

Book-2- Dr. 11-A

X

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

CO. RD. H

W. Co. Line to Irondale Rd. Profile Levels (1946)

From S.T.H. No 63 To Mounds View Rd.

Road Acc't. No. M 2

Date Filed 11-8-29

File M-V Twp.

1
From W. Co. Line to
Irondale Rd.

Bench Levels

C.O. R.D. "H"

Long Lake Rd to West Co. Line

Profiles
Drawn up Nov. 1946

Sta	+	π	-	Elev	
B.M.	4.69	909.66			(904.97)
T.P.	10.48	909.77	10.37	899.29	
B.M.	1.23	902.31	8.69	901.08	(901.13)
T.P.	1.24	899.93	3.62	898.69	
T.P.	5.83	901.54	4.22	895.71	
B.M.			2.27	899.27	(899.32)
T.P.	4.20	897.12	8.62	892.92	
B.M.			1.04	896.08	(896.13)
T.P.	12.07	896.07	13.12	884.00	
B.M.			3.79	892.28	(892.33)

L E R

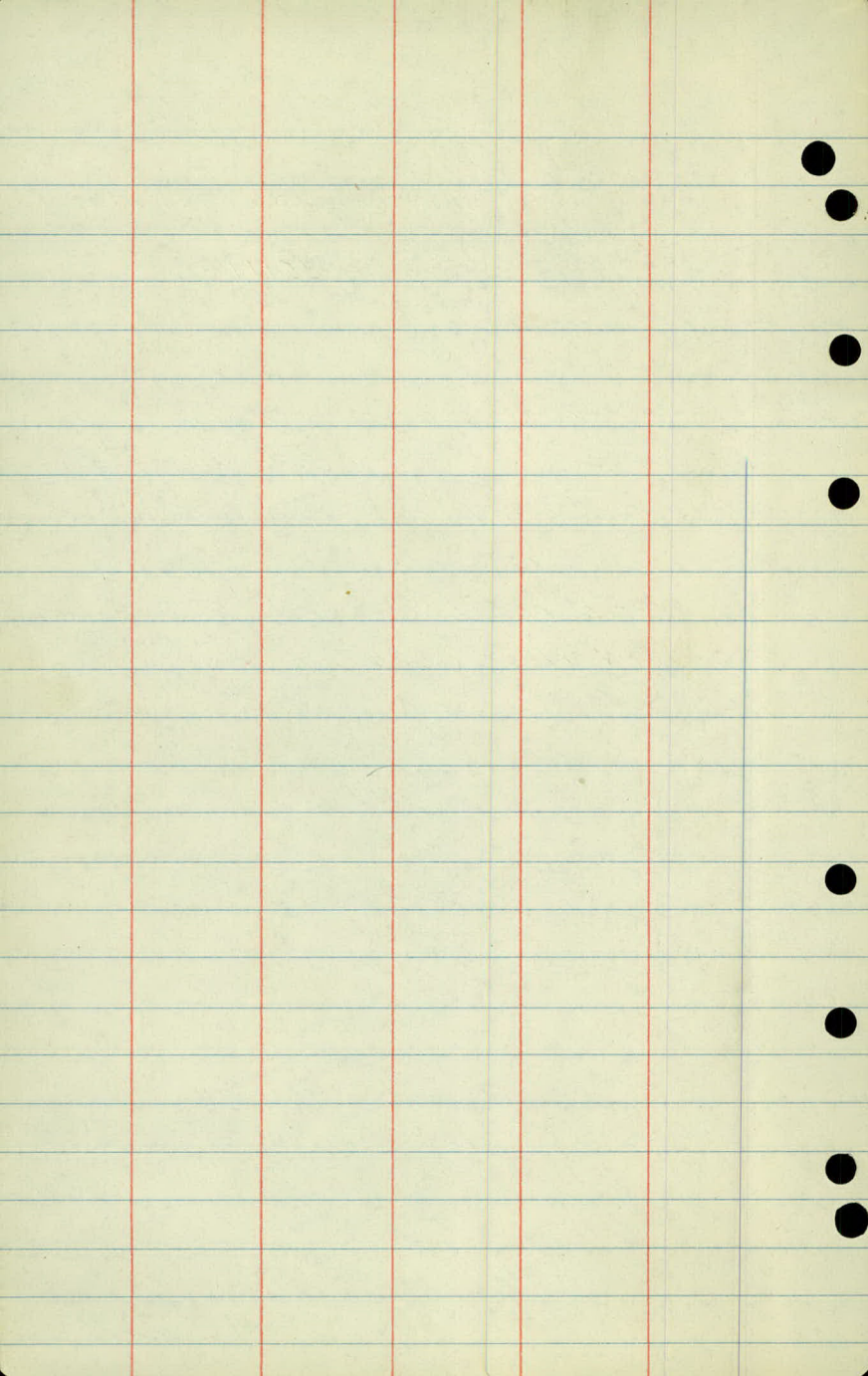
Top Mont. at Co. Rd. "H" + Long Lake Rd.
 Mont. tipped 15' N. assumed elev. ok

R.R. Spk. in 24" Oak 50' Lt. Sta 35+77

Top E. End of Door Saddle Front of Ho. at S.W. cor
 Fairchild Ave. + Co. Rd. "H" (2800 Co. Rd. "H")

Top E. End of Door Sill Front of Ho. at N.W. Cor.
 Knollwood Ave. + Co. Rd. "H"

Top E. End of Door Sill Front of Ho. 160' E. of Pleasant
 View Drive + N. Side of Co. Rd. "H"



3

Profile Levels

CO. R.D. "H"

West. Co. Line to Irendale Rd

Sta	+	π	-	Elev.
B.M.	411	896.39		992.28

0	+100			93.3
---	------	--	--	------

	+50			93.1
--	-----	--	--	------

1				93.4
---	--	--	--	------

	+50			92.9
--	-----	--	--	------

2				93.4
---	--	--	--	------

	+50			93.8
--	-----	--	--	------

3				94.5
---	--	--	--	------

+32	4 Pleasant View Rd.			94.2
-----	---------------------	--	--	------

	+60			93.9
--	-----	--	--	------

4				93.1
---	--	--	--	------

	+50			92.0
--	-----	--	--	------

K.A.
A.M.
M.B.

10-29-46

4

L

C

R

Top E. End of Door Sill Front of Ho. 140' E.
of Pleasant View Rd. & Co. Rd. "H"

92.94
31 345 340 92.94 Top Rail
8 14 48 53 93.0

33

28 30 27
33 33

35

2.9 3.0 3.3

26

2.4 19 21
33 33

2.2 2.6 3.2 3.0 3.0
50 100 200 300

25

2.5 3.3 2.8

44

Sta.	+	π	-	E/cv
		896.39		
5				90.2
	+50			87.7
6				84.2
	+50			80.3
T.P.	022	883.04	13.57	882.82
7				76.8
	+50			74.1
5	+74	ENH		
	+87			
8				72.7
	+50			73.5
9				75.3
	+50			77.2

L E R

4.5 62 2.4
33 33

6.1 87 4.8

8.8 12.2 10.0

14.1 16.1 16.3

5.37 62 10.4
Floor-Boss. Gor 70-76.0 Floor-Boss. Gor

9.8 8.9 14.2

66.3
16.7 Drains South
FL. 24' CM. - 16'

67.4 24' x 36' CM.

