

Dr 11-A - BK ¹⁷~~11~~

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ PLAN. _____ Survey

_____ ARBOGAST ROAD _____

From Victoria St. To N. Quassa Blvd.

Road Acc't. No. _____

Date Filed _____

File _____

ARBOGAST ROAD

From intersection with
Victoria St. to No Onassso Blvd.

5/12/38

Angle

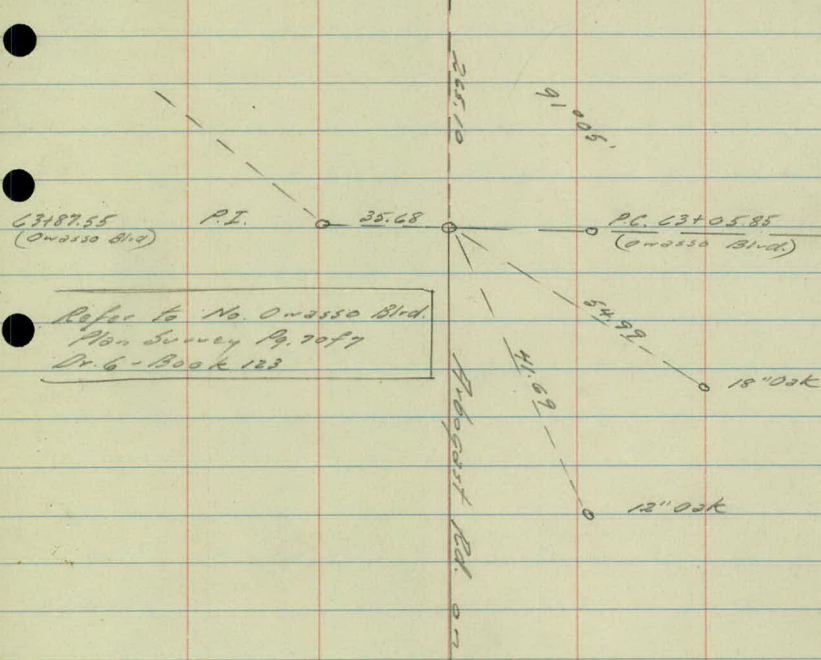
Sta.	Point	Lt.	Rt.
------	-------	-----	-----

+74.7 (Intersection with curve of Onwasso Blvd No. 27° curve)

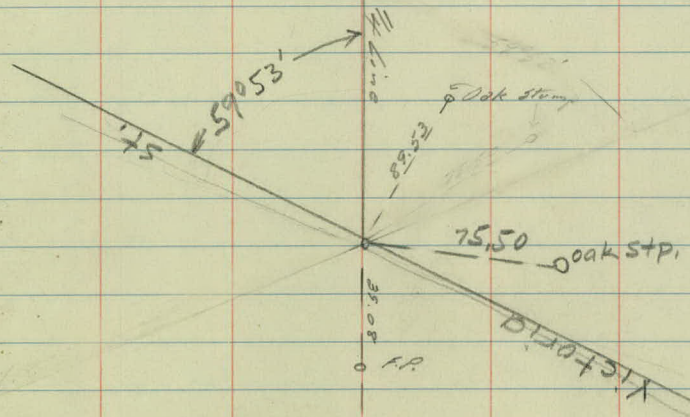
13+69.70 P.I. (No. Onwasso Blvd.)

0+00 = P.I. (Victoria St.)

E 1/4 Cor. Sec. 35 T 30 N. R 23 W. Stone Mon.

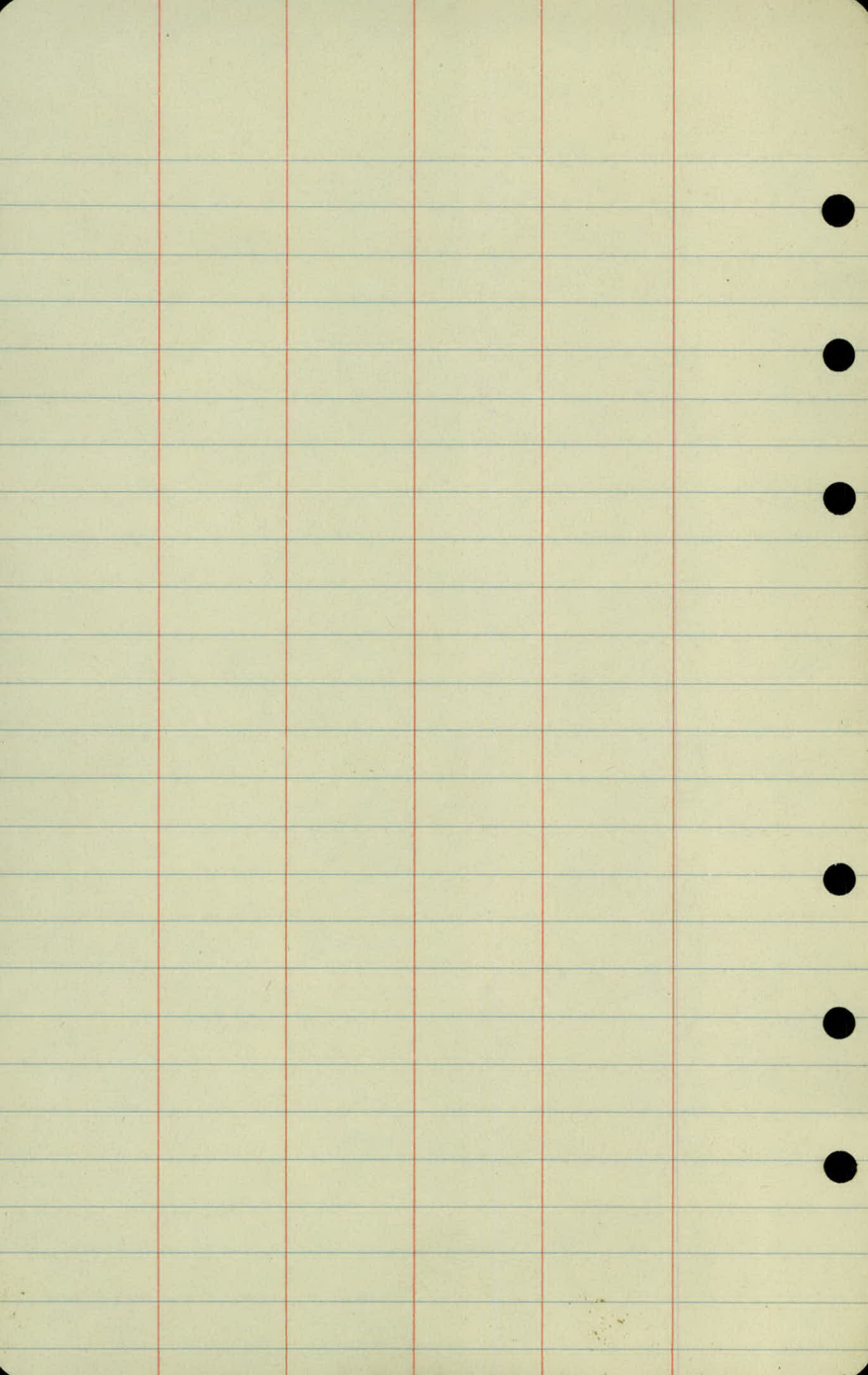


Refer to No. Onassso Blvd.
Non Survey Pg. 70 of 7
Dr. 6 - Book 123



Ch. Sec. 35

Stone Mon.



