

Book-11, Dr. 11-A

X

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

----- *Plains* Survey -----

From ----- To -----

Road Acc't. No. -----

Date Filed ----- File -----

SUNSET LANE

FAIRFIELD DRIVE

VALLEY VIEW ROAD

ORCHARD PLACE

OAKWOOD DRIVE

Alignment
Oakwood Drive
in
Mounds View Acres

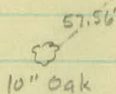
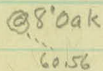
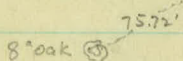
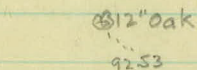
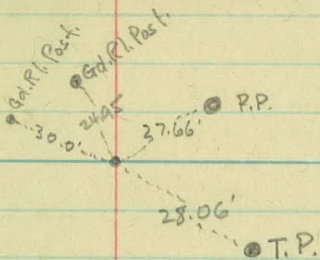
26+24.27 P.O.T

17+65.46 P.O.T.

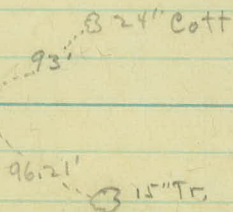
13+61 P.O.T.

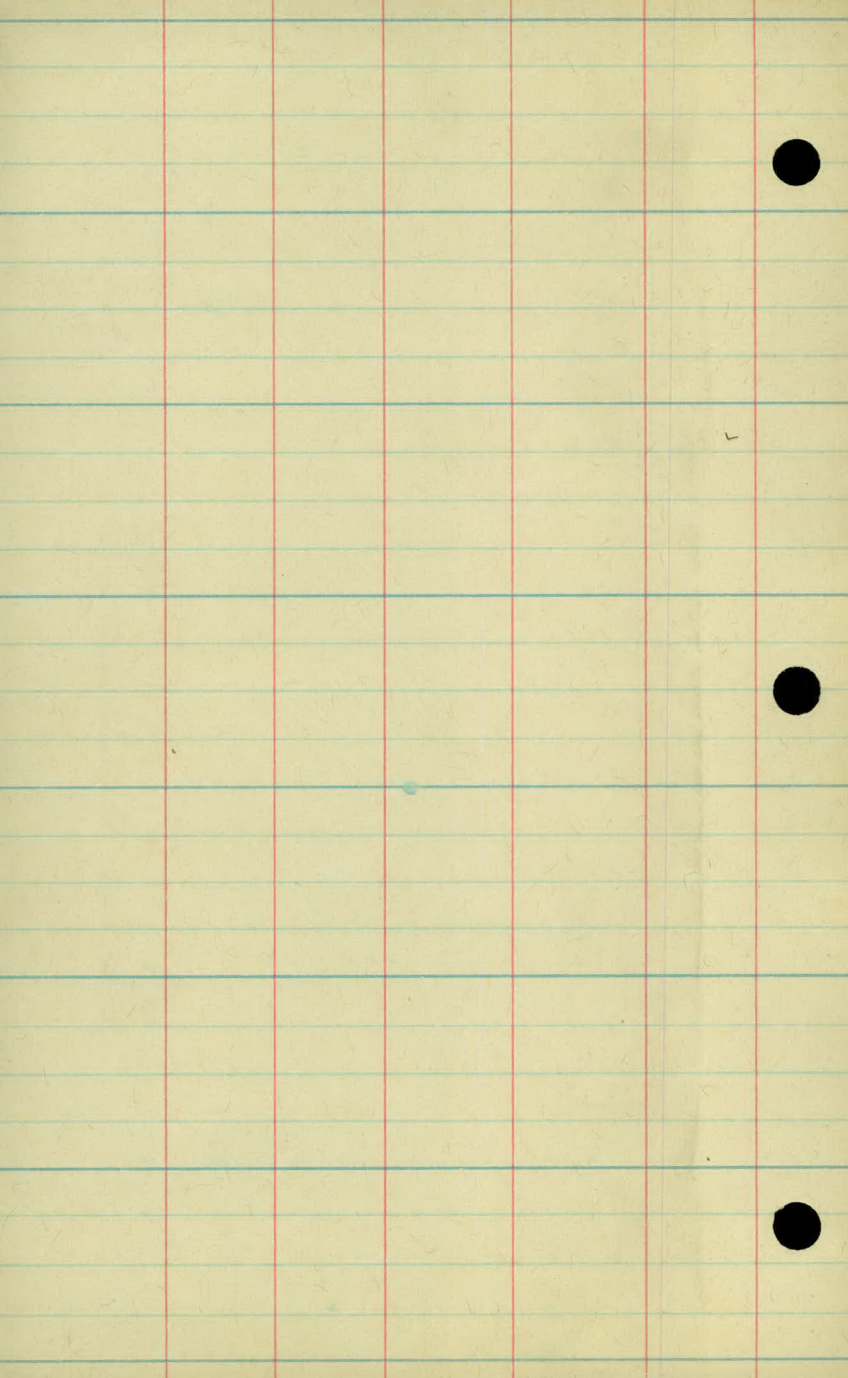
0+00 P.O.T

Co. Rd. E.



Orchard Pl.





Pirtell
9/30/35

TOPOGRAPHY
OAKWOOD DRIVE
IN
MOUNDS VIEW ACRES

Tr
3-3

Dt
175

Tr
176

5

Trail
5-2

9' Tr
160

Ditch
158

4

Trail
3-3

Ditch
136

3

Trail
1-7

+07-24" Tr
120

Ditch
123

+42-24" Tr
124

2

+51-10" Tr
28

+08-10" Tr
38

Trail
6-13

+22-24" Tr
110

Ditch
104

1

Trail
8-0

Ditch
87

+83-24" Tr
100

0 +00

Trail
7-0

Ditch
88

+93-24" Tr
83

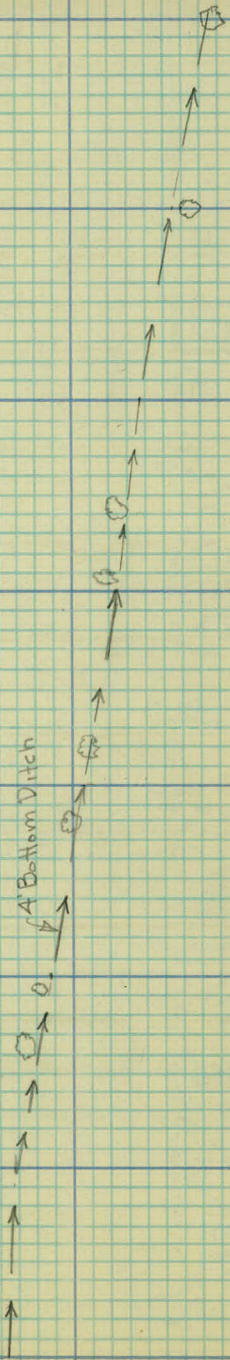
+57-30" Tr
74

HAY FIELD



Trail

A Bottom Ditch



Trail
2-9

+95-10'Stp
20

12

Trail
0-7

Trail
3-4

Trail
4-3

+62-30'Tr
23
+16-18'Tr
73
+08-24'Tr
12

Trail
4-4

+95-24'Tr
94

Trail
2-4

Trail
2-4

+15 Car Shed
30

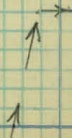
+60 Ditch
188

6

1



Shedg



+59 Beg Cult

21

+42 P.P.

16

+20-8" Tr

19

Rd
7-2

19

+16 Cor Ho

75

+01 P.P.

17

Rd
6-5

+135 stp

52

18

+90 stp +97 stp.

33

+70 stp 18"

33

37

+78 Cor Ho.

120

+59 Ent R/L

17

+00 End Woods

30

Rd
5-4

+62 PP

15

+33 End Garden

11

16

Woods

32

Rd
6-4

+87 Beg Grave

Top

+87 Ent

+50 Cor Ho

83

15

Woods

20

Trail

4-3

14

Woods

16

Trail

5-2

+25 Beg Wood

14

13

Cult

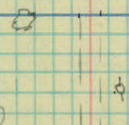
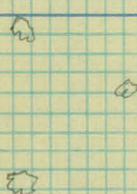
15.F.
28'

18
15.F.
26

n

n
n

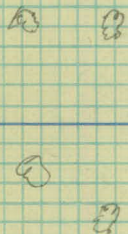
Ent ——— Ent



Garden
Ent

15.F.
24

WOODS



HAY



+35 Gd RI
23

+35 Shoulder
+13 Shoulder

+12 Gd RI
28

26-14
+08 12' x 36 CM +50 PP
9

+02 Cor Gr. RI
18

25-11
Rd
13-4

+85 Rd
11-1

+55 End Woods
68

+23 PP +99 T.P.
10 11

+06 Cor Ho

67

+45 Ent

+68 Row Trs +86 Row Trs
21 22

+63 End Cult.

+34 Beq Woods

45

+01 Cor Shed

115

Rd
12-3

+36 End Orchard
23

+82-18' Twin Oaks
40

+63 Beq Orchard
27

+45-30' Tr
36

+73 PP
12

Rd
10-2

+38 PP
14

Rd
9-0

Rd
8-1

+84 PP
14

+02-12' x 36 CM
20-16

Rd

7-2

26

25

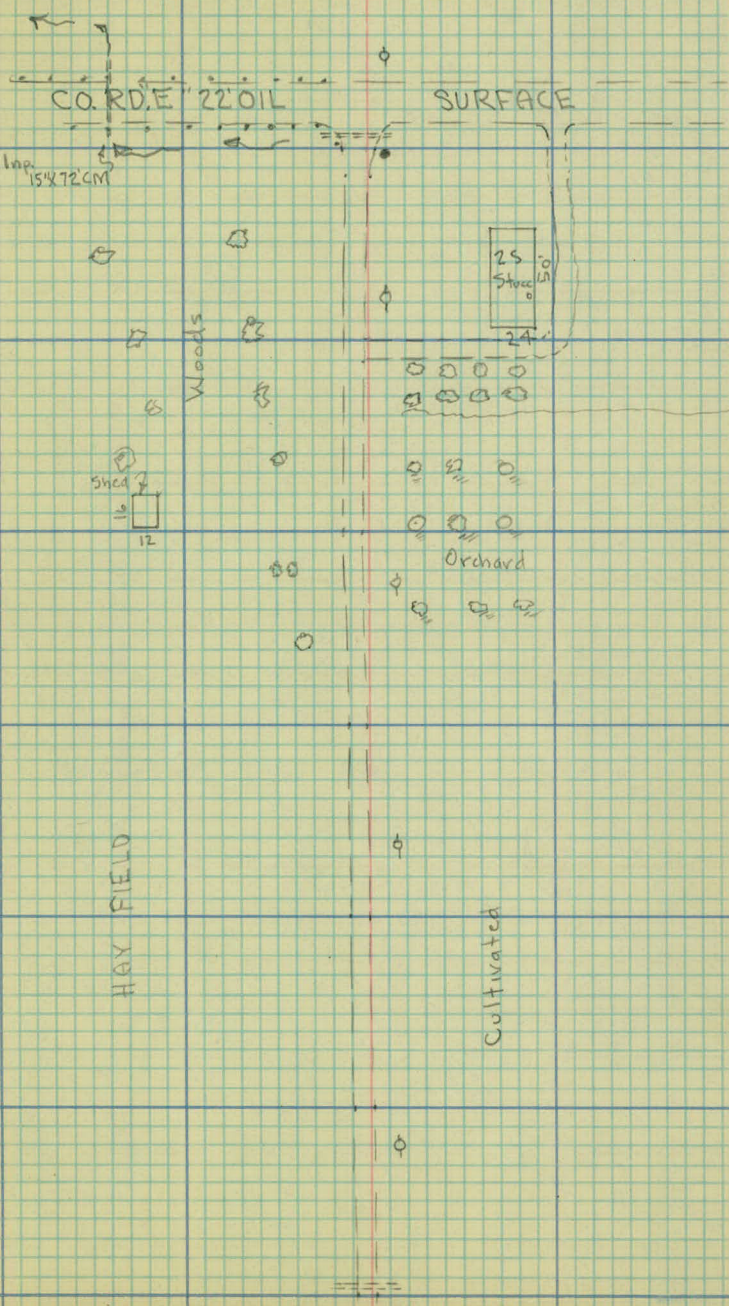
24

23

22

21

20



CO. RD. E 22' OIL

SURFACE

Inp. 15' x 72' CM

25' Storage
24'

5' x 12' shed

Woods

Orchard

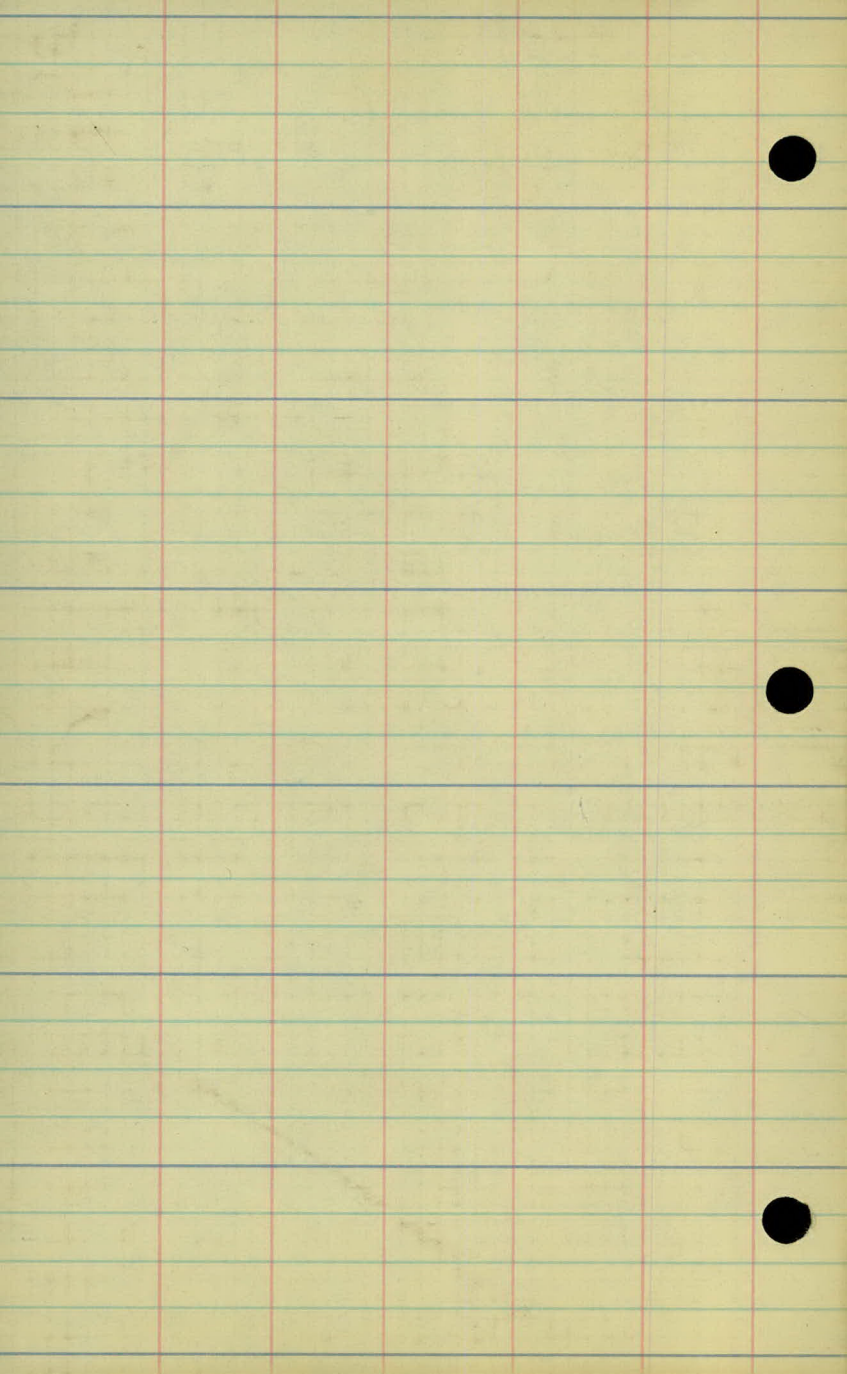
HAY FIELD

Cultivated

Well

Well





9/26/35

Portell

X-Sections

Oakwood Drive

10

Mounds View Acres

Spk. in 24" C.W. 100' N.E. of Orchard Place & Oakwood Drive

08.10

Ditch
 $\frac{5.7}{100}$ $\frac{8.8}{65}$ $\frac{10.7}{37}$ 12.3 $\frac{12.9}{54}$ $\frac{13.6}{63}$ $\frac{15.3}{67.6}$ $\frac{12.8}{74}$ $\frac{13.3}{100}$

$\frac{1.8}{100}$ $\frac{5.5}{73}$ $\frac{7.4}{41}$ $\frac{8.6}{42}$ $\frac{10.2}{21}$ $\frac{10.5}{11}$ $\frac{11.3}{7}$ 11.1 $\frac{12.4}{50}$ $\frac{12.7}{75}$ $\frac{12.2}{79}$ $\frac{15.6}{83-87}$ $\frac{12.6}{92-100}$

$\frac{00}{58}$ $\frac{1.0}{47}$ $\frac{7.8}{29}$ $\frac{10.2}{10}$ 10.8 $\frac{10.8}{13}$ $\frac{11.6}{42}$ $\frac{11.9}{87}$ $\frac{10.3}{92}$ $\frac{10.9}{95}$ $\frac{15.9}{100-103}$
 $\frac{11.3}{119}$ $\frac{11.4}{107}$

Top Stk @ Sta 2+00

07.3

$\frac{7.8}{16}$ $\frac{8.7}{10}$ $\frac{9.5}{8}$ 10.1 $\frac{10.5}{16}$ $\frac{11.2}{46}$ $\frac{10.7}{73}$ $\frac{9.9}{82}$ $\frac{9.3}{100-106}$ $\frac{16.4}{116-115}$
 $\frac{9.0}{123}$

$\frac{3.8}{18}$ $\frac{6.4}{12}$ $\frac{8.9}{8}$ 9.1 $\frac{9.9}{21}$ $\frac{9.8}{47}$ $\frac{9.0}{56}$ $\frac{9.5}{69}$ $\frac{10.9}{100}$

$\frac{5.4}{12}$ $\frac{7.9}{8}$ 8.2 $\frac{8.3}{30}$ $\frac{7.4}{75}$ $\frac{10.4}{100}$

'SS. = Same Slope

$$\frac{00}{59} \quad \frac{5.2}{31} \quad \frac{8.4}{9} \quad 8.8 \quad \frac{10.5}{16} \quad \frac{11.9}{66} \quad \frac{12.5}{100}$$

$$\frac{00}{83} \quad \frac{2.7}{65} \quad \frac{5.3}{29} \quad \frac{7.4}{7} \quad 8.0 \quad \frac{8.8}{8} \quad \frac{10.3}{21} \quad \frac{12.8}{71} \quad \frac{13.6}{100}$$

$$\frac{00}{40} \quad \frac{3.0}{13} \quad \frac{5.6}{8} \quad 5.8 \quad \frac{6.7}{6} \quad \frac{8.6}{24} \quad \frac{10.1}{37} \quad \frac{11.3}{49} \quad \frac{13.3}{79} \quad \frac{14.5}{100}$$

6.2

$$\frac{SS}{150} \quad \frac{5.2}{100} \quad \frac{7.7}{81} \quad -22.4$$

$$\frac{SS}{175} \quad \frac{0.6}{100} \quad \frac{5.0}{64} \quad \frac{8.8}{39} \quad \frac{14.4}{25} \quad -21.4$$

$$\frac{SS}{175} \quad \frac{00}{100} \quad \frac{7.2}{48} \quad \frac{8.9}{31} \quad -20.4$$

$$\frac{SS}{175} \quad \frac{0.4}{100} \quad \frac{2.8}{81} \quad \frac{9.4}{40} \quad \frac{11.5}{25} \quad -19.5$$

Sta + x -
935.05

4 14.9

+40 15.7

4 +93 17.9

5 +75 15.1

6 16.0

+75 21.3 -

0 0.48 923.31 ✓ 12.22 922.83 ✓

5+75 15.1 -

6 16.0 -

$$\frac{5.5}{17.5} \quad \frac{5.7}{100} \quad \frac{8.9}{80} \quad -20.2$$

$$\frac{0.5}{150} \quad \frac{8.8}{100}$$

$$-19.4$$

$$\frac{5.5}{250} \quad \frac{3.4}{150} \quad \frac{6.0}{125} \quad \frac{7.6}{100} \quad \frac{8.9}{64}$$

$$-17.7$$

$$\frac{3.7}{100} \quad \frac{5.1}{87} \quad \frac{12.1}{58}$$

$$-20.0$$

$$\frac{4.1}{100} \quad \frac{11.7}{65}$$

$$-19.1$$

11.7

$$\frac{6.5}{100} \quad \frac{9.9}{60} \quad \frac{11.5}{30} \quad \frac{11.7}{13} \quad \frac{13.2}{10} \quad 13.8 \quad \frac{14.5}{9} \quad \frac{13.7}{11}$$

$$\frac{5.5}{40} \quad \frac{7.4}{25} \quad \frac{8.1}{7} \quad 8.2 \quad \frac{8.5}{4} \quad \frac{9.4}{7} \quad \frac{11.0}{37} \quad \frac{13.2}{80} \quad \frac{14.5}{100}$$

$$\frac{4.5}{49} \quad \frac{6.9}{30} \quad \frac{7.5}{6} \quad 7.3 \quad \frac{7.3}{4} \quad \frac{8.3}{7} \quad \frac{9.5}{28} \quad \frac{11.0}{44} \quad \frac{12.7}{74} \quad \frac{14.5}{100}$$

Sta

+

π

-

923.31 ✓

6+75

21.3

0

302

925.85 ✓

0.48

922.83 ✓

7

19.0 -

+60

15.8 -

8

17.7 -

9

22.6 -

BM

13.24

935.43 ✓

3.66

922.19 ✓

+45

23.7 -

10

25.2 -

$$\textcircled{-20} \quad \frac{3.7}{23} \quad \frac{5.8}{41} \quad \frac{8.6}{56} \quad \frac{12.5}{85} \quad \frac{13.7}{100}$$

$$\frac{+1.7}{100} \quad \frac{00}{62} \quad \frac{3.0}{14} \quad \frac{5.8}{10} \quad \frac{6.6}{3} \quad 6.9 \quad \frac{6.6}{9} \quad \frac{13.6}{56} \quad \frac{15.3}{74} \quad \frac{15.8}{100}$$

$$\frac{7.4}{100} \quad \frac{8.6}{56} \quad \frac{10.6}{9} \quad \frac{9.9}{6} \quad 10.1 \quad \frac{10.4}{6} \quad \frac{12.4}{46} \quad \frac{13.2}{100}$$

$$\frac{9.0}{100} \quad \frac{10.1}{44} \quad \frac{9.3}{11} \quad \frac{8.4}{8} \quad 8.2 \quad \frac{8.2}{7} \quad \frac{7.9}{65} \quad \frac{7.7}{100}$$

$$\frac{3.6}{100} \quad \frac{3.1}{74} \quad \frac{4.8}{35} \quad \frac{4.5}{16} \quad \frac{3.2}{5} \quad 3.3 \quad \frac{3.2}{8} \quad \frac{1.5}{11} \quad \frac{00}{21} \quad \frac{+4.5}{49} \quad \frac{+5.0}{82} \quad \frac{+4.0}{100}$$

SpKin 24" W. Oak 100' Lt. Sta 9+00

$$\frac{9.9}{100} \quad \frac{11.0}{31} \quad \frac{10.7}{17} \quad \frac{10.6}{12} \quad \frac{11.4}{10} \quad 11.7 \quad \frac{11.4}{7} \quad \frac{9.7}{10} \quad \frac{6.7}{37} \quad \frac{5.2}{67} \quad \frac{6.2}{96} \quad \frac{6.9}{100}$$

$$\frac{8.7}{100} \quad \frac{10.3}{48} \quad \frac{10.2}{9} \quad 10.2 \quad \frac{10.3}{4} \quad \frac{10.4}{25} \quad \frac{6.4}{84} \quad \frac{6.7}{100}$$

