

Dr. 11A- BK. 12

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ *Plan* Survey

_____ *ATLANTIC AVE.* _____

From _____ To _____

Road Acc't. No. _____

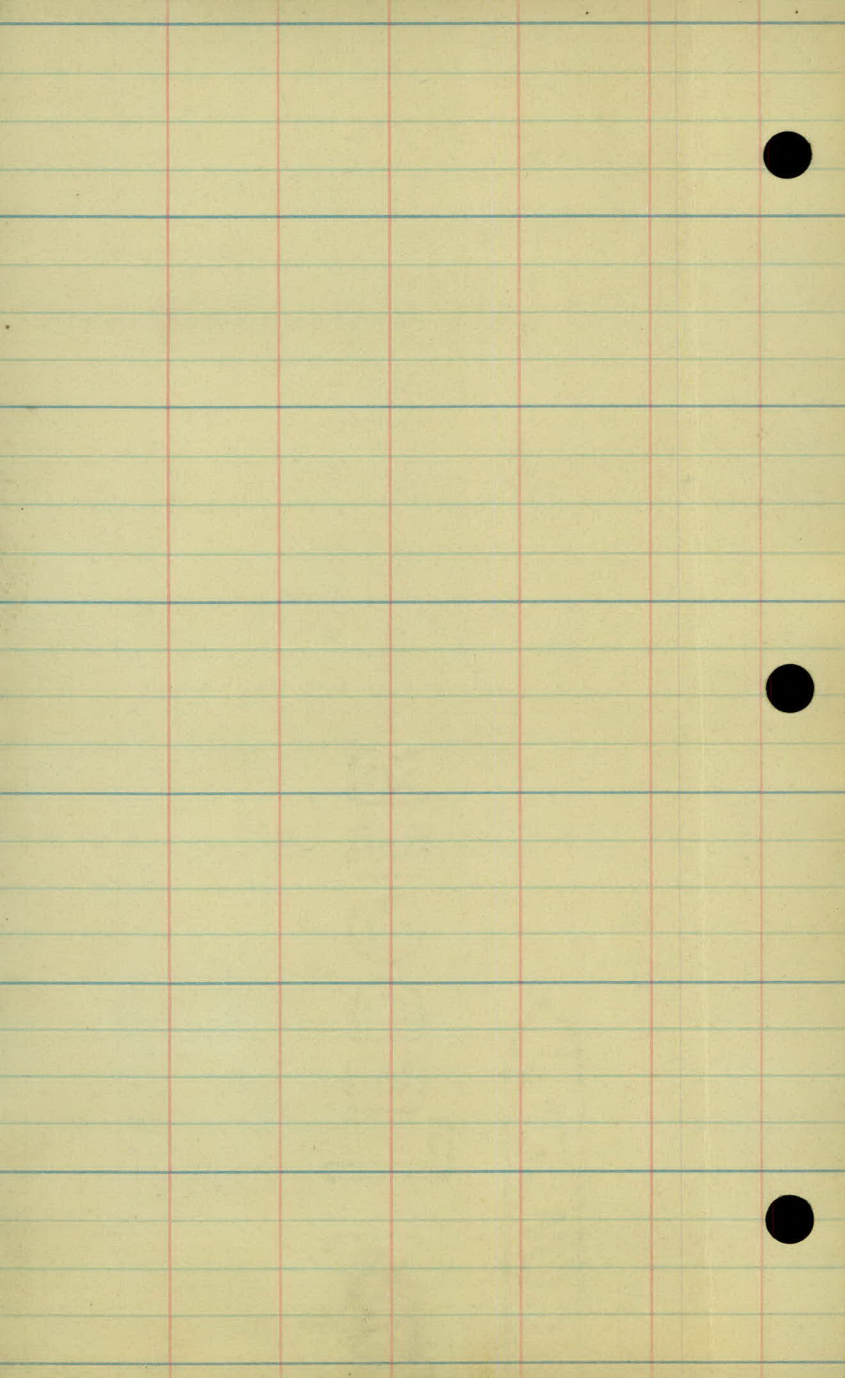
Date Filed _____ File *81* _____

440-67
1956
7-20

Plan Survey
Atlantic Avenue
(Or Snail Lake Blvd Ext'd)
From Hodgson Rd. to Rice St.

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alignment

Station Point

26+30.43 Rice St. (E. Line Sec. 24)

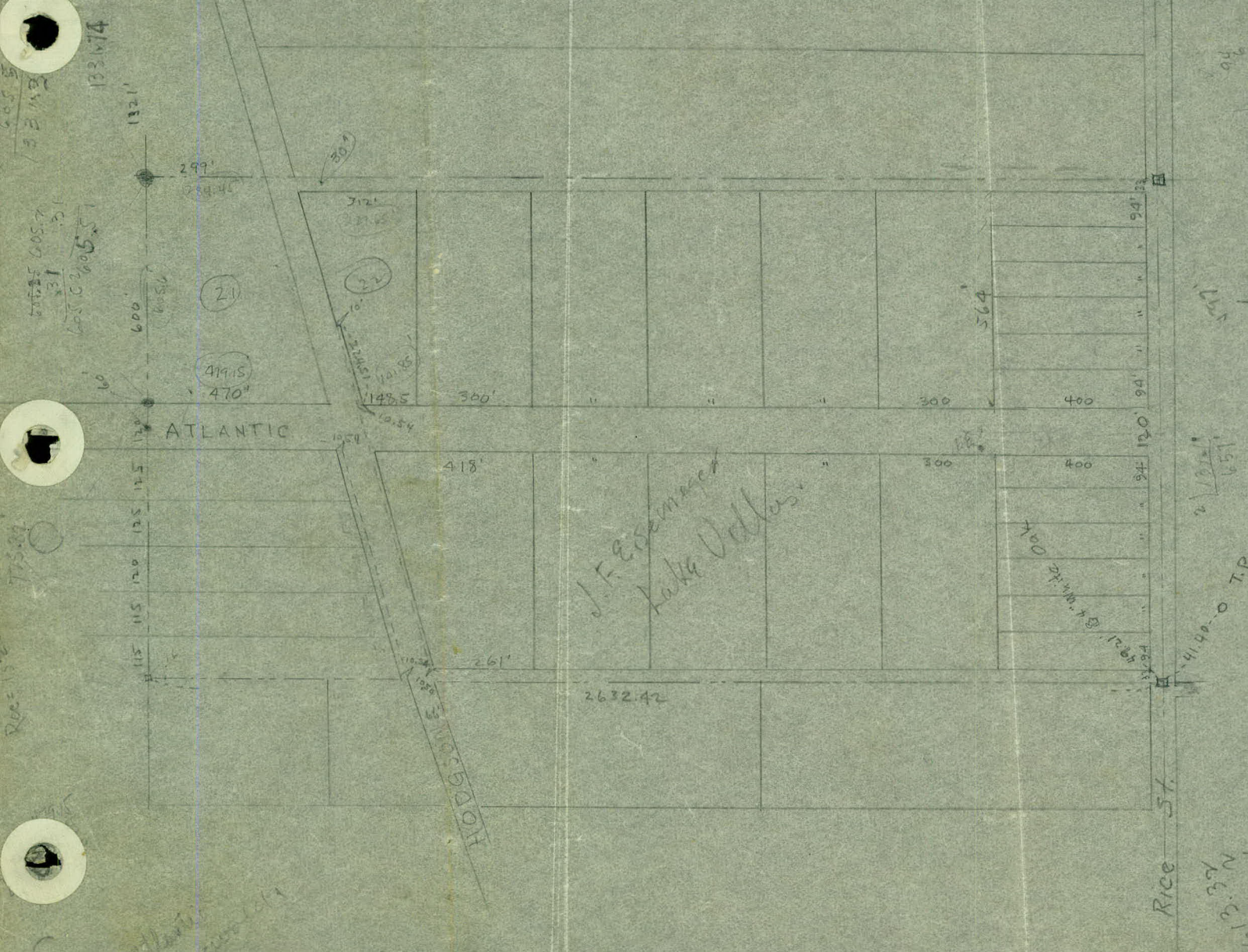
25+79.97 P.O.T.

