

Dr. 11A Bk 18

77-285

1090 Earl

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

-----PLAN-----Survey

-----CEMETARY ROAD-----

From Fairchild Ave To Long Lake Rd.

Road Acc't. No. 96-----

Date Filed-----

File-----

Plan Survey

Cemetery Road.

from,

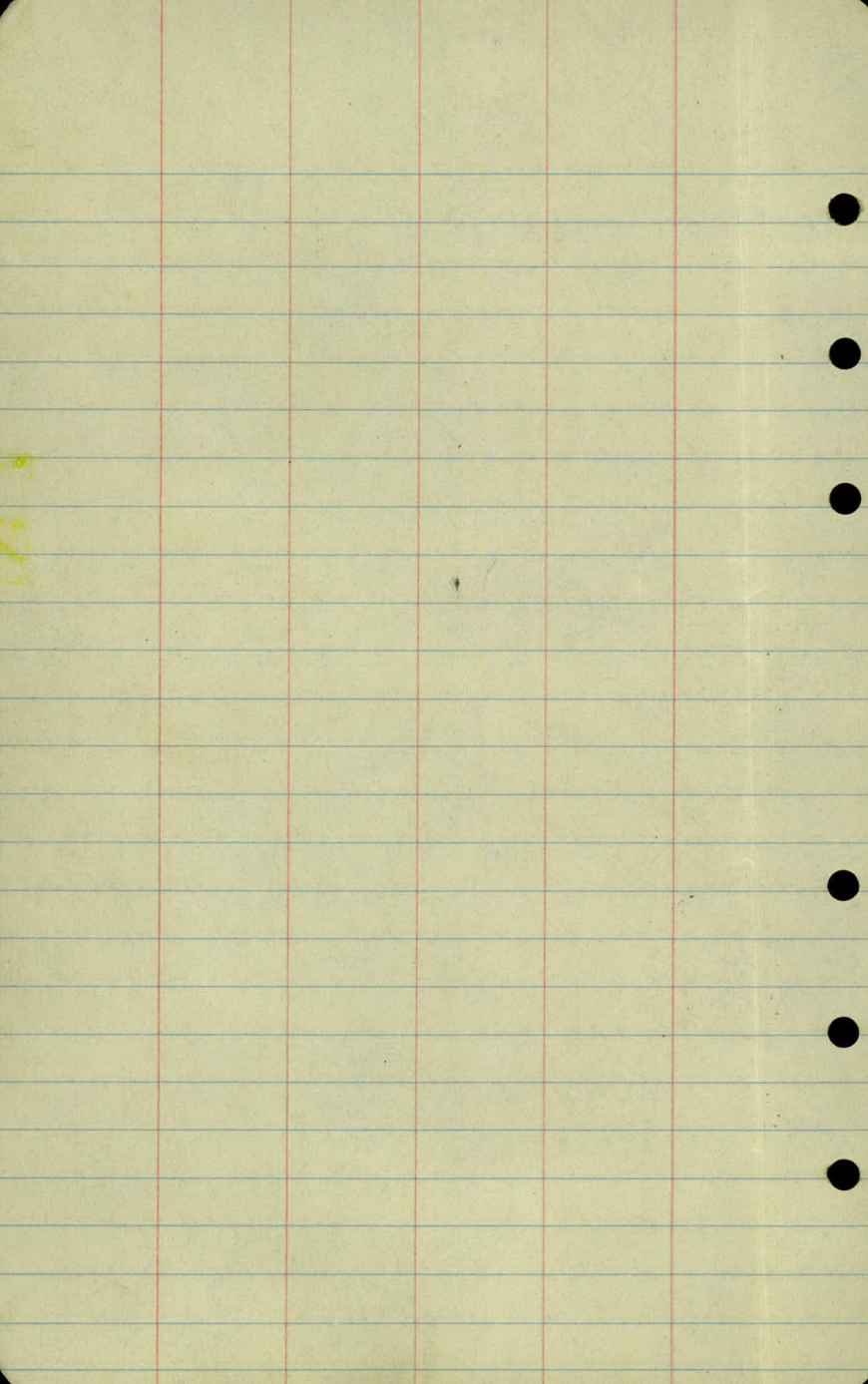
Fairchild Ave to Long Lake Rd.

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10/28/97

Wm. A. Baker.



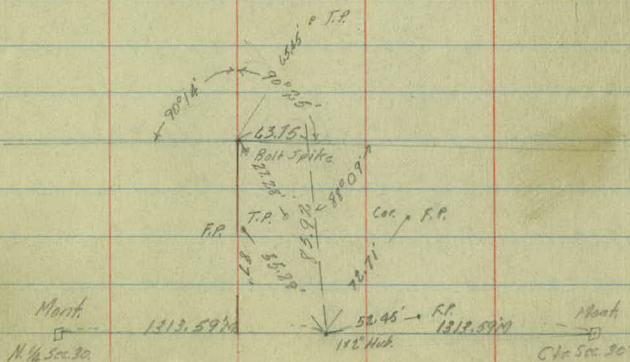
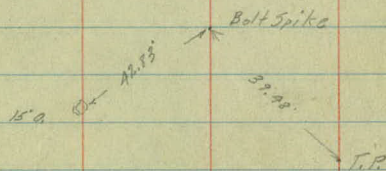
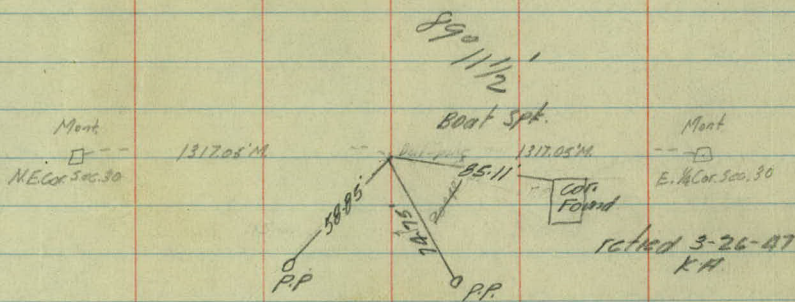
1

Alignment

25 + 57.54 P.O.T.

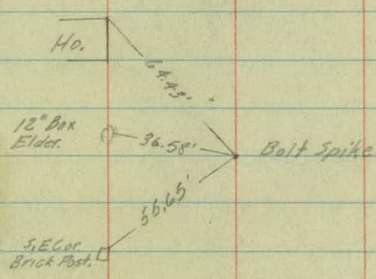
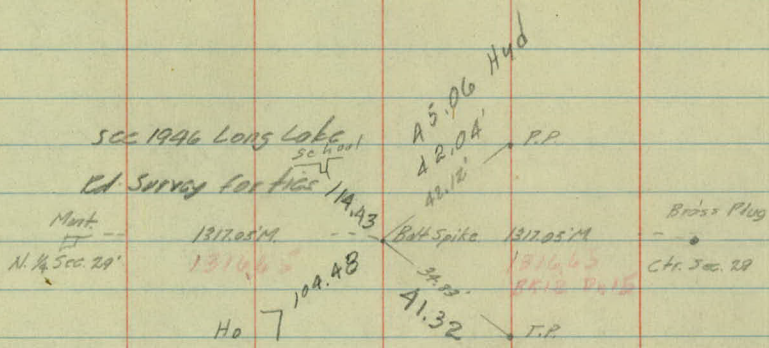
10 + 00 P.O.T.

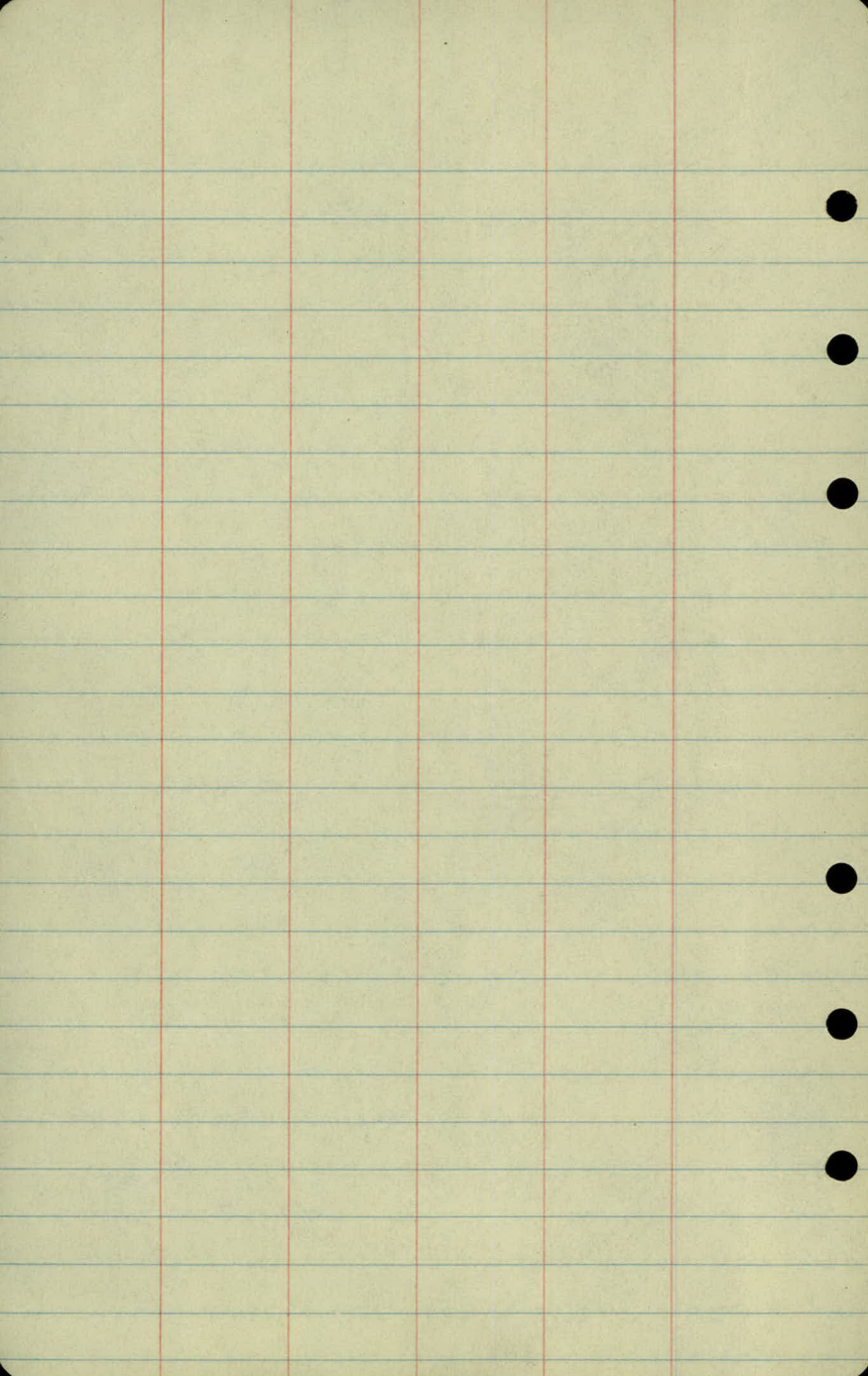
0 + 00 = ~~4~~ Fairchild Ave.



51+71.80 = to Long Lake Rd

42+01.71 P.O.T.





Topography

6

5

too 24' X 62' P₂

4

3

2

1

0+00

412 Rd. 43'

13

12

11

10

9

8

7

+85 T.P. 22'

+57 F.C. 34'

+45 Ext. 15" x 20" C.M. 16'

+45 Beg F.C. 38'

+41 T.P. 21'

F.C. 32'

+11 T.P. 27'

Pasture

F.C. 35'

+71 T.P. 27'

+64-15" O. 31'

+28 Ext. 15" x 20" C.M. 16'

+22 T.P. 28'

F.C. 36'

11'

11'

11'

9'

20

19

18

17

16

15

14

Cult.

Cult.

+23 T.P. 28'

+67 Fc. Cor. 34'

Fc. 34'

+86 T.P. 25'

+97 Fc. Cor. 35'

Fc. 29'

+102 T.P. 22'

Fc. 34'

+805 End Pot hole 20'

+55 Pot hole 55'

+92 Pot hole 25'-60'

+29 T.P. 20'

Fc. 31'

Fc. 23'

+95 End Pot hole 23' 55'

+45 Fc. 21'

+17-15" W.H. 33'

Fc. 22' Beg. Pot hole 22'

Fc. 31'

+66 Kangaroo

+48 R.O. Fc. Cor. 32'

+31 Fc. 22'

Water

Water

Pasture

27

26

25

24

101 - 24° 14' 11" P 8

23

22

21

Waste land

+99 T.P. 30'

+01 F.C. Cor 35'

+75 T.P. 29'

+88 Ent. 15" x 24" C.M. 19'

+41 T.P. 30'

End Cul. 31'

+01 End Cul. 25'
F.C. 32'

+01 T.P. 29'

Cult

F.C. 31'

+87 Ent. 12" x 24" C.M. 20'

+67 T.P. 25'

34

33

32

31

+02 k Gulu 30° 150° E. M.

30

29

28

Cult.

+28 T.P. 27'

Brush 27'

Fc. 48' Brush 28'

+90 T.P. 28'

Geo. Bush 25'

+23 Fc. Cor. 40

+98 T.P. 28'

+02 Cul. 24'

+02 Cul. 26'

+99 T.P. 28'

Cult.

+40 T.P. 29'

41

40

39

38

37

36

35

+99 Ent. 15" x 20" C.M. 17'
+87-12" O. 2.5'

+89 E. St.
15" x 20" C.M. 18' 10

+55 S.E. Cor. 2x2 Brick Post 30.7' X

+81 S.E. Cor. 2x2 Brick Post 30.7
+71 Ent. 15" x 20" C.M. 17'
+62 S.W. Cor. 2x2 Brick Post 30.7'

+77 S.E. Cor. 2' x 15' Brick Post 30.7
+98 Ent. 15" x 20" C.M. 18'
+99 S.W. Cor. 2' x 15' Brick Post 30.7'

Cemetery

Wire Mesh F.C.
+67-2x2 Brick Cor. Post 30'
+58 Ent. 15" x 20" C.M. 18'

+54 N.E. Cor. 4x4
+49 T.P. 29'
+41 Ent. 12" x 20" C.M. 19'
+34 S.W. Cor. 4x4

+90 T.P. 28'
+70 E. St.

+37 T.P. 28'

+92 Ent. 15" x 20" C.M. 17'

+15 No. 110'

+82 T.P. 28'

+30 End Brush 27'

48

47

46

45

44

43

42

+46 St. 12" K50C.M. 19'

+17 P.P. 26

+11 T.P. 29'



+82 R.E. Cor. No. 40

+60 N.W. Cor. No. 40

+69 T.P. 29'

+60 P.P. 26'

+55 Ent. 12" K50C.M. 17'

+14 T.P. 28'

 P.P. 26'
 +95 Ent. 15" K50C.M. 18'


+63 P.P. 26'

+56 T.P. 29'

+59 N.W. Cor. No. 70'

+80 Ent. 15" K50C.M. 17'

+28 Row 12" Trees 25'

+16 S.E. Cor. No. 48'

+02 Ent. 15" K50C.M. 17'

+75 S.W. Cor. No. 48'

+83 End Wood Picket Fg. 22'



+99 S.E. Cor. No. 48'



+19 S.W. Cor. No. 50'

+07 Beg Wood Picket Fg. 23'

+13 P.P. T.P. 26'

52

132.2 G/Lv. 24" X 42" P/E

51

50

49

+64 Rdwy of height 12'

+72 Cdn 21'

+20 B.E. Can No 38'

+65 S.W. Can No 78'

+32 Ent



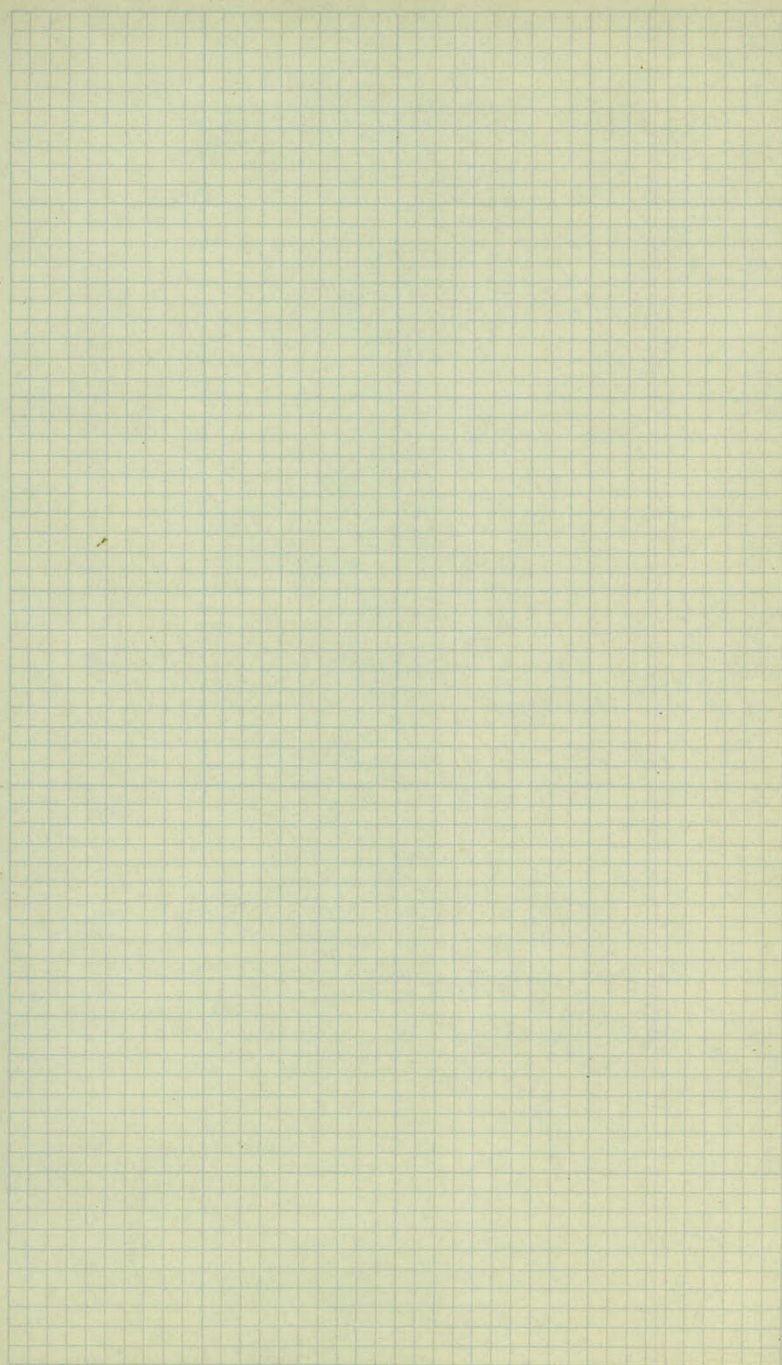
+52 P.P. T.P. 29'

+32 Cdn 22'

+04 P.P. T.P. 20'

+81 P.P. 26'

+60 T.P. 29'



Bench Levels.