ARBOGAST ROAD.

Topography from Victoria St.
to No. Arasso Blvd. 5/13/38

6500

25-6
Travelled
Road.

5400

25-6

4400

26-7

3400

26-7

2400

Travelled
Road

25-5

1400

Travelled
Road

0400

26-6

11.10.11

Travelled
Road.

12+00

25-7

11+00

27-8

10+00

28-6

9+00

27-7

Travelled Road

8+00

27-7 →

7+00

27-6

6+00

726

125-

Positive

100'

+ 04 - 14' wide Gate
Field Ent

470

200'

Scattered Oaks
& Brush

1001

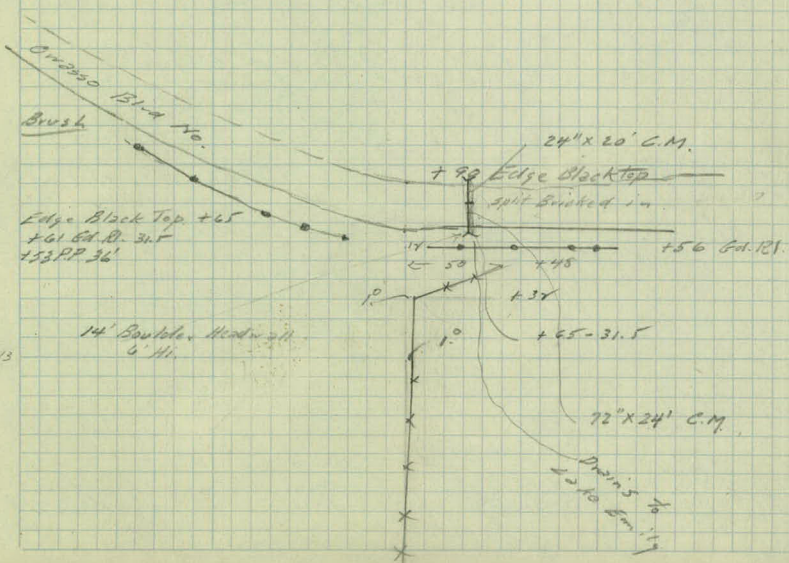
Cultivated

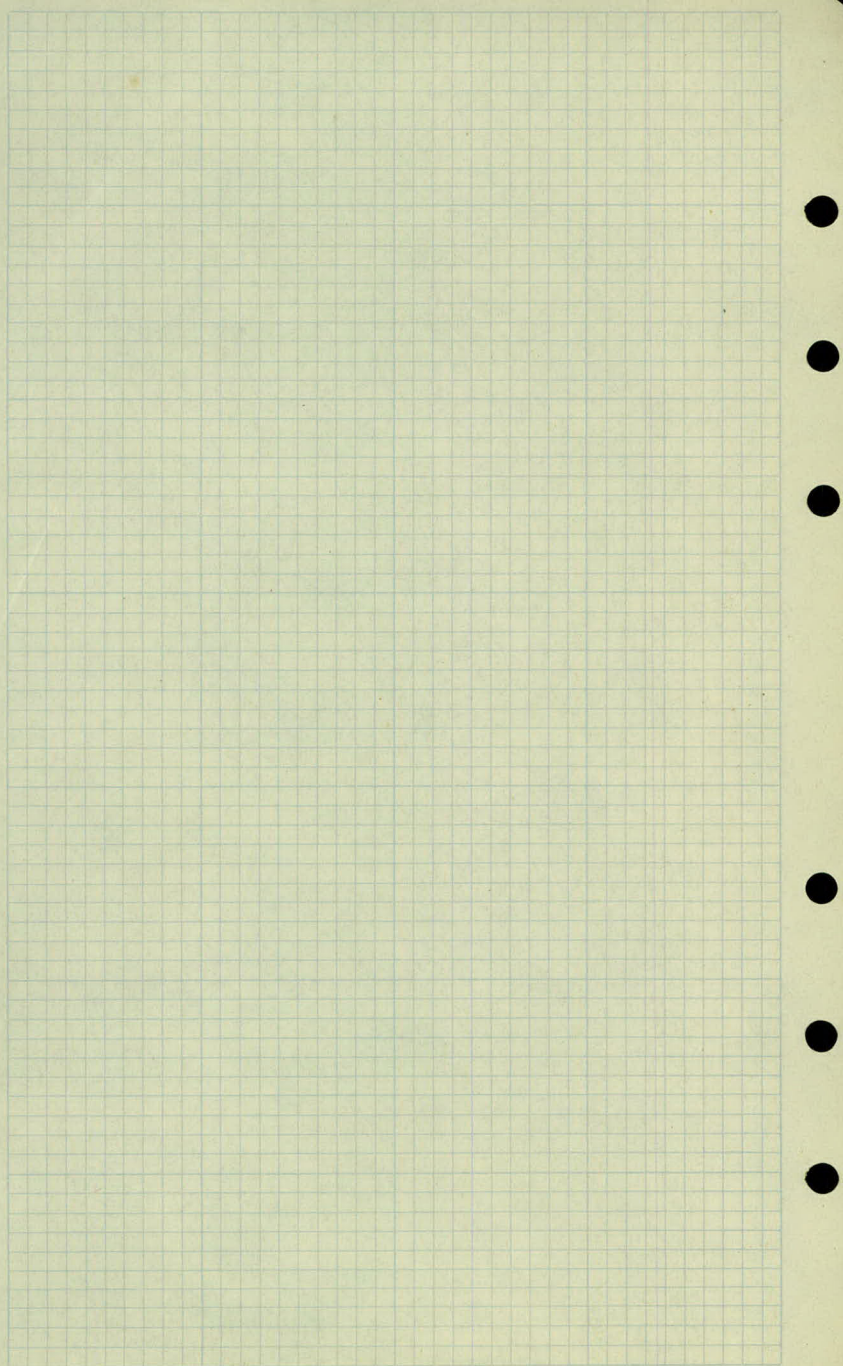
1000

Traveled
Road.

13400

25-7





2
ARBOGAST ROAD.

Cross Sections 8/3/58

Sta.	+	π	-	Elev.
B.M.	1.91	946.01		944.10

0+00	E Vict		43.3
------	--------	--	------

0+21	Shoulder Vict		42.6
------	---------------	--	------

0+25	} Ditch Vict.		40.6
0+34			40.4

24" C.M. Culvert 110' North of Arbogast Rt.

24" C.M. " 110' South of " "

0+37		41.2
------	--	------

0+63		42.4
------	--	------

1+00		42.6
------	--	------

+37		38.6
-----	--	------

+65		37.7
-----	--	------

+70		37.9
-----	--	------

Lt.