Sta + π -
935.43

11 23.6 -

+40 30.7 -

⊙ 13.01 948.10 0.34 935.09 ✓

12 37.6 -

+55 45.6 -

⊙ 12.18 959.62 0.66 947.44 ✓

13 51.5 -

+60 4 Shot 56.4 -

14 58.8 -

⊙ 13.42 972.58 0.46 959.16 ✓

$$\frac{+1.7}{100} \quad \frac{2.1}{53} \quad \frac{4.7}{29} \quad \frac{5.9}{13} \quad \frac{6.7}{11} \quad \frac{6.2}{9} \quad 6.8 \quad \frac{7.9}{8} \quad \frac{8.8}{66} \quad \frac{5.6}{100}$$

$$\frac{55.}{100} \quad \frac{+9.0}{80} \quad \frac{+4.4}{56} \quad \frac{+0.7}{41} \quad \frac{2.6}{24} \quad \frac{4.2}{13} \quad 4.7 \quad \frac{6.1}{9} \quad \frac{7.3}{65} \quad \frac{4.9}{100}$$

$$\frac{+6.6}{100} \quad \frac{+2.0}{67} \quad \frac{3.0}{35} \quad \frac{7.8}{12} \quad \frac{10.6}{8} \quad 10.5 \quad \frac{11.7}{7} \quad \frac{14.5}{24} \quad \frac{15.8}{83} \quad \frac{15.6}{100}$$

$$\frac{55.}{100} \quad + \frac{11.4}{87} \quad \frac{+8.0}{55} \quad \frac{+3.1}{14} \quad \frac{+2.0}{11} \quad \frac{2.5}{6} \quad 2.5 \quad \frac{2.4}{9} \quad \frac{8.5}{50} \quad \frac{11.9}{100}$$

$$\frac{+4.2}{100} \quad \frac{2.1}{32} \quad \frac{3.8}{12} \quad \frac{7.6}{7} \quad 8.1 \quad \frac{8.4}{10} \quad \frac{13.6}{50} \quad \frac{17.8}{100}$$

3.2

$$\frac{+8.0}{100} \quad \frac{+7.0}{70} \quad \frac{+3.7}{17} \quad \frac{+0.6}{11} \quad \frac{0.7}{10} \quad 0.8 \quad \frac{3.9}{19} \quad \frac{6.9}{73} \quad \frac{9.8}{100}$$

Sta + π -
972.58

14+30

60.8 -

15

64.2 -

+50

65.2 -

16

65.0 -

17

66.6 -

+70

69.1 -

○

4.40

✓
973.48

3.50

✓
969.08

18

68.2 -

+50

64.4 -

$$\frac{5.4}{100} \quad \frac{8.0}{53} \quad \frac{11.6}{11} \quad 11.8 \quad \frac{13.6}{52} \quad \frac{16.8}{100}$$

$$\frac{6.6}{100} \quad \frac{5.3}{59} \quad \frac{5.5}{22} \quad \frac{8.6}{10} \quad 8.4 \quad \frac{11.1}{33} \quad \frac{15.1}{100}$$

$$\frac{3.6}{100} \quad \frac{3.7}{63} \quad \frac{6.3}{14} \quad \frac{8.0}{10} \quad 7.4 \quad \frac{8.2}{15} \quad \frac{10.6}{60} \quad \frac{11.8}{100} \quad \text{Floor Ht. } \nearrow 9.05$$

$$\frac{4.0}{100} \quad \frac{4.2}{57} \quad \frac{6.7}{15} \quad \frac{8.0}{13} \quad 7.6 \quad \frac{7.7}{6} \quad \frac{10.2}{56} \quad \frac{11.3}{100}$$

$$\frac{3.8}{100} \quad \frac{7.2}{62} \quad \frac{5.9}{21} \quad \frac{6.1}{6} \quad 6.0 \quad \frac{6.1}{5} \quad \frac{6.7}{53} \quad \frac{6.5}{100}$$

$$\frac{5.0}{100} \quad \frac{4.4}{62} \quad \frac{1.9}{32} \quad \frac{1.8}{14} \quad \frac{3.6}{11} \quad 3.5 \quad \frac{3.9}{15} \quad \frac{1.4}{18} \quad \frac{1.2}{41} \quad \frac{0.4}{100}$$

Top Boat Spk Sta 17+65.46

$$\frac{6.5}{100} \quad \frac{6.0}{89} \quad \frac{4.4}{36} \quad \frac{3.1}{14} \quad \frac{5.9}{10} \quad \frac{5.8}{7} \quad 5.3 \quad \frac{5.8}{6} \quad \frac{5.9}{11} \quad \frac{2.2}{17} \quad \frac{0.9}{46} \quad \frac{1.0}{73} \quad \frac{1.3}{100}$$

Floor Ht. +2.65

$$\frac{7.0}{100} \quad \frac{9.1}{53} \quad \frac{8.3}{13} \quad \frac{9.8}{12} \quad \frac{9.4}{8} \quad 9.1 \quad \frac{9.1}{4} \quad \frac{9.4}{9} \quad \frac{6.2}{15} \quad \frac{4.1}{43} \quad \frac{2.5}{68} \quad \frac{1.2}{100}$$

$$\frac{10.2}{100} \quad \frac{13.0}{50} \quad \frac{14.5}{11} \quad \frac{13.4}{7} \quad 13.5 \quad \frac{13.5}{4} \quad \frac{14.6}{12} \quad \frac{12.4}{50} \quad \frac{10.6}{100}$$

$$\frac{7.3}{100} \quad \frac{8.4}{56} \quad \frac{8.8}{15} \quad \frac{5.5}{7} \quad 5.4 \quad \frac{5.5}{3} \quad \frac{8.8}{9} \quad \frac{7.6}{53} \quad \frac{4.0}{100}$$

$$\frac{8.5}{100} \quad \frac{8.6}{56} \quad \frac{9.0}{15} \quad \frac{6.3}{7} \quad 6.2 \quad \frac{6.3}{3} \quad \frac{8.6}{11} \quad \frac{7.4}{50} \quad \frac{4.2}{100}$$

FL 9.44 FL 9.32

$$\frac{8.1}{100} \quad \frac{7.9}{57} \quad \frac{8.1}{14} \quad \frac{6.4}{7} \quad 6.3 \quad \frac{6.3}{2} \quad \frac{8.5}{9} \quad \frac{5.0}{55} \quad \frac{1.3}{82} \quad \frac{5.5}{100}$$

Nail in Dead Oak Tr. SoLtSta 23+40

$$\frac{12.9}{100} \quad \frac{10.8}{75} \quad \frac{10.1}{38} \quad \frac{10.7}{22} \quad 16 \quad \frac{13.1}{14} \quad \frac{11.2}{9} \quad 10.9 \quad \frac{10.9}{2} \quad \frac{12.9}{9} \quad \frac{11.5}{43} \quad \frac{6.1}{82} \quad \frac{3.0}{100}$$

$$\frac{13.6}{100} \quad \frac{11.6}{76} \quad \frac{12.1}{38} \quad \frac{13.2}{16} \quad \frac{11.0}{9} \quad 11.0 \quad \frac{11.1}{1} \quad \frac{11.4}{5} \quad \frac{12.9}{8} \quad \frac{10.4}{51} \quad \frac{8.0}{80} \quad \frac{4.6}{100}$$

$$\frac{10.9}{100} \quad \frac{12.4}{76} \quad \frac{13.5}{23} \quad \frac{12.6}{16} \quad \frac{11.1}{11} \quad 11.0 \quad \frac{11.2}{2} \quad \frac{11.9}{6} \quad \frac{10.0}{47} \quad \frac{5.1}{80} \quad \frac{6.5}{100}$$

Sta + π ✓ -
966.56

23 57.7 -

24 60.4 -

+70 61.9 -

25 61.3 -

+80 57.1 -

26 56.6 -

+13 56.4 -

+24 56.3 -

B.M. 6.65 959.91 ✓

$$\frac{8.5}{46} \quad \frac{10.5}{48} \quad \frac{10.4}{28} \quad \frac{11.1}{26} \quad \frac{10.7}{20} \quad \frac{10.2}{19} \quad \frac{9.1}{11} \quad 9.3 \quad \frac{9.0}{7} \quad \frac{5.8}{44} \quad \frac{1.0}{100}$$

$$\frac{8.2}{100}$$

$$\frac{8.8}{100} \quad \frac{8.5}{53} \quad \frac{7.3}{28} \quad 23 \quad \frac{7.9}{20} \quad \frac{7.1}{19} \quad \frac{6.3}{12} \quad 6.2 \quad \frac{5.8}{1} \quad \frac{4.5}{21} \quad \frac{3.3}{54} \quad \frac{0.9}{100}$$

$$\frac{7.7}{100} \quad \frac{3.7}{42} \quad \frac{4.2}{16} \quad \frac{4.8}{15} \quad \frac{4.5}{11} \quad 4.7 \quad \frac{4.7}{1} \quad \frac{5.1}{3} \quad \frac{3.5}{52} \quad \frac{2.2}{100}$$

$$\frac{7.7}{100} \quad \frac{2.8}{43} \quad \frac{3.8}{27} \quad \frac{4.3}{17} \quad \frac{5.7}{15} \quad \frac{5.5}{12} \quad \frac{5.4}{11} \quad 5.3 \quad \frac{2.3}{59} \quad \frac{1.7}{90} \quad \frac{1.6}{100}$$

Floor Ho. +1.80

$$\frac{16.2}{100} \quad \frac{10.1}{40} \quad \frac{9.7}{15} \quad \frac{10.2}{13} \quad \frac{9.7}{10} \quad 9.5 \quad \frac{9.5}{2} \quad \frac{9.3}{8} \quad \frac{6.7}{17} \quad \frac{3.2}{59} \quad \frac{2.9}{32} \quad \frac{3.1}{100}$$

$$\frac{19.7}{100} \quad \frac{16.2}{58} \quad \frac{12.0}{24} \quad \frac{11.0}{14} \quad \frac{9.9}{5} \quad 10.0 \quad \frac{10.3}{5} \quad \frac{10.1}{10} \quad \frac{7.5}{18} \quad \frac{5.7}{58} \quad \frac{5.0}{100}$$

$$\frac{14.0}{100} \quad \frac{12.9}{65} \quad \frac{11.8}{29} \quad \frac{10.6}{9} \quad 10.2 \quad \frac{9.7}{34} \quad \frac{8.3}{67} \quad \frac{6.8}{100}$$

$$\frac{13.8}{100} \quad \frac{12.3}{53} \quad 10.3 \quad \frac{8.1}{65} \quad \frac{6.9}{100}$$

SPK in 12" W. Oak 130 Lt. Sta 2A+30

Sta

+

x

-

966.56 ✓

⊙

1.45

954.65 ✓

13.36

953.20 ✓

⊙

11.02

965.23 ✓

0.44

954.21 ✓

⊙

7.61

961.71 ✓

11.13

954.10 ✓

BM

6.23

955.48 ✓

⊙

0.37

948.88 ✓

13.20

948.51 ✓

⊙

0.76

939.33 ✓

10.31

938.57 ✓

⊙

6.60

945.15 ✓

0.78

938.55 ✓

⊙

4.76

947.21 ✓

2.70

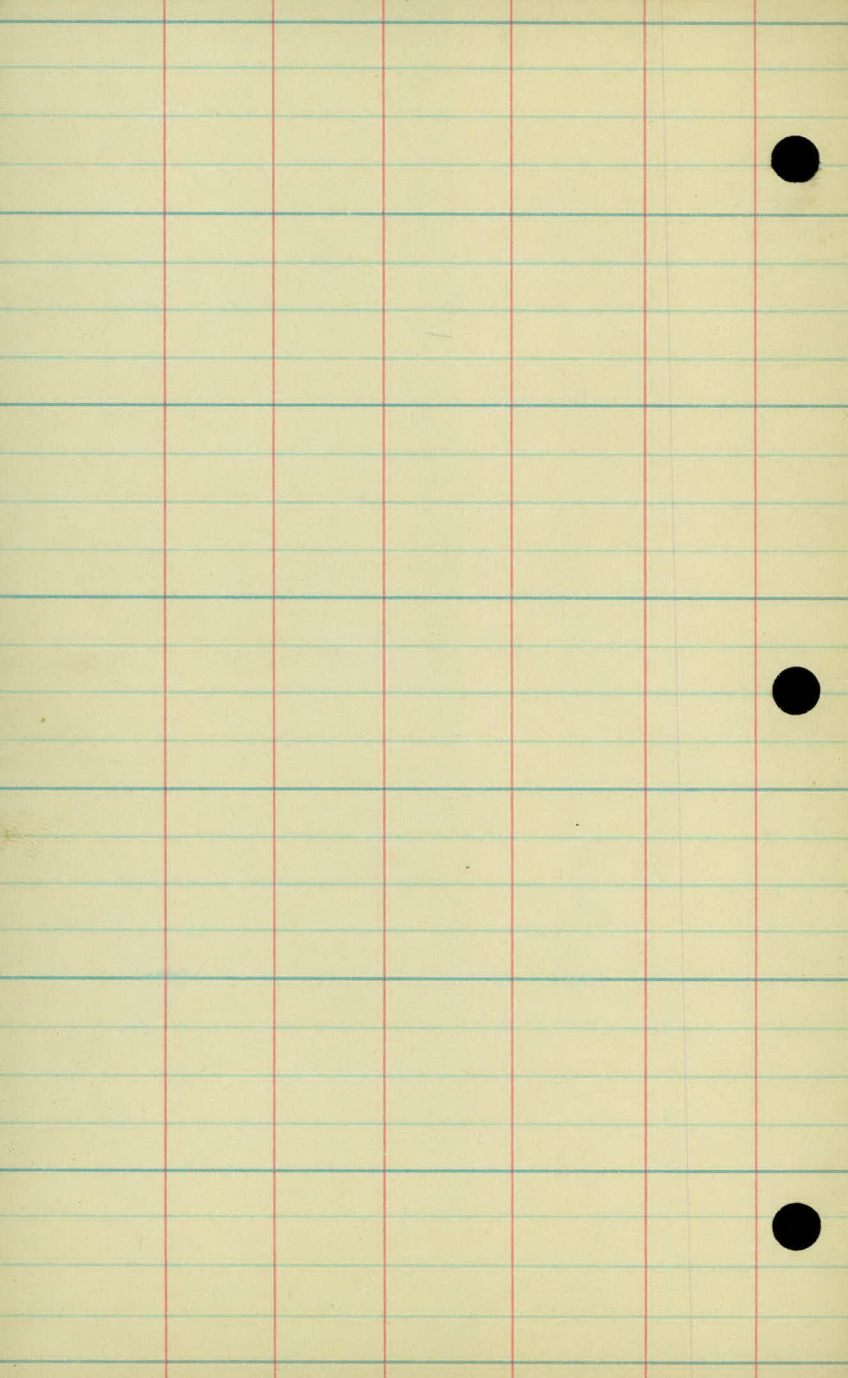
942.45 ✓

2.85

944.36 = 944.37 ✓

R.R. SpK in P.P. SE Cor. Co. Rd E and Fairchild

SpK in 10" Oak NW. Cor Silver Lake Rd. & Fairchild Ave



Fairfield Drive

Blue Tops

4/26/37

Sta.	+	π	-	Elev.	Grade Road
B.M.	2.46	950.41		947.95	
0+40				47.6	2.8
1				44.6	5.8
+50				47.1	8.3
+75				41.3	9.1
2				40.6	9.8
+40				39.5	10.9
3				38.4	11.0
T.P.	4.03	942.44	12.00	938.41	
+60				37.7	4.7
4				37.7	11.2
+50				36.6	5.9
+80				36.7	6.2
5				36.0	6.4

Sta. + π - Elev.

94844

+45

35.6

6.8

6

35.1

7.3

+50

34.9

7.5

+75

34.7

7.7

7

34.6

7.8

T.P.

391

937.93

8.46

933.98

+85

34.5

3.4

8

34.3

3.6

+44

34.0

3.9

9

33.3

4.6

+50

32.5

5.4

10

31.6

6.3

11

29.8

8.1

14

28.0

9.9

Sta.	+	K	-	Elev.
		937.93		
13				26.2 11.7
B.M.			8.37	929.56

Sta.	+	π	-	Grade
B.M.	12.44	923.77		911.33

0				19.3	4.5
---	--	--	--	------	-----

+50				17.8	6.0
-----	--	--	--	------	-----

1				16.8	7.0
---	--	--	--	------	-----

+50				16.5	7.3
-----	--	--	--	------	-----

2				16.7	7.1
---	--	--	--	------	-----

+50				17.1	6.7
-----	--	--	--	------	-----

3				17.5	6.3
---	--	--	--	------	-----

+50				17.9	5.9
-----	--	--	--	------	-----

4				18.3	5.5
---	--	--	--	------	-----

+50				18.7	5.1
-----	--	--	--	------	-----

5				19.1	4.7
---	--	--	--	------	-----

+50				19.5	4.3
-----	--	--	--	------	-----

6				19.9	3.9
---	--	--	--	------	-----

Check Pkgs
 Antennas Price
 6/11/97

Sta.	+	x	-	Erode	
		923.77			
+50				20.3	3.5
7				20.7	3.1
+50				21.1	2.7
8				21.7	2.1
+50				22.4	1.4
T.P.	12.18	935.15	0.80		922.97
9				24.0	11.1
+50				25.7	9.4
10				27.9	7.2
+50				30.2	4.9
11				33.4	1.7
T.P.	12.25	945.70	1.70		933.41
+40				36.0	9.7
12				40.2	5.5
+50				43.7	2.0

922.97
 12.18
 935.15
 12.8
 922.17 OK

922.97
 11.1
 932.19

25.

+

+

-

Grade

13

47.4

+50

50.7

14

54.2

+50

57.2

15

60.0

+50

62.1

16

63.5

+50

64.1

17

64.7

+50

64.4

18

64.1

+50

63.5

6.6

19

62.5

7.6

H.S. 945.70
 - 10.48

 T.P. 935.22
 + 11.84

 H.S. 947.06
 - 9.93

 T.P. 937.13
 + 13.18

 H.S. 950.31
 - 9.20

 T.P. 941.11

970.11

Sta	+	-	Grade
		970.11	
19			61.4 8.7
20			60.3 9.8
+50			59.4 10.7
T.P.	4.28	963.69	10.70 959.4)
21			58.6 5.1
+50			58.3 5.4
22			57.9 5.8
+50			58.0 6.9
23			58.2 5.5
+50			58.3 5.4
24		963.8	58.5 6.3
+70			58.3 5.5
25		$\begin{array}{r} 963.69 \\ 3.90 \\ \hline 959.79 \\ 963.81 \end{array}$	57.9 5.9
+80			56.8 7.0 7.4
26			56.4 959.91

9/13/35

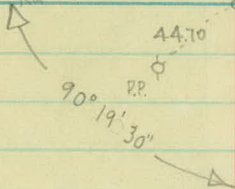
Alignment
Sunset Lane
in
Mounds View Acres

13+15.14 POT.

6+57.57 POT.

0+00 POT.

Valley View Rd

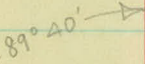


Boat SpK

31.71

Fcc Po.

Fairfield Dr



Boat SpK

650 Hub

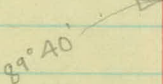
PP

nail

44.92

3" Willow

Fairchild Av



Boat SpK

35.56

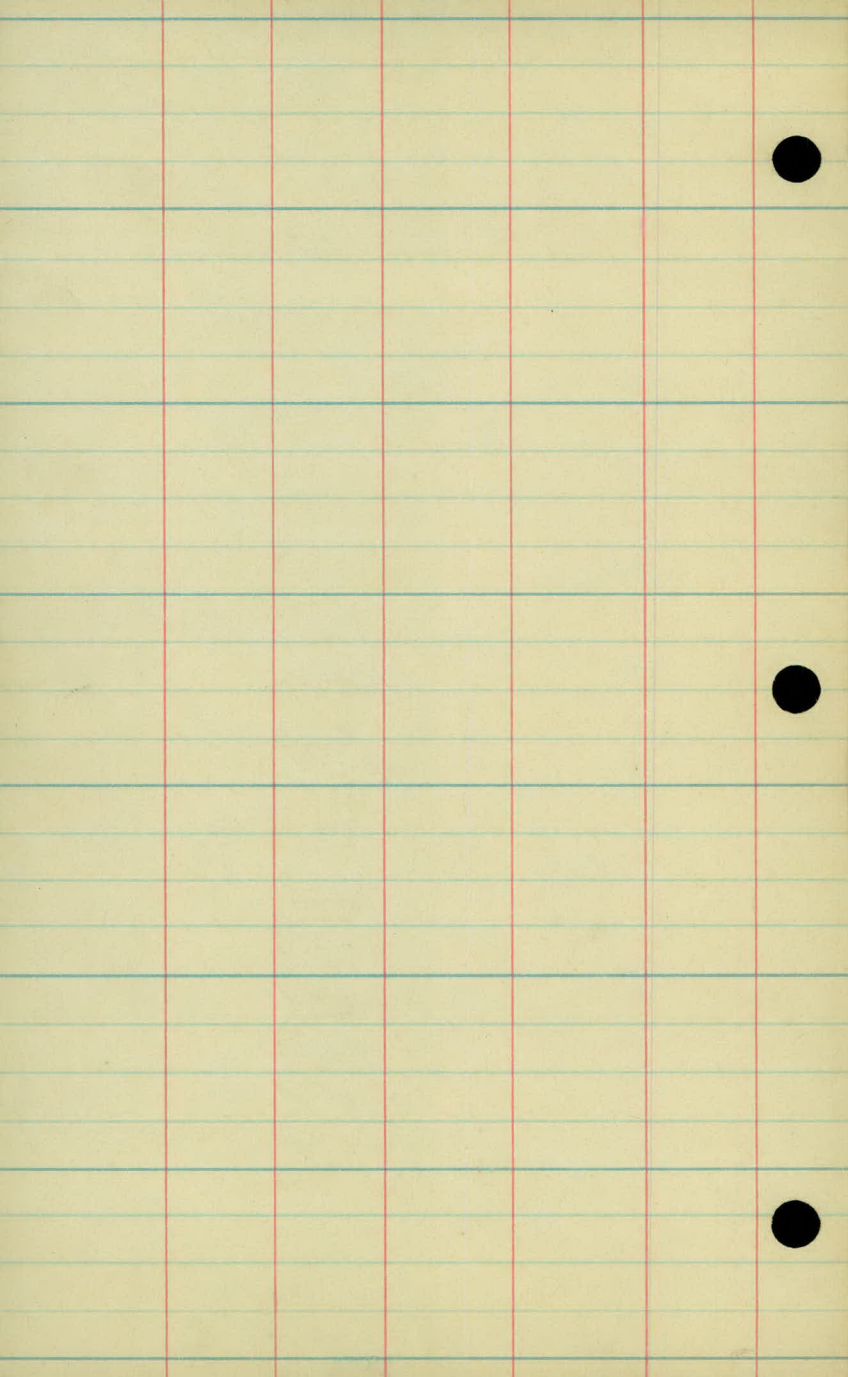
Guy Po.

P.P.

31.29

59.69

18" Oak



TOPOGRAPHY
SUNSET LANE
in
MOUNDS VIEW ACRES

Rd
8-6

Hoc
X

+77 Tr
37

+44 Ent R/L-10"x18"CM

+25 End berrie P
34

Hoculu - 11

+54 Beq Row Golden Willows
33

15'c-c

4

Rd
9-6

+30 PP +16 berrie Patch
30 36
+28 Fcc N+S
30

+91 Cor. Ho.
62
+35 Ent-10"x24"CM
14

+15-10"oak
34
+40-12"oak
33
+28 EC
31
+20 Fcc
28

3

Rd
8-8

Fcc
27

+95-12"x30"CM
14.5 15.5

+70 AppleTr
54
+92 Ap.Tr
54
+06 Car Shed

+08 Ent 15"x18"CM
18

2

Fcc
27

+45 PP
28

+45 Ent

1

Rd
8-11

Fcc
27

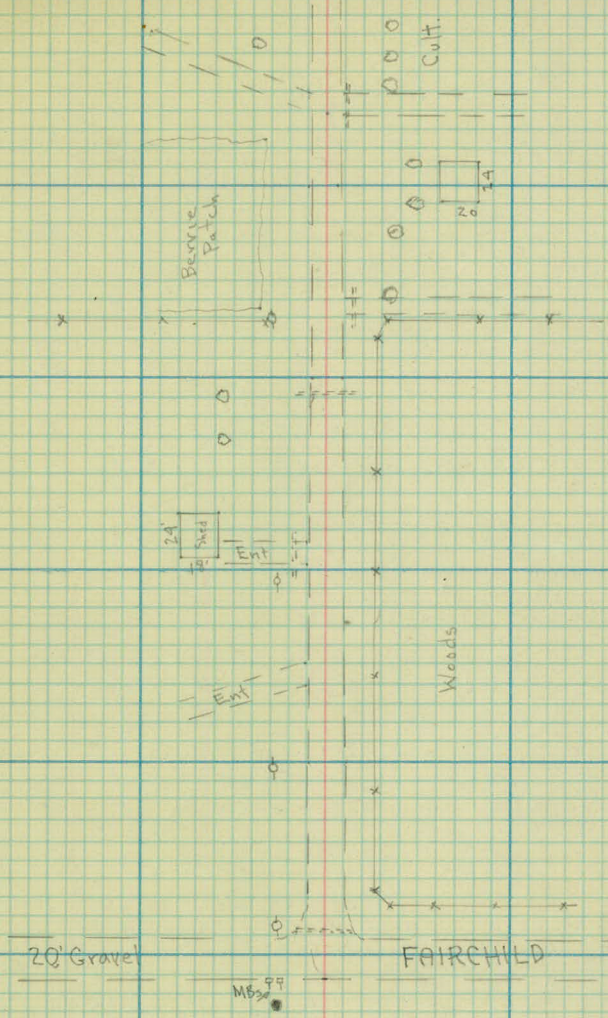
+99 PP
29

+15 PP
28

+33 Fcc
27
+25 Fcc
35

+11-12"x32"CM (buried)
14.5-17.5

0+00



20' Grave

20' Tang

24'
10'
Shed

Ent

M530 99

Cult.