	+	-	Elev	
B.M.	1.86	987.06	974.56	985.20
T.P.	0.35	974.91	974.76	
T.P.	0.12	961.75	13.28	961.63
T.P.	0.27	949.77	12.25	949.50
T.P.	0.11	937.33	12.55	937.22
B.M.	0.51	928.41	9.43	927.90
T.P.	0.52	915.77	13.16	915.25
T.P.	0.12	902.60	13.29	902.48
T.P.	4.09	893.30	13.39	889.21
B.M.	3.17	893.20	3.17	890.13
T.P.	13.07	899.74	6.63	886.67
T.P.	12.78	912.17	0.35	899.39
T.P.	12.84	924.63	0.38	911.79
B.M.	5.71	924.63	5.71	918.92
T.P.	1.51	921.90	4.24	920.39
T.P.	3.15	914.09	10.96	910.94
B.M.			7.33	906.76

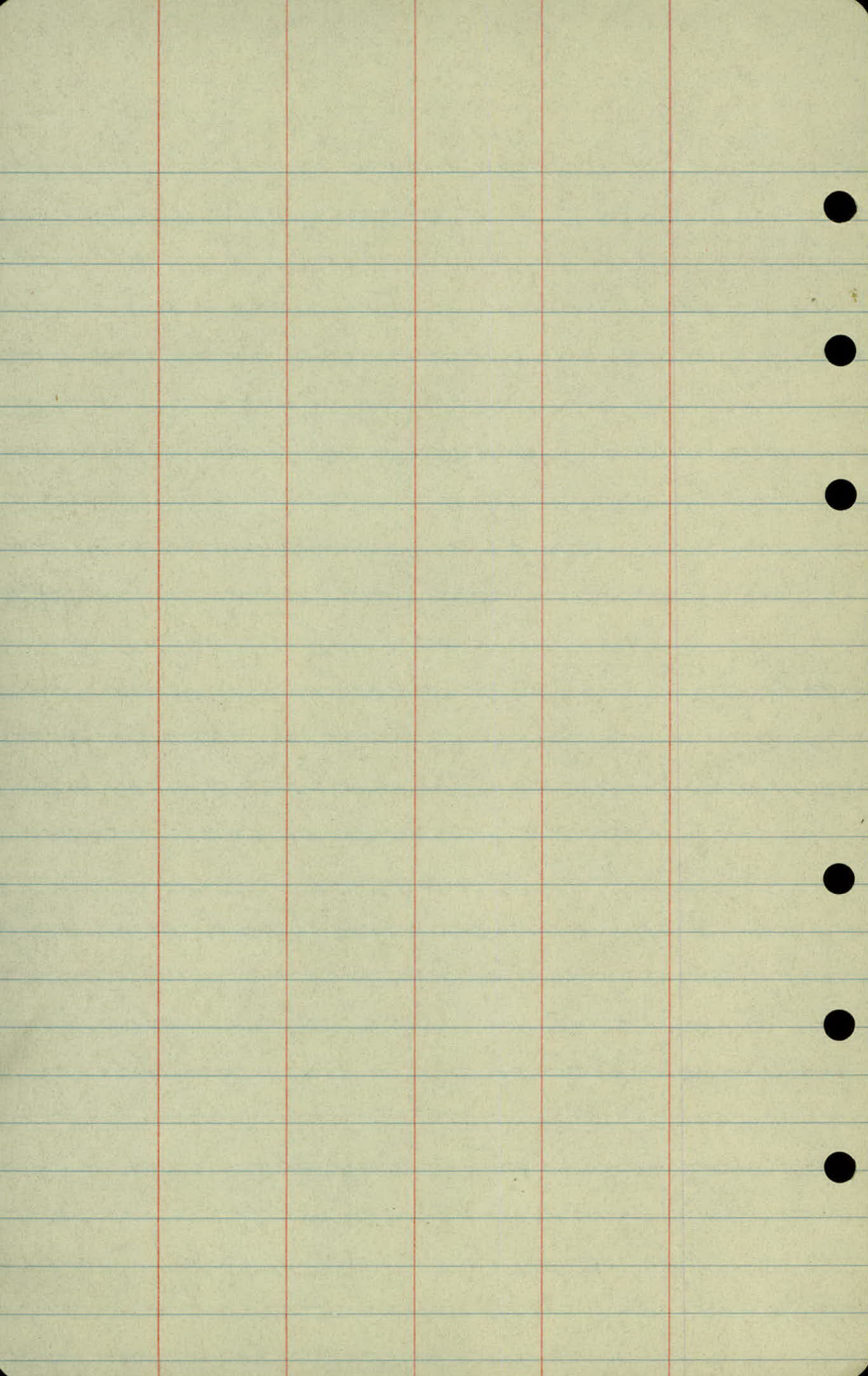
Spike in T.P. 25' Rt 0+61

Spike in 15" O. ht. 14+50

Spike 12" 50' Rt 27+95

Spike in Tw. Cuth. 38' ht. 40+17

Spike in R.P. 25' S.E. 51+71.80



X Sections.

Sta	+	π	-	Elev
B.M.	11.43	996.63		985.20
0+00				91.1
+13				90.4
+17				90.0
+37				88.0
+75				84.5
I.P.	11.3	989.77	12.99	983.61
1				82.2
+50				77.5
+75				75.3
I.P.	0.53	978.50	11.80	972.97
2				73.0
+50				68.7
+75				66.7

Lt

%

Rt

R.R. Spikes in T.P. 27' Rt. 0+61

11.1	7.5	55	43	37
100	50	—	50	100

80	80	62	53	49
50	74	—	39	50

89.93	83	66	69	74	71
50	42	33	30	42	50

1.0	2.4
138	150

16.8	122	8.2	24	0.6	00	63	76	106	94	85	86	91	101	104	68	21	29	4.0	37	2.1
150	125	100	72	50	42	40	56	23	16	4	—	16	22	27	36	37	50	67	83	100

11.0
150

170	121	103	73	68	136	145	126	121	125	139	140	79	97	103	126	125	11.1
125	100	87	50	42	30	23	14	00	12	17	27	34	50	55	82	100	125

1.5	0.6	46	55	48	31	26	30	41	44	35	51
50	36	30	24	20	15	11	17	29	33	50	

95	109	123	127	73	73	80	153	152	157
50	89	33	24	14	—	13	26	36	50

120	128	145	149	101	95	101	175	182	182
50	40	34	22	14	—	12	24	37	50

19	25	54	51	10	05	10	71	81	78	78
50	38	28	22	15	—	16	23	32	42	50

82	70	69	81	76	50	48	54	98	65	71	74
50	36	29	26	19	15	—	12	24	30	41	50

110	98	96	105	98	73	68	73	116	113	88	77	71
50	37	30	26	20	14	—	12	23	27	31	39	50

Sta	+	T	-	Elev
		973.50		
3400				64.8
+30				62.8
T.P.	0.17	✓ 960.50	13.17	960.33 ✓
+70				60.5
4				59.1
+50				57.3
5				56.1
+35				55.9
+60				55.9
6				56.2
T.P.	5.33	✓ 961.89	2.94	956.56 ✓
+28				56.5
+80				57.1

Lt

X

Rt

$\frac{116}{50}$	$\frac{98}{32}$	$\frac{120}{28}$	$\frac{116}{19}$	$\frac{91}{14}$	$\frac{87}{12}$	$\frac{93}{23}$	$\frac{130}{22}$	$\frac{133}{26}$	$\frac{104}{31}$	$\frac{83}{37}$	$\frac{81}{45}$	$\frac{75}{50}$
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$\frac{140}{50}$	$\frac{138}{41}$	$\frac{126}{35}$	$\frac{148}{28}$	$\frac{148}{21}$	$\frac{110}{13}$	107	$\frac{119}{12}$	$\frac{151}{20}$	$\frac{150}{25}$	$\frac{94}{35}$	$\frac{92}{42}$	$\frac{83}{50}$
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$\frac{73}{50}$	$\frac{66}{14}$	$\frac{65}{25}$	$\frac{95}{13}$	$\frac{90}{19}$	$\frac{98}{9}$	$\frac{50}{19}$	$\frac{53}{28}$	$\frac{34}{35}$	$\frac{19}{50}$
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$\frac{112}{50}$	$\frac{115}{37}$	$\frac{95}{26}$	$\frac{19}{14}$	$\frac{19}{12}$	$\frac{19}{21}$	$\frac{51}{32}$	$\frac{84}{36}$	$\frac{74}{36}$	$\frac{61}{50}$
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$\frac{159}{50}$	$\frac{156}{39}$	$\frac{140}{30}$	$\frac{39}{19}$	$\frac{32}{12}$	$\frac{37}{12}$	$\frac{119}{29}$	$\frac{119}{37}$	$\frac{108}{50}$
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$\frac{158}{50}$	$\frac{142}{33}$	$\frac{50}{14}$	$\frac{44}{12}$	$\frac{47}{31}$	$\frac{150}{31}$	$\frac{137}{50}$
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$\frac{127}{50}$	$\frac{125}{34}$	$\frac{62}{26}$	$\frac{52}{15}$	$\frac{46}{13}$	$\frac{55}{25}$	$\frac{127}{32}$	$\frac{135}{32}$	$\frac{130}{50}$
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$\frac{66}{50}$	$\frac{68}{42}$	$\frac{83}{37}$	$\frac{57}{27}$	$\frac{53}{16}$	$\frac{46}{13}$	$\frac{53}{26}$	$\frac{124}{33}$	$\frac{130}{38}$	$\frac{120}{50}$
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$\frac{60}{40}$	$\frac{45}{14}$	$\frac{43}{14}$	$\frac{47}{12}$	$\frac{79}{19}$	$\frac{79}{23}$	$\frac{86}{29}$	$\frac{71}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{62}{27}$	$\frac{19}{24}$	$\frac{19}{20}$	$\frac{59}{14}$	$\frac{54}{12}$	$\frac{56}{12}$	$\frac{77}{18}$	$\frac{77}{21}$	$\frac{57}{27}$	$\frac{50}{31}$	$\frac{40}{50}$
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$\frac{23}{26}$	$\frac{45}{22}$	$\frac{52}{16}$	$\frac{52}{13}$	$\frac{48}{13}$	$\frac{55}{13}$	$\frac{68}{16}$	$\frac{65}{19}$	$\frac{38}{24}$
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Sta	+	X	-	Elev
		961.89		

7				57.2
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	+50			57.3
--	-----	--	--	------

8				56.9
---	--	--	--	------

	+65			55.6
--	-----	--	--	------

T.P.	14.14	959.63	6.40	953.49
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6	+28			56.5
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	+80			57.1
--	-----	--	--	------

7				57.2
---	--	--	--	------

	+50			57.3
--	-----	--	--	------

8				56.9
---	--	--	--	------

T.P.	3.03	958.52	14.14	953.49
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9				54.7
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	+92			53.6
--	-----	--	--	------

Lt

E

Rt

$$\frac{17}{27} \frac{17}{21} \frac{52}{16} \frac{50}{13} \frac{41}{14} \frac{53}{16} \frac{66}{19} \frac{60}{28} \frac{12}{29}$$

$$\frac{38}{26} \frac{59}{19} \frac{60}{17} \frac{51}{14} \frac{46}{12} \frac{52}{17} \frac{76}{22} \frac{72}{22} \frac{26}{29}$$

$$\frac{59}{25} \frac{67}{18} \frac{56}{13} \frac{50}{13} \frac{56}{19} \frac{84}{19} \frac{82}{25} \frac{28}{30} \frac{17}{50}$$

$$\frac{54}{50} \frac{57}{40} \frac{55}{33} \frac{83}{28} \frac{81}{18} \frac{67}{14} \frac{63}{13} \frac{66}{18} \frac{93}{19} \frac{90}{25} \frac{49}{31} \frac{55}{37} \frac{68}{50}$$

$$\frac{81}{50} \frac{80}{33}$$

-13.1

$$\frac{56}{50} \frac{33}{34}$$

-12.5

$$\frac{23}{33} \frac{30}{50}$$

$$\frac{56}{50} \frac{30}{39}$$

-12.4

$$\frac{21}{33} \frac{31}{50}$$

$$\frac{74}{50} \frac{56}{38}$$

-12.3

$$\frac{60}{31} \frac{56}{50}$$

$$\frac{85}{50} \frac{76}{32}$$

-12.7

$$\frac{33}{50} \frac{52}{39} \frac{28}{32} \frac{63}{25} \frac{62}{20} \frac{40}{14} \frac{38}{13} \frac{43}{19} \frac{62}{24} \frac{62}{31} \frac{14}{36} \frac{13}{50} \frac{16}{50}$$

$$\frac{46}{50} \frac{39}{40} \frac{31}{32} \frac{75}{26} \frac{78}{21} \frac{52}{15} \frac{49}{12} \frac{54}{18} \frac{79}{22} \frac{80}{26} \frac{60}{31} \frac{15}{31} \frac{18}{50}$$

Sta	+	T	-	Elev
		958.52		
10				51.4
	+95			49.2
	+80			47.3
11				46.2
	+55			43.0
12				40.2
T.P.	1.25	946.23	13.54	944.98
11	+55			43.0
12				40.2
T.P.	3.66	939.94	9.95	936.28
	+40			37.8
	+20			35.9
12				34.0

L.T.

E

R.T.

$$\frac{146}{50} \quad \frac{134}{25} \quad \frac{78}{15} \quad \frac{7.1}{-} \quad \frac{76}{12} \quad \frac{106}{18} \quad \frac{105}{25} \quad \frac{66}{31} \quad \frac{52}{36} \quad \frac{46}{50}$$

$$\frac{100}{50} \quad \frac{105}{31} \quad \frac{125}{26} \quad \frac{125}{21} \quad \frac{99}{14} \quad \frac{93}{13} \quad \frac{99}{19} \quad \frac{119}{24} \quad \frac{121}{30} \quad \frac{78}{35} \quad \frac{64}{50} \quad \frac{54}{50}$$

$$\frac{66}{50} \quad \frac{67}{31} \quad \frac{109}{27} \quad \frac{133}{22} \quad \frac{132}{17} \quad \frac{112}{13} \quad \frac{112}{-} \quad \frac{119}{14} \quad \frac{137}{19} \quad \frac{155}{29} \quad \frac{92}{30} \quad \frac{98}{50}$$

$$\frac{68}{50} \quad \frac{61}{32} \quad \frac{106}{28} \quad \frac{140}{22} \quad \frac{141}{18} \quad \frac{129}{15} \quad \frac{123}{-} \quad \frac{129}{14} \quad \frac{142}{18} \quad \frac{102}{22} \quad \frac{93}{30} \quad \frac{105}{38} \quad \frac{126}{50}$$

$$\frac{84}{50} \quad \frac{77}{32}$$

-15.5

$$\frac{79}{30} \quad \frac{96}{50}$$

$$\frac{11.5}{50} \quad \frac{116}{32}$$

-18.3

$$\frac{42}{22} \quad \frac{46}{16} \quad \frac{37}{14} \quad \frac{32}{-} \quad \frac{38}{14} \quad \frac{48}{17} \quad \frac{4.8}{19} \quad \frac{23}{23}$$

$$\frac{73}{21} \quad \frac{72}{17} \quad \frac{62}{14} \quad \frac{60}{-} \quad \frac{67}{14} \quad \frac{77}{16} \quad \frac{72}{20} \quad \frac{59}{24} \quad \frac{20}{28} \quad \frac{47}{50}$$

No. 1 in T.P. 12+40

$$\frac{41.8}{50} \quad \frac{00}{41} \quad \frac{06}{32} \quad \frac{36}{26} \quad \frac{36}{18} \quad \frac{24}{15} \quad \frac{21}{-} \quad \frac{27}{13} \quad \frac{40}{16} \quad \frac{51}{31} \quad \frac{57}{50}$$

$$\frac{33}{50} \quad \frac{51}{39} \quad \frac{68}{25} \quad \frac{69}{22} \quad \frac{43}{14} \quad \frac{40}{-} \quad \frac{47}{14} \quad \frac{67}{18} \quad \frac{68}{31} \quad \frac{67}{50}$$

$$\frac{75}{50} \quad \frac{87}{34} \quad \frac{108}{30} \quad \frac{99}{22} \quad \frac{64}{14} \quad \frac{59}{-} \quad \frac{64}{14} \quad \frac{73}{17} \quad \frac{72}{27} \quad \frac{62}{31} \quad \frac{60}{50}$$

Sta	+	7.	-	Elev
		939.94		
13	+50			30.9
14				27.9
	+55			24.6
B.M.	0.22	928.97	11.99	921.95
14	+55			24.6
15				22.1
	+50			19.3
17	+40			13.4
	+70			12.5
18				11.6
	+50			09.4
19				07.3
T.P.	2.12	918.85	12.14	916.73

Lt.

