Book - 1 - Dr. 11-A

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

CEMETERY RD.

From Fairchild Ave. To Long Lake Rd.

Road Acc't. No. M 1

Date Filed 11-8-29 File M-V Twp.

PROJ. 29-MI

Plans for Survey
Cemetery Road
Mounds View Twp. Sept. 1929

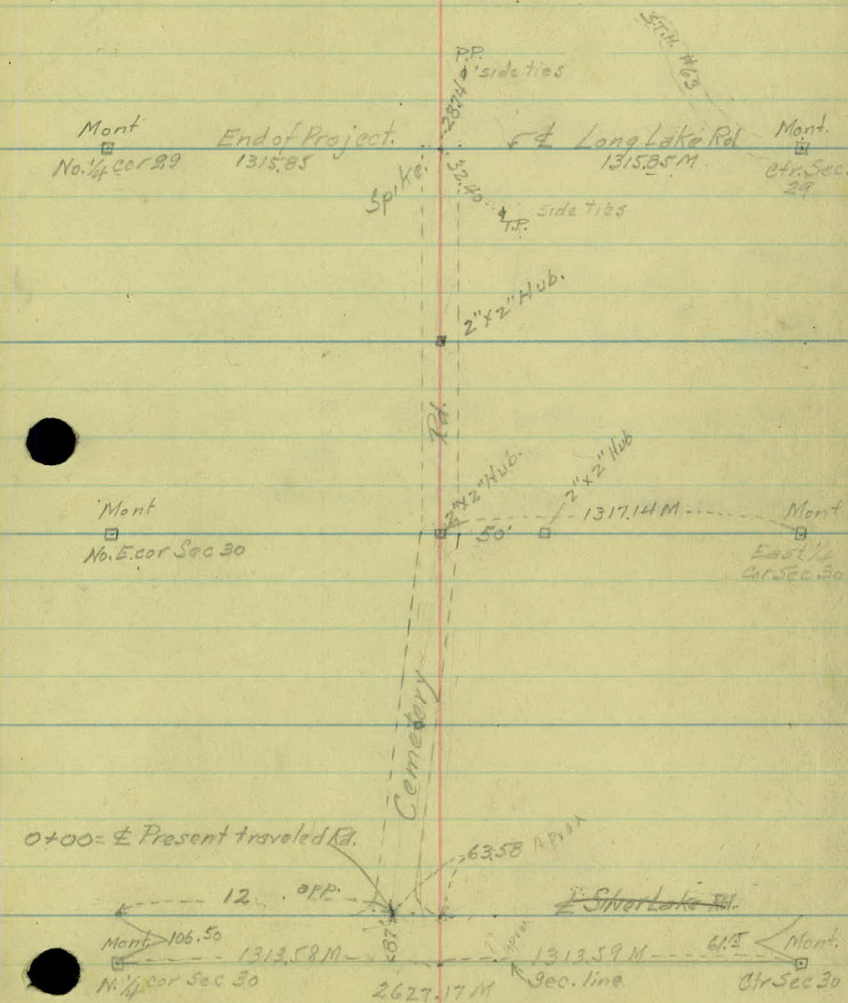
Proj 29-M1

From Fairchild Ave to Lodge Lake Road.

Sta.	Δ Lt	Δ Rt.	
52+53.64	End of Project		
42+00	P.O.T.		
25+57.05	> Equation 25+57.05 = 26+40.<		
8+36.36	P.O.T.	2"x2" Hub	
0+00	= a point	So. of N. ¼ cor. Sec 36	

Sept 10-11
Rainy weather.

X Weber
Beeton
Jim Bell



Topography Survey
Cemetery Road.
Mounds View Twp.
Sept. 18th 1929
Weber
Beaton
Bell.