Woods

FAIRCHILD

12 $\frac{Rd}{6-11}$

11 $\frac{+35 P.P.}{32}$ $\frac{Rd}{2-14}$

10 $\frac{+84 Cor. Hb}{73}$
 $+03 Ent$
End Fee $\frac{Rd}{2-12}$
31

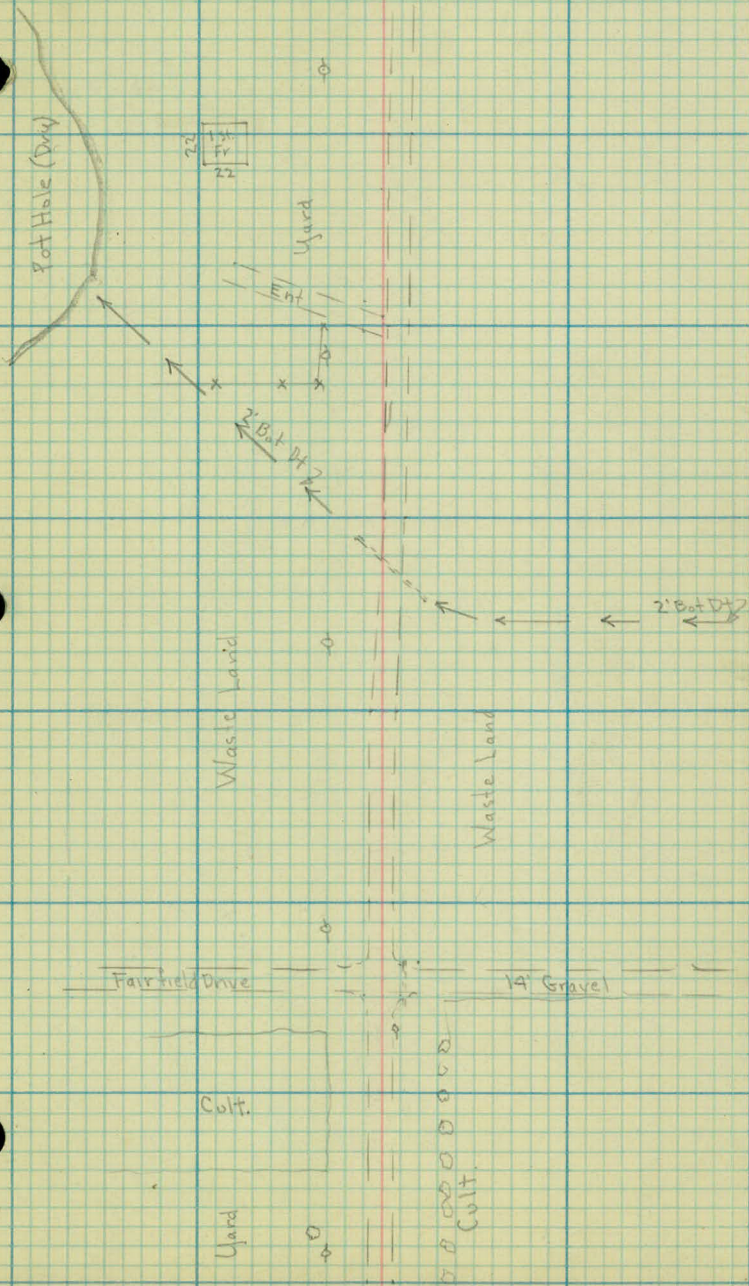
9 $\frac{+71 Fc.}{35}$ $\frac{+86 PP}{31}$
 $\frac{Rd}{0-11}$

8 $+79 = 18' \times 52' CM$
 $\frac{+89 End Culy}{16}$ $\frac{+56 End Culy}{22}$
 $\frac{+36 P.P.}{30}$ $\frac{Rd}{4-7}$

7 $\frac{Rd}{7-6}$
 $\frac{+87 PP}{30}$ $+58 \& Fairfield Dr$ $\frac{+58 Str. - 12' \times 20' CM}{12}$ $+47 End Cult$
 $+36 End Cult$ $\frac{+33 MBs}{7}$ $+27 End Willows$
33

6 $\frac{Rd}{8-6}$

5 $\frac{+60 Beg Cult}{30}$
 $\frac{+28 Tr}{29}$
 $\frac{+16 PP}{30}$



13

+15 Rd
80

Rd
34-11

+88 PP
35

+64 End Culv

+80 Trk

+59 Trk

+89 Edge Rd

+72-24'x40' CM

+65 Edge Rd

13+67 End RR Culv

+12+98 End 36"x86" Conc RR Pipe

22

In Sta 12

+94 End Culv (Hwd)
19

+50 Trk
107 - 130

13+47 Beg RR Fee
35

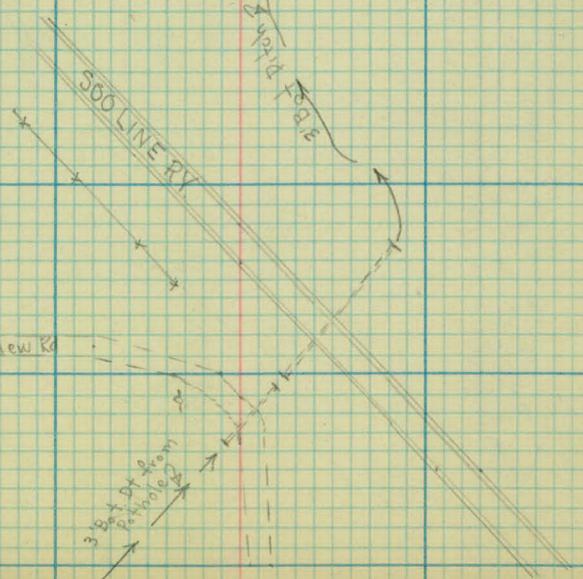
12

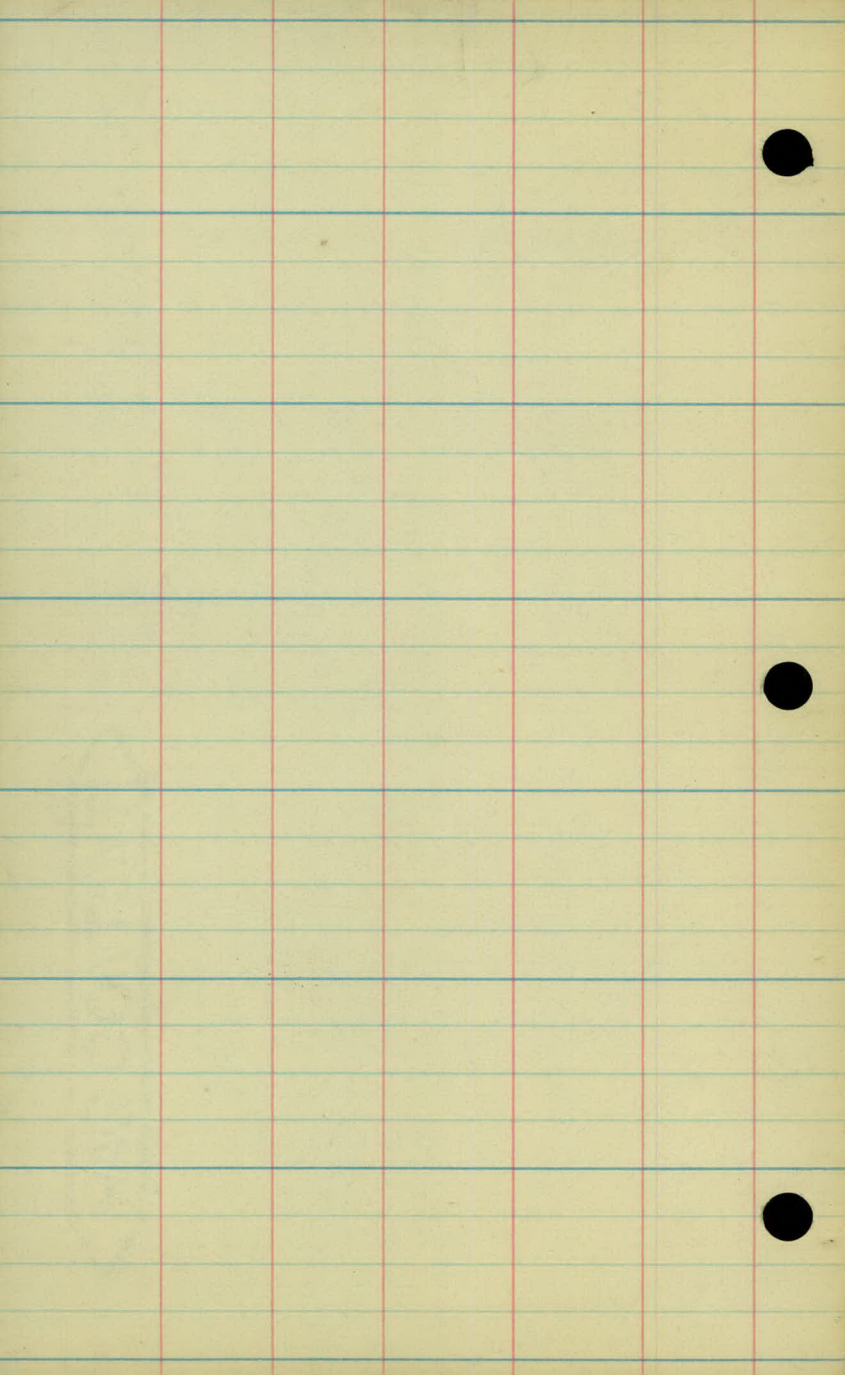
12' Gravel
+15 Valley View Rd

3 1/2' x 4' x 8' beam
Per hole

500 LINE RY

38' Pitch





9/12/35

Portell

x- sections Sunset Lane

in

Mounds View Acres

Sta	+	π	-	
B.M.	11.14	970.39 ✓		959.25 ✓

⊙	0.31	960.48 ✓	10.22	960.17 ✓
---	------	----------	-------	----------

⊙	6.06	957.84 ✓	8.70	951.78 ✓
---	------	----------	------	----------

B.M.	10.28	963.40 ✓	4.72	953.12 ✓
------	-------	----------	------	----------

0+00				52.2 ✓ ± Sunset Lane and Fairchild
------	--	--	--	---------------------------------------

+09				52.2 ✓
-----	--	--	--	--------

+50				53.8 ✓
-----	--	--	--	--------

1				54.1 ✓
---	--	--	--	--------

+70				51.3 ✓
-----	--	--	--	--------

Top Angle van @ base of Elec. Tower So pier NE.
 Cor. Fairchild and Co. Rd. D

R.R SpK in 30" Bl. Oak 25' W and 100' N. of Fairchild & Sunset Lane

$\frac{13}{100}$ $\frac{123}{63}$ 11.2 $\frac{10.6}{56}$ $\frac{10.4}{100}$

$\frac{13.3}{100}$ $\frac{123}{49}$ 11.2 $\frac{10.8}{56}$ $\frac{10.9}{100}$

$\frac{9.9}{100}$ $\frac{7.7}{58}$ $\frac{6.7}{51}$ $\frac{5.4}{19}$ $\frac{9.5}{13}$ $\frac{10.3}{11}$ 9.6 $\frac{10.0}{8}$ $\frac{10.2}{11-13}$ $\frac{9.5}{16}$ $\frac{7.9}{17}$ $\frac{7.6}{27}$ $\frac{6.7}{65}$ $\frac{7.6}{100}$

$\frac{8.4}{100}$ $\frac{7.5}{56}$ $\frac{2.8}{52}$ $\frac{2.1}{22}$ $\frac{9.1}{11}$ $\frac{9.6}{9}$ 9.3 $\frac{9.7}{11}$ $\frac{9.5}{15}$ $\frac{8.0}{18}$ $\frac{7.3}{26}$ $\frac{13.3}{57}$ $\frac{15.2}{100}$

$\frac{20.0}{85}$ $\frac{14.7}{57}$ $\frac{13.4}{14}$ $\frac{12.5}{7}$ 12.1 $\frac{12.9}{11}$ $\frac{13.0}{16}$ $\frac{12.2}{78}$ $\frac{13.1}{26}$ $\frac{15.1}{68}$ $\frac{15.3}{88}$ $\frac{13.8}{100}$

Sta

+

X

-

963.40

0

174

951.79 ✓

13.35

950.05 ✓

2+00

49.4 ✓

3+00

46.1 ✓

+40

46.0 ✓

4

46.7 ✓

+65

47.9 ✓

5

49.0 ✓

0

9.97

960.88 ✓

0.88

950.91 ✓

+65

50.8 ✓

$\frac{3.5}{100}$	$\frac{6.2}{60}$	$\frac{5.3}{45}$	$\frac{3.8}{20}$	$\frac{2.9}{7}$	2.4	$\frac{2.8}{7}$	$\frac{3.0}{10}$	$\frac{3.2}{13}$	$\frac{5.6}{26}$	$\frac{6.1}{34}$	$\frac{5.0}{47}$	$\frac{3.5}{60}$
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Fee

+95-12"X30'CM

F.L.EI 40.79

F.L.EI 41.68

$\frac{3.0}{100}$

$\frac{12.0}{100}$	$\frac{4.8}{87}$	$\frac{12.5}{57}$	$\frac{11.5}{28}$	$\frac{9.6}{15}$	$\frac{6.6}{9}$	5.7	$\frac{5.9}{9}$	$\frac{6.3}{12}$	$\frac{9.3}{17}$	$\frac{9.6}{27}$	$\frac{6.0}{52}$	$\frac{0.5}{87}$	+0.5
--------------------	------------------	-------------------	-------------------	------------------	-----------------	-----	-----------------	------------------	------------------	------------------	------------------	------------------	------

Fee

$\frac{15.0}{100}$	$\frac{11.0}{25}$	$\frac{7.9}{16}$	$\frac{6.9}{11}$	$\frac{6.4}{7}$	5.8	$\frac{6.0}{10}$	$\frac{7.1}{14}$	$\frac{5.9}{17}$	$\frac{5.6}{25}$	$\frac{6.0}{30}$	$\frac{4.5}{57}$	$\frac{2.3}{100}$
--------------------	-------------------	------------------	------------------	-----------------	-----	------------------	------------------	------------------	------------------	------------------	------------------	-------------------

over Hl.

$\frac{14.5}{100}$	$\frac{11.1}{58}$	$\frac{8.6}{34}$	$\frac{7.1}{31}$	$\frac{6.1}{16}$	$\frac{6.6}{15}$	$\frac{5.7}{10}$	5.1	$\frac{5.4}{8}$	$\frac{5.7}{11}$	$\frac{3.5}{15}$	$\frac{3.4}{13}$	$\frac{0.6}{27}$	+1.6
--------------------	-------------------	------------------	------------------	------------------	------------------	------------------	-----	-----------------	------------------	------------------	------------------	------------------	------

+H_o

$\frac{12.4}{100}$	$\frac{12.0}{84}$	$\frac{9.7}{63}$	$\frac{7.4}{33}$	$\frac{5.6}{13}$	$\frac{4.5}{10}$	3.9	$\frac{4.0}{8}$	$\frac{4.3}{11-12}$	$\frac{3.8}{14}$	$\frac{3.1}{28}$	$\frac{2.4}{37}$	$\frac{0.8}{58}$	+3.5
--------------------	-------------------	------------------	------------------	------------------	------------------	-----	-----------------	---------------------	------------------	------------------	------------------	------------------	------

$\frac{9.6}{100}$	$\frac{6.8}{72}$	$\frac{4.4}{42}$	$\frac{3.5}{18}$	$\frac{4.1}{16}$	$\frac{4.2}{12}$	$\frac{3.3}{9}$	2.8	$\frac{2.9}{8}$	$\frac{3.4}{10-13}$	$\frac{2.9}{15}$	$\frac{2.6}{28}$	$\frac{1.09}{65}$	+2.5
-------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----	-----------------	---------------------	------------------	------------------	-------------------	------

$\frac{6.4}{100}$	$\frac{5.7}{83}$	$\frac{4.6}{41}$	$\frac{5.7}{26}$	$\frac{11.4}{18}$	$\frac{11.6}{15}$	$\frac{10.4}{12}$	$\frac{16.3}{10}$	10.1	$\frac{10.5}{7}$	$\frac{11.1}{8-11}$	$\frac{8.9}{16}$	$\frac{9.0}{27}$	$\frac{9.4}{33}$	$\frac{8.6}{61}$	$\frac{7.7}{84}$
-------------------	------------------	------------------	------------------	-------------------	-------------------	-------------------	-------------------	------	------------------	---------------------	------------------	------------------	------------------	------------------	------------------

58. A
100

Sta

+

x

-

960.88 ✓

6

50.9 ✓

+23

50.7 ✓

+41

50.3 ✓

+48

50.1 ✓

+58

± Valley View Rd.

49.7 ✓

B.M.

6.35

954.53 ✓

+65

49.2 ✓

+68

49.0 ✓

+81

48.2 ✓

$\frac{64}{100}$ $\frac{41}{77}$ $\frac{4.0}{44}$ $\frac{53}{27}$ $\frac{11.2}{18-15}$ $\frac{10.1}{10}$ 10.0 $\frac{10.4}{6}$ $\frac{11.0}{9-11}$ $\frac{8.0}{16-27}$ $\frac{8.2}{63}$ $\frac{6.3}{100}$

$\frac{11.2}{100}$ $\frac{4.2}{50}$ $\frac{5.2}{29}$ $\frac{11.5}{17-15}$ $\frac{10.4}{11}$ 10.2 $\frac{10.8}{6}$ $\frac{11.4}{9-12}$ $\frac{8.5}{17}$ $\frac{8.7}{33}$ $\frac{8.8}{65}$ $\frac{7.0}{100}$

$\frac{13.4}{100}$ $\frac{9.5}{86}$ $\frac{12.6}{82}$ $\frac{11.9}{55}$ $\frac{12.1}{40}$ $\frac{11.7}{18}$ 10.6 $\frac{11.2}{7}$ $\frac{11.7}{11}$ $\frac{11.3}{13}$ $\frac{8.9}{18}$ $\frac{9.3}{46}$ $\frac{8.7}{74}$ $\frac{6.6}{100}$

$\frac{16.4}{100}$ $\frac{14.3}{76}$ $\frac{13.5}{52}$ $\frac{12.1}{28}$ 10.8 $\frac{11.2}{19}$ $\frac{9.8}{50}$ $\frac{6.6}{100}$

$\frac{16.3}{100}$ $\frac{13.8}{49}$ $\frac{12.1}{34}$ 11.2 $\frac{10.7}{24}$ $\frac{8.8}{57}$ $\frac{5.9}{100}$ $\frac{4.0}{130}$

RR Spk in PP. 125' S and 35' E of Sunset Lane + Fairfield Drive

$\frac{16.8}{100}$ $\frac{12.7}{41}$ 11.7 $\frac{12.5}{13}$ $\frac{10.6}{37}$ $\frac{8.6}{73}$ $\frac{7.1}{100}$

$\frac{17.7}{100}$ $\frac{12.7}{41}$ 11.9 $\frac{12.2}{8}$ $\frac{12.9}{11-13}$ $\frac{12.4}{15}$ $\frac{9.2}{17}$ $\frac{9.1}{43}$ $\frac{8.3}{69}$

$\frac{6.9}{100}$

$\frac{18.7}{100}$ $\frac{13.4}{77}$ $\frac{11.7}{13}$ $\frac{12.4}{18}$ $\frac{13.7}{15}$ $\frac{13.6}{11}$ $\frac{12.7}{8}$ 12.7 $\frac{13.0}{8}$ $\frac{13.8}{10}$ $\frac{14.5}{13}$ $\frac{13.9}{14}$ $\frac{10.0}{16}$ $\frac{9.2}{57}$
 $\frac{7.2}{100}$

Sta + π -
960.88 ✓

6 +82 48.0 ✓

0 2.54 950.43 ✓ 12.99 947.89 ✓

7 46.6 ✓

+55 41.3 ✓

0 0.17 937.58 ✓ 13.02 937.41 ✓

8 36.9 ✓

6.50 931.08 ✓

+54 39.0 ✓

+75 18" x 52' C.M. (Skewed)

9 31.1 ✓
~~24.5~~

$\frac{18.5}{100}$ $\frac{13.2}{74}$ $\frac{9.6}{49}$ $\frac{8.9}{22}$ $\frac{13.7}{16}$ $\frac{14.9}{13}$ $\frac{13.1}{9}$ 12.9 $\frac{13.1}{8}$ $\frac{13.9}{10}$ $\frac{14.6}{13}$ $\frac{14.0}{14}$ $\frac{10.1}{16}$ $\frac{9.3}{59}$ $\frac{7.5}{100}$

$\frac{10.0}{100}$ $\frac{5.7}{79}$ $\frac{1.5}{45}$ $\frac{4.9}{19}$ $\frac{5.0}{15}$ $\frac{4.3}{11}$ $\frac{3.9}{10}$ $\frac{3.9}{7}$ 3.8 $\frac{4.3}{7}$ $\frac{5.0}{10}$ $\frac{5.2}{14}$ $\frac{1.6}{18}$ $\frac{1.3}{50}$ $\frac{0.5}{100}$

$\frac{15.6}{100}$ $\frac{12.7}{84}$ $\frac{11.2}{47}$ $\frac{11.7}{16}$ $\frac{9.7}{11}$ $\frac{9.4}{6}$ 9.1 $\frac{9.5}{9}$ $\frac{12.3}{16}$ $\frac{15.0}{40}$ $\frac{14.6}{100}$

$\frac{5.9}{100}$ $\frac{5.5}{78}$ $\frac{6.2}{20}$ $\frac{1.6}{11}$ $\frac{0.8}{8}$ 0.7 $\frac{0.8}{9}$ $\frac{7.2}{22}$ $\frac{8.7}{64}$ $\frac{9.3}{100}$

mail in PP. 30' ht. Sta 8+35

$\frac{10.0}{100}$ $\frac{10.2}{53}$ $\frac{9.5}{22}$ $\frac{5.9}{14}$ $\frac{4.6}{6}$ 4.6 $\frac{4.9}{7}$ $\frac{11.8}{18}$ $\frac{10.5}{60}$ $\frac{9.8}{100}$

+89 End Cuv $\frac{12.4}{16}$
 25.13

+56 End Cuv $\frac{12.11}{22}$
 25.47

$\frac{10.8}{94}$ $\frac{11.4}{60}$ $\frac{11.0}{18}$ $\frac{7.3}{10}$ $\frac{6.4}{5}$ 6.5 $\frac{6.5}{11}$ $\frac{9.8}{19}$ $\frac{8.5}{66}$ $\frac{9.1}{106}$

Sta + π -

937.58 ✓

9+70

30.4 ✓

10

30.5 ✓

+55

31.0 ✓

11

29.7 ✓

+20

29.1 ✓

+22

29.8 ✓

+68

27.9 ✓

+70

27.4 ✓

$$\frac{11.6}{100} \quad \frac{11.1}{71} \quad \frac{11.0}{34} \quad \frac{9.9}{14} \quad \frac{7.7}{7} \quad 7.2 \quad \frac{7.4}{13} \quad \frac{9.0}{19-62} \quad \frac{10.2}{100}$$

$$\frac{10.8}{100} \quad \frac{10.2}{73} \quad \frac{8.5}{32} \quad \frac{7.6}{9} \quad 7.1 \quad \frac{7.0}{12} \quad \frac{7.9}{17-22} \quad \frac{7.6}{24} \quad \frac{7.2}{59} \quad \frac{8.2}{90} \quad \frac{9.5}{100}$$

$$\frac{9.9}{100} \quad \frac{6.8}{51} \quad \frac{4.8}{11} \quad \frac{7.2}{10} \quad \frac{6.9}{5} \quad 6.6 \quad \frac{6.5}{15} \quad \frac{7.4}{16} \quad \frac{7.2}{17} \quad \frac{2.4}{22} \quad \frac{3.2}{49} \quad \frac{5.1}{72} \quad \frac{8.3}{100}$$