15.6
FL. 24' CM. - 18'

19.0 10.3 14.6
33

9.5

11.4 7.7 10.0

5.8

Sta	+	π	-	Elev.
-----	---	-------	---	-------

88304

10				79.9
----	--	--	--	------

T.P.	13.72	896.41	0.35	882.69
------	-------	--------	------	--------

+50				83.1
-----	--	--	--	------

+88

11				86.4
----	--	--	--	------

+50				89.7
-----	--	--	--	------

12				92.4
----	--	--	--	------

+50				93.4
-----	--	--	--	------

+50

13				93.4
----	--	--	--	------

+50				93.1
-----	--	--	--	------

B.M.			0.35	896.06
------	--	--	------	--------

14				92.2
----	--	--	--	------

+44 = 2 Knollwood Drive				91.4
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15				91.0
T.P.	11.16	902.04	5.53	890.88

L E E

3.8 31 2.7
33 33

12.0 13.3 11.7

85.36

11.05

Floor-Bos Gap
10

7.1 10.0 7.2

4.7

1.9 4.0 1.9

3.0

2.4 3.0 1.5

3.3

Top E. End of Dear Sill Front of Ho. N.W. Cor Knollwood # "ft"

4.7 4.2 3.7

55 5.6 50 6.3 80 drains south
100 63 40 100

51 54 6.2
33 33

Sta.	+	π	-	Elev
		902.04		

15	+50			91.1
----	-----	--	--	------

16				91.2
----	--	--	--	------

	+50			91.3
--	-----	--	--	------

17				91.8
----	--	--	--	------

	+50			93.0
--	-----	--	--	------

18				94.7
----	--	--	--	------

	+50			96.3
--	-----	--	--	------

19				97.1
----	--	--	--	------

20				96.6
----	--	--	--	------

B.M			2.78	899.26
-----	--	--	------	--------

21				96.5
----	--	--	--	------

22				96.4
----	--	--	--	------

+52 = E Fairchild Ave				96.3
-----------------------	--	--	--	------

T.P	6.61	902.78	5.87	896.17
-----	------	--------	------	--------

L E E

10.9

8.4 10.8 12.9
33 33

10.7 1

7.7 10.2 13.4

9.0

6.1 7.3 8.0

5.7

5.1 4.9 4.7

5.2 5.4 5.6

Top E. End of Door Sill Front of Hn. at 2800 60. E.H.N.

5.5 5.5 5.8

5.5 5.6 4.8

5.7 5.8 5.7 5.2 5.4 drains South
100 50 65 100

Top Mont. sto 22+71

Sta.	+	π	-	Elev.
		902.78		
23				96.1
24				95.8
25				95.8
26				95.2
27	Beg. const. & subject to change			96.4
28				98.3
+50				98.6
29				98.4
30				97.2 ✓
31				96.0
32				95.6
33				95.2
T.P.	9.73	907.32	5.19	897.59

L

E

E

7.0	6.7	7.0
33		33

7.4	7.0	7.6
-----	-----	-----

6.3	7.0	7.3
-----	-----	-----

7.1	7.6	8.2
-----	-----	-----

6.4	6.4	7.0
-----	-----	-----

2.1	4.5	3.6
-----	-----	-----

0.5	4.2	2.8
-----	-----	-----

1.8	4.4	3.7
-----	-----	-----

7.0	5.6	6.7
-----	-----	-----

Low spot

11.0	9.7	6.8	7.2
55			

12.5	11.3	7.2	10.3	9.4	Low spot
40	33		20	33	

32/502

8.3	7.6	5.6
33		

Sta.	+	Σ	-	Elev.
		907.32		
33	+50			
34				96.9
35				99.2
B.M.		6.25		901.07
	+50			
36				01.6
37				04.1
38				04.8
	+60 = End const.			05.0
39				04.4
40.				02.5
T.P.	4.85	908.78	3.39	903.93
41				00.7
42				99.4

L E E

98.6
87
3399.7
82
33

6.6 10.4 7.5

7.9 8.1 7.4

R.R. Spt. 24" Oak 50' L. s/a 35+77

7.9 99.4

6.2 5.7 5.0

2.9 3.2 3.1

3.1 2.5 3.7

2.3

3.4 2.9 2.7

4.9 4.8 4.9

7.7 8.1 8.4

9.3 9.4 10.2

Sta	+	π	-	Elev.
-----	---	-------	---	-------

904.75

43				98.8
----	--	--	--	------

+50				99.0
-----	--	--	--	------

44				00.2
----	--	--	--	------

45				02.9
----	--	--	--	------

46				04.5
----	--	--	--	------

47				06.2
----	--	--	--	------

48				07.3
----	--	--	--	------

+75				05.2
-----	--	--	--	------

49 + 11.85 = 2 Long Lake rd.				05.0
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B.M.	3.86	904.92		(904.97)
------	------	--------	--	----------

L E F

Possible pocket

10.5	10.0	10.6
33		33
10.6	10.6	9.8
12.5		10.5

9.6	9.6	9.8
-----	-----	-----

6.6	5.9	5.5
-----	-----	-----

4.6	4.3	3.8
-----	-----	-----

3.0	2.6	3.2
-----	-----	-----

3.0	1.5	1.0
-----	-----	-----

4.5	3.6	
-----	-----	--

Gut barrel and
try to fit grade
for yard on left.

38

Top Mont. H" + Long Lake Rd.

Sta.	T	π	-	Elev
------	---	-------	---	------

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2014年12月

L

E

E

Profile Levels

Co Rd H'

Long Lake Rd-East

1000

Sta.	+	π	-	Elev
B.M.	5.33	910.30		904.97

49+11.85 = @ Long Lake Rd.

B.M.			2.35	907.95
+50				05.5

50				06.1
----	--	--	--	------

+50				06.0
-----	--	--	--	------

51				05.5
----	--	--	--	------

+50				05.4
-----	--	--	--	------

52				05.5
----	--	--	--	------

53				05.5
----	--	--	--	------

54				05.9
----	--	--	--	------

55				06.2
----	--	--	--	------

+75	@ Irondale Rd.			07.4
-----	----------------	--	--	------

56			1.8	08.5
----	--	--	-----	------

K.A.
A.M.
M.B.

10-30-46

12

L

E

F

Top. Mont.

B.R.

Spt. 10 16" Oak S.E. Cor. Co. Rd. "H" & Long Lake Rd.

48

4.4
33

4.2

28
33

43

5.5
33

4.6

4.1
33

49

5.9

4.8

5.3

6.1

4.8

5.5

4.7

4.4

4.9

2.7

4.1

2.9

Drains north 57 4.1 3.5 29 2.7 2.4 1.7
200 100 50 50 80 190

Sta	+	π	-	Elev
		910.30		
56	+50		2.4	07.9
57			2.9	07.4
	+50		4.7	05.6
58			7.9	02.4
B.M.			5.34	904.96
				904.97