7

6

5

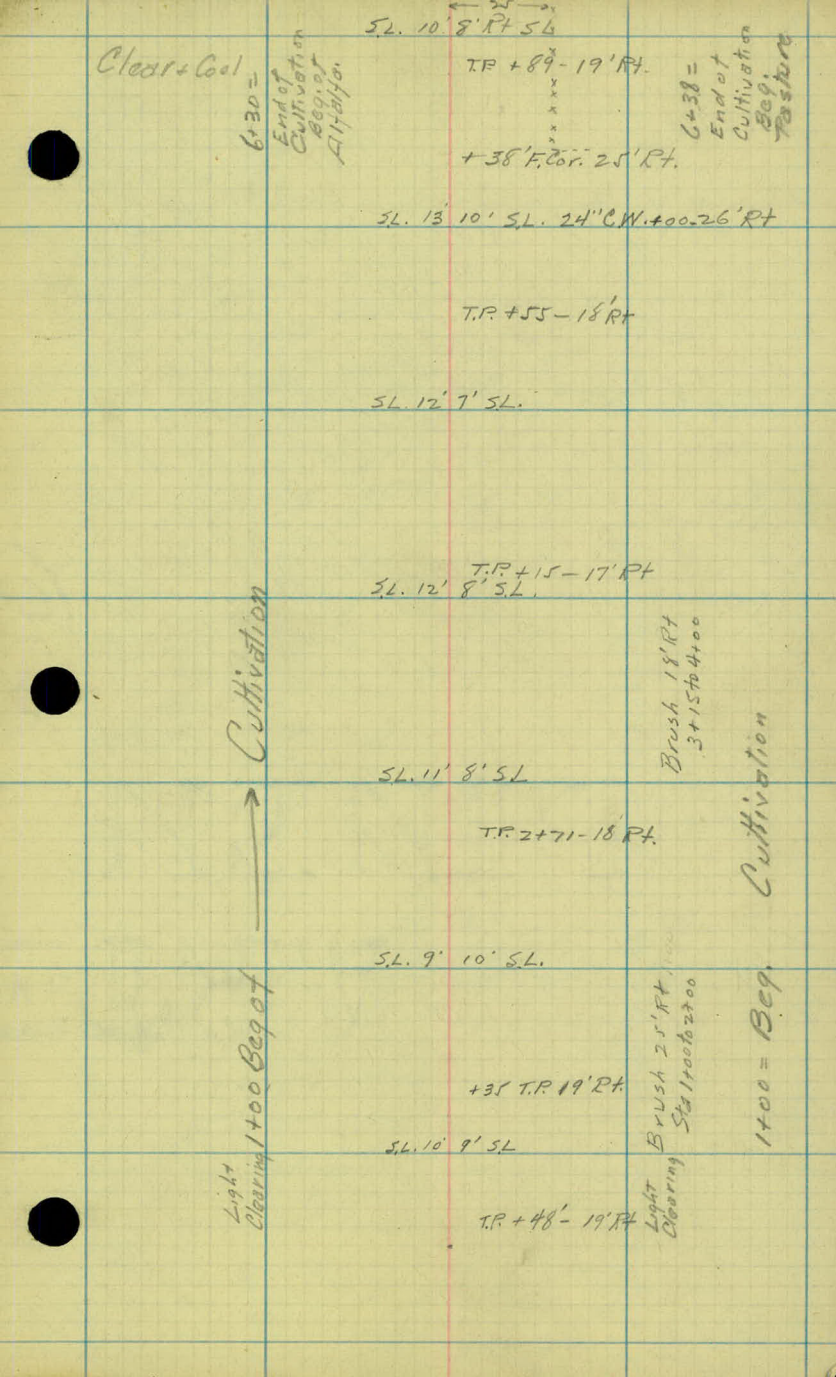
4

3

2 S.L. = Shoulder line.

1+00

0+00 ℄ Silver Lake Rd.


S.L. 10' 8' Rt S.L.
Clear & Cool
6+30 = End of Cultivation Beg. of Alfalfa
T.P. +89 - 19' Rt.
+38' F. Cor. 25' Rt.
6+38 = End of Cultivation Beg. Pasture
S.L. 13' 10' S.L. 24" C.W. +00-26' Rt
T.P. +55 - 18' Rt
S.L. 12' 7' S.L.
T.P. +15 - 17' Rt
S.L. 12' 8' S.L.
Cultivation
Brush 18' Rt 3+15 to 4+00
S.L. 11' 8' S.L.
T.P. 2+71 - 18' Rt.
S.L. 9' 10' S.L.
Cultivation
1+00 = Beg.
Light Clearing 1+00 Beg of
+35 T.P. 19' Rt.
Brush 25' Rt. Sta 1+00 to 2+00
S.L. 10' 9' S.L.
Light Clearing
T.P. +48 - 19' Rt

22

21

20

19

18

17

16

15

14

13

12

11

10

9

8

S. Line.

12' 3' Fence 30' Rt.

Private Drive +82

T.P. +63 – 16' Rt.

12' 3' Fence = 32' Rt.

19+00 = Starting Cultivation

T.P. = +24 – 20' Rt.

9' 6' Fence 32' Rt.

Pasture.

10' 7' Fence = 34'

Fence – +97 – 34' Lt Cor.

T.P. + 86 – 24' Rt

Fence = 26' Lt 10' 6' Fence = 34' Rt

+91 = 30" C.W. 28' Rt

Heavy Brushing 16+80 To 17+20 14' Lt

Fence cor +20 34' 20' Lt

10' 6' Fence 17+00 34' Rt

T.P. 17+00 – 25' Rt

Light Brushing +30 To 17+20 15' Rt.

+75 = 2-6" Will 15'

+55 = 2-6" Willows 15 Rt

+30 = 6" Will 13' Lt

+00 Brush 14' Lt 11' 4'

+64 – 10" Oak 28' Lt

+35 Brush 16' Rt.

+25 T.P. 24' Rt.

35' F. +25 Clump Oaks 11' Rt.

11' 5' Fence 31. Rt

+50 = 10" Oak 31. Lt

8' 6' Fence

31' T.P. 85' – 23'

F.E. +15

Brush 12+41 To 12+80 25' Rt.

30' Fence

Brush 13+15 To 13+60 15' Rt.

Brush 12+20 to 12+35 15' Rt.

11' 10'

T.P. +41 – 22' Rt.

10' 5'

23'

T.P. +12 – 22' Rt

11' 7'

23'

Pasture

Alfalfa.