22+06.62 P.O.T.

7+32.32 P.O.T.

5+32.5 { \neq Hodgson = 50+28.6
Beg. Proj.

0+00



605.00
S 31° 31' E
133.674

605.00
S 31° 31' E
605.00

115 115 120 125 125 125 130

115 115 120 125 125 125 130

ATLANTIC

HOBBS ST.

RICE ST.

J.F. Eisenbach
Luka Veloso

211

212

2632.42

299'

1321'

600'

419.15
470'

312'

212

148.5

300'

418'

261'

300'

400'

300'

400'

94'

94'

120'

84'

4140.0 T.P.

13.37 N

2 13.37 N

11.11 N

94'

784.43

30°

327.65

60.76

Stationed 60.63

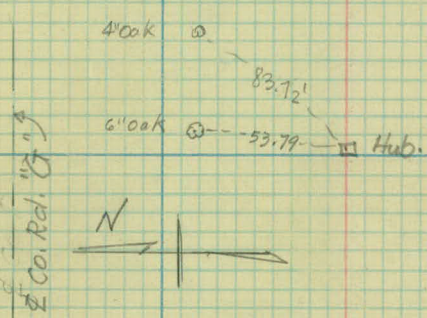
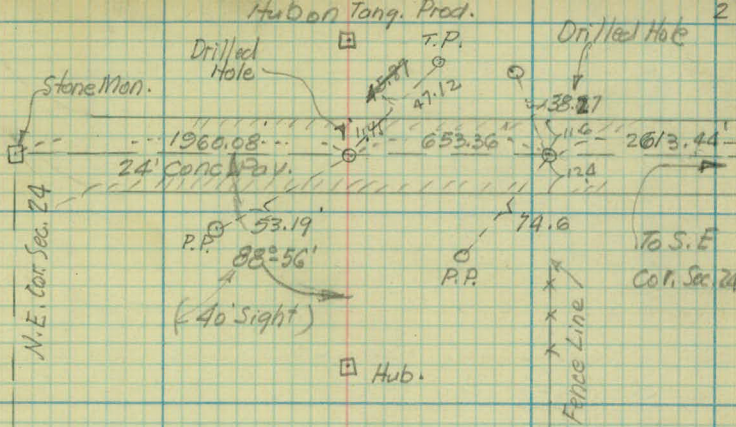
May 1911
Antismogey
Survey

572.38

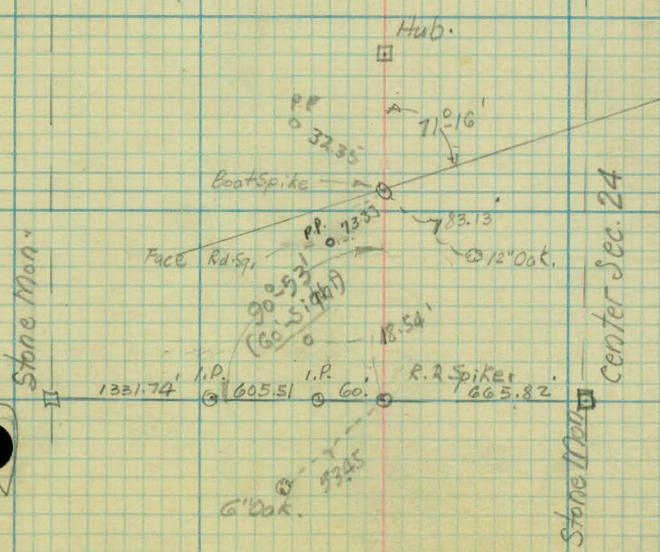
479.15

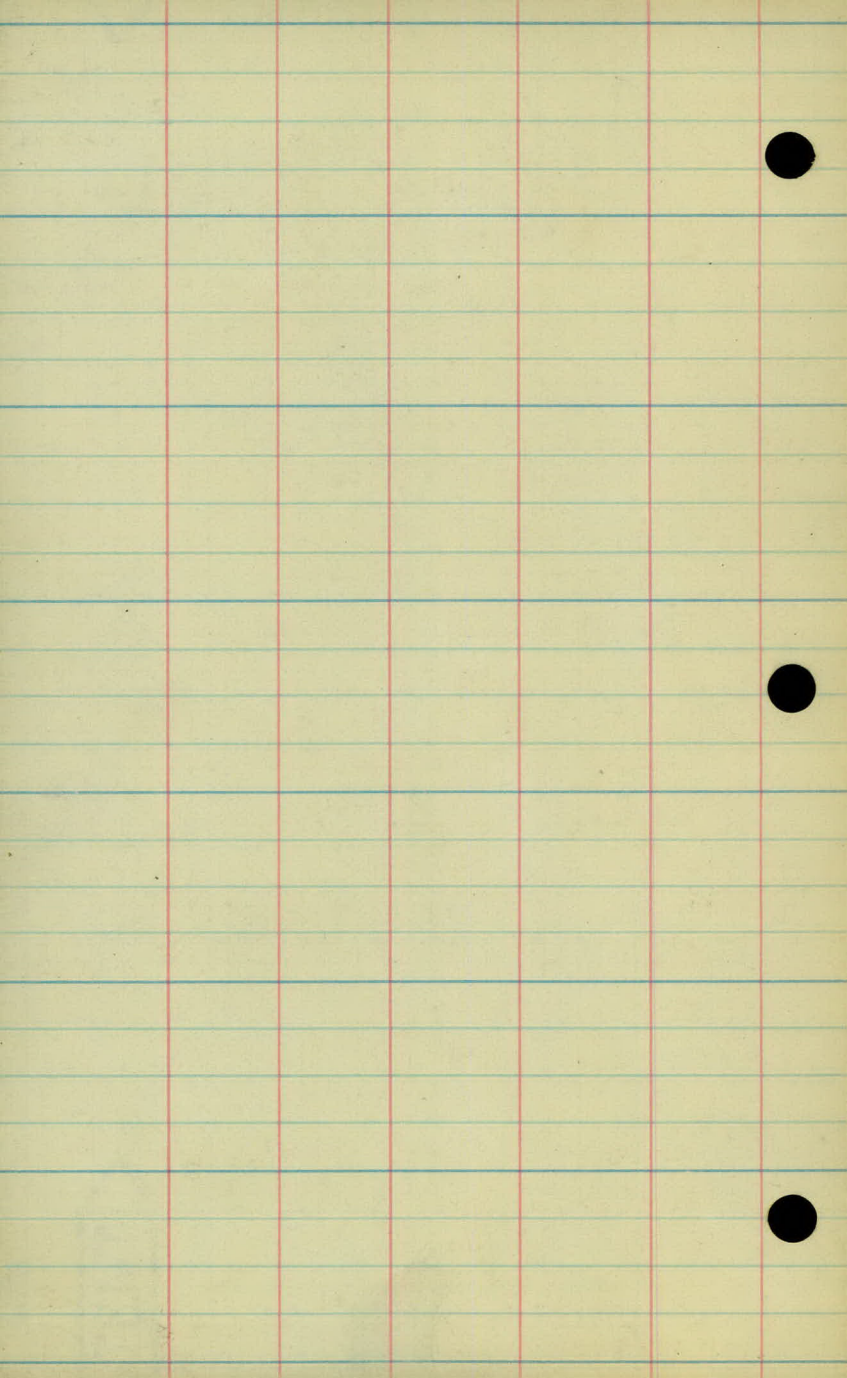
64

141.85



W.H.C. Jones
 H.W. Jones
 J.P.H. 1955





Topography.