Floor Hoj
10.0

$$\frac{10.7}{73} \quad \frac{9.1}{40} \quad \frac{7.5}{9} \quad \frac{8.6}{6-3} \quad 7.9 \quad \frac{7.8}{14} \quad \frac{8.8}{17} \quad \frac{8.6}{20} \quad \frac{5.4}{23} \quad \frac{2.8}{63} \quad \frac{3.5}{100}$$

$$\frac{10.2}{27} \quad \frac{9.2}{6} \quad 8.5 \quad \frac{8.3}{15} \quad \frac{9.3}{18} \quad \frac{9.1}{21} \quad \frac{7.4}{23}$$

$$\frac{10.5}{27} \quad \frac{9.2}{9} \quad \frac{8.2}{7} \quad 7.8 \quad \frac{8.3}{15} \quad \frac{9.4}{18} \quad \frac{9.1}{21} \quad \frac{7.4}{23}$$

$$\frac{13.1}{59} \quad \frac{12.6}{27} \quad \frac{9.6}{4} \quad 9.7 \quad \frac{9.7}{16} \quad \frac{10.4}{17} \quad \frac{10.3}{20} \quad \frac{9.6}{21}$$

$$\frac{11.2}{27} \quad \frac{11.2}{6} \quad 10.2 \quad \frac{9.7}{16} \quad \frac{10.4}{99} \quad \frac{10.3}{mc} \quad \frac{9.6}{20+68} \quad \frac{9.6}{21}$$

Sta + π -

937.58

12 25.2 ✓

+71 24' x 40' C.M. (skewed) 26.0 ✓

13 26.1 ✓

+15.14 End Sunset Lane + Int Valley View Rd 27.0 ✓

B.M. 8.83 928.75 ✓

Ditch

$\frac{13.4}{100}$	$\frac{13.8}{95}$	$\frac{14.0}{71}$	$\frac{14.5}{69-66}$	$\frac{13.5}{62}$	$\frac{12.2}{4}$	12.4	$\frac{10.5}{6}$	$\frac{11.0}{18}$	$\frac{11.9}{20-22}$	$\frac{11.3}{23}$	$\frac{8.6}{60}$	$\frac{4.2}{100}$
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+64 End Colv 14.86
8

$\frac{12.9}{106}$	$\frac{11.9}{52}$	$\frac{12.0}{18}$	$\frac{11.7}{4}$	$\frac{11.6}{5}$
--------------------	-------------------	-------------------	------------------	------------------

+91 End Colv 14.78 FL
18

$\frac{10.9}{8}$	$\frac{11.6}{18}$	$\frac{12.3}{20}$	$\frac{12.7}{23}$	$\frac{11.4}{40}$	$\frac{4.4}{59}$
			$\frac{1.35}{100}$	$\frac{2.1}{84}$	

FL RR Colv 14.38 N. End
FL 2 \rightarrow 923.20 A

$\frac{11.0}{100}$	$\frac{10.9}{72}$	$\frac{10.5}{35}$	$\frac{11.1}{22}$	$\frac{10.7}{16}$	$\frac{10.3}{9}$	11.5	$\frac{11.6}{12}$	$\frac{14.4}{22}$	$\frac{11.5}{30}$	$\frac{2.7}{55}$	$\frac{1.7}{74}$	$\frac{1.0}{100}$
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RR 2

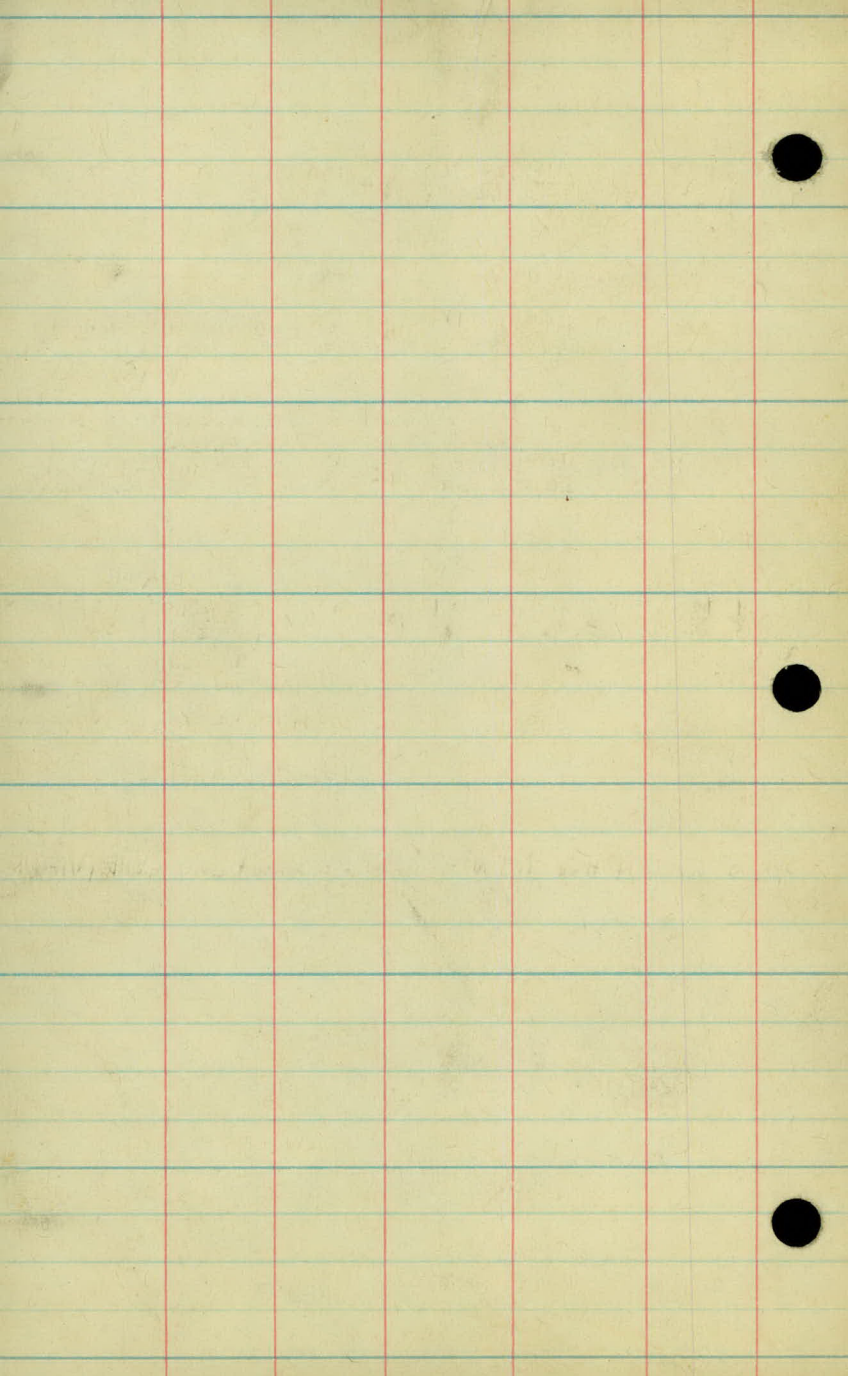
B/A ML

$\frac{10.3}{74}$	$\frac{9.9}{68}$	$\frac{9.4}{62}$	$\frac{10.0}{36}$	$\frac{10.0}{28}$	$\frac{11.0}{18}$	$\frac{11.2}{11}$	$\frac{10.7}{8}$	10.6	$\frac{9.6}{13}$	$\frac{2.9}{29}$	$\frac{2.8}{32}$	$\frac{1.8}{37}$	$\frac{1.3}{56}$	$\frac{1.0}{66}$
									$\frac{5.5}{110}$	$\frac{7.1}{100}$	$\frac{2.5}{87}$	$\frac{2.3}{73}$	$\frac{1.6}{69}$	

14.05 F.L. RR Colv 50 End

923.53

Spk in cut off tree 100' N x 100' W of Sunset Lane x Valley View Rd



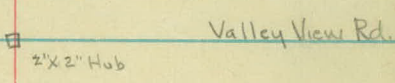
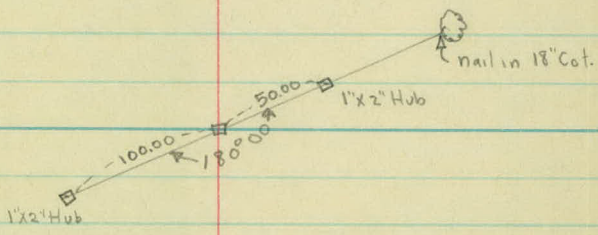
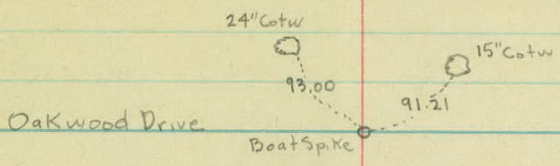
9/26/35
Portell

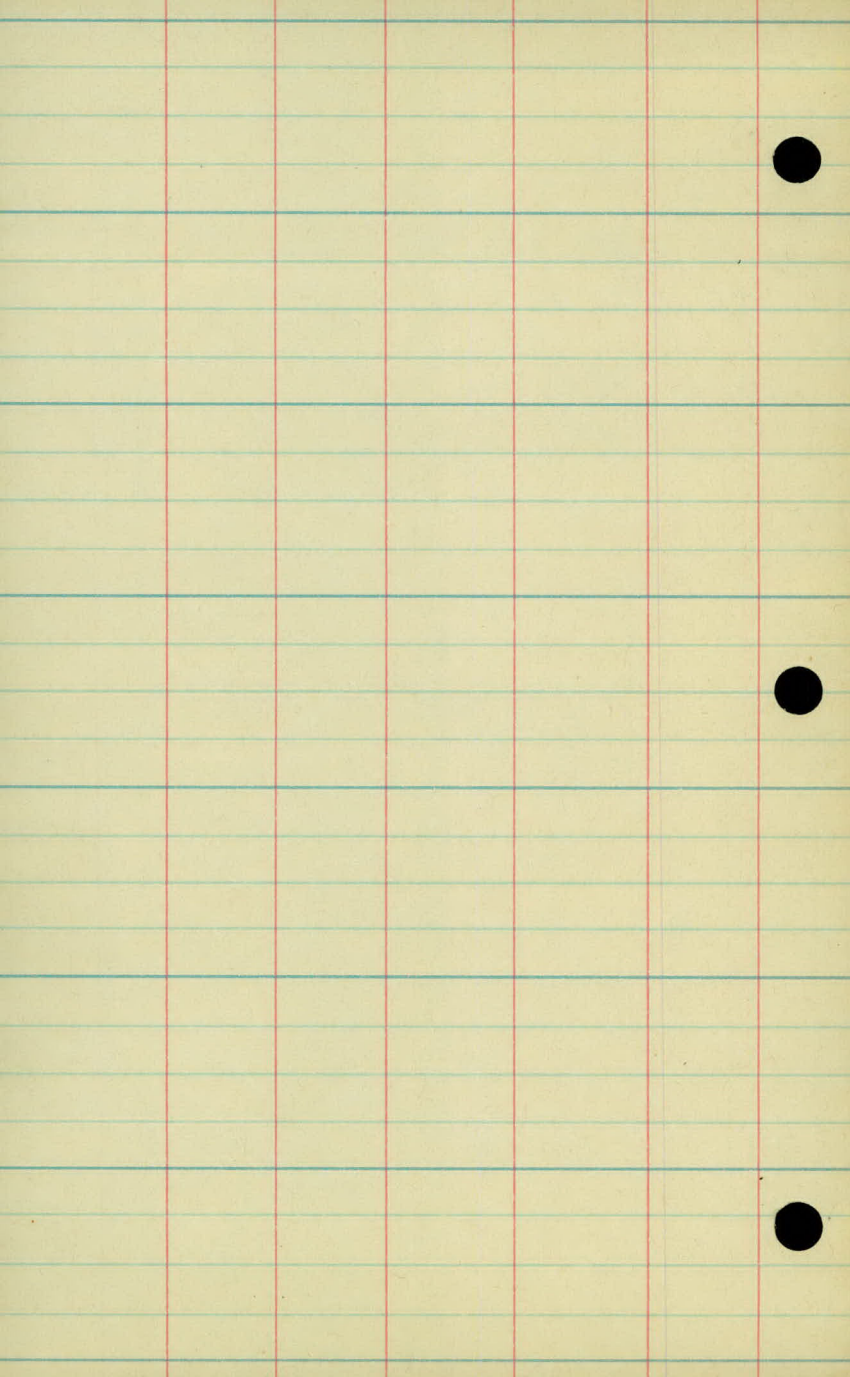
Alignment
Orchard Place
Valley View Road
to
Oakwood Drive

6+58.25

4+00 Po.T.

0+00 Po.T.





9/26/35
Purcell

TOPOGRAPHY
ORCHARD PLACE
IN
MOUNDS VIEW ACRES

4

3

2

1

0+00

+10 End Garden
45-95

+90 Garden
45-95

+22 Flag Pole
11
Rd
31

+44 Cor Barn
33

+82 10' Tr
40
+42 Rd
32

+90 Cor Ho
40
+57 Conc. Ret Wall
40'

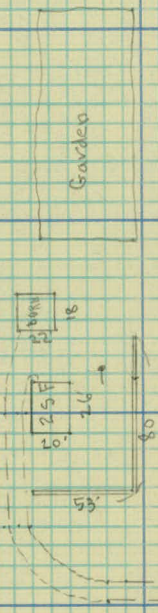
36" Cot. Tr
74

+08 Rd
84

HAY

Ⓢ

PASTURE



PASTURE

+22-30" Cot. Tr
54

+26-4' BotDt.

+37-20" Cot
52

+54 Wagon Tr. 1

7

6

5

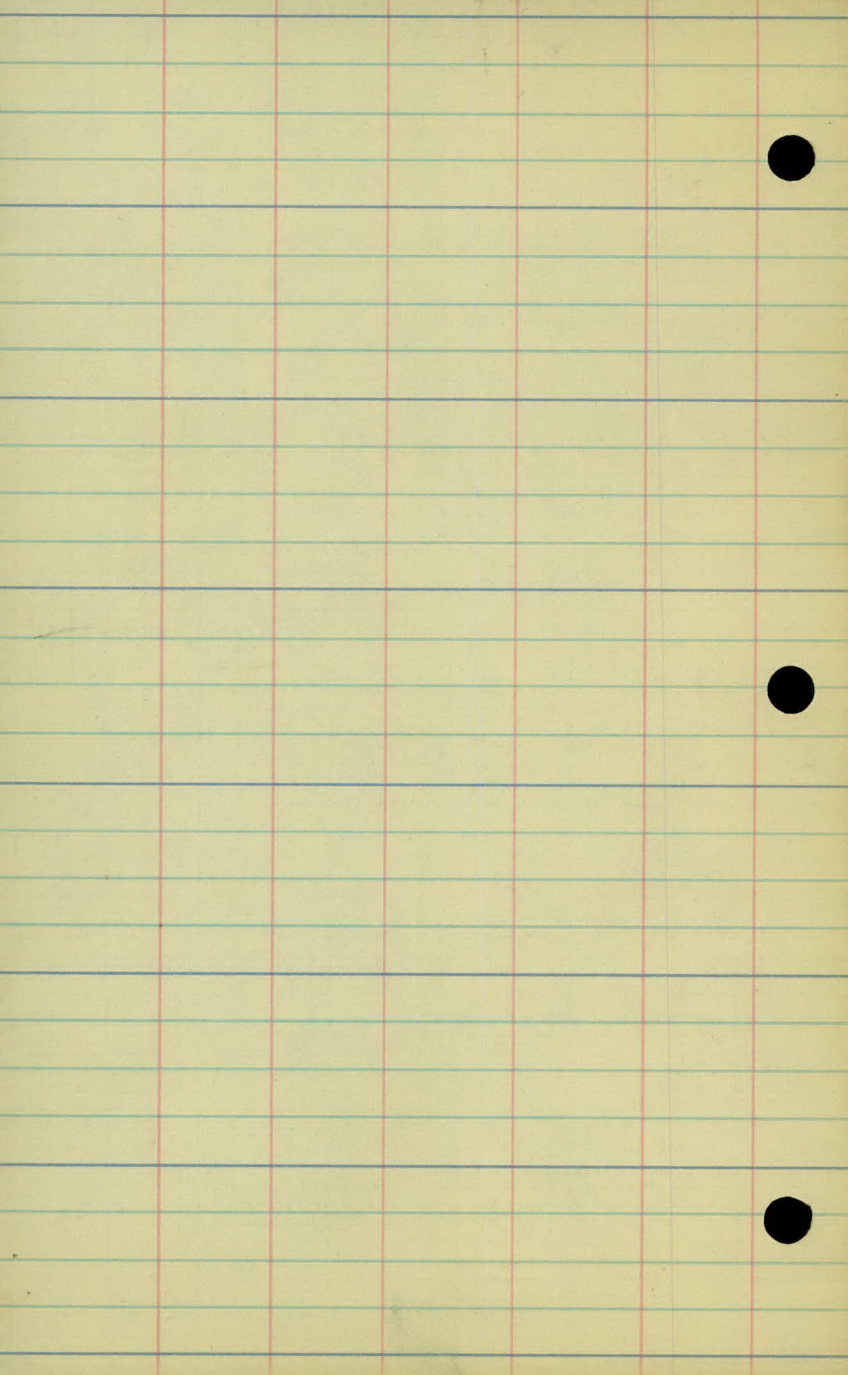
HAY MEADOW



Oakwood Drive

Wagon Trail

HAY MEADOW



9/19/35

Purtell

X-Sections
Orchard Place
in
Mounds View Acres

Sta + π -

B.M. 7.37 943.38 ✓ 936.01

0+00 Jct. Valley View Road 37.3 -

+33 42.2 -

○ 12.88 955.66 ✓ 0.60 942.78 ✓

0+00

+33

50.2 -

+32

52.3 -

+60

51.9 -

S.S. = Same Slope

SW Cor Ret. Wall 100' So. and 35' E. of Orchard Pl + Valley V. Rd

$$\frac{0.3}{16} \quad \frac{3.3}{4} \quad \frac{6.1}{1} \quad 6.1 \quad \frac{9.1}{11} \quad \frac{11.2}{30} \quad \frac{12.4}{54} \quad \frac{14.7}{100}$$

ERdy

$$1.2 \quad \frac{2.9}{9} \quad \frac{4.7}{16} \quad \frac{6.1}{23} \quad \frac{8.6}{31} \quad \frac{9.5}{41} \quad \frac{8.2}{42} \quad \frac{13.8}{100}$$

Top Hill

$$\frac{5.3}{115} \quad \frac{2.3}{71} \quad \frac{5.9}{48} \quad (18.4)$$

$$\frac{5.5}{100} \quad \frac{0.4}{71} \quad \frac{7.0}{37} \quad (13.5)$$

$$\frac{+4.6}{100} \quad \frac{+1.1}{90} \quad \frac{+1.9}{61} \quad \frac{0.5}{39} \quad 5.5 \quad \frac{5.9}{5} \quad \frac{7.3}{11} \quad \frac{8.1}{20} \quad \frac{13.0}{27} \quad \frac{13.4}{34} \quad \frac{12.7}{37-40}$$

Fl. Ho² 10.2 Ho²

$$\frac{+3.8}{100} \quad \frac{+1.8}{61} \quad \frac{0.3}{25} \quad 3.4 \quad \frac{5.4}{14} \quad \frac{11.7}{27} \quad \frac{12.3}{62} \quad \frac{15.1}{89} \quad \frac{15.8}{90} \quad \frac{17.4}{100}$$

Garage

$$\frac{+2.5}{100} \quad \frac{+1.7}{77} \quad \frac{0.6}{38} \quad 3.8 \quad \frac{5.5}{17} \quad \frac{7.4}{32} \quad \text{Gar Fl. } 12.1$$

Sta + π ✓ -

955.66

○ 6.82 956.63 ✓ 5.85 949.81 ✓

1 +90 49.6 -

2 +65 41.5

3 40.8

+50

40.7

A

○ 0.41 943.71 ✓ 13.33 943.30 ✓

2 +65 41.5 -

3 40.8 -

$$\frac{1.5}{100} \quad \frac{5.2}{42} \quad 7.0 \quad \frac{8.3}{20} \quad \frac{11.5}{53} \quad \frac{17.8}{100}$$

$$\frac{4.8}{100} \quad \frac{9.5}{62} \quad (15.1)$$

$$\frac{5.8}{100} \quad \frac{11.2}{51} \quad (15.8)$$

$$\frac{8.1}{100} \quad \frac{11.2}{56} \quad (17.9)$$

$$\frac{13.0}{100} \quad \frac{15.8}{50} \quad (17.4)$$

Top SKK @ Sta 2+50

$$2.2 \quad \frac{4.0}{33} \quad \frac{4.7}{50} \quad \frac{6.8}{100}$$

$$2.9 \quad \frac{4.0}{18} \quad \frac{6.1}{34} \quad \frac{8.9}{100}$$

Sta + π -
 943.71 ✓

3+50

40.7 -

4

39.2 -

+50

34.1 -

0

0.11

937.99 ✓

3.83

939.88 ✓

0

4.01

930.60 ✓

13.40

926.59 ✓

5

25.4 -

+35

19.5 -

0

0.46

926.55 ✓

4.51

926.09 ✓

6

13.8 -

SS = Same Slope

$$3.0 \quad \frac{4.2}{18} \quad \frac{8.1}{53} \quad \frac{14.2}{100}$$

$$4.5 \quad \frac{5.1}{20} \quad \frac{6.8}{38} \quad \frac{14.5}{75} \quad \frac{55}{100}$$

$$\frac{4.5}{100} \quad \frac{6.5}{73} \quad \frac{9.1}{23} \quad 9.6 \quad \frac{9.1}{16} \quad \frac{9.6}{15} \quad \frac{14.5}{51} \quad \frac{55}{100}$$

Top Stk @ Sta 4+00

$$\frac{35}{100} \quad \frac{0.1}{71} \quad \frac{2.2}{49} \quad 5.2 \quad \frac{5.1}{14} \quad \frac{7.2}{24} \quad \frac{11.7}{59} \quad \frac{14.7}{100}$$

$$\frac{7.4}{100} \quad \frac{10.4}{40} \quad 11.1 \quad \frac{12.9}{22} \quad \frac{15.2}{64} \quad \frac{15.7}{100}$$

Top Stk @ Sta 5+00

$$\frac{11.7}{100} \quad \frac{12.0}{84} \quad \frac{12.3}{45} \quad 12.8 \quad \frac{14.2}{41} \quad \frac{14.5}{100}$$

Sta + π ✓ -

926.55

~~923.35~~

~~933.36~~

914.54

○

8.81

12.01

924.55

11.2
21.2

6 + 58.25

7

10.8
20.8

B.M.

12.03

911.32

921.33

$$\frac{11.2}{100} \quad \frac{11.8}{50} \quad 12.2 \quad \frac{12.3}{53} \quad \frac{12.5}{100}$$

$$12.3 \quad \frac{12.6}{49} \quad 12.6 \quad \frac{13.0}{50} \quad \frac{13.1}{100}$$

SpK in 24' Cottonwood 100' NE. of Orchard Pl. and Oakwood Dr.