23'

11' 6'

+72 – T.P. 21' Rt.

+70 = 10" Oak 30' Lt

11' 8'

23' Fence

+27 – T.P. 19' Rt

10' 6.

23' Fence.

36

35

34

33

32

Culvert with Concrete abutments 1'x11'
= 30" x 30" C.M.

31

30

29

28

27

26

25

24

23

Cultivated

Light Clearing

10'x10'

6'13'

7'x13'

+90 Clump 3 oaks 16'24 ave. 7"

+06.0 = Light clearing

7'12'

+28 T.P. 38' Rt.

10'x9'

[18' - 12'] +85'

5'12

Cultivated

+82 T.P. 3# Rt.

3'x15'

+20 T.R. 26' = (City Dump)

3'15'

Hay Meadow = 29+00 To 33+00

Borrow Pit +25' Thick

+80 to 29+03. Clearing.

4'x13

+81. TP - 22' Rt

+43. = 8" Oak 13' Lt

4'13.

+82 - 34' Rt = End of Fence.

+57 T.P. 18' Rt.

Cultivated

Equation

8'10' Fence 33'

+50 Brush 20' Rt

+40 T.P. 15' Rt

Pasture.

10'x6' Fence 38'

+95 Bush 12' Rt

+33 Bush 20' Rt

17' 5' T.P. +01.0 - 13' Rt Fence 32' Rt

50

49

48

47

46

45

44

43

42

41

40

39

38

37

49+20 Beg. Cultivation
50+85 = End Cultivated

47+60 = Beg. Orchard

Row 7 Apple Trees 45 Lt.

+15 = 8" B.E. 18' Lt
+05. = 8" B.E. 18' Lt

+42 T.P. 18'

4' 11'

5' 10

+94 - T.P. 18'

7' 8'

+60 F. Cor. 25'

+44. T.P. 18'

24' 11.7

+83 = F.E.
+63 F.C. 24' Lt.

Pr. Drive

8' 7'

+93 - T.P. 18' Rt.

(Homestead)

8' 7'

+37 - T.P. 17 Rt.

Pr. Drive + 19

44+00 = End of Trees. 9' 8'

Pr. Drive + 40

42+82 = Beg. Cultivated Field To End of Proj.

42+88 = Row of 7 - 12" B.E. 20' Lt. 11.7
+76 - Private Drive
+37 - Pier 31' Lt.
End Cemt.
+67 - 2 - 6" Oaks 26' Lt.
Pier
+82 T.P. 17' Rt.
+72 Side Rd.
+21 = 12" Oak 21'
+13 = 12" Oak 31' Rt

Cemetery

12 5

+46 = 31' Lt Pier

2'x2' Brick Piers

+29 T.P. 17 Rt

12' 4'

+97 - 31' Lt
Drive + 89 Lt.
+81 - 31' Lt Pier
+21 = 24" C.W. 33' Lt

11 7'

39+72 - 24" C.W. 33' Lt.
Cor. Fence Pier + 48 - 31'
+72 T.P. 23 Rt
+53' Side Road.
+37 Side Road

+53 Ctr. = 10" C.M. 30 Long 12' Rt.

42+00 = End Clearing

10' 10'

+19 T.P. 30' Rt

8' 12'

Cultivated

Light Clearing

8' 12'

+

52

51

End of Project.
+35 T.P. 26

9' 8'

+57 = Pr. Drive +96 T.P. 17 RH

+05. ≤ Pr. Drive

5' 10'

Sta	+	H.I.	−	Elev		
	11.52	992.24			980.72	T.P
T.P.		✓	2.76	989.48		T.P.
T.P.	11.68	1001.16				
0+00					91.2	
+080					90.7	
+12					90.6	
+17					90.3	
+31					89.5	
+50		✓		✓	87.7	
T.P.	0.0	988.62	12.54	988.62		
1+00		✓		✓	82.1	
T.P.	1.0	976.85	12.77	975.85		
+50					75.4	
2					70.2	
+50		✓		✓	66.2	
T.P.	0.42	964.63	12.64	964.21		
3					62.0	
+50		✓		✓	57.7	
T.P.	3.05	958.67	9.01	955.62		
4					55.4	
+50					54.2	
5		✓		✓	53.5	
B.M.	7.46	959.56	6.53	952.14	952.10	
+50					54.1	
6		✓		✓	55.3	
T.P.	9.91	968.71	0.52	958.74		
+25					56.2	

Sept 13-29 Lt — Cold + Rainy ℄ — Rt. — ⊼ Weber, Rod Beaton, Jim Bell

B.M. spike in T.P. 150' Lt of Sta 0+00

Top of Sta 30' No. Sta 0+00

13.8/80 12.0/50 10.2/8 9.9 9.4/15 8.7/50 8.2/80

14.3/80 12.5/50 10.8/9 10.5 10.0/17 9.2/50 8.8/80

14.8/80 12.8/50 11.0/15 11.5/13 11.2/11 10.6 10.3/26 10.5/31 9.8/36 9.8/50 9.2/80