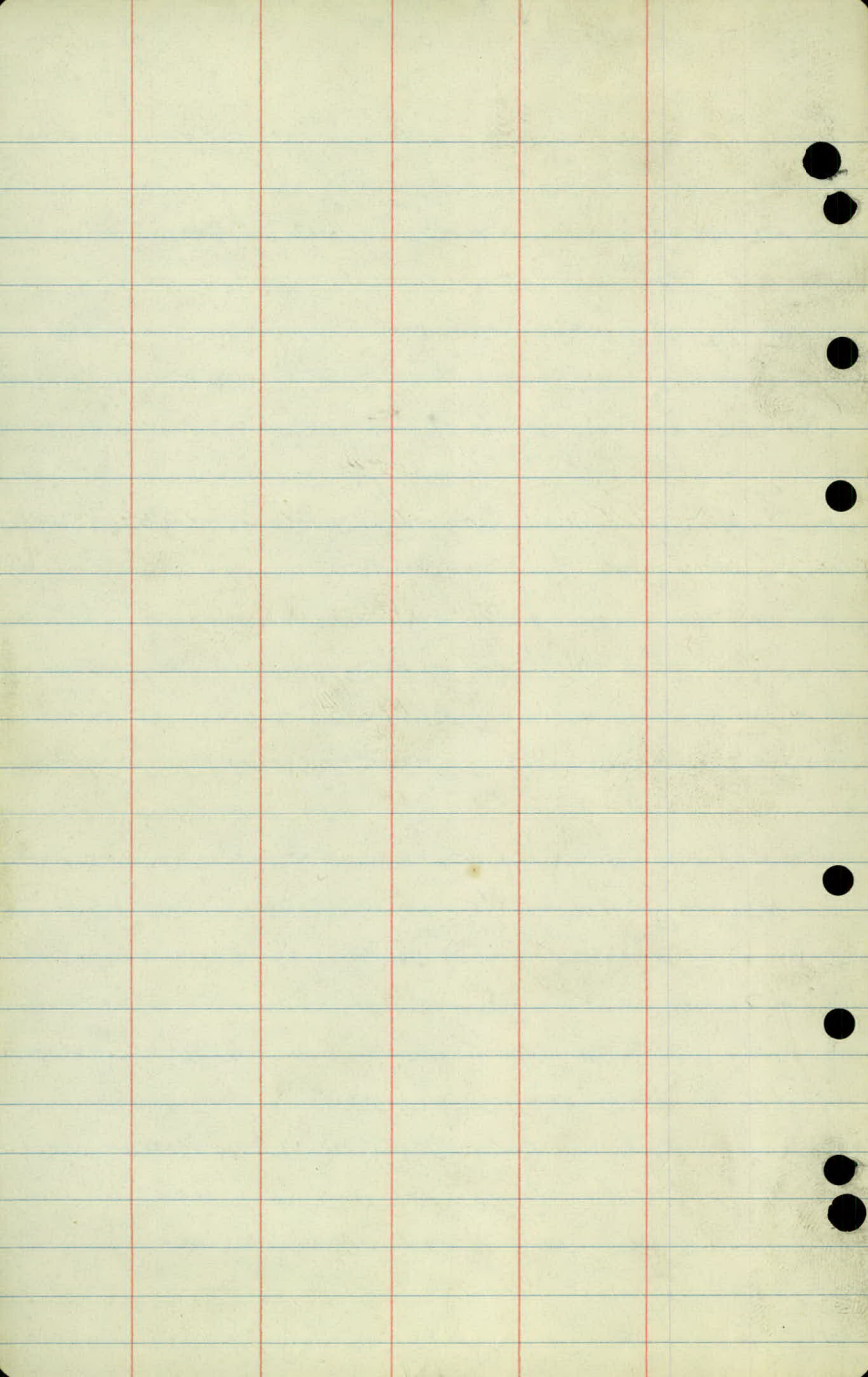
L

E

R

Drains east into Rice Creek Bottoms

Top Mont. Long Lake Rd + H^u



ALIGNMENT

MOUNDS VIEW TWP. ROAD. N. LINE

SEC. 16.-30-23.

STRA. POINT A LT. A RT.

26 + 41 ⁵

MOUNDS VIEW ROAD.

9 + 29 ⁹ P.O.T.

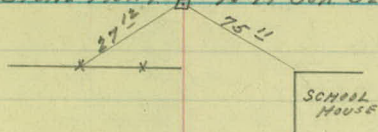
3 + 59 ⁸ P.O.T.

N 40° - 00' E.

0 + 00

CLEVELAND AVE.

STONE MONT N $\frac{1}{4}$ COR SEC. 16-30-23



65

50

11

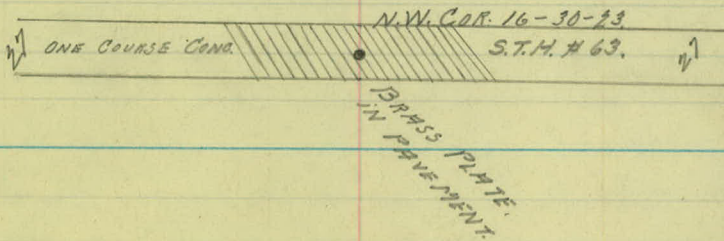
8" OR X

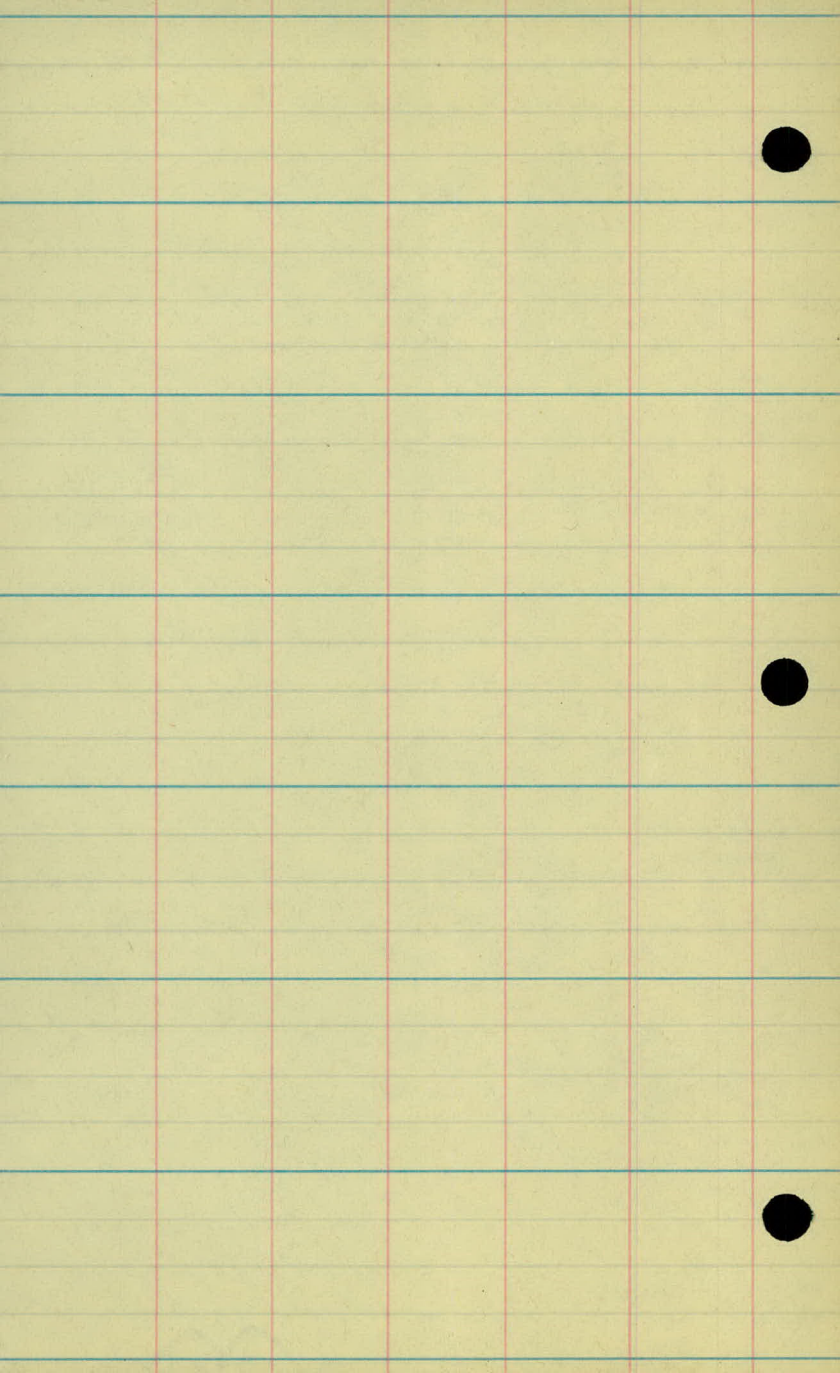
11

40

11

27





ART. TOPOG.
MOUNDS VIEW TWP. ROAD.