L

Rt

Spike in 10" Stump 35' Rt 56.0+22

Braille to Victoria

$$\frac{31}{100}$$

$$\frac{2.7}{1}$$

$$\frac{2.2}{100}$$

$$\frac{36}{100}$$

$$\frac{2.4}{1}$$

$$\frac{2.8}{100}$$

$$\frac{67}{100}$$

$$\frac{52}{61}$$

$$\frac{46}{57}$$

$$\frac{37}{23}$$

$$\frac{40}{9}$$

$$\frac{5.4}{1}$$

$$\frac{55}{50}$$

$$\frac{51}{100}$$

$$\frac{67}{100}$$

$$\frac{46}{44}$$

$$\frac{40}{29}$$

$$\frac{43}{9}$$

$$\frac{55}{5}$$

$$\frac{56}{1}$$

$$\frac{55}{50}$$

$$\frac{54}{100}$$

West End.

$$39.8$$

$$\frac{6.2}{1}$$

East End

$$\frac{6.7}{1}$$

$$39.3$$

West End.

$$40.5$$

$$\frac{5.5}{1}$$

East End

$$\frac{5.6}{1}$$

$$40.4$$

$$\frac{32}{50}$$

$$\frac{36}{26}$$

$$\frac{41}{10}$$

$$\frac{55}{6}$$

$$\frac{5.3}{1}$$

$$\frac{48}{1}$$

$$\frac{5.3}{28}$$

$$\frac{51}{50}$$

$$\frac{4.2}{50}$$

$$\frac{34}{28}$$

$$\frac{54}{25}$$

$$\frac{45}{19}$$

$$\frac{46}{7}$$

$$\frac{56}{5}$$

$$\frac{56}{2}$$

$$\frac{36}{1}$$

$$\frac{44}{26}$$

$$\frac{50}{50}$$

$$\frac{59}{50}$$

$$\frac{50}{31}$$

$$\frac{65}{29}$$

$$\frac{55}{15}$$

$$\frac{58}{7}$$

$$\frac{62}{3}$$

$$\frac{34}{1}$$

$$\frac{33}{20}$$

$$\frac{46}{50}$$

$$\frac{68}{50}$$

$$\frac{21}{39}$$

$$\frac{24}{31}$$

$$\frac{54}{26}$$

$$\frac{26}{15}$$

$$\frac{80}{6}$$

$$\frac{29}{4}$$

$$\frac{23}{2}$$

$$\frac{74}{1}$$

$$\frac{61}{15}$$

$$\frac{5.8}{20}$$

$$\frac{54}{50}$$

$$\frac{54}{45}$$

$$\frac{105}{39}$$

$$\frac{106}{28}$$

$$\frac{93}{25}$$

$$\frac{87}{15}$$

$$\frac{50}{3}$$

$$\frac{54}{2}$$

$$\frac{83}{1}$$

$$\frac{68}{14}$$

$$\frac{69}{50}$$

$$\frac{111}{50}$$

$$\frac{110}{20}$$

$$\frac{116}{27}$$

$$\frac{25}{25}$$

$$\frac{88}{15}$$

$$\frac{21}{3}$$

$$\frac{81}{1}$$

$$\frac{67}{20}$$

$$\frac{68}{50}$$

Sta.	+	Σ ✓ 946.01	-	Elev.
2+00				37.4
+65				35.4
+96	12" Culvert			
3+00				36.6
+42				40.3
T.P.	5.36	¹ 947.56	8.81	937.20 ✓
+72				40.8
4+00				39.7
+55				35.2
5+00				32.6
+50				31.5
6+00				30.6
+45				32.3

Lt.

E

Rt.

9

$\frac{116}{100}$	$\frac{116}{50}$	$\frac{109}{27}$	$\frac{100}{25}$	$\frac{92}{15}$	$\frac{96}{3}$	$\frac{89}{1}$	$\frac{86}{1}$	$\frac{80}{9}$	$\frac{76}{26}$	$\frac{70}{50}$
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$\frac{118}{100}$	$\frac{115}{50}$	$\frac{110}{27}$	$\frac{100}{27}$	$\frac{97}{17}$	$\frac{101}{7}$	$\frac{106}{1}$	$\frac{103}{6}$	$\frac{87}{50}$
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34.3 33.9 $\frac{1}{100}$ Ditch 32.0

34.7	$\frac{100}{11.3}$	$\frac{100}{11.7}$	$\frac{121}{100}$	$\frac{140}{200}$
------	--------------------	--------------------	-------------------	-------------------

$\frac{114}{100}$	$\frac{114}{50}$	$\frac{113}{30}$	$\frac{97}{26}$	$\frac{93}{16}$	$\frac{97}{7}$	$\frac{102}{4}$	$\frac{94}{1}$	$\frac{93}{23}$	$\frac{95}{50}$
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$\frac{108}{50}$	$\frac{98}{37}$	$\frac{91}{34}$	$\frac{88}{29}$	$\frac{87}{18}$	$\frac{81}{8}$	$\frac{56}{4}$	$\frac{57}{1}$	$\frac{64}{13}$	$\frac{76}{50}$
------------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------

$\frac{47}{50}$	$\frac{30}{36}$	$\frac{55}{28}$	$\frac{52}{17}$	$\frac{56}{8}$	$\frac{24}{3}$	$\frac{18}{1}$	$\frac{24}{18}$	$\frac{37}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------

$\frac{41}{50}$	$\frac{33}{34}$	$\frac{61}{27}$	$\frac{58}{16}$	$\frac{64}{7}$	$\frac{34}{3}$	$\frac{29}{1}$	$\frac{35}{20}$	$\frac{44}{50}$
-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------

$\frac{75}{50}$	$\frac{81}{40}$	$\frac{27}{30}$	$\frac{81}{27}$	$\frac{28}{16}$	$\frac{83}{6}$	$\frac{75}{3}$	$\frac{74}{1}$	$\frac{29}{21}$	$\frac{82}{50}$
-----------------	-----------------	-----------------	-----------------	-----------------	----------------	----------------	----------------	-----------------	-----------------

$\frac{88}{50}$	$\frac{91}{44}$	$\frac{101}{27}$	$\frac{81}{26}$	$\frac{83}{16}$	$\frac{97}{6}$	$\frac{101}{4}$	$\frac{100}{1}$	$\frac{104}{20}$	$\frac{105}{50}$
-----------------	-----------------	------------------	-----------------	-----------------	----------------	-----------------	-----------------	------------------	------------------

$\frac{108}{50}$	$\frac{115}{33}$	$\frac{108}{30}$	$\frac{102}{26}$	$\frac{100}{16}$	$\frac{104}{6}$	$\frac{111}{3}$	$\frac{111}{1}$	$\frac{112}{14}$	$\frac{108}{34}$	$\frac{110}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{173}{50}$	$\frac{173}{38}$	$\frac{113}{30}$	$\frac{107}{27}$	$\frac{105}{25}$	$\frac{102}{16}$	$\frac{106}{7}$	$\frac{118}{4}$	$\frac{170}{1}$	$\frac{124}{3}$	$\frac{118}{18}$	$\frac{118}{41}$	$\frac{112}{50}$
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$\frac{110}{50}$	$\frac{112}{44}$	$\frac{115}{30}$	$\frac{109}{28}$	$\frac{106}{26}$	$\frac{100}{14}$	$\frac{102}{6}$	$\frac{103}{1}$	$\frac{115}{37}$	$\frac{118}{50}$
------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------

Drains to →
Lake Equia

Sta.	+	$\bar{K}_s$	-	Elev.
		947.56		
7+00				36.5
T.P.	5.78	939.12	9.22	933.34
+50				36.9
8+00				35.2
+50				33.8
9+00				32.6
+32				29.5
T.P.	6.48	935.46	10.14	928.98
+55				26.6
+80				26.5
10+00				27.5
+35				29.1
+70				27.6
11+00				24.8

17.

