

B-19 D11A Dr. 11A - Bk. 19

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

GROVELAND STREET

From So. Line Sec 6-³⁰⁻²³ To Co. Rd. "J"

Road Acc't. No. M-45

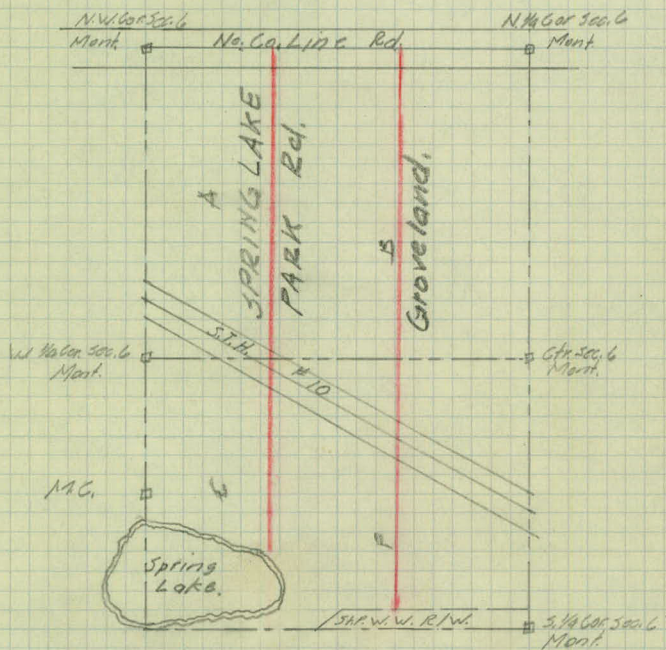
Date Filed 12-23-38

File

M.V. Twp.

PLAN SURVEY

AUD. SUB. #89



INDEX

Wm. C. Coker.
June 28, 1938



Alignment
Groveland St. -

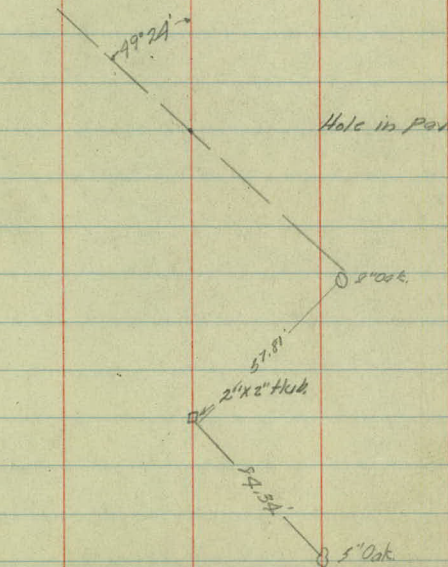
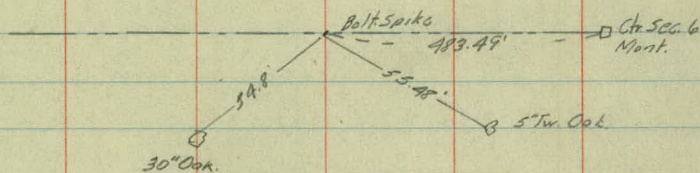
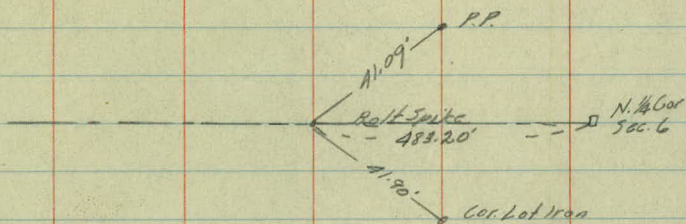
Sta	Point	ΔL	ΔR
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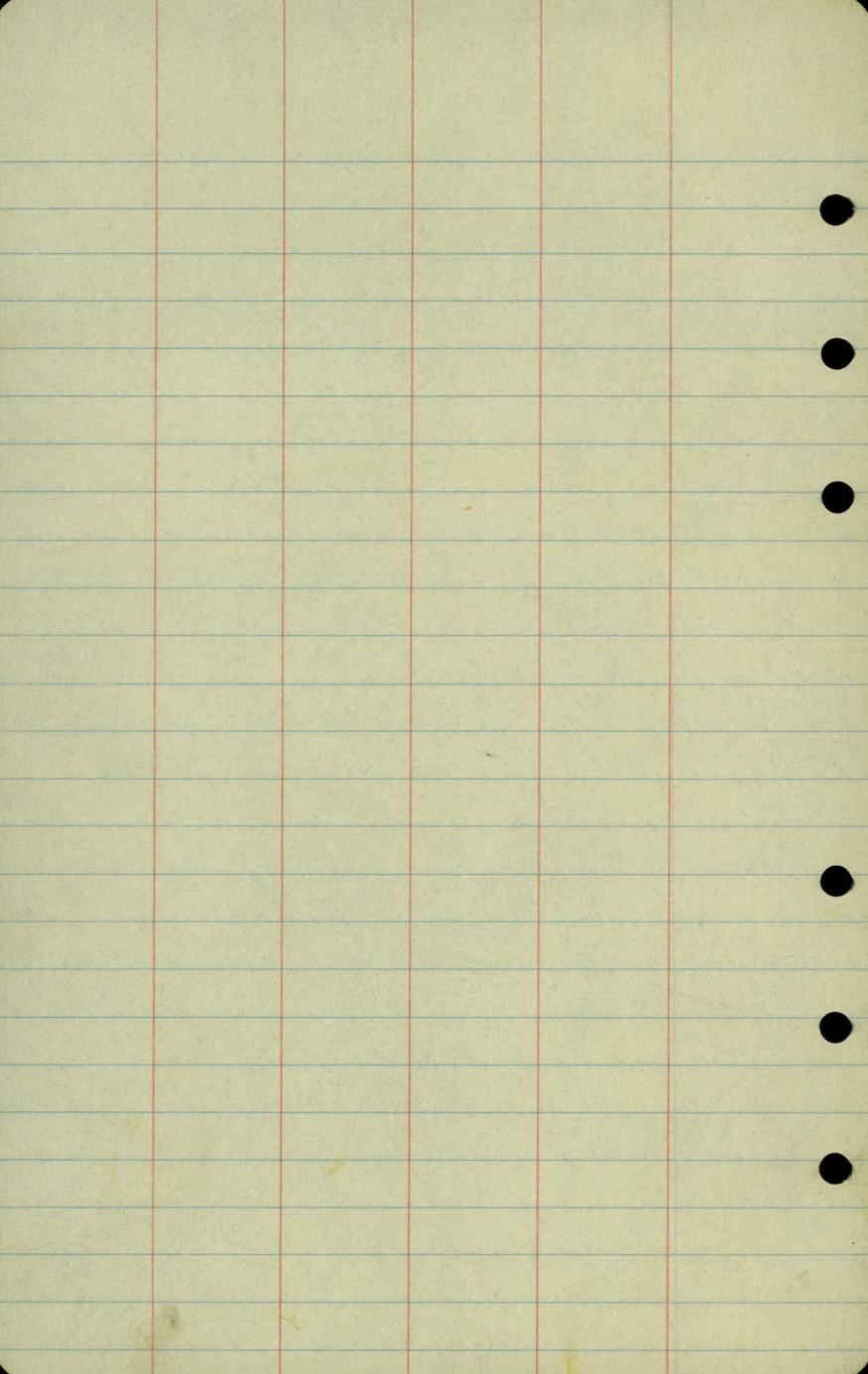
60	+19.2	Co. Rd. "J"	
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25	+86.52		
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15	+38.63	P.O.T. = R. U.S. Highway #10	
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0	+0.0		
---	------	--	--





Topography

5

4

3

2

1

0100

+78-G.P.-20'

+71-PP-26'

+19-6"Oak-9'
Woods-35

+32-PP-20'

+02-Em
+07-5" W. Cor. Ho. - 158'

+79-Woods-15

+81-PP-20'

+33-PP-20'
+24-Woods-18'

+92-Woods-18

+53-0"Oak-55'

+22-6"Oak-24'

+50-Bog Turnpike-1'-24'

Scrub Oaks

Scrub Oaks

Scrub Oaks

x x x x x x x +98 Woods 18'

+34 Fc.

12

11

10

9

8

7

6

+70 End Cult. - 26'

+60-P.P. - 20'

K.P.
L.C.
R.P.

17'

5

10'

Cult

+18-6" Oak - 21'

17'

+57-End Woods - 32'

32'

+11-End Woods - 28'
Beg Cult. - 27'

+89-P.P. - 20'

Woods 20'

15'

32'

Scrub Oaks

Woods 20'

15'

+19-P.P. - 20'

+88-Beg Woods - 29'

+57-Cult - 27'

Scrub Oaks

Woods 27'
+70-End
+80-Ho. - 250'

15'

Cult

+50-P.P. - 20'

+25-Cult - 27'

+11-Woods - 31'

Woods - 19'

15'

+85-End

Woods - 20'

15'

+36-S. W. Cor. Ho. - 222'

Woods - 9-35

24'

19

18

17

16

15

14

13

+10-6" Oak - 20'

SW Cor. Ho. 115
+99-6" Oak - 18'



+96-Ent.

+85-4" Oak - 12'

+104-8" Oak - 9'

+130-4" Oak - 12'

+150-4" Oak - 20'

+185-16" Oak Ho. 95'

+157-Ent.



Scrub Oaks

Cult.

+150-8" Oak - 25'
+147-PP - 24'
+151-Ent Cult - 58'

+140-8" Oak Cult - 38'
+128-4" Oak - 28'

+102-PP - 26'

+146-8" Oak - 38'
+110-3" Oak Ho. - 105'
+120-Ent.

+199-6" Oak - 37'
+180-PP - 27'

+131-PP - 19'

26

25

24

23

22

21

20

14'

6'

10'

Scrub
Oak 5

+84 Woods - 15'

+86 P.R.

+90 - 26' Oak - 27'

0

5'

12'

+90 - 5' Oak - 16'

2'

14'

+98 - 6' Tw Oak - 18'

+99 - 6' Oak - 17'

2'

14'

+85 Ent

+63 - 4' Oak 15'
+95 Cult. - 14'

0

+88 - 6' Oak - 28'

+92 Scrub Oak Wa. 18'

+72 Ent.

+99 - P.R. 29'

Cult.

1'

15'

Scrub Oak 5

+99 Cult. 10'

+95 - P.P. - 21'

32'

30'

33

32

31

30

29

28

27

Cult.

+35-Ent.

+80-Bog Cult. 27'

+58-Woods-15'

Scrub Oaks

Scrub Oaks

+28-Ent.

Scrub Oaks

Scrub Oaks

38'

24'

24'

24'

21'

19'

17'

3'

13'

3'

19'

1'

15'

1'

16'

4'

14'

5'

13'

7'

9'

11'

25'-10'

13'

15'

13'

40

39

38

37

36

35

34

Cult.

5'

12'

3'

12'

3'

13'

3'

12'

Meadow

+96-Ent.

+88-P.R.-21'

+56-Ent.

4'

13'

Cult.

3'

14'

+10-Ent.

3'

13'

45

47

46

45

44

43

42

41

+186-Ent.

14'

6'

11'

50

Scrub Oaks

14'

7'

11'

Scrub Oaks

17'

6'

10'

+180-Ent.

15'

17'

5'

11'

20

+123-Ent.

Scrub Oaks

4'

12'

Scrub Oaks

12'

4'

13'

19'

+97-Cult-28'

Cult.