5

4

3

2

1

0700

2-5-29

F 2

FL3

F 4

F. 5

718 DEG. OF PEOPLE

F. 6

440 F. Cor 5

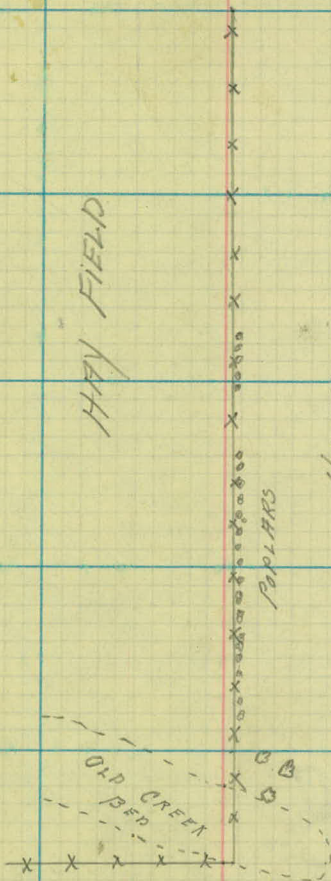
71

HAY FIELD

Uncultivated

POPULARS

OLD CREEK
BED



11

10

9

8

7

6

5

2-5-29

F. 1

F. 25

F. 3

75° X. F

HAY FIELD

HAY FIELD

F. 1873

OHNS

OHNS

POPLARS & WILLOWS

UNCULTIVATED

F. 0

F. 1

17

16

15

14

13

12

11

2-5-29

F3⁵

F4

F4

F4

186 X.F

135 DITCH 45

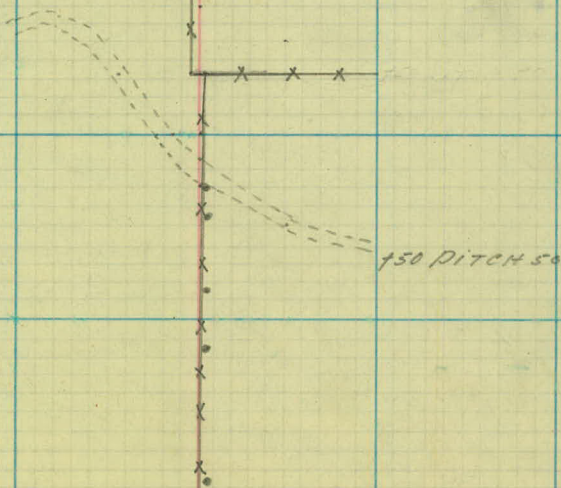
133 F3

F. ϕ

F1

CULTIVATED

CULTIVATED



23

22

21

20

19

18

17

2-5-29

F1

X

X

X

F.2

X

X

X

F.25

X

X

X

F.25

X

X

X

F.3

X

X

X

F.3

X

X

X

X

CULTIVATED

CULTIVATED

27

26

25

24

23

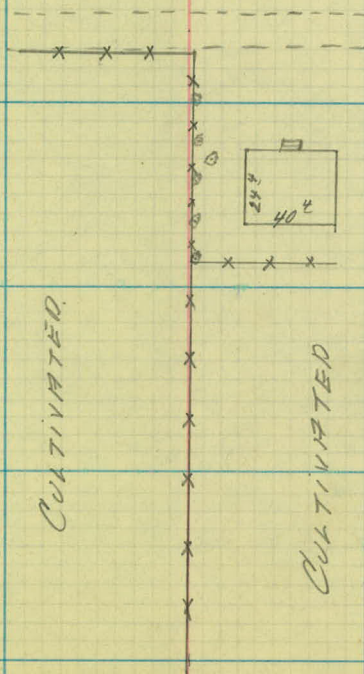
2-5-29

F. 2

F. 1

CULTIVATED

CULTIVATED

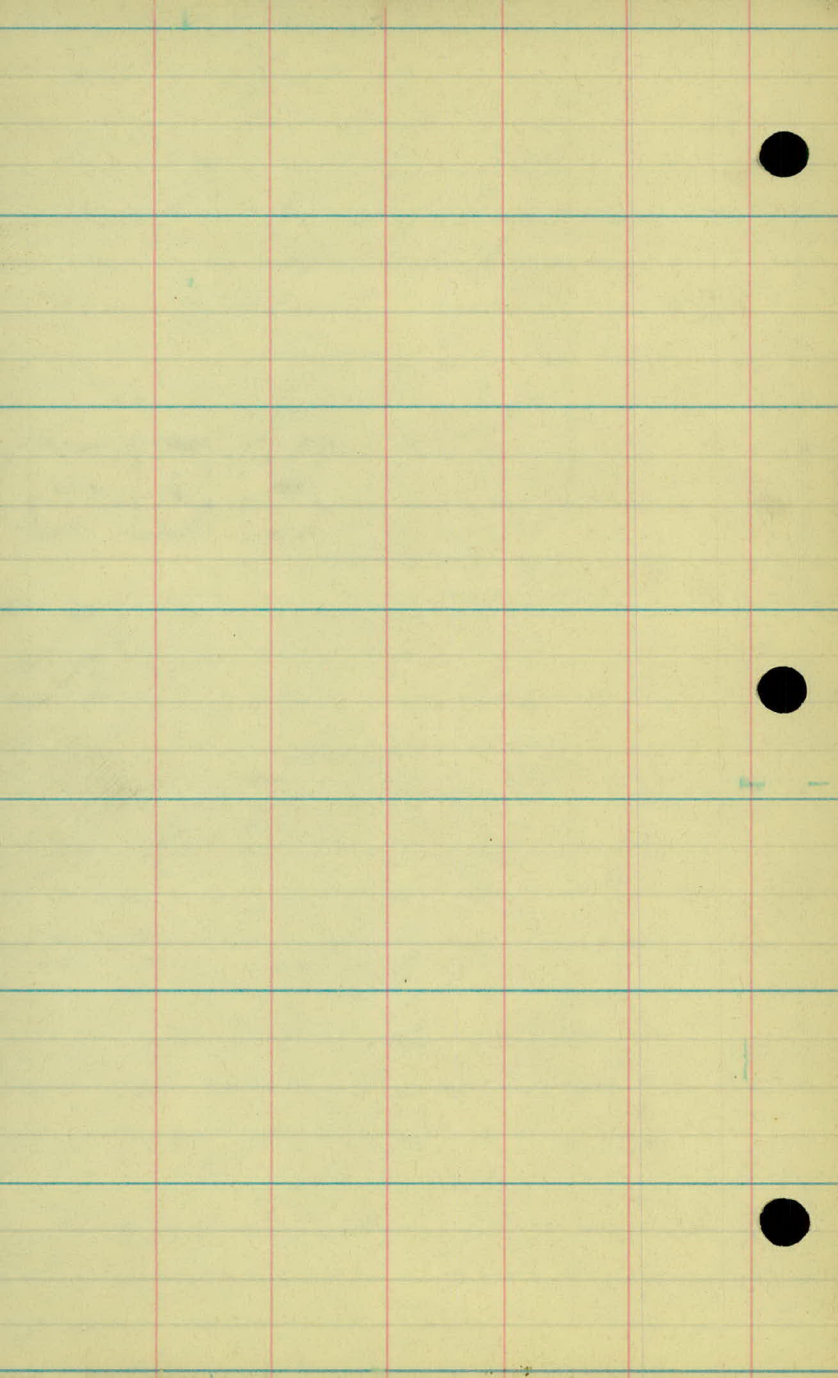


128 F. COR 1

194 PUMP 21
176 SANITARY HOUSE 34

135 SCHOOL HOUSE 34

113 X F.



X

CHECK LEVELS.