Sta.

5

4

3

2

1

oto

Rd. 8'
+71 - Guy Wire 16'
+51 - Shldr. Rd.
+58 - P.P. 15'
+60 - Rd. 12'
+14 - Shldr. Rd.
Rd. 19'
+91 - Rd. 59, 18'
+75 - Rd. 10'
+71 - P.P. 16'

Hedgson
Black

(T.H.#49) Top.

Rd. 8'
+70 - Rd. 59'
Rd. 18'
+85 - Rd. 89, Stop
20'
+75 - Rd. 17

Rd. 9'

Rd. 17'

+07 - P.P. 17'
Rd. 9'

Rd. 17'

+50 - F. Cor 38'

Rd. 9'

(June 5, 1935)

Rd. 17'

Rd. 9'

+89 - Beg. F 32'

Rd. 16'

+35 - F. Ent.

Rd. 9'

Rd. 16'

cultivated.

Timber

12

11

10

9

8

7

6

+88 Cor. Cult.

Cult.

E Rd. 2'

5

Cult

+60 Cor. Cult.
30'

E Rd. 9'

E Rd. 11'

Open Field.

E Rd. 12'

E Rd. 9'

+14 Apple Tree 50'

+00 Ent.

E Rd. 4'

+85-10" Bx. E. 33'

+66-10" Bx. E. 33'

+45-12" Bx. E. 32'

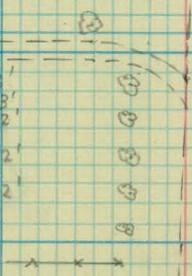
+26-10" Bx. E. 32'

+05-8" Bx. E. 32'

Rd. 2'

+90 F. Line 36'

Rd. 8'



19

18

17

16

15

14

13

+100 Cor. Timber - 64'
 100 ϕ Rd. 5' 6
 +94 - 4-5 small oaks
 15
 +82 - 3-10' oaks
 31

Timber 64'
 ϕ Rd. 8'

ϕ Rd. 7'

ϕ Rd. 6'
 +70 - Cor. Timber
 68'

+100 Cor. Cult - 0

Cultivated.

+75 - Cor. Cult
 70

Cult.

ϕ Rd. 4'

ϕ Rd. 3'

ϕ Rd. 8'



+42 - E. edge Pave.

+18 - W. edge Pave.

26

25

24

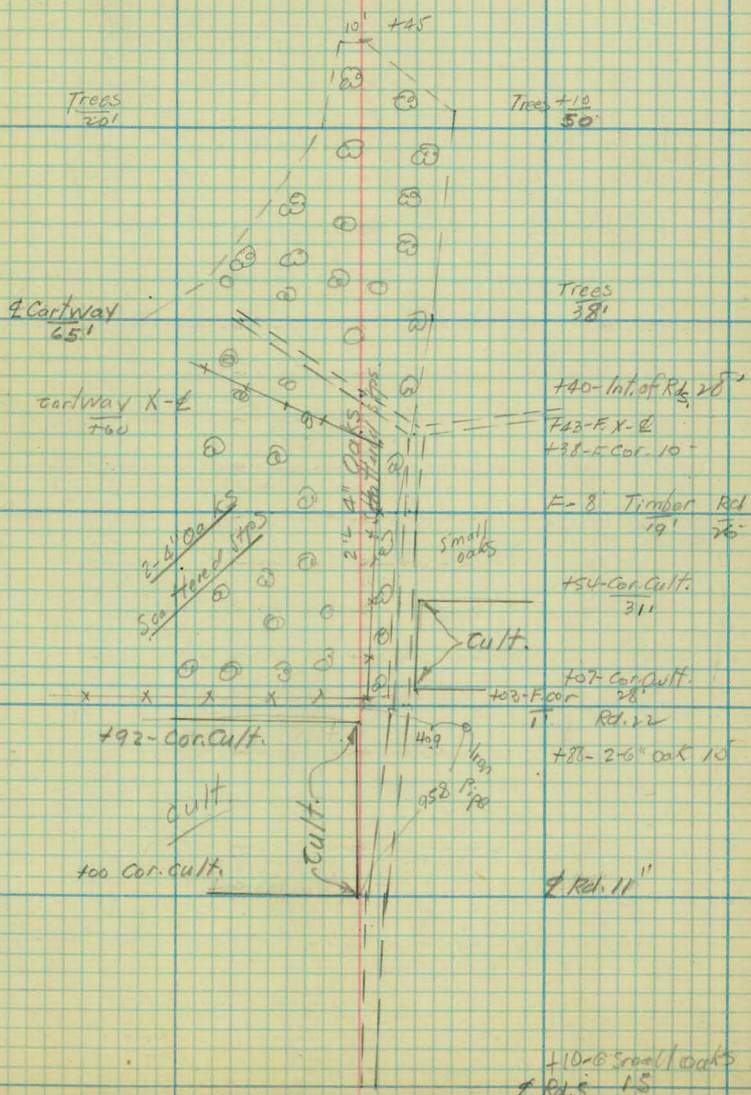
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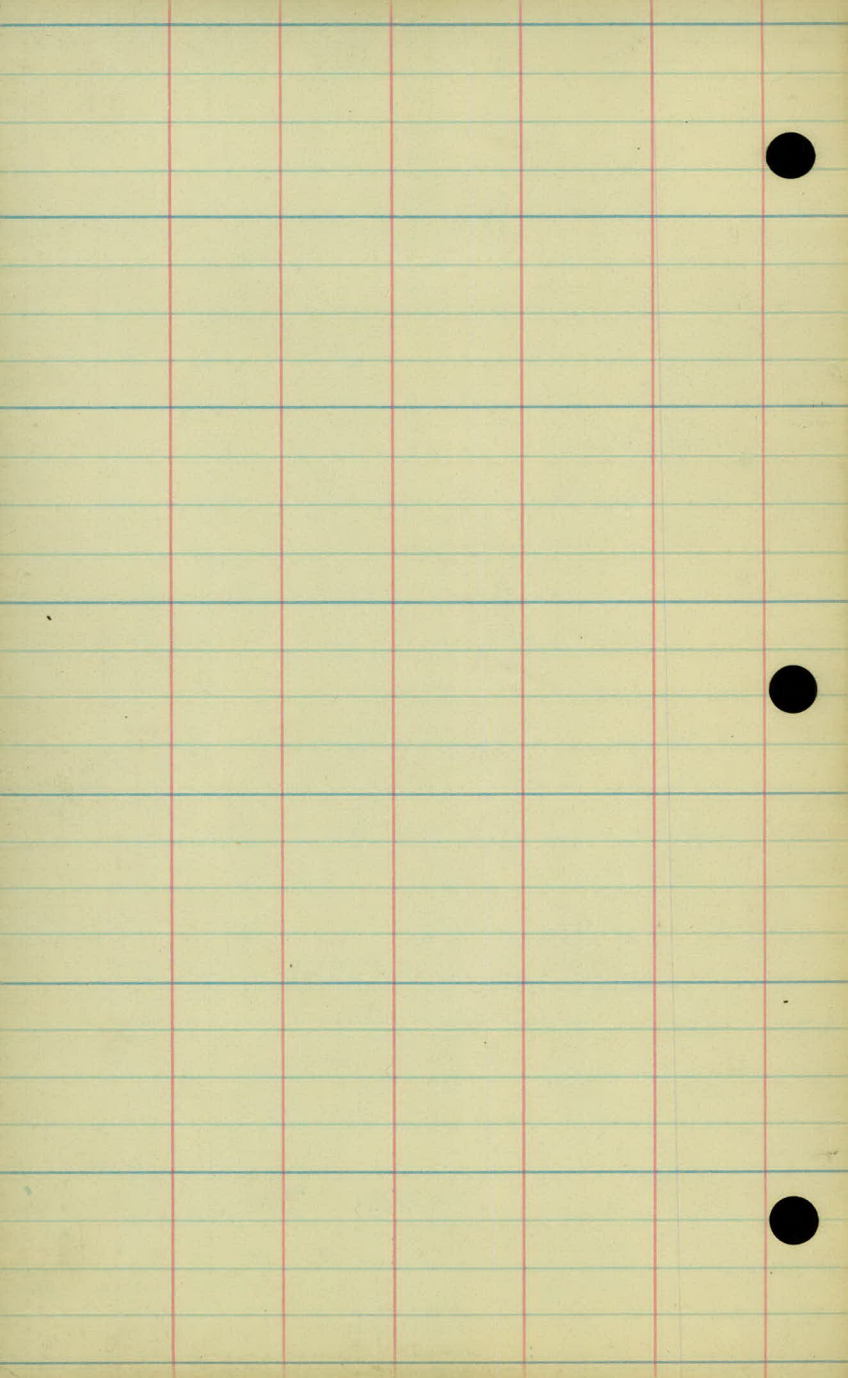
22