2

18.

10

$$\frac{94}{50} \frac{86}{33} \frac{84}{31} \frac{82}{17} \frac{86}{6} \frac{61}{1} \frac{61}{1} \frac{66}{1} \frac{72}{21} \frac{82}{34} \frac{96}{50}$$

$$\frac{56}{50} \frac{58}{44} \frac{50}{34} \frac{58}{31} \frac{58}{27} \frac{52}{17} \frac{56}{7} \frac{51}{4} \frac{23}{1} \frac{22}{1} \frac{22}{18} \frac{35}{34} \frac{51}{50}$$

$$\frac{60}{50} \frac{60}{47} \frac{50}{34} \frac{60}{31} \frac{58}{15} \frac{62}{5} \frac{39}{1} \frac{44}{9} \frac{48}{24} \frac{68}{50}$$

$$\frac{70}{50} \frac{66}{34} \frac{72}{31} \frac{68}{17} \frac{75}{8} \frac{72}{5} \frac{54}{1} \frac{53}{1} \frac{56}{5} \frac{62}{20} \frac{77}{39} \frac{82}{50}$$

$$\frac{98}{50} \frac{98}{31} \frac{92}{27} \frac{86}{16} \frac{90}{7} \frac{87}{4} \frac{65}{1} \frac{66}{5} \frac{67}{23} \frac{106}{50}$$

$$\frac{104}{50} \frac{108}{30} \frac{102}{28} \frac{98}{17} \frac{100}{8} \frac{101}{2} \frac{96}{1} \frac{99}{12} \frac{44}{37} \frac{145}{50}$$

$$\frac{59}{50} \frac{68}{37} \frac{75}{34} \frac{72}{29} \frac{69}{18} \frac{74}{7} \frac{89}{1} \frac{96}{1} \frac{125}{36} \frac{137}{50}$$

$$\frac{48}{50} \frac{65}{39} \frac{75}{35} \frac{76}{29} \frac{75}{17} \frac{78}{8} \frac{90}{1} \frac{104}{1} \frac{124}{24} \frac{150}{50}$$

$$\frac{30}{50} \frac{35}{42} \frac{74}{35} \frac{76}{28} \frac{77}{15} \frac{83}{4} \frac{77}{2} \frac{80}{1} \frac{92}{4} \frac{116}{22} \frac{145}{50}$$

$$\frac{21}{50} \frac{26}{43} \frac{86}{32} \frac{80}{28} \frac{80}{16} \frac{86}{7} \frac{84}{4} \frac{63}{2} \frac{64}{1} \frac{53}{5} \frac{90}{14} \frac{111}{32} \frac{133}{50}$$

$$\frac{68}{50} \frac{70}{39} \frac{95}{34} \frac{92}{28} \frac{93}{19} \frac{99}{7} \frac{81}{2} \frac{79}{1} \frac{91}{6} \frac{100}{20} \frac{132}{50}$$

$$\frac{100}{50} \frac{105}{34} \frac{102}{28} \frac{105}{26} \frac{103}{16} \frac{107}{9} \frac{104}{7} \frac{107}{10} \frac{110}{7} \frac{111}{16} \frac{129}{36} \frac{147}{50}$$

Sta.	+	K _v	-	Elev.
		935.46		
T.P.	8.67	933.27	10.86	924.60
11+50				23.5
12+00				21.6
+34				20.7
+77				23.7
13+00				26.2
+31				32.5
T.P.	11.20	943.53	0.94	934.33
+45				35.8
+54				37.2
+55				37.3
+63				38.5
+74.7	End of Blvd. No. (Parallel)			38.6
B.M.	1.25	943.53	1.25	942.28

Lt.

E

Rt.

11

Boulder 11x15 Rt. 2'

89	54	89	87	87	98	104	116	130	153
<u>50</u>	<u>34</u>	<u>26</u>	<u>17</u>	<u>7</u>	<u>58</u>	<u>2</u>	<u>24</u>	<u>37</u>	<u>50</u>

85	86	105	86	85	117	126	138	149	168
<u>50</u>	<u>37</u>	<u>31</u>	<u>25</u>	<u>7</u>	<u>57</u>	<u>2</u>	<u>18</u>	<u>23</u>	<u>50</u>

102	117	76	77	126	139	150	162	166
<u>50</u>	<u>31</u>	<u>25</u>	<u>8</u>	<u>56</u>	<u>3</u>	<u>13</u>	<u>46</u>	<u>50</u>

118	118	51	49	51	96	106	107	120	122	121
<u>50</u>	<u>37</u>	<u>25</u>	<u>16</u>	<u>7</u>	<u>46</u>	<u>2</u>	<u>10</u>	<u>15</u>	<u>35</u>	<u>50</u>

111	93	32	30	32	71	81	82	73	20	20
<u>50</u>	<u>37</u>	<u>25</u>	<u>15</u>	<u>7</u>	<u>21</u>	<u>3</u>	<u>6</u>	<u>12</u>	<u>40</u>	<u>50</u>

54	42	30	103	105	105	08	20	22	53	53	15	08
<u>50</u>	<u>34</u>	<u>32</u>	<u>26</u>	<u>7</u>	<u>4</u>	<u>08</u>	<u>6</u>	<u>20</u>	<u>25</u>	<u>28</u>	<u>34</u>	<u>50</u>

132	128	104	82	77	80	100	105	125	128	112	101	101	89
<u>50</u>	<u>48</u>	<u>31</u>	<u>25</u>	<u>27</u>	<u>10</u>	<u>17</u>	<u>24</u>	<u>28</u>	<u>33</u>	<u>35</u>	<u>39</u>	<u>44</u>	<u>50</u>

65	58	57	55	61	61	63	20	24	51	122	125	125	125	125	125	125	125
<u>50</u>	<u>48</u>	<u>38</u>	<u>31</u>	<u>26</u>	<u>10</u>	<u>63</u>	<u>6</u>	<u>14</u>	<u>17</u>	<u>24</u>	<u>29</u>	<u>31</u>	<u>31</u>	<u>31</u>	<u>31</u>	<u>31</u>	<u>31</u>

East End
78

61	58	57	55	61	61	62	60	56	50
<u>50</u>	<u>48</u>	<u>38</u>	<u>31</u>	<u>26</u>	<u>10</u>	<u>62</u>	<u>8</u>	<u>30</u>	<u>50</u>

58	48	48	50	50	49	47
<u>50</u>	<u>47</u>	<u>32</u>	<u>14</u>	<u>50</u>	<u>10</u>	<u>50</u>

2.3	4.4	4.9	4.5	2.9
<u>100</u>	<u>50</u>	<u>49</u>	<u>50</u>	<u>100</u>

Pike in 14" oak 50' 50' Arbogast Rt. 40' East Orissa Blvd. No

Sta.

+

K

-

Elev.

943.53

T.P.

6.44

946.74

2.23

940.30

OP

B.M.

2.60

944.14

944.10

ARBORWAY ST.

Victoria St to No. 5000

Blvd. Slope Stakes

6/2/38

Plans dated May 1938.

O - Easements.