MOUNDS VIEW TWP ROAD.

B.M.	11.19	885.36		874.17
B.M.	13.76	896.25	2.87	882.49
	12.16	907.11	1.30	894.95
B.M.			1.48	905.63
	0.04	897.13	10.02	897.09
	10.04	898.15	7.02	888.11
	7.84	902.95	3.04	895.11
B.M.			4.40	898.55

B.M.

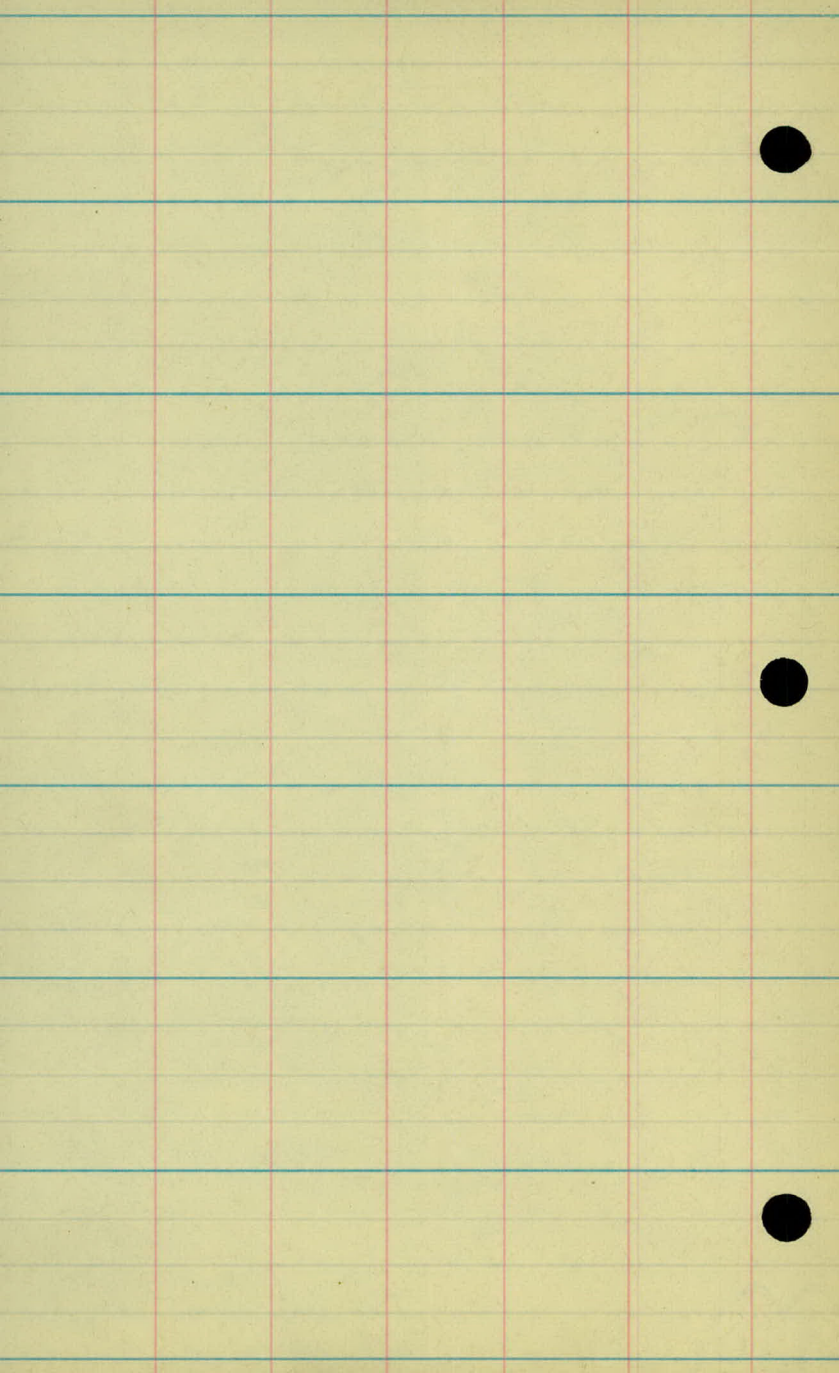
882.49

Spk. in 10' Birch. To Lt. Sta 436+70 on S.T.H. No. 62

ON BRASS MONT.

SPK IN 8" OAK 100 FT STA 8+75.

N. E. COR OF BOTTOM STEP OF SCHOOL HOUSE.



CENTER LINE LEVELS AND
X SECTIONS.

MOUNDS VIEW TWP. ROAD.

B.M.	4.70	887.19		882.49	
0+00					82.49
0+13	BOTTOM OF CURB		4.58		82.61
0+13 ⁵	TOP OF CURB				82.39
0+21					82.29
		84.2 ✓			
	7.09	883.94	10.34	876.85	
0+40					72.54
0+62					71.54 70.14
0+81					71.54
0+94					80.74
1+00					81.34
1+50					81.14
2+00					
	12.20	894.79 ✓	1.35	882.59 ✓	
1+00		81.2			
1+50					
2+00					84.79

ON BRASS MONT.

$\frac{560}{200}$ $\frac{560}{150}$ $\frac{545}{100}$ $\frac{516}{50}$ 4.70 $\frac{4.10}{50}$ $\frac{3.18}{100}$ $\frac{2.19}{150}$ $\frac{1.27}{200}$

$\frac{491}{33}$ 4.80 $\frac{4.25}{33}$

$\frac{54}{33}$ 4.9 $\frac{4.6}{33}$

$\frac{10.1}{33}$ $\frac{11.2}{20}$ 11.4 $\frac{11.9}{20}$ $\frac{11.9}{33}$

$\frac{14.0}{33}$ 12.4 $\frac{13.8}{33}$ $\rightarrow$ TOP OF ICE

$\frac{14.0}{33}$ 12.4 $\frac{1.7}{28}$ $\frac{1.7}{32}$

$\frac{14.0}{33}$ $\frac{12.4}{30}$ 3.2 $\frac{0.6}{25}$ $\frac{0.6}{33}$

$\frac{8.0}{33}$ $\frac{5.0}{17}$ 2.6

$\frac{8.2}{33}$ $\frac{5.8}{12}$ 2.8

$\frac{6.4}{33}$ $\frac{3.4}{19}$ $\frac{1.4}{10}$ (+0.9)

(13.4) $\frac{11.8}{15}$ $\frac{7.5}{33}$

(13.6) $\frac{8.5}{16}$ $\frac{7.5}{33}$

10.0 $\frac{5.8}{14}$ $\frac{5.0}{33}$

894.79

+50

92.19

5.21 899.13 0.87 893.92

3+00

93.53

+60

95.33

4+00

95.63

+50

95.43

5+00

94.03

+35

93.53

6+00

95.63

8.59 903.50 2.22 896.91
95.6
9.9

6+00

+50

97.30

7+00

99.60

+50

01.40

8+00

00.5

$$\begin{array}{r} 7.7 \\ 33 \end{array} \quad \begin{array}{r} 5.5 \\ 19 \end{array} \quad 2.6 \quad \begin{array}{r} 1.6 \\ 11 \end{array} \quad \begin{array}{r} 2.5 \\ 33 \end{array}$$

$$\begin{array}{r} 7.3 \\ 33 \end{array} \quad \begin{array}{r} 6.7 \\ 22 \end{array} \quad 5.6 \quad \begin{array}{r} 5.4 \\ 8 \end{array} \quad \begin{array}{r} 4.6 \\ 11 \end{array} \quad 3.8$$