Q

Rt.

$\frac{90}{50}$	$\frac{102}{33}$	$\frac{111}{31}$	$\frac{106}{18}$	$\frac{96}{14}$	$\frac{90}{13}$	$\frac{93}{15}$	$\frac{105}{19}$	$\frac{108}{21}$	$\frac{98}{33}$	$\frac{81}{33}$	$\frac{73}{50}$
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$\frac{142}{50}$	$\frac{130}{26}$	$\frac{135}{24}$	$\frac{134}{18}$	$\frac{123}{14}$	$\frac{120}{13}$	$\frac{124}{15}$	$\frac{139}{20}$	$\frac{135}{22}$	$\frac{118}{31}$	$\frac{104}{31}$	$\frac{74}{50}$
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15.3

$\frac{88}{31}$	$\frac{5.8}{50}$
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Spike in 15° Q. Lt. 14+50

$\frac{38}{50}$	$\frac{24}{30}$	$\frac{62}{23}$	$\frac{62}{18}$	$\frac{46}{14}$	$\frac{43}{13}$	$\frac{44}{13}$	$\frac{59}{16}$	$\frac{56}{21}$
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$\frac{70}{50}$	$\frac{60}{31}$	$\frac{99}{25}$	$\frac{96}{21}$	$\frac{75}{15}$	$\frac{68}{13}$	$\frac{69}{16}$	$\frac{82}{22}$	$\frac{83}{22}$	$\frac{92}{29}$	$\frac{24}{35}$	$\frac{0.8}{50}$
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$\frac{130}{50}$	$\frac{136}{35}$	$\frac{146}{32}$	$\frac{145}{29}$	$\frac{10.2}{14}$	$\frac{9.6}{14}$
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$\frac{102}{14}$	$\frac{140}{21}$	$\frac{15.5}{35}$	$\frac{12.6}{50}$
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15.5

$\frac{96}{30}$	$\frac{7.5}{37}$	$\frac{7.5}{50}$
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$\frac{15.8}{50}$	$\frac{126}{26}$
-------------------	------------------

16.4

$\frac{8.2}{31}$	$\frac{6.9}{36}$	$\frac{6.6}{50}$
------------------	------------------	------------------

$\frac{14.2}{50}$	$\frac{114}{33}$	$\frac{11.5}{29}$
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17.3

$\frac{71}{32}$	$\frac{6.2}{39}$	$\frac{6.7}{50}$
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19.5

$\frac{50}{33}$	$\frac{80}{38}$	$\frac{9.7}{50}$
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21.6

$\frac{132}{33}$	$\frac{12.2}{38}$	$\frac{13.3}{50}$
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Sta.	+	Δ	-	Elev
		918.85		
16				17.2
	+40			15.8
	+70			15.0
17				14.2
	+40			13.4
	+70			12.5
18				11.6
	+50			09.4
19				07.3
	+50			05.0
20				02.4
T.P.	0.49	905.86	13.48	905.37

Lt

R

Rt

$$\frac{58}{50} \quad \frac{85}{45} \quad \frac{87}{29} \quad \frac{77}{22} \quad \frac{24}{13} \quad \frac{17}{12} \quad \frac{22}{24} \quad \frac{84}{50} \quad \frac{87}{50}$$

$$\frac{99}{50} \quad \frac{100}{23} \quad \frac{87}{21} \quad \frac{35}{14} \quad \frac{31}{12} \quad \frac{34}{22} \quad \frac{94}{22} \quad \frac{94}{50}$$

$$\frac{105}{50} \quad \frac{113}{33} \quad \frac{102}{23} \quad \frac{87}{21} \quad \frac{44}{14} \quad \frac{39}{13} \quad \frac{42}{24} \quad \frac{94}{32} \quad \frac{105}{40} \quad \frac{95}{50} \quad \frac{69}{50}$$

$$\frac{100}{50} \quad \frac{92}{30} \quad \frac{82}{20} \quad \frac{50}{13} \quad \frac{47}{13} \quad \frac{48}{18} \quad \frac{75}{21} \quad \frac{75}{23} \quad \frac{66}{33} \quad \frac{54}{39} \quad \frac{42}{39} \quad \frac{25}{50}$$

$$\frac{80}{50} \quad \frac{57}{28} \quad \frac{43}{29} \quad \frac{76}{19} \quad \frac{75}{16} \quad \frac{60}{13} \quad \frac{55}{13} \quad \frac{58}{13} \quad \frac{78}{16} \quad \frac{76}{19}$$

$$\frac{79}{18} \quad \frac{79}{16} \quad \frac{67}{14} \quad \frac{69}{13} \quad \frac{66}{13} \quad \frac{82}{16} \quad \frac{81}{18}$$

$$\frac{85}{18} \quad \frac{87}{16} \quad \frac{77}{14} \quad \frac{73}{13} \quad \frac{76}{13} \quad \frac{91}{16} \quad \frac{90}{18}$$

$$\frac{65}{50} \quad \frac{40}{35} \quad \frac{39}{29} \quad \frac{110}{19} \quad \frac{110}{17} \quad \frac{98}{14} \quad \frac{95}{13} \quad \frac{96}{13} \quad \frac{113}{16} \quad \frac{111}{19}$$

$$\frac{86}{50} \quad \frac{58}{34} \quad \frac{110}{36} \quad \frac{120}{21} \quad \frac{121}{19} \quad \frac{120}{17} \quad \frac{116}{14} \quad \frac{121}{14} \quad \frac{136}{17} \quad \frac{137}{19}$$

$$\frac{12.9}{50} \quad \frac{10.0}{27}$$

13.9

$$\frac{7.2}{50} \quad \frac{6.3}{35} \quad \frac{9.0}{50}$$

16.5

$$\frac{12.8}{27} \quad \frac{11.5}{34} \quad \frac{11.6}{50}$$

Sta	+	X	-	Elev
		905.86		
19	+50			905.0
20				02.4
	+50			99.5
21				96.9
	+50			94.4
BM	1.84	898.64	13.46	898.40
22				92.2
	+50			89.7
23				87.9
	+50			86.7
	+85			86.2
24				86.1

Lt R Rt

$\frac{2.5}{19}$ $\frac{2.7}{16}$ $\frac{1.9}{13}$ $\frac{0.9}{14}$ $\frac{1.2}{16}$ $\frac{2.7}{19}$ $\frac{2.9}{19}$

$\frac{4.5}{50}$ $\frac{5.3}{23}$ $\frac{5.2}{19}$ $\frac{5.1}{16}$ $\frac{4.2}{14}$ $\frac{3.5}{13}$ $\frac{3.2}{13}$ $\frac{4.5}{14}$ $\frac{4.7}{20}$

$\frac{8.2}{50}$ $\frac{7.3}{31}$ $\frac{6.3}{22}$ $\frac{8.0}{19}$ $\frac{7.5}{15}$ $\frac{6.7}{14}$ $\frac{6.4}{14}$ $\frac{6.8}{14}$ $\frac{8.1}{17}$ $\frac{8.2}{19}$ $\frac{6.1}{22}$ $\frac{5.0}{33}$ $\frac{4.5}{50}$

$\frac{11.8}{50}$ $\frac{11.2}{30}$ $\frac{11.0}{17}$ $\frac{9.2}{14}$ $\frac{9.0}{13}$ $\frac{9.7}{13}$ $\frac{10.6}{14}$ $\frac{11.5}{31}$ $\frac{10.8}{35}$ $\frac{11.0}{50}$

$\frac{14.5}{50}$ $\frac{14.7}{31}$ $\frac{14.3}{18}$ $\frac{11.9}{14}$ $\frac{11.5}{13}$ $\frac{11.2}{13}$ $\frac{15.6}{22}$ $\frac{15.7}{31}$ $\frac{14.9}{34}$ $\frac{15.1}{50}$

R.R. Spike in T.P.Rt. 21461

$\frac{4.5}{50}$ $\frac{4.9}{41}$ $\frac{4.2}{23}$ $\frac{4.6}{22}$ $\frac{4.6}{20}$ $\frac{1.8}{13}$ $\frac{1.4}{14}$ $\frac{1.9}{14}$ $\frac{4.8}{20}$ $\frac{4.9}{22}$ $\frac{5.9}{50}$

$\frac{7.2}{30}$ $\frac{7.9}{32}$ $\frac{7.0}{20}$ $\frac{4.3}{14}$ $\frac{3.9}{14}$ $\frac{9.0}{14}$ $\frac{6.9}{18}$ $\frac{6.5}{25}$ $\frac{5.2}{27}$ $\frac{5.2}{50}$

$\frac{8.9}{50}$ $\frac{9.5}{32}$ $\frac{9.5}{20}$ $\frac{6.0}{14}$ $\frac{5.7}{14}$ $\frac{6.0}{14}$ $\frac{6.6}{19}$ $\frac{6.7}{24}$ $\frac{6.5}{32}$ $\frac{6.7}{50}$

$\frac{10.1}{50}$ $\frac{10.7}{31}$ $\frac{10.4}{21}$ $\frac{7.4}{18}$ $\frac{6.9}{13}$ $\frac{7.9}{13}$ $\frac{11.8}{22}$ $\frac{12.1}{35}$ $\frac{10.8}{50}$

$\frac{10.8}{50}$ $\frac{10.9}{41}$ $\frac{12.5}{33}$ $\frac{12.1}{21}$ $\frac{7.9}{18}$ $\frac{7.4}{18}$ $\frac{7.8}{12}$ $\frac{14.0}{23}$ $\frac{14.0}{35}$ $\frac{13.6}{50}$

$\frac{11.1}{50}$ $\frac{12.3}{38}$ $\frac{12.9}{21}$ $\frac{8.0}{12}$ $\frac{7.5}{14}$ $\frac{8.3}{14}$ $\frac{12.7}{23}$ $\frac{13.8}{38}$ $\frac{13.6}{50}$

Sta	+	π	-	Elev
		893.64		
24	+50			86.3
25				87.4
	+50			89.0
T.P.	10.20	899.89	3.95	899.69
26				89.7
	+50			89.7
27				88.8
	+09			88.5
	+18			88.2
	+30			87.8
	+70			86.1
	+85			85.3
T.P.	1.50	982.97	13.42	986.47

Lt.

L

Rt.

$$\frac{10.5}{50} \quad \frac{10.8}{21} \quad \frac{7.6}{13} \quad \frac{7.3}{14} \quad \frac{7.7}{14} \quad \frac{11.2}{21} \quad \frac{11.5}{33} \quad \frac{11.6}{50}$$

$$\frac{6.7}{50} \quad \frac{6.9}{23} \quad \frac{7.6}{19} \quad \frac{7.8}{16} \quad \frac{6.6}{13} \quad \frac{6.2}{14} \quad \frac{6.5}{14} \quad \frac{7.5}{18} \quad \frac{7.8}{23} \quad \frac{7.3}{25} \quad \frac{8.3}{50}$$

$$\frac{1.4}{50} \quad \frac{1.4}{32} \quad \frac{0.3}{26} \quad \frac{5.5}{19} \quad \frac{6.1}{16} \quad \frac{5.0}{13} \quad \frac{4.6}{14} \quad \frac{4.9}{14} \quad \frac{6.0}{16} \quad \frac{5.9}{20} \quad \frac{2.0}{25} \quad \frac{1.6}{34} \quad \frac{8.3}{50}$$

$$\frac{3.8}{50} \quad \frac{2.9}{34} \quad \frac{2.5}{29} \quad \frac{9.1}{20} \quad \frac{10.6}{14} \quad \frac{10.2}{14} \quad \frac{10.5}{12} \quad \frac{11.5}{16} \quad \frac{11.3}{19} \quad \frac{4.0}{28} \quad \frac{4.1}{50}$$

$$\frac{3.6}{50} \quad \frac{3.3}{36} \quad \frac{2.5}{31} \quad \frac{9.0}{21} \quad \frac{10.5}{14} \quad \frac{10.2}{14} \quad \frac{10.6}{14} \quad \frac{11.4}{15} \quad \frac{11.5}{19} \quad \frac{4.2}{29} \quad \frac{5.0}{50}$$

11.1

$$\frac{4.9}{50} \quad \frac{4.1}{29} \quad \frac{11.5}{19} \quad \frac{12.1}{17} \quad \frac{12.3}{14} \quad \frac{11.7}{13} \quad \frac{11.4}{14} \quad \frac{11.3}{12} \quad \frac{12.7}{15} \quad \frac{12.3}{19} \quad \frac{4.4}{29} \quad \frac{4.3}{50}$$

$$\frac{14.2}{50} \quad \frac{12.3}{35} \quad \frac{10.8}{26} \quad \frac{13.0}{18} \quad \frac{13.0}{16} \quad \frac{12.0}{13} \quad \frac{11.7}{14} \quad \frac{12.2}{12} \quad \frac{13.0}{16} \quad \frac{12.8}{19} \quad \frac{9.3}{26} \quad \frac{4.4}{29} \quad \frac{4.3}{50}$$

$$\frac{17.5}{50} \quad \frac{16.0}{46} \quad \frac{12.7}{23} \quad \frac{13.6}{19} \quad \frac{13.4}{15} \quad \frac{12.5}{13} \quad \frac{12.1}{14} \quad \frac{12.6}{14} \quad \frac{13.8}{17} \quad \frac{13.6}{20} \quad \frac{9.3}{26} \quad \frac{10.4}{50}$$

$$\frac{20.8}{50} \quad \frac{14.8}{27} \quad \frac{15.7}{20} \quad \frac{15.3}{16} \quad \frac{14.2}{14} \quad \frac{13.8}{14} \quad \frac{14.2}{12} \quad \frac{14.9}{15} \quad \frac{14.7}{20} \quad \frac{11.9}{27} \quad \frac{11.6}{41} \quad \frac{12.8}{50}$$

14.6

$$\frac{7.4}{27} \quad \frac{8.2}{50}$$

Sta	+	Δ	-	Elev
		987.97		
27 + 85				85.3
28				84.6
+20				83.6
+45				82.3
29				79.9
+50				78.3
30				77.6
+50				77.6
31				78.3
+02		to Ditch		
+60				79.3

Lt.

K

Rt.

$$\frac{44}{50} \quad \frac{18}{29} \quad \frac{43}{19} \quad \frac{43}{16} \quad \frac{32}{13} \quad \frac{27}{14} \quad \frac{30}{19} \quad \frac{41}{16} \quad \frac{42}{19}$$

34

$$\frac{6.1}{50} \quad \frac{6.2}{21} \quad \frac{6.2}{17} \quad \frac{8.7}{13} \quad \frac{4.8}{14} \quad \frac{4.7}{14} \quad \frac{5.8}{16} \quad \frac{5.7}{20} \quad \frac{4.8}{22} \quad \frac{6.5}{50}$$

$$\frac{8.1}{50} \quad \frac{8.8}{19} \quad \frac{5.9}{14} \quad \frac{5.7}{14} \quad \frac{5.8}{13} \quad \frac{7.1}{16} \quad \frac{6.8}{21} \quad \frac{5.8}{31} \quad \frac{8.8}{30}$$

$$\frac{10.0}{50} \quad \frac{11.0}{21} \quad \frac{11.2}{19} \quad \frac{8.5}{13} \quad \frac{8.1}{14} \quad \frac{8.3}{14} \quad \frac{10.5}{19} \quad \frac{10.9}{25} \quad \frac{12.3}{30} \quad \frac{12.9}{50}$$

$$\frac{10.9}{50} \quad \frac{11.6}{26} \quad \frac{11.4}{20} \quad \frac{10.1}{15} \quad \frac{9.7}{14} \quad \frac{9.8}{14} \quad \frac{12.3}{18} \quad \frac{12.9}{50}$$

$$\frac{11.0}{50} \quad \frac{11.9}{19} \quad \frac{10.8}{14} \quad \frac{10.4}{13} \quad \frac{10.6}{13} \quad \frac{12.9}{18} \quad \frac{13.0}{35} \quad \frac{13.2}{40} \quad \frac{12.9}{50}$$

$$\frac{12.7}{33} \quad \frac{12.5}{19} \quad \frac{10.6}{13} \quad \frac{10.4}{14} \quad \frac{10.5}{13} \quad \frac{12.6}{16} \quad \frac{12.5}{18} \quad \frac{13.1}{26} \quad \frac{12.2}{39}$$

$$\frac{13.7}{33} \quad \frac{13.5}{19} \quad \frac{10.3}{13} \quad \frac{9.7}{14} \quad \frac{10.0}{13} \quad \frac{12.8}{22} \quad \frac{13.0}{27} \quad \frac{13.4}{33}$$

$$\frac{16.6}{125} \quad \frac{16.3}{50} \quad \frac{17.6}{100} \quad \frac{16.2}{50} \quad \frac{16.0}{100}$$

$$\frac{13.6}{33} \quad \frac{12.5}{21} \quad \frac{8.9}{14} \quad \frac{8.7}{14} \quad \frac{8.9}{12} \quad \frac{12.2}{20} \quad \frac{12.8}{33}$$

Sta	T	π	-	Elev
		987.97		
32				81.0
	+50			83.3
33				85.6
T.P.	12.24	898.96	1.25	✓ 86.12
	+50			88.0
34				90.3
	+50			92.5
35				94.7
T.P.	11.27	908.59	1.64	✓ 897.32
	+50			96.9
36				99.0
	+50			901.2
37				03.4

