

Book-10, Dr. 11-A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

GRAMSIE RD.

From Victoria St. To 1/2 mi. W. of Rice

Road Acc't. No. M18

Date Filed. 3-21-35

File 11

Feb. -35

-1-

— Gramsie —

Road

Ext.

0400 Spike in E of Victoria St.

E

Feb. 25-35

511009/44
STAINMAN
Bell

-2-

Tel. Pole

27°

Tel. Pole

13972

E of Victoria ST.

82°35'

94°08'

100'

100'

200'

200'

82°00'

93°17'

145760
092560

A of Co. Ref. F

21.91 POST

1320.40

iron

1320.40

MONT. Tipped

Ties O.K.

15' oak

22

61.5

12" Stump

Center 2/6
Section

20" oak

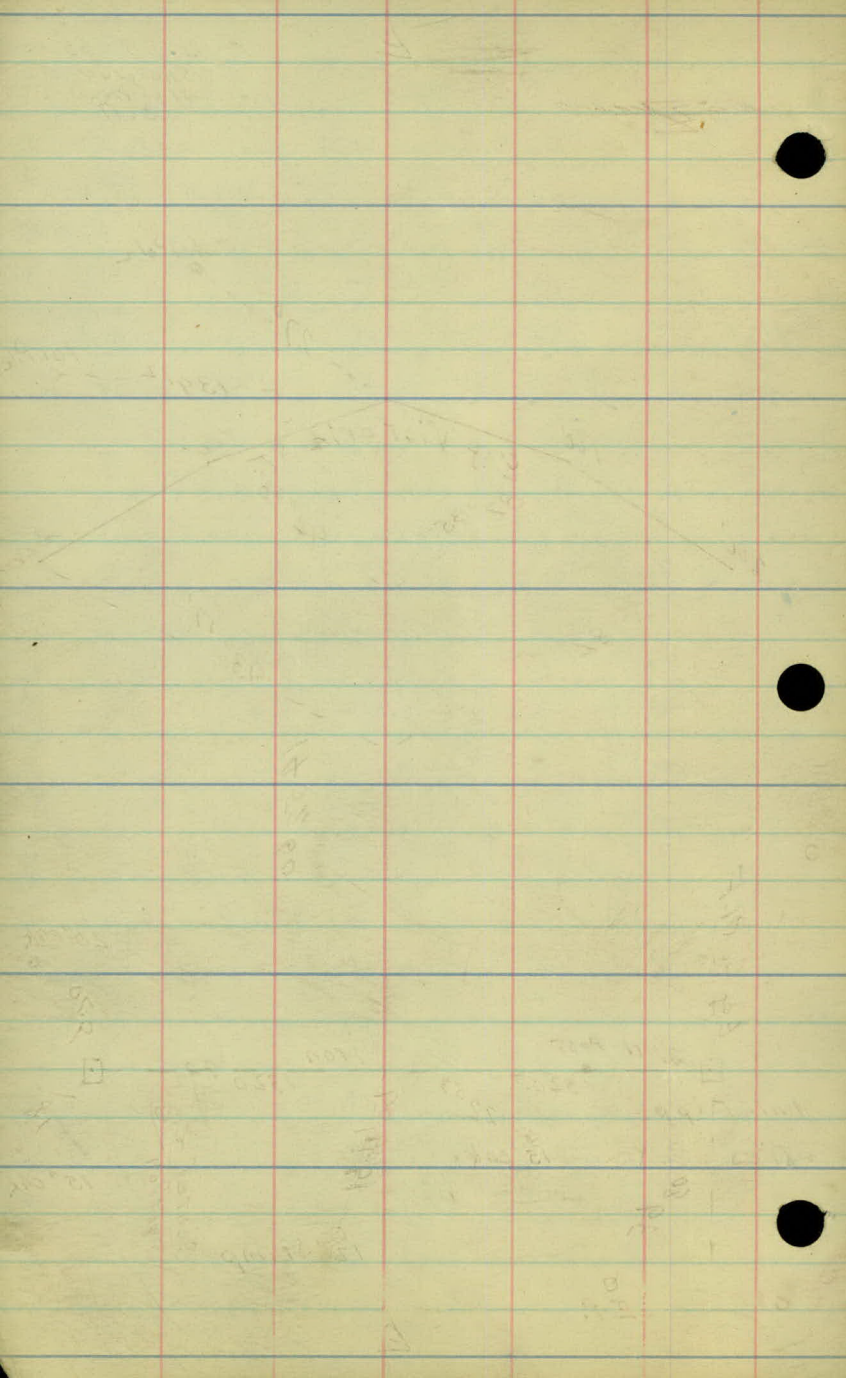
9.70

15" oak

39.60

E.P.

E



- 3 -

Feb 16' at 28

E of Rice St.

P.I. $37+25.75$ $\Delta 0^{\circ}2'$ Right.

P.O.T. $35+29^{\circ}$

P.O.T. $16+57.90$

P.I. $11+84.75$ $\Delta 13'$ Right.

P.O.T. $6+95^{10}$

Hole in Pavement

18" oak

13

70 02

0 2 18 17

Hub.

63 03

Nail

12" oak

12 23

Nail

18 90

13 18

Cor. F. Post. 77

iron

4" Stamp

21

18

12

23

F.P.

F.P.

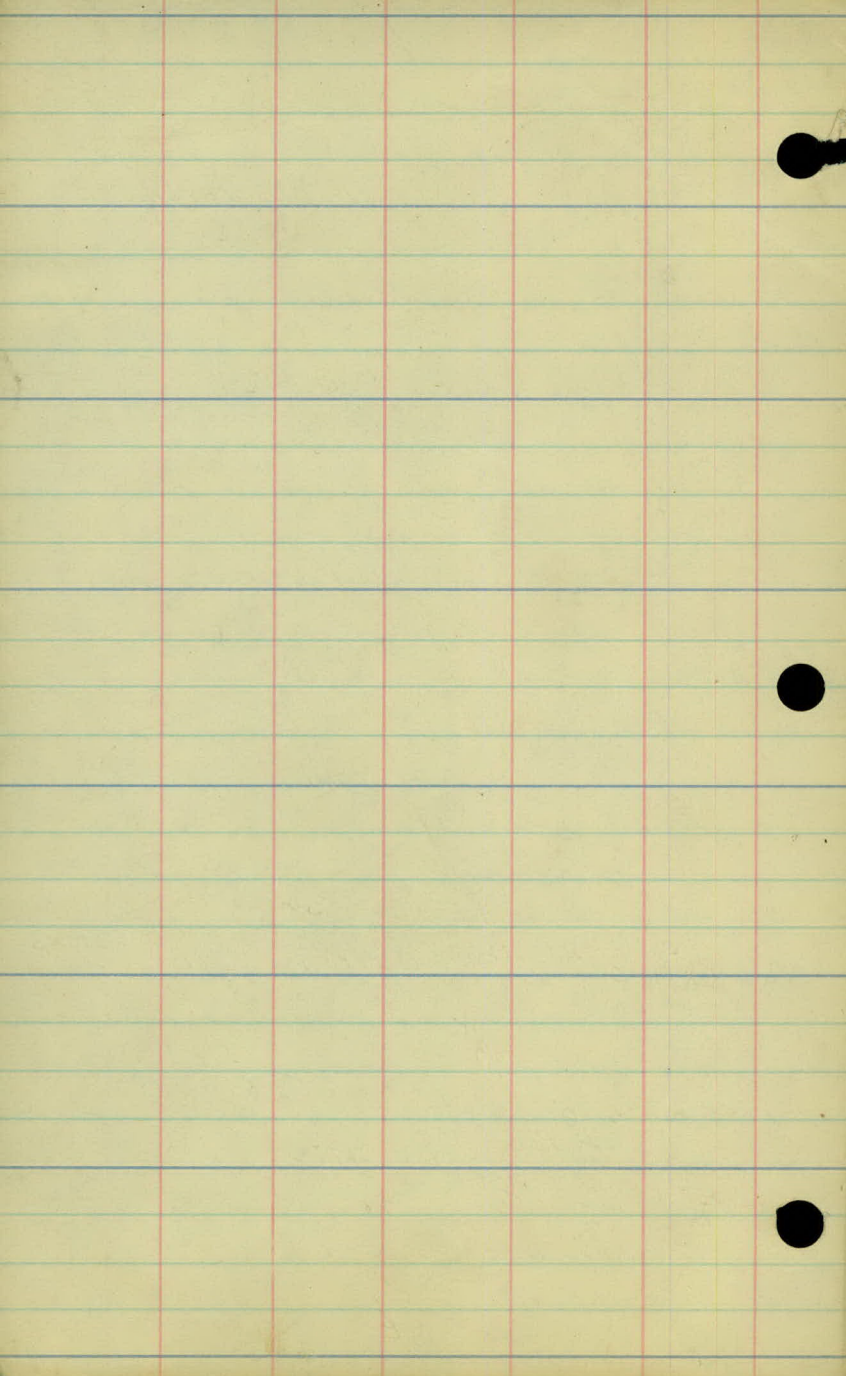
F. Post

2620

80

Spike

52



Feb 27-35

-1-

C

Levels

- Gramsie -

Road.

Profile

+ H.1 - E/V

B.M. 211 982.97 ✓ 980.86 ✓

0+00

80.7

+15

80.0

+25

80.8

1+00

79.5

+50

77.0

2+0

77.4

+50

76.3

3+0

73.3

+50

72.5

4+0

71.0

+50

71.5

5+00

72.0

spike in tel. Pole 140' Right of
STG. 0+30 on Victoria St. East Side

2³

3⁰

2²

3⁵

6⁰

5⁶

6⁷

9⁷

973.50

$\frac{9.5}{100}$

10⁵

69.2

$\frac{13.8}{100}$

12⁰

11⁵

11⁰

+ H.1 - EIV

982.97

+50

971.9

0⁰⁷ 972⁷⁷ ✓

T.P.

10²⁷ 972⁷⁰ ✓

6+00

69.3

+50

66.6

7+00

63.7

1⁶⁷ 962³¹ ✓

T.P.

12¹³ 960⁶⁴ ✓

+50

53.4

0¹⁰ 948⁶⁹ ✓

T.P.

13⁷² 948⁵⁹ ✓

8+00

40.7

+50

37.9

9+00

36.2

0⁶⁵ 937⁷⁹ ✓

T.P.

11⁵⁵ 937¹⁴ ✓

+50

30.7

L

R

R -3-

11⁰

3⁵

6²

9¹

6⁷

8⁰

10⁸

12⁵

7¹

+ H.I. - E.I.V.
937.79

10+00

925.4

2⁷⁸

927²⁹ ✓

T.P.

13²⁸

924.⁵¹ ✓

B.M.

923.⁴³

386

923⁴³

+50

20.0

11+00

12.9

0⁰⁰

914⁹¹ ✓

T.P.

12³⁸

914⁹¹ ✓

+50

05.5

12+00

99.1

0¹⁰

901⁵⁷ ✓

T.P.

13⁴⁴

901⁴⁷ ✓

+50

94.4

13+00

96.4

+50

01.6

10⁹⁶

912¹⁴ ✓

T.P.

0³⁹

901¹⁸ ✓

14+00

06.2

B.M.

907²²

493

907²¹

-L-

2

-R-

-9-

12⁴

7³

14⁴

9⁴

15⁸

887.3

$\frac{14.3}{50}$

7²

5²

0⁰

5⁹

891.20

$\frac{10.4}{50}$

Stump

+ H.I. - E/v.
912.14

+50

902.8

15+00

06.3

6⁹² 917⁷⁵ ✓

T. P.

1 31

910⁸³ ✓

+50

13.5

16+00

15.6

+50

17.0

17+00

16.5

+50

16.5

18+00

15.1

+50

13.3

19+00

10.5

+50

02.2

1²⁵

905⁵² ✓

T. P.

13⁴⁸

904²⁷ ✓

20+00

893.3

1⁷¹

894⁵¹

T. P.

12⁷²

892⁸⁰

-2-

2

-R--5-

9³

5⁸

4³

2²

0⁸

1³

1³

2⁷

916.1

$\frac{1.7}{50}$

4⁵

902.8

$\frac{15.0}{50}$

7³

15⁶

12²

+	H.I.	-	EIV.
	894.51		

+50	87.1
21+00	85.1

+50	85.0
22+00	86.3

+50	88.4
23+00	89.8

+50	89.8
24+00	88.8

+50	88.4
25+00	90.1

10³⁶ 902⁹³ ✓

T.P.

B.M.

1⁹⁴

892⁵⁷ ✓

895⁶⁷

7²³

89570

+50	93.7
26+00	95.9

L.

£

R.