- 30' Crown

Slopes 2 to 1. Conform to Easements

Ditch 2' Deep. 19 + 23

27' Backslope to profile grade &

Bratager

Wilke

Goldberg

Moeschter

Sta.	+	π	-	Grade.
B.M.	1.76	945.86		944.10

0+00				43.3
------	--	--	--	------

+21				42.5
-----	--	--	--	------

+25				42.3
-----	--	--	--	------

+34				42.0
-----	--	--	--	------

+37				41.9
-----	--	--	--	------

+63				41.1
-----	--	--	--	------

1+00				39.8
------	--	--	--	------

+37				38.6
-----	--	--	--	------

Lt.

Q

Rt.

2

Spike in 10" stump 35' Rt. 0+22

2.6
4.6

X

3.4
5.4

X

27

3.6
5.6Radios
33
~~27.6~~5.2
F1.65.6
F2.0
19.0

15

27

3.9
5.9

X

24

29

4.0
6.03.4
C.O.B
28.24.7
F0.75.1
D.C.O.9
24.8

25

27

4.8
6.84.6
C.O.2
27.43.5
C1.33.9
C.O.9
28.8

28

27

6.1
8.16.2
D.C.1.9
26.83.3
2.83.5
C.2.6
32.2

32

Daylight
317.3
9.39.3
D.C.00
31.07.3
C.O.05.3
C.2.0
31.0

30

5/2 + π - Grade.

945.86

1+65

37.8

+70

37.7

2

36.9

+65

35.6

T.P.

7.30

944.15

9.01

936.85

3

35.0

+42

34.4

+72

34.0

4

33.6

Lt.

Z

124.

3

Daylight
288.1
10.1

X

30

Daylight
26.58.7
10.7
$$\begin{array}{r} 10.7 \\ DC.00 \\ \hline 27.0 \end{array}$$

$$\begin{array}{r} 8.0 \\ \hline 6.0.7 \end{array}$$

$$\begin{array}{r} 6.4 \\ \hline 6.1.8 \\ \hline 30.6 \end{array}$$

30

Daylight
279.0
11.0
$$\begin{array}{r} 11.0 \\ DC.00 \\ \hline 29.0 \end{array}$$

$$\begin{array}{r} 8.5 \\ \hline 6.0.1 \end{array}$$

$$\begin{array}{r} 7.9 \\ \hline 6.1.1 \\ \hline 29.2 \end{array}$$

30.5

Daylight
2910.3
12.3
$$\begin{array}{r} 11.1 \\ DC.1.4 \\ \hline 30.1 \end{array}$$

$$\begin{array}{r} 10.5 \\ \hline 6.0.7 \end{array}$$

$$\begin{array}{r} 9.3 \\ \hline 6.1.0 \\ \hline 29 \end{array}$$

29

Daylight
30.09.1
11.1
$$\begin{array}{r} 9.4 \\ DC.1.7 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 7.5 \\ \hline 6.1.6 \end{array}$$

$$\begin{array}{r} 6.0 \\ \hline 3.1 \\ \hline 33.0 \end{array}$$

31

32

9.7
11.7
$$\begin{array}{r} 7.4 \\ \hline 6.2.3 \\ \hline 31.6 \end{array}$$

$$\begin{array}{r} 3.8 \\ \hline 6.1.9 \end{array}$$

$$\begin{array}{r} 5.5 \\ \hline 6.4.2 \\ \hline 35.4 \end{array}$$
+20
(36)

(38)

10.1
12.1
$$\begin{array}{r} 5.1 \\ \hline 6.5.0 \\ \hline 37.0 \end{array}$$

$$\begin{array}{r} 3.4 \\ \hline 6.7 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline 6.5.6 \\ \hline 38.2 \end{array}$$

(38)

(39)

10.5
12.5
$$\begin{array}{r} 5.3 \\ \hline 6.5.4 \\ \hline 37.4 \end{array}$$

$$\begin{array}{r} 4.5 \\ \hline 6.0 \end{array}$$

$$\begin{array}{r} 5.4 \\ \hline 6.5.1 \\ \hline 37.2 \end{array}$$

(38)

(430)

Sta.	+	π	-	Elev.
		944.15		

4+55				32.8
------	--	--	--	------

T.P.	4.42	938.16	10.41	933.24
------	------	--------	-------	--------

5				32.2
---	--	--	--	------

+50				31.6
-----	--	--	--	------

6				31.0
---	--	--	--	------

+45				30.5
-----	--	--	--	------

7				30.0
---	--	--	--	------

+50				29.6
-----	--	--	--	------

T.P.	5.66	938.83	4.99	933.17
------	------	--------	------	--------

8				29.2
---	--	--	--	------

LT.

E

RT.

4

31.5

11.3
13.3

94
C.1.9
30.8

90
C.2.3

96
C.1.7
30.4

31

(32) Daylight

6.0
8.0

54
C.0.6
28.2

57
C.0.3

60
D.C.2.0
27.0

27

33 Day

6.6
8.6

70
D.C.1.6
33.0

66
C.0.0

66
D.C.2.0
27

27

(38) Day

7.2
9.2

76
D.C.1.6
38.0

76
F.0.4

73
D.C.1.9
26.8

27

28.5 Daylight

7.7
9.7

77
D.C.2.0
31

61
C.1.1

69
C.0.8
28.6

28

(35)

8.2
10.2

44
C.3.8
34.6

18
C.6.4

40
C.4.2
35.4

180
(36)

(36)

86
10.6

42
C.4.4
35.8

12
C.7.4

30
C.5.6
38.2

(35)

(36)

96
11.6

17
C.4.9
36.8

37
C.8.9

55
C.4.1
35.2

(36)

Sta.	+	π	-	Grade.
		938.83		

8+50				28.8
------	--	--	--	------

9				28.4
---	--	--	--	------

+32				28.1
-----	--	--	--	------

+55				28.0
-----	--	--	--	------

T.P.	3.61	938.50	9.94	928.89
------	------	--------	------	--------

+80				27.8
-----	--	--	--	------

				Ditch Grade
10				27.6 25.6

+35				27.7 25.5
-----	--	--	--	-----------

+70				28.1 25.3
-----	--	--	--	-----------

17.

2

12.

34

10.0
12.0

6.3
C.3.7
34.4

5.0
C.5.0

2.0
C.3.0
33.0

33.5

29.5

10.4
12.4

9.3
C.1.1
29.2

6.2
C.4.2

7.3
C.3.1
33.0

32.5

28.2

10.7
12.7

10.0
C.0.7
28.4

9.4
C.1.3

11.1
D.C.1.6
26.2

26.5

28

10.8
12.8

10.6
C.0.2
27.4

12.4
F.1.6

15.1
F.4.3
23.6

23

27

4.7
6.7

6.7
D.C.2.0
27.0

6.2
F.1.5

9.7
F.5.0
25.0

24.5

27

6.9

4.7
D.C.2.2
27.4

5.1
F.0.2

8.8
F.3.9
22.8

4.9

22

Special Ditch 17.1
- 0.4 Grade.