3'

12'

54

53

52

51

50

49

48

+85-Ent
+70-End Cult-25

Cult

6'

13'

6'

13'

6'

12'

+70-Cult-25

+65-Cult-27'

6'

11'

Ent

6'

14'

Cult

+60-Woods-35'

23'

5'

13'

+08-Cult-28'

57

60

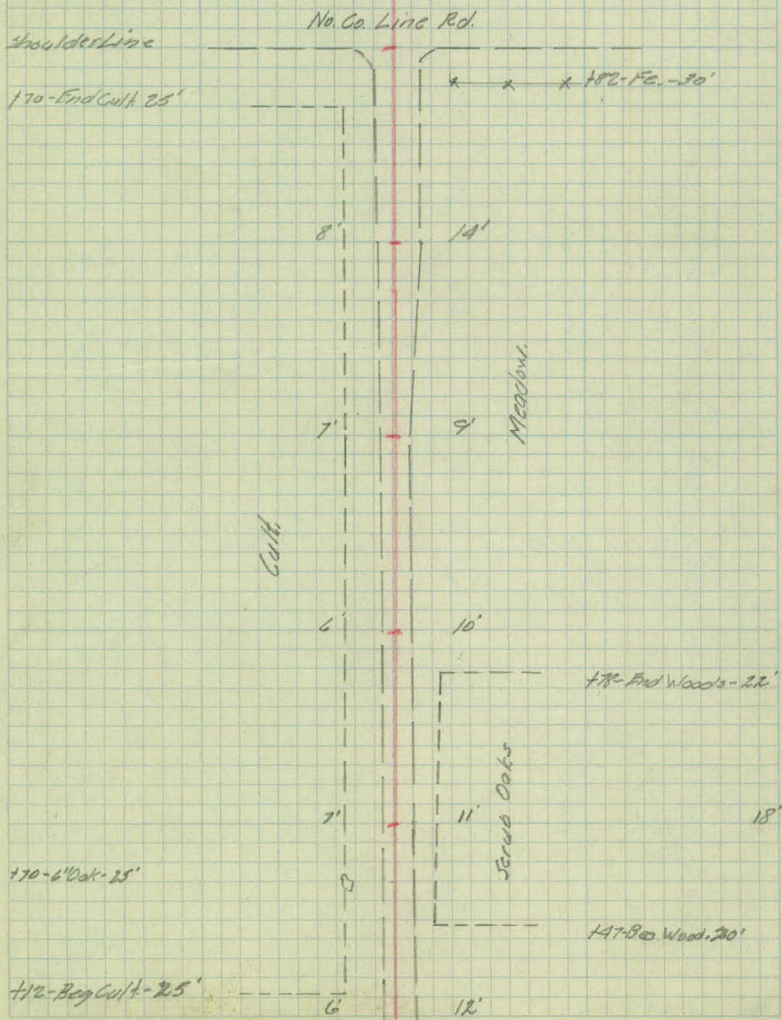
59

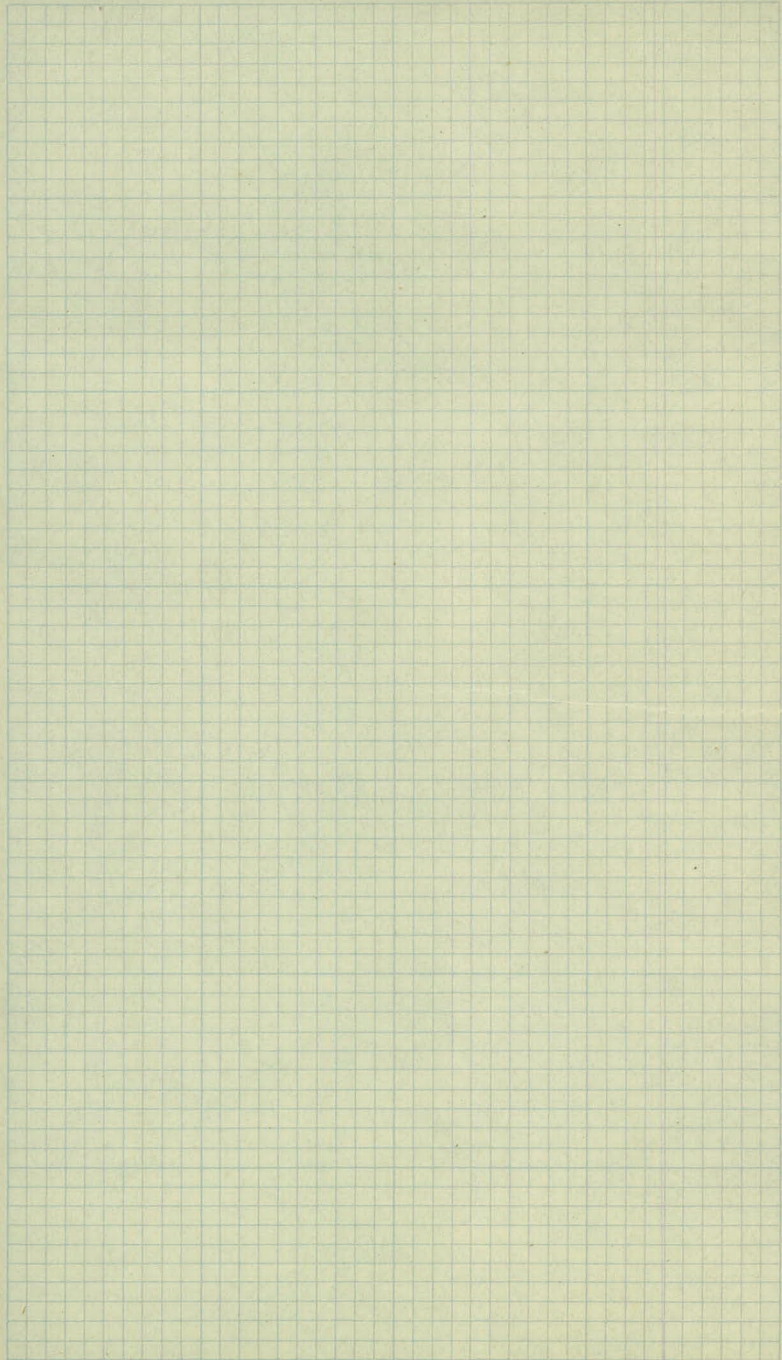
58

57

56

55





Bench Levels

Sta.	+	-	-	Elev.
B.M.	7.37	917.96		910.63
B.M.			5.04	912.92
B.M.	8.39	916.54	4.81	913.15
T.P.	7.80	918.72	5.62	912.96
B.M.			4.80	913.92
T.P.	5.23	917.95	4.00	914.72
T.P.	3.49	916.57	6.87	913.08
T.P.	11.03	918.96	8.64	907.93
B.M.			2.61	916.35
T.P.	8.18	923.02	4.12	914.84
T.P.	4.15	921.91	5.26	917.76
T.P.	2.77	914.09	10.59	911.32
B.M.			5.70	908.89
T.P.	6.20	912.10	7.19	906.90
T.P.	8.22	918.40	2.92	910.18
B.M.	4.75	916.58	6.57	911.83
T.P.	4.08	915.65	5.01	911.57
T.P.	7.11	917.74	5.82	910.63
B.M.			4.67	913.17
T.P.	5.86	920.46	3.14	914.60
B.M.	1.73	916.26	5.93	914.53
T.P.	2.61	913.22	5.65	910.61
T.P.	11.62	917.27	7.57	905.65
B.M.			2.95	914.32
T.P.	0.63	913.70	4.20	913.07

Top Mont. N.W. Cor. Sec. 6

Spt. in 12" Oak 50' Lt. 24+83 N. Co. Line Sta.

Spt. in P.P. N.E. Cor. "J"

Spt. in P.P. End. 22' Lt. 42+82

Spt. in 6" Tw. Oak 3 W. Cor. 60' Lt. 18+70

Spt. in 18" Oak. 24' Lt. Sta. 2134

Spt. in P.P. 75' Lt. Sta. 1124

Top & Pav.

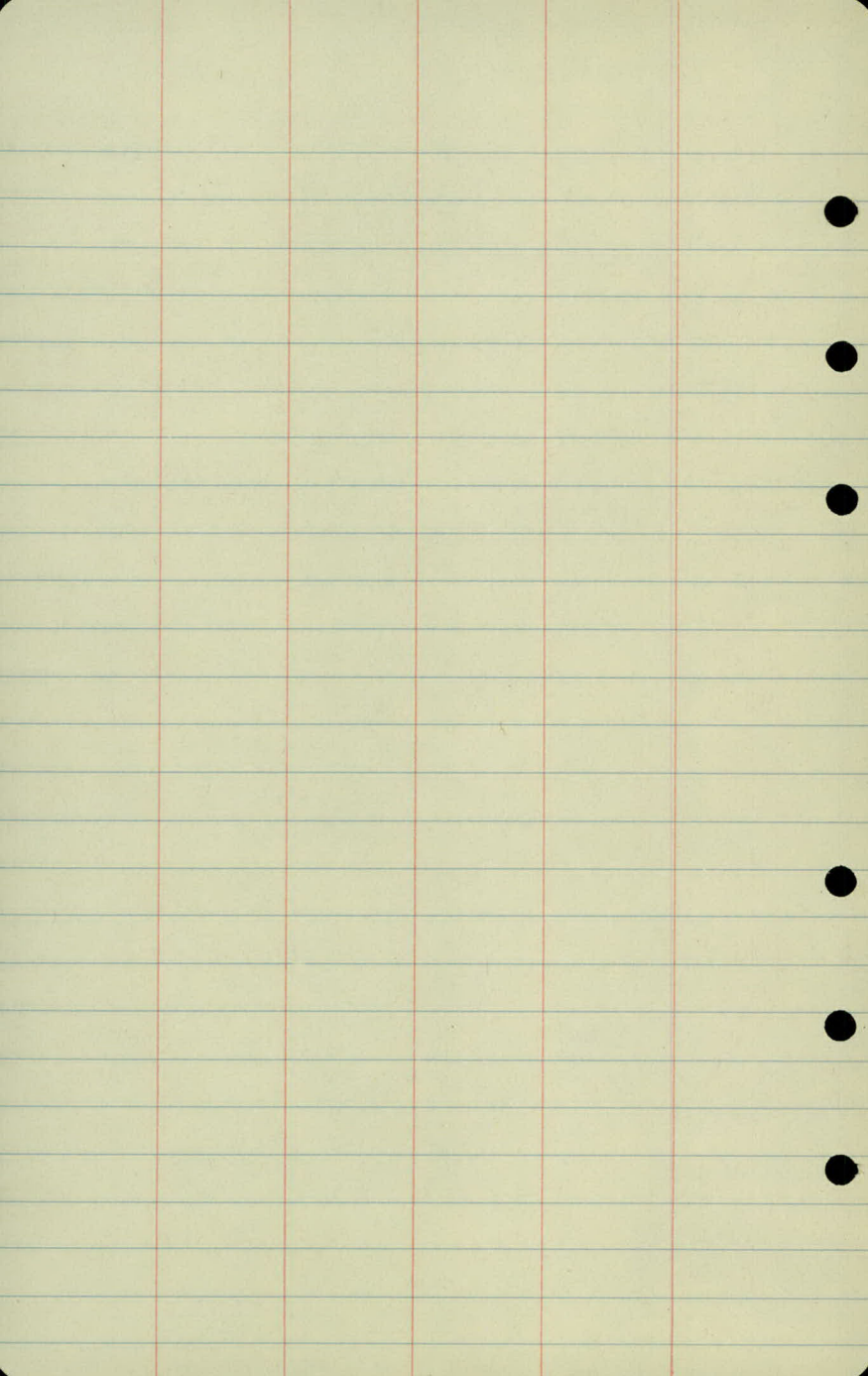
Spt. in 24" Oak 26' Lt. Sta. 25+38

Spt. in 8" Oak 50' Lt. Sta. 42+40

Sta.	+	Σ	-	Elev.
		913.70 ✓		
T.P.	8.51	915.93 ✓	6.28	907.42 ✓
B.M.	4.96	915.66 ✓	5.23	910.70 ✓
B.M.				913.20
				(913.15)

3pk in P.P. M.F. Co Rd. "J" +

3pk in P.P. N.E. Cor.