2.6/80 5.5/50 5.0/34 7.5/15 11.8/10 11.3/7 10.9 10.8/21 11.3/23 11.3/25 9.6/28 5.5/32 5.1/40 7.0/80

7.4/80 4.7/50 4.2/29 8.6/14 12.8/10 12.8/8 12.1/7 11.7 11.9/15 12.7/16 12.7/18 10.1/21 5.9/30 7.2/50 8.6/80

9.9/80 7.2/50 6.4/30 10.2/24 13.1/13 14.5/10 14.5/8 13.7/6 13.5 12.7/11 14.6/13 14.6/15 13.0/18 13.0/24 8.7/29 12.0/50 14.0/80

5.4/80 5.1/50 4.8/30 6.1/25 5.3/17 7.2/12 6.5 7.2/14 8.2/20 7.9/31 9.2/50 11.1/80

1.8/40 1.8/14 5.7/27 4.8/14 2.2/9 1.5 2.6/10 6.9/16 6.8/40

L.O. 5.7/40 6.8/32 8.9/26 9.2/16 7.2/7 6.7 7.2/9 11.0/16 10.0/40

10.8/40 10.2/30 11.8/25 11.0/16 12.0/14 10.7 11.6/12 10.9/13 13.2/22 10.0/29 10.0/40

2.0/40 1.0/30 2.0/23 2.4/21 2.4/17 3.9/13 3.2/10 2.6 3.6/9 3.3/13 2.2/14 2.6/19 4.4/22 2.1/26 -1.0/40

7.8/40 7.5/27 9.2/24 9.2/22 7.8/20 7.7/18 8.6/17 8.6/15 7.0/11 6.9 7.3/7 8.7/10 8.7/12 7.3/15 9.9/19 9.9/22 5.7/28 3.2/40

9.8/40 8.4/17 4.2/12 3.3 3.6/8 7.4/15 8.3/26 7.0/31 5.1/38 5.1/40

14.7/40 13.0/23 5.0/10 4.5 4.7/6 10.6/15 11.0/30 10.6/40

14.3/40 13.7/24 5.4/12 5.2 5.1/5 13.4/19 13.0/40

Spike in 24" Cottonwood 25' Rt Sta 6+00

7.4/45 8.0/40 8.6/35 7.8/17 6.1/14 5.5 5.6/7 14.2/19 14.2/25 11.9/40 L.O.

16.3/60 12.2/50 9.1/35 5.8/21 4.7/13 4.3 4.6/10 7.3/15 8.5/28 8.5/40

7.3/[illegible] 7.0/37 9.1/21 13.5/19 13.5/12 12.8/9 12.5 13.0/10 13.5/15 13.5/17 12.5/18 11.8/40

Sta.	+	H.I.	−	Elev	
		968.71			
6+50					57.1
7					58.4
+50					57.9
8					58.3
+50					57.1
T.P.	0.98	958.08	11.61	957.10	
9					55.3
+50					53.6
10					51.2
+50					49.5
11					47.2
+50					44.0
T.P.	3.56	948.55	13.09	944.99	
12					40.8
T.P.	2.27	937.98	12.84	935.71	
+50					36.9
13					33.5
T.P.	6.54	934.39	10.13	927.85	
+50					30.2
14					26.9
+50					23.0
B.M.			6.50	927.89	927.90
15					19.9
T.P.	0.83	922.49	12.73	921.66	
+50					17.2
16					15.5

Lt [illegible] & Rt π Weber

Sept 14-29 Clear. Rod. Beaton

5.7/40 4.9/35 5.4/25 12.7/17 12.7/14 11.9/10 11.6
12.3/16 11.5/22 5.8/24 4.9/36 5.3/40 L.O.

3.4/40 2.0/32 2.0/23 8.2/19 11.2/14 10.5/9 10.3
11.1/13 1.5/25 1.5/40 L.O.

5.7/40 4.9/33 4.7/22 10.3/15 20.0/8 10.8
10.2/12 4.8/18 4.5/40 L.O

7.2/40 6.6/35 7.1/23 11.1/17 10.4
11.4/11 9.5/19 9.9/29 9.1/40

S.S. 11.0/40 11.7/23 12.7/19 12.7/9 11.6
11.6/2 12.7/11 10.3/13 11.8/40

3.0/40 2.3/33 1.6/20 3.6/18 2.8
3.6/12 0.7/14 0.7/26 0.0/40

5.3/40 3.8/32 3.6/22 5.6/19 4.6
5.0/8 5.7/10 5.7/13 3.9/14 3.9/16 2.5/19 2.3/28 1.3/34 1.3/40

14.1/40 13.5/23 8.6/15 7.2/9 6.9
8.7/12 8.1/24 4.9/36 4.8/40

9.7/40 9.3/35 10.4/24 10.1/17 8.7/7 8.6
9.3/15 8.7/27 6.5/35 6.5/40

6.3/40 5.5/33 6.0/23 10.5/19 10.5/14 11.5/12 10.9
11.2/10 7.1/16 7.7/24 10.5/40

Lt. S.S 7.4/41 6.7/35 7.4/25 14.0/9 14.1
14.4/4 11.5/10 8.6/12 6.4/15 6.5/24 7.8/40 Rt