27

7.0

5.2
D.C.1.8
26.6

3.5
C.1.3

6.8
D.C.0.0
20.2

4.8

19.2 DC 21

18.5

2.2

6.5
D.C.0.7
24.4

4.9
F.2.0
19.0
F.0.5

7.0
F.2.2
20.2

4.4

20

Sta.	+	π	-	Grade
		931.50		
11+00				28.8 25.2

+50				30.4
T.P.	6.86	931.58	7.78	924.24

12				32.8
----	--	--	--	------

+34				34.5
-----	--	--	--	------

+77				36.5
-----	--	--	--	------

13				37.3
T.P.	8.79	937.27	3.10	928.48

+31				38.1
-----	--	--	--	------

+45				38.3
-----	--	--	--	------

LT.

E

RT.

6

↓ 22.1

2.3

7.3

End of period
Ditch

2.5

F3.8

22.6

7.7

F4.0

8.9

F5.2

25.4

3.7

28

27

2.1

8.3

F6.2

27.4

9.0

F6.9

11.2

F9.6

34.2

34 ↑ +40

34

+1.2

8.3

F9.5

34.0

10.0

F11.2

15.2

F16.4

47.8

(47)

↑

38.5

+2.9

9.4

F12.3

39.6

10.8

F13.7

15.0

F17.9

50.8

(53)

(46)

45.2

+4.9

10.3

F15.2

45.4

7.8

F17.7

F.

9.3

F14.2

43.4

47.5

↓

43

+5.7

7.9

F13.6

42.7

5.3

F9.6

F.

5.1

F10.8

36.6

37

29

+0.8

3.8

F4.6

24.2

5.3

F6.1

F.

6.8

F7.6

30.4

42.0

3)

28.5

+1.0

7.0

F3.0

21.0

5.2

F2.7

6.2

F7.2

29.4

30

Sta. + π - Grade.

13+54 937.27 38.4
T.P. 784 943.73 1.38 935.89

+55 38.5

+63 38.6

13+74.7 38.6

B.M. 1.45 942.28 942.28

Lt.

E

Rt.

7

25

22

25

25

Spike in 14" Oak 50' So. Arbogast Rd.
& 40' East Ona 550 Blvd. No.

$5/2$ + π - Grade

4/21 AM
L.E
M.Mc

1

X-SECTIONS

ARBOGAST-ST

FROM VICTORIA TO 1000' EAST

Plotted

STA + π - ELEV

B.M 3.26 945.83 - 942.51

0+00 = $\frac{1}{2}$ VICTORIA

+30

+50

+75

+50

2

+50

T.P 5.01 940.07-10.83 935.00

E

RT

SPIKE IN 15" OAK S.E. COR ARBOGAST + VICTORIA 200'

2.9 42.90

42.1 41.4 41.3 40.1 39.8 40.5 40.6 41.1

3.7 4.4 4.5 5.7 6.0 5.3 5.2 4.7
10 16 18 20-23 26 39 50

41.1

41.7 40.4 39.7 40.6 40.4 40.7

4.7

5.1 5.4 6.1 6.1 5.2 5.4 5.1
11 17 19 23 26 39 50

40.6 40.7 40.0 39.2 38.6 42.1 41.3 40.8

5.2 5.6 5.8 6.6 7.2 3.7 4.5 5.0
11 16 18 21-24 29 42 50

39.9 39.7 39.3 38.2 38.8 42.3 41.8 41.2

5.9 6.1 6.5 7.6 7.0 3.5 4.0 4.6
10 16 20-22 25 33 39 50

38.1 37.9 37.5 37.1 36.9 37.5 39.6 35.5 39.3

7.7 7.9 8.3 8.7 8.9 8.3 6.2 6.3 6.5
10 15 19 24 26 30 37 50

36.9

36.8 36.4 35.5 38.3 38.9

8.9

9.0 9.4 10.3 7.5 7.5 6.9
10 16 19-25 30 37 50

35.8 35.5 35.1 34.4 35.8 36.1 36.8

10.0 10.3 10.7 11.4 10.0 9.7 9.0
12 16 19-24 27 38 50

STA + π - ELEV

940.07

2 +78

+86

3 = π RD

+18

+22

+68

4

+50

Z

RT

35.5 35.✓ 34.7 33.7 36.7 37.2

4.6	4.9	5.4	6.4	3.4	2.9
10	16	19-24	30	50	

35.4 35.1 34.8 33.7 35.1 34.9

4.7	5.0	5.3	6.4	5.0	5.2
	16	19-25	33	50	

35.1 34.9 33.6 32.9 34.9

5.0	5.2	15" CM X 40	W.E	E END	5.2
21	21	6.5	21	21	50

34.9 34.7 34.5 33.0 34.5 34.7 34.7

5.2	5.4	5.6	7.1	5.6	5.4	5.4
10	20	22	25	34	50	

34.8 34.7 34.✓ 33.0 34.5 37.3

5.3	5.4	5.9	7.1	5.6	2.8	2.8
	10	16	22	25	34	50

34.✓ 34.1 33.6 32.6 32.3 35.✓ 39.2 38.9 38.5

5.9	6.0	6.5	7.5	7.8	4.9	0.8	1.2	1.6
10	15	18	23	30	38	45	50	

33.7 33.6 33.✓ 32.1 31.8 34.0 38.6 37.8

6.4	6.5	6.9	8.0	8.3	6.1	1.5	2.3
	10	15	19	23	28	37	50

33.0 32.7 32.1 31.✓ 34.8 34.4

7.1	7.4	8.0	8.9	5.3	5.7
10	17	20-24	31	50	

STA + π - ELEV
940.07

4+80 $\frac{1}{2}$ ENT 15" x 20 C.M

5

+50

6

+22 $\frac{1}{2}$ ENT 12" x 30' C.M

+50

T.P 5.82 936 10 9.79 930.28

7

+50

E.

R.T.

3270

31.17

30.82

W.END

E-END

7.4

8.90

9.25

21

21

324

32.1

31.7

31.0

32.1

32.0

7.7

8.0

8.4

9.1

8.0

8.1

11

17

19-25

27

50

317

31.5

30.9

29.9

31.5

32.3

8.4

8.6

9.2

10.2

8.6

7.8

10

17

19-24

27

50

30.9

30.7

30.4

29.1

30.8

31.1

31.3

9.2

9.4

9.7

11.0

9.3

9.0

8.8

10

17

20-23

26

35

50

307

29.02

28.74

W.END

E-END

9.4

11.05

11.33

21.5

21.5

30.6

30.5

30.7

29.1

31.3

30.9

9.5

9.6

9.9

11.0

8.8

9.2

10

16

18-24

28

50

30.3

30.1

29.7

28.6

30.5

33.9

33.3

32.4

5.8

6.0

6.4

7.5

5.6

2.2

2.8

3.5

10

15

19-23

28

35

42

50

30.0

29.7

29.1

28.1

28.5

29.9

35.1

33.8

6.1

6.4

7.0

8.0

7.6

6.2

1.0

2.3

10

16

19-22

23

28

39

50

STA	+	π	-	ELEV
		936.10		

7+78

8

+50

9

T.P.	4.43	933.07	7.46	928.64
------	------	--------	------	--------

B.M	6.23	933.07	6.23	926.84
-----	------	--------	------	--------

+50

T.P	8.91	939.04	2.94	930.13
-----	------	--------	------	--------

	6.96	945.17	0.83	938.21
--	------	--------	------	--------

B.M			2.59	942.58
-----	--	--	------	--------

942.57

2.59

2.46

2 RT

29.7	29.6	29.2	27.8	28.3	29.7	34.9	33.6
6.4	6.5	6.9	8.3	7.8	6.4	1.2	2.5
	10	15	21-19	23	27	38	50