-6-

878.2

$$\frac{16.3}{50'}$$

74

94

95

82

6'

47

47

57

6'

44

92

70

888.0

$$\frac{6.5}{50'}$$

+	H.I.	-	EIV.
	902.93		

+50			98.4
27+00			00.5

+50			899.0
28+00			96.9

0⁶³ 891⁹¹

11⁶⁵ 891²⁸

T.P.			
+50			89.1
29+00			83.7

+50			81.2
30+00			79.2

+50			79.6
-----	--	--	------

31+00			84.4
-------	--	--	------

+50			91.9
-----	--	--	------

3⁷⁴ 894³⁴

1³¹ 890⁶⁰

T. P.			
32+00			93.7

+50			90.9
-----	--	--	------

33+00			84.3
-------	--	--	------

-L-

2

-R-

-7-

4⁵

2⁴

3⁰

6⁰

875.9

$\frac{16.0}{50}$

2⁸

8²

885.1

$\frac{68}{50}$

10⁷

12⁷

12³

7⁵

0⁰

0⁶

3⁴

10⁰

+ H.I. - EIV.

894.34

+50

82.1

34+00

80.9

+50

84.3

35+00

94.1

9⁰⁵

901⁶⁰ ✓

T. P.

1⁷⁹

892⁵⁵ ✓

+38

01.6

+50

898.1

36+00

94.5

0⁴²

894⁹³ ✓

T. P.

7⁰⁹

894⁵¹ ✓

+50

92.3

37+00

89.4

+25

(Hub)

88.1

38+00

86.4

B.M

888²¹

6⁶⁷

= 888²⁶

-L-

L

-R- -8-

8796 $\frac{14.7}{50}$

12²

13⁴

$\frac{14.0}{50}$ 880.3

10⁰

0²

0⁰

3⁵

7¹

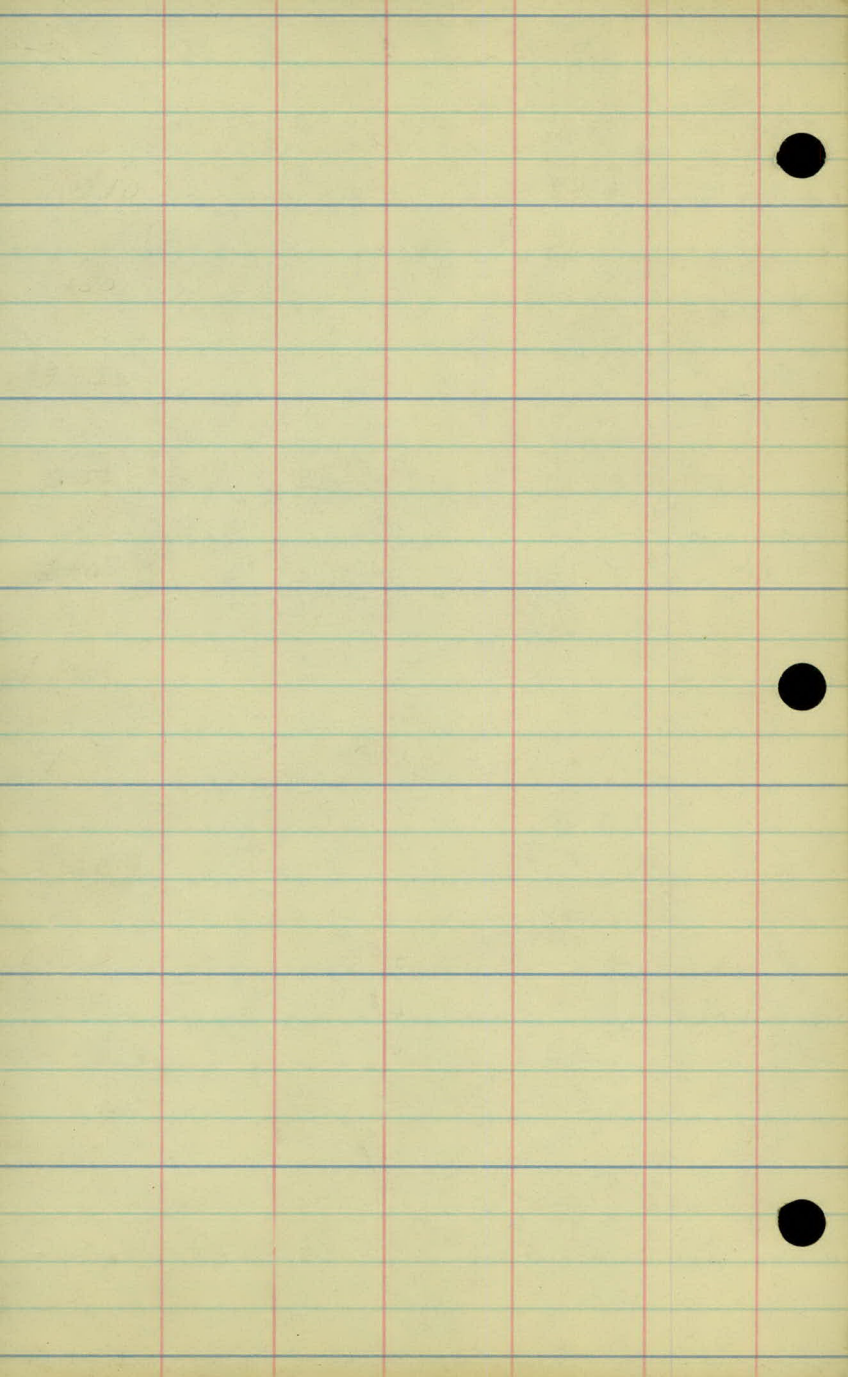
2⁶

5⁵

6⁸

8⁵

Spike in 12" oak 60' left of Sta
0700 = 888.2'



146 h 4-35

-1-

- X -

- Section's -

- Gramsie -

- Road -

+ H.I. - E/V.

B.M. 1.73 982⁵⁹ 98086

0+00 E of Victoria St. 80.7

1+13 80.1

+20 80.4

+50 80.3

1+0 79.5

+50 77.3

2+0 77.3

2+50 76.1

3+0 73.0

T. P. 8.94 973⁶⁵

MLH 4-35

- 2 -

Spr. in rel. Pale 140' R of Sta 0+30

$$\frac{10}{50} \quad 1.9 \quad \frac{2.3}{50}$$

$$\frac{1.7}{50} \quad 2.5 \quad \frac{2.7}{50}$$

$$\frac{1.5}{50} \quad \frac{2.0}{19} \quad 2.2 \quad \frac{2.8}{10} \quad \frac{4.0}{50}$$

$$\frac{1.8}{50} \quad \frac{2.0}{26} \quad 2.3 \quad \frac{2.3}{2} \quad \frac{3.2}{5} \quad \frac{3.5}{28} \quad \frac{4.0}{50}$$

$$\frac{3.3}{50} \quad \frac{3.2}{26} \quad 3.1 \quad \frac{4.0}{4} \quad \frac{4.0}{27} \quad \frac{4.2}{50}$$

$$\frac{5.0}{50} \quad \frac{5.1}{28} \quad 5.3 \quad \frac{6.4}{4} \quad \frac{6.4}{29} \quad \frac{6.4}{50}$$

$$\frac{4.1}{50} \quad \frac{4.1}{21} \quad 5.3 \quad \frac{6.7}{4} \quad \frac{7.4}{26} \quad \frac{8.0}{50}$$

$$\frac{6.4}{50} \quad \frac{6.6}{24} \quad 6.5 \quad \frac{7.6}{2} \quad \frac{9.3}{26} \quad \frac{10.2}{50}$$

$$\frac{8.3}{50} \quad \frac{8.7}{26} \quad 9.6 \quad \frac{10.2}{3} \quad \frac{11.4}{30} \quad \frac{11.6}{50}$$

Top of rock 3+30

+ H.I. - EIV
5.35 9790 97365

3+50

72.5

4+0

71.4

4+50

71.5

5+0

72.0

+50

69.9

T.P.

0.64

969.47

10.17

968.83

6+0

68.2

6+50

66.7

7+0

63.6

-3-

$$\frac{57}{50}$$

$$\frac{61}{23}$$

$$65$$

$$\frac{80}{5}$$

$$\frac{87}{24}$$

$$\frac{95}{50}$$

$$\frac{64}{50}$$

$$\frac{70}{25}$$

$$7.6$$

$$\frac{84}{5}$$

$$\frac{80}{27}$$

$$\frac{72}{50}$$

$$\frac{78}{50}$$

$$\frac{80}{20}$$

$$7.5$$

$$\frac{57}{6}$$

$$\frac{54}{28}$$

$$\frac{36}{50}$$

$$\frac{92}{50}$$

$$\frac{86}{26}$$

$$7.0$$

$$\frac{52}{8}$$

$$\frac{46}{28}$$

$$\frac{34}{50}$$

$$\frac{104}{50}$$

$$\frac{101}{27}$$

$$9.1$$

$$\frac{78}{6}$$

$$\frac{75}{29}$$

$$\frac{73}{50}$$

$$\frac{11}{50}$$

$$\frac{15}{21}$$

$$1.3$$

$$\frac{08}{7}$$

$$\frac{16}{16}$$

$$\frac{10}{50}$$

$$\frac{37}{50}$$

$$\frac{31}{39}$$

$$\frac{38}{19}$$

$$28$$

$$\frac{26}{4}$$

$$\frac{21}{6}$$

$$\frac{30}{24}$$

$$\frac{30}{50}$$

$$\frac{64}{50}$$

$$\frac{55}{37}$$

$$\frac{64}{10}$$

$$59$$

$$\frac{59}{3}$$

$$\frac{48}{7}$$

$$\frac{56}{11}$$

$$\frac{50}{29}$$

$$\frac{43}{50}$$

+ H. 1 -

969⁴⁷

7+25

61.0

T.P. 1.52 961⁹⁶ 9.03 960.44

7+50

55.2

T.P. 1.13 949⁷⁴ 13³⁵ 948⁶¹

8+0

40.7

+50

37.6

T.P. 4.47 941⁶³ 12⁵⁸ 937¹⁶

8+78

36.8

9+0

36.0

+50

30.3

T.P. 0.21 928²² 13⁶² 928⁰¹

B.M.

4.77 923⁴⁵ = 923⁴³

-4-

$\frac{90}{50}$ $\frac{75}{35}$ $\frac{84}{9}$ 85 $\frac{82}{3}$ $\frac{71}{7}$ $\frac{81}{14}$ $\frac{62}{50}$

$\frac{90}{50}$ $\frac{77}{24}$ 68 $\frac{60}{2}$ $\frac{43}{5}$ $\frac{38}{7}$ $\frac{50}{9}$ $\frac{60}{14}$ $\frac{35}{50}$

$\frac{114}{50}$ $\frac{98}{27}$ 90 $\frac{80}{7}$ $\frac{13}{25}$ $\frac{56}{50}$

$\frac{170}{50}$ $\frac{153}{25}$ 121 $\frac{103}{9}$ $\frac{94}{25}$ $\frac{83}{50}$

$\frac{101}{50}$ $\frac{65}{14}$ 48 $\frac{24}{8}$ $\frac{27}{10}$ $\frac{20}{27}$ $\frac{05}{50}$

$\frac{108}{50}$ $\frac{78}{28}$ $\frac{65}{9}$ 56 $\frac{44}{6}$ $\frac{46}{10}$ $\frac{40}{27}$ $\frac{30}{50}$

$\frac{152}{50}$ $\frac{128}{24}$ 113 $\frac{110}{16}$ $\frac{87}{50}$

Nail in 6" oak 2' left of Sta. 10+25
EIV 923.43

+ 4.1 - E/V

928²²

10+0

25.3

10+50

19.9

B.M.

4.77

92345 - 923.43

B.M.

1.11

924⁵⁴

923⁴³

T.P.

3.55

918⁴⁶

9.63

914.91

11+0

12.7

T.P.

2.20

908⁶⁵

12.01

906⁴⁵

11+50

05.2

11+80

03.1

T.P.

0.23

901.71

7.17

901.48

12+0

98.9

12+60

94.0

-L-

-R-5-

$$\frac{90}{50} \quad \frac{55}{20} \quad \frac{38}{2} \quad 29 \quad \frac{1.8}{24} \quad \frac{+0.5}{50}$$

$$\frac{15.5}{50} \quad \frac{118}{27} \quad \frac{93}{4} \quad 83 \quad \frac{93}{5} \quad \frac{61}{24} \quad \frac{32}{50}$$

Nail in 6" oak 2' left of Sta. 10+25

$$\frac{11.7}{50} \quad \frac{92}{33} \quad \frac{6.3}{9} \quad \frac{5.4}{4} \quad 5.8 \quad \frac{42}{20} \quad \frac{0.0}{50}$$

$$\frac{95}{50} \quad \frac{37}{12} \quad \frac{28}{6} \quad 9.63 \quad 34 \quad \frac{30}{22} \quad \frac{26}{50}$$

$$\frac{153}{50} \quad \frac{95}{35} \quad \frac{65}{10} \quad 55 \quad \frac{64}{25} \quad \frac{78}{50}$$

$$\frac{100}{50} \quad \frac{50}{24} \quad \frac{1.7}{20} \quad \frac{1.5}{8} \quad 28 \quad \frac{5.0}{23} \quad \frac{64}{50}$$

$$\frac{124}{50} \quad \frac{107}{30} \quad \frac{73}{16} \quad 77 \quad \frac{98}{30} \quad \frac{103}{50}$$

901.71

13+0

896.4

13+50

01.7

T.P.