24

23

22

9/16/35

Alignment
Valley View Road
in
Mound View Acres

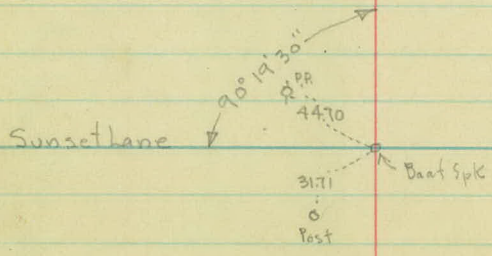
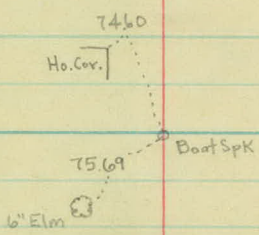
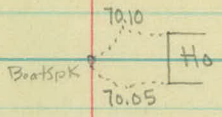
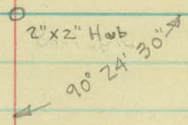
13+10.75 POT.
(Measured)

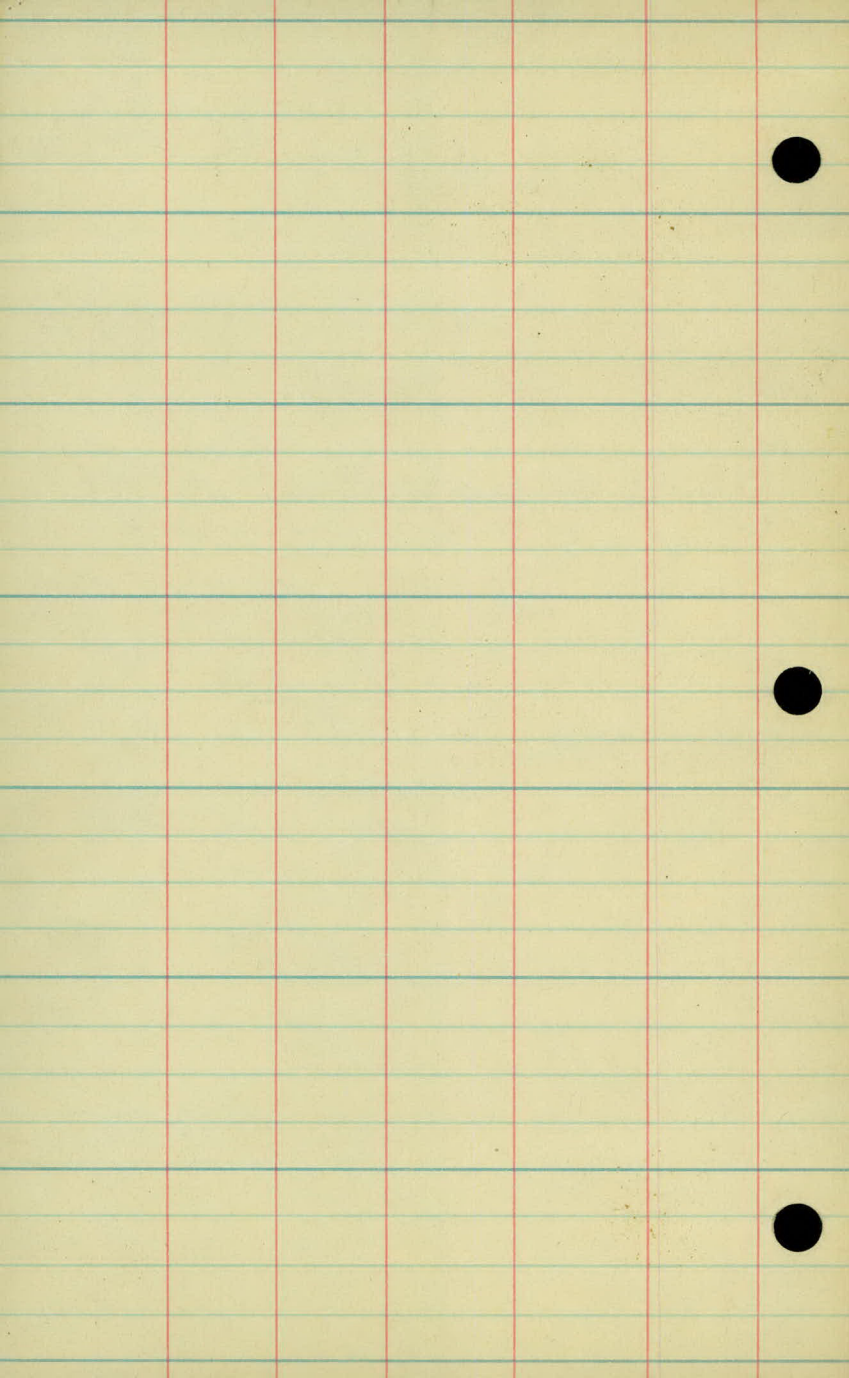
8+48.00 POT.

3+75 POT.

13+15.14 Sunset Lane =
0+00 Valley View Rd

Orchard Place





9/16/35

Purcell

TOPOGRAPHY
VALLEY VIEW ROAD
SUNSET LANE TO ORCHARD PL.
MOUNDSⁱⁿ VIEW ACRES

5 Rd 1-10

4 $\frac{+06 PP}{21}$ Rd 1-11 $\frac{End Colt}{40}$

$\frac{+69 Cor Ho}{72}$
 $+45 Ent$ $\frac{+45 Beg Colt.}{40}$

3 Rd 1-10

$\frac{+86 PP}{21}$ $\frac{+12 Ent - 10 \times 18 CM}{15}$

2 Rd 4-8

$\frac{+59 PP}{23}$

Rd 3-6 Fcs 83 $\frac{\$ Trk}{124}$ $\frac{\$ Trk}{147}$

$\frac{+54 Rd Sn}{+37 PP 34}$
 $\frac{27}{12-0}$

$\frac{+65 Rd}{5-5}$
 $\frac{+40 Rd}{12-0}$

$\frac{+36 Beg RR Fcs}{31}$

0+00

$\frac{+26 Rd}{25-8}$
 $\frac{Rd}{50-27}$

$\frac{\$ Trk}{59}$ $\frac{\$ Trk}{81}$

25th Fr 38

Cult

Cult.

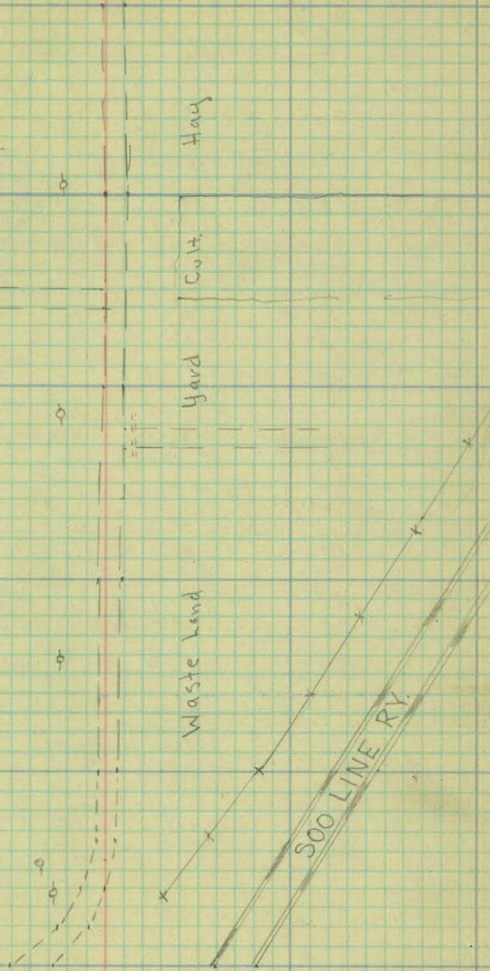
Hay

Cult.

Yard

Waste Land

500 LINE RY.



12

Rd
0-11

+51 PP
21

+53 Beg Garden
18

11

Rd
2-8

+01 Ent

10

Rd
4-6

+99 PP
21

9

Rd
5-6

+46 PP
21

+36 Cov Ho (Being Const)
68
+15 Ent

8

Rd
7-5

7

Rd
12-2

+87 PP
21

+55 FC
33

+55 Rd
10-0

+23 Cov Ho
82

6

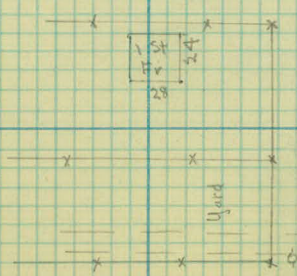
Rd
6-5

+85 FC
33

+40 Ent - 10' x 12' CM
7

+31 PP - Fee Cov
21 33

5



Hay

Yard



Hay

Garden

0

0

0

0

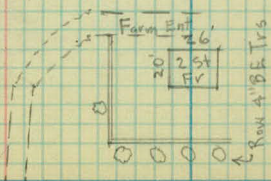
Station 14.00 Lat 14

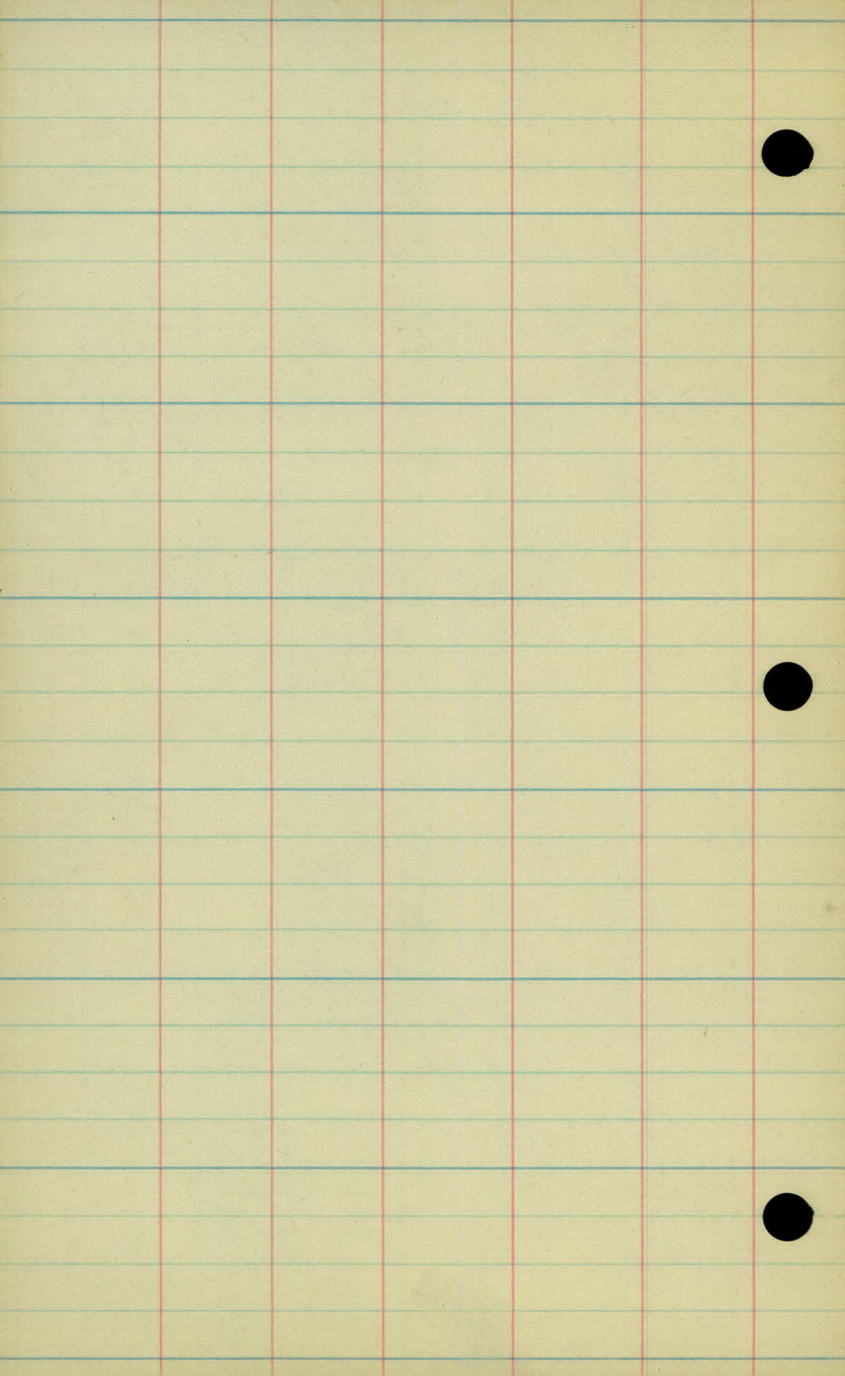
13

<u>+50 Rd</u>	+79 Ent
3-14	
<u>+47 E Cond Ret Wall</u>	
56	+50 Curbs
<u>+20 Ret Wall</u>	88
56	

12

1000





9/14/35

Purtell

X-Sections

Valley View Road

10

Mounds View Acres

Sta + π -

BM. 9.23 937.98 ✓ 928.75 ✓

0+00 Jct. Sunset Lane 27.1 ✓

+50 28.0 ✓

1 28.4 ✓

+50 29.1 ✓

2 8.87 945.87 ✓ 0.98 937.00 ✓

32.5 ✓

+50 37.2 ✓

+75 37.6 ✓

3 37.4 ✓

SpK in Cutoff tree 100' N and 100' W of Sunset Lane + Valley View

		ER		ER				B/R	B/R				
$\frac{12.9}{100}$	$\frac{12.8}{80}$	$\frac{13.1}{55}$	$\frac{11.5}{39}$	$\frac{11.0}{24}$	$\frac{11.6}{13}$	10.9	$\frac{9.7}{15}$	$\frac{3.2}{33}$	$\frac{2.44}{40}$	$\frac{2.06}{64}$	$\frac{1.8}{73}$	$\frac{2.5}{80}$	$\frac{3.2}{100}$

Dt. 2					ER		ER									
$\frac{15.0}{89}$	$\frac{13.7}{87}$	$\frac{12.4}{62}$	$\frac{11.4}{31}$	$\frac{10.6}{15}$	$\frac{10.8}{14}$	$\frac{10.7}{11}$	$\frac{10.0}{9}$	$\frac{9.8}{4}$	100	$\frac{10.2}{3}$	$\frac{11.6}{4}$	$\frac{10.7}{6}$	$\frac{8.3}{10}$	$\frac{4.2}{34}$	$\frac{3.8}{65}$	$\frac{2.6}{75}$
													$\frac{2.2}{100}$	$\frac{2.3}{92}$		

						ER		ER						
$\frac{14.4}{100}$	$\frac{13.9}{80}$	$\frac{13.3}{69}$	$\frac{12.3}{47}$	$\frac{11.0}{11}$	$\frac{10.8}{8}$	$\frac{9.1}{4}$	9.6	$\frac{9.8}{7}$	$\frac{10.4}{10}$	$\frac{10.2}{12}$	$\frac{9.5}{13}$	$\frac{7.0}{42}$	$\frac{3.1}{67}$	$\frac{2.8}{77}$
												$\frac{3.4}{100}$	$\frac{3.6}{81}$	

$\frac{11.9}{100}$	$\frac{10.9}{40}$	$\frac{9.5}{5}$	$\frac{9.2}{4}$	8.9	$\frac{8.8}{7}$	$\frac{8.9}{10}$	$\frac{9.0}{12}$	$\frac{8.9}{14}$	$\frac{8.3}{15}$	$\frac{6.5}{36}$	$\frac{3.1}{61}$	$\frac{1.4}{80}$
											$\frac{1.8}{100}$	

$\frac{16.2}{100}$	$\frac{15.0}{88}$	$\frac{13.3}{28}$	$\frac{12.9}{19}$	$\frac{12.7}{13}$	$\frac{13.3}{4}$	13.4	$\frac{13.1}{10}$	$\frac{12.9}{12}$	$\frac{13.8}{14}$	$\frac{11.8}{17}$	$\frac{9.0}{41}$	$\frac{6.4}{72}$	$\frac{6.0}{100}$
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$\frac{15.5}{100}$	$\frac{10.5}{51}$	$\frac{9.6}{22}$	$\frac{8.7}{3}$	8.7	$\frac{8.4}{12}$	$\frac{9.1}{14.6}$	$\frac{7.2}{18}$	$\frac{4.9}{50}$	$\frac{4.3}{100}$
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$\frac{15.5}{100}$	$\frac{12.2}{58}$	$\frac{9.9}{11}$	$\frac{8.5}{3}$	8.3	$\frac{7.9}{11}$	$\frac{9.0}{13}$	$\frac{8.7}{16}$	$\frac{6.3}{18}$	$\frac{4.8}{30}$	$\frac{4.0}{100}$
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$\frac{15.0}{100}$	$\frac{13.6}{81}$	$\frac{12.0}{28}$	$\frac{10.6}{9}$	$\frac{8.6}{1}$	8.5	$\frac{8.3}{12}$	$\frac{8.9}{13}$	$\frac{8.8}{15}$	$\frac{7.4}{17}$	$\frac{3.8}{69}$	$\frac{2.9}{100}$
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Sta

+

π

-

945.87 ✓

3+50

38.3 ✓

4

40.4 ✓

+30

40.2 ✓

+80

38.0 ✓

5

37.5 ✓

+30

37.4 ✓

6

37.5 ✓

7

37.2 ✓

$$\frac{12.6}{100} \frac{12.2}{85} \frac{10.6}{42} \frac{8.5}{5} 7.6 \frac{7.6}{10} \frac{8.3}{13} \frac{7.8}{23} \frac{6.5}{67} \frac{4.6}{28} \frac{3.6}{100}$$

Floor Hd 7.44 = 38.43

$$\frac{8.5}{74} \frac{9.0}{26} \frac{5.5}{5} 5.5 \frac{5.4}{10} \frac{5.7}{11} \frac{5.4}{13} \frac{3.8}{15} \frac{5.8}{37} \frac{5.6}{65} \frac{1.5}{100}$$

$$\frac{12.5}{100} \frac{11.1}{86} \frac{8.3}{50} \frac{5.7}{25} \frac{4.3}{10} \frac{5.6}{4} 5.7 \frac{5.5}{9} \frac{5.9}{11} \frac{6.0}{13} \frac{4.7}{15} \frac{5.5}{34} \frac{5.1}{48} \frac{3.1}{70} \frac{1.7}{100}$$

$$\frac{12.6}{100} \frac{10.6}{54} \frac{10.2}{28} \frac{9.4}{10} \frac{8.2}{2} 7.9 \frac{8.1}{10} \frac{8.6}{12} \frac{8.7}{14} \frac{6.3}{41} \frac{3.1}{74} \frac{2.8}{100}$$

$$\frac{12.8}{100} \frac{11.5}{74} \frac{10.8}{53} \frac{10.0}{10} \frac{8.5}{2} 8.4 \frac{8.5}{10} \frac{9.6}{16} \frac{8.4}{19} \frac{6.6}{44} \frac{4.2}{77} \frac{3.7}{100}$$

$$\frac{11.9}{100} \frac{11.3}{85} \frac{9.7}{49} \frac{9.4}{19} \frac{8.6}{3} 8.5 \frac{8.6}{11} \frac{9.0}{14} \frac{8.1}{40} \frac{6.7}{77} \frac{5.3}{100}$$

$$\frac{2.6}{87} \frac{2.3}{48} \frac{3.7}{32} \frac{6.8}{10} \frac{8.7}{7} 8.4 \frac{8.5}{5} \frac{9.9}{13} \frac{7.3}{33} \frac{10.7}{70} \frac{6.9}{91} \frac{6.5}{100}$$

$$\frac{3.6}{100} \frac{3.1}{74} \frac{4.8}{36} \frac{7.2}{17} \frac{8.7}{13} \frac{8.2}{11} 8.7 \frac{10.6}{5} \frac{11.7}{38} \frac{10.6}{59} \frac{9.1}{83} \frac{7.2}{100}$$

$$\frac{5.5}{100} \frac{6.4}{59} \frac{8.1}{10} \frac{7.3}{7} \quad 7.2 \quad \frac{7.4}{5} \frac{9.8}{13} \frac{10.2}{42} \frac{8.6}{70} \frac{8.4}{100}$$

6.7

$$\frac{6.1}{100} \frac{3.3}{52} \frac{4.2}{17} \frac{10.1}{10} \frac{10.5}{7} \quad 10.2 \quad \frac{10.4}{6} \frac{10.3}{10} \frac{8.0}{13} \frac{10.0}{40} \frac{9.8}{62} \quad \frac{7.02}{Fl. House} \quad 63$$

$$\frac{2.9}{100} \frac{8.7}{49} \frac{12.7}{10} \frac{12.9}{6} \quad 12.8 \quad \frac{12.8}{7} \frac{13.8}{12} \frac{15.2}{42} \frac{15.5}{100}$$

$$\frac{0.0}{100} \frac{3.3}{51} \frac{5.2}{9} \frac{3.9}{6} \quad 3.8 \quad \frac{4.2}{7} \frac{6.2}{12} \frac{7.1}{70} \frac{7.7}{100}$$

$$\frac{3.0}{100} \frac{3.2}{50} \frac{4.6}{6} \quad 4.6 \quad \frac{4.8}{6} \frac{6.0}{43} \frac{10.9}{100}$$

SW. Car Ret Wall Rt Sta 12+15

$$\frac{4.7}{110} \frac{2.1}{45} \frac{2.2}{8} \frac{3.3}{4} \quad 3.4 \quad \frac{3.8}{9} \frac{2.6}{11} \frac{4.1}{28} \frac{8.3}{68} \frac{10.5}{100}$$

Sta + π -

936.86 ✓

10 + 50

32.2 ✓

11



28.8 ✓

+45

27.3 ✓

12

28.5 ✓

+50

30.6 ✓

13

34.4 ✓

+10.75

37.4 ✓

BM

0.85

936.01 - 936.01 ✓

$$\frac{8.3}{100} \quad \frac{7.9}{92} \quad \frac{5.2}{63} \quad \frac{3.6}{40} \quad \frac{2.4}{8} \quad \frac{4.8}{4} \quad 4.7 \quad \frac{4.6}{8} \quad \frac{4.1}{13} \quad \frac{6.0}{25} \quad \frac{9.8}{66} \quad \frac{11.6}{100}$$

$$\frac{12.6}{100} \quad \frac{11.7}{65} \quad \frac{10.2}{31} \quad \frac{8.9}{7} \quad \frac{8.0}{3} \quad 8.1 \quad \frac{8.4}{8} \quad \frac{10.0}{15} \quad \frac{12.0}{52} \quad \frac{12.9}{100}$$

$$\frac{13.3}{100} \quad \frac{13.2}{76} \quad \frac{12.4}{38} \quad \frac{10.9}{4} \quad \frac{9.7}{2} \quad 9.6 \quad \frac{9.7}{9} \quad \frac{10.5}{14-47} \quad \frac{8.5}{91} \quad \frac{7.7}{100}$$

$$\frac{13.4}{100} \quad \frac{12.2}{46} \quad \frac{11.4}{32} \quad \frac{9.9}{3} \quad 8.4 \quad \frac{8.3}{11} \quad \frac{9.0}{13} \quad \frac{7.7}{41} \quad \frac{10.2}{100}$$

Ret Wall }
Hwy

$$\frac{12.4}{100} \quad \frac{11.4}{66} \quad \frac{9.0}{30} \quad \frac{7.2}{4} \quad 6.3 \quad \frac{5.8}{3} \quad \frac{5.5}{14} \quad \frac{5.8}{21} \quad \frac{3.0}{53} \quad \frac{1.6}{56} \quad \frac{0.30}{57} \quad \frac{+4.9}{75} \quad \frac{+5.1}{87}$$

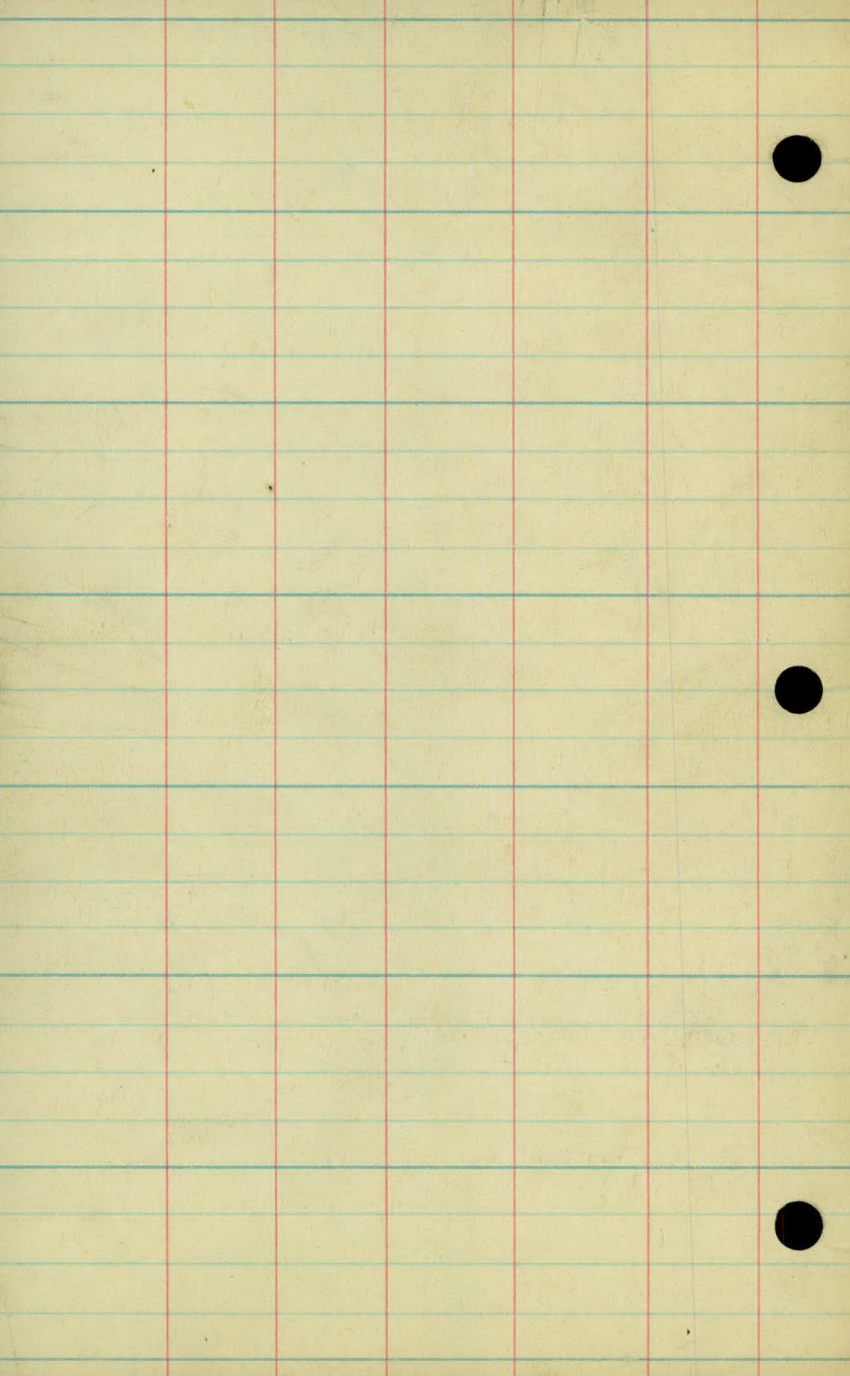
Over H.L. (Hand Level)
used

$$\frac{11.0}{100} \quad \frac{7.8}{46} \quad \frac{4.9}{21} \quad \frac{3.5}{9} \quad 2.5 \quad \frac{1.8}{5} \quad \frac{0.8}{20} \quad \frac{+2.0}{32} \quad \frac{+3.2}{35} \quad \frac{+6.6}{64} \quad \frac{+11.0}{100}$$

Hand Level - over H.L.
13-100

$$\frac{9.5}{100} \quad \frac{8.1}{73} \quad \frac{5.5}{48} \quad \frac{1.6}{28} \quad \frac{+1.3}{13} \quad \frac{+2.9}{4} \quad \frac{+0.5}{2} \quad +0.5 \quad \frac{+1.7}{5-14} \quad \frac{+4.1}{23} \quad \frac{+7.9}{52} \quad \frac{+12.9}{100}$$

SW Cor Ret Wall Rt Sta 12+15



9/19/35

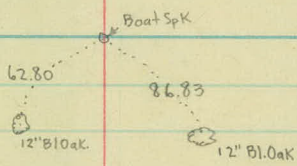
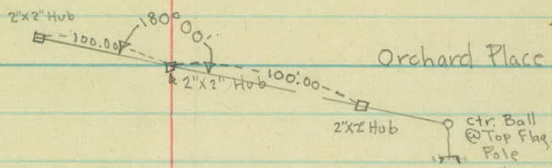
Portell

Alignment
Fairfield Drive
in
Mounds View Acres

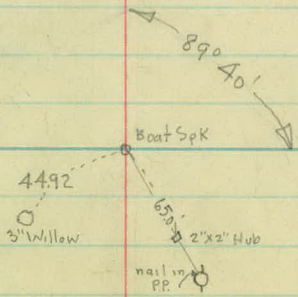
13+09.82 POT.