Lt

E

Rt

$$\frac{12.4}{33} \quad \frac{11.4}{22} \quad \frac{6.7}{14} \quad \frac{7.0}{14} \quad \frac{6.3}{14} \quad \frac{11.4}{22} \quad \frac{11.7}{33}$$

$$\frac{9.0}{33} \quad \frac{8.2}{22} \quad \frac{4.1}{14} \quad \frac{4.7}{14} \quad \frac{4.5}{14} \quad \frac{6.9}{21} \quad \frac{6.6}{33}$$

$$\frac{5.7}{33} \quad \frac{5.9}{27} \quad \frac{4.7}{21} \quad \frac{2.1}{13} \quad \frac{2.4}{14} \quad \frac{1.7}{14} \quad \frac{3.9}{19} \quad \frac{4.0}{24} \quad \frac{3.1}{26} \quad \frac{3.1}{33}$$

$$\frac{13.3}{33} \quad \frac{13.1}{22} \quad \frac{12.9}{19} \quad \frac{10.6}{13} \quad \frac{11.0}{15} \quad \frac{10.5}{15} \quad \frac{11.8}{19} \quad \frac{11.8}{21} \quad \frac{11.5}{23} \quad \frac{11.8}{33}$$

$$\frac{9.5}{33} \quad \frac{9.4}{24} \quad \frac{9.8}{19} \quad \frac{10.1}{16} \quad \frac{8.8}{13} \quad \frac{8.7}{15} \quad \frac{8.1}{15} \quad \frac{9.6}{18} \quad \frac{9.6}{22} \quad \frac{9.2}{33}$$

$$\frac{5.0}{23} \quad \frac{4.5}{23} \quad \frac{7.2}{18} \quad \frac{7.3}{16} \quad \frac{6.5}{14} \quad \frac{6.5}{13} \quad \frac{6.3}{13} \quad \frac{7.3}{17} \quad \frac{7.5}{21} \quad \frac{5.2}{23} \quad \frac{4.4}{33}$$

$$\frac{2.2}{23} \quad \frac{2.0}{23} \quad \frac{5.2}{18} \quad \frac{5.1}{16} \quad \frac{4.4}{14} \quad \frac{4.3}{13} \quad \frac{4.0}{13} \quad \frac{4.9}{17} \quad \frac{5.2}{20} \quad \frac{2.2}{24} \quad \frac{1.4}{33}$$

$$\frac{10.1}{33} \quad \frac{10.0}{23} \quad \frac{12.5}{19} \quad \frac{12.4}{17} \quad \frac{11.9}{15} \quad \frac{11.7}{15} \quad \frac{11.4}{12} \quad \frac{12.6}{19} \quad \frac{12.3}{21} \quad \frac{9.3}{25} \quad \frac{8.7}{33}$$

$$\frac{5.2}{33} \quad \frac{7.9}{22} \quad \frac{10.3}{19} \quad \frac{10.1}{15} \quad \frac{9.5}{14} \quad \frac{9.6}{14} \quad \frac{9.5}{14} \quad \frac{10.5}{18} \quad \frac{10.5}{21} \quad \frac{7.2}{25} \quad \frac{6.7}{33}$$

$$\frac{7.1}{33} \quad \frac{6.7}{22} \quad \frac{8.3}{18} \quad \frac{8.4}{17} \quad \frac{7.5}{15} \quad \frac{7.4}{15} \quad \frac{7.2}{11} \quad \frac{8.4}{18} \quad \frac{8.3}{19} \quad \frac{6.3}{23} \quad \frac{6.5}{33}$$

$$\frac{6.3}{33} \quad \frac{5.8}{21} \quad \frac{6.4}{19} \quad \frac{6.3}{16} \quad \frac{5.5}{14} \quad \frac{5.2}{16} \quad \frac{5.2}{16} \quad \frac{5.8}{18} \quad \frac{6.0}{24} \quad \frac{5.6}{27} \quad \frac{5.2}{33}$$

Sta	+	π	-	Elev
		908.59		
37 +50				05.6
38				07.8
T.P.	13.09	921.44	0.24	908.25
+50				09.9
39				12.3
+50				14.7
40				17.0
+50				19.1
B.M.	7.68	926.53	2.57	918.87
41				20.7
+50				21.5
42				21.9
+50				21.8

Lt.

L

Rt.

$\frac{48}{33}$	$\frac{49}{19}$	$\frac{43}{16}$	$\frac{34}{14}$	$\frac{30}{-}$	$\frac{32}{12}$	$\frac{48}{18}$	$\frac{50}{23}$	$\frac{39}{26}$	$\frac{37}{33}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{28}{33}$	$\frac{28}{21}$	$\frac{23}{16}$	$\frac{13}{13}$	$\frac{08}{-}$	$\frac{10}{13}$	$\frac{38}{19}$	$\frac{28}{23}$	$\frac{16}{25}$	$\frac{14}{33}$
-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{125}{33}$	$\frac{116}{22}$	$\frac{115}{14}$	$\frac{115}{-}$	$\frac{154}{13}$	$\frac{118}{33}$
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$\frac{100}{33}$	$\frac{99}{20}$	$\frac{146}{18}$	$\frac{106}{16}$	$\frac{96}{13}$	$\frac{91}{-}$	$\frac{92}{14}$	$\frac{101}{17}$	$\frac{103}{19}$	$\frac{93}{21}$	$\frac{89}{33}$
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$\frac{67}{33}$	$\frac{67}{22}$	$\frac{80}{19}$	$\frac{80}{16}$	$\frac{70}{14}$	$\frac{67}{-}$	$\frac{67}{14}$	$\frac{77}{17}$	$\frac{77}{19}$	$\frac{61}{22}$	$\frac{57}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{38}{33}$	$\frac{35}{21}$	$\frac{50}{19}$	$\frac{50}{18}$	$\frac{46}{12}$	$\frac{44}{-}$	$\frac{44}{14}$	$\frac{56}{17}$	$\frac{56}{20}$	$\frac{37}{22}$	$\frac{33}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{19}{33}$	$\frac{22}{21}$	$\frac{38}{18}$	$\frac{36}{15}$	$\frac{28}{14}$	$\frac{23}{-}$	$\frac{24}{15}$	$\frac{38}{18}$	$\frac{37}{20}$	$\frac{18}{23}$	$\frac{15}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

Spike in Twin Cott. 58' Lt 40+17

$\frac{55}{33}$	$\frac{55}{22}$	$\frac{72}{19}$	$\frac{73}{16}$	$\frac{64}{14}$	$\frac{59}{-}$	$\frac{62}{11}$	$\frac{73}{18}$	$\frac{72}{20}$	$\frac{56}{22}$	$\frac{54}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{44}{33}$	$\frac{44}{24}$	$\frac{62}{20}$	$\frac{63}{17}$	$\frac{54}{14}$	$\frac{51}{-}$	$\frac{47}{18}$	$\frac{65}{16}$	$\frac{61}{20}$	$\frac{48}{22}$	$\frac{51}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

$\frac{47}{33}$	$\frac{50}{21}$	$\frac{57}{19}$	$\frac{59}{16}$	$\frac{50}{14}$	$\frac{47}{-}$	$\frac{50}{10}$	$\frac{55}{18}$	$\frac{57}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------

$\frac{51}{33}$	$\frac{52}{21}$	$\frac{64}{18}$	$\frac{64}{15}$	$\frac{52}{13}$	$\frac{48}{-}$	$\frac{46}{14}$	$\frac{62}{17}$	$\frac{62}{20}$	$\frac{57}{21}$	$\frac{60}{33}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	-----------------	-----------------	-----------------	-----------------	-----------------

Sta	+	π	-	Elev
		926.55		
43				21.6
+50				21.2
44				20.5
+50				19.5
45				18.2
T.P.	320	918.57	8.18	918.73
+50				16.7
46				15.4
+50				14.1
47				13.1
+41				12.4
+44				12.4

918.37

Lt.

K

Rt.

$$\frac{59}{33} \quad \frac{57}{21} \quad \frac{65}{18} \quad \frac{65}{16} \quad \frac{58}{13} \quad \frac{50}{14} \quad \frac{48}{14} \quad \frac{64}{17} \quad \frac{65}{19} \quad \frac{52}{22} \quad \frac{57}{33}$$

$$\frac{57}{33} \quad \frac{55}{24} \quad \frac{67}{20} \quad \frac{67}{17} \quad \frac{56}{14} \quad \frac{54}{14} \quad \frac{54}{14} \quad \frac{65}{17} \quad \frac{63}{20} \quad \frac{52}{22} \quad \frac{57}{33}$$

$$\frac{59}{33} \quad \frac{59}{23} \quad \frac{65}{19} \quad \frac{66}{16} \quad \frac{62}{14} \quad \frac{61}{14} \quad \frac{63}{15} \quad \frac{74}{18} \quad \frac{59}{22} \quad \frac{62}{33}$$

$$\frac{59}{33} \quad \frac{56}{22} \quad \frac{76}{18} \quad \frac{73}{16} \quad \frac{72}{14} \quad \frac{71}{13} \quad \frac{73}{13} \quad \frac{80}{17} \quad \frac{81}{21} \quad \frac{65}{23} \quad \frac{73}{33}$$

$$\frac{72}{33} \quad \frac{76}{21} \quad \frac{91}{18} \quad \frac{90}{16} \quad \frac{85}{14} \quad \frac{84}{14} \quad \frac{85}{14} \quad \frac{96}{18} \quad \frac{98}{23} \quad \frac{85}{25} \quad \frac{88}{33}$$

$$\frac{15}{33} \quad \frac{20}{21} \quad \frac{26}{18} \quad \frac{26}{16} \quad \frac{20}{14} \quad \frac{19}{13} \quad \frac{20}{15} \quad \frac{35}{19} \quad \frac{47}{33}$$

$$\frac{50}{33} \quad \frac{43}{17} \quad \frac{36}{14} \quad \frac{32}{14} \quad \frac{33}{15} \quad \frac{53}{20} \quad \frac{43}{33}$$

$$\frac{74}{33} \quad \frac{68}{18} \quad \frac{49}{14} \quad \frac{45}{14} \quad \frac{45}{15} \quad \frac{68}{21} \quad \frac{72}{33}$$

$$\frac{85}{33} \quad \frac{83}{19} \quad \frac{57}{13} \quad \frac{55}{14} \quad \frac{56}{14} \quad \frac{76}{19} \quad \frac{79}{33}$$

$$\frac{85}{33} \quad \frac{84}{18} \quad \frac{63}{12} \quad \frac{66}{14} \quad \frac{65}{14} \quad \frac{81}{17} \quad \frac{80}{21} \quad \frac{82}{33}$$

$$\frac{88}{33} \quad \frac{85}{18} \quad \frac{63}{12} \quad \frac{62}{14} \quad \frac{65}{14} \quad \frac{85}{18} \quad \frac{85}{20} \quad \frac{71}{24} \quad \frac{71}{33}$$

Sta	+	π	-	Elev
		918.57		
48				11.5
	+50			10.9
49				10.6
I.P.	3.07	913.56	8.08	910.49
	+50			10.2
50				10.0
	+50			09.6
51				09.1
	+36			08.9
	+45			08.9
	+52			08.8
	+62			08.7

Lt

K

Rt

$$\frac{78}{33} \quad \frac{77}{24} \quad \frac{89}{18} \quad \frac{86}{16} \quad \frac{73}{13} \quad \frac{71}{14} \quad \frac{82}{17} \quad \frac{86}{20} \quad \frac{71}{23} \quad \frac{70}{33}$$

$$\frac{82}{33} \quad \frac{80}{20} \quad \frac{82}{18} \quad \frac{90}{16} \quad \frac{79}{13} \quad \frac{77}{14} \quad \frac{74}{14} \quad \frac{70}{33}$$

$$\frac{74}{33} \quad \frac{90}{20} \quad \frac{94}{18} \quad \frac{95}{18} \quad \frac{82}{13} \quad \frac{80}{14} \quad \frac{78}{14} \quad \frac{93}{18} \quad \frac{93}{20} \quad \frac{72}{24} \quad \frac{79}{33}$$

$$\frac{48}{33} \quad \frac{56}{22} \quad \frac{49}{18} \quad \frac{48}{15} \quad \frac{85}{18} \quad \frac{34}{14} \quad \frac{35}{14} \quad \frac{44}{17} \quad \frac{45}{20} \quad \frac{27}{24} \quad \frac{25}{30}$$

$$\frac{38}{33} \quad \frac{30}{22} \quad \frac{47}{17} \quad \frac{46}{18} \quad \frac{39}{12} \quad \frac{36}{14} \quad \frac{37}{14} \quad \frac{49}{17} \quad \frac{48}{22} \quad \frac{32}{24} \quad \frac{38}{33}$$

$$\frac{43}{33} \quad \frac{43}{23} \quad \frac{48}{16} \quad \frac{43}{12} \quad \frac{40}{14} \quad \frac{48}{14} \quad \frac{56}{18} \quad \frac{56}{25} \quad \frac{42}{27} \quad \frac{43}{33}$$

$$\frac{54}{33} \quad \frac{57}{23} \quad \frac{64}{19} \quad \frac{64}{17} \quad \frac{46}{18} \quad \frac{45}{14} \quad \frac{47}{14} \quad \frac{74}{18} \quad \frac{74}{23} \quad \frac{63}{26} \quad \frac{68}{33}$$

Ck

$$\frac{62}{33} \quad \frac{68}{28} \quad \frac{81}{21} \quad \frac{48}{18} \quad \frac{47}{16} \quad \frac{53}{16} \quad \frac{87}{24} \quad \frac{83}{33}$$

$$\frac{105}{50} \quad \frac{94}{33} \quad \frac{53}{23} \quad \frac{47}{17} \quad \frac{53}{17} \quad \frac{87}{26} \quad \frac{96}{33}$$

$$\frac{101}{50} \quad \frac{93}{39} \quad \frac{59}{30} \quad \frac{48}{23} \quad \frac{52}{30} \quad \frac{85}{30} \quad \frac{100}{50}$$

$$\frac{53}{50}$$

$$\frac{49}{50}$$

$$\frac{58}{50}$$

Sta + π - Elev.

913.56

51 +71.80 = 1. Hong Lake Rd. 08.7

B.M. 6.85 906.71

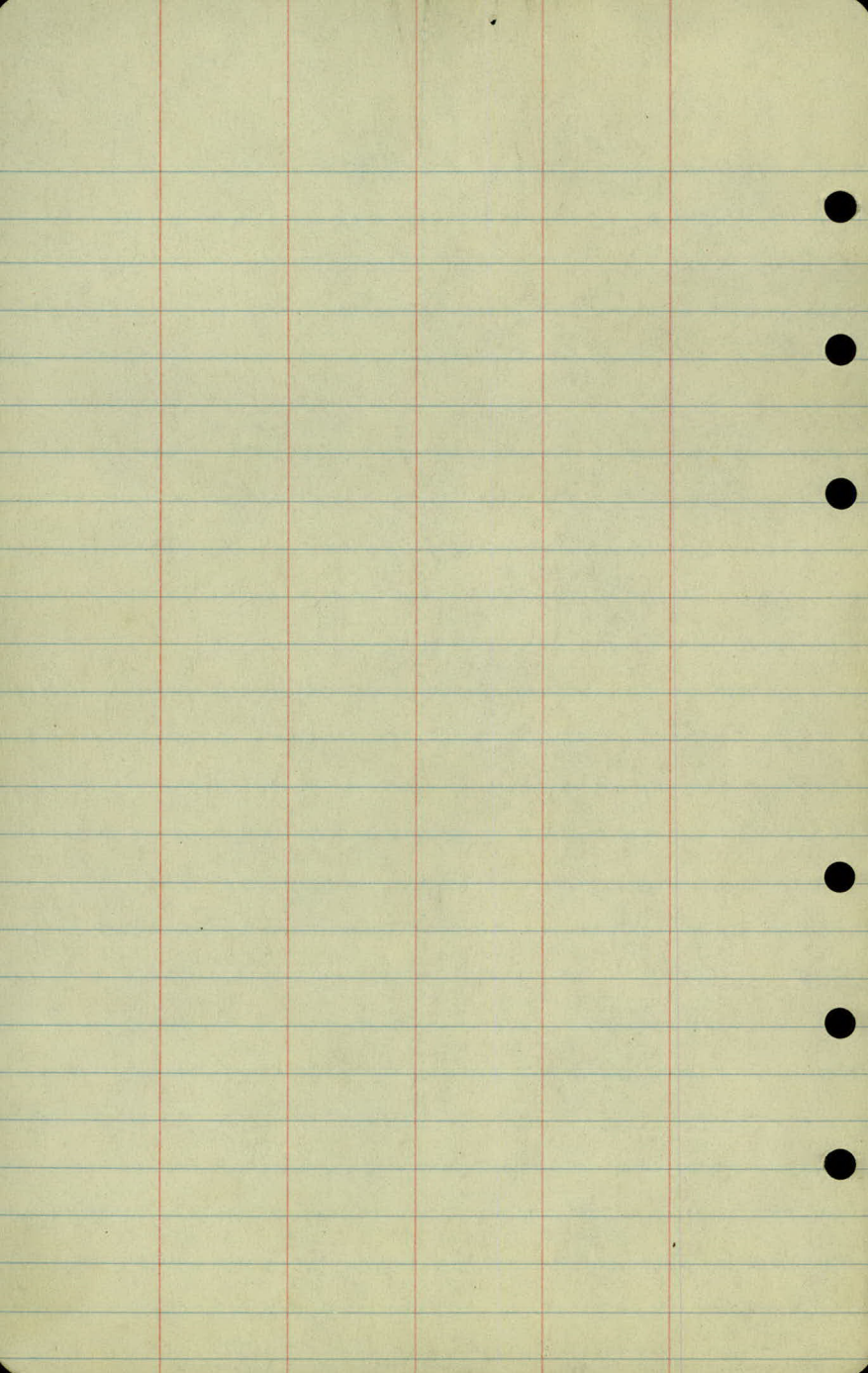
Lt

L

Rt

 $\frac{37}{100}$ $\frac{49}{50}$ $\frac{49}{50}$ $\frac{59}{50}$ $\frac{57}{100}$

Spike in P.P. 25' S.W. 51+7180



CEMETERY RD.