7³⁴

908⁵²

0⁵³

901¹⁸

14+0

06.3

B.M

1.31

907²¹

= 907²²

14+50

02.5

15+0

06.5

T.P.

10⁰⁵

916⁹⁴

1.63

906.89

15+50

13.6

16+0

15.5

T.P.

508

920⁶⁴

1.38

915.56

15.5

-6-

$$\frac{134}{50} \quad \frac{122}{33} \quad \frac{108}{28} \quad \frac{58}{12} \quad 53 \quad \frac{65}{12} \quad \frac{91}{50}$$

$$\frac{132}{50} \quad \frac{90}{30} \quad \frac{20}{11} \quad 00 \quad \frac{03}{16} \quad \frac{20}{50}$$

$$\frac{191}{50} \quad \frac{160}{39} \quad \frac{85}{29} \quad \frac{48}{16} \quad 22 \quad \frac{30}{30} \quad \frac{43}{50}$$

Nail in top Stump 4' Left STA. 14+30

$$\frac{178}{50} \quad \frac{124}{39} \quad \frac{78}{20} \quad \frac{65}{5} \quad 60 \quad \frac{65}{12} \quad \frac{65}{32} \quad \frac{40}{50}$$

$$\frac{85}{50} \quad \frac{66}{42} \quad \frac{50}{32} \quad \frac{26}{11} \quad 20 \quad \frac{26}{7} \quad \frac{20}{28} \quad \frac{05}{50}$$

$$\frac{118}{50} \quad \frac{75}{32} \quad \frac{95}{14} \quad 33 \quad \frac{47}{21} \quad \frac{58}{50}$$

$$\frac{61}{50} \quad \frac{37}{33} \quad \frac{18}{11} \quad \frac{12}{8} \quad 14 \quad \frac{18}{6} \quad \frac{28}{26} \quad \frac{48}{50}$$

+ H.I - E/V.

920⁶⁴

16+50 16.7

17+0 16.7

+

17+50 16.4

18+0 14.7

+50 12.9

+70 12.8

19+0 09.6

T.P. 0.16 910⁰⁰ 1080 909⁸⁴

19+50 02.2

T.P. 4.18 900⁹¹ 1327 896⁷³

20+0 893.4

T.P. 1.31 892⁵⁴ 968 891²³

$$\frac{75}{50} \quad \frac{62}{32} \quad \frac{45}{13} \quad \frac{38}{10} \quad 39 \quad \frac{25}{13} \quad \frac{72}{36} \quad \frac{95}{50}$$

$$\frac{77}{50} \quad \frac{74}{33} \quad \frac{53}{14} \quad \frac{44}{10} \quad 39 \quad \frac{40}{15} \quad \frac{51}{31} \quad \frac{80}{50}$$

$$\frac{57}{50} \quad \frac{55}{34} \quad \frac{48}{13} \quad \frac{40}{11} \quad 42 \quad \frac{47}{20} \quad \frac{72}{50}$$

$$\frac{53}{50} \quad \frac{51}{30} \quad \frac{47}{7} \quad 59 \quad \frac{93}{29} \quad \frac{133}{50}$$

$$\frac{51}{50} \quad \frac{48}{38} \quad \frac{60}{12} \quad 77 \quad \frac{126}{28} \quad \frac{170}{50}$$

$$\frac{51}{50} \quad \frac{51}{32} \quad \frac{62}{14} \quad 78 \quad \frac{126}{30} \quad \frac{167}{50}$$

$$\frac{114}{50} \quad \frac{108}{32} \quad \frac{108}{9} \quad 107 \quad \frac{125}{23} \quad \frac{161}{50}$$

$$\frac{116}{50} \quad \frac{116}{23} \quad \frac{94}{9} \quad 78 \quad \frac{32}{26} \quad \frac{25}{40} \quad \frac{30}{50}$$

$$\frac{121}{50} \quad \frac{104}{24} \quad \frac{90}{11} \quad 75 \quad \frac{52}{24} \quad \frac{18}{50}$$

+ H. I. - EIV

892⁵⁴

20+5.0

87.0

21+0

85.1

+50.

85.0

22+0

86.2

T.P.

5.83

89656

1.81

89073

B.M

0.91

89565 = 89567

-8-

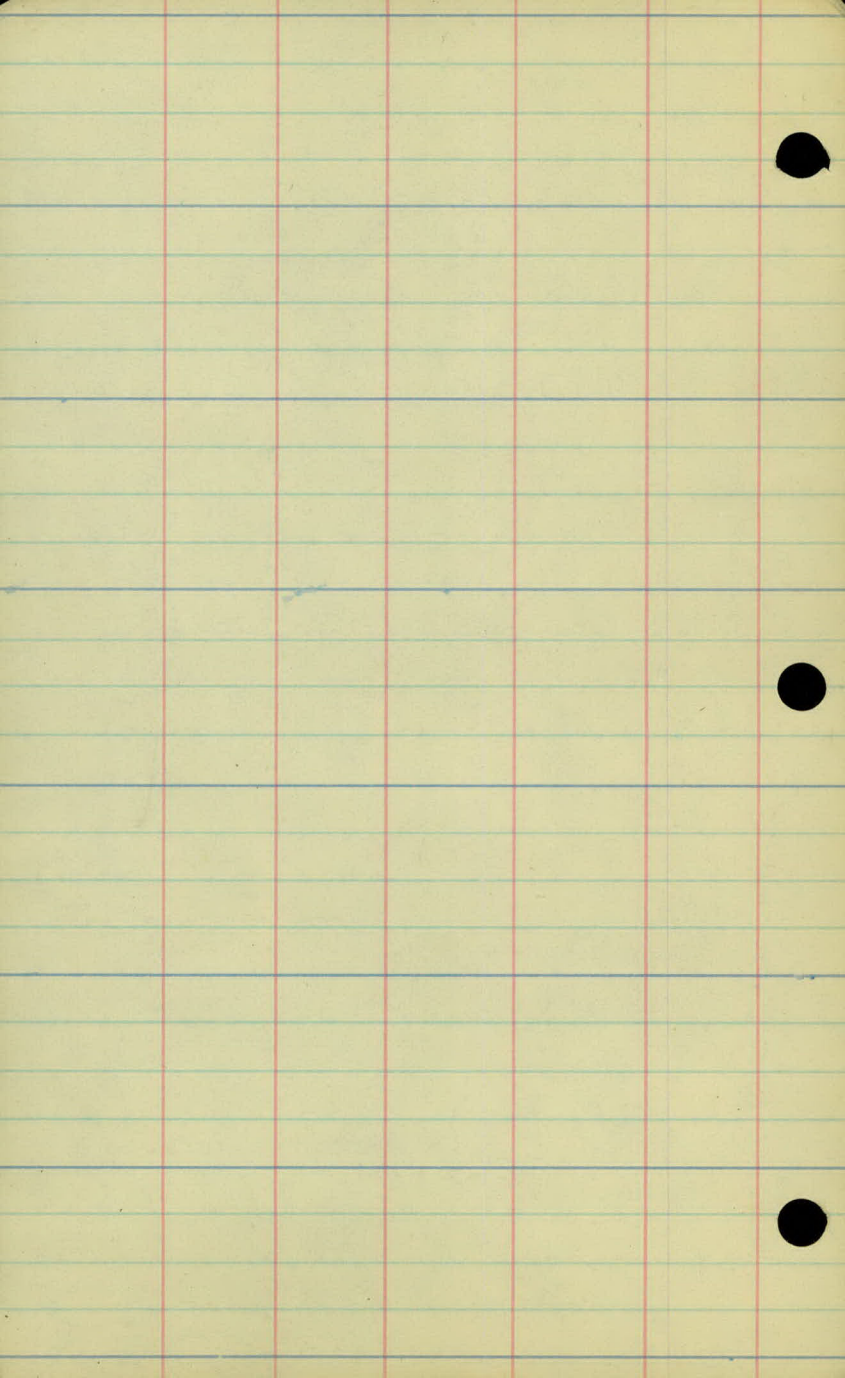
$$\frac{106}{50} \quad \frac{96}{33} \quad \frac{70}{12} \quad \frac{55}{7} \quad 55 \quad \frac{45}{11} \quad \frac{25}{27} \quad \frac{1.2}{50}$$

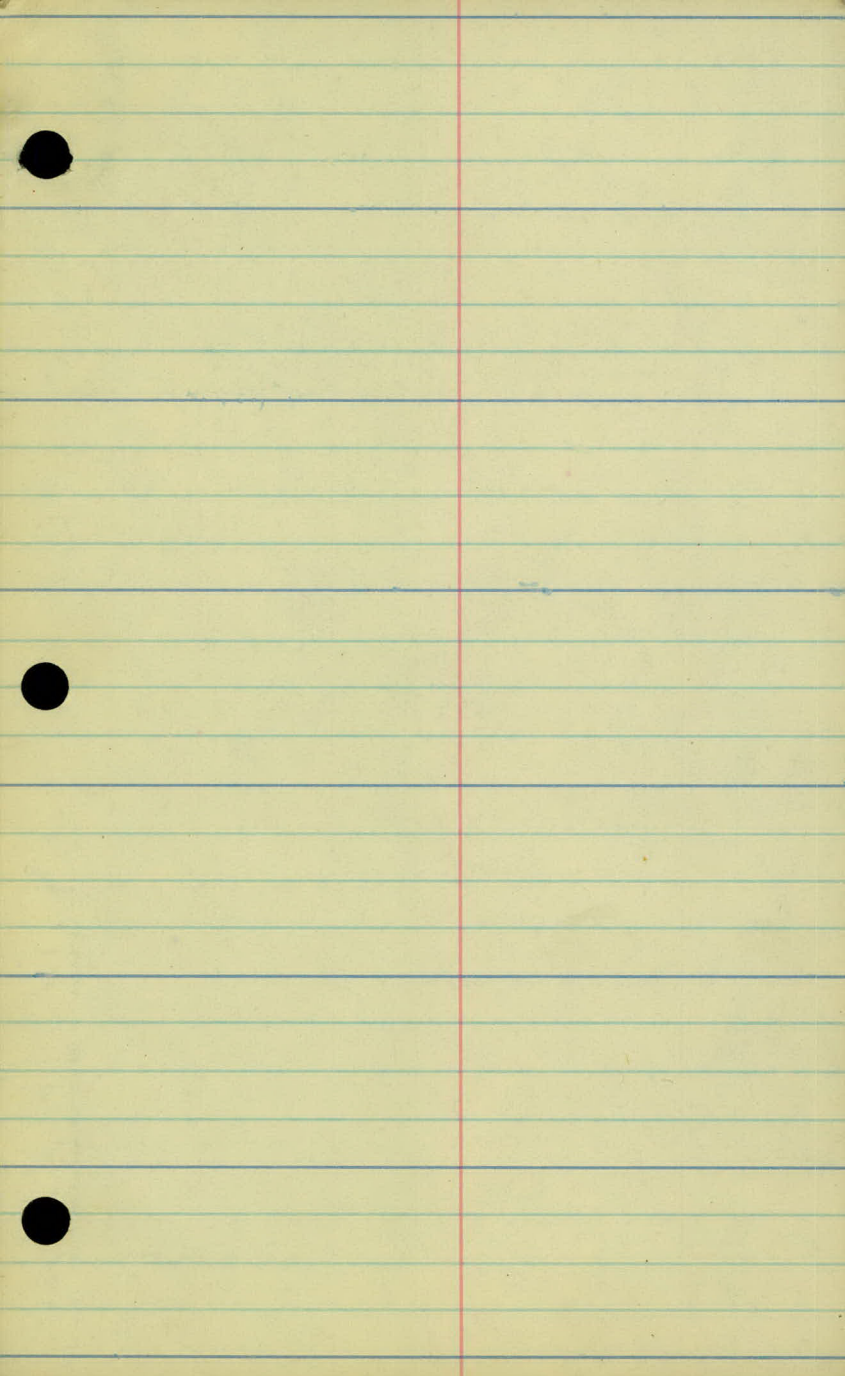
$$\frac{127}{50} \quad \frac{112}{38} \quad \frac{86}{13} \quad \frac{76}{7} \quad 74 \quad \frac{61}{25} \quad \frac{46}{50}$$

$$\frac{121}{50} \quad \frac{98}{21} \quad \frac{90}{13} \quad \frac{80}{8} \quad 75 \quad \frac{48}{25} \quad \frac{33}{50}$$

$$\frac{104}{50} \quad \frac{85}{23} \quad \frac{73}{15} \quad 63 \quad \frac{37}{28} \quad \frac{17}{50}$$

Nail Top STump 20' Left Sta 25+50





+ H.1 - E/V.