21

20

Rice st
 26+11 - T.P. 29.5
 +42 - P. Paving
 24' - Coror. Paving
 +18 - Pav. Edge
 +11 - Shoulder Line





Cross-Sections

Sta.	+	π	-	Elev.
B.M.	4.00	928.84		924.84 ✓
3				923.5 ✓
+50				24.1 ✓
4				24.3 ✓
+50				24.2 ✓
5				24.3 ✓
+20				24.2 ✓
+32.5 ^s ₁₀₀ (Begin Proj)				24.2 ✓
+57				24.0 ✓
+80				24.7 ✓
6				25.3 ✓
T.P.	3.06	931.42 ✓	0.48	928.36 ✓
+65				27.8 ✓

Lt.

±

Rt.

W.H.G. } 6/6/35
A.A.W. }
J.R.H. }
L.B.H. }

R.R. Spike 18" Oak 55' Lt. (Sta. 48+85 Hodgson Rd.)

" " " " 143' Lt. Sta. 5+30

$\frac{4.9}{39}$	$\frac{4.5}{25}$	$\frac{5.3}{17}$	$\frac{5.0}{13}$	$\frac{5.7}{9}$	$\frac{5.3}{17}$	$\frac{5.8}{17}$	$\frac{5.1}{20}$	$\frac{4.5}{29}$	$\frac{4.7}{37}$
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$\frac{4.1}{40}$	$\frac{4.5}{21}$	$\frac{4.0}{15}$	$\frac{5.2}{11}$	$\frac{4.7}{17}$	$\frac{5.1}{16}$	$\frac{4.0}{21}$	$\frac{3.6}{28}$	$\frac{3.6}{40}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

$\frac{4.2}{70}$	$\frac{4.1}{25}$	$\frac{4.0}{13}$	$\frac{5.0}{8}$	$\frac{4.5}{17}$	$\frac{4.5}{6}$	$\frac{4.9}{18}$	$\frac{4.1}{20}$	$\frac{3.7}{35}$
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$\frac{5.7}{44}$	$\frac{5.5}{35}$	$\frac{5.5}{20}$	$\frac{4.5}{12}$	$\frac{4.9}{9}$	$\frac{4.6}{6}$	$\frac{4.6}{12}$	$\frac{4.7}{18}$	$\frac{5.0}{23}$	$\frac{4.1}{23}$	$\frac{3.5}{35}$
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Shldr } $\frac{5.1}{50}$	$\frac{5.0}{45}$	$\frac{6.1}{31}$	$\frac{5.1}{24}$	$\frac{4.5}{17}$	$\frac{4.7}{13}$	$\frac{5.1}{21}$	$\frac{3.6}{23}$	$\frac{3.6}{50}$
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± Hodg = $\frac{4.6}{50}$

$\frac{4.6}{15}$	$\frac{4.8}{15}$	$\frac{5.5}{34}$	$\frac{7.1}{42}$	$\frac{7.5}{50}$
------------------	------------------	------------------	------------------	------------------

Shldr } $\frac{5.0}{50}$
Hodg } $\frac{5.0}{50}$

$\frac{4.6}{2-Hodg}$	$\frac{5.4}{50}$	$\frac{5.6}{60}$ - Shldr. Hodg.
----------------------	------------------	---------------------------------

$\frac{3.2}{60}$	$\frac{3.2}{50}$	$\frac{2.7}{32}$	$\frac{5.4}{26}$	$\frac{4.8}{18}$	$\frac{5.1}{11}$	$\frac{4.8}{17}$	$\frac{5.1}{22}$	$\frac{4.8}{50}$ = ± Hodg.
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	----------------------------

$\frac{2.7}{60}$	$\frac{2.5}{44}$	$\frac{1.6}{30}$	$\frac{2.7}{13}$	$\frac{3.9}{7}$	$\frac{4.1}{17}$	$\frac{4.8}{17}$	$\frac{5.8}{56}$	$\frac{6.1}{50}$	$\frac{5.8}{60}$ - Shldr.
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27.0	$\frac{1.8}{60}$	$\frac{1.5}{36}$	$\frac{1.7}{14}$	$\frac{3.1}{8}$	3.5	$\frac{3.6}{6}$	$\frac{2.2}{10}$	$\frac{2.3}{29}$	$\frac{3.0}{60}$ ^{27.8}
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27.9	$\frac{3.5}{60}$	$\frac{3.5}{25}$	$\frac{3.0}{7}$	3.6	$\frac{3.4}{6}$	$\frac{3.8}{25}$	$\frac{4.3}{60}$ ^{27.1}
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Sta.	+	π	-	Elev.
		931.42		
7				27.7 ✓
+50				27.6 ✓
8				27.3 ✓
+50				26.5 ✓
9				25.3 ✓
+50				25.0 ✓
10				25.0 ✓
T.P.	5.59	931.28	5.73	925.69 ✓
+50				25.8 ✓
11				26.0 ✓
+50				26.3 ✓
12				26.9 ✓
+50				27.7 ✓

Lt.

E

Pt.

