red

Lt

R

Rt

52

$$\begin{array}{r} 5.2 \\ \text{C.O.0} \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 5.5 \\ \text{F.O.3} \end{array}$$

$$\begin{array}{r} 5.2 \\ \text{C.O.0} \\ \hline 2.5 \end{array}$$

54

$$\begin{array}{r} 4.9 \\ \text{C.O.5} \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 4.8 \\ \text{C.O.6} \end{array}$$

$$\begin{array}{r} 4.3 \\ \text{C.I.1} \\ \hline 2.5 \end{array}$$

56

$$\begin{array}{r} 5.2 \\ \text{C.O.4} \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 4.9 \\ \text{C.O.7} \end{array}$$

$$\begin{array}{r} 3.8 \\ \text{C.I.8} \\ \hline 2.5 \end{array}$$

58

$$\begin{array}{r} 6.3 \\ \text{DC 1.5} \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 5.7 \\ \text{C.O.1} \end{array}$$

$$\begin{array}{r} 4.9 \\ \text{C.O.9} \\ \hline 2.5 \end{array}$$

60

$$\begin{array}{r} 6.9 \\ \text{DC 1.1} \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 6.8 \\ \text{F.O.8} \end{array}$$

$$\begin{array}{r} 5.9 \\ \text{C.O.1} \\ \hline 2.5 \end{array}$$

62

$$\begin{array}{r} 7.8 \\ \text{DC 0.4} \\ \hline 21.8 \end{array}$$

$$\begin{array}{r} 7.9 \\ \text{F.I.7} \end{array}$$

$$\begin{array}{r} 7.2 \\ \text{DC 1.0} \\ \hline 23.0 \end{array}$$

64

$$\begin{array}{r} 7.7 \\ \text{DC 0.7} \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 7.4 \\ \text{F.I.0} \end{array}$$

$$\begin{array}{r} 6.9 \\ \text{DC 1.5} \\ \hline 24.0 \end{array}$$

66

$$\begin{array}{r} 6.9 \\ \text{DC 1.7} \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 6.8 \\ \text{F.O.2} \end{array}$$

$$\begin{array}{r} 6.6 \\ \text{C.O.0} \\ \hline 2.5 \end{array}$$

68

$$\begin{array}{r} 6.7 \\ \text{C.O.1} \\ \hline 25.0 \end{array}$$

$$\begin{array}{r} 6.7 \\ \text{C.O.1} \end{array}$$

$$\begin{array}{r} 6.9 \\ \text{DC 1.9} \\ \hline 24.8 \end{array}$$

Spk in 8" Oak 45 Lt Sta 20 +20

3.2

$$\begin{array}{r} 3.0 \\ \text{C.O.2} \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 3.2 \\ \text{C.O.0} \end{array}$$

$$\begin{array}{r} 3.5 \\ \text{DC 1.7} \\ \hline 24.4 \end{array}$$

3.4

$$\begin{array}{r} 3.4 \\ \text{C.O.0} \\ \hline 2.5 \end{array}$$

$$\begin{array}{r} 3.9 \\ \text{F.O.5} \end{array}$$

$$\begin{array}{r} 4.3 \\ \text{DC 1.1} \\ \hline 23.2 \end{array}$$

37

$$\begin{array}{r} 4.6 \\ \text{DC 4.1} \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ \text{F.I.3} \end{array}$$

$$\begin{array}{r} 5.5 \\ \text{DC 0.2} \\ \hline 21.4 \end{array}$$

Sta	+	π	-	Elev
		915.56 ⁶		
21+82				11.7
22				11.6
+50				11.3
23				11.0
+50				10.7
24				10.4
+25				10.3
+38				10.2
+50				10.1
+65				10.0
25				09.8
+50				09.5