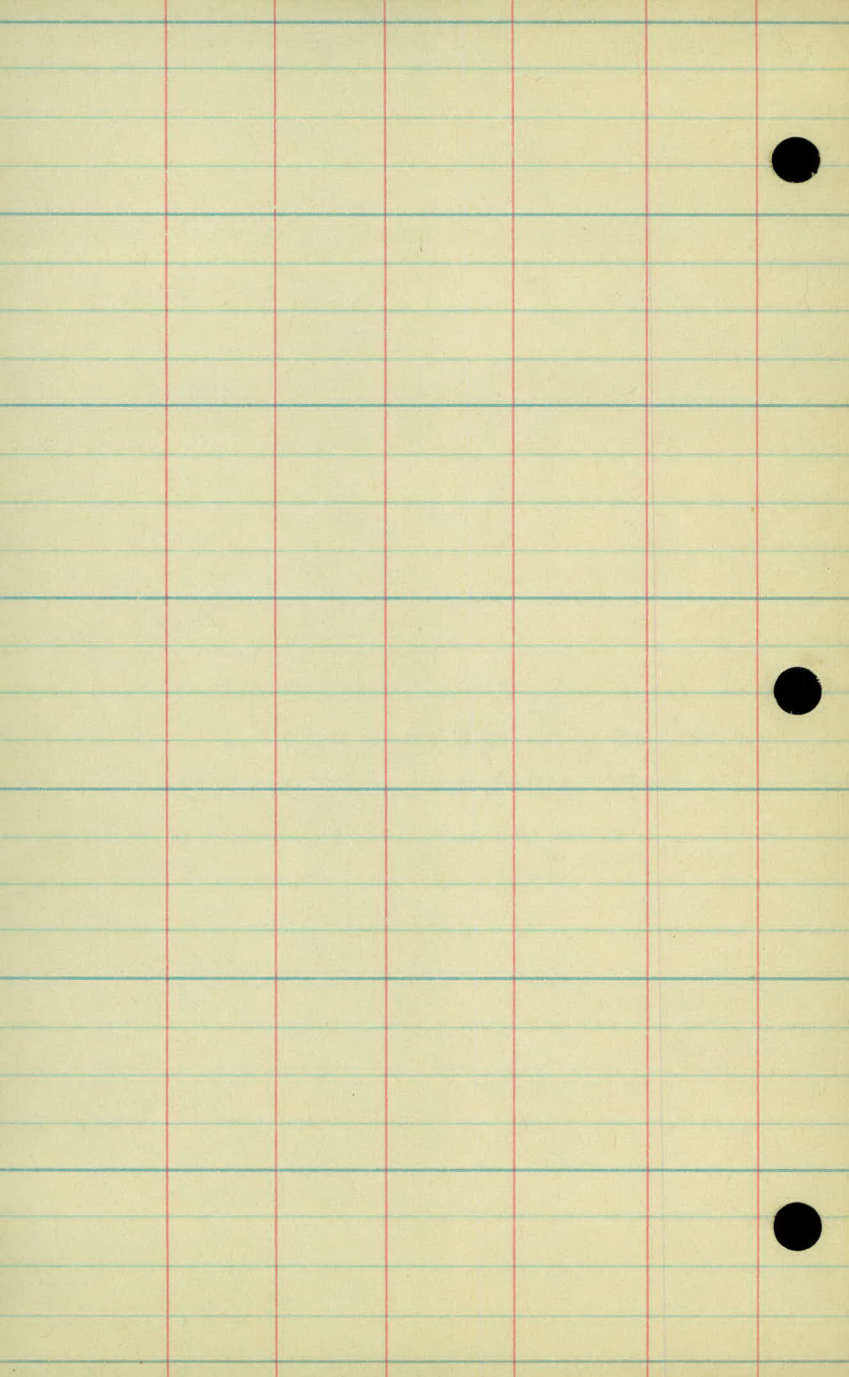
7+55 POT.

6+57.57 Sunset Lane =
0+00 Fairfield Drive



Sunset Lane





9/19/35
Furtell

TOPOG
FAIRFIELD DRIVE
IN
MOUNDS VIEW ACRES

$$\frac{Rd}{15-2}$$

$$\frac{+86-10' \times 24' CM}{19-5}$$

5

$$\frac{Rd}{13-2}$$

$$\frac{+65 Ent-6' \times 20' Steel}{3}$$

4

$$\frac{Rd}{9-3}$$

$$+68 Ent$$

3

$$\frac{Rd}{6-4}$$

$$\frac{+93 PP}{30}$$

$$\frac{+10' \times 24' CM}{15.5-18.5}$$

$$\frac{+48 Cor Garden}{26}$$

2

$$\frac{Rd}{5-5}$$

$$\frac{+48 PP}{30}$$

1

$$\frac{Rd}{5-6}$$

$$\frac{+30 PP}{29}$$

0+00

+08 Shoulder

-06 Shoulder

$$\frac{-12-10' \times 20' CM}{12-8}$$

→ → → → →
Pot Hole (Dry)

Garden

Garden

Garden

→ → → → →
Pot Hole (Dry)

Waste Land

Gravel Top

13

Fcc
6

+29 Ent to Field
3

Fcc
3

12

11

Fcc
6

Trail
8-18

+70.8" BE
61

+66.8" BE
37

+33-12' Cottw. Tr

77

10

Fcc
3

+33 End Gravel Top

+59 FC
4

+33 End Rd + Field Ent No. (Trail)

+33 Ent-12"x14'CM
6

9

Rd
0-12

+85 Cor Ho

65
+41 Fcc

11

8

Rd
6-6

+65 Ent

+56 Cor Ho

+77 FC

+50 FC

+62 Cor Ho

106

20
+62 Ent

26

70

+13 Stp

17

+14 Stp

+02 18' Oak

30

Fcc

Rd
10-2

Fcc

19

+44.8" oak

42

+85 Beg Fcc

31

+93 12' oak

25

+95 Stp

11

+42 Ent 12"x14'CM

21

+37 Cor Ho

68

+89 12' oak

19

+30 10' oak

40

+58-2 oaks

38

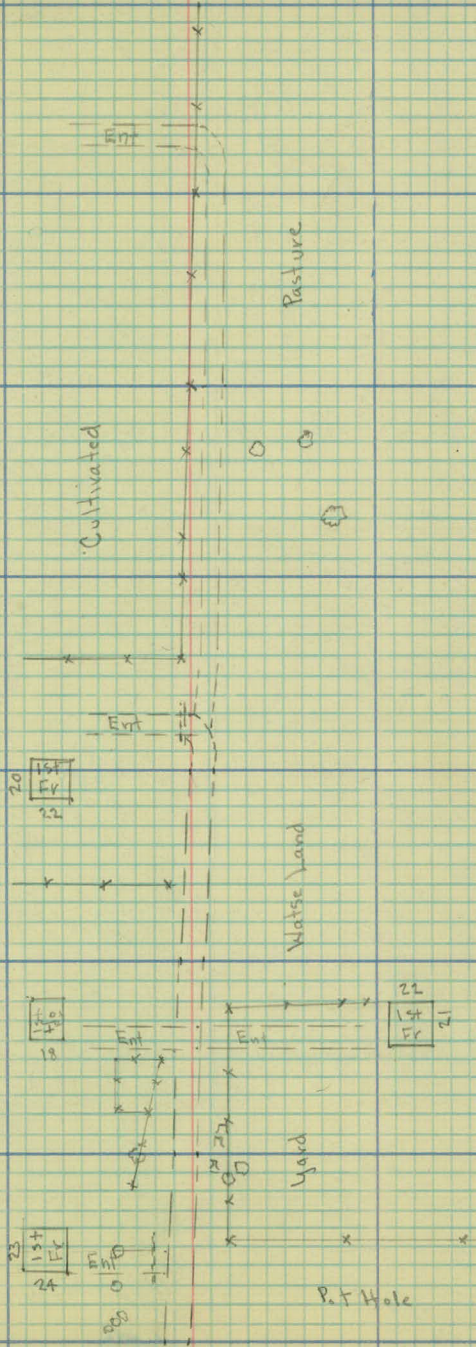
+54 FC

18

+13 3 oak's

41

6



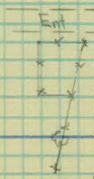
Cultivated

Pasture

Waste land

Yard

P.F. Hole



$$\frac{+43 FC}{34}$$

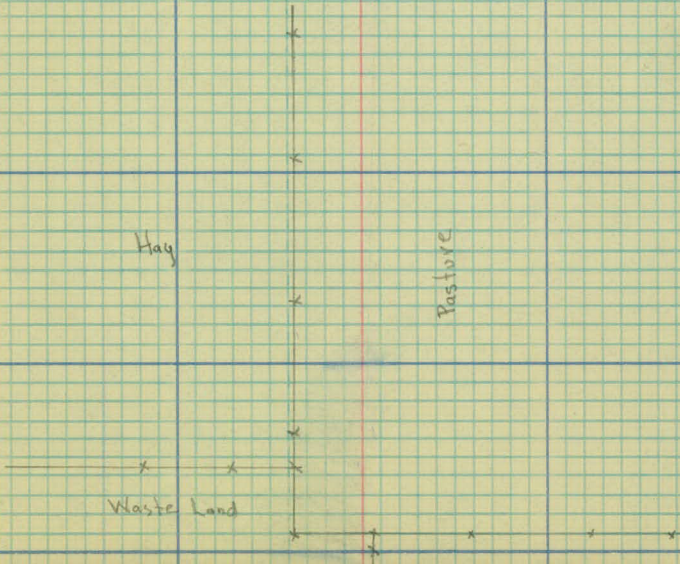
$$\frac{+14 FC}{28}$$

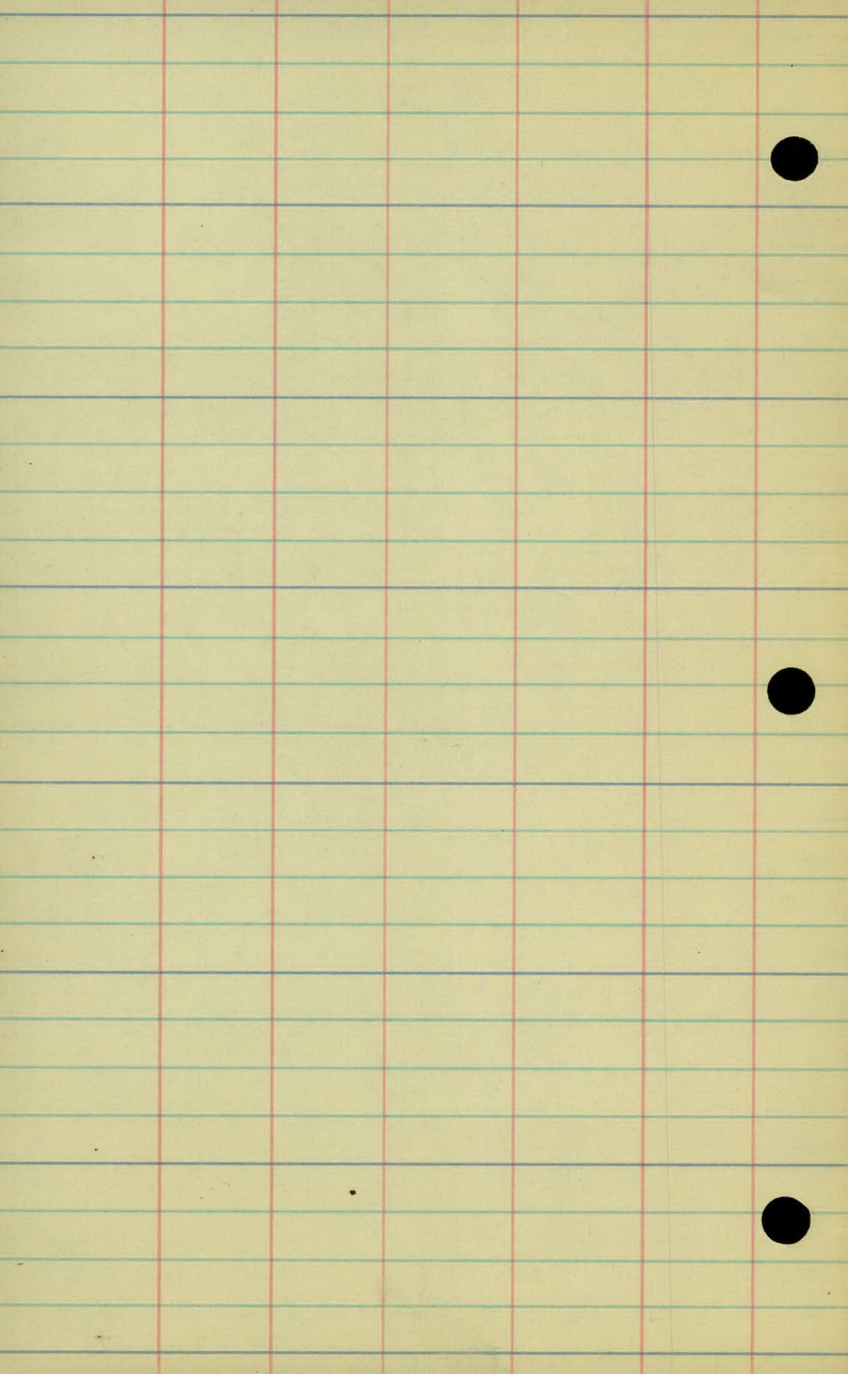
$$\frac{+10 FC}{5}$$

Hay

Pasture

Waste Land





Portell

9/17/35

X- Sections
Fairfield Drive
in
Mounds View Acres

Sta. + π -

B.M. 3.62 958.15 954.53

0+00 E Sunset Lane 49.6 ✓

+11 Shoulder 49.4 ✓

+17 Ditch 49.3 ✓

+21 49.1 ✓

+26 49.0 ✓

+40 48.5 ✓

44.9 ✓

⊙ 0.85 945.48 ✓ 13.52 944.63 ✓

Spk. in PP. 125' So. + 35' E of Janset Lane + Fairfield Drive

$$\frac{7.5}{100} \quad \frac{7.4}{38} \quad 8.5 \quad \frac{10.3}{27} \quad \frac{12.4}{53} \quad \frac{15.2}{83} \quad \frac{17.0}{100}$$

$$\frac{8.0}{100} \quad \frac{7.5}{38} \quad 8.7 \quad \frac{11.2}{38} \quad \frac{13.6}{44} \quad \frac{17.2}{100}$$

$$\frac{9.1}{100} \quad \frac{8.6}{56} \quad \frac{9.1}{25} \quad \frac{8.8}{20} \quad 8.8 \quad \frac{9.4}{8} \quad \frac{10.3}{12} \quad \frac{12.0}{32} \quad \frac{11.5}{62} \quad \frac{16.6}{100}$$

$$\frac{7.5}{100} \quad \frac{7.1}{50-23} \quad \frac{9.0}{15} \quad 9.0 \quad \frac{9.5}{6-24} \quad \frac{6.2}{27} \quad \frac{9.4}{46} \quad \frac{12.5}{70} \quad \frac{13.8}{76} \quad \frac{19.5}{100}$$

$$\frac{3.3}{100} \quad \frac{2.7}{76} \quad \frac{2.4}{37} \quad \frac{6.8}{29} \quad \frac{8.6}{23} \quad \frac{9.2}{13} \quad 9.1 \quad \frac{9.5}{4} \quad \frac{9.3}{23} \quad \frac{5.8}{25} \quad \frac{9.6}{47} \quad \frac{13.0}{70} \quad \frac{19.9}{100}$$

$$\frac{3.8}{105} \quad \frac{1.7}{86} \quad \frac{1.2}{58} \quad \frac{1.6}{26} \quad \frac{8.4}{18} \quad \frac{10.0}{13} \quad \frac{9.8}{8} \quad 9.6 \quad \frac{9.9}{6} \quad \frac{9.5}{9} \quad \frac{9.6}{24} \quad \frac{6.1}{25} \quad \frac{9.2}{44} \quad \frac{12.4}{67} \quad \frac{18.9}{100} \quad \frac{13.8}{78}$$

$$\frac{5.0}{100} \quad \frac{3.5}{87} \quad \frac{4.9}{56} \quad \frac{8.3}{34} \quad \frac{9.4}{16} \quad \frac{13.1}{11} \quad 13.2$$

Sta

+

π

-

945.48 ✓

44.9 ✓

+25

43.0 ✓

+75

38.9 ✓

2

37.7 ✓

+10

10" X 34' CM.

37.4 ✓

+40

36.9 ✓

3

39.6 ✓

0

8.38

950.51 ✓

3.35

942.13 ✓

+60

42.2 ✓

106

$\frac{1.7}{12}$ $\frac{1.3}{15}$ $\frac{5.3}{49}$ $\frac{10.0}{87}$ $\frac{10.4}{100}$

$\frac{+3.9}{100}$ $\frac{+4.7}{73}$ $\frac{6.0}{35}$ $\frac{1.0}{21}$ $\frac{1.9}{20}$ $\frac{2.4}{8}$ 2.5 $\frac{2.7}{8}$ $\frac{7.6}{20}$ $\frac{11.7}{35}$ $\frac{13.3}{42}$ $\frac{14.2}{71}$ $\frac{13.2}{100}$

$\frac{3.7}{100}$ $\frac{3.4}{84}$ $\frac{7.3}{41}$ $\frac{7.8}{31}$ $\frac{8.1}{16}$ $\frac{6.5}{11}$ 6.6 $\frac{7.3}{9}$ $\frac{13.8}{20}$ $\frac{15.0}{47-82}$ $\frac{13.9}{100}$

7.8

$\frac{4.8}{100}$ $\frac{4.3}{82}$ $\frac{7.3}{49}$ $\frac{9.3}{30}$ $\overset{FL-2}{\frac{10.32}{16}}$ $\frac{9.6}{16}$ $\frac{8.2}{12}$ 8.1 $\frac{8.8}{9}$ $\frac{10.7}{14}$ $\overset{FL-2}{\frac{11.95}{19}}$ $\frac{12.4}{29}$ $\frac{13.3}{53}$ $\frac{13.8}{83}$ $\frac{12.7}{100}$

$\frac{7.3}{100}$ $\frac{6.7}{82}$ $\frac{7.7}{60}$ $\frac{8.8}{40}$ $\frac{9.6}{11}$ $\frac{8.7}{9}$ 8.6 $\frac{9.0}{6}$ $\frac{10.1}{13}$ $\frac{10.2}{32}$ $\frac{11.6}{58}$ $\frac{13.2}{67}$ $\frac{13.7}{100}$

$\frac{7.3}{100}$ $\frac{5.4}{64}$ $\frac{5.7}{19}$ $\frac{5.6}{14}$ $\frac{6.4}{10}$ $\frac{5.9}{6}$ 5.9 $\frac{6.1}{10}$ $\frac{4.4}{12}$ $\frac{5.7}{39}$ $\frac{10.1}{77}$ $\frac{13.1}{100}$

$\frac{8.8}{100}$ $\frac{4.3}{70}$ $\frac{3.5}{50}$ $\frac{4.2}{16}$ $\frac{8.1}{11}$ $\frac{8.5}{7}$ 8.3 $\frac{8.4}{9}$ $\frac{6.0}{11}$ $\frac{7.7}{29}$ $\frac{11.2}{64}$ $\frac{14.0}{100}$

Sta + π -

950.51 ✓

4

41.0 ✓

0

4.29

941.45 ✓

13.35

937.16 ✓

+80

36.7 ✓

5

34.7 ✓

+45

31.4 ✓

+86

10" X 24 CM.