29.5	29.3	28.9	27.1	28.8	33.3	32.1
6.6	6.8	7.2	8.5	7.3	2.8	4.0
	10	15	20-23	26	36	50

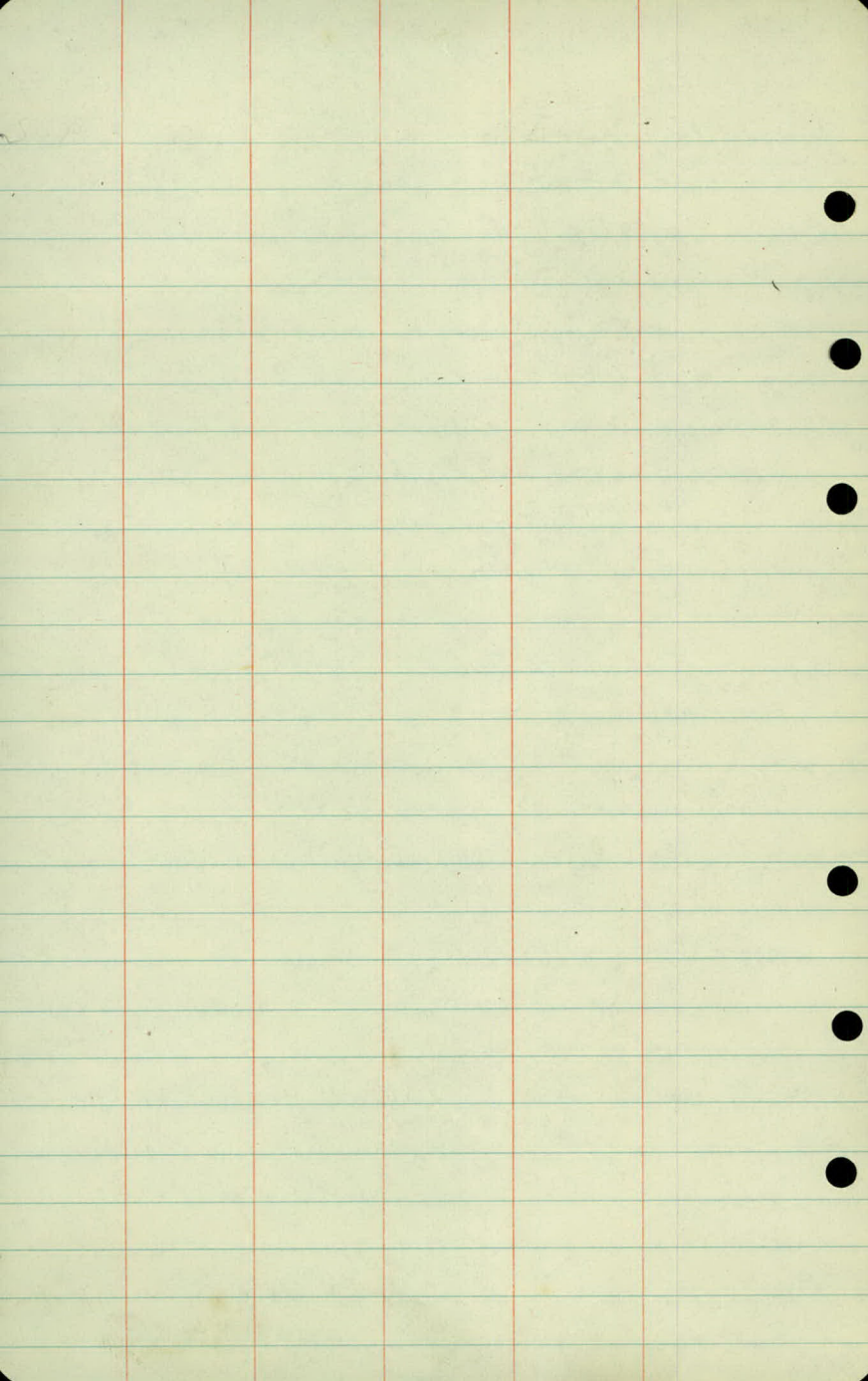
29.0	28.8	28.4	27.4	31.7	30.8	29.7
7.1	7.3	7.7	8.7	4.4	5.3	6.4
	10	15	19-23	34	41	50

28.6	28.3	27.8	26.1	29.1	31.2	28.8
7.5	7.8	8.3	9.9	7.0	4.9	7.3
	10	16	19-22	29	34	50

SPIKE - 18" OAK 50' RT - STA 9+15

28.5	28.1	27.8	24.2	23.4	24.2	22.9	21.9	17.1
4.6	5.0	5.3	8.9	9.5	8.9	10.2	11.2	4.21
	10	15	24	27	29	41	50	W.S
								LAKE-EMULY
								16.0

SPIKE-IN 15" OAK S.E. COR ARBOGAST + VICTORIA 200'



4/23

A.M.⁶
L.C.
M.Mc

X-SECTIONS

VICTORIA - ST STA 192150 TO ARBOGAST

STA	+	π	-	ELEV
B.M.	259	945.16.		942.57
T.B.M.	6.40	949.10.	24694	2.70.

192+50 45.8

193 45.6

+50 45.3

194 45.0

+16 X DRAIN 24" X 58' C.M

+50 45.0

+80 ϕ ENT 15" X 40' C.M - RT

195 44.8

LT

E

RT

SPIKE - IN 15" OAK S.E. COR - ARBOREAST + VICTORIA

45.8 45.4 44.7 44.6 42.6 43.4 43.2
 3.3 3.7 4.4 6.5 6.5 5.7 5.8
 14 21 25 32 35 50

44.9 43.4 43.5 42.5 42.5 44.8 45.5 45.6 45.1 44.5 42.5 41.9 42.3 41.8
 4.2 5.7 5.6 6.6 6.6 4.3 3.6 3.5 3.9 4.6 6.6 7.2 6.8 7.3
 50 43 34 30 22 17 9 13 18 22 30 33 50

41.0 41.0 41.5 45.0 45.7 45.3 45.0 44.3 40.7 40.3
 8.1 8.1 7.6 4.1 3.9 3.8 4.1 4.8 8.4 8.8
 50 39 26 15 10 10 17 27 50

41.7 41.3 40.7 40.6 44.5 44.9 45.0 44.7 44.7 40.7 39.2 39.2
 7.9 7.8 8.9 8.5 4.5 4.2 4.1 4.4 4.9 8.9 9.5 9.8
 50 46 41 29 16 10 18 17 26 30 50

39.57
 F.L.
 9.53
 29

38.95
 F.L.
 14.15
 29

41.3 39.6 40.8 41.7 44.1 44.7 45.0 44.5 44.7 43.3 39.9 40.7 40.9
 7.8 9.5 8.3 7.9 5.0 4.4 4.1 4.6 4.9 5.8 9.2 8.4 8.2
 50 45 43 47 40 25 18 10 11 15 26 30 32 33 50

39.65 40.0
 S. END No. END
 F.L. F.L.
 9.45 9.10
 31 31

43.9 43.6 41.4 41.7 44.4 44.6 44.8 44.4 43.6 40.7 39.8
 5.2 5.5 7.1 7.4 4.7 4.5 4.3 4.7 5.5 8.9 9.3
 50 34 29 23 17 10 10 19 27 50