Slope Stakes

13 Pages

Sta	+	x	-	Grade.
B.M.	11.64	896.84		985.20
0+00				990.8
+13				89.7
+17				89.3
+37				87.5
+75				84.2
B.M.	0.51	985.71		985.20
1				82.0
+50				77.6
T.P.	0.11	973.09	12.73	972.98
+75				75.4
2				73.2
+50				69.1
+75				67.3

Cor. Rod

Lt

C

Rt.

Spk in T.P. 25 R10461

9.3

$$\begin{array}{r} 880/4.7 \\ 176 \end{array}$$

$$\begin{array}{r} 120/0.2 \\ 121 \end{array}$$

$$\begin{array}{r} 21 \\ 105 \end{array}$$

$$\begin{array}{r} 29/10 \\ 169 \end{array}$$

$$\begin{array}{r} 80/10 \\ 119 \end{array}$$

$$\begin{array}{r} 1.5/1.2 \\ 128 \end{array}$$

12.6

$$\begin{array}{r} 50/55 \\ 118 \end{array}$$

$$\begin{array}{r} 20/6.6 \\ 16.0 \end{array}$$

$$\begin{array}{r} 10.3 \\ 103 \end{array}$$

$$\begin{array}{r} 91/429 \\ 135 \end{array}$$

$$\begin{array}{r} 109/570 \\ 117 \end{array}$$

3.7

$$\begin{array}{r} 490/10.7 \\ 10.7 \end{array}$$

$$\begin{array}{r} 35 \\ 102 \end{array}$$

$$\begin{array}{r} 54/16.0 \\ 103 \end{array}$$

8.1

$$\begin{array}{r} 256/184 \\ 53 \end{array}$$

$$\begin{array}{r} 8.2 \\ 101 \end{array}$$

$$\begin{array}{r} 105/36.8 \\ 84 \end{array}$$

-2.3

$$\begin{array}{r} 26.0/3.2 \\ 5.5 \end{array}$$

$$\begin{array}{r} 6.1/31.8 \\ 84 \end{array}$$

-0.1

$$\begin{array}{r} 25.6/5.2 \\ 53 \end{array}$$

$$\begin{array}{r} 0.1 \\ 10.2 \end{array}$$

$$\begin{array}{r} 7.5/10.2 \\ 76 \end{array}$$

4.0

$$\begin{array}{r} 266/78 \\ 28 \end{array}$$

$$\begin{array}{r} 4.3 \\ 93 \end{array}$$

$$\begin{array}{r} 9.3/256 \\ 13 \end{array}$$

5.8

$$\begin{array}{r} 228/3.7 \\ 3.9 \end{array}$$

$$\begin{array}{r} 0.4 \\ 10.6 \end{array}$$

$$\begin{array}{r} 106/296 \\ 48 \end{array}$$

Sta	+	Δ	-	Grade
		973.09		
				65.7
I.P.	0.23	962.10	11.22	961.87
+20				63.9
+70				61.9
				60.7
+50				59.1
				58.2
+35				57.8
+60				57.5
				57.0
I.P.	12.08	966.78	7.45	954.65
+28				56.7
P	3.87	969.20	1.40	
+80				56.0

Gr Rod

Lt

R

Rt

7.4

$$228 / \begin{matrix} 11.5 \\ -3.9 \end{matrix}$$

$$\frac{84}{-10}$$

$$\frac{128}{-57} / 25.8$$

+1.8

$$260 / \begin{matrix} 3.7 \\ -5.5 \end{matrix}$$

$$\frac{36}{-54} / 25.8$$

0.2

$$308 / \begin{matrix} 5.1 \\ -7.9 \end{matrix}$$

$$\frac{18}{-16}$$

$$\frac{70}{-48} / 25.8$$

1.4

$$318 / \begin{matrix} 13.3 \\ -10.9 \end{matrix}$$

$$\frac{29}{-15}$$

$$\frac{100}{-86} / 36.2$$

3.0

$$44.8 / \begin{matrix} 17.4 \\ -14.4 \end{matrix}$$

$$\frac{98}{-18}$$

$$\frac{134}{-104} / 36.8$$

2.9

$$43.2 / \begin{matrix} 17.5 \\ -13.6 \end{matrix}$$

$$\frac{60}{-21}$$

$$\frac{161}{-12.2} / 40.4$$

4.3

$$\frac{62}{-19}$$

$$\frac{151}{-108} / 37.6$$

4.6

$$\frac{61}{-15}$$

$$\frac{140}{-92} / 34.8$$

5.1

$$\frac{58}{-27}$$

$$\frac{99}{-73} / 22.6$$

10.0

$$360 / \begin{matrix} 5.0 \\ +5.0 \end{matrix}$$

$$\frac{102}{-0.2}$$

$$\frac{102}{15.18} / 25.6$$

13.2

$$436 / \begin{matrix} 44 \\ +8.8 \end{matrix}$$

$$\frac{121}{+41}$$

$$\frac{2.5}{+10.7} / 47.4$$

Sta.	+	X	-	Grade
------	---	---	---	-------

		969.20		
--	--	--------	--	--

1				55.8
---	--	--	--	------

+50				55.2
-----	--	--	--	------

1				54.6
---	--	--	--	------

+65				53.5
-----	--	--	--	------

T.P.	2.17	957.73	13.66	955.84
------	------	--------	-------	--------

7				52.7
---	--	--	--	------

+72				51.5
-----	--	--	--	------

0				49.4
---	--	--	--	------

+75				47.5
-----	--	--	--	------

+80				45.7
-----	--	--	--	------

1				44.7
---	--	--	--	------

+85				41.7
-----	--	--	--	------

P.	0.91	945.08	13.56	944.17
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Gr. Red

Lt

E

Rt.

$$18.4 \quad \frac{44.4/4.3}{+9.2} \quad \frac{18.0}{+1.4} \quad \frac{26}{+108/47.6}$$

$$140 \quad \frac{41.6/6.2}{+7.8} \quad \frac{18.2}{+5.1} \quad \frac{4.8}{+9.2/49.9}$$

$$146 \quad \frac{40.0/7.4}{+7.0} \quad \frac{12.3}{+2.3} \quad \frac{96}{+50/36.0}$$

$$15.7 \quad \frac{32.0/12.7}{+3.0} \quad \frac{19.6}{+2.1} \quad \frac{118}{+5.9/33.8}$$

$$50 \quad \frac{32.8/16}{+3.4} \quad \frac{30}{+20} \quad \frac{0.4}{+9.6/35.2}$$

$$6.2 \quad \frac{38.8/8.3}{+3.9} \quad \frac{41}{+2.1} \quad \frac{0.5}{+5.7/31.4}$$

$$8.3 \quad \frac{19.3/10.5}{+20.0} \quad \frac{6.3}{+2.0} \quad \frac{5.1}{+3.2/30.4}$$

$$10.2 \quad \frac{22.8/11.8}{+20.4} \quad \frac{8.5}{+1.7} \quad \frac{5.4}{+4.8/35.6}$$

$$12.0 \quad \frac{37.8/6.1}{+5.9} \quad \frac{10.4}{+1.6} \quad \frac{8.4}{+3.6/33.2}$$

$$13.0 \quad \frac{40.6/5.7}{+7.3} \quad \frac{11.5}{+1.5} \quad \frac{8.9}{+7.1/34.2}$$

$$16.0 \quad \frac{43.4/7.3}{+8.7} \quad \frac{14.8}{+1.2} \quad \frac{7.8}{+5.2/42.4}$$

Sta	+	π	-	Grade
		945.08		
12				39.3
+40				371
+70				355
13				33.9
T.P.	1.45	935.26	11.27	933.81
+50				31.2
14				28.5
+55				25.6
B.M.	0.97	928.87	7.30	927.96
				927.90
15				23.3
+50				20.9
T.P.	0.59	917.59	11.87	912.00
16				18.6
+40				16.9

Cor. Rod

L_tL_eR_t

$$58 \quad 40.4 / \begin{array}{r} +1.4 \\ +7.2 \end{array} \quad \begin{array}{r} 48 \\ +1.0 \end{array} \quad \begin{array}{r} 15 \\ +43 / 346 \end{array}$$

$$80 \quad 24.9 / \begin{array}{r} 8.8 \\ 27.2 \end{array} \quad \begin{array}{r} 7.8 \\ +0.7 \end{array} \quad \begin{array}{r} 9.5 \\ 27.03 / 29.0 \end{array}$$

$$76 \quad 19.2 / \begin{array}{r} 11.6 \\ 20.0 \end{array} \quad \begin{array}{r} 9.2 \\ +0.4 \end{array} \quad \begin{array}{r} 11.6 \\ 25.20 / 22.0 \end{array}$$

$$112 \quad 22.2 / \begin{array}{r} 15.3 \\ -4.1 \end{array} \quad \begin{array}{r} 11.1 \\ +0.1 \end{array} \quad \begin{array}{r} 12.5 \\ 27.07 / 29.4 \end{array}$$

$$41 \quad 22.0 / \begin{array}{r} 6.1 \\ 20.0 \end{array} \quad \begin{array}{r} 4.3 \\ -0.2 \end{array} \quad \begin{array}{r} 3.6 \\ +0.5 / 27.0 \end{array}$$

$$68 \quad 22.0 / \begin{array}{r} 8.2 \\ 20.0 \end{array} \quad \begin{array}{r} 7.4 \\ -0.6 \end{array} \quad \begin{array}{r} 6.8 \\ +0.0 / 26.0 \end{array}$$

$$97 \quad 20.0 / \begin{array}{r} 12.7 \\ -3.0 \end{array} \quad \begin{array}{r} 10.7 \\ -1.0 \end{array} \quad \begin{array}{r} 2.4 \\ +7.3 / 40.6 \end{array}$$

$$56 \quad 23.0 / \begin{array}{r} 10.1 \\ -4.5 \end{array} \quad \begin{array}{r} 6.8 \\ -1.2 \end{array} \quad \begin{array}{r} 4.0 \\ +1.6 / 29.2 \end{array}$$

$$80 \quad 28.6 / \begin{array}{r} 14.8 \\ -6.8 \end{array} \quad \begin{array}{r} 9.7 \\ \end{array} \quad \begin{array}{r} 15.0 \\ -7.0 / 29.0 \end{array}$$

$$+11 \quad 0 \quad \begin{array}{r} 0.5 \\ -1.6 \end{array} \quad \begin{array}{r} 7.6 \\ -8.7 / 32.4 \end{array}$$

$$0.7 \quad \begin{array}{r} 1.7 \\ -1.2 \end{array}$$

Sta	+	Σ	-	Grade
		917.54		
16	+70			15.6
17				14.4
	+40			13.2
T.P.	4.12	917.82	3.24	913.70
	+70			11.6
18				10.4
	+50			08.4
19				06.4
	+50			04.4
T.P.	2.11	907.12	12.80	905.02
20				02.4
	+50			00.4
21				898.4

Gr. Rod

Lt.

E

Rt.

$$1.9 \quad \frac{27}{-0.8}$$

$$3.1 \quad \frac{23.0}{-9.5} \quad \frac{34}{-0.9} \quad \frac{4.5}{-3.4} / 20.8$$

$$4.7 \quad \frac{27.0}{+0.5} \quad \frac{4.5}{+0.4} \quad \frac{+3.3}{+8.0} / 42.0$$

Top Shape Stake A/L

$$6.2 \quad \frac{34.0}{+2.0} \quad \frac{54}{+0.8} \quad \frac{+2.3}{+18.5} / 47.0$$

$$7.4 \quad \frac{37.6}{+5.0} \quad \frac{64}{+1.0} \quad \frac{+4.1}{+11.5} / 49.0$$

$$9.4 \quad \frac{37.6}{+5.8} \quad \frac{85}{+0.9} \quad \frac{+2.0}{+11.4} / 48.8$$

$$11.4 \quad \frac{37.4}{+5.7} \quad \frac{106}{+0.8} \quad \frac{2.8}{+8.6} / 43.2$$

$$13.4 \quad \frac{39.2}{+2.6} \quad \frac{130}{+0.4} \quad \frac{6.2}{+2.2} / 40.4$$

$$4.7 \quad \frac{38.9}{+1.2} \quad \frac{48}{-0.1} \quad \frac{+0.1}{+4.8} / 25.6$$

$$6.7 \quad \frac{23.4}{+0.7} \quad \frac{77}{-1.0} \quad \frac{7.1}{+0.6} / 25.2$$

$$8.7 \quad \frac{20.8}{-3.4} \quad \frac{104}{-1.7} \quad \frac{12.3}{-3.6} / 21.2$$

Sta	T	X	-	Grade
		707.12		

21	+50			896.4
----	-----	--	--	-------

T.P	0.59	894.42	13.29	893.83
-----	------	--------	-------	--------

22				94.4
----	--	--	--	------

	+50			92.4
--	-----	--	--	------

23				90.8
----	--	--	--	------

	+50			89.6
--	-----	--	--	------

	+85			88.9
--	-----	--	--	------

24				85.7
----	--	--	--	------

	+50			88.2
--	-----	--	--	------

25				88.1
----	--	--	--	------

T.P	11.72	899.14	7.00	887.42
-----	-------	--------	------	--------

	+50			88.3
--	-----	--	--	------

26				88.5
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9/24/38

Cemetery Rd.
Grade Revision

Sta	+	π	-	Grade
B.M.		98.4		(892.40)
22	+50			92.6
23				91.1
	+50			90.0
24				89.2
	+50			88.6
25				88.4
	+50			88.3
I.P.	7.0	99.5	0.90	92.5
26				88.2
	+50			87.9
27				87.1
	+09			86.9

1st Top
 H.O.O = 22'
 Cut 00 = 26'
 2:1 Slopes.

Gr. Rod. Lt. E Rt.

Spk in T.P. Rt 21461

$$0.8 \quad 27.4 / \begin{array}{r} 7.0 \\ -6.2 \end{array} \quad \begin{array}{r} 98 \\ -40 \end{array} / 23.0$$

$$2.3 \quad 27.6 / \begin{array}{r} 8.6 \\ -6.3 \end{array} \quad \begin{array}{r} 24 \\ -91 \end{array} \quad \begin{array}{r} 74 \\ -51 \end{array} / 25.2$$

$$3.4 \quad 27.0 / \begin{array}{r} 9.4 \\ -6.0 \end{array} \quad \begin{array}{r} 39 \\ -95 \end{array} \quad \begin{array}{r} 109 \\ -75 \end{array} / 30.0$$

$$4.2 \quad 29.2 / \begin{array}{r} 11.8 \\ -7.1 \end{array} \quad \begin{array}{r} 46 \\ -94 \end{array} \quad \begin{array}{r} 114 \\ -74 \end{array} / 29.8$$

$$4.8 \quad 26.2 / \begin{array}{r} 10.4 \\ -5.6 \end{array} \quad \begin{array}{r} 51 \\ -93 \end{array} \quad \begin{array}{r} 109 \\ -61 \end{array} / 27.2$$

$$5.0 \quad \begin{array}{r} \text{B. Top} \\ 22.0 \end{array} / \begin{array}{r} 7.0 \\ -0.0 \end{array} \quad \begin{array}{r} 53 \\ -93 \end{array} \quad \begin{array}{r} \text{B. Top} \\ 7.0 \end{array} / \begin{array}{r} 40.0 \\ -20 \end{array}$$

$$5.1 \quad 32.9 / \begin{array}{r} 14 \\ +9.7 \end{array} \quad \begin{array}{r} 50 \\ +0.1 \end{array} \quad \begin{array}{r} 2.3 \\ +2.8 \end{array} / 30.0$$

$$11.3 \quad 42.8 / \begin{array}{r} 2.9 \\ +8.9 \end{array} \quad \begin{array}{r} 109 \\ +0.9 \end{array} \quad \begin{array}{r} 39 \\ +7.4 \end{array} / 30.0$$

$$11.6 \quad 42.7 / \begin{array}{r} 2.9 \\ +8.7 \end{array} \quad \begin{array}{r} 109 \\ +0.7 \end{array} \quad \begin{array}{r} 35 \\ +8.1 \end{array} / 30.0$$

$$12.4 \quad \quad \quad \begin{array}{r} 11.6 \\ +0.8 \end{array} \quad \begin{array}{r} 43 \\ +8.1 \end{array} / 50.0$$

$$12.6 \quad 42.0 / \begin{array}{r} 9.6 \\ +8.0 \end{array}$$

569 + 7 - Google

99.5

27 +18

84.7

+20

84.9

T.P. 0.10 986.93 1267

986.83

+70

85.2

+85

89.7

28

84.2

+20

83.4

+95

82.7

29

81.2

+50

80.2

T.P. 7.96 994.88 10.01

994.92

30

79.8

+50

79.7

Gr. Rod.