6

30.5 ✓

+75

32.2 ✓

7

33.9 ✓

+35

35.9 ✓

$\frac{6.0}{100}$ $\frac{4.0}{93}$ $\frac{3.8}{81}$ $\frac{2.1}{67}$ $\frac{5.5}{17}$ $\frac{9.7}{11}$ $\frac{9.4}{7}$ 9.5 $\frac{9.9}{5}$ $\frac{7.6}{11}$ $\frac{11.0}{42}$ $\frac{13.5}{100}$

$\frac{0.8}{100}$ $\frac{2.1}{77}$ $\frac{2.3}{63}$ $\frac{3.4}{25}$ $\frac{3.1}{18}$ $\frac{5.0}{15}$ $\frac{4.5}{11}$ 4.7 $\frac{5.5}{3}$ $\frac{4.7}{6}$ $\frac{6.3}{31}$ $\frac{10.2}{82}$ $\frac{10.0}{100}$

6.7

$\frac{+1.1}{125}$ $\frac{+1.4}{100}$ $\frac{2.0}{43}$ $\frac{10.4}{20}$ $\frac{9.1}{14}$ $\frac{9.2}{3}$ 10.0 $\frac{12.8}{6}$ $\frac{13.7}{22}$ $\frac{14.2}{64}$ $\frac{14.7}{100}$
FL. $\frac{11.65}{19}$ FL. $\frac{12.47}{5}$

$\frac{1.1}{100}$ $\frac{2.5}{82}$ $\frac{5.8}{58}$ $\frac{10.8}{35}$ $\frac{11.8}{20}$ $\frac{10.4}{15-2}$ 10.9 $\frac{13.5}{5}$ $\frac{14.6}{57}$ $\frac{14.1}{100}$

FL. $\frac{6.7}{100}$ $\frac{8.4}{80}$ $\frac{9.5}{59}$ $\frac{10.8}{17}$ $\frac{9.2}{12}$ 9.2 $\frac{9.4}{2}$ $\frac{11.8}{19}$ $\frac{12.1}{40}$ $\frac{13.7}{89}$ $\frac{14.3}{100}$

7.5

$\frac{4.3}{56}$ $\frac{4.7}{27}$ $\frac{5.2}{22}$ $\frac{6.0}{19}$ $\frac{6.4}{14}$ $\frac{5.4}{9}$ 5.5 $\frac{5.6}{6}$ $\frac{5.9}{14}$ $\frac{4.1}{16}$ $\frac{Fce}{19}$ $\frac{2.8}{37}$ $\frac{4.5}{62}$ $\frac{7.0}{77}$

$\frac{8.1}{84}$

Sta	+	π	-	
		941.45 ✓		
8				36.8 ✓
0	5.61	942.24 ✓	4.82	936.63 ✓
	+42			36.8 ✓
9				35.2 ✓
	+29			34.0 ✓
	+70			29.6 ✓
0	8.71	937.75 ✓	13.20	929.04 ✓
B.M.			8.19	929.56 ✓
10				128.2 ✓
B.M.	7.74	937.81 ✓	7.71	930.04 ✓
				930.07 ✓

Fl. Ho. = +1.1 = El. 42.5

Fl. Ho. 10.1 = El. 31.3

$\frac{1.8}{100}$	$\frac{0.6}{83}$	$\frac{0.3}{68}$	$\frac{0.6}{47}$	$\frac{3.7}{13}$	$\frac{5.2}{9}$	$\frac{4.7}{6}$	4.6	$\frac{4.9}{7}$	$\frac{5.6}{10}$	$\frac{5.3}{13}$	$\frac{6.3}{44}$	$\frac{9.0}{79}$	$\frac{11.1}{100}$
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$\frac{4.9}{100}$	$\frac{6.7}{60}$	$\frac{0.1}{45}$	$\frac{3.8}{10}$	$\frac{5.6}{8}$	5.4	$\frac{6.0}{9}$	$\frac{6.9}{12}$	$\frac{8.8}{33}$	$\frac{11.8}{76}$	$\frac{13.2}{100}$
-------------------	------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------	-------------------	--------------------

Fl. Ho. 3.8
El. 38.4

$\frac{5.5}{64}$	$\frac{4.0}{40}$	$\frac{5.6}{7}$	$\frac{7.3}{5}$	$\frac{7.0}{3}$	7.0	$\frac{7.4}{11}$	$\frac{8.2}{14}$	$\frac{11.1}{43}$	$\frac{12.6}{77}$	$\frac{13.1}{100}$
------------------	------------------	-----------------	-----------------	-----------------	-----	------------------	------------------	-------------------	-------------------	--------------------

8.2

$\frac{12.1}{100}$	$\frac{12.5}{69}$	$\frac{12.7}{30}$	12.6	$\frac{12.8}{12}$	$\frac{14.7}{53}$	$\frac{13.8}{100}$
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Top Stake @ Sta 10+00

SpK in 12" Cot. Wood 77' Rt Sta 10+33

$\frac{7.2}{100}$	$\frac{8.6}{49}$	$\frac{9.1}{3}$	9.6	$\frac{9.4}{12}$	$\frac{10.0}{17}$	$\frac{10.4}{52}$	$\frac{9.4}{94}$	$\frac{8.3}{100}$
-------------------	------------------	-----------------	-----	------------------	-------------------	-------------------	------------------	-------------------

Top Rock 3' Rt. Sta 11+15

Sta + π -

937.81 ✓

11

28.9 ✓

12

28.3 ✓

+22

28.7 ✓

13

26.2 ✓

+0982

26.2 ✓

+50

25.6 ✓

$$\frac{1.7}{100} \quad \frac{3.9}{66} \quad 8.9 \quad \frac{9.5}{5} \quad \frac{10.7}{43} \quad \overset{100 \cancel{d} 7}{\frac{11.8}{45 \cdot 47}} \quad \frac{10.6}{48} \quad \frac{10.0}{72} \quad \frac{9.9}{100}$$

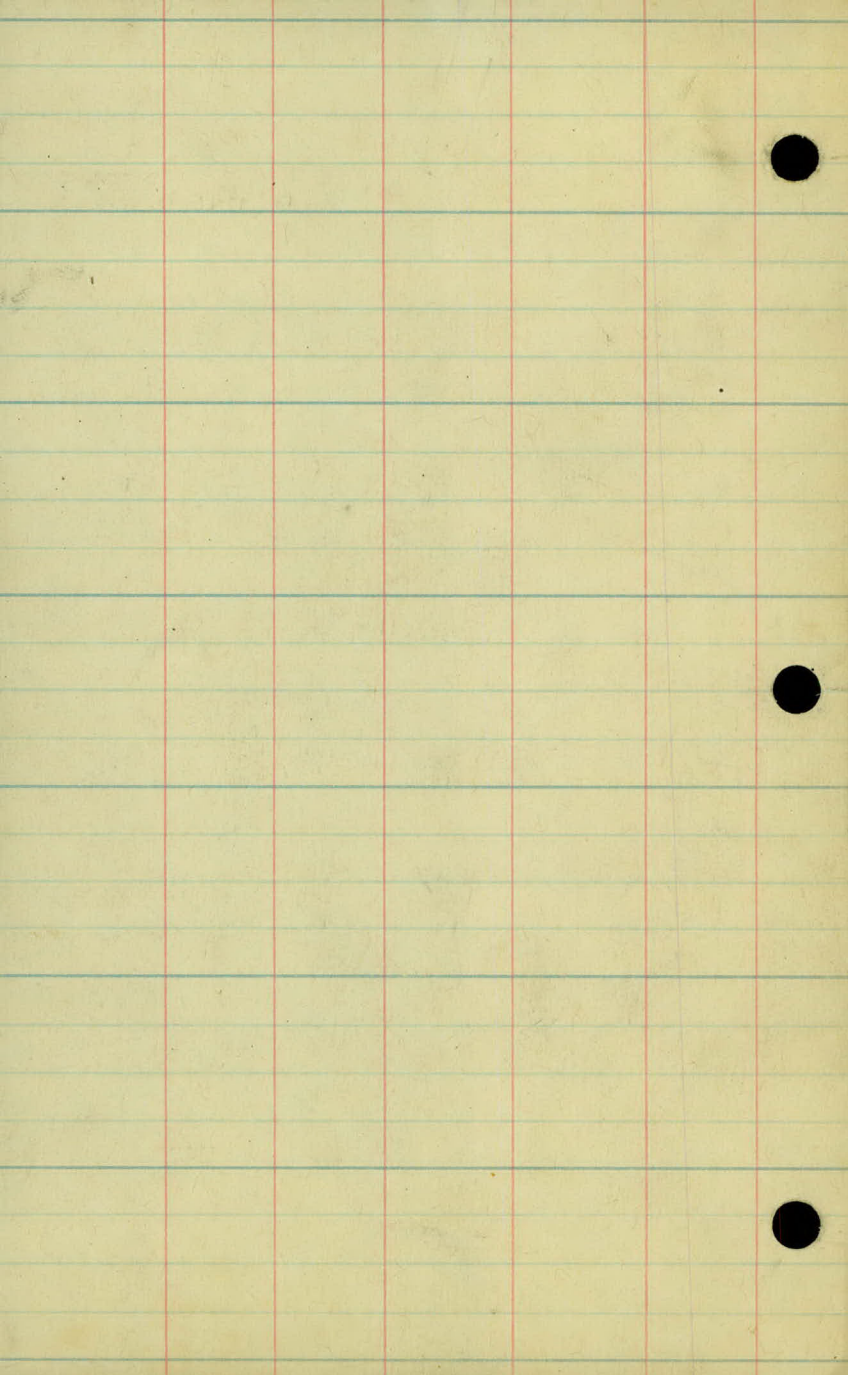
$$\frac{5.2}{100} \quad \frac{8.1}{52} \quad 9.5 \quad \frac{11.2}{58} \quad \frac{11.4}{63} \quad \overset{D \cancel{7}}{\frac{12.4}{64 \cdot 66}} \quad \frac{11.9}{67} \quad \frac{12.6}{100}$$

$$\frac{6.5}{100} \quad \frac{8.6}{51} \quad 9.1 \quad \frac{9.2}{11} \quad \frac{12.1}{64} \quad \overset{D \cancel{7}}{\frac{12.7}{65 \cdot 66}} \quad \frac{12.7}{67 \cdot 100}$$

$$\frac{5.8}{100} \quad \frac{10.6}{38} \quad 11.6 \quad \frac{12.9}{60} \quad \frac{13.5}{100}$$

$$\frac{5.8}{100} \quad \frac{10.3}{40} \quad 11.6 \quad \frac{13.4}{50} \quad \frac{14.5}{100}$$

$$\overset{F \cancel{e} 7}{\frac{10.1}{40}} \quad 12.8 \quad \frac{13.4}{48}$$



1

Oakwood Drive

Slope Stakes

{ H. Bratager

H. Wilke

C. Gottfried

Goldberg

Feist

Sta.	+	-	Grade	Ditch	Grade	Elev
B.M.	6.13	917.46				911.33
1+00				16.5		
2+00				16.7		
2+55				17.1		
B.M.	8.85	920.18				911.33
3+00				17.5		
3+35				17.8		
	$\left. \begin{array}{l} 1.2 \\ 11 \\ 33 \end{array} \right\} \begin{array}{l} \text{Temp Zero} \\ \text{Light Wind} \end{array}$					
4+00				18.3	16.1	
4+40				18.6	16.1	
4+93				19.0		
5+25				19.7		
6+00				19.9		
T.P.		2.98				917.20

Grade
Rod.

Lt.

L

Rt.

Spike in 24" Cottonwood 100' N.E.
of Orchard Place & Oakwood Drive

0.7

$$\begin{array}{r} 4.1 \\ F.3.4 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 5.3 \\ F.4.6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.9 \\ F.5.2 \\ \hline 28.6 \end{array}$$

0.8

$$\begin{array}{r} 3.0 \\ F.7.2 \\ \hline 19.6 \end{array}$$

$$\begin{array}{r} 4.8 \\ F.4.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ F.4.6 \\ \hline 26.8 \end{array}$$

0.4

$$\begin{array}{r} 3.7 \\ F.3.3 \\ \hline \end{array}$$

$$\begin{array}{r} 4.5 \\ F.4.1 \\ \hline 25.3 \end{array}$$

2.7

$$\begin{array}{r} 5.5 \\ F.2.8 \\ \hline \end{array}$$

$$\begin{array}{r} 6.6 \\ F.3.9 \\ \hline 24.7 \end{array}$$

2.4

$$\begin{array}{r} 4.8 \\ F.2.4 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ F.2.9 \\ \hline 31.7 \end{array}$$

Spec. Ditch

1.9
(4.1)

$$\begin{array}{r} 1.4 \\ D.C. 2.7 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 5.3 \\ F.3.4 \\ \hline \end{array}$$

$$\begin{array}{r} 7.1 \\ F.5.2 \\ \hline 28.6 \end{array}$$

1.6
(4.1)

$$\begin{array}{r} 1.9 \text{ Spec. Ditch} \\ D.C. 2.4 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 4.6 \\ F.3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 7.0 \\ F.5.4 \\ \hline 29.2 \end{array}$$

1.2

$$\begin{array}{r} 2.3 \\ F.1.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.3 \\ F.4.1 \\ \hline 25.3 \end{array}$$

0.5

$$\begin{array}{r} 5.1 \\ F.4.6 \\ \hline \end{array}$$

$$\begin{array}{r} 7.6 \\ F.7.1 \\ \hline 34.3 \end{array}$$

F.7.0
30 No
Easement.

0.3

$$\begin{array}{r} 4.7 \\ F.3.9 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ F.6.1 \\ \hline 31.3 \end{array}$$

F.6.1
30

Sta.	+	-	Grade	Ditch Grade
		920.18	0.67	
2+55	13.00	932.51	17.1	15.6
3+00	Begin Spec. Ditch Lt.		17.5	16.0
3+25			17.8	16.0
4+93			19.0	16.3
T.P.	9.49	926.69		917.20
5+25			19.7	16.3
6+00	Check on Bench 926.69 4.50 <hr/> 922.19 O.K.		19.9	16.3
6+75			20.5	19.0
7+00			20.7	19.2
7+60			21.2	
8+00			21.7	
9+00			24.0	
9+45			25.7	24.2
T.P.		0.40		926.29

Grade Rods.
Grade/In. Ditch.

Lt Rt

$$\begin{array}{r}
 5.6 \\
 \text{D.C. } 11.3 \\
 \hline
 44.1
 \end{array}$$

$$\begin{array}{r}
 4.7 \\
 \text{D.C. } 11.8 \\
 \hline
 45.1
 \end{array}$$

Begin Spec. Ditch on Lt.

$$\begin{array}{r}
 7.1 \\
 \text{D.C. } 9.4 \\
 \hline
 41.2
 \end{array}$$

Spec Ditch

$$\begin{array}{r}
 9.4 \\
 \text{D.C. } 6.8 \\
 \hline
 38.7
 \end{array}$$

Spec. Ditch.

$$\begin{array}{r}
 10.2 \\
 \text{D.C. } 0.2 \\
 \hline
 31.0
 \end{array}$$

Spec. Ditch.

$$\begin{array}{r}
 10.3 \\
 \text{D.C. } 0.1 \\
 \hline
 31.0
 \end{array}$$

End of spec. ditch on Lt

$$\begin{array}{r}
 2.7 \\
 \text{D.C. } 5.0 \\
 \hline
 31.5
 \end{array}$$

$$\begin{array}{r}
 5.7 \\
 \text{C. } 0.5 \\
 \hline

 \end{array}$$

$$\begin{array}{r}
 7.7 \\
 \text{D.C. } 0.0 \\
 \hline
 30.3
 \end{array}$$

$$\begin{array}{r}
 2.6 \\
 \text{D.C. } 2.9 \\
 \hline
 31.0
 \end{array}$$

$$\begin{array}{r}
 7.8 \\
 \text{F. } 1.8 \\
 \hline

 \end{array}$$

$$\begin{array}{r}
 8.8 \\
 \text{F. } 2.8 \\
 \hline
 21.4
 \end{array}$$

$$\begin{array}{r}
 10.8 \\
 \text{F. } 5.3 \\
 \hline
 28.9
 \end{array}$$

$$\begin{array}{r}
 11.0 \\
 \text{F. } 5.5 \\
 \hline

 \end{array}$$

$$\begin{array}{r}
 13.7 \\
 \text{F. } 7.7 \\
 \hline
 36.1
 \end{array}$$

$$\begin{array}{r}
 11.1 \\
 \text{F. } 6.1 \\
 \hline
 31.3
 \end{array}$$

$$\begin{array}{r}
 9.2 \\
 \text{F. } 4.2 \\
 \hline

 \end{array}$$

$$\begin{array}{r}
 8.9 \\
 \text{F. } 3.9 \\
 \hline
 24.7
 \end{array}$$

$$\begin{array}{r}
 5.7 \\
 \text{F. } 3.0 \\
 \hline
 22.0
 \end{array}$$

$$\begin{array}{r}
 4.2 \\
 \text{F. } 1.5 \\
 \hline

 \end{array}$$

$$\begin{array}{r}
 2.3 \\
 \text{D.C. } 0.2 \\
 \hline
 31.0
 \end{array}$$

$$\begin{array}{r}
 3.0 \\
 \text{F. } 2.0 \\
 \hline

 \end{array}$$

Sta.	+	-	Grade	Ditch Grade	Elev.
T.P.	13.33	959.67			926.29
9+00			24.0	22.5	
9+45			25.7	24.7	
10+00			27.9	26.4	
11+00			33.4		
11+40			36.0		
12+00			40.7		
T.P.	11.89	950.17	1.34		938.28
12+00			40.7	38.7	
12+55			44.1	42.6	
13+00			47.7	45.7	
T.P.	12.87	962.20	0.84		949.33
12+55			44.1	42.6	
13+00			47.7	45.7	

Grade Rod
Ditch Rod

LT.

E

RT.

17.1

15.4

11.7 13.4

6.2

3.6

10.6

11.5

6.1 7.6

4.5

19.6

15.0 16.5

$$\begin{array}{r} 14.7 \\ F. 3.0 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 9.4 \\ F. 3.2 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 7.0 \\ F. 3.4 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 7.0 \\ O.C. 4.5 \\ \hline 31 \end{array}$$

$$\begin{array}{r} 7.5 \\ O.C. 12.1 \\ \hline 45.7 \end{array}$$

$$\begin{array}{r} 3.0 \\ O.C. 13.5 \\ \hline 48.5 \end{array}$$

$$\begin{array}{r} 14.4 \\ F. 2.7 \\ \hline \end{array}$$

$$\begin{array}{r} 10.9 \\ F. 4.7 \\ \hline \end{array}$$

$$\begin{array}{r} 8.7 \\ F. 5.1 \\ \hline \end{array}$$

$$\begin{array}{r} 2.0 \\ F. 2.6 \\ \hline \end{array}$$

$$\begin{array}{r} 4.7 \\ C. 1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 11.7 \\ C. 3.3 \\ \hline \end{array}$$

$$\begin{array}{r} 11.3 \\ O.C. 5.8 \\ \hline 33.1 \end{array}$$

$$\begin{array}{r} O.C. 5.2 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 11.7 \\ O.C. 3.7 \\ \hline 31 \end{array}$$

$$\begin{array}{r} O.C. 2.6 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 14.7 \\ F. 3.0 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 12.8 \\ F. 6.6 \\ \hline 37.8 \end{array}$$

$$\begin{array}{r} F. 6.6 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 11.5 \\ F. 7.9 \\ \hline 36.7 \end{array}$$

$$\begin{array}{r} F. 7.6 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 5.9 \\ F. 6.5 \\ \hline 37.5 \end{array}$$

$$\begin{array}{r} F. 6.3 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 7.6 \\ O.C. 0.0 \\ \hline 29.6 \end{array}$$

$$\begin{array}{r} 1.8 \\ O.C. 2.7 \\ \hline 31 \end{array}$$

$$\begin{array}{r} O.C. 2.7 \\ \hline 30 \end{array}$$

Sta.	+	-	Grade	Ditch Grade
		962.20		
13+60			51.4	49.9
T.P.	4.54	966.59	0.15	967.05
13+60			51.4	49.9
T.P.				967.05
	+7.20	969.25		
			9.38	959.87
T.P.	8.88	970.93		962.05
14			54.2	
+30			56.7	
15			60.0	
+50			62.1	
16			63.5	
17			64.7	
	5.73	973.80	2.86	968.07
+70			64.4	
18			64.1	

$$\frac{12}{15} = \frac{36}{36}$$

Rod

Grade

Ditch

LT.

R

RT.

5

10.8 17.3

$\frac{5.5}{6.5.0}$

$\frac{9.8}{D.C. 2.5}$
31.0

D.C. 25
30

16.7

$\frac{3.5}{D.C. 13.7}$
47.9

check on Bench Mark

959.91

16.7 18.7

$\frac{6.3}{D.C. 11.9}$
45.3

$\frac{12.1}{6.4.6}$

$\frac{15.5}{D.C. 2.7}$
31

D.C. 27
30

14.7 16.7

$\frac{7.6}{D.C. 8.6}$
38.7

$\frac{10.7}{6.4.5}$

$\frac{11.7}{D.C. 5.0}$
31.5

D.C. 47
30

10.7 12.4

$\frac{3.1}{D.C. 9.3}$
40.1

$\frac{6.9}{6.4.0}$

$\frac{9.3}{D.C. 3.1}$
31

D.C. 28
30

8.8 10.3

$\frac{3.0}{D.C. 7.3}$
36.1

$\frac{5.8}{6.2.0}$

$\frac{8.8}{D.C. 1.5}$
31

D.C. 15
30

7.4 8.9

$\frac{4.1}{D.C. 4.8}$
31.1

$\frac{6.0}{6.1.4}$

$\frac{7.7}{D.C. 1.7}$
31

D.C. 12
30

6.7 7.7

$\frac{4.8}{D.C. 2.9}$
31

$\frac{4.5}{6.1.7}$

$\frac{4.8}{D.C. 2.9}$
31

9.4 10.9

$\frac{5.2}{D.C. 5.7}$
37.9

$\frac{4.8}{6.4.6}$

$\frac{2.4}{D.C. 8.5}$
38.5

9.7 11.7

$\frac{4.6}{D.C. 6.6}$
34.7

$\frac{5.9}{6.3.8}$

$\frac{1.5}{D.C. 9.7}$
40.9

Sta.	+	X	-	Grade.	Elev.
18+50		973.80		63.5	
	2.15	963.74	12.21		961.59
19				62.5	
+75				60.9	
20				60.3	
T.P.	7.68	960.48	10.94		952.80
+65				59.1	
21				58.6	
+45				58.2	
22				57.9	
23				58.2	
B.M.	6.80	966.67	0.61		959.87 ^{OK}
24				58.5	959.91
+70				58.3	
25				57.9	

Grade
Rod.

4.

2

24.

$$\begin{array}{r} 10.3 \\ \boxed{17.8} \end{array}$$

$$\begin{array}{r} 9.2 \\ \text{O.C. } 2.6 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 9.7 \\ \text{C.O. } 6 \\ \hline \end{array}$$

$$\begin{array}{r} 5.0 \\ \text{O.C. } 6.8 \\ \hline 35.1 \end{array}$$

$$\begin{array}{r} 1.2 \\ \boxed{2.7} \end{array}$$

$$\begin{array}{r} 4.0 \\ \text{F. } 2.8 \\ \hline 31.4 \end{array}$$

$$\begin{array}{r} 4.0 \\ \text{F. } 2.8 \\ \hline \end{array}$$

$$\begin{array}{r} 4.6 \\ \text{F. } 3.4 \\ \hline 23.2 \end{array}$$

$$\begin{array}{r} 2.8 \\ \boxed{4.3} \end{array}$$

$$\begin{array}{r} 11.4 \\ \text{F. } 8.6 \\ \hline 38.8 \end{array}$$

$$\begin{array}{r} 7.8 \\ \text{F. } 5.0 \\ \hline \end{array}$$

$$\begin{array}{r} 10.6 \\ \text{F. } 7.8 \\ \hline 36.4 \end{array}$$

$$\begin{array}{r} 3.4 \\ \boxed{4.9} \end{array}$$

$$\begin{array}{r} 11.7 \\ \text{F. } 8.3 \\ \hline 37.9 \end{array}$$

$$\begin{array}{r} 8.7 \\ \text{F. } 5.3 \\ \hline \end{array}$$

$$\begin{array}{r} 10.7 \\ \text{F. } 7.3 \\ \hline 34.9 \end{array}$$

$$\begin{array}{r} 1.4 \\ \boxed{2.9} \end{array}$$

$$\begin{array}{r} 7.3 \\ \text{F. } 5.9 \\ \hline 30.7 \end{array}$$

$$\begin{array}{r} 5.4 \\ \text{F. } 4.0 \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ \text{F. } 5.1 \\ \hline 28.3 \end{array}$$

$$\begin{array}{r} 1.9 \\ \boxed{3.4} \end{array}$$

$$\begin{array}{r} 4.7 \\ \text{F. } 2.8 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 5.0 \\ \text{F. } 3.1 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ \text{F. } 4.3 \\ \hline 25.9 \end{array}$$

$$\begin{array}{r} 2.3 \\ \boxed{3.8} \end{array}$$

$$\begin{array}{r} 6.9 \\ \text{F. } 4.6 \\ \hline 26.8 \end{array}$$

$$\begin{array}{r} 5.1 \\ \text{F. } 2.8 \\ \hline \end{array}$$

$$\begin{array}{r} 6.2 \\ \text{F. } 3.9 \\ \hline 24.7 \end{array}$$

$$\begin{array}{r} 2.6 \\ \boxed{4.1} \end{array}$$

$$\begin{array}{r} 7.0 \\ \text{F. } 4.4 \\ \hline 26.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ \text{F. } 2.4 \\ \hline \end{array}$$

$$\begin{array}{r} 5.6 \\ \text{F. } 3.0 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 2.3 \\ \boxed{3.8} \end{array}$$

$$\begin{array}{r} 4.0 \\ \text{F. } 1.7 \\ \hline 18.1 \end{array}$$

$$\begin{array}{r} 3.3 \\ \text{F. } 1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 0.8 \\ \text{O.C. } 3.0 \\ \hline 31.0 \end{array} \quad \text{O.C. } \frac{3.0}{30}$$

$$\begin{array}{r} 8.2 \\ \boxed{9.7} \end{array}$$

$$\begin{array}{r} 7.3 \\ \text{O.C. } 2.4 \\ \hline 31.0 \end{array}$$

$$\begin{array}{r} 6.3 \\ \text{C. } 1.9 \\ \hline \end{array}$$

$$\begin{array}{r} 4.3 \\ \text{O.C. } 5.4 \\ \hline 32.3 \end{array} \quad \text{O.C. } \frac{5.4}{30}$$

$$\begin{array}{r} 8.4 \\ \boxed{9.9} \end{array}$$

$$\begin{array}{r} 3.8 \\ \text{O.C. } 6.1 \\ \hline 33.7 \end{array}$$

$$\begin{array}{r} 4.8 \\ \text{C. } 3.6 \\ \hline \end{array}$$

$$\begin{array}{r} 4.5 \\ \text{O.C. } 5.4 \\ \hline 32.3 \end{array} \quad \text{O.C. } \frac{5.4}{30}$$

$$\begin{array}{r} 8.8 \\ \boxed{10.3} \end{array}$$

$$\begin{array}{r} 3.3 \\ \text{O.C. } 7.0 \\ \hline 35.5 \end{array}$$

$$\begin{array}{r} 5.5 \\ \text{C. } 3.3 \\ \hline \end{array}$$

$$\begin{array}{r} 4.3 \\ \text{O.C. } 6.0 \\ \hline 33.0 \end{array} \quad \text{O.C. } \frac{6.0}{30}$$

Sta.	+	K	-	Grade.	Elev.
25+80		966.67		56.8	
26				56.4	
B.M.			6.80		959.87 959.91

Grade
Rod.