X sections

Sta	+	Σ	-	Elev.
B.M.	5.31	917.14		911.83

0	+0.0			913.3
---	------	--	--	-------

	+5.0			12.1
--	------	--	--	------

1				11.8
---	--	--	--	------

	+5.0			11.1
--	------	--	--	------

2				11.6
---	--	--	--	------

	+5.0			12.8
--	------	--	--	------

3				12.6
---	--	--	--	------

	+5.0			11.5
--	------	--	--	------

4				10.0
---	--	--	--	------

	+5.0			09.0
--	------	--	--	------

5				09.8
---	--	--	--	------

Lt

L

Rt

Spk in P.P. 75' Lt 1424

$\frac{29}{50}$

$\frac{35}{50}$

$\frac{49}{50}$

$\frac{38}{50}$

$\frac{44}{15}$

$\frac{50}{25}$

$\frac{60}{25}$

$\frac{68}{50}$

$\frac{49}{50}$ $\frac{49}{23}$ $\frac{55}{22}$

$\frac{49}{13}$

$\frac{59}{3}$

$\frac{53}{25}$

$\frac{57}{25}$

$\frac{66}{50}$

$\frac{54}{50}$

$\frac{58}{20}$

$\frac{58}{19}$

$\frac{51}{16}$

$\frac{60}{1}$

$\frac{56}{25}$

$\frac{58}{25}$

$\frac{59}{50}$

$\frac{54}{50}$

$\frac{48}{20}$

$\frac{52}{19}$

$\frac{47}{9}$

$\frac{58}{2}$

$\frac{56}{3}$

$\frac{50}{25}$

$\frac{52}{25}$

$\frac{52}{50}$

$\frac{36}{50}$

$\frac{38}{18}$

$\frac{44}{17}$

$\frac{38}{8}$

$\frac{43}{4}$

$\frac{45}{5}$

$\frac{43}{25}$

$\frac{46}{25}$

$\frac{48}{50}$

$\frac{39}{50}$

$\frac{43}{17}$

$\frac{49}{16}$

$\frac{41}{7}$

$\frac{45}{5}$

$\frac{49}{6}$

$\frac{46}{26}$

$\frac{47}{26}$

$\frac{49}{50}$

$\frac{51}{50}$

$\frac{55}{15}$

$\frac{60}{14}$

$\frac{54}{5}$

$\frac{56}{7}$

$\frac{62}{8}$

$\frac{56}{33}$

$\frac{57}{33}$

$\frac{56}{50}$

$\frac{63}{50}$

$\frac{69}{14}$

$\frac{73}{13}$

$\frac{69}{4}$

$\frac{71}{8}$

$\frac{74}{13}$

$\frac{77}{13}$

$\frac{77}{50}$

$\frac{70}{50}$

$\frac{77}{16}$

$\frac{83}{15}$

$\frac{78}{5}$

$\frac{81}{7}$

$\frac{84}{8}$

$\frac{87}{22}$

$\frac{86}{22}$

$\frac{86}{50}$

$\frac{68}{50}$

$\frac{69}{16}$

$\frac{74}{15}$

$\frac{70}{4}$

$\frac{73}{6}$

$\frac{75}{7}$

$\frac{77}{30}$

$\frac{77}{30}$

$\frac{81}{50}$

Low Point
125'

Sta	+	X	-	Elev.
		912.14		
5	+50			910.3
6				10.7
T.P.	5.10	916.91	5.83	911.31
	+50			11.2
7				11.6
	+50			12.0
8				12.2
	+50			11.7
9				11.4
	+50			11.2
10				10.8
	+50			10.5

Lt

A

Rt

$$\frac{6.7}{50} \quad \frac{6.3}{17} \quad \frac{6.9}{16} \quad \frac{6.3}{6} \quad \frac{6.8}{5} \quad \frac{6.9}{5} \quad \frac{6.5}{6} \quad \frac{7.0}{28} \quad \frac{7.4}{30}$$

$$\frac{6.0}{30} \quad \frac{6.2}{16} \quad \frac{6.7}{15} \quad \frac{6.0}{5} \quad \frac{6.4}{4} \quad \frac{6.8}{4} \quad \frac{6.1}{5} \quad \frac{6.5}{25} \quad \frac{6.9}{50}$$

$$\frac{5.0}{50} \quad \frac{5.1}{15} \quad \frac{5.5}{14} \quad \frac{5.0}{4} \quad \frac{5.2}{6} \quad \frac{5.7}{6} \quad \frac{5.2}{7} \quad \frac{5.7}{27} \quad \frac{5.9}{30}$$

$$\frac{4.7}{50} \quad \frac{4.7}{14} \quad \frac{5.1}{15} \quad \frac{4.7}{4} \quad \frac{4.8}{8} \quad \frac{5.3}{8} \quad \frac{4.8}{9} \quad \frac{5.2}{27} \quad \frac{5.2}{50}$$

$$\frac{4.3}{50} \quad \frac{4.2}{15} \quad \frac{4.5}{14} \quad \frac{4.2}{4} \quad \frac{4.4}{4} \quad \frac{4.8}{7} \quad \frac{4.6}{8} \quad \frac{4.4}{28} \quad \frac{4.4}{50}$$

$$\frac{4.2}{50} \quad \frac{4.2}{14} \quad \frac{4.7}{13} \quad \frac{4.1}{3} \quad \frac{4.2}{7} \quad \frac{4.5}{7} \quad \frac{4.2}{8} \quad \frac{4.1}{50}$$

$$\frac{4.7}{50} \quad \frac{4.4}{15} \quad \frac{5.0}{14} \quad \frac{4.6}{9} \quad \frac{4.7}{4} \quad \frac{5.3}{6} \quad \frac{4.9}{7} \quad \frac{4.8}{32} \quad \frac{4.6}{50}$$

$$\frac{5.3}{50} \quad \frac{5.3}{39} \quad \frac{5.0}{16} \quad \frac{5.5}{18} \quad \frac{4.8}{4} \quad \frac{5.0}{4} \quad \frac{5.2}{6} \quad \frac{4.9}{7} \quad \frac{4.8}{31} \quad \frac{4.7}{50}$$

$$\frac{5.8}{50} \quad \frac{5.2}{16} \quad \frac{5.6}{15} \quad \frac{4.9}{4} \quad \frac{5.2}{4} \quad \frac{5.6}{6} \quad \frac{5.1}{7} \quad \frac{5.1}{50}$$

$$\frac{6.1}{50} \quad \frac{5.6}{14} \quad \frac{5.9}{19} \quad \frac{5.5}{4} \quad \frac{5.6}{4} \quad \frac{5.8}{7} \quad \frac{5.4}{8} \quad \frac{5.6}{27} \quad \frac{5.6}{50}$$

$$\frac{6.3}{50} \quad \frac{6.0}{18} \quad \frac{6.8}{14} \quad \frac{5.7}{5} \quad \frac{5.9}{4} \quad \frac{6.3}{7} \quad \frac{5.8}{8} \quad \frac{5.6}{26} \quad \frac{5.9}{50}$$

Sta + X - Elev.

916.41 ✓

11

910.2

+50

10.0

12

09.5

T.P.

6.10

915.68 ✓

6.83

909.88 ✓

+50

09.2

13

09.2

+50

09.5

14

09.5

+65

10.3

15

11.7

+13

12.8

+21

13.69

12.96

Lt

K

Rt

$$\frac{6.6}{50} \quad \frac{6.1}{17} \quad \frac{6.7}{16} \quad \frac{5.9}{6} \quad \frac{6.2}{5} \quad \frac{6.3}{5} \quad \frac{5.9}{6} \quad \frac{5.7}{27} \quad \frac{5.7}{50}$$

$$\frac{6.9}{50} \quad \frac{6.6}{16} \quad \frac{7.2}{15} \quad \frac{6.2}{5} \quad \frac{6.4}{5} \quad \frac{6.5}{6} \quad \frac{6.1}{7} \quad \frac{5.8}{24} \quad \frac{5.7}{50}$$

$$\frac{7.0}{50} \quad \frac{6.9}{18} \quad \frac{7.4}{17} \quad \frac{6.6}{7} \quad \frac{6.9}{5} \quad \frac{7.2}{4} \quad \frac{6.7}{5} \quad \frac{6.4}{29} \quad \frac{6.2}{50}$$

$$\frac{6.5}{50} \quad \frac{6.3}{19} \quad \frac{6.9}{18} \quad \frac{6.1}{7} \quad \frac{6.5}{5} \quad \frac{6.8}{4} \quad \frac{6.2}{5} \quad \frac{6.2}{25} \quad \frac{6.2}{50}$$

$$\frac{6.2}{50} \quad \frac{6.3}{19} \quad \frac{6.7}{18} \quad \frac{6.0}{6} \quad \frac{6.5}{5} \quad \frac{6.6}{4} \quad \frac{6.1}{5} \quad \frac{6.2}{24} \quad \frac{6.2}{50}$$

$$\frac{6.3}{50} \quad \frac{6.3}{18} \quad \frac{6.7}{17} \quad \frac{6.0}{7} \quad \frac{6.2}{5} \quad \frac{6.5}{4} \quad \frac{6.1}{5} \quad \frac{6.0}{25} \quad \frac{5.8}{50}$$

$$\frac{6.3}{50} \quad \frac{6.2}{22} \quad \frac{6.8}{21} \quad \frac{6.1}{6} \quad \frac{6.2}{5} \quad \frac{6.7}{7} \quad \frac{6.0}{8} \quad \frac{5.9}{26} \quad \frac{5.9}{50}$$

$$\frac{5.4}{50} \quad \frac{5.6}{20} \quad \frac{6.0}{19} \quad \frac{5.2}{4} \quad \frac{5.4}{5} \quad \frac{6.4}{10} \quad \frac{5.5}{11} \quad \frac{5.3}{29} \quad \frac{5.0}{50}$$

$$\frac{5.2}{50} \quad \frac{4.8}{K} \quad \frac{5.4}{17} \quad \frac{4.3}{8} \quad \frac{4.0}{5} \quad \frac{3.5}{10} \quad \frac{3.2}{21} \quad \frac{2.90}{25} \quad \frac{1.44}{50}$$

$$\frac{4.9}{50} \quad \frac{4.7}{18} \quad \frac{4.4}{11} \quad \frac{3.4}{8} \quad \frac{2.9}{5} \quad \frac{2.77}{10}$$

$$\frac{4.7}{50} \quad \frac{4.8}{28} \quad \frac{3.0}{14} \quad \frac{2.72}{5}$$

Sta + π - E/cv

915.68 ✓

15 +38.63

913.14 ✓

B.M.

2.54

913.14 ✓

913.17

+56

13.01

+85

12.3

16

12.2

+19

12.4 ✓

+35

12.9

+70

13.1

17

12.9

+50

12.5

18

12.0

T.P.