12.8

$$\frac{36}{192/300}$$

13.1

$$\frac{26.9}{10.2}/\frac{12.7}{10.2}$$

$$\frac{12.1}{11.0}$$

$$\frac{9.3}{138/30.0}$$

1.7

$$\frac{0.7}{11.0}$$

$$\frac{11.0}{12.7/30.0}$$

2.2

$$\frac{25.6}{18.8}/\frac{2.4}{18.8}$$

$$\frac{2.0}{10.7}$$

$$\frac{10.9}{13.1/30.0}$$

2.7

$$\frac{26.6}{10.3}/\frac{2.4}{10.3}$$

$$\frac{2.0}{10.7}$$

$$\frac{10.9}{12.6/30.0}$$

3.5

$$\frac{22.6}{12.3}/\frac{5.2}{12.3}$$

$$\frac{2.9}{10.6}$$

$$\frac{3.5}{10.0/26.0}$$

4.2

$$\frac{21.2}{-3.1}/\frac{7.8}{-3.1}$$

$$\frac{3.9}{10.8}$$

$$\frac{5.5}{15.7/23.4}$$

5.7

$$\frac{23.2}{-4.1}/\frac{9.8}{-4.1}$$

$$\frac{5.2}{10.5}$$

$$\frac{9.7}{-2.0/22.0}$$

6.6

$$\frac{23.0}{-4.0}/\frac{10.6}{-4.0}$$

$$\frac{5.9}{10.7}$$

$$\frac{11.6}{-5.0/25.0}$$

5.1

$$\frac{22.2}{-3.6}/\frac{8.7}{-3.6}$$

$$\frac{4.6}{10.5}$$

$$\frac{9.1}{-4.0/23.0}$$

5.2

$$\frac{5.2}{10.0}$$

Sta

+

1

-

Grade

80.1

+30

80.9

14' Top 1' Windings
 2300 = 22'
 60400 = 26'

Cor. Rod

Lt.

8

Rt.

10.7	$\begin{array}{r} 25.6 / 16.0 \\ -5.9 \\ \hline \end{array}$	$\begin{array}{r} 12.9 \\ -2.2 \\ \hline \end{array}$	$\begin{array}{r} 16.7 \\ -5.0 / 25.0 \\ \hline \end{array}$
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Nail in T. P. rod

0.0	$\begin{array}{r} 25.4 / 5.2 \\ -5.2 \\ \hline \end{array}$	$\begin{array}{r} 2.3 \\ -2.3 \\ \hline \end{array}$	$\begin{array}{r} 5.9 \\ -5.9 / 26.8 \\ \hline \end{array}$
-----	---	--	---

2.0	$\begin{array}{r} 27.9 / 8.2 \\ -6.2 \\ \hline \end{array}$	$\begin{array}{r} 4.8 \\ -4.8 \\ \hline \end{array}$	$\begin{array}{r} 7.2 \\ -5.2 / 25.4 \\ \hline \end{array}$
-----	---	--	---

3.4	$\begin{array}{r} 29.2 / 10.2 \\ -6.6 \\ \hline \end{array}$	$\begin{array}{r} 6.5 \\ -6.5 \\ \hline \end{array}$	$\begin{array}{r} 9.0 \\ -5.4 / 25.8 \\ \hline \end{array}$
-----	--	--	---

4.8	$\begin{array}{r} 28.8 / 11.7 \\ -6.9 \\ \hline \end{array}$	$\begin{array}{r} 7.7 \\ -2.7 \\ \hline \end{array}$	$\begin{array}{r} 12.8 \\ -8.0 / 31.0 \\ \hline \end{array}$
-----	--	--	--

5.5

5.7	$\begin{array}{r} 30.6 / 13.5 \\ -6.8 \\ \hline \end{array}$	$\begin{array}{r} 8.4 \\ -6.7 \\ \hline \end{array}$	$\begin{array}{r} 14.3 \\ -8.6 / 32.5 \\ \hline \end{array}$
-----	--	--	--

6.2	$\begin{array}{r} 25.8 / 11.4 \\ -5.4 \\ \hline \end{array}$	$\begin{array}{r} 8.1 \\ -1.9 \\ \hline \end{array}$	$\begin{array}{r} 11.5 \\ -5.3 / 26.6 \\ \hline \end{array}$
-----	--	--	--

6.3	$\begin{array}{r} 23.2 / 7.7 \\ -10.6 \\ \hline \end{array}$	$\begin{array}{r} 7.0 \\ -0.7 \\ \hline \end{array}$	$\begin{array}{r} 8.4 \\ -2.1 / 18.2 \\ \hline \end{array}$
-----	--	--	---

10.8	$\begin{array}{r} 33.4 / 7.1 \\ -13.7 \\ \hline \end{array}$	$\begin{array}{r} 10.2 \\ -10.6 \\ \hline \end{array}$	$\begin{array}{r} 7.7 \\ -13.1 / 30.0 \\ \hline \end{array}$
------	--	--	--

10.6	$\begin{array}{r} 42.4 / 2.9 \\ -18.2 \\ \hline \end{array}$	$\begin{array}{r} 9.5 \\ -11.1 \\ \hline \end{array}$	$\begin{array}{r} 3.5 \\ -17.1 / 30.0 \\ \hline \end{array}$
------	--	---	--

Sta	+	x	-	Grade	
		899.19			
26	+50			88.5	
27				87.8	
	+09			87.8	
	+18			87.5	
	+30			87.3	
	+70			86.1	
	+85			85.5	
B.M.	-003	890.10			890.13
28				84.9	
	+20			84.1	
	+45			83.2	
29				81.7	
T.P.	7.01	899.22	12.58	877.52	

Gr. Rod

Lt

R

Rt

$$10.6 \quad \begin{array}{r} 12.9 \\ \times 18.2 \\ \hline \end{array} \quad \begin{array}{r} 78 \\ \times 1.1 \\ \hline \end{array} \quad \begin{array}{r} 3.0 \\ \times 7.6 \\ \hline 30.0 \end{array}$$

$$11.3 \quad \begin{array}{r} 30.0 \\ \times 7.7 \\ \hline \end{array} \quad \begin{array}{r} 10.4 \\ \times 0.9 \\ \hline \end{array} \quad \begin{array}{r} 3.9 \\ \times 7.4 \\ \hline 40.8 \end{array}$$

$$11.3 \quad \begin{array}{r} 41.8 \\ \times 7.9 \\ \hline \end{array}$$

$$11.6 \quad \begin{array}{r} 11.0 \\ \times 0.6 \\ \hline \end{array} \quad \begin{array}{r} 9.2 \\ \times 8.4 \\ \hline 30.0 \end{array}$$

$$11.8 \quad \begin{array}{r} 24.6 \\ \times 12.3 \\ \hline \end{array} \quad \begin{array}{r} 11.4 \\ \times 0.4 \\ \hline \end{array} \quad \begin{array}{r} 9.0 \\ \times 2.8 \\ \hline 30.0 \end{array}$$

$$12.0 \quad \begin{array}{r} 26.8 \\ \times 10.2 \\ \hline \end{array} \quad \begin{array}{r} 13.1 \\ - 0.1 \\ \hline \end{array} \quad \begin{array}{r} 11.1 \\ \times 1.9 \\ \hline 30.0 \end{array}$$

$$13.6 \quad \begin{array}{r} 27.2 \\ \times 0.6 \\ \hline \end{array} \quad \begin{array}{r} 15.8 \\ - 0.2 \\ \hline \end{array} \quad \begin{array}{r} 8.6 \\ \times 3.0 \\ \hline 30.0 \end{array}$$

Spk. in Oak Rt 27+90

$$5.2 \quad \begin{array}{r} 25.2 \\ \times 1.6 \\ \hline \end{array} \quad \begin{array}{r} 5.6 \\ - 0.4 \\ \hline \end{array} \quad \begin{array}{r} 1.9 \\ \times 3.3 \\ \hline 30.0 \end{array}$$

$$6.0 \quad \begin{array}{r} 19.4 \\ \times 2.7 \\ \hline \end{array} \quad \begin{array}{r} 6.6 \\ - 0.6 \\ \hline \end{array} \quad \begin{array}{r} 5.1 \\ - 2.1 \\ \hline 15.2 \end{array}$$

$$6.9 \quad \begin{array}{r} 22.0 \\ \times 10.9 \\ \hline - 4.0 \end{array} \quad \begin{array}{r} 7.8 \\ - 0.9 \\ \hline \end{array} \quad \begin{array}{r} 9.3 \\ - 2.4 \\ \hline 18.8 \end{array}$$

$$8.1 \quad \begin{array}{r} 23.4 \\ \times 13.1 \\ \hline - 9.7 \end{array} \quad \begin{array}{r} 10.2 \\ - 1.8 \\ \hline \end{array} \quad \begin{array}{r} 12.9 \\ - 4.5 \\ \hline 28.0 \end{array}$$

Sta.	+	X	-	Grade
		889.53		
29	+50			80.6
30				80.1
	+50			79.9
31				80.3
	+50			80.9
32				82.1
	+50			83.6
I.P.	13.10	897.63	0.0	884.53
33				85.6
	+50			87.8
34				90.0
	+50			92.2

Gr. Rod

Lt

¢

Rt.

$$3.9 \quad 22.4 / \frac{8.2}{-9.3}$$

$$\frac{6.2}{2.3}$$

$$\frac{9.3}{-5.9 / 25.8}$$

$$4.4 \quad 22.4 / \frac{8.6}{-9.2}$$

$$\frac{7.0}{-8.9}$$

$$\frac{9.4}{-5.0 / 25.0}$$

$$4.6 \quad 23.0 / \frac{9.1}{-9.5}$$

$$\frac{7.1}{-2.5}$$

$$\frac{9.6}{-5.0 / 25.0}$$

$$4.2 \quad 27.0 / \frac{10.2}{-6.0}$$

$$\frac{6.3}{-2.1}$$

$$\frac{9.7}{-5.5 / 26.0}$$

$$3.6 \quad 22.2 / \frac{9.7}{-6.1}$$

$$\frac{5.3}{-1.7}$$

$$\frac{9.4}{-5.8 / 26.6}$$

$$2.4 \quad 27.0 / \frac{8.4}{-6.0}$$

$$\frac{3.4}{-1.0}$$

$$\frac{7.8}{-5.4 / 25.8}$$

$$0.9 \quad 22.0 / \frac{4.9}{-4.0}$$

$$\frac{1.2}{-0.3}$$

$$\frac{3.6}{-2.7 / 19.4}$$

$$12.0 \quad 19.8 / \frac{14.0}{R9.0}$$

$$\frac{12.0}{20}$$

$$\frac{13.8}{R9.2 / 22.4}$$

$$9.8 \quad 22.0 / \frac{11.8}{R9.0}$$

$$\frac{9.8}{9.0}$$

$$\frac{10.5}{R9.5 / 24.6}$$

$$7.6 \quad 24.6 / \frac{8.3}{R7.5}$$

$$\frac{7.4}{+0.2}$$

$$\frac{8.1}{R9.5 / 25.0}$$

$$5.4 \quad 29.0 / \frac{3.7}{+1.5}$$

$$\frac{5.3}{+0.1}$$

$$\frac{2.8}{+2.6 / 30.0}$$

Sta	+	x	-	Grade
-----	---	---	---	-------

897.63

35				94.9
----	--	--	--	------

T.P.	13.00	910.63	0.0	897.63
------	-------	--------	-----	--------

+50				96.6
-----	--	--	--	------

36				898.8
----	--	--	--	-------

+50				901.0
-----	--	--	--	-------

37				03.2
----	--	--	--	------

+50				05.4
-----	--	--	--	------

38				07.6
----	--	--	--	------

+50				09.8
-----	--	--	--	------

T.P.	13.55	929.10	0.08	910.58
------	-------	--------	------	--------

39				12.0
----	--	--	--	------

+50				14.2
-----	--	--	--	------

40				16.4
----	--	--	--	------

B.M.	5.21	924.13	5.21	918.92
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Gr. Rod

Lt

F

Rt.

$$2.2 \quad 30.0 / \frac{0.9}{+2.3}$$

$$\frac{3.0}{+0.7}$$

$$\frac{0.2}{+1.0/30.0}$$

$$14.0 \quad 30.0 / \frac{12.0}{+2.0}$$

$$\frac{13.7}{+0.3}$$

$$\frac{10.2}{+3.8/30.0}$$

$$11.8 \quad 29.4 / \frac{10.1}{+1.7}$$

$$\frac{11.7}{+0.1}$$

$$\frac{8.7}{+3.1/30.0}$$

$$9.6 \quad 27.9 / \frac{8.9}{+0.7}$$

$$\frac{9.6}{0.0}$$

$$\frac{8.4}{+1.2/28.4}$$

$$7.4 \quad 24.6 / \frac{8.1}{+1.3}$$

$$\frac{7.2}{+0.2}$$

$$\frac{7.3}{+1.1/27.2}$$

$$5.2 \quad 22.6 / \frac{6.3}{+0.3}$$

$$\frac{5.1}{+0.1}$$

$$\frac{6.0}{+0.2/24.9}$$

$$3.0 \quad 20.6 / \frac{4.7}{+0.3}$$

$$\frac{2.3}{+0.1}$$

$$\frac{3.7}{+0.3/24.6}$$

$$0.8 \quad 24.6 / \frac{1.5}{+1.3}$$

$$\frac{0.7}{+0.1}$$

$$\frac{1.0}{+0.1/25.6}$$

$$12.1 \quad 24.9 / \frac{12.7}{+2.4}$$

$$\frac{11.8}{+0.2}$$

$$\frac{15.1}{+0.9/25.8}$$

$$9.9 \quad 21.0 / \frac{9.4}{+0.5}$$

$$\frac{9.3}{+0.6}$$

$$\frac{9.6}{+1.3/28.6}$$

$$7.7 \quad 28.2 / \frac{6.6}{+1.1}$$

$$\frac{7.1}{+0.6}$$

$$\frac{5.9}{+1.8/29.6}$$

Spk in Tw. Coll. 5324 40417

Sta.	+	+	-	Grade.	
		922.13			
40	+50			18.4	
41				20.0	
	+50			21.1	
42	+10			22.0	
B.M.		6.23	923.62	2.10	922.03
	+50			22.1	917.29
43				22.0	
	+50			21.6	
44				20.6	
	+50			19.5	
45				18.3	
	+50			17.2	
T.P.		2.67	918.53	9.76	915.86

Gr. Rod

Lt.

E

Pt.

$$5.7 \quad 28.0 / \frac{4.7}{+1.0} \quad \frac{5.0}{+0.7} \quad \frac{4.4}{+1.3 / 29.6}$$

$$4.1 \quad 28.0 / \frac{3.1}{+1.0} \quad \frac{3.5}{+0.6} \quad \frac{2.8}{+1.3 / 28.6}$$

$$3.0 \quad 28.2 / \frac{1.9}{+1.1} \quad \frac{2.6}{+0.9} \quad \frac{2.5}{+0.5 / 27.0}$$

$$2.1 \quad 25.6 / \frac{2.3}{+1.8} \quad \frac{2.2}{-0.1} \quad \frac{3.1}{+1.0 / 29.0}$$

Top Iron S.E. Cor. Cemetery

$$3.5 \quad 29.6 / \frac{9.2}{+0.3} \quad \frac{3.9}{-0.4} \quad \frac{4.1}{+0.8 / 29.6}$$

$$3.6 \quad 29.2 / \frac{5.0}{+0.6} \quad \frac{4.2}{-0.6} \quad \frac{7.9}{+1.2 / 29.9}$$

$$4.0 \quad 29.8 / \frac{4.6}{+1.4} \quad \frac{4.5}{-0.5} \quad \frac{7.3}{+1.7 / 25.9}$$

$$5.0 \quad 27.0 / \frac{4.5}{-0.5} \quad \frac{5.2}{-0.2} \quad \frac{5.0}{+0.0 / 26.0}$$

$$6.1 \quad 27.4 / \frac{4.4}{+1.7} \quad \frac{6.2}{-0.1} \quad \frac{5.7}{-0.4 / 26.5}$$

$$7.3 \quad 27.4 / \frac{4.6}{+0.7} \quad \frac{7.6}{-0.8} \quad \frac{7.9}{+1.9 / 25.9}$$

$$8.4 \quad 29.2 / \frac{9.3}{+1.1} \quad \frac{8.9}{-0.5} \quad \frac{10.4}{+2.0 / 22.0}$$

Sta	+	Δ	-	Grade
		918.53		

46				14.0
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	+50			14.9
--	-----	--	--	------

47				13.7
----	--	--	--	------

	+41			12.8
--	-----	--	--	------

	+44			12.8
--	-----	--	--	------

48				11.7
----	--	--	--	------

	+50			10.9
--	-----	--	--	------

T.P.	4.06	914.91	7.68	910.85
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49				10.2
----	--	--	--	------

	+50			09.8
--	-----	--	--	------

50				09.4
----	--	--	--	------

	+50			09.0
--	-----	--	--	------

Gr. Rod.

Lt.

E.