B.M.

0.47

896[✓]14

895[✓]67

88.4

22+50

88.4

23+0

89.6

+50

89.5

24

88.7

+50

88.3

25+0

90.0

B.M.

631

901[✓]98

0.47

895[✓]67

25+50

93.8

26+0

95.7

26+50

98.2

T.P.

589

905[✓]92

1.95

900[✓]03

- L -

E - R - Mch-35
- 9 -

Nail Top stump 20' Left Sta 25+50

$$\frac{130}{50}$$

$$\frac{105}{24}$$

$$\frac{90}{18}$$

77

$$\frac{57}{21}$$

$$\frac{31}{50}$$

$$\frac{117}{50}$$

$$\frac{82}{21}$$

65

$$\frac{43}{24}$$

$$\frac{25}{50}$$

$$\frac{92}{50}$$

$$\frac{71}{21}$$

66

$$\frac{50}{25}$$

$$\frac{31}{50}$$

$$\frac{88}{50}$$

$$\frac{76}{28}$$

$$\frac{70}{20}$$

74

$$\frac{68}{25}$$

$$\frac{4.5}{50}$$

$$\frac{100}{50}$$

$$\frac{96}{30}$$

$$\frac{87}{20}$$

78

$$\frac{61}{20}$$

$$\frac{17}{50}$$

$$\frac{126}{50}$$

$$\frac{100}{26}$$

$$\frac{78}{16}$$

61

$$\frac{24}{23}$$

$$\frac{00}{41}$$

$$\frac{+1.0}{50}$$

$$\frac{140}{50}$$

$$\frac{100}{23}$$

81

$$\frac{62}{24}$$

$$\frac{36}{50}$$

$$\frac{87}{50}$$

$$\frac{68}{24}$$

63

$$\frac{60}{25}$$

$$\frac{50}{50}$$

$$\frac{46}{50}$$

$$\frac{32}{24}$$

38

$$\frac{47}{22}$$

$$\frac{51}{50}$$

+ H.1 - EIV.

✓
905.92

27+0

00.4

+36

00.2

27+70

99.1

T.P.

0.11

✓
897.31

8.72

✓
897.20

28+0

97.0

+30

93.2

T.P.

4.28

✓
889.99

11.60

✓
885.71

+70

86.5

29+0

83.6

+50

81.2

30+0

79.3

+50

79.6

-L-

E

-R-

-10-

$$\frac{48}{50}$$

$$\frac{43}{23}$$

$$55$$

$$\frac{71}{25}$$

$$\frac{85}{50}$$

$$\frac{28}{50}$$

$$\frac{24}{37}$$

$$\frac{38}{20}$$

$$57$$

$$\frac{77}{24}$$

$$\frac{90}{50}$$

$$\frac{97}{50}$$

$$\frac{76}{39}$$

$$\frac{54}{20}$$

$$68$$

$$\frac{88}{25}$$

$$\frac{105}{50}$$

$$\frac{120}{50}$$

$$\frac{104}{42}$$

$$\frac{46}{29}$$

$$\frac{11}{18}$$

$$\frac{06}{16}$$

$$03$$

$$\frac{20}{26}$$

$$\frac{36}{50}$$

$$\frac{145}{50}$$

$$\frac{115}{33}$$

$$\frac{78}{18}$$

$$\frac{53}{12}$$

$$41$$

$$\frac{45}{25}$$

$$\frac{64}{50}$$

$$\frac{101}{50}$$

$$\frac{85}{24}$$

$$\frac{65}{15}$$

$$\frac{38}{6}$$

$$35$$

$$\frac{25}{23}$$

$$\frac{47}{50}$$

$$\frac{127}{50}$$

$$\frac{110}{35}$$

$$\frac{86}{15}$$

$$64$$

$$\frac{54}{25}$$

$$\frac{50}{50}$$

$$\frac{142}{50}$$

$$\frac{133}{35}$$

$$\frac{97}{10}$$

$$88$$

$$\frac{72}{15}$$

$$\frac{35}{31}$$

$$\frac{21}{50}$$

$$\frac{148}{50}$$

$$\frac{138}{31}$$

$$\frac{117}{10}$$

$$107$$

$$\frac{77}{22}$$

$$\frac{14}{41}$$

$$\frac{03}{50}$$

$$\frac{143}{50}$$

$$\frac{142}{32}$$

$$\frac{125}{11}$$

$$104$$

$$\frac{80}{11}$$

$$\frac{37}{32}$$

$$\frac{+05}{50}$$

T.P. + H.I. ✓ - EIV.
889.99

31+0 84.3

T.P. 9.87 ✓ 897⁸⁴ 2.02 ✓ 887⁹⁷

31+00

31+50 91.5

31+75 93.4

32+0 93.7

32+30 92.5

32+60 90.1

T.P. 5.00 ✓ 890⁹⁶ 1188 ✓ 885⁹⁶

33+0 84.3

33+50 82.5

+80 80.4

34+0 80.8

- L - $\frac{1}{2}$ - R - -11-

$$\frac{130}{50}$$

$$\frac{97}{30}$$

$$\frac{75}{11}$$

$$57$$

$$\frac{15}{25}$$

$$13.5$$

$$\frac{34}{50}$$

$$\frac{163}{50}$$

$$\frac{154}{43}$$

$$\frac{127}{29}$$

$$\frac{84}{11}$$

$$63$$

$$\frac{25}{26}$$

$$\frac{00}{50}$$

$$\frac{135}{50}$$

$$\frac{107}{31}$$

$$\frac{61}{15}$$

$$44$$

$$\frac{18}{26}$$

$$\frac{00}{50}$$

$$\frac{102}{50}$$

$$\frac{26}{32}$$

$$\frac{49}{13}$$

$$41$$

$$\frac{21}{27}$$

$$\frac{00}{50}$$

$$\frac{80}{50}$$

$$\frac{72}{32}$$

$$\frac{56}{12}$$

$$53$$

$$\frac{38}{26}$$

$$\frac{22}{50}$$

$$\frac{107}{50}$$

$$\frac{95}{31}$$

$$\frac{77}{13}$$

$$77$$

$$\frac{67}{23}$$

$$\frac{48}{50}$$

$$\frac{94}{50}$$

$$\frac{84}{34}$$

$$\frac{77}{14}$$

$$67$$

$$\frac{63}{13}$$

$$\frac{14}{50}$$

$$\frac{128}{50}$$

$$\frac{124}{36}$$

$$\frac{93}{17}$$

$$85$$

$$\frac{80}{24}$$

$$\frac{63}{50}$$

$$\frac{97}{50}$$

$$\frac{95}{29}$$

$$\frac{106}{22}$$

$$\frac{112}{9}$$

$$106$$

$$\frac{97}{24}$$

$$\frac{90}{50}$$

$$\frac{77}{50}$$

$$\frac{70}{45}$$

$$\frac{90}{31}$$

$$\frac{102}{12}$$

$$102$$

$$\frac{108}{24}$$

$$\frac{101}{50}$$

+

H.1 ✓
89096

EIV

34+50

✓

✓

83.9

T. P. 937

89875

1.58

889.38

34+86

90.9

35+0

✓

✓

94.0

T. P. 9.22

90774

0.23

898.52

35+35

01.7

35+60

96.7

35+80

95.4

36+0

✓

✓

94.2

T. P. 0.65

89623

1216

895.58

B. M.

B. M.

8.05

888.18

= 88821

B. M.

1103

89924

88821

36+50

92.1

36+80

90.4

- L -

E

- R -

- 12 -

 $\frac{+1.5}{50}$ $\frac{00}{44}$ $\frac{40}{25}$ $\frac{51}{11}$ 70 $\frac{85}{25}$ $\frac{90}{50}$
 $\frac{20}{50}$ $\frac{52}{21}$ 78 $\frac{100}{12}$ $\frac{110}{25}$ $\frac{101}{39}$ $\frac{105}{50}$
 $\frac{+2.2}{50}$ $\frac{00}{36}$ $\frac{16}{27}$ 48 $\frac{78}{24}$ $\frac{92}{27}$ $\frac{94}{44}$ $\frac{104}{50}$
 $\frac{26}{50}$ $\frac{45}{24}$ 60 $\frac{144}{9}$ $\frac{163}{16}$ $\frac{163}{23}$ $\frac{145}{31}$ $\frac{125}{38}$ $\frac{135}{50}$
 $\frac{08}{50}$ $\frac{16}{26}$ $\frac{20}{9}$ $\frac{80}{6}$ 110 $\frac{150}{8}$ $\frac{150}{20}$ $\frac{110}{29}$ $\frac{76}{37}$ $\frac{98}{50}$
 $\frac{14}{50}$ $\frac{06}{24}$ $\frac{18}{14}$ $\frac{34}{10}$ $\frac{110}{6}$ 123 $\frac{138}{4}$ $\frac{142}{12}$ $\frac{130}{21}$ $\frac{55}{37}$ $\frac{51}{43}$ $\frac{61}{50}$
 $\frac{27}{50}$ $\frac{37}{18}$ $\frac{53}{11}$ 135 $\frac{138}{9}$ $\frac{80}{21}$ $\frac{58}{27}$ $\frac{66}{50}$

Spk. in 12" oak 60' Left Stg. 37+10

 $\frac{28}{50}$ $\frac{24}{8}$ $\frac{24}{8}$ $\frac{68}{3}$ 71 $\frac{70}{6}$ $\frac{57}{12}$ $\frac{36}{19}$ $\frac{27}{50}$
 $\frac{75}{50}$ $\frac{98}{17}$ $\frac{98}{8}$ $\frac{88}{4}$ 88 $\frac{88}{10}$ $\frac{103}{16}$ $\frac{108}{30}$ $\frac{108}{50}$

+ H.I. - EIV.

✓
899²⁴ 11.03

✓
88821 B.M.

89.2

37+0

B.M

3.80

✓
892⁰¹

✓
?

✓
88821

37+25

88.2

37+50

87.4

37+75

86.8

38+0

86.2

+50

84.7

39+0

83.9

B.M

3.80

✓
88821

-L-

-R-

-13-

$\frac{115}{50}$ $\frac{132}{31}$ $\frac{133}{14}$ $\frac{120}{7}$ $\frac{98}{2}$ 100 $\frac{100}{10}$ $\frac{143}{20}$ $\frac{145}{50}$

Spk. in 12" oak 60' Left Sta. 37+10

$\frac{72}{50}$ $\frac{82}{15}$ $\frac{37}{2}$ 38 $\frac{38}{9}$ $\frac{87}{17}$ $\frac{97}{50}$

$\frac{71}{50}$ $\frac{77}{18}$ $\frac{47}{5}$ 46 $\frac{47}{7}$ $\frac{53}{11}$ $\frac{80}{17}$ $\frac{90}{50}$

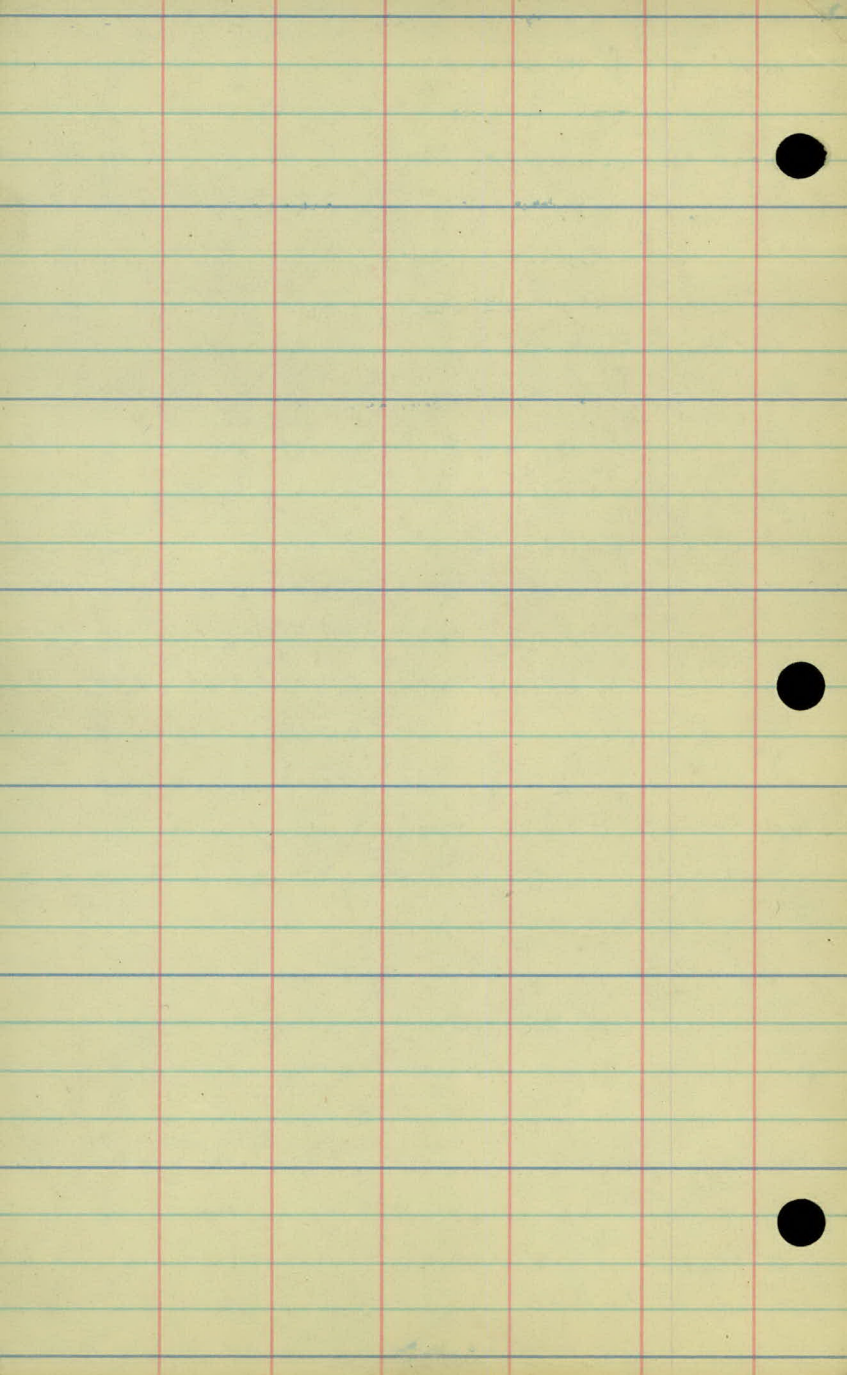
$\frac{47}{50}$ $\frac{50}{24}$ $\frac{68}{21}$ $\frac{68}{18}$ $\frac{54}{13}$ 52 $\frac{55}{13}$ $\frac{68}{16}$ $\frac{68}{21}$ $\frac{60}{24}$ $\frac{72}{50}$