2.2/40 1.7/34 3.5/18 7.9/13 7.8
7.8/7 4.8/10 3.7/15 3.7/23 4.3/40

0.0/40 0.3/33 2.3/23 2.1/16 1.3/14 1.1/11 1.1
1.4/9 2.9/15 3.8/31 3.8/40

6.7/40 6.4/33 8.4/24 8.4/19 4.9/9 4.5
5.0/10 6.1/13 4.9/30 3.8/33 4.2/40

5.1/40 4.8/32 5.9/29 6.1/18 4.4/9 4.2
4.7/8 5.3/11 2.9/30 2.0/35 2.0/40

5.3/40 7.2/33 7.1/19 8.0/18 7.5
8.3/11 6.8/12 3.9/34 3.7/40

8.7/40 7.8/22 12.0/19 11.4/10 11.4
11.8/11 10.9/25 10.6/20 8.0/24 3.4/31 1.7/40

Spike in 12" B.O. 40' Lt 5+B. 14+50

11.8/40 11.3/21 12.4/24 15.6/19 15.6/14 14.8/11 14.5
14.3/18 12.6/21 12.6/24 9.5/29 7.6/35 7.7/42

Top of Stake.

7.0/40 7.8/35 8.7/32 8.2/17 6.4/14 5.2/10 5.3
5.5/4 9.1/11 10.8/26 10.2/40

12.3/40 12.0/18 3.0/10 7.0
7.3/4 13.0/13 14.0/40

Sta	+	H.I.	—	Elev	
		922.49			
T.P.	5.00	919.87	7.62	914.87	
16+50					14.6
T.P.	4.42	918.72	5.57	914.30	
17+00					13.9
T.P.	8.60	923.52	3.80	914.92	
+50					13.0
18					12.0
+50					10.5
T.P.	4.97	915.79	12.70	910.82	
19					07.8
+50					05.3
20.					02.6
T.P.	2.77	905.71	12.85	902.94	
+25					901.9
+50					899.5
21.					96.0
+50					93.2
T.P.	0.35	893.85	12.21	893.50	Rock
	0.16	890.71	3.30	890.55	Pole.
22.					89.8
+50					87.8
23					86.4
+50					85.5
24					85.3
+50					85.8

Lt ℄ Rt 9-6

11.7/40 11.7/28 11.2/18 6.0/10 5.3 5.6/5 10.7/13 11.8/22 11.3/40

9.9/40 8.0/16 5.4/11 4.8 5.0/7 7.4/13 6.1/30 4.3/40

11.4/40 9.1/28 9.7/24 8.5/21 11.0/17 10.5 10.5/12 7.4/15 6.8/22 3.2/30 2.6/40
7.5/40 6.4/34 6.9/23 11.9/17 11.5 11.3/13 9.6/15 9.0/20 2.2/30 1.0/40
10.1/40 8.6/34 8.6/30 13.3/21 14.2/14 13.0 13.6/18 10.7/23 7.2/30 2.3/34 L.0.

4.3/40 2.7/32 8.3/26 9.0/17 8.2/14 8.0 7.9/17 6.0/20 5.4/23 0.0/30 L.0
8.3/40 7.8/30 6.8/29 7.1/24 11.1/20 10.5/16 11.3/14 10.5 10.5/18 8.8/24 4.3/29 3.5/35 4.0/40
13.2/40 13.2/29 12.3/28 12.3/21 14.0/18 13.2 14.5/21 9.5/26 8.4/35 L.0

4.5/40 4.7/29 3.7/28 3.3/20 4.6/18 3.8 4.5/13 1.6/15 0.2/38 0.7/40
6.4/40 6.6/29 5.8/28 5.2/19 6.8/17 6.2 6.6/10 4.7/13 3.8/40
10.6/40 10.7/30 9.8/27 10.0/20 10.7/17 9.7 10.2/32 L.0
13.2/40 13.8/18 13.4/9 12.5 14.2/11 14.5/30 13.6/34 14.0/40

1.9/40 1.1/10 0.9 1.8/9 2.3/29 2.3/40
4.3/40 4.2/19 2.7/7 2.9 3.6/25 2.3/27 2.3/40

6.4/40 6.6/15 4.2/9 4.3 4.3/5 5.9/9 6.2/22 5.2/26 3.3/35 3.8/40
8.1/40 7.8/26 8.4/24 8.9/16 5.2/11 5.2 5.0/6 8.1/12 7.8/16 8.3/36 6.3/40
8.6/42 9.4/40 10.1/28 8.8/16 6.2/12 5.4 6.1/7 9.6/12 11.2/21 L.0
8.7/40 8.2/25 7.7/16 6.2/13 4.9/6 4.9 4.9/4 6.0/9 8.0/13 8.6/32 8.3/40