2.28

916.19 ✓

1.77

913.91 ✓

+50

11.9

Lt

L

Rt

254

Top to Pav

$$\frac{267}{20} \quad \frac{21}{29} \quad \frac{55}{40} \quad \frac{61}{45} \quad \frac{28}{50}$$

$$\frac{297}{33} \quad \frac{29}{21} \quad \frac{34}{16} \quad \frac{36}{20} \quad \frac{52}{23} \quad \frac{25}{25} \quad \frac{23}{50}$$

$$\frac{238}{49} \quad \frac{25}{39} \quad \frac{47}{28} \quad \frac{48}{13} \quad \frac{37}{10} \quad \frac{35}{9} \quad \frac{34}{21} \quad \frac{37}{22} \quad \frac{30}{50}$$

$$\frac{50}{50} \quad \frac{59}{26} \quad \frac{50}{10} \quad \frac{33}{2} \quad \frac{33}{8} \quad \frac{33}{23} \quad \frac{29}{50}$$

$$\frac{53}{50} \quad \frac{55}{41} \quad \frac{29}{33} \quad \frac{25}{10} \quad \frac{37}{7} \quad \frac{37}{4} \quad \frac{30}{2} \quad \frac{28}{9} \quad \frac{25}{22} \quad \frac{29}{23} \quad \frac{29}{50}$$

$$\frac{23}{50} \quad \frac{25}{36} \quad \frac{22}{7} \quad \frac{30}{5} \quad \frac{26}{8} \quad \frac{21}{21} \quad \frac{24}{22} \quad \frac{19}{22} \quad \frac{18}{50}$$

$$\frac{28}{50} \quad \frac{26}{27} \quad \frac{25}{8} \quad \frac{30}{7} \quad \frac{28}{9} \quad \frac{23}{22} \quad \frac{30}{23} \quad \frac{22}{50} \quad \frac{21}{50}$$

$$\frac{34}{50} \quad \frac{31}{27} \quad \frac{28}{2} \quad \frac{32}{8} \quad \frac{27}{17} \quad \frac{31}{18} \quad \frac{27}{50} \quad \frac{30}{50}$$

$$\frac{37}{50} \quad \frac{33}{25} \quad \frac{32}{2} \quad \frac{37}{2} \quad \frac{33}{18} \quad \frac{36}{50} \quad \frac{34}{50}$$

$$\frac{43}{50} \quad \frac{42}{38} \quad \frac{40}{4} \quad \frac{43}{7} \quad \frac{41}{16} \quad \frac{44}{17} \quad \frac{40}{36} \quad \frac{40}{50} \quad \frac{37}{50}$$

Sta.	+	x	-	Elev
		916.19		
19				911.5
	+50			11.4
20				11.8
	+50			13.7
T.P	4.59	919.86	0.92	915.27
21				15.3
	+50			16.2
22				16.6
	+50			16.3
23				15.1
	+50			14.5
24	x			13.4 13.4

Rt.

4

Rt.

$$\frac{41}{50} \quad \frac{42}{24} \quad \frac{42}{5} \quad \frac{48}{2} \quad \frac{47}{6} \quad \frac{44}{6} \quad \frac{47}{15} \quad \frac{43}{16} \quad \frac{36}{40} \quad \frac{39}{50}$$

$$\frac{36}{50} \quad \frac{49}{15} \quad \frac{48}{16} \quad \frac{50}{16} \quad \frac{45}{33} \quad \frac{40}{50}$$

$$\frac{31}{50} \quad \frac{34}{21} \quad \frac{39}{3} \quad \frac{42}{2} \quad \frac{44}{7} \quad \frac{41}{7} \quad \frac{46}{16} \quad \frac{43}{17} \quad \frac{43}{33} \quad \frac{40}{50}$$

$$\frac{18}{50} \quad \frac{19}{29} \quad \frac{22}{4} \quad \frac{26}{3} \quad \frac{25}{6} \quad \frac{21}{6} \quad \frac{28}{17} \quad \frac{24}{18} \quad \frac{28}{50}$$

$$\frac{39}{50} \quad \frac{40}{28} \quad \frac{42}{5} \quad \frac{48}{9} \quad \frac{46}{9} \quad \frac{43}{5} \quad \frac{49}{14} \quad \frac{44}{15} \quad \frac{48}{33} \quad \frac{52}{50}$$

$$\frac{34}{50} \quad \frac{33}{29} \quad \frac{33}{4} \quad \frac{38}{3} \quad \frac{37}{9} \quad \frac{33}{5} \quad \frac{39}{14} \quad \frac{36}{15} \quad \frac{39}{50}$$

$$\frac{35}{50} \quad \frac{32}{29} \quad \frac{30}{5} \quad \frac{34}{9} \quad \frac{33}{9} \quad \frac{30}{5} \quad \frac{33}{14} \quad \frac{31}{15} \quad \frac{27}{50}$$

$$\frac{38}{50} \quad \frac{34}{27} \quad \frac{34}{5} \quad \frac{36}{4} \quad \frac{36}{9} \quad \frac{34}{4} \quad \frac{36}{14} \quad \frac{34}{14} \quad \frac{35}{50}$$

$$\frac{46}{50} \quad \frac{44}{30} \quad \frac{44}{4} \quad \frac{48}{3} \quad \frac{48}{6} \quad \frac{43}{6} \quad \frac{47}{14} \quad \frac{42}{15} \quad \frac{34}{50}$$

$$\frac{65}{50} \quad \frac{59}{29} \quad \frac{52}{5} \quad \frac{56}{4} \quad \frac{54}{9} \quad \frac{50}{5} \quad \frac{58}{14} \quad \frac{46}{15} \quad \frac{38}{50}$$

$$\frac{74}{50} \quad \frac{69}{25} \quad \frac{63}{5} \quad \frac{67}{4} \quad \frac{65}{5} \quad \frac{62}{5} \quad \frac{64}{14} \quad \frac{58}{15} \quad \frac{53}{50}$$

Sta	+	π	-	Elev
		919.86 ✓		
24	+50			912.8
25				13.0
	+50			13.5 ✓
B.M.	1.75	916.26 ✓	5.35	914.51
				914.53
26				13.0 ✓
	+50			12.2 ✓
27				11.6 ✓
	+50			11.5 ✓
28				11.8 ✓
	+50			11.3 ✓
29				10.6 ✓
	+50			10.8 ✓

L1

L2

R1

$\frac{7.2}{50}$	$\frac{7.3}{30}$	$\frac{7.0}{6}$	$\frac{7.3}{5}$	$\frac{7.1}{5}$	$\frac{7.0}{13}$	$\frac{6.9}{14}$	$\frac{6.8}{34}$	$\frac{6.5}{50}$
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$\frac{6.2}{50}$	$\frac{6.5}{30}$	$\frac{6.8}{6}$	$\frac{7.1}{5}$	$\frac{6.9}{3}$	$\frac{6.8}{11}$	$\frac{7.2}{12}$	$\frac{6.9}{35}$	$\frac{7.2}{50}$
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$\frac{6.0}{50}$	$\frac{6.1}{29}$	$\frac{6.3}{6}$	$\frac{6.6}{5}$	$\frac{6.4}{3}$	$\frac{6.3}{11}$	$\frac{6.8}{12}$	$\frac{6.5}{29}$	$\frac{6.5}{50}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

3pk in 2d'ant 26'ht. 25+38

$\frac{3.1}{50}$	$\frac{2.9}{24}$	$\frac{3.2}{6}$	$\frac{3.6}{5}$	$\frac{3.3}{3}$	$\frac{3.1}{11}$	$\frac{3.5}{12}$	$\frac{2.9}{27}$	$\frac{3.2}{50}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{3.2}{50}$	$\frac{4.0}{23}$	$\frac{4.0}{7}$	$\frac{4.4}{6}$	$\frac{4.1}{2}$	$\frac{3.9}{10}$	$\frac{4.5}{11}$	$\frac{4.0}{27}$	$\frac{3.9}{50}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{4.3}{50}$	$\frac{4.5}{32}$	$\frac{4.6}{7}$	$\frac{5.0}{6}$	$\frac{4.7}{2}$	$\frac{5.1}{10}$	$\frac{4.8}{11}$	$\frac{4.8}{31}$	$\frac{4.9}{50}$
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$\frac{4.4}{30}$	$\frac{4.3}{20}$	$\frac{4.6}{7}$	$\frac{4.8}{6}$	$\frac{4.8}{3}$	$\frac{4.6}{12}$	$\frac{4.7}{13}$	$\frac{5.0}{34}$	$\frac{5.1}{50}$
------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

$\frac{4.3}{50}$	$\frac{4.3}{30}$	$\frac{4.3}{5}$	$\frac{4.6}{4}$	$\frac{4.5}{3}$	$\frac{4.3}{4}$	$\frac{4.6}{13}$	$\frac{4.3}{14}$	$\frac{4.3}{50}$
------------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{5.0}{50}$	$\frac{5.0}{28}$	$\frac{4.9}{3}$	$\frac{5.1}{7}$	$\frac{5.0}{5}$	$\frac{4.7}{13}$	$\frac{5.3}{14}$	$\frac{4.4}{32}$	$\frac{4.4}{50}$
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$\frac{5.7}{50}$	$\frac{5.8}{25}$	$\frac{5.4}{7}$	$\frac{5.7}{3}$	$\frac{5.1}{5}$	$\frac{5.5}{6}$	$\frac{5.7}{14}$	$\frac{5.2}{15}$	$\frac{5.1}{39}$	$\frac{5.0}{50}$
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$\frac{6.0}{50}$	$\frac{5.7}{33}$	$\frac{5.8}{3}$	$\frac{5.6}{2}$	$\frac{5.5}{5}$	$\frac{5.2}{7}$	$\frac{5.6}{13}$	$\frac{5.2}{16}$	$\frac{5.0}{50}$
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Sta + π - Elev.

9/6/26

30 + 00

✓
10.5

I.P. 2.45 913.67 5.04

911.22
911.24

+50

910.9

31

11.1

+50

10.5

32

09.5

+50

08.9

33

08.5

+50

08.3

34

08.2

+50

07.9

35

07.6

K.R
L.C
R.R
6/24/28

Lt

R

Rt

$\frac{66}{50}$ $\frac{61}{50}$ $\frac{55}{2}$ $\frac{58}{1}$ $\frac{58}{1}$ $\frac{55}{8}$ $\frac{58}{16}$ $\frac{59}{17}$ $\frac{51}{50}$

Top stamp ²⁸ 29180

$\frac{31}{50}$ $\frac{25}{30}$ $\frac{25}{2}$ $\frac{28}{1}$ $\frac{28}{1}$ $\frac{24}{7}$ $\frac{26}{16}$ $\frac{24}{17}$ $\frac{25}{30}$ $\frac{29}{50}$

$\frac{32}{50}$ $\frac{29}{30}$ $\frac{26}{4}$ $\frac{26}{4}$ $\frac{23}{7}$ $\frac{27}{15}$ $\frac{22}{16}$ $\frac{28}{50}$

$\frac{46}{50}$ $\frac{38}{31}$ $\frac{29}{3}$ $\frac{33}{2}$ $\frac{32}{1}$ $\frac{27}{6}$ $\frac{28}{15}$ $\frac{24}{16}$ $\frac{20}{50}$

$\frac{49}{30}$ $\frac{48}{29}$ $\frac{44}{4}$ $\frac{42}{1}$ $\frac{38}{6}$ $\frac{40}{13}$ $\frac{36}{14}$ $\frac{29}{40}$ $\frac{27}{50}$

$\frac{56}{50}$ $\frac{54}{28}$ $\frac{50}{3}$ $\frac{48}{1}$ $\frac{45}{6}$ $\frac{47}{13}$ $\frac{41}{14}$ $\frac{28}{50}$

$\frac{62}{50}$ $\frac{58}{23}$ $\frac{52}{5}$ $\frac{51}{4}$ $\frac{52}{1}$ $\frac{50}{7}$ $\frac{52}{13}$ $\frac{46}{19}$ $\frac{29}{50}$

$\frac{61}{30}$ $\frac{61}{35}$ $\frac{54}{6}$ $\frac{59}{5}$ $\frac{54}{1}$ $\frac{51}{5}$ $\frac{53}{13}$ $\frac{49}{14}$ $\frac{44}{27}$ $\frac{29}{50}$

$\frac{62}{50}$ $\frac{58}{24}$ $\frac{57}{5}$ $\frac{61}{4}$ $\frac{58}{1}$ $\frac{52}{5}$ $\frac{53}{13}$ $\frac{50}{14}$ $\frac{42}{32}$ $\frac{27}{50}$

$\frac{64}{50}$ $\frac{61}{25}$ $\frac{57}{5}$ $\frac{62}{4}$ $\frac{58}{1}$ $\frac{53}{6}$ $\frac{57}{13}$ $\frac{54}{14}$ $\frac{43}{38}$ $\frac{34}{50}$

$\frac{65}{50}$ $\frac{64}{25}$ $\frac{60}{5}$ $\frac{64}{3}$ $\frac{61}{1}$ $\frac{56}{5}$ $\frac{59}{14}$ $\frac{56}{15}$ $\frac{47}{38}$ $\frac{37}{50}$