Rt.

$$2.5 \quad \begin{array}{r} 22.0 / 4.5 \\ \underline{90.0} \end{array} \quad \begin{array}{r} 3.2 \\ \underline{-0.7} \end{array} \quad \begin{array}{r} 45 \\ \underline{-23} / 18.6 \end{array}$$

$$3.6 \quad \begin{array}{r} 20.2 / 6.7 \\ \underline{-91} \end{array} \quad \begin{array}{r} 44 \\ \underline{-0.8} \end{array} \quad \begin{array}{r} 75 \\ \underline{-57} / 15.8 \end{array}$$

$$4.8 \quad \begin{array}{r} 21.0 / 8.8 \\ \underline{-35} \end{array} \quad \begin{array}{r} 55 \\ \underline{-0.7} \end{array} \quad \begin{array}{r} 76 \\ \underline{-38} / 19.6 \end{array}$$

5.7

$$5.7 \quad \begin{array}{r} 19.6 / 8.5 \\ \underline{-38} \end{array} \quad \begin{array}{r} 62 \\ \underline{-0.5} \end{array} \quad \begin{array}{r} 71 \\ \underline{120.6} / 23.2 \end{array}$$

$$6.8 \quad \begin{array}{r} 24.6 / 7.5 \\ \underline{413} \end{array} \quad \begin{array}{r} 71 \\ \underline{-0.3} \end{array} \quad \begin{array}{r} 70 \\ \underline{4.18} / 25.4 \end{array}$$

$$7.6 \quad \begin{array}{r} 25.0 / 8.1 \\ \underline{215} \end{array} \quad \begin{array}{r} 76 \\ \underline{00} \end{array}$$

$$7.7 \quad \begin{array}{r} 25.2 / 5.1 \\ \underline{816} \end{array} \quad \begin{array}{r} 43 \\ \underline{104} \end{array} \quad \begin{array}{r} 32 \\ \underline{+1.5} / 29.0 \end{array}$$

$$5.1 \quad \begin{array}{r} 26.0 / 5.1 \\ \underline{100} \end{array} \quad \begin{array}{r} 47 \\ \underline{104} \end{array} \quad \begin{array}{r} 37 \\ \underline{+1.4} / 28.8 \end{array}$$

$$5.5 \quad \begin{array}{r} 27.4 / 4.8 \\ \underline{40.7} \end{array} \quad \begin{array}{r} 50 \\ \underline{105} \end{array} \quad \begin{array}{r} 43 \\ \underline{+1.2} / 28.9 \end{array}$$

$$5.9 \quad \begin{array}{r} 26.4 / 5.7 \\ \underline{10.2} \end{array} \quad \begin{array}{r} 53 \\ \underline{106} \end{array} \quad \begin{array}{r} 57 \\ \underline{+0.2} / 26.4 \end{array}$$

Sta.	+	π	-	Grade	
		714.91			
51				088	
+36				085	
+95				085	
+52				084	
+62				084	
+718				80.3	
RM			8.16	906.15	906.76

Gr. Rod

LH

K

RH

61

$$24.8 / \frac{6.7}{2.9}$$

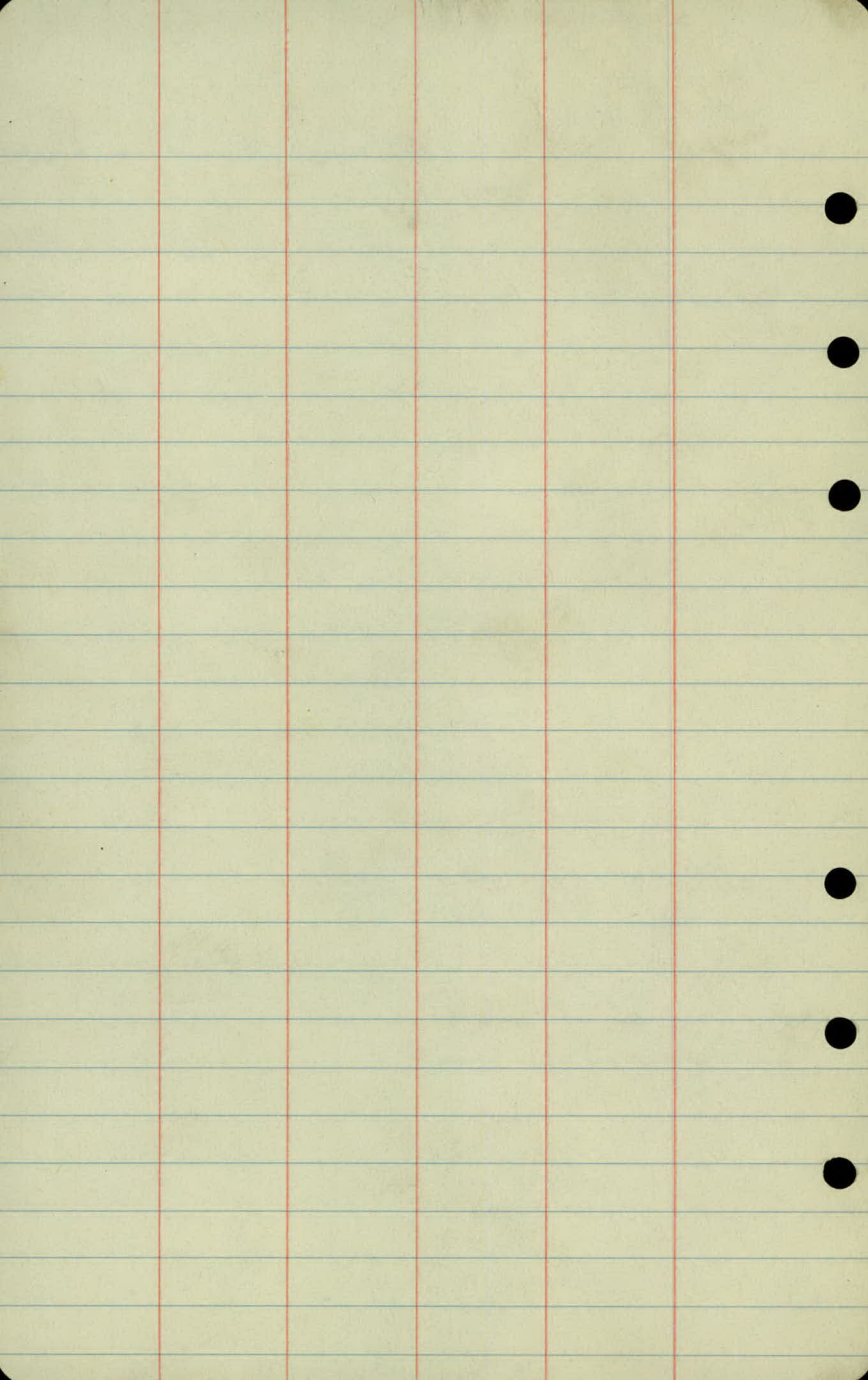
$$\frac{38}{10.3}$$

$$\frac{6.1}{-0.0} / 14.0$$

64

$$\frac{60}{10.4}$$

Spk. in P.A. 85' SE. 10th



Slope Stakes

CEMETARY ROAD

Long Lake Road. 400' W.

Staked - 9-26-39 - 2 sheets

Party
R.O.P.
A.M.
L.G.
C.F.

Sta	+	π	-	Elev.
B.M.	8.37	915.13		906.76
0				05.6

+50				06.0
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1				06.5
---	--	--	--	------

+50				07.0
-----	--	--	--	------

2				07.9
---	--	--	--	------

+50				08.8
-----	--	--	--	------

3				10.0
---	--	--	--	------

+50				11.1
-----	--	--	--	------

4				12.3
---	--	--	--	------

Spike in P.P 32' S.E Sta 7713.5 (Long Lake)

9.5

9.1

$$\begin{array}{r} 9.5 \\ 21.6 \\ \hline 25.2 \end{array}$$

$$\begin{array}{r} 5.9 \\ 3.2 \\ \hline 3.2 \end{array}$$

$$\begin{array}{r} 7.5 \\ 1.6 \\ \hline 29.2 \end{array}$$

8.6

$$\begin{array}{r} 6.8 \\ 1.8 \\ \hline 29.6 \end{array}$$

$$\begin{array}{r} 5.2 \\ 3.4 \\ \hline 3.4 \end{array}$$

$$\begin{array}{r} 6.2 \\ 2.4 \\ \hline 30.8 \end{array}$$

8.1

$$\begin{array}{r} 5.0 \\ 3.1 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 4.9 \\ 3.2 \\ \hline 3.2 \end{array}$$

$$\begin{array}{r} 5.5 \\ 2.6 \\ \hline 31.2 \end{array}$$

7.2

$$\begin{array}{r} 4.5 \\ 2.7 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 4.6 \\ 2.6 \\ \hline 2.6 \end{array}$$

$$\begin{array}{r} 5.4 \\ 1.8 \\ \hline 29.6 \end{array}$$

6.3

$$\begin{array}{r} 3.6 \\ 2.7 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 4.2 \\ 2.1 \\ \hline 2.1 \end{array}$$

$$\begin{array}{r} 6.0 \\ 0.3 \\ \hline 26.6 \end{array}$$

5.1

$$\begin{array}{r} 2.9 \\ 2.2 \\ \hline 30.4 \end{array}$$

$$\begin{array}{r} 3.7 \\ 1.4 \\ \hline 1.4 \end{array}$$

$$\begin{array}{r} 5.0 \\ 0.1 \\ \hline 26.2 \end{array}$$

4.0

$$\begin{array}{r} 3.5 \\ 0.5 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 3.3 \\ 0.7 \\ \hline 0.7 \end{array}$$

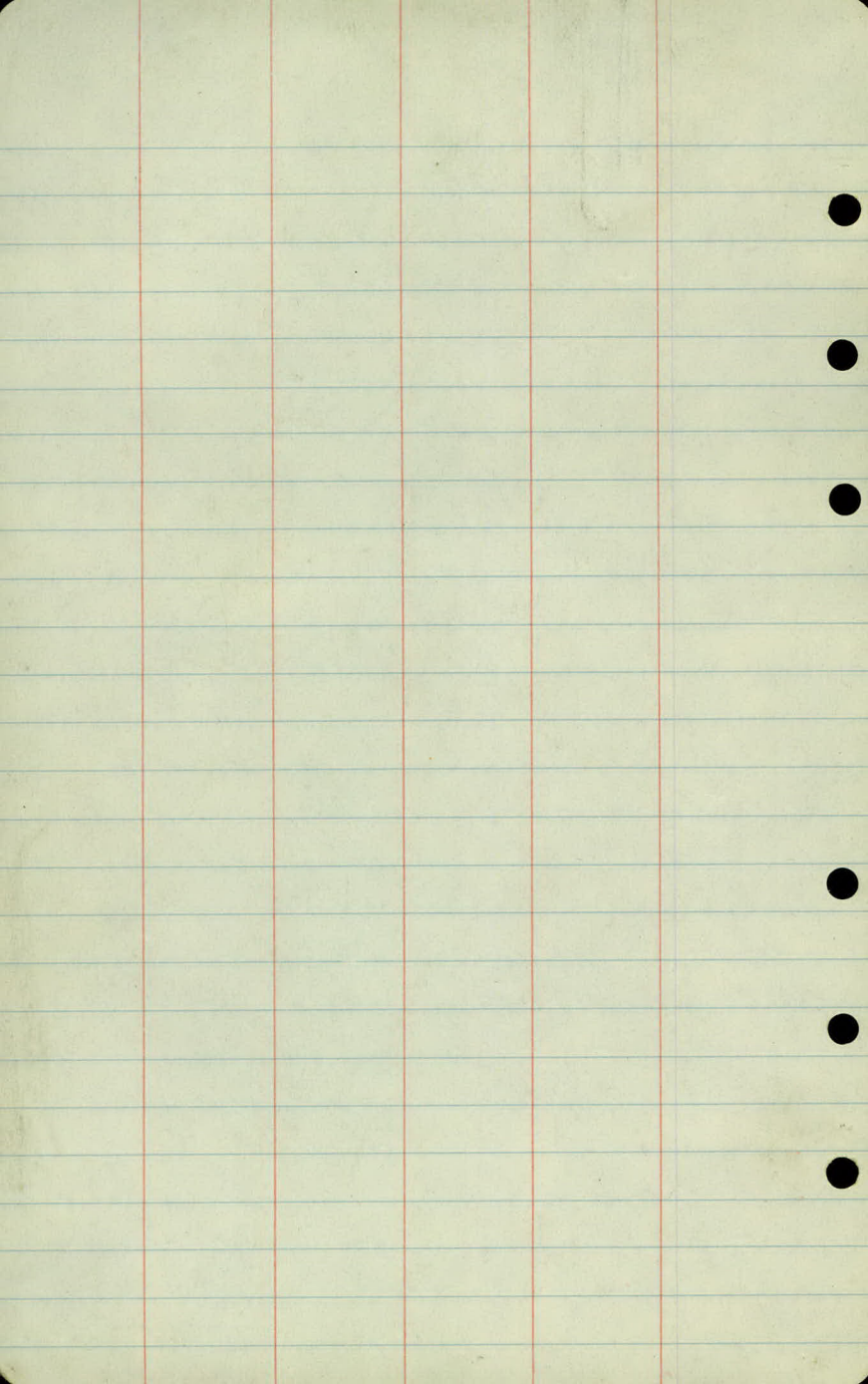
$$\begin{array}{r} 4.0 \\ 0.9 \\ \hline 26.0 \end{array}$$

2.8

$$\begin{array}{r} 4.8 \\ 0.0 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 2.8 \\ 0.0 \\ \hline 0.0 \end{array}$$

$$\begin{array}{r} 4.7 \\ 0.1 \\ \hline 22.2 \end{array}$$



June 19, 1967

1

CEMETERY ROAD

Silver Lake Road to 1000' East

PROFILE

Sta Point ΔL ΔR

0+00

0+00 According to R.L. S. No 74 + 41

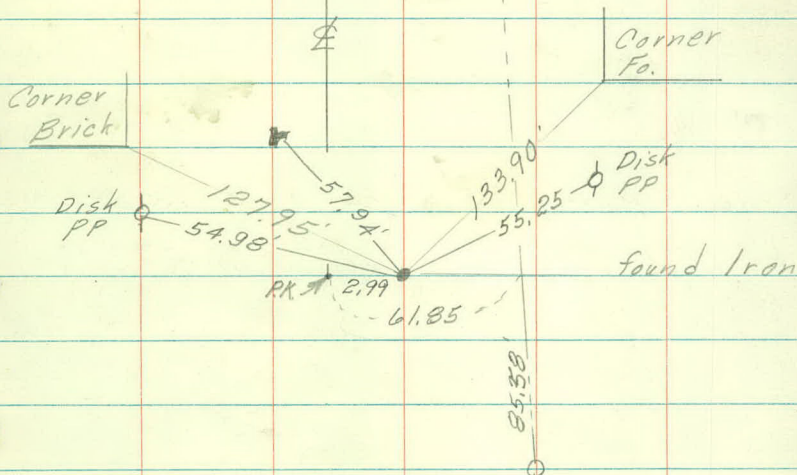
P. I. of $\pm$ Silver Lake Road = Iron

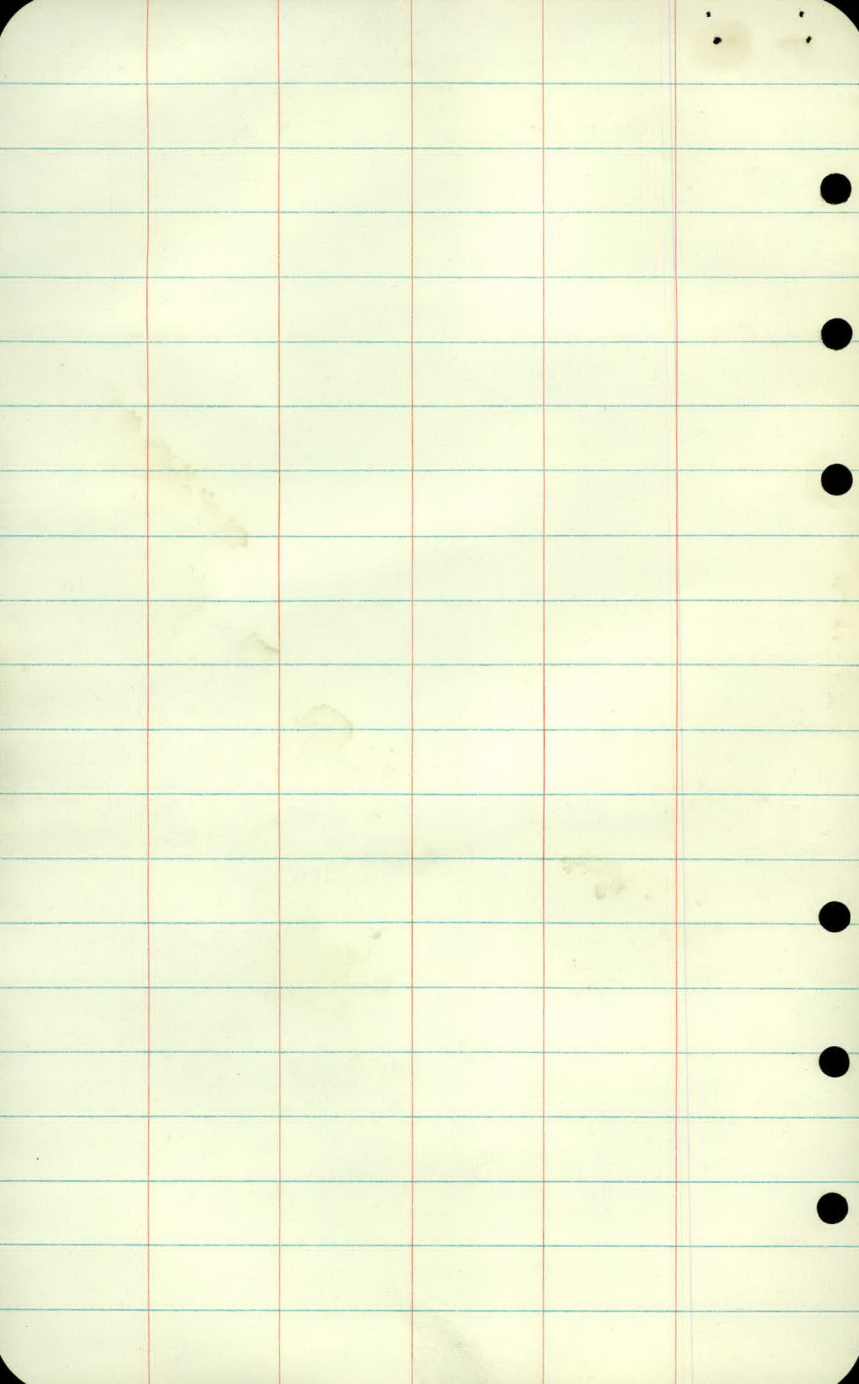
FK
LPD
HL

June 19, 1967

2

⊥





June 20, 1967

3

Profile

Sta	+	π	-	Elev.
BM	3.33	993.43		990.10

	1.80	991.63	91.5
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	3.0	90.4	90.5
--	-----	------	------

0+00 $\nless$ Silver Lake Road

+27 Gutter Line

+45		5.0	88.4
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+63 $\nless$ Ent Lt

1		10.5	82.9
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TP	1.98	983.74	11.67	981.76
----	------	--------	-------	--------

+50		5.7	78.0
-----	--	-----	------

2		9.9	73.8
---	--	-----	------

PK
LPD
HL

June 20, 1967 4

Top Hyd N.E. Corner Cemetery Road
and Silver Lake Road

Garage floor Rt 90468

86.4	88.5	89.9	90.8	91.5
7.0	4.9	3.5	2.6	1.9
100	50		50	100

		89.4		
5.4	4.7	4.0	3.5	3.0
50	25		25	50

87.8	86.5	86.6	86.2	86.6
5.6	6.9	6.8	7.2	6.8
54	36	22	19	

W Edge MH & Sta 1+11

Sta + π - Elev

983.74

2+40 E Ent Rt

✓

TP 0.22 970.17 13.79 969.95

+93 2.81 67.4

3

+10 W. Edge Ent

+33 E. Edge Ent

+58 6.5 63.7

+89 W. Edge Ent

June 29, 1967

5

10.8	10.5	10.7	10.2
12.9	13.2	13.0	13.5
	15	17	25

11.5	11.1	10.9	10.6
12.2	12.6	12.8	13.1
Garage 100	67	47	

W. Kim MH

66.9
3.3

66.3	66.0	66.2	65.7	65.6	65.7
3.9	4.2	4.0	4.5	4.6	4.5
	15	18	32	59	Apron 83

65.0	64.9	65.1	64.8	64.9	65.4
5.2	5.3	5.1	5.4	5.3	4.75
	15	19	31	55	Apron 82

62.3	62.1	62.3	62.0	62.3	62.8	62.2
7.9	8.1	7.9	8.2	7.9	7.4	7.0
	15	18	29	58	81	99

Sta + Δ - Elev.