$$\begin{array}{r} 4.8 \\ 33 \end{array} \quad \begin{array}{r} 4.5 \\ 16 \end{array} \quad 3.8 \quad \begin{array}{r} 3.7 \\ 7 \end{array} \quad \begin{array}{r} 3.2 \\ 12 \end{array} \quad 3.5$$

$$\begin{array}{r} 4.6 \\ 33 \end{array} \quad \begin{array}{r} 4.2 \\ 17 \end{array} \quad 3.5 \quad \begin{array}{r} 2.7 \\ 11 \end{array} \quad \begin{array}{r} 3.3 \\ 15 \end{array} \quad 3.8$$

$$\begin{array}{r} 6.8 \\ 33 \end{array} \quad \begin{array}{r} 5.1 \\ 15 \end{array} \quad 3.7 \quad \begin{array}{r} 3.9 \\ 7 \end{array} \quad \begin{array}{r} 3.2 \\ 10 \end{array} \quad \begin{array}{r} 3.7 \\ 15 \end{array} \quad 4.0$$

$$\begin{array}{r} 11.3 \\ 33 \end{array} \quad \begin{array}{r} 8.8 \\ 24 \end{array} \quad \begin{array}{r} 7.3 \\ 16 \end{array} \quad 5.1 \quad \begin{array}{r} 5.0 \\ 9 \end{array} \quad \begin{array}{r} 4.1 \\ 13 \end{array} \quad \begin{array}{r} 4.7 \\ 20 \end{array} \quad 4.7$$

$$\begin{array}{r} 12.7 \\ 33 \end{array} \quad \begin{array}{r} 11.8 \\ 30 \end{array} \quad \begin{array}{r} 9.9 \\ 24 \end{array} \quad \begin{array}{r} 7.4 \\ 15 \end{array} \quad 5.6 \quad \begin{array}{r} 5.1 \\ 10 \end{array} \quad \begin{array}{r} 4.2 \\ 16 \end{array} \quad \begin{array}{r} 4.8 \\ 21 \end{array} \quad 4.8$$

$$\begin{array}{r} 6.6 \\ 33 \end{array} \quad \begin{array}{r} 6.0 \\ 29 \end{array} \quad \begin{array}{r} 4.8 \\ 15 \end{array} \quad 3.5$$

(9.9)

$$\begin{array}{r} 7.5 \\ 8 \end{array} \quad \begin{array}{r} 8.8 \\ 15 \end{array} \quad \begin{array}{r} 7.3 \\ 22 \end{array} \quad 9.3$$

$$\begin{array}{r} 10.5 \\ 33 \end{array} \quad \begin{array}{r} 9.1 \\ 16 \end{array} \quad 8.2 \quad \begin{array}{r} 7.7 \\ 8 \end{array} \quad \begin{array}{r} 7.0 \\ 15 \end{array} \quad \begin{array}{r} 7.4 \\ 21 \end{array} \quad 7.8$$

$$\begin{array}{r} 8.1 \\ 33 \end{array} \quad \begin{array}{r} 7.1 \\ 15 \end{array} \quad 5.9 \quad \begin{array}{r} 5.8 \\ 8 \end{array} \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad \begin{array}{r} 6.0 \\ 21 \end{array} \quad 6.2$$

$$\begin{array}{r} 6.3 \\ 33 \end{array} \quad \begin{array}{r} 5.5 \\ 19 \end{array} \quad 4.1 \quad \begin{array}{r} 4.4 \\ 7 \end{array} \quad \begin{array}{r} 3.9 \\ 15 \end{array} \quad \begin{array}{r} 4.3 \\ 14 \end{array} \quad 4.9$$

$$\begin{array}{r} 5.9 \\ 33 \end{array} \quad \begin{array}{r} 5.6 \\ 17 \end{array} \quad 5.0 \quad \begin{array}{r} 4.8 \\ 10 \end{array} \quad \begin{array}{r} 3.6 \\ 15 \end{array} \quad \begin{array}{r} 4.3 \\ 20 \end{array} \quad 3.9$$

905.50

+50

01.8

9 + 00

03.0

4.30 907.08 2.72 902.78

+50

01.98

B.M. 1.47 907.10 1.47 905.61 905.63

10 + 00

99.2

+50

94.9

0.08 875.44 11.74 875.36

11 + 00

90.04

+50

87.74

12 + 00

86.54

+50

86.44

+70

9.4

86.04

+73

12.0

83.44

+77 CENTER OF DITCH

14.7

80.74

+82

12.0

83.44

+86

9.7

85.74

5.70 893.80 7.34 888.10

13 + 00

86.4

<u>43</u>	<u>42</u>		<u>3.7</u>	<u>2.6</u>	<u>2.9</u>	<u>2.8</u>
33	20	3.7	11	17	24	33

$$\begin{array}{r} 3.7 \\ \hline 39 \end{array} \quad \begin{array}{r} 3.1 \\ \hline 15 \end{array} \quad 2.5 \quad \begin{array}{r} 2.6 \\ \hline 9 \end{array} \quad \begin{array}{r} 2.1 \\ \hline 13 \end{array} \quad \begin{array}{r} 2.0 \\ \hline 39 \end{array}$$

6.7 6.0 5.2 3.8
33 17 31 9 33

$\frac{9.6}{33}$	$\frac{9.5}{19}$	7.9	$\frac{7.4}{21}$	$\frac{6.7}{33}$
------------------	------------------	-------	------------------	------------------

$\frac{13.5}{33}$	$\frac{13.4}{17}$	12.2	$\frac{11.9}{20}$	$\frac{11.4}{33}$
-------------------	-------------------	--------	-------------------	-------------------

$$\begin{array}{r} 60 \\ 33 \overline{) 198} \\ \underline{99} \\ 99 \\ \underline{99} \\ 0 \end{array}$$

$\frac{7.4}{33}$	$\frac{8.3}{20}$	7.7	$\frac{7.2}{7}$	$\frac{7.7}{11}$	$\frac{7.7}{20}$	$\frac{7.7}{35}$
------------------	------------------	-----	-----------------	------------------	------------------	------------------

$$\begin{array}{r} 8.4 \\ 33 \end{array} \quad \begin{array}{r} 8.9 \\ 17 \end{array} \quad 89 \quad \begin{array}{r} 8.7 \\ 6 \end{array} \quad \begin{array}{r} 9.5 \\ 10 \end{array} \quad \begin{array}{r} 8.9 \\ 33 \end{array}$$

<u>8.5</u>	<u>9.1</u>	<u>9.7</u>	<u>9.0</u>	<u>12.2</u>
33	17	13	41	50

→ BOTTOM OF DITCH

D. Tech							
7.2	7.0	8.6	11.6	8.6	7.4	7.1	
33	28	24	22	17	74	17	33

893.80

13+50

87.5

14+00

87.3

+50

87.3

15+00

88.2

+50

89.7

16+00

90.2

+50

89.4

17+00

90.1

+50

91.6

5.42 898.30 ✓ 0.72 892.88 ✓

18+00

92.8

+50

94.1

19+00

93.6

+50

91.7

$$\frac{8.0}{33} \quad \frac{8.0}{24} \quad 4.3 \quad \frac{6.6}{11} \quad \frac{5.4}{33}$$

$$\frac{7.7}{33} \quad \frac{6.9}{21} \quad 6.5 \quad \frac{6.2}{17} \quad \frac{5.7}{33}$$

$$\frac{7.3}{33} \quad \frac{7.1}{21} \quad 6.5 \quad \frac{6.4}{29} \quad \frac{6.1}{33}$$

$$\frac{6.2}{33} \quad \frac{5.7}{19} \quad 5.6 \quad \frac{5.6}{17} \quad \frac{5.4}{33}$$

$$\frac{4.7}{33} \quad \frac{4.4}{21} \quad 4.1 \quad \frac{4.4}{17} \quad \frac{4.5}{33}$$