STA	+	⌞	-	ELEV
-----	---	---	---	------

949.10

195+50

44.6

196

44.6

+50

44.1

197

43.9

+45

43.7

+70

43.5

198

43.4

+43 W-END 24"X54 CONC LT

43.1

LT

L

RT

44.6 44.3 43.6 40.7 40.7 40.2

4.5 4.8 5.5 8.4 8.4 8.9
11 18 25 31 50

44.4 44.0 43.5 41.4 41.2 42.3 40.8

4.7 5.1 5.6 7.7 7.9 6.8 8.3
11 17 22 29 32 50

44.1 43.8 43.3 41.2 41.1 42.3 42.0

5.0 5.3 5.8 7.9 8.0 6.8 7.1
11 17 22 30 33 50

43.9 43.7 43.3 41.3 41.0 42.7 41.6

5.2 5.4 5.8 7.8 8.1 6.4 7.5
11 17 22 30 33 50

43.7 43.5 43.1 41.0 40.7 42.7 41.6

5.4 5.6 6.0 8.1 8.4 6.4 7.5
11 18 22 30 33 50

43.5 43.3 43.0 40.9 40.5 41.5 40.5

5.6 5.8 6.1 8.2 8.6 7.6 8.6
11 18 22 31 33 50

43.4 43.2 42.8 40.9 40.6 43.2 42.4

5.7 5.9 6.3 8.2 8.5 5.9 6.7
11 17 22 30 34 50

43.1 42.8 42.3 40.5 40.2 42.0 41.8

6.0 6.3 6.8 8.6 8.9 7.1 7.3
11 18 22 30 33 50

39.85

F.L

9.25

23

STA + π - ELEV
949.10

198+70 E-~~END~~ 24" X 54' CONC X DRAIN^{RT} 43.0

+84.24 = $\pm$ ARBOGAST 47.9

B.M 654 942.56 (942.57)

LT

L

RT

430

6.1

39.56

F.L

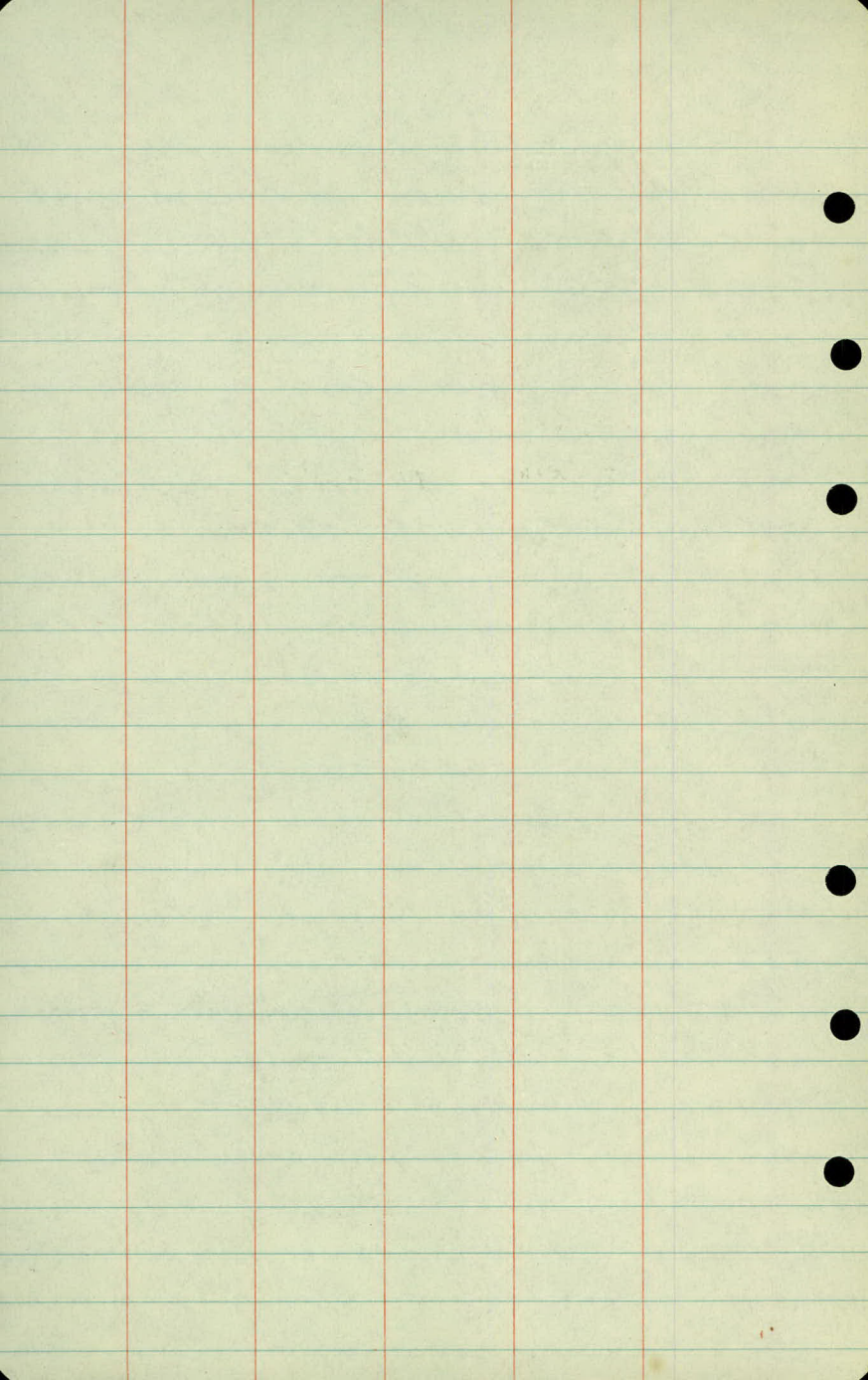
9.54

24

942.9

6.2

SPIKE-IN-15° OAK-S.E. COR-ARBORCAST + VICTORIA



DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV
-------	----------------	---------------	-----	-------	------

DITCH - LOCATION
VICTORIA + ARBOGAST

OBJECT

AZ.

STADIA

H.I. 5.40

AT-STA 195+00

TO-STA 198+84.24

0° 00'

W.END 24" C.M.

DITCH

199° 40' 88'

202° 45' 89'

211° 40' 77'

221° 30' 63'

235° 46'

260° 20' 54'

273° 91'

C of ENT. CLUV. BURNED

274° 30' 102'

276° 40' 110'

273° 40' 128'

273° 20' 182'

267° 228'

265° 35' 286'

EDGE OF SWAMP

262° 25' 318'

W.S. 4/22

DIST.	VERT. ANGLE	ROD EQUIV.	ROD	DIFF.	ELEV.
-------	----------------	---------------	-----	-------	-------

10.72

10.6

10.7

10.6

10.6

10.3

9.9

6.5

9.3

9.0

9.2

9.3

9.0

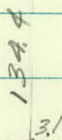
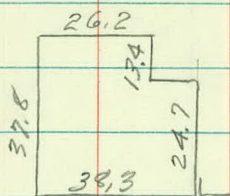
8.9

8.48

OBJECT

AZ.

STADIA



£ Arbogast

528.3
531.4

E 1/4 Cor
Sec. 35
□