				Elev	
		890.71			
25					87.7
T.P.	11.92	899.61	3.02	887.69	
+50					89.4
25+57.05 = 26+40.0					
-27					91.0
+50					90.7
~~+50~~					
28					88.9
T.P.	6.18	895.52	10.27	889.34	
~~+50~~					
+60					85.7
+67					~~84.8~~
T.P.	1.54	885.38	11.68	883.84	
29					83.5
+50					81.3
30					79.6
+50					78.1
T.P.	6.59	884.19	7.78	877.60	
31 ~~32~~					77.4
+50					77.3
~~+50~~			Co. Ditch		~~77.5~~
32					77.8
+50					79.3
33					80.9
T.P.	8.84	892.25	0.78	883.41	
+50					83.3

Lt & Rt

3.6 4.0 3.2 3.0 5.2 4.1 5.0 4.5 5.0
40 23 12 80 13 20 30 40

6.8 6.2 7.5 10.0 10.2 10.3 8.7 7.6 9.0
40 17 11 6 15 17 33 40

2.6 2.3 6.9 8.6 8.6 8.5 6.7 3.3 2.5 4.0 4.9
40 15 8 3 18 20 26 30 37 40

3.7 2.9 6.4 7.1 8.6 8.9 9.1 7.3 6.6 4.6 4.7 4.0 4.8
40 16 7 9 7 19 20 22 25 31 33 40

Lt only. ~~4.4 4.0 10.7 10.4~~
40 3 8

13.8 12.1 12.0 10.6 10.7 10.8 3.8 3.8
40 25 12 8 18 27 40

~~7.0 7.1 4.9 5.6~~
11
21 40

L.O. 18.0 9.8 8.4 9.8 10.0 8.2 7.5 7.6
40 28 14 17 22 35 40

10.7 10.4 4.8 4.5
19 27 40

3.9 2.7 1.9 2.0 2.7 8.1
40 9 19 32 40

7.4 7.0 4.4 4.1 4.9 7.2 9.7
40 9 3 19 25 40

7.9 9.0 7.1 5.8 6.2 9.5 10.0
40 8 5 15 23 14

9.0 9.1 7.4 7.3 7.6 9.9 10.0
40 7 3 14 17 40

7.8 8.7 7.0 6.8 6.6 8.2 9.0
40 9 6 11 14 40

9.4 8.8 7.2 6.9 7.1 9.9 10.3 9.4 9.0
40 12 8 7 10 7.2 13 40

Flexline 14.5 10.7 7.9 8.2 6.7 13.2 ~~Flexline~~
18 14 8 7 6 13

10.9 9.6 6.8 6.4 6.8 8.8 9.3
40 14 10 5 12 40

9.2 8.9 5.4 4.9 5.6 8.1 8.8
40 15 8 10 14 40

7.9 6.8 4.0 3.3 3.6 5.3 6.6
40 13 8 13 16 40

11.7 11.0 9.7 9.0 9.4 10.6 10.7 10.2
40 11 8 14 19 34 40

	+	892.25 −	Elev	
34				85.7
+50				88.6
35				91.6
T.P.	9.65	901.66	0.24	892.01
+50				94.6
36				97.2
+50				899.3
T.P.	11.16	912.76	0.06	901.60
37				900.9
+50				02.6
38				04.2
+50				06.0
39				08.0
+50				10.3
T.P.	11.01	922.05	1.72	911.04
40				13.0
+50				15.8
41				18.4
B.M.	7.93	926.81	3.16	918.89	918.89
+50				20.2
42				21.8
+50				22.1
43				21.6
+50				21.6
44				21.6
+50				21.9

LT ℄ RT

8.9	7.4	6.5	6.6	6.4	8.0	6.1	6.3	7.6	7.6
40	9	8		13	28	32	38	40	42
5.4	4.7	3.7	3.7	4.2	4.4	4.2			
40	7	6		22	33	40			
11	12		0.7	1.2	0.9	1.3	0.4	0.4	
40	12			16	19	24	26	40	

6.8	5.9	8.4	7.6	7.1	7.0	7.6	7.6	6.8	7.2	8.1	7.6	5.9
40	14	12	10		4	4	6	9	16	18	20	40
	4.7	3.7	5.1	4.5	4.6	5.4	4.6	5.4	3.9	4.3	3.3	3.2
	40	14	12		4	5	6	19	19	26	30	40
2.5	2.4	2.9	2.4	2.7	2.1	3.2	1.7	1.7	1.2	1.2		
40	13	12		5	6	18	20	28	30	40		

12.0	11.5	12.2	11.9	11.8	11.4	12.2	10.7	11.4	10.3	10.4	
40	17	11		5	10	17	19	26	34	40	
11.2	11.0	10.2	10.4	9.8	10.7	10.0					
40	13		16	20	26	40					
10.0	9.6	8.6	9.0	8.4	9.1	9.1	9.1				
40	16		16	19	22	33	40				
8.5	7.5	8.0	7.6	6.8	7.3	7.0	6.7	6.7			
40	14	13	11		8	16	18	40			
6.3	5.5	5.0	4.8	5.1	4.7	4.8	5.3	4.8	4.8		
40	13	9		14	12	22	26	27	40		
2.0	2.1	3.3	2.5	1.8	1.3						
40	29	25		19	40						