Sta.	+	Δ	-	Elev.
		✓		
		913.67		
35	+50			907.7
36				07.5
T.P.	1.55	✓	4.50	909.17
	+50			06.8
37				06.4
	+50			05.8
38				05.3
	+50			05.5
39				05.5
	+50			04.8
40				04.2
	+50			05.6

14

9

14

 $\frac{6.5}{50}$ $\frac{6.4}{22}$ $\frac{6.1}{5}$ $\frac{6.4}{4}$ $\frac{6.0}{5}$ $\frac{5.6}{5}$ $\frac{6.1}{14}$ $\frac{5.6}{15}$ $\frac{5.1}{43}$ $\frac{4.7}{50}$
 $\frac{5.7}{50}$ $\frac{6.0}{21}$ $\frac{6.2}{5}$ $\frac{6.7}{4}$ $\frac{6.2}{5}$ $\frac{6.0}{5}$ $\frac{6.6}{14}$ $\frac{6.1}{15}$ $\frac{5.7}{50}$
 $\frac{4.7}{50}$ $\frac{3.3}{22}$ $\frac{3.7}{5}$ $\frac{4.3}{4}$ $\frac{3.9}{5}$ $\frac{3.8}{5}$ $\frac{4.4}{13}$ $\frac{4.2}{14}$ $\frac{4.4}{36}$ $\frac{4.3}{50}$
 $\frac{3.1}{50}$ $\frac{3.7}{23}$ $\frac{4.0}{6}$ $\frac{4.6}{5}$ $\frac{4.3}{5}$ $\frac{4.1}{4}$ $\frac{4.8}{12}$ $\frac{4.5}{13}$ $\frac{5.3}{33}$ $\frac{5.5}{50}$
 $\frac{3.5}{50}$ $\frac{4.1}{22}$ $\frac{4.7}{6}$ $\frac{5.3}{5}$ $\frac{4.9}{5}$ $\frac{4.6}{3}$ $\frac{5.9}{12}$ $\frac{5.1}{13}$ $\frac{5.6}{33}$ $\frac{6.2}{50}$
 $\frac{4.2}{50}$ $\frac{5.0}{21}$ $\frac{5.4}{5}$ $\frac{5.8}{4}$ $\frac{5.4}{4}$ $\frac{5.3}{4}$ $\frac{5.7}{14}$ $\frac{6.2}{32}$ $\frac{6.6}{50}$
 $\frac{4.9}{50}$ $\frac{4.8}{21}$ $\frac{5.0}{6}$ $\frac{5.5}{5}$ $\frac{5.2}{5}$ $\frac{4.9}{3}$ $\frac{5.3}{13}$ $\frac{5.6}{33}$ $\frac{6.4}{50}$
 $\frac{4.8}{50}$ $\frac{4.9}{22}$ $\frac{5.0}{6}$ $\frac{5.4}{5}$ $\frac{5.2}{5}$ $\frac{4.9}{4}$ $\frac{5.6}{11}$ $\frac{5.3}{12}$ $\frac{5.8}{32}$ $\frac{6.2}{50}$
 $\frac{5.8}{50}$ $\frac{5.6}{25}$ $\frac{5.7}{6}$ $\frac{6.2}{5}$ $\frac{5.9}{5}$ $\frac{5.8}{3}$ $\frac{6.7}{12}$ $\frac{6.2}{13}$ $\frac{6.5}{32}$ $\frac{6.7}{50}$ $\frac{6.9}{75}$ $\frac{6.8}{100}$
 $\frac{6.6}{125}$ $\frac{6.6}{100}$ $\frac{6.2}{50}$ $\frac{6.2}{25}$ $\frac{6.3}{8}$ $\frac{6.8}{7}$ $\frac{6.3}{5}$ $\frac{6.2}{3}$ $\frac{6.8}{14}$ $\frac{6.4}{14}$ $\frac{6.4}{33}$ $\frac{6.4}{50}$
 $\frac{5.0}{50}$ $\frac{5.1}{23}$ $\frac{5.0}{6}$ $\frac{5.4}{5}$ $\frac{5.1}{5}$ $\frac{4.8}{3}$ $\frac{5.4}{13}$ $\frac{5.0}{14}$ $\frac{4.8}{33}$ $\frac{4.6}{50}$

Sta.	+	π ✓	-	Elev.
		910.72		
41				907.0
	+50			08.1
T.P.	1.38	912.46 ✓	0.64	910.08 ✓
B.M.			4.19	914.32 ✓
				914.32
42				10.1
	+50			13.2
43				13.9
	+50			13.6
44				14.0
	+50			14.1
45				14.6
	+50			14.4
46				13.5
T.P.	0.75	914.64 ✓	4.57	913.89 ✓

Lt.

R.

Rt.

35	33	36	40	37	33	40	36	35	35
50	24	5	4	4	4	13	19	33	50

27	29	26	30	26	22	29	23	25	24
50	28	5	4	9	9	13	14	35	50

Spk. in 8" Oct 30' Lt 42+50.

82	88	81	89	84	81	85	81	82	86
50	30	5	9	5	13	14	37	50	

49	49	52	54	53	58	55	59	60	
50	28	6	5	13	19	35	50		

40	41	45	48	46	46	52	49	54	59
50	28	6	5	5	13	13	14	36	50

40	43	48	50	49	48	52	49	52	59
50	27	6	5	5	15	16	38	50	

46	45	45	49	45	49	49	46	47	47
50	26	8	7	4	12	13	32	50	

49	47	44	51	44	42	46	43	41	41
50	30	8	7	9	9	11	12	33	50

49	44	41	45	39	43	39	36	35	
50	23	7	6	11	12	32	50		

51	47	44	48	41	40	45	41	37	29
50	29	8	7	2	11	12	31	50	

58	52	52	57	50	49	56	52	51	52
50	30	7	6	2	11	12	33	50	

Sta	t	x	-	Elev
		914.64		
46	+50			911.9
47				11.1
	+50			10.7
48				10.6
	+50			10.0
49				09.3
	+50			08.8
50				08.3
	+50			07.4
51				08.9
	+50			09.2
T.P.	6.21	914.32	6.53	908.11

Lt

R

Rt

 $\frac{23}{50}$ $\frac{24}{28}$ $\frac{26}{7}$ $\frac{31}{6}$ $\frac{27}{2}$ $\frac{26}{2}$ $\frac{33}{12}$ $\frac{29}{12}$ $\frac{32}{33}$ $\frac{32}{50}$
 $\frac{31}{50}$ $\frac{31}{23}$ $\frac{34}{7}$ $\frac{38}{8}$ $\frac{35}{-}$ $\frac{40}{10}$ $\frac{32}{32}$ $\frac{37}{50}$
 $\frac{26}{50}$ $\frac{26}{26}$ $\frac{39}{7}$ $\frac{48}{6}$ $\frac{39}{8}$ $\frac{38}{3}$ $\frac{45}{12}$ $\frac{41}{13}$ $\frac{41}{38}$ $\frac{39}{50}$
 $\frac{35}{50}$ $\frac{38}{25}$ $\frac{40}{7}$ $\frac{45}{6}$ $\frac{40}{-}$ $\frac{39}{4}$ $\frac{43}{14}$ $\frac{40}{15}$ $\frac{39}{36}$ $\frac{39}{50}$
 $\frac{34}{5}$ $\frac{37}{29}$ $\frac{44}{6}$ $\frac{49}{5}$ $\frac{46}{-}$ $\frac{43}{3}$ $\frac{52}{12}$ $\frac{47}{13}$ $\frac{51}{50}$
 $\frac{43}{50}$ $\frac{47}{25}$ $\frac{51}{7}$ $\frac{56}{6}$ $\frac{53}{-}$ $\frac{51}{3}$ $\frac{58}{14}$ $\frac{55}{15}$ $\frac{60}{50}$
 $\frac{44}{50}$ $\frac{50}{33}$ $\frac{55}{7}$ $\frac{61}{6}$ $\frac{58}{-}$ $\frac{56}{3}$ $\frac{63}{14}$ $\frac{60}{15}$ $\frac{62}{50}$
 $\frac{54}{50}$ $\frac{60}{27}$ $\frac{62}{7}$ $\frac{67}{6}$ $\frac{63}{-}$ $\frac{62}{3}$ $\frac{70}{12}$ $\frac{66}{18}$ $\frac{65}{50}$
 $\frac{68}{50}$ $\frac{73}{25}$ $\frac{71}{8}$ $\frac{75}{7}$ $\frac{70}{-}$ $\frac{69}{2}$ $\frac{73}{11}$ $\frac{69}{12}$ $\frac{61}{50}$
 $\frac{54}{50}$ $\frac{60}{31}$ $\frac{59}{7}$ $\frac{64}{6}$ $\frac{58}{-}$ $\frac{55}{2}$ $\frac{61}{11}$ $\frac{56}{12}$ $\frac{53}{33}$ $\frac{47}{50}$
 $\frac{54}{50}$ $\frac{56}{23}$ $\frac{55}{7}$ $\frac{59}{6}$ $\frac{54}{-}$ $\frac{53}{3}$ $\frac{58}{12}$ $\frac{54}{13}$ $\frac{51}{30}$ $\frac{46}{50}$

Sta.	+	X	-	Elev
		914.32		
52				908.3
	+50			07.0
53				07.2
	+50			08.7
54				08.8
	+50			08.5
55				09.2
	+50			10.6
56				10.8
	+50			10.4
57				10.3
B.M.		3.60		910.72 ✓
				910.10

11

9

11

$\frac{5.9}{50}$ $\frac{6.1}{23}$ $\frac{6.3}{7}$ $\frac{6.7}{6}$ $\frac{6.1}{11}$ $\frac{6.7}{12}$ $\frac{6.2}{32}$ $\frac{5.7}{50}$

$\frac{7.2}{50}$ $\frac{7.3}{25}$ $\frac{7.4}{7}$ $\frac{7.7}{6}$ $\frac{7.3}{4}$ $\frac{7.2}{11}$ $\frac{7.4}{12}$ $\frac{6.8}{33}$ $\frac{6.7}{50}$

$\frac{7.6}{50}$ $\frac{7.9}{25}$ $\frac{7.1}{7}$ $\frac{7.4}{6}$ $\frac{7.1}{3}$ $\frac{6.9}{11}$ $\frac{7.3}{12}$ $\frac{6.9}{30}$ $\frac{6.5}{50}$

$\frac{6.2}{50}$ $\frac{5.7}{23}$ $\frac{5.6}{6}$ $\frac{6.0}{5}$ $\frac{5.4}{4}$ $\frac{5.9}{12}$ $\frac{6.8}{13}$ $\frac{5.4}{37}$ $\frac{5.3}{50}$

$\frac{5.8}{50}$ $\frac{5.7}{25}$ $\frac{5.6}{6}$ $\frac{5.9}{5}$ $\frac{5.5}{4}$ $\frac{5.2}{12}$ $\frac{5.8}{13}$ $\frac{5.2}{35}$ $\frac{4.9}{50}$

$\frac{6.0}{50}$ $\frac{6.0}{25}$ $\frac{5.8}{7}$ $\frac{6.1}{6}$ $\frac{5.8}{9}$ $\frac{5.5}{12}$ $\frac{6.0}{13}$ $\frac{5.5}{35}$ $\frac{5.1}{50}$

$\frac{5.1}{50}$ $\frac{5.2}{28}$ $\frac{5.1}{8}$ $\frac{5.4}{7}$ $\frac{6.1}{3}$ $\frac{4.8}{12}$ $\frac{5.3}{13}$ $\frac{5.0}{30}$ $\frac{5.2}{50}$

$\frac{3.7}{50}$ $\frac{3.7}{28}$ $\frac{3.7}{8}$ $\frac{4.0}{7}$ $\frac{3.7}{2}$ $\frac{3.6}{10}$ $\frac{4.1}{11}$ $\frac{3.6}{36}$ $\frac{3.5}{50}$

$\frac{3.9}{50}$ $\frac{3.9}{33}$ $\frac{3.6}{8}$ $\frac{4.2}{7}$ $\frac{3.6}{11}$ $\frac{3.5}{12}$ $\frac{3.2}{27}$ $\frac{3.1}{50}$

$\frac{4.9}{50}$ $\frac{4.5}{23}$ $\frac{4.2}{8}$ $\frac{4.4}{7}$ $\frac{3.9}{10}$ $\frac{4.0}{11}$ $\frac{3.7}{23}$ $\frac{3.4}{50}$

$\frac{5.4}{50}$ $\frac{4.6}{23}$ $\frac{4.3}{7}$ $\frac{4.4}{6}$ $\frac{4.0}{11}$ $\frac{4.3}{12}$ $\frac{3.9}{24}$ $\frac{4.0}{50}$

Spk in R.P. N.E. GOLF "4"

Sta	+	-	Elev.
B.M.	3.55	914.25	910.70

57	+50		909.4
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58			09.0
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	+50		09.7
--	-----	--	------

59			09.8
----	--	--	------

	+50		09.7
--	-----	--	------

	+95		11.0
--	-----	--	------

60			11.2
----	--	--	------

	+19.20		11.8
--	--------	--	------

Lt.