$\frac{20}{50}$ $\frac{20}{28}$ $\frac{26}{22}$ $\frac{76}{17}$ $\frac{60}{13}$ 58 $\frac{60}{13}$ $\frac{76}{16}$ $\frac{75}{22}$ $\frac{46}{30}$ $\frac{50}{50}$

73

81

Spk. in 12" oak 60' Left Sta 37+10



No. 1 10p STAMP 25+50

+ H.I - EIV

B.M 13 48 909 15 895 67

13 48 895 67 B.M

19+25

895 67
+ 13 48

909.15

- L -

E

R

Nail top stump Sta 25+50 20' left

$$\frac{57}{50}$$

$$\frac{52}{23}$$

$$\frac{43}{11}$$

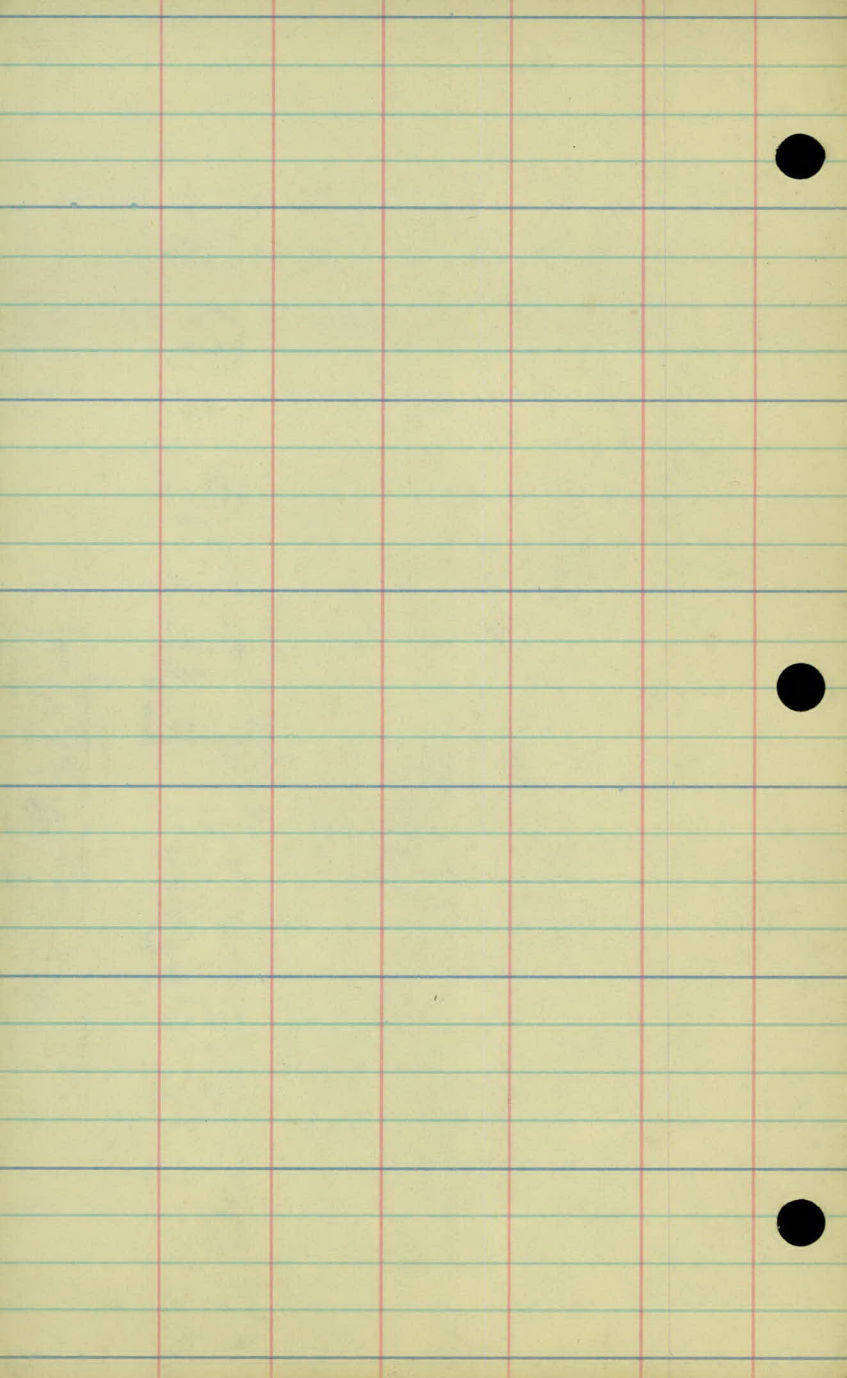
05.9

33

$$\frac{14}{25}$$

$$\frac{22}{41}$$

$$\frac{32}{50}$$



Moh 1935

X

Section's

Sta.

38+25 TO 41+50

+ H.1 - EIV

B.M. 1.27 88948 88821

38+25 85.5

+50 84.8

39+0 84.0

+50 83.1

40+0 81.9

40+46 E of P³ 24" x 48' 80.8

41+0 81.4

41+50 81.9

B.M. 1.27 888.21

-L-

-R-

spr in 12" oak 60' Left of 37+10

$\frac{104}{50}$ $\frac{06}{29}$ $\frac{56}{21}$ $\frac{58}{17}$ $\frac{41}{13}$ 40 $\frac{41}{13}$ $\frac{58}{17}$ $\frac{54}{21}$ $\frac{20}{29}$ $\frac{25}{50}$

$\frac{54}{50}$ $\frac{45}{24}$ $\frac{60}{21}$ $\frac{60}{17}$ $\frac{47}{13}$ 47 $\frac{47}{13}$ $\frac{62}{17}$ $\frac{58}{21}$ $\frac{31}{30}$ $\frac{25}{50}$

$\frac{97}{50}$ $\frac{91}{22}$ $\frac{57}{13}$ 56 $\frac{58}{13}$ $\frac{74}{17}$ $\frac{77}{22}$ $\frac{72}{50}$

$\frac{125}{50}$ $\frac{130}{28}$ $\frac{120}{24}$ $\frac{67}{13}$ 64 $\frac{68}{13}$ $\frac{91}{17}$ $\frac{100}{50}$

$\frac{128}{50}$ $\frac{125}{37}$ $\frac{122}{23}$ $\frac{76}{13}$ 76 $\frac{81}{13}$ $\frac{121}{20}$ $\frac{121}{28}$ $\frac{115}{50}$

$\frac{152}{24}$
Flow line

$\frac{138}{24}$
Water

87

$\frac{126}{24}$
Water
Flow line

81

76

spr in 12" oak 60' Left of 37+10

20-0

21-0

22-0

23-0

24-0

25-0

26-0

Moh-35

-1

- Topog -

- Gramsie -

- Road -

6+0

5+0

4+0

3+0

2+0

0+00. E of Victoria St.

Cultivated

Light Clearing

Cultivated

Handwritten notes and symbols along the center line.

Handwritten notes and symbols at the bottom of the page, including a small circle and lines.

12

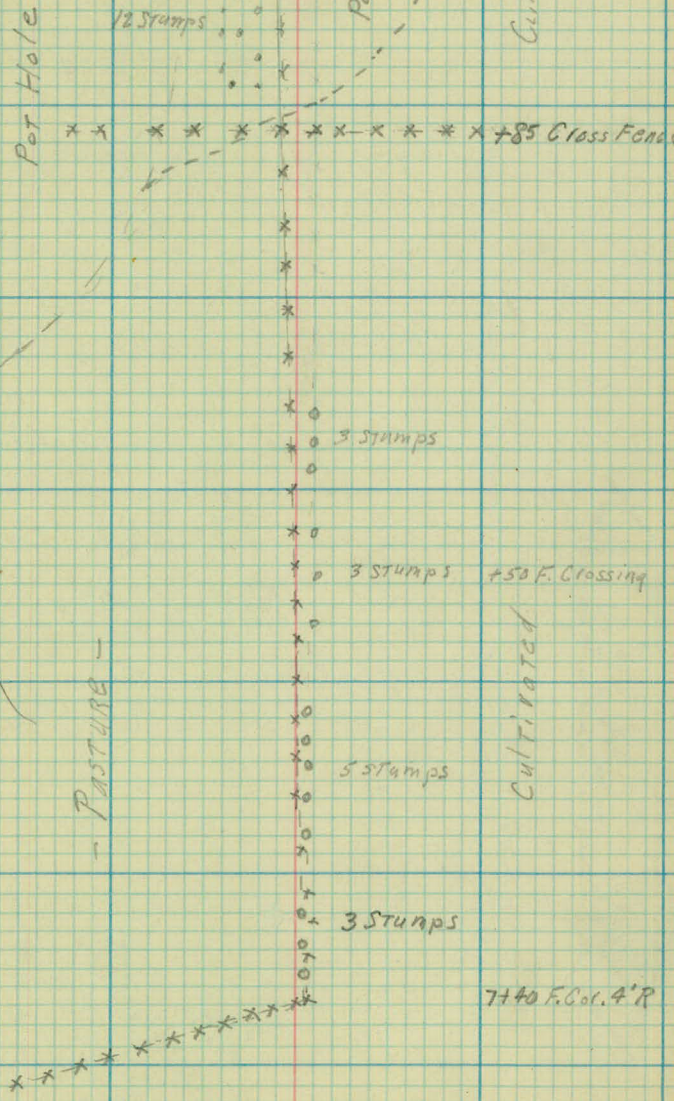
11

10

9

8+0

7+0



18

17

16

15

14

13

F.L. 10'L

F.L. 8'L

FL. 6'L

Woods

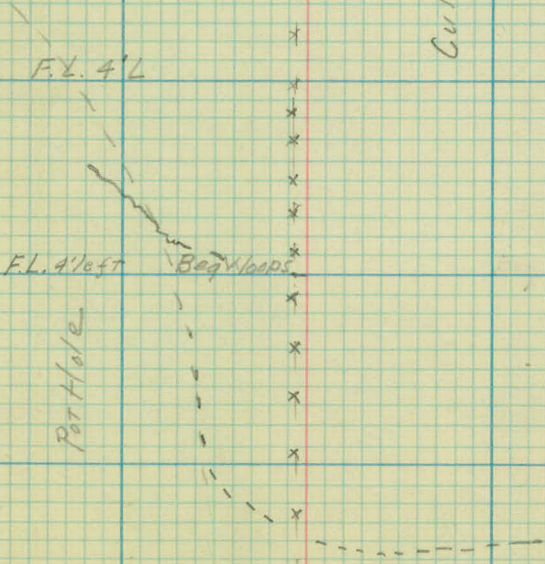
F.L. 4'L

F.L. 4' left

Bag Woods

Port Hole

Cultivated



24+0

23+0

22+0

21+0

20+0

19+0

E

-5-

F.L. 21'

A22

F.L. 19'

F.L. 16' Beg. Woods

Por Hole

F.L. 12'