10

28.0	$\frac{34}{60}$	$\frac{35}{30}$	$\frac{3.1}{7}$	$\frac{3.7}{-}$	$\frac{3.2}{11}$	$\frac{3.4}{25}$	$\frac{3.7}{50}$	$\frac{3.8}{60}$	27.6
27.4	$\frac{40}{60}$	$\frac{38}{33}$	$\frac{3.5}{10}$	$\frac{3.8}{-}$	$\frac{3.2}{14}$	$\frac{3.4}{30}$	$\frac{3.5}{50}$	$\frac{3.7}{60}$	27.7
26.7	$\frac{47}{60}$	$\frac{4.5}{32}$	$\frac{4.7}{25}$	$\frac{4.0}{11}$	$\frac{4.1}{-}$	$\frac{4.0}{28}$		$\frac{4.1}{60}$	27.3
25.9	$\frac{55}{60}$		$\frac{5.1}{28}$	$\frac{4.9}{-}$		$\frac{4.9}{25}$		$\frac{4.9}{60}$	26.5
25.1	$\frac{6.3}{60}$		$\frac{6.4}{25}$	$\frac{6.1}{-}$		$\frac{5.2}{25}$		$\frac{4.6}{60}$	26.4
24.9	$\frac{6.5}{60}$		$\frac{6.6}{25}$	$\frac{6.4}{-}$		$\frac{5.9}{28}$		$\frac{5.2}{60}$	26.2
25.4	$\frac{6.0}{60}$		$\frac{6.2}{25}$	$\frac{6.4}{-}$		$\frac{6.2}{25}$		$\frac{6.0}{60}$	25.4
26.3	$\frac{5.0}{60}$		$\frac{5.5}{25}$	$\frac{6.0}{-}$	$\frac{6.2}{13}$	$\frac{6.3}{25}$		$\frac{6.1}{60}$	25.2
27.1	$\frac{4.2}{60}$		$\frac{4.7}{25}$	$\frac{5.3}{-}$	$\frac{5.7}{11}$	$\frac{6.0}{25}$		$\frac{6.5}{60}$	24.4
27.8	$\frac{3.5}{60}$		$\frac{4.3}{25}$	$\frac{5.0}{-}$	$\frac{5.1}{10}$	$\frac{6.0}{30}$		$\frac{6.0}{60}$	25.3
27.6	$\frac{3.7}{60}$		$\frac{4.0}{25}$	$\frac{4.4}{-}$	$\frac{4.5}{13}$	$\frac{5.5}{30}$		$\frac{5.8}{60}$	25.5
28.1	$\frac{3.2}{60}$		$\frac{3.5}{25}$	$\frac{3.8}{-}$	$\frac{3.7}{14}$	$\frac{4.7}{25}$		$\frac{5.0}{60}$	26.3

Sale trees

Tree Line

ENT.

Sta.

+

 π ✓

-

Elev.

931.28

13

28.5 ✓

+50

29.4 ✓

14

29.4 ✓

T.P.

5.11

935.24 ✓

1.15

930.13 ✓

+50

29.6 ✓

15

29.0 ✓

+50

28.8 ✓

16

28.7 ✓

+50

28.4 ✓

B.M.

5.56

935.24 ✓

5.56

729.68 ✓

17

29.1 ✓

+50

30.7 ✓

18

32.2 ✓

+50

33.0 ✓

Lt. ♀ Rt. //

28.4 $\frac{2.9}{60}$ 2.8 $\frac{2.8}{15}$ $\frac{3.6}{15}$ $\frac{3.9}{30}$ $\frac{4.3}{60}$ 27.0

28.1 $\frac{3.2}{60}$ $\frac{2.2}{25}$ $\frac{1.9}{9}$ $\frac{1.9}{9}$ $\frac{3.0}{30}$ $\frac{3.6}{60}$ 27.7

28.6 $\frac{2.7}{60}$ $\frac{2.2}{25}$ $\frac{1.9}{9}$ $\frac{2.0}{25}$ $\frac{2.4}{60}$ 28.9

27.9 $\frac{7.3}{60}$ $\frac{6.4}{25}$ $\frac{5.6}{25}$ $\frac{5.6}{25}$ $\frac{5.7}{60}$ 29.5

28.1 $\frac{7.1}{60}$ $\frac{6.6}{25}$ $\frac{6.2}{25}$ $\frac{6.3}{25}$ $\frac{5.6}{60}$ 29.6

28.2 $\frac{7.0}{60}$ $\frac{6.9}{25}$ $\frac{6.4}{25}$ $\frac{6.6}{25}$ $\frac{6.2}{60}$ 29.0

28.2 $\frac{7.0}{60}$ $\frac{7.1}{25}$ $\frac{6.5}{25}$ $\frac{6.8}{25}$ $\frac{6.5}{60}$ 28.7

28.4 $\frac{6.8}{60}$ $\frac{6.8}{25}$ $\frac{6.8}{25}$ $\frac{7.2}{25}$ $\frac{7.1}{60}$ 28.1

R.R. Spike in 12" Oak 64' Rt Sta 16+72

29.4 $\frac{5.8}{60}$ $\frac{5.9}{25}$ $\frac{6.1}{25}$ $\frac{6.3}{25}$ $\frac{7.1}{60}$ 28.1

31.3 $\frac{3.9}{60}$ $\frac{4.2}{25}$ $\frac{4.5}{25}$ $\frac{5.0}{25}$ $\frac{6.2}{60}$ 29.0

32.2 $\frac{3.0}{60}$ $\frac{3.1}{25}$ $\frac{3.0}{10}$ $\frac{3.3}{10}$ $\frac{3.6}{33}$ $\frac{5.2}{60}$ 30.0

32.5 $\frac{2.7}{60}$ $\frac{2.7}{25}$ $\frac{2.2}{25}$ $\frac{3.0}{25}$ $\frac{4.3}{60}$ 31.0

Sandy Loam

Sta.	+	π ✓	-	Elev.
		935.24		
19				9 33.0 ✓
T.P.	6.99	939.78 ✓	2.45	932.79 ✓
+50				33.4 ✓
20				33.8 ✓
+50				34.5 ✓
21				34.6 ✓
+50				35.0 ✓
22				35.7 ✓
T.P.	1.14	937.26 ✓	3.66	936.12 ✓
+50				34.3 ✓
23				32.8 ✓
+50				32.5 ✓
24				33.9 ✓
+50				34.5 ✓
T.P.	3.82	937.60 ✓	3.48	933.78 ✓

Lt.

E

Rt.

12

$$32.9 \quad \frac{2.3}{60} \quad \frac{2.4}{25} \quad \frac{2.2}{-} \quad \frac{2.9}{16} \quad \frac{2.7}{35} \quad \frac{3.8}{60} \quad 31.4$$

$$33.7 \quad \frac{6.1}{60} \quad \frac{6.4}{25} \quad \frac{6.4}{-} \quad \frac{6.6}{14} \quad \frac{7.0}{25} \quad \frac{8.0}{60} \quad 31.8$$

$$34.8 \quad \frac{5.0}{60} \quad \frac{5.6}{25} \quad \frac{6.0}{-} \quad \frac{5.9}{10} \quad \frac{6.8}{60} \quad 33.0$$

$$35.1 \quad \frac{4.7}{60} \quad \frac{5.1}{30} \quad \frac{5.3}{-} \quad \frac{6.1}{25} \quad \frac{7.0}{60} \quad 32.8$$

$$35.6 \quad \frac{4.2}{60} \quad \frac{4.7}{25} \quad \frac{5.2}{-} \quad \frac{6.2}{28} \quad \frac{7.1}{60} \quad 32.7$$

$$36.0 \quad \frac{3.8}{60} \quad \frac{4.3}{25} \quad \frac{4.8}{-} \quad \frac{5.2}{19} \quad \frac{6.4}{30} \quad \frac{6.7}{60} \quad 33.1$$

$$37.1 \quad \frac{2.7}{60} \quad \frac{3.4}{25} \quad \frac{4.1}{-} \quad \frac{4.9}{18} \quad \frac{5.7}{33} \quad \frac{6.4}{60} \quad 33.4$$

$$34.5 \quad \frac{2.8}{60} \quad \frac{2.7}{32} \quad \frac{3.0}{-} \quad \frac{3.4}{23} \quad \frac{4.0}{50} \quad \frac{4.0}{60} \quad 33.3$$

$$33.1 \quad \frac{4.2}{60} \quad \frac{4.4}{25} \quad \frac{4.5}{-} \quad \frac{5.3}{25} \quad \frac{4.7}{60} \quad 32.6$$

$$33.4 \quad \frac{3.9}{60} \quad \frac{4.3}{25} \quad \frac{4.8}{-} \quad \frac{5.5}{25} \quad \frac{6.0}{60} \quad 31.3$$

$$34.3 \quad \frac{3.0}{60} \quad \frac{3.0}{25} \quad \frac{3.4}{-} \quad \frac{4.0}{25} \quad \frac{5.2}{60} \quad 32.1$$

$$34.1 \quad \frac{3.1}{60} \quad \frac{3.3}{25} \quad \frac{2.8}{-} \quad \frac{2.8}{25} \quad \frac{3.0}{60} \quad 34.3$$