Gr. Rod	Lt	X	Rt
3.9	$\begin{array}{r} 5.4 \\ DC 0.5 \\ \hline 22.0 \end{array}$	$\begin{array}{r} 5.8 \\ F 1.9 \\ \hline \end{array}$	$\begin{array}{r} 6.1 \\ F 2.2 \\ \hline 17.4 \end{array}$
4.0	$\begin{array}{r} 5.9 \\ DC 0.1 \\ \hline 21.2 \end{array}$	$\begin{array}{r} 6.0 \\ F 2.0 \\ \hline \end{array}$	$\begin{array}{r} 6.1 \\ F 2.1 \\ \hline 17.2 \end{array}$
4.3	$\begin{array}{r} 5.2 \\ DC 1.1 \\ \hline 23.2 \end{array}$	$\begin{array}{r} 5.1 \\ F 0.8 \\ \hline \end{array}$	$\begin{array}{r} 4.7 \\ DC 1.6 \\ \hline 24.2 \end{array}$
4.6	$\begin{array}{r} 4.8 \\ DC 1.8 \\ \hline 24.6 \end{array}$	$\begin{array}{r} 5.0 \\ F 0.4 \\ \hline \end{array}$	$\begin{array}{r} 4.7 \\ DC 1.9 \\ \hline 24.8 \end{array}$
4.9	$\begin{array}{r} 5.0 \\ DC 1.9 \\ \hline 24.8 \end{array}$	$\begin{array}{r} 5.4 \\ F 0.5 \\ \hline \end{array}$	$\begin{array}{r} 5.7 \\ DC 1.2 \\ \hline 23.4 \end{array}$
5.2	$\begin{array}{r} 5.9 \\ DC 1.3 \\ \hline 23.6 \end{array}$	$\begin{array}{r} 6.2 \\ F 1.0 \\ \hline \end{array}$	$\begin{array}{r} 6.5 \\ DC 0.7 \\ \hline 22.4 \end{array}$
5.3	$\begin{array}{r} 6.6 \\ DC 0.7 \\ \hline 22.4 \end{array}$	$\begin{array}{r} 6.7 \\ F 1.4 \\ \hline \end{array}$	$\begin{array}{r} 6.6 \\ DC 0.7 \\ \hline 22.4 \end{array}$
5.4	$\begin{array}{r} 6.1 \\ DC 1.3 \\ \hline 23.6 \end{array}$	$\begin{array}{r} 6.6 \\ F 1.2 \\ \hline \end{array}$	$\begin{array}{r} 5.9 \\ DC 1.5 \\ \hline 24.0 \end{array}$
5.5	$\begin{array}{r} 6.0 \\ DC 1.5 \\ \hline 24.0 \end{array}$	$\begin{array}{r} 6.8 \\ F 1.3 \\ \hline \end{array}$	$\begin{array}{r} 7.5 \\ DC 0.0 \\ \hline 21.0 \end{array}$
5.6	$\begin{array}{r} 7.4 \\ DC 0.2 \\ \hline 21.4 \end{array}$	$\begin{array}{r} 7.6 \\ F 2.0 \\ \hline \end{array}$	$\begin{array}{r} 8.7 \\ F 3.1 \\ \hline 19.2 \end{array}$
5.8	$\begin{array}{r} 7.4 \\ DC 0.4 \\ \hline 21.8 \end{array}$	$\begin{array}{r} 7.9 \\ F 2.1 \\ \hline \end{array}$	$\begin{array}{r} 8.8 \\ F 3.0 \\ \hline 19.0 \end{array}$
6.1	$\begin{array}{r} 9.1 \\ F 3.0 \\ \hline 19.0 \end{array}$	$\begin{array}{r} 8.8 \\ F 2.7 \\ \hline \end{array}$	$\begin{array}{r} 9.1 \\ F 3.0 \\ \hline 19.0 \end{array}$