+50 Edge Woods

D. 37

Cultivated

31+0

30+0

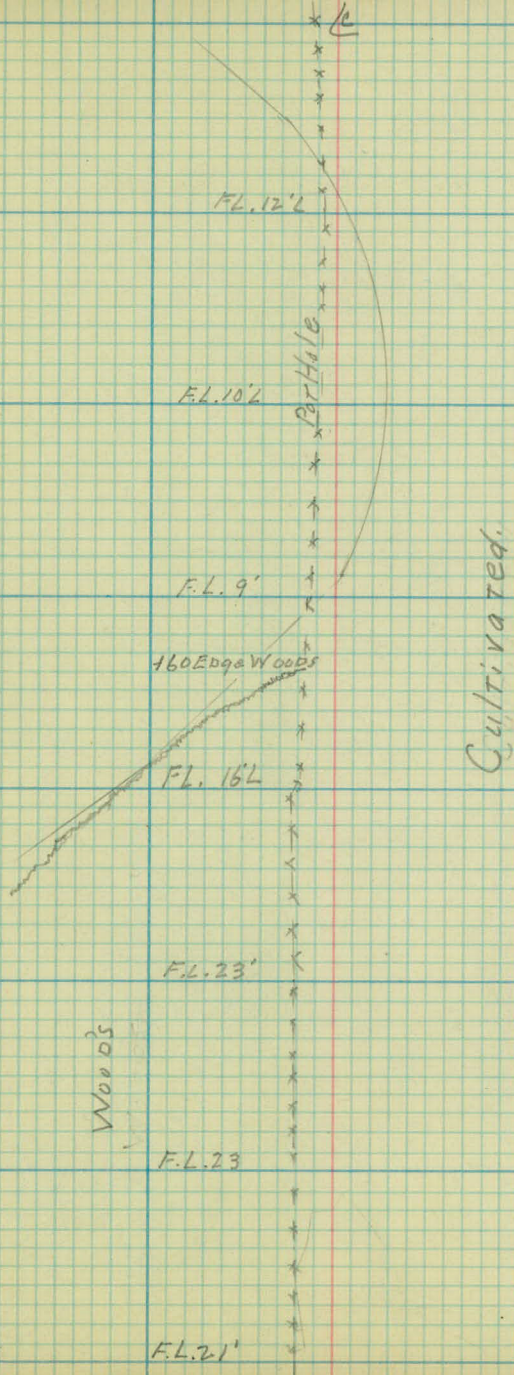
29+0

28+0

27+0

26+0

25+0



38+0

37+0

36+0

35+0

34+0

33+0

32+0

+70 END G.R.
+59 Edge Rd.

x
x
x
x
x
x
x

+70 Drive. E
+59 20' F.L.

+35 4 12" TREN
12' R

F.L. 13'

F.L. 14'

+70 15' oak 30' L

F.L. 28' R

Read 35'

+70 F. Cor.

+80 12" oak 30'

Drive

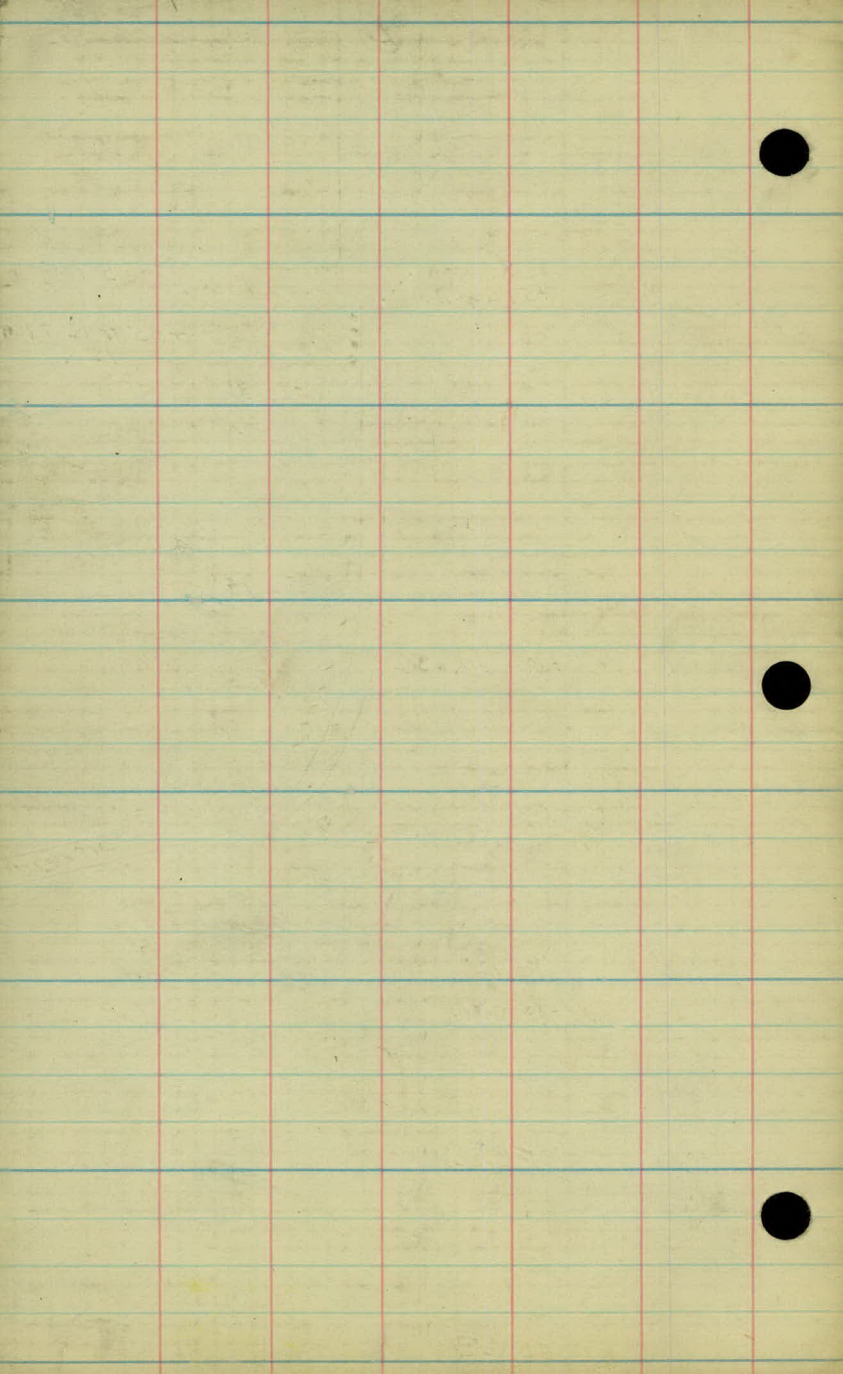
F.L. 12'

+85 ditch

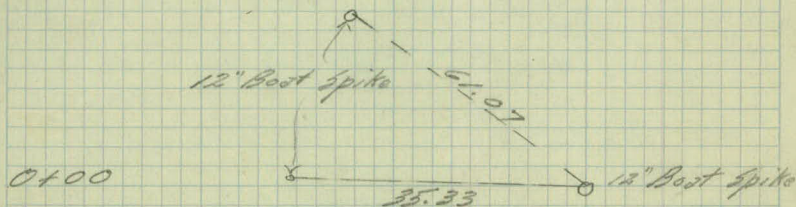
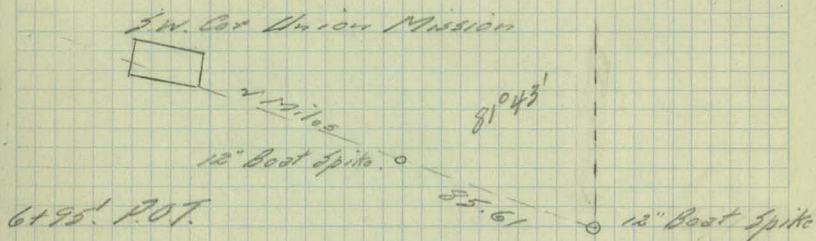
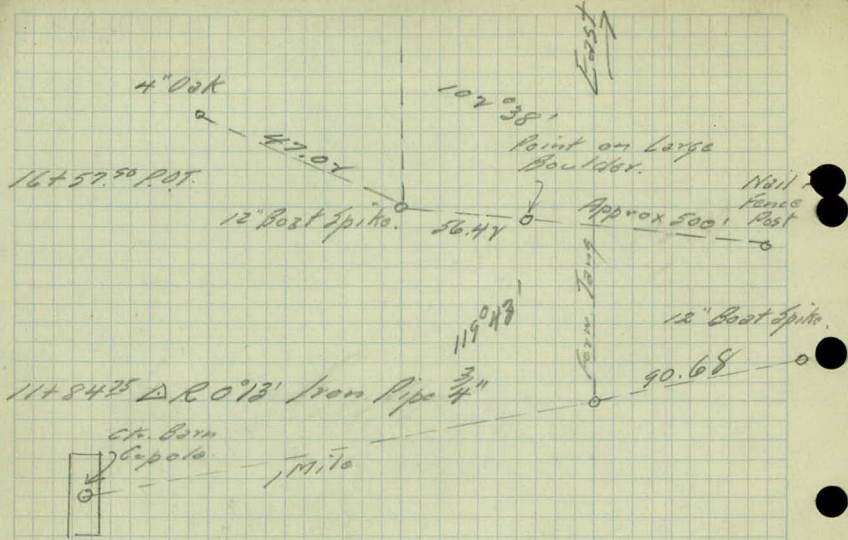
Pot Hole

F.L. 12'

F.L. 12' L



Reference Point Gramsc
Road from Sta. 0+00 at
Victoria St. to Sta. 16+57.90



1
Slope Slokes Grammie Road.
Victoria St. East. Sta. 0+00 to 20±

575	+	K	-	Grade
-----	---	---	---	-------

B.M.	6.94	985.05		978.11
------	------	--------	--	--------

0+20				80.0
------	--	--	--	------

+50				79.6
-----	--	--	--	------

1				79.0
---	--	--	--	------

+50				78.3
-----	--	--	--	------

2				77.7
---	--	--	--	------

+50				77.0
-----	--	--	--	------

3				76.4
---	--	--	--	------

T.P.	4.24	977.67	11.62	973.43
------	------	--------	-------	--------

+50				75.4
-----	--	--	--	------

Grade
Rod.

Lt.

Rt.

2' Ditch. 26' top
2 to 1, Fine
Lt.

Spike in T.P. 1st Rt St. 0+00 Victoria St.

Sumo. Two Hens says to stake
all into to 33 ft. Sta 0 to 38+

5.0

5.4
7.4

4.9
D.C. 1.9
33

Co. 4

6.2
D.C. 1.2
33

6.0
5.0

6.1
D.C. 1.9
33

5.9
C.O. 1

Grade Plug
let. 8

6.7
D.C. 1.3
33

6.7
6.7

7.9
D.C. 0.8
33

7.8
F. 1.1

7.1
F. 2.4
17.8

7.3
9.3.

7.3
D.C. 2.0
33

7.9
F. 0.6

9.8
F. 1.8
18

8.0
10.0

9.4
D.C. 0.6
33

9.3
F. 1.3

11.8
F. 3.8
20.6

8.6
10.6

11.6
F. 3.0
19.0

11.9
F. 3.3

13.7
F. 5.1
23.4

2.3
4.3

5.0
F. 2.7
18.4

5.4
F. 3.1

7.7
F. 5.4
23.8

Sta. + K - Grade

977.67

4

74.1

+50

78.0

5

69.4

+50

66.3

6

62.7

+50

58.4

7

53.8

✓ T.P. BM
+25

2.14

966.45

13.36
(3.46)

964.31

962.99

51.3

Grade
Rod

LT

E

RT

3.6
5.6

6.1
~~4.5~~
11.0

6.5
~~4.5~~
11.0

6.9
~~3.3~~
19.6

5.7
7.7

7.1
~~0.0~~
33

6.5
~~0.5~~ Grade Plug
11.0

3.6
~~DC 4.1~~
33

8.3
10.3

7.9
~~DC 2.0~~
33

5.6
~~C 2.7~~

3.1
~~DC 7.2~~
33

11.4
13.4

9.1
~~DC 4.3~~
33

7.5
~~C 3.9~~

6.6
~~DC 6.8~~
33

15.0
17.0

9.5
~~DC 7.1~~
33

9.5
~~C 5.1~~

9.5
~~DC 7.5~~
33

19.3
21.0

11.7
~~DC 9.3~~
33

11.3
~~C 8.0~~

11.5
~~DC 9.5~~
33

23.9
25.9

13.6
~~DC 12.3~~
33

13.3
~~C 10.6~~

13.5
~~DC 12.4~~
33 ✓

Drill on FP 100' Rt. Sta. 7700

5.7
17.2

4.2
~~DC 13.0~~
33

5.1
~~C 9.7~~ +

5.0
~~DC 12.2~~
33

Sta. + π - Grade

966.45

7+50

48.8

T.P. 1.86 954.67 13.64 955.81

8

43.8

T.P. 1.17 948.36 13.48 941.19

+50

38.8

+78

36.0

(B.M.)