L

Rt.

Spt. in RA NE Cor. "J"

$\frac{41}{50}$	$\frac{44}{50}$	$\frac{48}{8}$	$\frac{52}{7}$	$\frac{49}{11}$	$\frac{57}{12}$	$\frac{54}{12}$	$\frac{59}{24}$	$\frac{62}{50}$
-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{36}{50}$	$\frac{43}{24}$	$\frac{52}{7}$	$\frac{56}{6}$	$\frac{53}{11}$	$\frac{61}{12}$	$\frac{58}{12}$	$\frac{69}{34}$	$\frac{73}{50}$	$\frac{73}{75}$	$\frac{72}{100}$	Pot hole.
-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	-----------

$\frac{40}{50}$	$\frac{40}{24}$	$\frac{46}{9}$	$\frac{50}{8}$	$\frac{46}{10}$	$\frac{54}{10}$	$\frac{50}{11}$	$\frac{55}{24}$	$\frac{63}{50}$
-----------------	-----------------	----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{52}{50}$	$\frac{43}{24}$	$\frac{47}{10}$	$\frac{56}{9}$	$\frac{45}{15}$	$\frac{58}{16}$	$\frac{47}{16}$	$\frac{52}{50}$
-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------

$\frac{57}{50}$	$\frac{53}{50}$	$\frac{50}{13}$	$\frac{57}{12}$	$\frac{46}{16}$	$\frac{57}{16}$	$\frac{46}{17}$	$\frac{42}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{48}{50}$	$\frac{45}{16}$	$\frac{36}{10}$	$\frac{53}{15}$	$\frac{36}{15}$	$\frac{46}{18}$	$\frac{47}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{34}{50}$

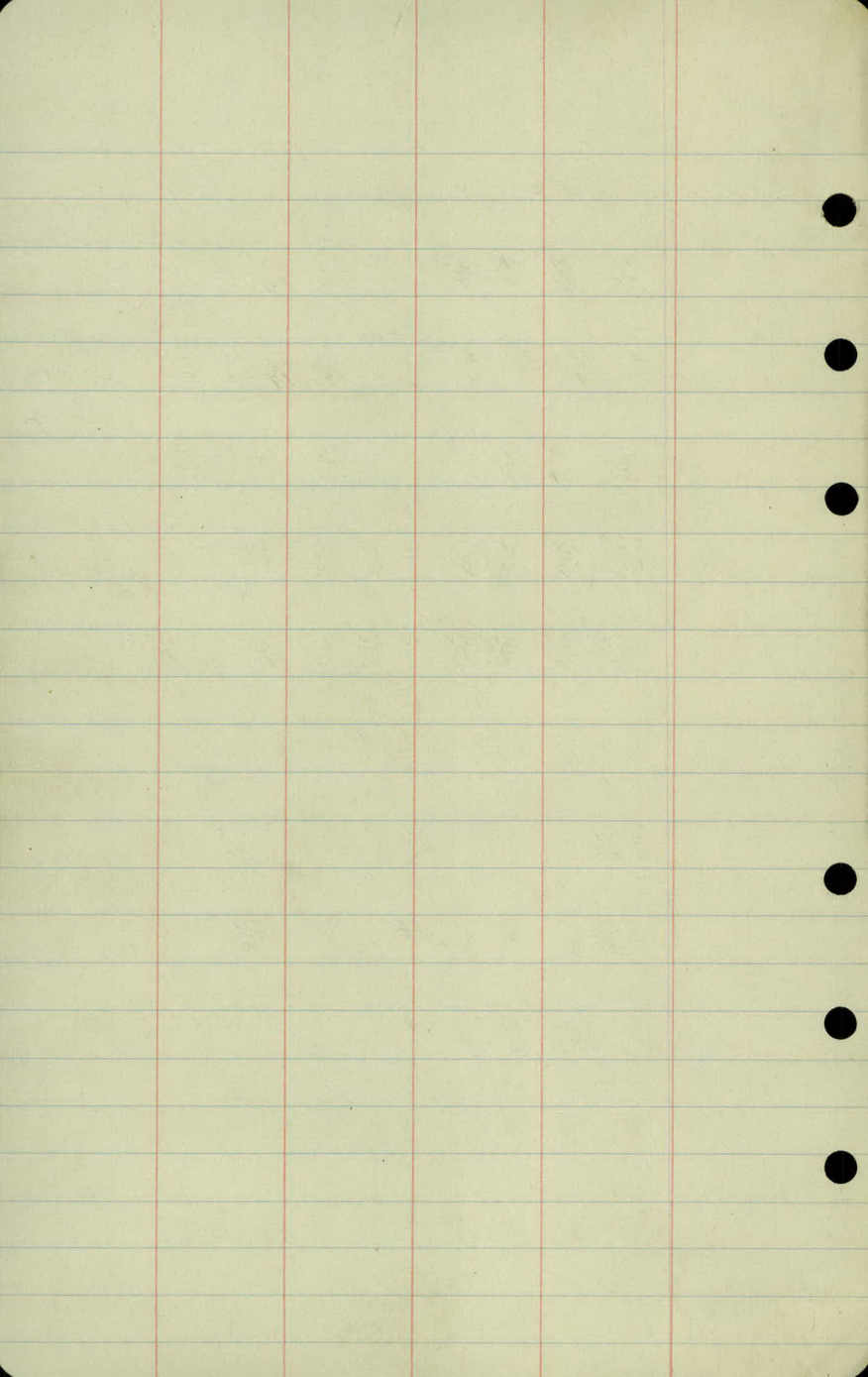
$\frac{31}{50}$

$\frac{27}{50}$

$\frac{26}{50}$

$\frac{25}{50}$

$\frac{23}{50}$



Groveland St.
slope stakes

13 Pages

Sta.	+	x	-	Grade
B.M.	3.22	917.05		911.83
04 00				913.3
+50				13.0
1				12.8
+50				12.5
2				12.3
+50				12.0
3				11.9
+50				11.7
4				11.6
T.P.	4.30	915.12	6.23	910.82
+50				11.4
5				11.4

8/17/38

C.M.

R.P.

L.C.

M.G.

1

Cor. Rod.

Lt

R

Rt.

3pk in R.P. 76' Lt 1/24

$$3.0 \quad 25.0 / \begin{array}{r} 9.5 \\ + 0.3 \\ \hline 9.8 \end{array} \quad \begin{array}{r} 57 \\ + 0.1 \\ \hline 57.1 \end{array} \quad \begin{array}{r} 48 \\ 2.10 / 230 \end{array}$$

$$4.1 \quad 24.9 / \begin{array}{r} 4.4 \\ 40.17 \\ \hline 44.57 \end{array} \quad \begin{array}{r} 49 \\ - 0.8 \\ \hline 48.2 \end{array} \quad \begin{array}{r} 57 \\ 40.04 / 248 \end{array}$$

$$4.3 \quad 24.0 / \begin{array}{r} 4.8 \\ 40.15 \\ \hline 44.95 \end{array} \quad \begin{array}{r} 52 \\ - 0.9 \\ \hline 51.05 \end{array} \quad \begin{array}{r} 57 \\ 42.06 / 22.2 \end{array}$$

$$4.6 \quad 23.8 / \begin{array}{r} 5.2 \\ 40.19 \\ \hline 45.99 \end{array} \quad \begin{array}{r} 58 \\ - 1.3 \\ \hline 56.69 \end{array} \quad \begin{array}{r} 57 \\ 44.09 / 228 \end{array}$$

$$4.8 \quad 25.0 / \begin{array}{r} 4.6 \\ + 0.2 \\ \hline 4.8 \end{array} \quad \begin{array}{r} 55 \\ - 0.2 \\ \hline 54.8 \end{array} \quad \begin{array}{r} 51 \\ 45.17 / 24.4 \end{array}$$

$$5.1 \quad 25.0 / \begin{array}{r} 3.6 \\ + 1.5 \\ \hline 5.1 \end{array} \quad \begin{array}{r} 42 \\ + 0.9 \\ \hline 42.9 \end{array} \quad \begin{array}{r} 44 \\ 40.7 / 230 \end{array}$$

$$5.2 \quad 25.0 / \begin{array}{r} 3.9 \\ + 1.3 \\ \hline 5.2 \end{array} \quad \begin{array}{r} 44 \\ + 0.8 \\ \hline 44.8 \end{array} \quad \begin{array}{r} 45 \\ 40.7 / 250 \end{array}$$

$$5.4 \quad 25.0 / \begin{array}{r} 5.1 \\ + 0.3 \\ \hline 5.4 \end{array} \quad \begin{array}{r} 54 \\ + 0.0 \\ \hline 54.0 \end{array} \quad \begin{array}{r} 57 \\ 41.7 / 24.4 \end{array}$$

$$5.5 \quad 23.2 / \begin{array}{r} 6.4 \\ 40.1 \\ \hline 46.5 \end{array} \quad \begin{array}{r} 70 \\ - 1.5 \\ \hline 68.5 \end{array} \quad \begin{array}{r} 74 \\ 40.1 / 21.2 \end{array}$$

$$5.7 \quad 21.0 / \begin{array}{r} 5.7 \\ 40.0 \\ \hline 45.7 \end{array} \quad \begin{array}{r} 40 \\ - 3.3 \\ \hline 36.7 \end{array} \quad \begin{array}{r} 64 \\ - 2.7 / 18.4 \end{array}$$

$$5.7 \quad 22.8 / \begin{array}{r} 4.8 \\ 40.9 \\ \hline 45.7 \end{array} \quad \begin{array}{r} 52 \\ - 1.6 \\ \hline 50.4 \end{array} \quad \begin{array}{r} 57 \\ 45.00 / 21.0 \end{array}$$

Sta	+	π	-	Grade
		915.12		
5	+50			11.4
6				11.4
T.P.	9.81	916.09	3.84	911.28
	+50			11.4
7				11.5
	+50			11.6
8				11.6
	+50			11.6
9				11.5
	+50			11.4
T.P.	9.25	915.65	4.69	911.40
10				11.3
	+50			11.2

Gr Rod	Lt	R	Rt
3.7	$23.6 / \frac{44}{23.13}$	$\frac{46}{-09}$	$\frac{45}{23.09} / 22.5$
3.7	$24.4 / \frac{40}{23.17}$	$\frac{49}{-07}$	$\frac{46}{23.11} / 23.2$
4.7	$25.0 / \frac{47}{24.0}$	$\frac{49}{-02}$	$\frac{53}{23.94} / 23.8$
4.6	$25.0 / \frac{43}{24.3}$	$\frac{45}{24.1}$	$\frac{49}{24.17} / 24.4$
4.5	$25.0 / \frac{39}{24.6}$	$\frac{40}{24.5}$	$\frac{41}{24.9} / 25.0$
4.5	$25.0 / \frac{38}{24.7}$	$\frac{39}{24.6}$	$\frac{37}{24.8} / 25.0$
4.5	$25.0 / \frac{43}{24.2}$	$\frac{44}{24.1}$	$\frac{43}{24.2} / 25.0$
4.6	$25.0 / \frac{40}{24.0}$	$\frac{47}{-01}$	$\frac{45}{24.1} / 25.0$
4.7	$24.2 / \frac{51}{24.16}$	$\frac{49}{-02}$	$\frac{46}{24.1} / 25.0$
4.4	$24.2 / \frac{48}{24.16}$	$\frac{48}{-03}$	$\frac{48}{24.16} / 24.2$
4.5	$23.6 / \frac{52}{23.13}$	$\frac{53}{-07}$	$\frac{49}{23.14} / 24.2$

Sta	+	π	-	Grade
-----	---	-------	---	-------

915.65

11				11.1
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+50				11.0
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12				10.9
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+50				10.9
-----	--	--	--	------

13				11.0
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T.P.	7.05	917.89	4.81	910.89
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+50				11.3
-----	--	--	--	------

14				11.8
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+65				12.5
-----	--	--	--	------

15				12.9
----	--	--	--	------

B.M.	9.75	912.92	4.75	913.14
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913.17

+56				12.9
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+85				12.8
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Gr. Rod.