8.9	9.3	9.8	9.3	9.1	8.8	9.5	8.9	8.5
40	19	17	9		4	13	15	40
6.0	5.9	6.9	6.3	6.3	6.0	6.8	5.7	5.7
40	19	17	10		4	12	15	40
	3.8	3.5		3.7	3.7	4.4	3.5	3.4
	40	7			3	13	14	40

Spike in twin C.W. 5.3 LT 5.4 RT 41+00

6.8	6.8	6.6	7.2	6.6	6.5	6.5	
40	18		12	13	20	40	
5.7	5.4	5.0	5.10	5.6	5.0	5.3	5.7
40	19	10		11	13	20	40
5.2	5.4	4.5	4.7	5.1	5.4	5.4	
40	31	12		14	27	40	
	4.9	5.4	5.2	5.2	5.8	6.2	
	48	10		5	10	40	
	5.9	5.6	5.2	5.1	5.8	6.3	
	40	11		6	12	40	
	6.0	5.8	5.2	5.2		6.2	
	40	11		8		40	
5.6	5.6	4.8	4.9	5.0	5.6	6.1	
40	12	7		7	13	40	

	+	926.81	−		
T.P.	0.16	924.10	3.27	923.54	
45					21.6
+50					17.7
46					15.3
+50					13.0
47					11.1
+50					09.9
T.P.	4.31	915.93	12.48	911.62	
48					11.7
+50					11.8
49					12.0
+50					11.4
50					10.9
+50					10.8
51					09.9
+50					08.8
52					08.3
+33		Toe of Slope			08.6
+43		Top Shoulder			08.9
+53.64			℄ Long Lake Rd.		08.7
B.M.			12.61	903.32	905.34

Lt. ℄ Rt.

2.4/40 2.3/15 2.7/11 2.5 2.7/8 3.3/13 5.4/40

3.2/40 3.4/15 3.9 4.4/19 5.7/40

5.3/40 6.2/14 6.7/12 6.3 7.0/19 7.9/40

8.9/40 8.6/19 8.6 8.5/5 10.0/17 11.2/40

11.3/40 11.3/21 10.5/10 10.5 10.4/6 11.9/19 12.4/40

13.2/40 13.2/14 11.8/8 11.7 11.6/7 12.9/14 12.1/15 13.0/22 13.6/24 13.2/40

6.0/40 5.6/12 4.3/5 4.2 4.3/8 5.2/13 5.7/40

5.2/40 5.2/27 6.0/22 5.9/15 4.3/5 4.1 4.4/9 5.1/40

5.2/40 5.3/22 4.2/7 3.8/5 3.9 3.7/9 4.1/28 4.1/40

6.5/40 5.7/19 5.1/15 5.0/8 4.6/5 4.5 4.6/15 4.2/16 3.5/40

7.5/40 6.3/26 5.8/7 4.8/4 5.0 4.6/11 5.1/13 4.3/40

5.9/40 6.4/31 5.3/23 6.5/20 6.0/8 5.4/5 5.1 5.0/10 6.0/20 5.1/25 5.5/40

6.4/40 6.3/19 6.0 5.7/8 6.2/17 7.0/14 6.9/21 5.6/25 6.1/40

7.0/40 6.8/21 7.9/16 8.1/11 7.0/5 7.1 7.1/7 8.7/13 9.0/23 7.4/27 7.6/40

8.6/40 8.6/21 9.4/17 9.6/13 8.0/10 7.6 8.0/8 11.0/14 11.3/20 10.3/22 10.1/40

13.2/40 13.0/35 10.3/22 7.4/16 7.3 7.9/11 11.0/13 13.1/40

7.2/40 7.3/29 7.4/16 7.0 7.9/12 7.6/28 7.8/40

6.8/40 7.1/20 7.2 7.3/20 7.5/50

Sp. in P.P. #9 - 30' East of end of Proj.

	+	H.I.	—	Elev.
B.M.				910.82
T.P.	8.29	919.11		
			0.25	918.86
" "	13.08	931.94		
			5.46	926.48
" "	0.74	927.22		
			11.21	916.01
" "	0.99	917.00		
			10.01	906.99
" "	6.75	913.74		
B.M			10.40	903.34
T.P.	12.45	915.79		
			4.01	911.78
T.P.	12.30	924.08		
			2.19	921.89
	3.04	924.93		
B.M.			6.04	918.89
			12.57	912.36
T.P.	1.26	913.62		
			12.90	900.72
T.P.	0.48	901.20		
			11.69	889.51
T.P.	0.43	889.94		
B.M.			1.34	888.60
			11.93	878.01
T.P.	11.85	889.86		
			0.50	889.36

Fair. Sept- 12-13

x Weber
Rod. Boston.

Top of Hyd. at intersection of #63 and Long Lake Rd.

Spike in P.P. #9 - 30' East of End Proj.
Sta. 52-53.64

Spike in Twin Cottonwood 53' Lt Sta. 41+00.

Spike in 18" Oak Sta 34+25 — 50' Rt.