Sta	+	π	-	Elev
-----	---	-------	---	------

915.56

26				09.4
----	--	--	--	------

T.P	6.46	913.16	8.86	906.70
-----	------	--------	------	--------

+50				09.3
-----	--	--	--	------

27				09.3
----	--	--	--	------

+50				09.4
-----	--	--	--	------

28				09.4
----	--	--	--	------

+50				09.5
-----	--	--	--	------

29				09.5
----	--	--	--	------

+50				09.6
-----	--	--	--	------

30				09.6
----	--	--	--	------

+50				09.7
-----	--	--	--	------

+94				09.7
-----	--	--	--	------

31				09.7
----	--	--	--	------

T.P	4.49	914.95	2.70	910.46
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B.M			3.96	910.99 (910.91)
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Gr. Rod	LT	R	RT
6.2	$\begin{array}{r} 9.1 \\ F 2.9 \\ \hline 18.8 \end{array}$	$\begin{array}{r} 8.8 \\ F 2.6 \\ \hline \end{array}$	$\begin{array}{r} 9.0 \\ F 2.8 \\ \hline 18.6 \end{array}$
3.9	$\begin{array}{r} 5.4 \\ DC 0.5 \\ \hline 22.0 \end{array}$	$\begin{array}{r} 5.6 \\ F 1.7 \\ \hline \end{array}$	$\begin{array}{r} 6.0 \\ F 2.1 \\ \hline 17.2 \end{array}$
3.9	$\begin{array}{r} 5.4 \\ DC 0.5 \\ \hline 22.0 \end{array}$	$\begin{array}{r} 5.1 \\ F 1.2 \\ \hline \end{array}$	$\begin{array}{r} 5.6 \\ DC 0.3 \\ \hline 21.6 \end{array}$
3.8	$\begin{array}{r} 4.8 \\ DC 1.0 \\ \hline 23.0 \end{array}$	$\begin{array}{r} 4.5 \\ F 0.7 \\ \hline \end{array}$	$\begin{array}{r} 4.4 \\ DC 1.4 \\ \hline 23.8 \end{array}$
3.8	$\begin{array}{r} 4.5 \\ DC 1.3 \\ \hline 23.6 \end{array}$	$\begin{array}{r} 4.5 \\ F 0.7 \\ \hline \end{array}$	$\begin{array}{r} 4.8 \\ DC 1.0 \\ \hline 23.0 \end{array}$
3.7	$\begin{array}{r} 4.2 \\ DC 1.5 \\ \hline 24.6 \end{array}$	$\begin{array}{r} 4.1 \\ F 0.4 \\ \hline \end{array}$	$\begin{array}{r} 4.8 \\ DC 0.9 \\ \hline 22.8 \end{array}$
3.7	$\begin{array}{r} 3.8 \\ DC 1.9 \\ \hline 24.8 \end{array}$	$\begin{array}{r} 4.0 \\ F 0.3 \\ \hline \end{array}$	$\begin{array}{r} 4.7 \\ DC 1.0 \\ \hline 23.0 \end{array}$
3.6	$\begin{array}{r} 3.6 \\ C 0.0 \\ \hline 25.0 \end{array}$	$\begin{array}{r} 3.5 \\ C 0.1 \\ \hline \end{array}$	$\begin{array}{r} 4.4 \\ DC 1.2 \\ \hline 23.4 \end{array}$
3.6	$\begin{array}{r} 2.4 \\ C 1.2 \\ \hline 25 \end{array}$	$\begin{array}{r} 3.1 \\ C 0.5 \\ \hline \end{array}$	$\begin{array}{r} 3.8 \\ DC 1.8 \\ \hline 24.6 \end{array}$
3.5	$\begin{array}{r} 2.3 \\ C 1.2 \\ \hline 25 \end{array}$	$\begin{array}{r} 2.7 \\ C 0.8 \\ \hline \end{array}$	$\begin{array}{r} 3.0 \\ C 0.5 \\ \hline 25 \end{array}$
3.5	$\begin{array}{r} 2.1 \\ C 1.4 \\ \hline 25 \end{array}$	$\begin{array}{r} 2.6 \\ C 0.9 \\ \hline \end{array}$	$\begin{array}{r} 2.7 \\ C 0.8 \\ \hline 25 \end{array}$

SpK in 14" Oak 150 RT ST 32 f o d

Sta + π - Elev