Lt.

R

Rt.

$$4.6 \quad 22.8 / \begin{array}{r} 52 \\ R.14 \\ -98 \end{array} \quad \begin{array}{r} 54 \\ -98 \end{array} \quad \begin{array}{r} 98 \\ R.18 / 24.6 \end{array}$$

$$4.6 \quad 22.2 / \begin{array}{r} 60 \\ R.06 \\ -11 \end{array} \quad \begin{array}{r} 57 \\ -11 \end{array} \quad \begin{array}{r} 51 \\ R.15 / 24.0 \end{array}$$

$$4.7 \quad 22.0 / \begin{array}{r} 62 \\ R.05 \\ -14 \end{array} \quad \begin{array}{r} 61 \\ -14 \end{array} \quad \begin{array}{r} 50 \\ R.11 / 23.2 \end{array}$$

$$4.7 \quad 22.0 / \begin{array}{r} 62 \\ R.05 \\ -17 \end{array} \quad \begin{array}{r} 64 \\ -17 \end{array} \quad \begin{array}{r} 61 \\ R.04 / 22.2 \end{array}$$

$$4.6 \quad 22.0 / \begin{array}{r} 61 \\ R.05 \\ -19 \end{array} \quad \begin{array}{r} 65 \\ -19 \end{array} \quad \begin{array}{r} 62 \\ R.04 / 21.8 \end{array}$$

Night in R.R.

$$6.6 \quad 21.2 / \begin{array}{r} 85 \\ R.01 \end{array} \quad \begin{array}{r} 84 \end{array} \quad \begin{array}{r} 82 \\ R.04 / 21.8 \end{array}$$

$$6.1 \quad 18.2 / \begin{array}{r} 87 \\ -2.6 \end{array} \quad \begin{array}{r} 84 \\ -2.3 \end{array} \quad \begin{array}{r} 80 \\ R.01 / 17.2 \end{array}$$

$$5.8 \quad 18.6 / \begin{array}{r} 82 \\ -2.8 \end{array} \quad \begin{array}{r} 76 \\ -2.2 \end{array} \quad \begin{array}{r} 75 \\ -2.1 / 17.2 \end{array}$$

5.0

Top Row to 15+38.63

5.0

5.1

Sta	+	X	-	Grade
		91292		

16				12.8
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	+19			12.8
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	+35			12.7
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	+20			12.7
--	-----	--	--	------

17				12.6
----	--	--	--	------

	+50			12.5
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18				12.4
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	+50			12.4
--	-----	--	--	------

19				12.5
----	--	--	--	------

	+50			12.8
--	-----	--	--	------

I.P.	2.27	919.99	620	911.72
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20				13.2
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Gr. Rod.

Lt

R

Rt.

5.1		$\frac{57}{-96}$	$\frac{5.3}{R.18/24.6}$
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5.1	$\frac{25.0}{10.2} / \frac{7.7}{10.2}$	$\frac{50}{10.1}$	$\frac{4.3}{10.7/25.0}$
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5.2	$\frac{25.0}{10.2} / \frac{7.7}{10.2}$	$\frac{50}{10.1}$	$\frac{4.3}{10.7/25.0}$
-----	--	-------------------	-------------------------

5.2

5.3	$\frac{25.0}{10.3} / \frac{7.8}{10.3}$	$\frac{51}{10.2}$	$\frac{4.3}{11.0/25.0}$
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5.4	$\frac{25.0}{10.2} / \frac{5.2}{10.2}$	$\frac{53}{10.1}$	$\frac{5.0}{10.4/25.0}$
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5.5	$\frac{25.0}{10.0} / \frac{5.5}{10.0}$	$\frac{57}{-0.7}$	$\frac{5.5}{10.0/25.0}$
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5.5	$\frac{24.6}{R.18} / \frac{5.7}{R.18}$	$\frac{0.0}{-0.5}$	$\frac{5.7}{R.18/24.6}$
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5.4	$\frac{24.0}{R.15} / \frac{5.9}{R.15}$	$\frac{0.5}{-1.1}$	$\frac{5.7}{R.17/24.4}$
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5.1	$\frac{22.6}{R.28} / \frac{6.3}{R.28}$	$\frac{0.4}{-1.3}$	$\frac{0.4}{R.27/22.4}$
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6.8	$\frac{23.8}{12.4} / \frac{7.4}{12.4}$	$\frac{8.1}{-1.3}$	$\frac{8.0}{R.08/22.6}$
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Sta	+	π	-	Grade	
		919.99			
20	+50			13.8	
21				14.5	
	+50			15.2	
22				15.5	
	+50			15.7	
23				15.5	
	+50			15.2	
24				14.9	
	+50			14.6	
25				14.3	
B.M.	2.61	917.14	546	914.53	914.53
	+50			14.0	

Gr. Rod

L_tL_eR_h

$$6.2 \quad 25.0 / \frac{4.6}{+0.6} \quad \frac{4.2}{0.0} \quad \frac{4.1}{+0.1/25.0}$$

$$5.5 \quad 25.0 / \frac{4.1}{+1.4} \quad \frac{4.6}{+0.9} \quad \frac{4.9}{+0.6/25.0}$$

$$4.8 \quad 25.0 / \frac{3.5}{+1.3} \quad \frac{3.8}{+1.0} \quad \frac{3.6}{+1.2/25.0}$$

$$4.5 \quad 25.0 / \frac{3.4}{+1.1} \quad \frac{3.3}{+1.2} \quad \frac{3.2}{+1.3/25.0}$$

$$4.3 \quad 25.0 / \frac{3.5}{+0.8} \quad \frac{3.7}{+0.6} \quad \frac{3.5}{+0.8/25.0}$$

$$4.5 \quad 24.6 / \frac{4.7}{+0.18} \quad \frac{4.9}{-0.4} \quad \frac{4.0}{+0.5/25.0}$$

$$4.8 \quad 22.6 / \frac{6.0}{+0.08} \quad \frac{5.5}{-0.7} \quad \frac{4.5}{+0.3/25.0}$$

$$5.1 \quad 21.6 / \frac{6.8}{+0.3} \quad \frac{6.6}{-1.5} \quad \frac{5.9}{+0.2/23.9}$$

$$5.4 \quad 21.4 / \frac{7.2}{+0.02} \quad \frac{7.3}{-1.9} \quad \frac{6.9}{+0.5/22.0}$$

$$5.7 \quad 23.0 / \frac{4.7}{+0.10} \quad \frac{4.1}{-1.4} \quad \frac{7.2}{+0.05/22.0}$$

2.4" Oak 24.4 25.4 25.8

$$3.1 \quad 29.0 / \frac{3.6}{+0.15} \quad \frac{3.7}{-0.6} \quad \frac{3.4}{+0.1/24.4}$$

Sta	+	π	-	Grade
		712.14		

26				13.7
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+50				13.4
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27				13.1
----	--	--	--	------

+50				12.8
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28				12.5
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T.P.	2.95	915.71	9.38	912.76
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+50				12.2
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29				11.9
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+50				11.6
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30				11.3
----	--	--	--	------

+50				11.0
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31				10.7
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T.P.	2.09	913.48	4.32	911.39
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Cor Rod

Lt

R

Rt

$$3.4 \quad 24.0 / \begin{array}{r} 59 \\ R15 \end{array} \quad \begin{array}{r} 42 \\ -68 \end{array} \quad \begin{array}{r} 41 \\ R19/23.6 \end{array}$$

$$3.7 \quad 22.8 / \begin{array}{r} 48 \\ R09 \end{array} \quad \begin{array}{r} 50 \\ -13 \end{array} \quad \begin{array}{r} 48 \\ R09/22.8 \end{array}$$

$$4.0 \quad 22.4 / \begin{array}{r} 53 \\ R07 \end{array} \quad \begin{array}{r} 56 \\ -16 \end{array} \quad \begin{array}{r} 57 \\ R03/21.6 \end{array}$$

$$4.3 \quad 22.2 / \begin{array}{r} 57 \\ R06 \end{array} \quad \begin{array}{r} 57 \\ -19 \end{array} \quad \begin{array}{r} 57 \\ R00/22.2 \end{array}$$

$$4.6 \quad 24.2 / \begin{array}{r} 50 \\ R16 \end{array} \quad \begin{array}{r} 53 \\ -06 \end{array} \quad \begin{array}{r} 51 \\ R15/24.0 \end{array}$$

$$3.5 \quad 23.4 / \begin{array}{r} 43 \\ R12 \end{array} \quad \begin{array}{r} 45 \\ -10 \end{array} \quad \begin{array}{r} 39 \\ R16/24.2 \end{array}$$

$$3.8 \quad 22.6 / \begin{array}{r} 50 \\ R08 \end{array} \quad \begin{array}{r} 53 \\ -1.5 \end{array} \quad \begin{array}{r} 48 \\ R10/23.0 \end{array}$$

$$4.1 \quad 24.0 / \begin{array}{r} 51 \\ R10 \end{array} \quad \begin{array}{r} 50 \\ -09 \end{array} \quad \begin{array}{r} 46 \\ R15/24.0 \end{array}$$

$$4.4 \quad 23.0 / \begin{array}{r} 54 \\ R10 \end{array} \quad \begin{array}{r} 53 \\ -09 \end{array} \quad \begin{array}{r} 48 \\ R16/24.2 \end{array}$$

$$4.7 \quad 25.0 / \begin{array}{r} 47 \\ +0.0 \end{array} \quad \begin{array}{r} 49 \\ -0.2 \end{array} \quad \begin{array}{r} 43 \\ +0.4/25.0 \end{array}$$

$$5.0 \quad 25.0 / \begin{array}{r} 47 \\ +0.3 \end{array} \quad \begin{array}{r} 46 \\ +0.4 \end{array} \quad \begin{array}{r} 41 \\ +0.9/25.0 \end{array}$$

Nail in 4" Oct Lt +

Sta	+	X	-	Grade
		713.48		
31	+50			10.4
32				10.1
	+50			09.8
33				09.5
	+50			09.3
34				09.1
	+50			08.9
35				08.7
	+50			08.5
36				08.3
T.P.	207	710.87	5.68	907.80
	750			08.1