Lt.

L

Rt.

$$\begin{array}{r} 9.9 \\ \hline 11.4 \end{array}$$

$$\begin{array}{r} 10.6 \\ 06.08 \\ \hline 31 \end{array}$$

$$\begin{array}{r} 9.6 \\ \hline 6.03 \end{array}$$

$$\begin{array}{r} 5.0 \\ 06.64 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 06.64 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 10.3 \\ \hline 11.8 \end{array}$$

$$\begin{array}{r} 11.8 \\ 06.00 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 10.2 \\ \hline 6.01 \end{array}$$

$$\begin{array}{r} 6.4 \\ 06.54 \\ \hline 37.3 \end{array}$$

$$\begin{array}{r} 06.54 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 52 + 69.94 \\ \hline \end{array}$$

$$\begin{array}{r} 158 + 18.58 \\ 105 + 48.64 \\ \hline \end{array}$$

$$\begin{array}{r} 26 + 35.60 \\ \hline \end{array}$$

$$\begin{array}{r} 158 + 18.58 \\ 131 + 82.98 \\ \hline \end{array}$$

$$\begin{array}{r} 26 + 34.34 \\ \hline \end{array}$$

$$\begin{array}{r} 105 + 48.64 \\ 131 + 82.98 \\ \hline \end{array}$$

$$\begin{array}{r} 52 + 69.94 \\ 26 + 35.60 \\ \hline \end{array}$$

$$26 + 34.34$$

11/19/36

Slope Stakes
Orchard Place

P>M. 13.74 949.75 936.01

0 6.93 955.29 13.9 948.36

0 38.2 37.3

0 13.61 957.95 11.03 944.26

+33 40.3 42.2

42.1 50.2

+32 43.5 52.3

+60 43.6 51.9

+90 43.4 49.6

42.8

0 2.23 947.74 12.44 945.51

+65 40.9 41.5

39.6 40.8

+50 37.5 40.7

34.9 39.2

14.4
 10.7
 11.3
 13.1
 26.2
 21
 10.6
 5.6
 11.2
 23.5
 32.7

2.14
 6.8
 9.3
 R.6
 21.5
 40.1
 9.1
 5.5
 11.0
 21.5
 32.5

11.9
 3.0
 13.8
 4.8
 9.6
 21.5
 31.1
 7.4
 6.9
 13.8
 21.5
 35.3

31' Min 3:1 FS
 13'Sh 2:1 BS
 4' Wid Dt.
 1.5' Deep
 3.7
 4.6
 9.2
 21.5

215 Base
 5.1
 11.4
 22.8
 21.5
 49.3
 0.2
 13.7
 2
 27.4
 21.5
 48.9
 14
 1.2
 2
 22.4
 21.5
 53.9
 15.1
 2
 20.2
 21.5
 51.7
 11
 15.4
 30.8
 21.5
 52.3
 1.0
 14.9
 2
 29.8
 21.5
 51.3

S.W. Cor Ret. Wall Cor Orchard Pl. + Valley V. Road

9.5
 11.0
 15.0
 16.5

DC.14
 5.1
 44.3

H.1.9498
 F23
 11.8

12.4
 13.9
 16.0
 14.5

DC.154
 1.1
 52.3

H.1.9553
 C7.2
 5.2

14.4
 15.9

DC.149
 6.0
 51.3

C8.7
 5.7

14.3
 15.8

DC.131
 2.7
 47.7

C8.1
 6.2

DC.6.0
 9.8
 33

14.6
 16.1

DC.9.9
 6.8
 40.1

C6.2
 8.9
 0

DC.56
 10.6
 32.7

6.8
 8.3

DC.146
 3.7
 31.0

C0.5
 6.3

DC.1.00
 8.3
 31.0

8.1
 9.6

DC.55
 4.1
 32.5

C1.2
 6.9

DC.00
 9.6
 31.0

10.2
 11.7

DC.73
 4.4
 36.1

C3.2
 7.0

DC.2.2
 9.5
 31.0

12.8
 14.3

DC.6.9
 7.4
 35.3

C4.3
 8.5

DC.3.2
 10.1
 31.0

47.74

4 + 50

32.0

34.1

0

1.10

935.74

13.10

934.64

5

1.9

28.7

25.4

0

1.93

925.47

12.20

923.54

+35

26.2

19.5

16.5

6

22.2

13.8

0

5.78

920.46

10.79

914.68

+58

19.4

11.2

B.M.

9.14

911.32

911.32

10.2
6.9
3.3
20.7
7.2
8.1
3
24.3
12.0

5.1
5.8
3
16.4
1.8

10.4
7.1
3
21.3
1.3

6.7
2.4
9.1
3
27.3
13
40.3
18
42.1

8.4 9.0

12.8
4.4
8.8

13.0
6.0
18.0
13.0

15.7
17.2

DL4.3
12.9
31.0

C2.1
13.6

DL1.9
15.3
31.0

12.7
9.4
28.1
1.3

7.0
8.5

DL0.0
8.5
31.0

F3.2
10.2

F6.0
13.0
31.0

TD #1

0.7

DL5.8
5.1
29.4

F6.7
6.0

F9.7
9.0
42.1

3.3
4.8

F6.9
10.2
33.7

F8.4
11.7

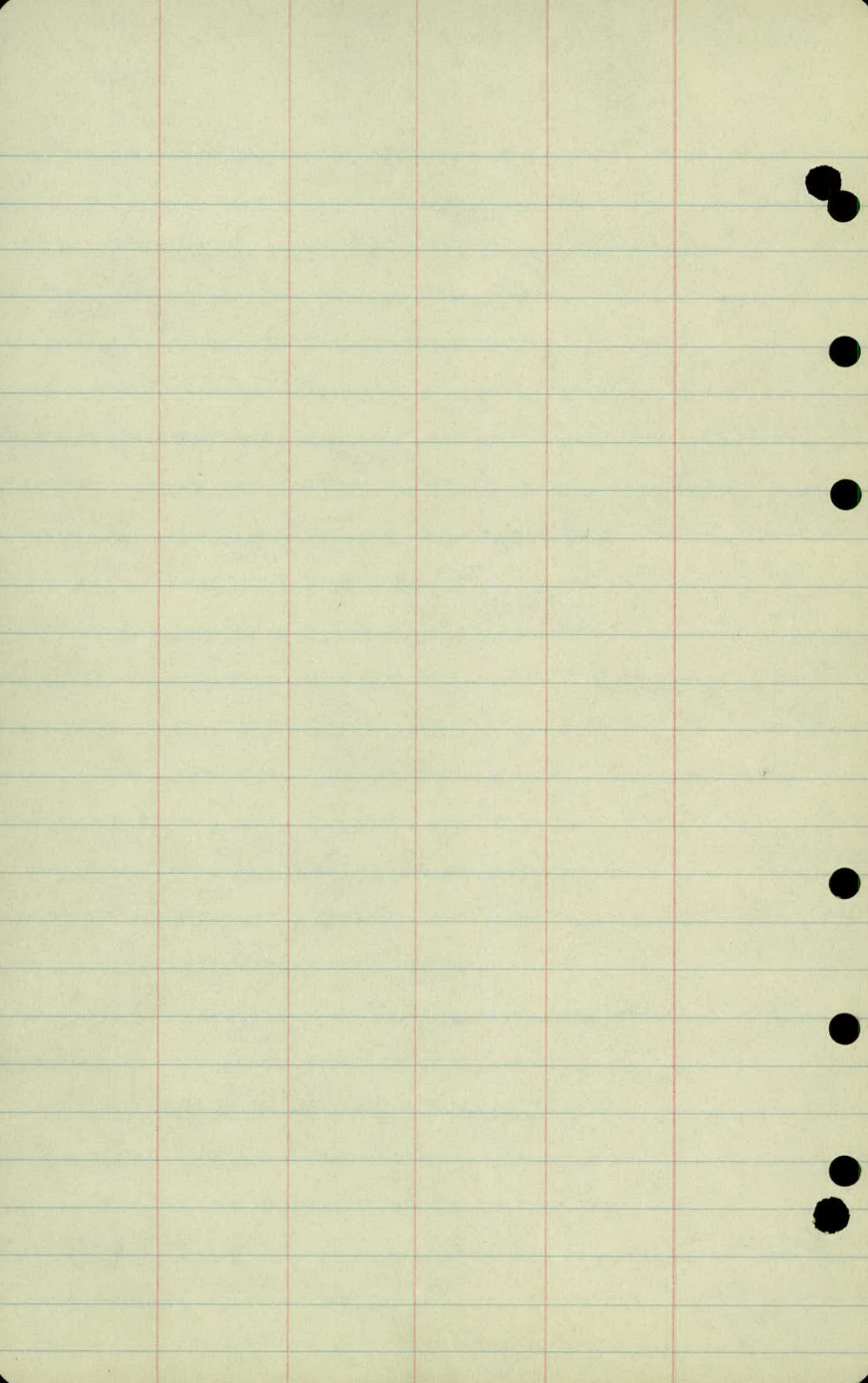
F9.4
12.7
41.2

1.1
2.6

F8.2
9.3

F8.1
9.2
37.3

Spk. in 24" Coll. 100' NE Orchard Place & Oakwood Drive



11.6

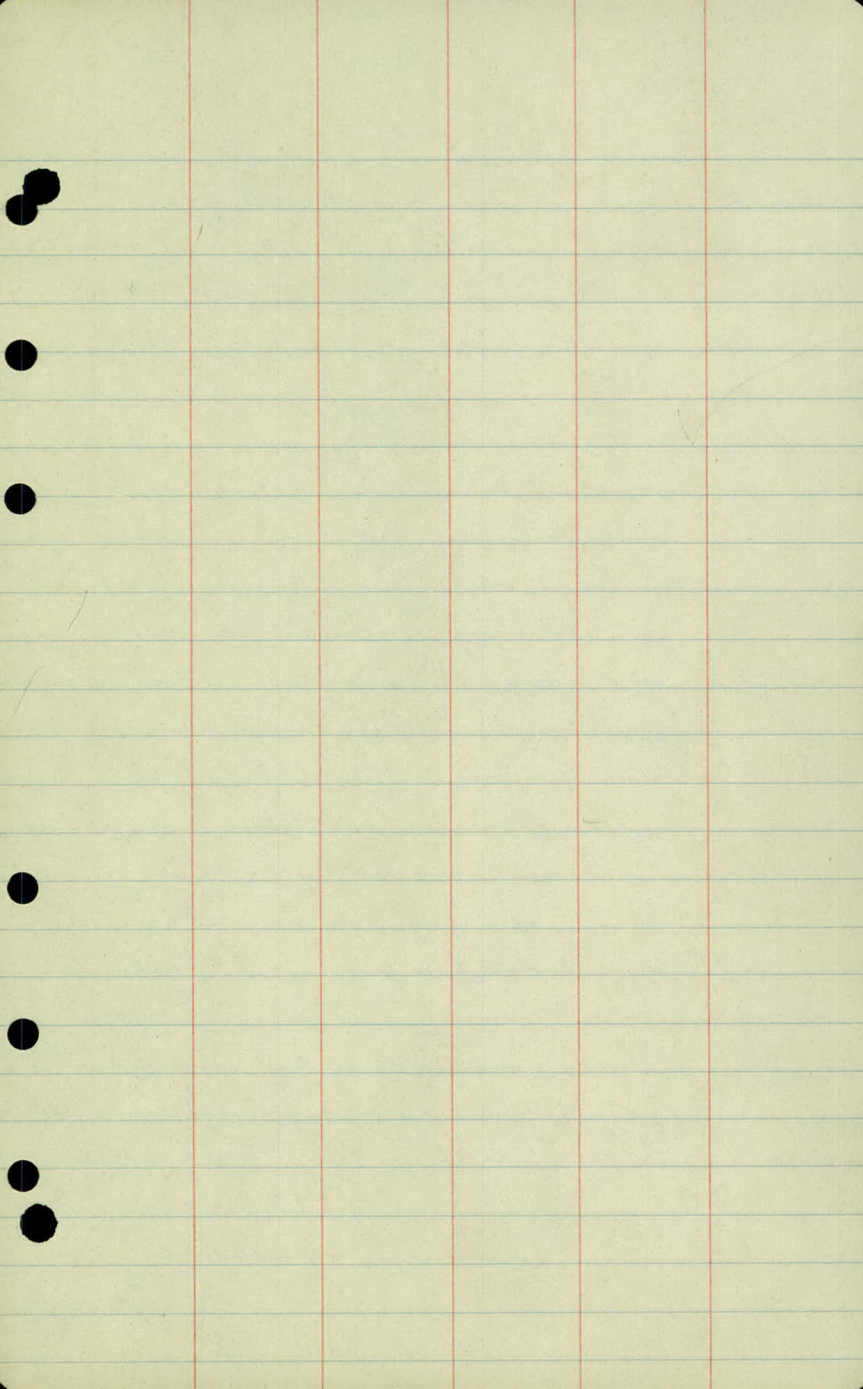
11/19/32

2

Levels

Orchard Place

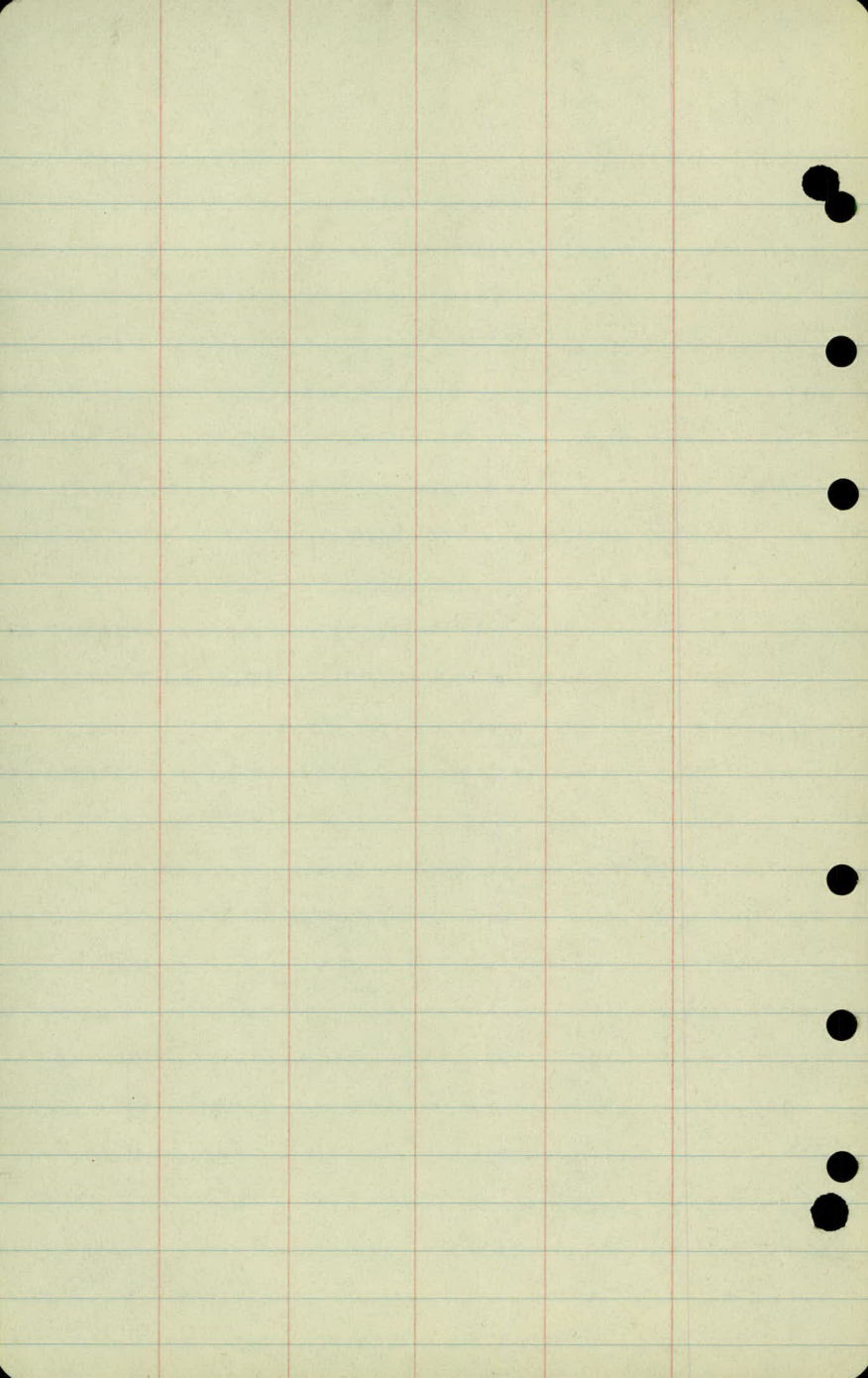
B.M.	13.74	949.75		936.01
0	6.81	955.17	1.39	948.36
0				
1	5.1			50.1
+32	3.0			52.2
+60	3.3			51.9
+90			5.6	49.6
2			6.6	48.6
+50			12.7	42.5
+65			13.7	41.5
0	0.68	943.07	12.78	942.39
3	2.2			40.9
+50	2.3			40.8
4	3.9			39.2

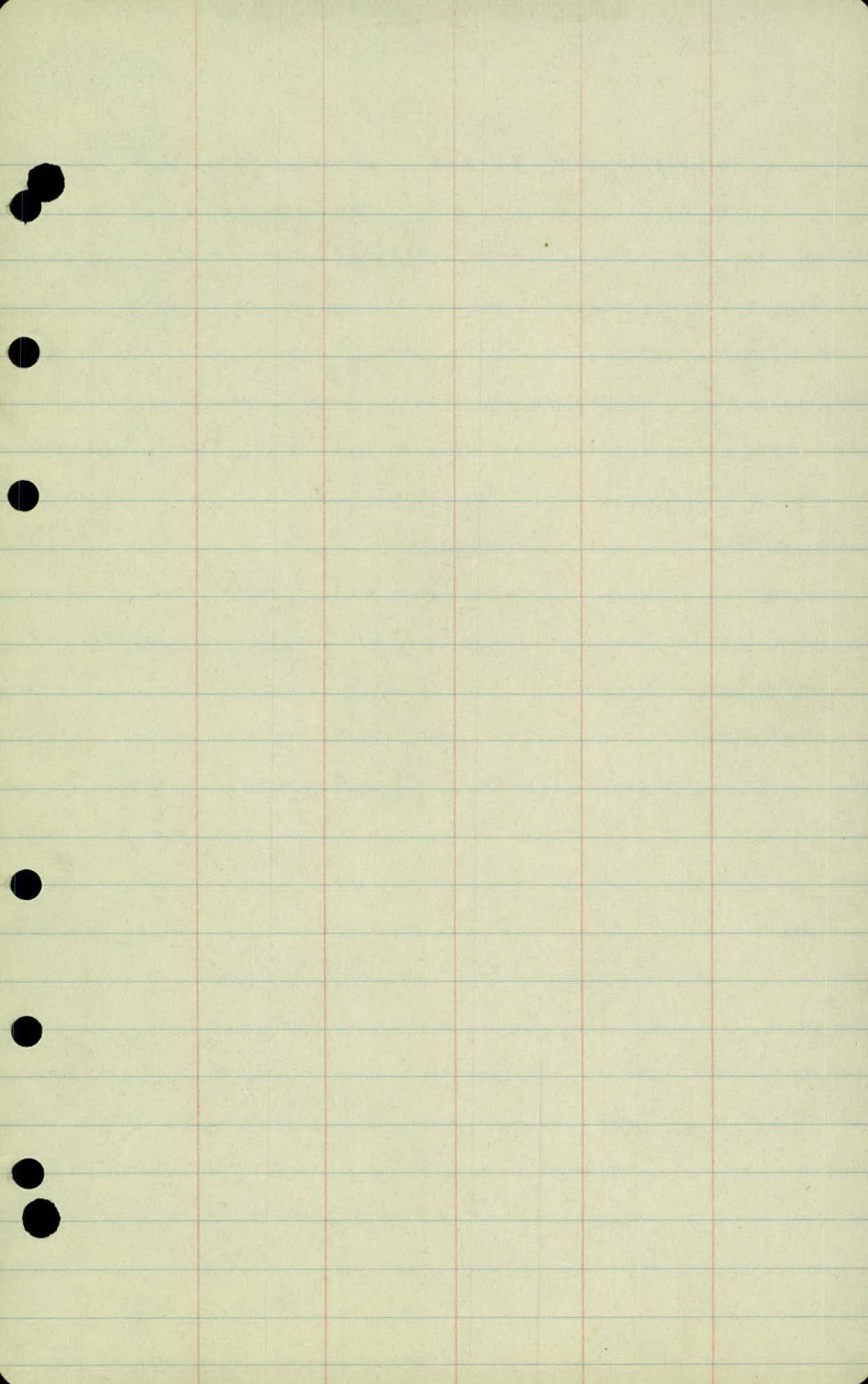


4 + 50			9.0	34.1	
0	0.93	932.49	11.51		931.56
5			7.1		
+35	12.		12.9		
0	1.77	921.76	12.50		919.99
6			7.94	13.9	
+58			10.7	11.1	
B.M.			10.40		911.36

Sta. 1 + 80 Rock 50' N.

Spk. in 24" Cott. 100' NE Orchard Place + Oakwood Drive





Fairchild Drive

5.1
33.3
4.4

B.M. 11.71 941.28 929.56

6 + 75 34.7 32.2

7 34.6 33.9

+35 34.5 35.9

8 34.3 36.8

+42 34.0 36.8

9 33.3 35.2

+29 32.8 34.0

+70 32.1 29.6

0 31.6 28.2

B.M. 929.56

1 29.8 28.9

12 28.0 28.3

2.8
2

57
11.4
21.5
32.9

10.4
3.8
3.3
11.4

12.1
5.5
3
16.5

13th Top

21.5 base
31' Min sec 2:18.5
3:1.15

13.4
21.5
34.9

10

13

5.5
11

12.73
14.6
24.9
39.1

10/29/96

15.0
21.5
36.5

7.5

5.8
2
17.6
21.6
39.1
9.8
2
19.0
21.5
41.1

6.6
8.1

F3.8
10.4
24.4

F2.5
9.1

F5.5
12.1
27.5

6.7
8.2

PC.00
8.2
30.0

F6.6
7.3

PC.1.5
6.7
30.0

12.7
3.5
3

6.8
8.3

OC.37
4.6
30.0

C1.5
5.3

PC.8.5
2.8
32.5

10.5

7.0
8.5

OC.7.5
1.2
35.1

C2.6
4.4

PC.2.9
5.6
30.0

11.6
2.4
3
7.2

7.3
8.8

PC.7.8
+1.0
46.1

C2.9
4.4

PC.1.4
7.4
30.0

13.4
3.7
3
11.1

8.0
9.3

OC.5.7
3.8
37.9

C2.0
6.0

OC.0.7
8.8
30.0

12.5
2.6
3
5.6

8.5
10.0

OC.3.1
6.9
30.0

C1.1
7.4

PC.0.3
9.7
30.0

13.4
2.4
3
8.7

9.2
10.7

F2.4
11.6
20.2

F2.5
11.7

F3.5
12.7
23.5

9.7
11.2

+ F2.8
12.5
21.4

F3.4
13.1

F3.7
13.4
24.1

Spk in 12" Cottonwood 77th RT Sta 10+33

10.5
12.0

PC.7.9
10.1
30.0

F1.8
12.3

F2.9
13.4
21.7

13.3
14.8

PC.2.9
12.4
30.0

C0.4
12.9

OC.0.9
13.9
30.0

12 + 22

27.6

28.7

13

26.2

26.2