	+	H.I.	−	
		889.86		889.36
T.P	3.85	~~893.71~~ ~~894.21~~		~~890.56~~ ~~891.06~~
			2.67	
TP	12.77	~~903.71~~ ~~904.21~~		
			0.28	903.03
TR	12.69	915.72 ~~916.92~~		
			0.40	915.32 ~~916.52~~
	12.97	928.29 ~~929.49~~		
B.M.			0.39	927.90 ~~929.10~~
			0.43	927.86 ~~929.06~~
T.P.	12.37	940.23 ~~941.43~~		
			0.23	940.00 ~~941.20~~
T.P.	11.68	951.68 ~~952.88~~		
			0.33	951.35 ~~952.55~~
T.P	11.46	962.81 ~~964.01~~		
B.M.			10.72	952.09 ~~953.29~~
	7.26	959.35 ~~960.55~~		
			0.29	959.06 ~~960.26~~
	11.90	971.96 ~~973.16~~		
			0.87	971.09 ~~972.29~~
	11.88	981.97 ~~983.17~~		
			0.58	981.39 ~~982.59~~
	12.99	994.38 ~~995.58~~		
			4.93	989.45 ~~990.65~~
	3.07	992.52 ~~993.72~~		
B.M.			11.82	980.70 ~~981.90~~

T.P. 20' Rt Sta 21+50

890.36
3.85
892.21

Spike in 12" B.O. 40' Lt Sta 11+50 929.10
929.10

Spike in 24" Cottonwood 25' Rt. Sta. 6+00

Spike in T.R. 150' Lt of Sta. 0+00 → No.

				Elev	
				918.89	
	1.95	920.84			
	0.32	909.08	12.08	908.76	
	0.39	897.05	12.42	896.66	
			8.46	888.59	888.60 orig
	7.55	892.01	12.59	884.46	
	8.99	896.66	4.34	887.67	
	12.53	903.07	6.09	890.57	890.54
	12.98	915.99	0.06	903.01	
	13.24	928.51 (928.49)	0.72	915.27	
			.59	927.92	927.90
	12.10	940.49	0.10	928.41 (928.39)	
	12.98	953.04	.43	940.06	
	10.79	963.49	.34	952.70	
B.M.			11.39	952.10	
	12.94	976.01	.42	963.07	
	12.51	988.41	.11	975.9	
	7.45	994.99	.87	987.54	
	2.76	992.24	5.51	989.48	
			11.52	980.72	

Spike in Twin C.W. 53' Lt Sta 41+00

Spike in 18" Oak 50' Rt Sta. 34+25

T.P. 20' Rt Sta 21+55

Spike in 14" B.O. 40' Lt Sta 14+50

Spike 24" Cottonwood 24' Rt Sta 6+00

Spike in T.P. 150' East Sta 0.00

CEMETERY ROAD 9/24/29

O.RVK
W.B.N.

✓ 3+00 to 4+00 = Cl. - 20' wide on Rt. 0.05 ac

✓ 5+00 - P-24" P_3 x 60' Haul. 14.96 T.M.

✓ 6+20 - Rt. - P-15" x 20' C.M.

✓ 8+00 - Rt. - No culv req.

✓ 8+75 - Lt. - P-15" x 20' C.M.

✓ 10+00 - to 13+50 - Cl. + Gr. 15' wide on Rt. 0.12 Ac.

✓ 12+50 to 13+50 - " " " " on Lt. 0.03 Ac

✓ 13+75 - Rt. - P-15" x 20' C.M.

✓ 14+00 - Lt. " "

✓ 15+00 to 17+25 - Rt. Cl. 15' wide 0.08 Ac.

✓ 15+50 to 17+25 - Lt. " " " 0.06 Ac

✓ 17+25 to 19+00 - Cl. + Gr. 10' wide - Rt. 0.04 Ac.

✓ 21+82 - Lt. - P-15" x 20' C.M.

✓ 21+82 - Rt. - " "

23+25 to 24+75 - Cl - 15' wide on Rt. 0.05 Ac.

✓ 24+00 - P-24" P_3 x 42' Haul 7.67 T.M.

✓ 27+00 to 29+00 - Lt. - Cl. + Gr. 5' wide 0.02 Ac.

✓ 28+50 to 29+00 Rt. - Cl. + Gr. 10 " 0.01 Ac.

✓ 28+25 - Lt. - P-15" x 20' C.M.

✓ 29+00 - Rt. Remove + dispose of rubbish 75^{00}

✓ 31+85 - Extend 30" x 12' C.M. Rt.
30" x 8' C.M. Lt.

✓ 37+75 - Rt. - P-15" x 20' C.M.

✓ 39+37 - Lt. - P-15" x 30' C.M.

✓ 39+53 - Rt. - "

40+89 - Lt. - P- 15" x 24' C.M.
42+72 - Rt. - Ho culv. reg.
42+76 - Lt. - " "
43+50 to 44+00 - Cl. 9 - Gr. 10
43+40 - Lt. - Ho culv. reg.
44+19 - Lt. - " " "
46+83 - Lt. - P. 15" x 20' C.M.
49+50 to 50+00 - Cl. 3 Gr. 6
51+50 - Lt. - P - 15" x 20' C.M.
46+83 - Rt. - P - 15" x 20' C.M.
52+30 - P. 24" P_3 x 42' Haul 3.51 F.M.