(13.90)

(928.46)

9

33.8

+50

28.8

T.P. 0.82 930.52 12.66 929.70

(B.M.)

(7.09)

(923.43)

10

23.8

+50

18.8

T.P. 0.30 917.56 12.26 917.26

Grade
Road.

LT

2

RT

17.7
19.7

11.7
D.C. 8.0
33

11.6
6.1
C

10.3
D.C. 9.4
33

10.9
12.9

14.3
F. 3.4
19.8

14.1
F. 3.2

11.6
D.C. 1.3
33

3.6
5.6

7.6
F. 4.0
21

4.6
F. 1.0

18
D.C. 38
33

6.4
8.4

8.4
D.C. 0.0
20.8

5.6
C. 0.8

2.4
D.C. 6.0
33

8.6
10.6

9.5
D.C. 1.1
33

6.4
E. 2.2

5.4
D.C. 1.2
33

13.6
15.6

13.6
D.C. 2.0
33

11.9
C. 1.7

11.6
D.C. 4.0
33

Trail in 6" Oak 2' Lt. Sta 10+25

6.7
8.7

8.7
D.C. 2.0
33

4.9
C. 1.8

3.3
D.C. 5.4
33

11.7
13.7

13.7
D.C. 0.0
25.3

10.6
C. 1.1

7.3
D.C. 6.4
33

Sta. + π - Grade.

917.56

11

13.9

+50

09.8

T.P.

0.17

904.49

13.24

904.32

+80

07.6

12

06.4

+50

03.9

13

02.1

+50

01.2

T.P.

6.42

910.50

0.41

904.08

(B.M.)

0.42

910.42

(3.37)
0.50

(907.13)

910.00

14

01.1

K 907.13 Old Bench may be moved

Grade
Rod.

4

2

RT

3.7
5.9

6.8
F.3.1
19.2

5.1
F.1.4

1.5
D.C.4.2
33

7.8
9.8

14.3
F.6.1
26

12.2
F.4.4

11.9
F.4.1
21.2

+3.1
21.1

3.0
F.6.1
21.4

1.3
F.4.4

2.2
F.5.3
27.6

+1.9

6.3
F.8.2
27.4

5.4
F.7.3

9.0
F.10.9
33

0.6

13.6
F.13.0
33

10.2
F.9.6

12.5
F.11.9
33

2.4
4.4

14.9
F.18.5
33

8.2
F.1.8

10.2
F.7.8
28.6

3.3
5.9

13.7
F.10.4
33

2.8
C.0.1

3.6
D.C. 1.7
33

2011 in F.P. 250 RT 11485

11.3

11.3
D.C. 0.9
24

4.2
C.5.1

5.1
D.C. 6.2
33

5/2. + π - Grade.

910.44

14+50

01.8

15

03.4

T.P.

11.38

910.90

0.90

909.50

+50

04.5

16

05.5

+50

06.1

17

06.3

+50

06.4

18

06.7

Grade Lt.

E

E1

6

$$\begin{array}{r} 8.6 \\ 10.6 \end{array}$$

$$\begin{array}{r} 10.6 \\ D.C. 0.0 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 8.0 \\ C 0.6 \end{array}$$

$$\begin{array}{r} 8.0 \\ D.C. 2.6 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 7.2 \\ 9.1 \end{array}$$

$$\begin{array}{r} 7.2 \\ D.C. 4.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.1 \\ C 3.1 \end{array}$$

$$\begin{array}{r} 3.6 \\ D.C. 5.6 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 16.4 \\ 18.4 \end{array}$$

$$\begin{array}{r} 11.3 \\ D.C. 7.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 7.3 \\ C 9.1 \end{array}$$

$$\begin{array}{r} 9.1 \\ D.C. 9.3 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 15.4 \\ 17.4 \end{array}$$

$$\begin{array}{r} 7.4 \\ D.C. 10.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ C 10.1 \end{array}$$

$$\begin{array}{r} 7.3 \\ D.C. 10.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 14.8 \\ 16.8 \end{array}$$

$$\begin{array}{r} 6.2 \\ D.C. 10.6 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.4 \\ C 10.4 \end{array}$$

$$\begin{array}{r} 6.9 \\ D.C. 9.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 14.6 \\ 16.6 \end{array}$$

$$\begin{array}{r} 7.5 \\ D.C. 9.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.4 \\ C 10.2 \end{array}$$

$$\begin{array}{r} 5.8 \\ D.C. 10.8 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 14.7 \\ 16.7 \end{array}$$

$$\begin{array}{r} 5.8 \\ D.C. 10.9 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 4.6 \\ C 10.1 \end{array}$$

$$\begin{array}{r} 5.7 \\ D.C. 11.0 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 15.2 \\ 17.2 \end{array}$$

$$\begin{array}{r} 5.1 \\ D.C. 12.1 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 8.2 \\ C 10.0 \end{array}$$

$$\begin{array}{r} 10.0 \\ D.C. 12.2 \\ \hline 33 \end{array}$$

5/2	+	x	-	Grade
		970.90		

18150				04.8
-------	--	--	--	------

T.P.	1.98	909.84	13.04	907.86
------	------	--------	-------	--------

+ 70				04.4
------	--	--	--	------

19				03.6
----	--	--	--	------

100				
+ 50				02.2

20				00.8
----	--	--	--	------

	2.86.	900.21	12.49	897.35
--	-------	--------	-------	--------

+ 10				
B.M.			12.71	887.50

Grade
Rod

LT

2

RT

2

16.1
18.1

5.2
D.C. 17.9
33

10.2
C 5.9

13.9
D.C. 17.2
33

5.4
7.4

+6.1
D.C. 13.5
33

2.4
D.C. 17.0
33

6.2
8.2

0.0
D.C. 8.2
33

2.6
C 3.6

2.8
D.C. 5.4
33

7.6
9.6

10.8
F 3.2
19.4

10.5
F 2.9

2.6
D.C. 7.0
33

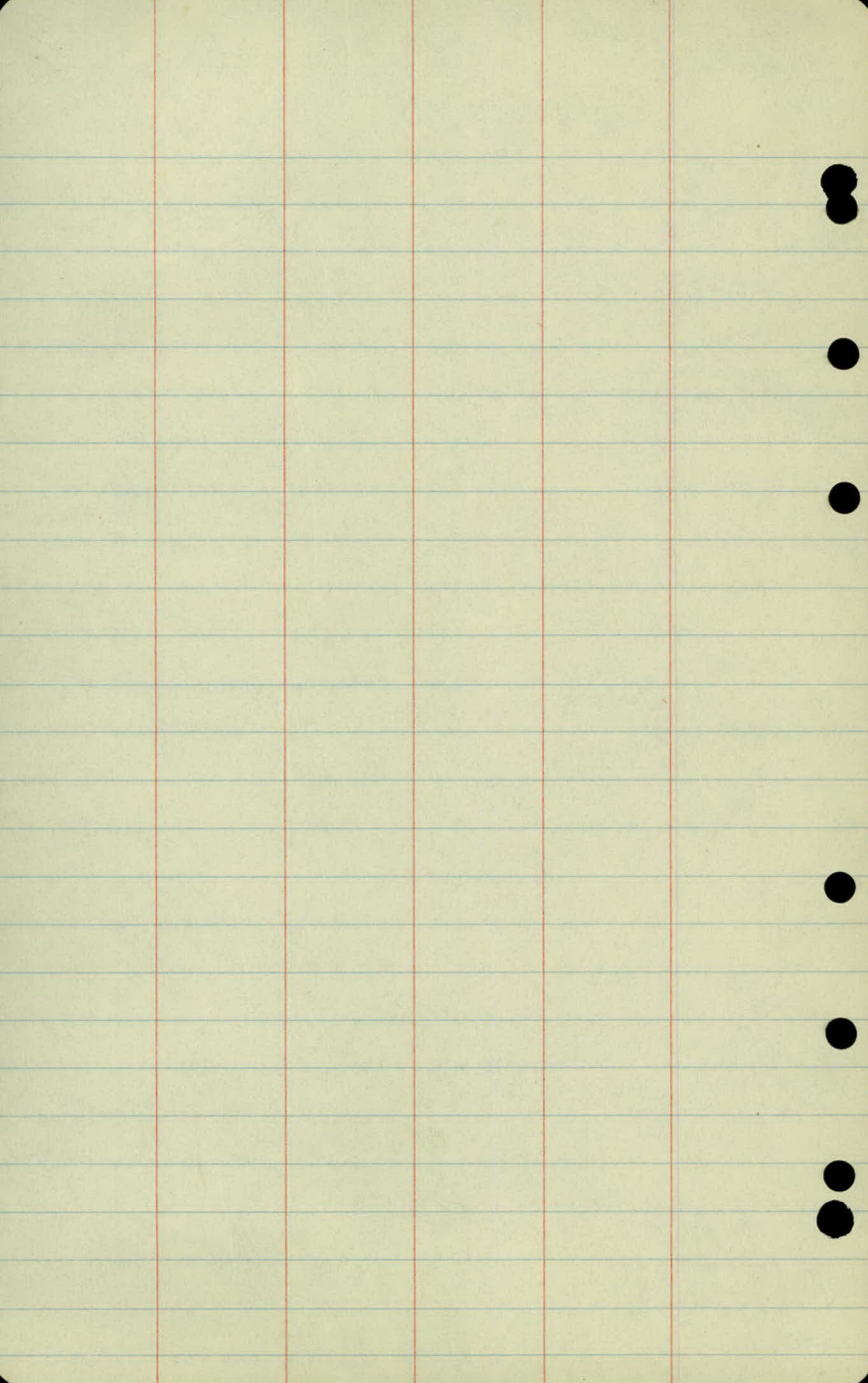
9.0
11.0

Has
been
Set

13.2
F 4.1

13.1
F 4.1
21.2

Spike 18" Oak - 60' Lt. Sta. 23+65



Gransie Road Bench Levels ^{4/37}

Sta. 0+00 Victoria St to Sta 10+25

<u>Sta.</u>	<u>+</u>	<u>π</u>	<u>-</u>	<u>Elev</u>
B.M.				973.43
B.M.	13.39	936.8V	8.49	978.33
T.P.	8.49	936.8V	1.05	935.77
T.P.	13.06	948.83	0.93	947.90
T.P.	13.10	961.00	1.29	959.71
B.M.	13.43	973.14	10.15	962.99
T.P.	10.15	973.14	3.09	970.05
B.M.	10.42	980.47	2.36	978.11

Nail in 6" Oak 2' Lt. Sta 10+25

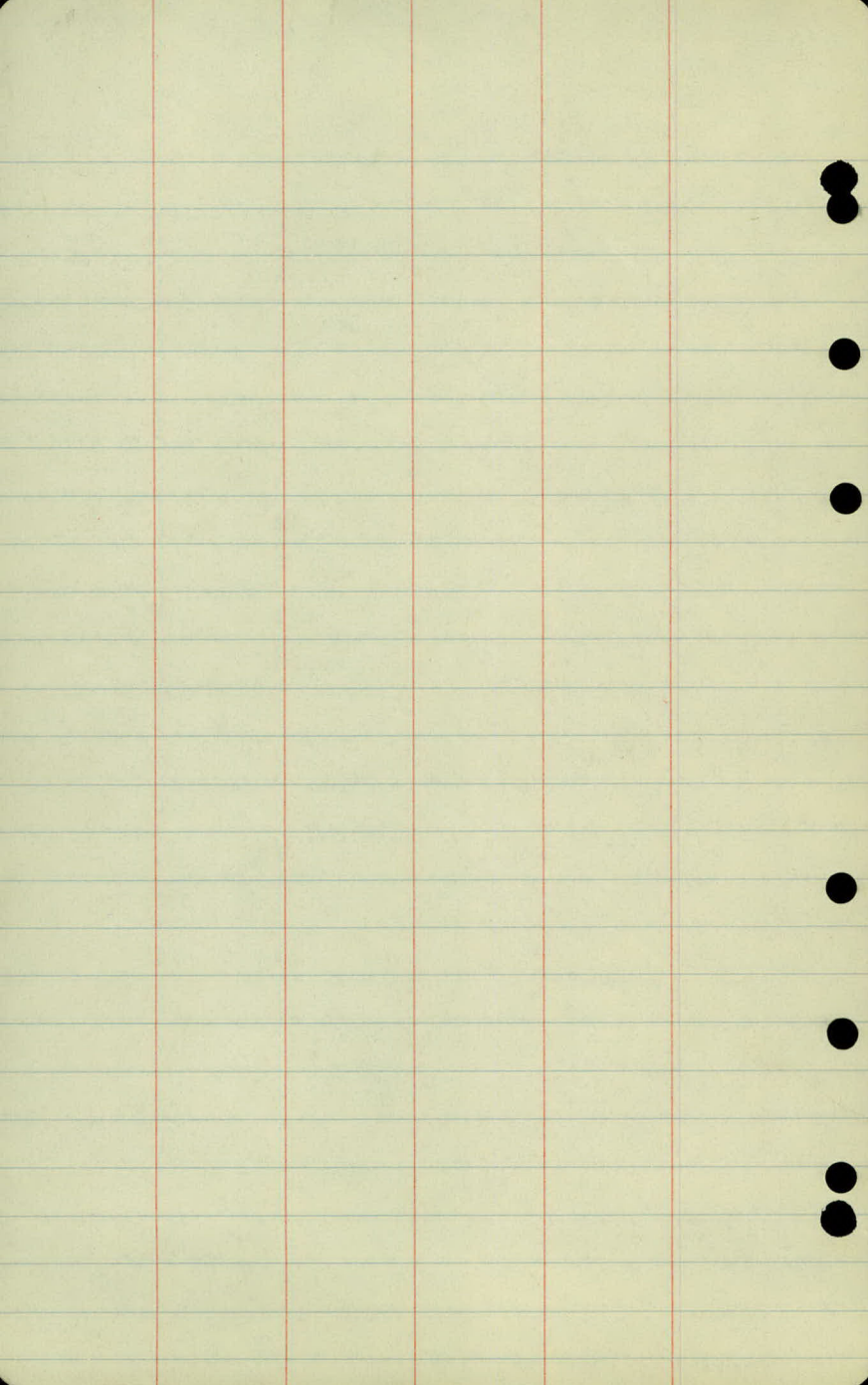
Top of granite boulder 150' Lt. Sta 8+50

Nail in Fence Post

Top of Boulder on E

Nail in Fence Post 100' Rt. 7+00

Spike in T.P. 125' Rt. Sta 0+00 Victoria St.