Sandy Town

Sta.	+	∇ ✓ 937.60	-	Elev.
25				33.2 ✓
+50				33.0 ✓
+84				32.4 ✓
T.P.	1.04	925.87 ✓	12.77	924.83 ✓
26				20.3 ✓
+00				17.6 ✓
+13				17.7 ✓
118	-	W. edge of Conc. Pavement		17.87 ✓
26+30.43	±	Rice St.		17.97 ✓
B.M.	5.82	925.87	5.82	920.05 ✓
<u>check Level</u> T.P.	12.89	937.72	1.04	924.83
✓	2.02	938.14	1.61	936.11 (936.12)
✓	3.88	933.63	8.39	929.75
B.M.	3.95	933.63	3.95	929.68
T.P.	3.80	931.28	6.15	927.48
Int. B.M.			6.47	924.81 (924.84)

Lt.

E

Rt.

13

32.7	$\frac{4.9}{60}$	$\frac{4.8}{25}$	$\frac{4.4}{-}$	$\frac{3.1}{21}$	$\frac{3.1}{45}$	$\frac{3.4}{60}$	34.2
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32.2	$\frac{5.4}{60}$	$\frac{5.0}{25}$	$\frac{4.6}{-}$	$\frac{4.6}{25}$	$\frac{4.5}{60}$		33.1
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31.6	$\frac{6.0}{60}$	$\frac{5.4}{25}$	$\frac{5.2}{-}$	$\frac{5.0}{25}$	$\frac{5.1}{60}$		32.9
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No

56

X-Sec.

15.7	$\frac{10.2}{60}$	$\frac{9.0}{25}$	8.3	$\frac{8.0}{25}$	$\frac{8.5}{60}$		17.4
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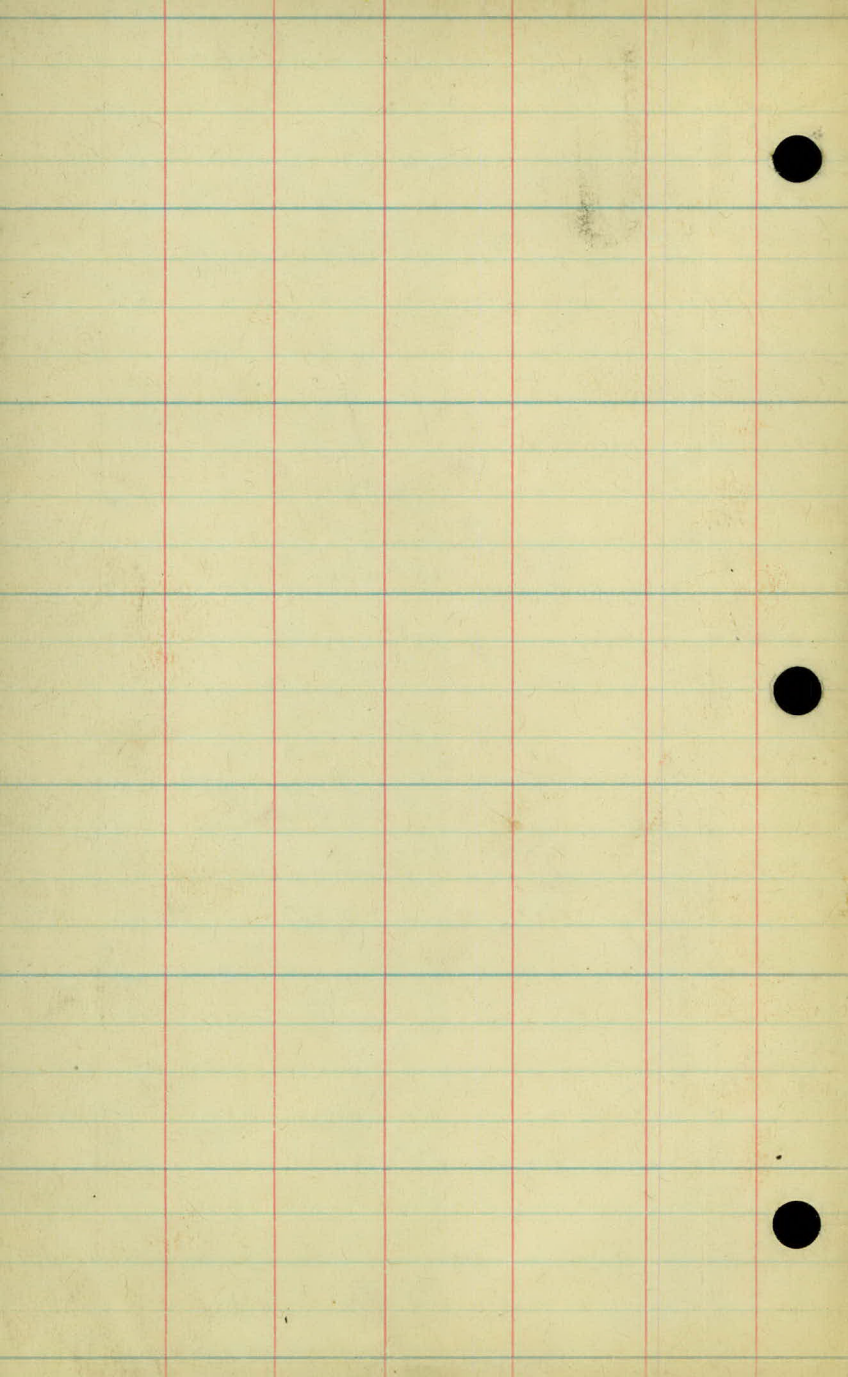
26+10 - P & Culv. Drains North.

16.1	$\frac{9.8}{60}$	$\frac{8.9}{28}$	$\frac{8.2}{-}$	$\frac{8.0}{25}$	$\frac{7.4}{60}$		14.5
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16.4	$\frac{9.51}{60.0}$	$\frac{9.22}{50.0}$	$\frac{8.57}{25.0}$	$\frac{8.00}{0.0}$	$\frac{7.56}{25.0}$	$\frac{7.17}{50.0}$	$\frac{7.09}{60.0}$	- 18.4
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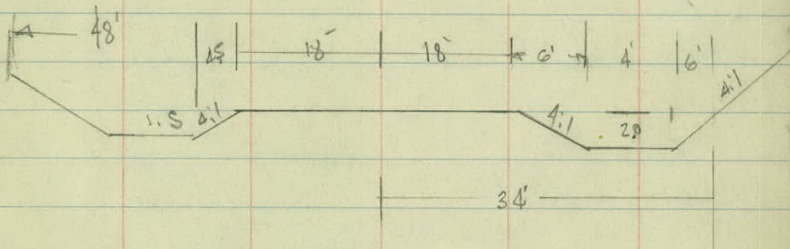
15.3	$\frac{10.59}{100.}$	$\frac{9.14}{50.0}$		7.90	$\frac{7.05}{50.0}$	$\frac{6.66}{100.}$		19.2
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R.R. Spike in T.P. 40'-Rt. Sta. 26+57



Dr 11A BK 12

Slope Stakes
Atlantic Ave.