$$\frac{4.2}{33} \quad \frac{3.9}{21} \quad 3.6 \quad \frac{3.8}{14} \quad \frac{3.7}{33}$$

$$\frac{4.3}{33} \quad \frac{4.7}{23} \quad 4.4 \quad \frac{3.9}{20} \quad \frac{3.6}{33}$$

$$\frac{4.3}{33} \quad \frac{4.4}{17} \quad 3.7 \quad \frac{3.3}{16} \quad \frac{2.6}{33}$$

$$\frac{2.2}{33} \quad \frac{2.2}{20} \quad 2.2 \quad \frac{2.2}{19} \quad \frac{1.8}{33}$$

$$\frac{5.3}{33} \quad \frac{5.5}{20} \quad 5.5 \quad \frac{5.7}{22} \quad \frac{5.7}{33}$$

$$\frac{5.8}{33} \quad \frac{5.1}{20} \quad 4.2 \quad \frac{4.5}{20} \quad \frac{4.9}{33}$$

$$\frac{7.2}{33} \quad \frac{5.8}{15} \quad 4.7 \quad \frac{4.7}{20} \quad \frac{4.5}{33}$$

$$\frac{7.9}{33} \quad \frac{7.1}{16} \quad 6.4 \quad \frac{6.0}{17} \quad \frac{6.1}{33}$$

898.30

20+00

91.8

+50

93.2

21+00

93.6

+50

93.3

22+00

93.5

+50

93.3

23+00

93.5

+50

95.2

6.17 902.91 1.50 896.80

24+00

97.07

+50

97.87

25+00

98.57

+50

99.37

26+00

98.97

$$\frac{7.8}{33} \quad \frac{7.2}{18} \quad 6.5 \quad \frac{6.5}{24} \quad \frac{5.9}{33}$$

$$\frac{6.6}{33} \quad \frac{5.6}{21} \quad 5.1 \quad \frac{5.7}{21} \quad \frac{6.0}{33}$$

$$\frac{5.2}{33} \quad \frac{4.5}{15} \quad 4.7 \quad \frac{5.3}{18} \quad \frac{5.6}{33}$$

$$\frac{5.7}{33} \quad \frac{5.3}{20} \quad 5.0 \quad \frac{5.5}{20} \quad \frac{5.4}{33}$$

$$\frac{6.2}{33} \quad \frac{5.5}{15} \quad 4.8 \quad \frac{4.8}{18} \quad \frac{5.0}{33}$$

$$\frac{6.7}{33} \quad \frac{5.8}{15} \quad 5.0 \quad \frac{4.7}{27} \quad \frac{4.5}{33}$$

$$\frac{6.1}{33} \quad \frac{5.6}{15} \quad 4.8 \quad \frac{5.1}{20} \quad \frac{4.7}{33}$$

$$\frac{4.5}{33} \quad \frac{3.7}{10} \quad 3.1 \quad \frac{3.8}{20} \quad \frac{4.1}{33}$$

$$\frac{7.2}{33} \quad \frac{6.4}{10} \quad 5.9 \quad \frac{6.4}{11} \quad \frac{7.0}{33}$$

$$\frac{6.1}{33} \quad \frac{5.8}{13} \quad 5.1 \quad \frac{6.0}{16} \quad \frac{6.3}{33}$$

$$\frac{5.2}{33} \quad \frac{4.8}{11} \quad 4.4 \quad \frac{5.6}{20} \quad \frac{5.5}{33}$$

$$\frac{4.3}{33} \quad \frac{3.8}{10} \quad 3.6 \quad \frac{5.1}{6} \quad \frac{4.6}{17} \quad \frac{4.6}{33}$$

$$\frac{5.1}{33} \quad \frac{4.7}{20} \quad 4.0 \quad \frac{5.4}{9} \quad \frac{4.9}{24} \quad \frac{5.4}{33}$$

902.97

+28

96.57

+41⁵

B.M.

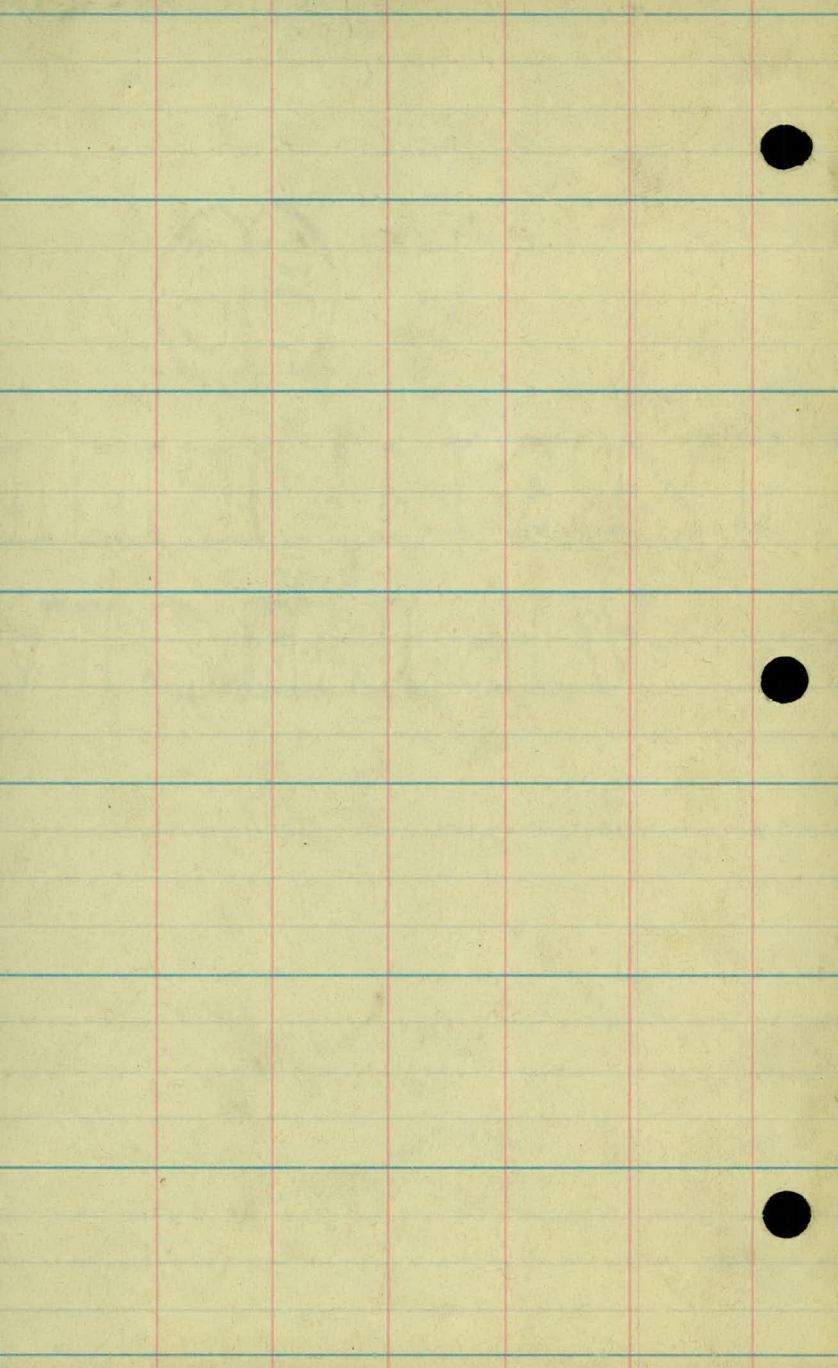
97.07

4.43 ✓ 998.54 898.55

2-6-29

$\frac{6.3}{33}$	$\frac{6.7}{22}$	6.4	$\frac{6.0}{24}$	$\frac{5.7}{33}$
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$\frac{7.4}{200}$	$\frac{8.5}{150}$	$\frac{7.4}{100}$	$\frac{6.5}{50}$	$\frac{6.2}{33}$	5.9	$\frac{5.5}{33}$	$\frac{5.3}{50}$	$\frac{5.0}{100}$	$\frac{4.6}{150}$	$\frac{3.6}{200}$
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Co Rd "H"

for Culvert near Pleasant
View Drive

Sta	+	x	-	Elev
BM	0.14	896.27		(896.13)
TP	2.20	885.73	12.74	883.53
BM			6.06	879.67 (879.65)
T.P.	11.65	894.96	2.42	883.31
BM			10.04	892.33
BM			2.68	892.28 892.33
BM			0.87	(894.09)
BM	0.32	879.97		(879.65)
S. End Culvert			12.97	867.00
N. End Culvert			11.40	868.57
7 Garage			2.22	877.75
7			2.0	878.0
+50			4.1	875.9
8			5.5	874.5
+50			5.5	874.5
9			3.8	876.2