Lude Plugs
Grassie Road

Sta. + π - Elev. *Gravel Road*

B.M. 2.82 891.03 888.21 888.2

34 86.2 4.8

+50 86.0 5.0

35 85.8 5.2

+60 $4/3/37$ 85.6 5.4

36 85.5 5.5

+50 85.4 5.6

37 85.3 5.7

+25 85.2 5.8

Quinn
changed back off line
previously

Sta.	+	π	-	Elev.			
	5.55	989.91		984.36			
26				22.1	20.1	9.8	9.4
25				22.3	20.3	9.6	
24				22.4	20.4	9.5	
23				21.7	19.7	10.7	

Cranston Road

Blue Tops

5/19/
37

Sta	+	X	-	Elev.
B.M.	3.41	888.84		885.43

37+25.75

38

38+25.75

=
0+00

85.0 3.8

+50

84.9 3.9

1

84.8 4.0

+50

84.7 4.1

2

84.7 4.1

+50

84.7 4.1

3

84.7 4.1

+50

84.6 4.2

4

84.6 4.2

B.M.
412 v. 50' Rt.

885.43

Sta. + T - Elev.

Spike in 12" oak

4+50 888.84 84.6 4.2

5 84.6 4.2

+50 84.7 4.1

T.P. 3.59 888.33 4.10 884.74

6 84.8 3.5 3.3

+50 84.9 3.4 3.2

7 84.9 3.4 3.2

+50 85.0 3.3 3.1

8 85.0 3.3 3.1

+50 85.1 3.2 3.0

9 85.1 3.2 3.0

+50 85.2 3.1 3.0

10 85.2 3.1 3.0

+45 85.2 3.1 3.0

Sta.	+	Σ	-	Elev.		
		888.33				
11				85.3	3.0	2.8
+50				85.3	3.0	2.7
12				85.5	2.8	2.4
+50				85.9	2.4	2.0
13				86.7	1.6	1.3
T.P.	10.61	897.66	1.28		887.05	
+50				87.7	9.9	9.8
14				89.0	8.6	8.5
+50				90.4	7.2	
15				91.3	5.3	
+50				94.3	3.3	3.2
		907.62 11.08 896.54 896.51				
16		B.M.		96.5	1.1	1.0
T.P.	10.96	907.62	1.00		896.66	
+50				98.7	8.9	8.8

Sta. + X - Elev.

907.62

17

00.9 6.7 6.6

+50

03.1 4.5

18

05.3 2.3

T.P.

14.22

919.74 0.10

907.52

+50

07.5 12.2

19

09.7 10.0

+50

11.9 7.8

20

14.0 5.7

+65

16.4 3.3

21

17.5 2.2

+50

18.9 0.8

T.P.

8.14

927.09 0.79

918.95

22

20.0 7.1

+50

21.0 6.1

Sta. + π - Elev.

927.09

23 21.7 5.4

+50 22.1 5.0

24 22.4 4.7

+50 22.4 4.7

25 22.3 4.8

+50 22.2 4.9

26 22.1 5.0

+37.75 22.3 4.8

B.M. 2.70 924.39 924.36

Mr. Hoss:-

Culverts required on Grams Road.
Between Sta. 0+00 & Rice

2+20 - Present culvert 24" x 48' Conc. pipe.
Extend 4' on each end.

9+40 - Side culvert on Lt. 15" x 20' C.M.
Remove & use elsewhere.

9+90 - Place 12" x 12' side culvert on Rt.

⁰⁰
12+25 - 24" x 36' Conc. pipe in place.

^{Post}
_{Box} Pipe badly bowed in center.
Relay & extend 4' on each end.

Between Sta. 0+00 (Victoria St.) & Sta. 38±.

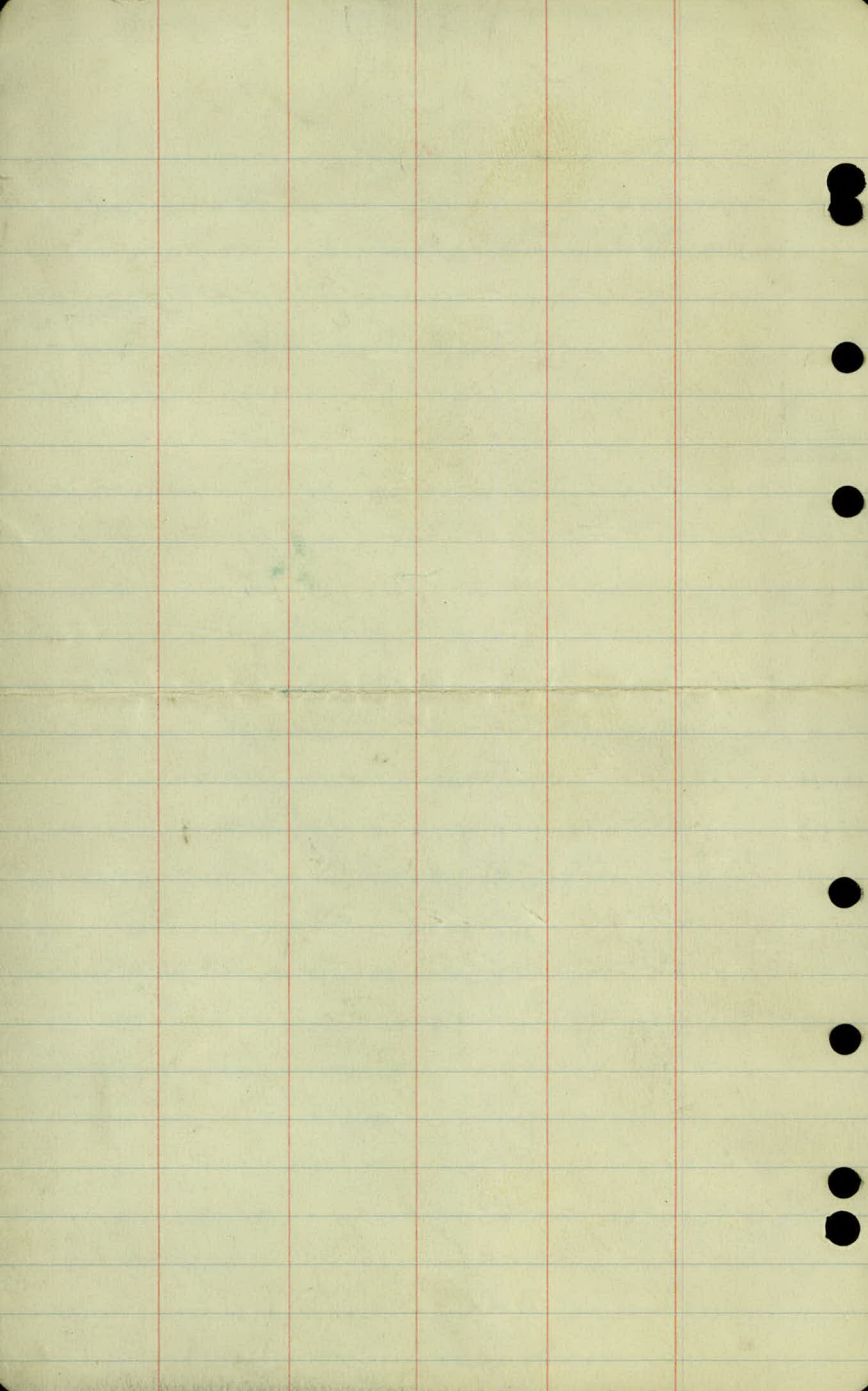
No grading { 0+20 (Victoria St.) Place 15" x 34' C.M.
25 to 30 ft. {
0 to 18 { ¹⁵
12+50 Place 24" x 64' Conc. Pipe

20+95 Place 24" x 64' Conc. Pipe

28+95 ~~29+50~~ Place 24" x 4³4' Conc. Pipe

✓ 33+75 Place 24" x 40' Conc. Pipe

37+50 Side culvert on Rt. Place 15" x 20'
C.M. (Pipe on Hand)



1
GRAMSIE RD.

800' West of Vivian to
' East of Vivian

7 pages

Rec 1/22/57
Z.C.

plotted
1/22/57

Sta + π - Elev

B.M. 11.68954.29

(942.61)

T.P. 12.86966.88 0.27 954.02

" 12.48978.57 0.79 966.09

" 0.98967.10 12.45 966.12

Iron $\angle$ Gramsie & Vivian 4.39 962.71

B.M. 3.08964.02

FK
RG
KP
WH

Jan 11, 1957
Clear Cold. 15°

2

Water surface Island Lake

Spike in 20" Oak 150' N. of Vivian & Gramsie

Sta	+	π	-	Elev
BM	8.31	954.75		946.44

0+00			0.5	54.3
------	--	--	-----	------

+50			4.5	50.3
-----	--	--	-----	------

/			6.6	48.2
---	--	--	-----	------

+50	Edge Lowland		9.3	45.5
-----	--------------	--	-----	------

2	Edge of Ditch		10.4	44.4
---	---------------	--	------	------

+05	Edge of Ditch on Ice		10.5	44.3
-----	----------------------	--	------	------

+12	Edge of Ditch		10.2	44.6
-----	---------------	--	------	------

+50	Edge of Cornfield		10.4	44.4
-----	-------------------	--	------	------

3			9.9	44.9
---	--	--	-----	------

FK W
RG ϕ
AP π
WH RG.

£ Jan 22, 1957
Cold Windy 0°

3

Island Lake outlet stadia D K.

Sta	+	π	-	Elev.
		954.75		
3+58			7.8	45.0
4			8.9	45.9
+11	Fe Cor.		7.8	47.0
+42			5.7	49.1
+61			4.0	50.8
TP	9.96	964.25	0.46	954.29
+86			8.0	56.3
5			7.4	56.9
+45			6.2	58.1

Jan 22, 1957

4

Sta	+	π	-	Elev
-----	---	-------	---	------

964.25

5+57			6.6	57.7
------	--	--	-----	------

6			9.7	54.6
---	--	--	-----	------

+14			10.4	53.9
-----	--	--	------	------

+16	Ex-Ditch		11.7	52.6
-----	---------------------	--	------	------

+23			10.1	54.2
-----	--	--	------	------

+30	Point at Which a x-Drain should Be placed at 45° Angle or 30° Angle			
-----	---	--	--	--

+53			9.2	55.1
-----	--	--	-----	------

+79			5.2	59.1
-----	--	--	-----	------

7			2.9	61.4
---	--	--	-----	------

BM	7.51	971.53	0.30	963.95	964.02
----	------	--------	------	--------	--------

Jan 22, 1957

5

Spike in 20" oak 150' N. of $\pm$ Vivian & Gramste

Sta + π - Elev

971.53

7+0.5 at Iron & Vivian 9.4 62.1 (62.1)

+30

9.1

62.4

+50

8.8

62.7

8

8.5

63.0

+50

8.8

62.7

9

7.2

64.3

Jan 22, 1957

6

Lt

Σ of Grams
as Graded

59.1
12.4

62.4
9.1

59.1
12.4

62.7
8.8

59.8
11.7

62.8
8.7

66.9
4.6

Sta + π - Elev

971.53

9 + 21

+60

+92

Lt

£ Jan 22, 1957

7

68.7
2.8

70.5
1.0

71.5
0.0