Sta. 2625 to 2630

Sta	+	1	-	Grade
B.M.	7.68	932.52		924.84
5				24.2
+20				24.2
+32 S. of Highway				24.4
+57				24.8
+80				24.5
6				24.6
+65				24.8
7				25.0
+50				25.2
8				25.4
+50				25.6

Cr Rod Lt L Rt

R.R. Spike 18' oak 143 ct 5+30

$$8.0 \quad 48 \left| \begin{array}{r} 54 \\ +16 \end{array} \right.$$

$$7.9 \quad 48 \left| \begin{array}{r} 56 \\ +20 \end{array} \right. \quad \begin{array}{r} 72 \\ +0.7 \end{array} \quad \begin{array}{r} 64 \\ +1.5 \end{array} / 48$$

$$7.7 \quad 48 \left| \begin{array}{r} 46 \\ +3.1 \end{array} \right. \quad \begin{array}{r} 47 \\ +3.0 \end{array} \quad \begin{array}{r} 53 \\ +2.4 \end{array} / 48$$

$$7.5 \quad 48 \left| \begin{array}{r} 46 \\ +2.9 \end{array} \right. \quad \begin{array}{r} 48 \\ +2.7 \end{array} \quad \begin{array}{r} 47 \\ +2.8 \end{array} / 48$$

$$7.3 \quad 48 \left| \begin{array}{r} 52 \\ +2.1 \end{array} \right. \quad \begin{array}{r} 50 \\ +2.0 \end{array} \quad \begin{array}{r} 47 \\ +2.6 \end{array} / 48$$

$$7.1 \quad 48 \left| \begin{array}{r} 58 \\ +1.3 \end{array} \right. \quad \begin{array}{r} 52 \\ +1.9 \end{array} \quad \begin{array}{r} 51 \\ +2.0 \end{array} / 48$$

$$6.9 \quad 48 \left| \begin{array}{r} 67 \\ +2.2 \end{array} \right. \quad \begin{array}{r} 60 \\ +2.9 \end{array} \quad \begin{array}{r} 58 \\ +1.1 \end{array} / 48$$

Sta	+	↑	-	Grade
		932.52		
9				25.8
	+50			26.0
10				26.2
	+50			26.4
	7.81	934.25	6.08	976.44
11				26.6
	+50			26.8
12				27.0
	+50			27.2
13				27.4
	+50			27.6
14				27.8

Gr. Rod

Lt

E

Rt

$$6.7 \begin{array}{r} 8.2 \\ 48 \overline{) 7.4} \\ \underline{10.8} \end{array} \quad \begin{array}{r} \times \\ 7.3 \\ 18 \end{array} \quad \begin{array}{r} 7.1 \\ -0.4 \end{array} \quad \begin{array}{r} 5.8 \\ 10.9 \overline{) 48} \end{array}$$

$$6.5 \begin{array}{r} 8.0 \\ 48 \overline{) 7.6} \\ \underline{10.4} \end{array} \quad \begin{array}{r} \times \\ 7.5 \\ 18 \end{array} \quad \begin{array}{r} 7.5 \\ -1.0 \end{array} \quad \begin{array}{r} \times \\ 7.2 \\ 18 \end{array} \quad \begin{array}{r} 6.5 \\ 10.8 \overline{) 48} \end{array}$$

$$6.3 \begin{array}{r} 7.9 \\ 48 \overline{) 7.2} \\ \underline{10.6} \end{array} \quad \begin{array}{r} \times \\ 7.5 \\ 18 \end{array} \quad \begin{array}{r} 7.5 \\ -1.2 \end{array} \quad \begin{array}{r} \times \\ 7.0 \\ 18 \end{array} \quad \begin{array}{r} 7.2 \\ 10.6 \overline{) 48} \end{array}$$

$$6.1 \begin{array}{r} 7.6 \\ 48 \overline{) 6.2} \\ \underline{10.4} \end{array} \quad \begin{array}{r} \times \\ 6.9 \\ 18 \end{array} \quad \begin{array}{r} 7.3 \\ -1.2 \end{array} \quad \begin{array}{r} \times \\ 7.0 \\ 18 \end{array} \quad \begin{array}{r} 7.0 \\ 10.2 \overline{) 48} \end{array}$$

Blue top 18' Lt. 6th. 10750

$$7.7 \begin{array}{r} 7.2 \\ 48 \overline{) 7.1} \\ \underline{10.3} \end{array} \quad \begin{array}{r} \times \\ 7.9 \\ 18 \end{array} \quad \begin{array}{r} 8.3 \\ -0.6 \end{array} \quad \begin{array}{r} \times \\ 9.1 \\ 18 \end{array} \quad \begin{array}{r} 9.1 \\ 10.1 \overline{) 48} \end{array}$$

$$7.5 \begin{array}{r} 9.0 \\ 48 \overline{) 7.0} \\ \underline{10.5} \end{array} \quad \begin{array}{r} \times \\ 7.2 \\ 18 \end{array} \quad \begin{array}{r} 7.8 \\ -0.3 \end{array} \quad \begin{array}{r} \times \\ 7.8 \\ 18 \end{array} \quad \begin{array}{r} 7.0 \\ 10.0 \overline{) 48} \end{array}$$

$$7.3 \begin{array}{r} 6.5 \\ 48 \overline{) 6.8} \\ \underline{10.8} \end{array} \quad \begin{array}{r} \times \\ 7.1 \\ 18 \end{array} \quad \begin{array}{r} 7.1 \\ -0.1 \end{array} \quad \begin{array}{r} \times \\ 8.1 \\ 18 \end{array} \quad \begin{array}{r} 8.3 \\ 10.5 \overline{) 48} \end{array}$$

$$7.1 \begin{array}{r} 5.4 \\ 48 \overline{) 4.2} \\ \underline{11.2} \end{array} \quad \begin{array}{r} \times \\ 6.6 \\ 18 \end{array} \quad \begin{array}{r} 6.6 \\ -0.5 \end{array} \quad \begin{array}{r} \times \\ 7.3 \\ 18 \end{array} \quad \begin{array}{r} 7.6 \\ 10.0 \overline{) 48} \end{array}$$

$$6.9 \begin{array}{r} 5.7 \\ 48 \overline{) 4.2} \\ \underline{11.2} \end{array} \quad \begin{array}{r} \times \\ 5.7 \\ 18 \end{array} \quad \begin{array}{r} 5.7 \\ -1.2 \end{array} \quad \begin{array}{r} 7.3 \\ 10.1 \overline{) 48} \end{array}$$

$$6.7 \begin{array}{r} 5.6 \\ 48 \overline{) 4.1} \\ \underline{11.1} \end{array} \quad \begin{array}{r} \times \\ 4.9 \\ 18 \end{array} \quad \begin{array}{r} 4.9 \\ -1.8 \end{array} \quad \begin{array}{r} 6.1 \\ 10.6 \overline{) 48} \end{array}$$

$$6.5 \begin{array}{r} 5.7 \\ 48 \overline{) 4.8} \\ \underline{11.7} \end{array} \quad \begin{array}{r} \times \\ 4.8 \\ 18 \end{array} \quad \begin{array}{r} 4.8 \\ -1.7 \end{array} \quad \begin{array}{r} 5.2 \\ 11.2 \overline{) 48} \end{array}$$

Sta	+	π	-	Grade
		934.25		
14+50				28.0
15				28.3
+50				28.6
16				29.0
+50				29.43
	8.68	938.36	4.88	29.8
17				29.8
+50				30.2
18				30.7
+50				31.2
19				31.7
+50				32.2

929.68

Pr. Rod

Lt

Q

Rt.