Top E. End door Sill Front House NW Cor

MH Knollwood Drive & Co Rd H

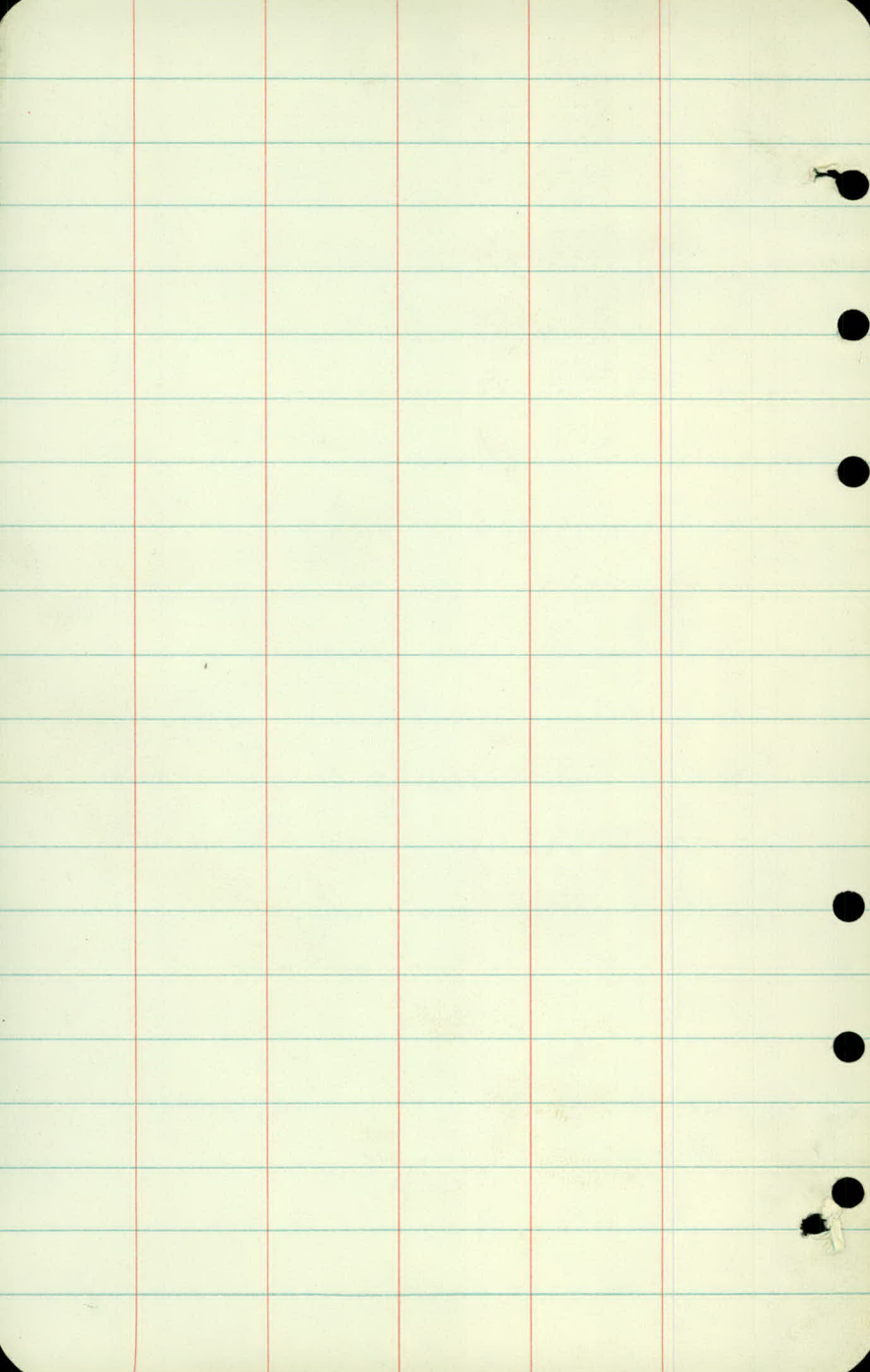
Top Hyd Sta 9+25[±] N. Side H

Top E. End door Sill

Top E. End door Sill

Top Hyd NE Cor Pleasant View Drive & "H"

Top Hyd Sta 9+25[±] N. Side H



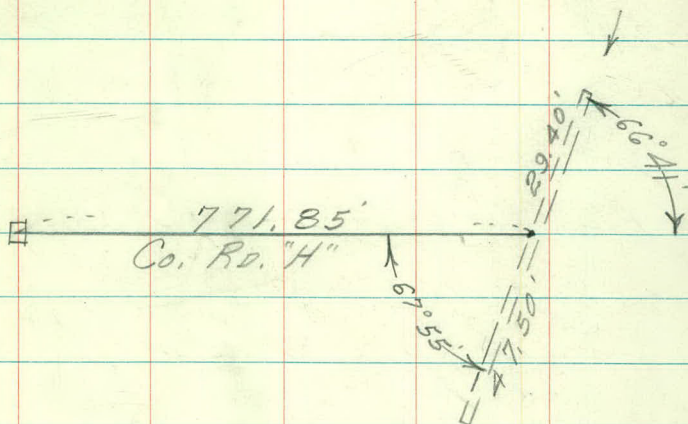
Dec. 20, 1968

1

Culvert Elevation

Co Rd "H"

Near West County Line



Culvert = 36" SCP ↓

Length = 76.90'

Elevation on next page

Sta + Δ - Elev.

BM 3.08 902.04 898.96

BM 3.00 902.63 2.41 899.63 898.06

BM 2.81 896.49 8.95 893.68

BM 1.05 884.07 13.47 883.02

Top S. End culvert 15.34

Top N. End culvert 12.33

BM 12.60 895.48 1.19 882.88

BM 9.00 902.69 1.79 893.69

BM 2.57 902.20 3.06 899.63

BM 3.23 898.97

BM 4.15 898.05

BM 3.09 899.11

Dec. 20, 1968

2

FK WS GA CM
H
T
+
H

Top Hyd. S. W. Corner Silver Lake Rd & "H"

Top Hyd. by Ho #2001 W. Co Rd "H"

Top Hyd S.E. Corner Knollwood Dr. & "H"

Top Hyd by Ho #1850 W. Co. Rd. "H"

Top Hyd N. Side Co Rd "H" from Ho #1850

Top Hyd. S. E. Corner Knollwood Dr & "H"

Top Hyd By Ho #2001 W. Co Rd "H"

Top Hyd S.W. Corner Silver Lake Rd & H

R.R. Spike in PP S.W. Corner " " " " "

Top Hyd N.W. Corner " " " " "