970.17

4+06

+50

9.9

603

+88 Walk Rt

5

11.0

592

BM 4.70 965.37 9.50 960.67

+50

6.7

58.7

+77 $\pm$ 23 Rd Ave N.W.

✓

6

7.0

58.4

June 20, 1967 6

6.1	6.3	6.5	6.1	6.3	6.2
8.5	8.9	8.7	8.5	7.9	7.0
	15	18	33	67	99
				Walk	Apron

59.4	60.0	62.0
10.8	10.2	8.2
	29	62
	Walk	

Top Hyd

58.5	58.3	58.6	59.2	60.0
6.87	7.1	6.8	6.2	5.4
MH	25	50	75	100

64.3	61.9
1.1	3.5
200	150

Sta + π - Elev.

965.37

6 +37 $\pm$ Ent Lt.

+50

74

58.0

7

8.1

57.3

8.9

+50

8.8

56.6

+69 MA $\pm$

9.07

56.3

+78 Ent Rt.

8 = T.P. 2.18 957.91 9.64 955.73

+50

3.2

54.7

+86 $\pm$ Ent Lt.

9

44

53.5

June 20, 1967

7

58.4	58.3	57.9	57.7	57.6	58.1
7.0	7.1	7.5	7.7	7.8	7.3
69	56	32	19	17	

Garage

56.2	55.9	56.1	56.7	59.2
9.2	9.5	9.3	8.7	6.2
16	17	34	63	

53.9	53.5	53.7	54.7	55.9	57.1
4.0	4.4	4.2	3.2	2.0	0.80
17	19	30	54	74	

Apron

Sta	+	-	Elev.
-----	---	---	-------

957.91

9+06	MH $\pm$	4.50	53.4
------	----------	------	------

+50		58	52.1
-----	--	----	------

+75	$\pm$ Ent Lt.		
-----	---------------	--	--

10		7.8	50.1
----	--	-----	------

+12	$\pm$ Ent Rt.		
-----	---------------	--	--

+50		10.1	47.8
-----	--	------	------

11		12.5	45.4
----	--	------	------

T.P.	8.32	965.59	0.64	957.27
------	------	--------	------	--------

T.P.	13.25	978.22	0.62	964.97
------	-------	--------	------	--------

T.P.	13.62	990.52	1.32	976.90
------	-------	--------	------	--------

BM			0.43	990.09 (990.10)
----	--	--	------	-----------------

Lt.

June 20, 1967 8
RT

5.5	52.9	52.2	51.2	51.0	51.2
4.35	5.0	5.7	6.7	6.9	6.7
5.06	6.9	4.8	2.5	1.6	
8.7					

49.6	49.2	49.9	50.9	52.1
8.3	8.7	8.0	7.0	5.8
	1.7	4.1	6.9	10.0

Top Hyd NE Corner Silver Lake Road and
Cemetery Road

Sta	+	π	-	Elev.
BM	0.18	990.28		990.10

0445

✓

+75

✓

/

FX
LPR
HL

June 26, 1967 9

88.2	88.1	88.4	88.0	88.5	88.8	89.3	89.1/2	89.6
21	22	19	23	18	15	10	11.5	0.7
53	31	23	22		17	18	23	45
							NH	

87.5-
28
65

90.4
101
87

89.3
0.5
63

87.2	85.6	85.2	84.9	85.4	85.2	85.5	85.9	86.3
3.1	4.7	5.1	5.4	4.9	5.1	4.8	4.4	4.0
42	31	21	19		16	17	20	28

88.2
2.1
54

88.3
2.0
64

88.3
2.0
81

89.9
0.4
72

89.3
1.0
58

89.2
2.1
43

84.1	82.6	82.7	82.4	82.9	82.6	83.3	83.8	84.2
6.2	7.7	7.6	7.9	7.4	7.7	7.0	6.5	4.1
33	22	20	18		16	19	27	42

87.4
2.9
46

88.5/2
17.5
65

88.5/0
17.8
81

Conc. Ent.

90.0
0.3
87
H0
Elev.

94.0
0.3
78

88.9
1.4
60

Sta + π - Elev.

990.28

1+25

✓

+50

✓

TP 1.02 979.11 12.19 978.09 1+50 $\angle$

+75

✓

June 26, 1967

10

Lt.

RT

83.8	81.0	80.5	80.0	80.4	80.2	81.0	81.9	86.0
6.5	9.3	9.8	10.3	9.9	10.1	9.3	7.4	4.3
39	27	20	18		16	19	32	51

87.1	88.0	88.59
3.2	2.3	1.59
52	59	60

Conc Stoop

94.0	89.1
0.3	1.2
87	70

78.8	77.9	78.2	78.0	77.1	77.7	78.3	79.0
11.5	12.4	12.1	12.3	12.2	12.6	12.0	11.3
32	23	19	17		16	18	21

80.5	81.5	87.3	85.2	83.5	80.8	78.9
9.8	8.8	3.0	5.1	6.8	9.5	11.4
45	64	82	71	58	42	28

76.2	75.9	76.1	75.8	75.9	75.6	76.1	76.7	76.7
2.9	3.2	3.0	3.3	3.3	3.5	3.0	2.4	2.2
38	28	19	18		15	17	21	34

77.4	77.7	77.9	80.2	79.2	78.4
1.7	1.4	1.2	+11	+0.1	0.7
54	72	100	80	63	47

Sta + π - Elev

979.11

2+00

✓

+28

✓

3 $\pm$

12.20 966.91 (66.9)

June 26, 1967

Lt.

£

51

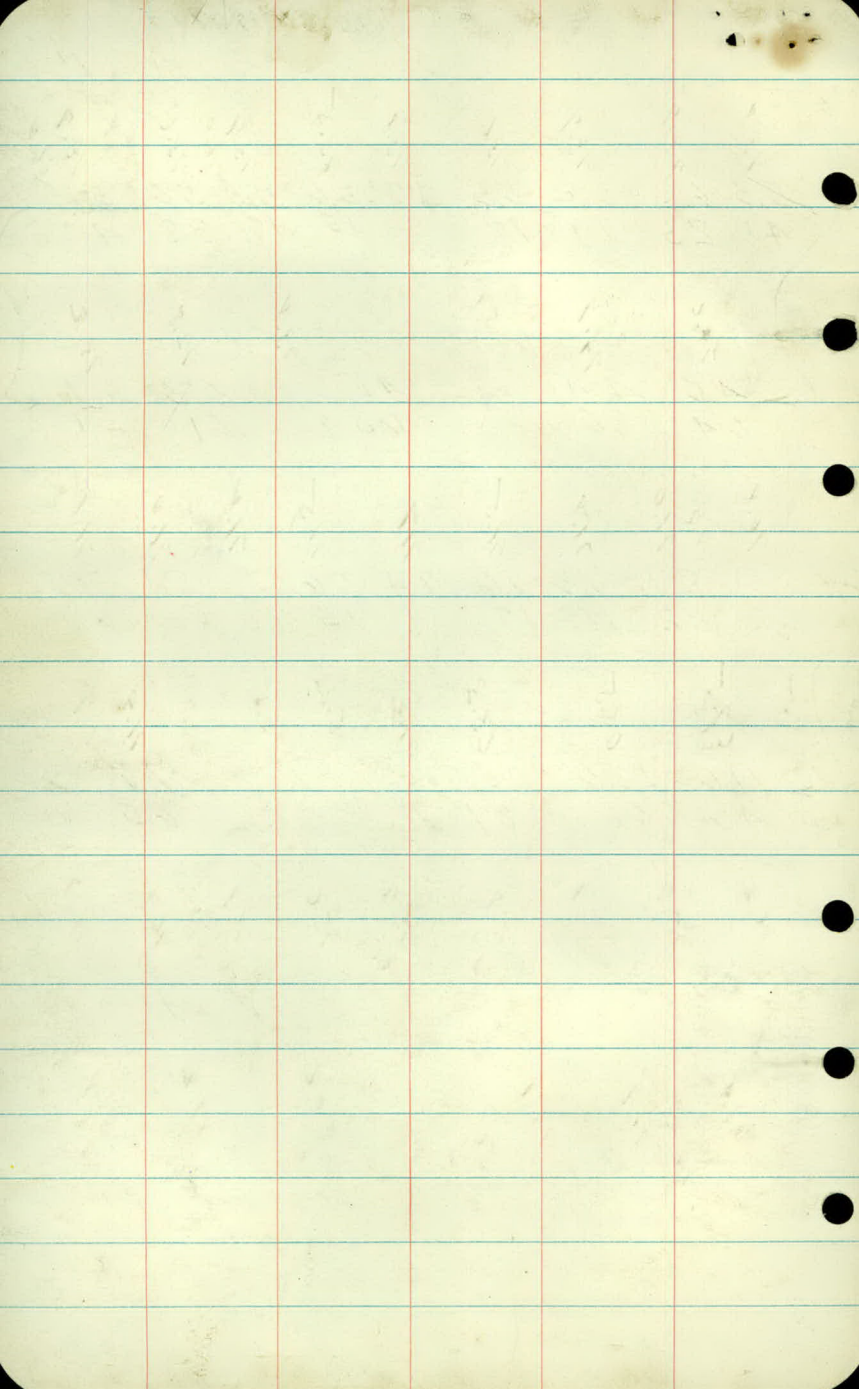
11

73.8	72.9	73.9	73.6	73.8	73.5	73.9	73.6	73.9
5.3	6.2	5.2	5.5	5.3	5.6	5.2	5.5	5.2
40	25	19	18	15	18	28	42	

74.6	74.7	73.8	72.8	73.2
4.5	4.4	4.1	5.2	6.3
64	88	100	80	61

70.8	71.0	71.8	71.5	71.7	71.5	71.8	71.0	71.1
8.3	8.1	7.3	7.6	7.4	7.6	7.3	8.1	8.0
32	22	18	17	15	18	30	47	

62.5	63.5	63.3	71.4
11.6	15.6	15.8	7.7
45	61	81	65



EX
DM
DM
WF

July 10, 1968

12

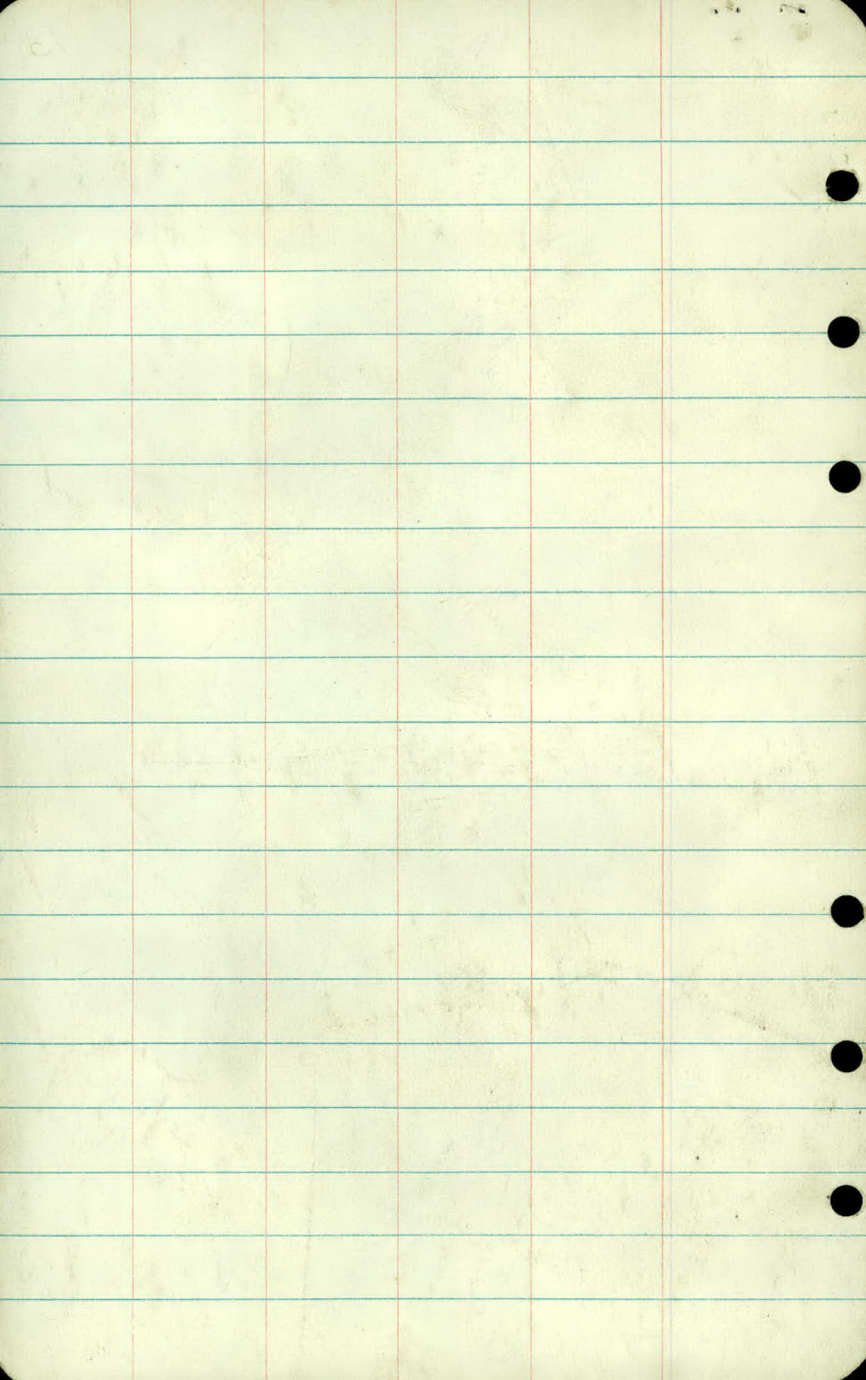
Staking Grade
at
Property Line

33' Lt. Sta to 7+50

Sta	PG	PGR	SWGR	Elev.
BM	2.64	963.31		960.67
4+50	59.91	3.40	2.90	✓
5	58.97	4.34	3.84	✓
+50	58.61	4.70	4.20	✓
6	58.30	5.01	4.51	✓
			4.78	958.53
+50	957.90	5.41	4.91	✓
7	57.30	6.01	5.51	✓
+50	56.52	6.79	6.29	✓
8	55.59			

July 10, 1968

13



7TH St. N.W

Culvert Elevations

Sta	+	X	-	Elev.
TBM	2.07	920.75		918.68
BM			7.04	913.71
TP	0.47	908.46	12.76	907.99
BM			9.64	898.82
TP	1.35	896.39	13.42	895.04
TP	0.71	885.89	11.21	885.18 (884.7)

Inv. Elev.

E. Pipe	Top	12.29	873.70 - 15 =	872.2
Ct. Pipe	Top	12.29		-872.2
W. Pipe	Top	12.18		-872.3
MH		0.58	885.31	(884.8)
BM	2.49	885.89	2.49	883.40
TP	11.97	897.14	0.72	885.17
TP	13.10	909.87	0.37	896.77
T.P.	12.44	920.07	2.24	907.63
TBM			1.33	918.74 918.68

EX.
LPD
RP
HL

August 17, 1965

Clear 70°

2

Spike in P.P. S. side 7th Opp. Ent. to Cemetery

Top Hyd S.W. Cor 12th Ave N.W. & 7th St.

Top Hyd S.W. Cor 13th Ave N.W. & 7th St.

Top M.H.

} S. Side 7th St.

Top of Gas pipe at House

M.H.

Spike in PP S. side 7th Opp. Ent. to Cemetery