8/18/37

7

K. A.

R. P.

L. C.

M. A. G.

Cor. Rod

Lt

R

Lt

$$3.1 \quad 24.6 / \frac{3.3}{R.18} \quad \frac{30}{+91} \quad \frac{22}{10.9/25.0}$$

$$3.4 \quad 22.4 / \frac{4.7}{R.07} \quad \frac{41}{-0.7} \quad \frac{31}{10.3/25.0}$$

$$3.7 \quad 22.2 / \frac{5.1}{R.06} \quad \frac{46}{-0.9} \quad \frac{36}{10.1/25.0}$$

$$4.0 \quad 22.4 / \frac{5.3}{R.07} \quad \frac{50}{-1.0} \quad \frac{4.0}{+0.0/25.0}$$

$$4.2 \quad 22.0 / \frac{5.7}{R.05} \quad \frac{52}{-1.0} \quad \frac{4.7}{R.15/29.0}$$

$$4.4 \quad 22.4 / \frac{5.7}{R.07} \quad \frac{54}{-1.0} \quad \frac{4.7}{R.17/29.4}$$

$$4.6 \quad 22.4 / \frac{5.9}{R.07} \quad \frac{56}{-1.0} \quad \frac{4.8}{R.19/24.6}$$

$$4.8 \quad 22.2 / \frac{6.2}{R.06} \quad \frac{59}{-1.1} \quad \frac{5.0}{R.18/24.6}$$

$$5.0 \quad 22.6 / \frac{6.2}{R.08} \quad \frac{58}{-0.8} \quad \frac{5.3}{R.17/24.4}$$

$$5.2 \quad 23.2 / \frac{6.1}{R.11} \quad \frac{60}{-0.8} \quad \frac{5.9}{R.13/23.6}$$

$$2.8 \quad 23.2 / \frac{3.7}{R.11} \quad \frac{41}{-1.3} \quad \frac{4.2}{R.05/22.0}$$

Sta.	+	π	-	Grade
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910.87

37				079
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750				07.7
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38				07.5
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f50				07.3
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39				072
----	--	--	--	-----

450			073
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40				0.76
----	--	--	--	------

750					081
-----	--	--	--	--	-----

41				087
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T.R.	960	917.31	316	907.71
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150				09.3
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42				099
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Gr. Rod.

Lt

R

Rt.

20

20

$$23.0 / \begin{array}{r} 20 \\ 21.0 \end{array}$$

$$\begin{array}{r} 45 \\ -15 \end{array}$$

$$\begin{array}{r} 50 \\ 2000 / 21.0 \end{array}$$

22

$$23.2 / \begin{array}{r} 21 \\ 21.1 \end{array}$$

$$\begin{array}{r} 50 \\ -18 \end{array}$$

$$\begin{array}{r} 53 \\ 21 / 17.2 \end{array}$$

24

$$21.6 / \begin{array}{r} 51 \\ 20.3 \end{array}$$

$$\begin{array}{r} 40 \\ -26 \end{array}$$

$$\begin{array}{r} 58 \\ -2.4 / 17.8 \end{array}$$

26

$$22.4 / \begin{array}{r} 49 \\ 20.7 \end{array}$$

$$\begin{array}{r} 54 \\ -18 \end{array}$$

$$\begin{array}{r} 55 \\ -1.7 / 16.8 \end{array}$$

27

$$22.4 / \begin{array}{r} 50 \\ 20.7 \end{array}$$

$$\begin{array}{r} 54 \\ -17 \end{array}$$

$$\begin{array}{r} 56 \\ -1.9 / 16.8 \end{array}$$

26

$$17.4 / \begin{array}{r} 58 \\ -2.2 \end{array}$$

$$\begin{array}{r} 62 \\ -26 \end{array}$$

$$\begin{array}{r} 64 \\ -2.8 / 18.6 \end{array}$$

23

$$19.9 / \begin{array}{r} 65 \\ -2.2 \end{array}$$

$$\begin{array}{r} 72 \\ -39 \end{array}$$

$$\begin{array}{r} 67 \\ -5.4 / 19.8 \end{array}$$

28

$$17.8 / \begin{array}{r} 52 \\ -2.4 \end{array}$$

$$\begin{array}{r} 53 \\ -25 \end{array}$$

$$\begin{array}{r} 51 \\ -2.3 / 17.6 \end{array}$$

22

$$22.2 / \begin{array}{r} 36 \\ 20.6 \end{array}$$

$$\begin{array}{r} 40 \\ -1.8 \end{array}$$

$$\begin{array}{r} 39 \\ 20.3 / 21.6 \end{array}$$

20

$$22.8 / \begin{array}{r} 21 \\ 20.9 \end{array}$$

$$\begin{array}{r} 42 \\ -12 \end{array}$$

$$\begin{array}{r} 42 \\ 20.8 / 22.6 \end{array}$$

24

$$24.4 / \begin{array}{r} 77 \\ 22.17 \end{array}$$

$$\begin{array}{r} 73 \\ +0.1 \end{array}$$

$$\begin{array}{r} 66 \\ +2.8 / 26.6 \end{array}$$

Sta	+	π	-	Grade	
		917.31			
42	+50			10.5	
B.M.	303	917.35	3.03	914.28	914.32
43				11.1	
	+50			11.6	
44				12.0	
T.P.	451	918.52	3.40	913.25	
	+50			12.3	
45				12.4	
	+50			12.3	
46				12.2	
	+50			11.9	
47				11.7	
	+50			11.4	
T.P.	314	913.75	2.91	910.61	

Gr. Rod

L_t

K

R_t

$$6.8 \quad 38.0 / \frac{3.8}{+3.0} \quad \frac{9.2}{+2.6} \quad \frac{9.6}{+2.2} / 29.4$$

5 pr 125" oak 50' L_t 42+80

$$6.3 \quad 31.8 / \frac{2.9}{+2.4} \quad \frac{3.5}{+2.8} \quad \frac{4.1}{+2.2} / 29.4$$

$$5.8 \quad 30.2 / \frac{3.2}{+2.6} \quad \frac{3.8}{+2.0} \quad \frac{4.0}{+1.8} / 28.6$$

$$5.3 \quad 28.8 / \frac{3.4}{+1.9} \quad \frac{3.4}{+1.9} \quad \frac{3.5}{+1.8} / 28.6$$

$$6.2 \quad 27.8 / \frac{4.1}{+1.9} \quad \frac{4.9}{+1.8} \quad \frac{4.3}{+1.9} / 28.8$$

$$6.1 \quad 28.0 / \frac{4.6}{+1.5} \quad \frac{4.0}{+2.1} \quad \frac{3.7}{+2.4} / 29.8$$

$$6.2 \quad 27.8 / \frac{4.8}{+1.9} \quad \frac{4.2}{+2.0} \quad \frac{4.8}{+2.4} / 29.8$$

$$6.3 \quad 25.0 / \frac{5.3}{+1.0} \quad \frac{5.1}{+1.2} \quad \frac{4.2}{+1.1} / 25.0$$

$$6.6 \quad 25.0 / \frac{6.3}{+0.3} \quad \frac{6.6}{+0.0} \quad \frac{6.7}{+1.9} / 24.8$$

$$6.8 \quad 29.6 / \frac{7.0}{+0.18} \quad \frac{7.5}{+0.7} \quad \frac{7.8}{+2.0} / 23.0$$

$$7.1 \quad 24.0 / \frac{7.6}{+1.5} \quad \frac{7.8}{-0.7} \quad \frac{6.9}{+2.7} / 23.8$$

Sta + π = Grade

913.75

48 11.2

+50 10.9

49 10.7

+50 10.4

50 10.2

+50 09.9

51 09.7

+50 09.4

52 09.3

+50 09.2

T.P. 8.58 915.70 6.63 907.12

53 09.2

Gr. Rod

L

R

R_H

$$2.5 \quad 29.4 / \frac{2.9}{42.17} \quad \frac{31}{-0.6} \quad \frac{31}{42.14} / 23.8$$

$$2.8 \quad 24.8 / \frac{2.9}{42.19} \quad \frac{37}{-0.9} \quad \frac{40}{42.08} / 22.6$$

$$3.0 \quad 23.2 / \frac{3.9}{40.11} \quad \frac{44}{-1.4} \quad \frac{47}{42.03} / 21.6$$

$$3.3 \quad 23.2 / \frac{4.2}{40.11} \quad \frac{50}{-1.7} \quad \frac{53}{42.00} / 21.0$$

$$3.5 \quad 21.8 / \frac{5.1}{40.4} \quad \frac{53}{-2.0} \quad \frac{59}{-2.8} / 17.8$$

$$3.6 \quad 18.4 / \frac{6.3}{-2.7} \quad \frac{6.2}{-2.5} \quad \frac{6.0}{-2.4} / 17.8$$

$$4.0 \quad 22.6 / \frac{5.2}{42.08} \quad \frac{5.0}{-1.0} \quad \frac{4.5}{42.15} / 29.0$$

$$4.3 \quad 24.2 / \frac{6.7}{41.6} \quad \frac{4.7}{-0.9} \quad \frac{4.4}{42.10} / 24.8$$

$$4.7 \quad 22.8 / \frac{5.5}{42.09} \quad \frac{5.7}{-1.3} \quad \frac{5.4}{42.10} / 22.0$$

$$4.8 \quad 17.6 / \frac{6.8}{-2.3} \quad \frac{6.7}{-2.2} \quad \frac{6.2}{42.23} / 21.6$$

$$6.5 \quad 21.0 / \frac{8.6}{40.0} \quad \frac{8.6}{-2.1} \quad \frac{8.3}{42.02} / 21.4$$

Sta	+	X	-	Grade
		913.70		

53	150			092
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54				094
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	150			095
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55				096
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	150			098
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56				100
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	150			101
--	-----	--	--	-----

57				102
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	150			104
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58				106
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T.P.	4.49	919.65	5.54	910.16
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	150			107
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Gr. Rod

Lt.

R

Rt.

$$6.5 \quad 236 / \frac{7.2}{18.13} \quad \frac{70}{-95} \quad \frac{68}{18.17} / 24.9$$

$$6.3 \quad 234 / \frac{70}{18.13} \quad \frac{70}{-97} \quad \frac{67}{18.16} / 24.2$$

$$6.2 \quad 226 / \frac{74}{18.08} \quad \frac{72}{-10} \quad \frac{69}{18.13} / 23.6$$

$$6.1 \quad 240 / \frac{66}{18.18} \quad \frac{65}{-94} \quad \frac{64}{18.17} / 24.4$$

$$5.9 \quad 250 / \frac{51}{19.8} \quad \frac{52}{107} \quad \frac{48}{11.1} / 250$$

$$5.7 \quad 250 / \frac{49}{19.8} \quad \frac{49}{19.8} \quad \frac{45}{11.2} / 250$$

$$5.6 \quad 248 / \frac{51}{19.9} \quad \frac{53}{10.3} \quad \frac{47}{10.9} / 250$$

$$5.5 \quad 249 / \frac{58}{19.7} \quad \frac{59}{101} \quad \frac{51}{10.4} / 250$$

$$5.3 \quad 242 / \frac{57}{19.14} \quad \frac{65}{-40} \quad \frac{63}{18.09} / 21.8$$

$$5.1 \quad 23.2 / \frac{60}{18.11} \quad \frac{71}{-2.0} \quad \frac{77}{-2.0} / 18.2$$

$$4.0 \quad 244 / \frac{43}{18.17} \quad \frac{53}{-1.2} \quad \frac{58}{18.17} / 21.4$$

Sta + π - Grade

714.65

59

108

+50

11.0

+79

11.1

B.M.

2.25

710.70

910.70

Cor. Rod.

Lt

Rt

Rt

3.9

$$22.6 / \frac{5.1}{4.08}$$

$$\frac{5.1}{-1.2}$$

$$\frac{5.2}{4.07} / 22.4$$

3.7

$$21.4 / \frac{5.5}{4.07}$$

$$\frac{5.0}{-1.3}$$

$$\frac{4.9}{4.08} / 22.6$$

3.6

$$22.2 / \frac{5.0}{4.06}$$

$$\frac{4.1}{-0.5}$$

$$\frac{4.7}{4.09} / 22.8$$

Spt in Cor. N.E. Cor. Cor. Rod. 1"