6.3

6.3

$$48 \overline{) \frac{60}{103}}$$

$$\frac{46}{+1.7}$$

$$\frac{47}{+1.6} / 48$$

6.0

$$48 \overline{) \frac{60}{100}}$$

$$\frac{5.1}{+0.9}$$

$$\frac{46}{+1.4} / 48$$

5.7 7.2

$$48 \overline{) \frac{60}{121.2}}$$

$$\begin{array}{r} \times \\ 5.7 \\ 18 \\ \hline 5.5 \\ +0.2 \end{array}$$

$$\begin{array}{r} \times \\ 5.3 \\ 18 \\ \hline 5.3 \\ +0.4 \end{array}$$

$$\frac{5.3}{+0.4} / 48$$

5.3

4.8

$$48 \overline{) \frac{61}{100.7}}$$

$$\begin{array}{r} \times \\ 6.0 \\ 18 \\ \hline 5.8 \\ -0.2 \end{array}$$

$$\begin{array}{r} \times \\ 5.8 \\ 18 \\ \hline 5.8 \\ +0.2 \end{array}$$

$$\frac{5.8}{+0.2} / 48$$

4.8

6.3

$$48 \overline{) \frac{62}{100.1}}$$

$$\frac{6.0}{18}$$

$$\frac{5.9}{-1.1}$$

$$\frac{6.3}{-1.5} / 24.0$$

$$\frac{6.0}{+0.3} / 48$$

Spike in 1/2"

Oak Rt. side. 16 x 72

8.5

$$48 \overline{) \frac{91}{101.0}}$$

$$\frac{9.2}{-0.6}$$

$$\begin{array}{r} \times \\ 9.5 \\ 18 \\ \hline 9.5 \\ +0.5 \end{array}$$

$$\frac{10.0}{+0.5} / 48.0$$

8.2

9.7

$$48 \overline{) \frac{73}{109}}$$

$$\begin{array}{r} 0.06 \\ 7.6 \\ 18 \\ \hline 7.6 \\ +0.5 \end{array}$$

$$\frac{7.7}{+0.5}$$

$$\begin{array}{r} \times \\ 8.2 \\ 18 \\ \hline 8.2 \\ +0.8 \end{array}$$

$$\frac{8.2}{+0.8} / 48$$

7.7

$$48 \overline{) \frac{6.5}{+1.2}}$$

$$\frac{6.7}{+1.5}$$

$$\frac{7.6}{+0.1} / 48$$

-7.2

$$48 \overline{) \frac{6.0}{+1.2}}$$

$$\frac{5.4}{+1.8}$$

$$\frac{6.8}{+0.4} / 48$$

6.7

$$48 \overline{) \frac{5.6}{+1.1}}$$

$$\frac{5.0}{+1.7}$$

$$\frac{6.4}{+0.3} / 48$$

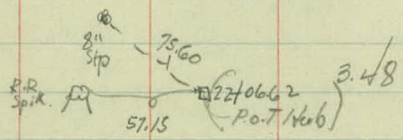
6.2

$$48 \overline{) \frac{4.7}{+1.8}}$$

$$\frac{5.2}{+1.0}$$

$$\frac{6.2}{+0.5} / 48$$

Sta	+	-	Grade
		938.36	
20			32.7
+50			33.2
21			33.7
+50			34.2
	10.60	940.28	8.68
22			34.7
B.M.			936.80
+75			34.8
	57.15	2210662 (P.O.T/Vob)	3.48
+50			34.6
+75			34.25
23			33.20
+75			32.05
+50		938.42	30.60



C.R. Rod Lt. S Rt.

5.7 $48 \begin{array}{r} / 3.9 \\ + 1.8 \end{array}$ $\frac{4.5}{+ 1.2}$ $\frac{5.6}{+ 0.1} / 48'$

5.2 ^{6.7} $48 \begin{array}{r} / 3.5 \\ + 1.7 \end{array}$ $\frac{3.6}{+ 1.0}$ $\frac{5.5}{+ 0.2} / 48'$

4.7 $48 \begin{array}{r} / 2.7 \\ + 2.0 \end{array}$ $\frac{3.7}{+ 1.0}$ $\frac{5.2}{+ 1.0} / 48'$

4.2 ^{5.7} $48 \begin{array}{r} / 2.3 \\ + 1.9 \end{array}$ $\frac{3.4}{+ 0.8}$ $\frac{5.2}{+ 0.5} / 48'$

5.6 ^{7.1} $48 \begin{array}{r} / 3.3 \\ + 2.3 \end{array}$ $\frac{4.5}{+ 1.1}$ $\frac{6.2}{+ 0.9} / 48'$

R.R. spike Top 8' cut stump 58' Lt. 22 to 6
 5.5 $\frac{5.3}{+ 0.2}$

5.7 ^{7.2} $48 \begin{array}{r} / 5.5 \\ + 0.2 \end{array}$ $\frac{5.8}{- 0.1}$ $\frac{6.8}{+ 0.4} / 48'$

6.2 ^{7.7} $48 \begin{array}{r} / 6.5 \\ + 0.3 \end{array}$ $\frac{6.7}{- 0.5}$ $\frac{7.5}{+ 0.2} / 48'$

7.1 ^{9.1} $48 \begin{array}{r} / 7.0 \\ + 0.1 \end{array}$ $\frac{7.4}{- 0.3}$ $\frac{7.8}{+ 0.3} / 48'$

8.2 ^{10.2} $48 \begin{array}{r} / 7.6 \\ + 0.6 \end{array}$ $\frac{7.8}{+ 0.4}$ $\frac{8.4}{+ 0.8} / 48'$

7.8 $48 \begin{array}{r} / 5.4 \\ + 2.4 \end{array}$ $\frac{5.9}{+ 1.9}$ $\frac{7.0}{+ 0.8} / 48'$

Sta. + π - Grade.

98842

23+75 28.8

24 26.7

+25 24.6

+50 22.8

+75 21.2

25 19.95

+25 19.0

+50 18.3

+75 17.84

+84 17.7

26 17.7

B.M. 9.025

Gr. Rod

Lt

Σ

Rt

$$9.6 \quad \begin{array}{r} 45 \\ +51 \\ \hline 96 \end{array} \quad \begin{array}{r} 45 \\ +51 \\ \hline 96 \end{array} \quad \begin{array}{r} 60 \\ +80 \\ \hline 140 \end{array}$$

$$11.7 \quad \begin{array}{r} 41 \\ +76 \\ \hline 117 \end{array} \quad \begin{array}{r} 45 \\ +72 \\ \hline 117 \end{array} \quad \begin{array}{r} 60 \\ +55 \\ \hline 115 \end{array} / 60$$

±5

$$15.6 \quad \begin{array}{r} 47 \\ +109 \\ \hline 156 \end{array} \quad \begin{array}{r} 37 \\ +119 \\ \hline 156 \end{array} \quad \begin{array}{r} 43 \\ +113 \\ \hline 156 \end{array} / 60$$

$$18.4 \quad \begin{array}{r} 58 \\ +126 \\ \hline 184 \end{array} \quad \begin{array}{r} 40 \\ +144 \\ \hline 184 \end{array} / 60$$

$$20.1 \quad \begin{array}{r} 61 \\ +140 \\ \hline 201 \end{array} \quad \begin{array}{r} 50 \\ +151 \\ \hline 201 \end{array} / 60$$

$$20.7 \quad \begin{array}{r} 67 \\ +140 \\ \hline 207 \end{array} \quad \begin{array}{r} 58 \\ +149 \\ \hline 207 \end{array} / 60$$

40. Rt. Sta. 76+57 Spk in T.P.

917.97
CROW

Sta.

+

π

-

Grade.