

BK 42 Dr. 11

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

Co Rd "B2"

From Lexington To Victoria St.

Also Co Rd B2 & Fulham
Road Acc't. No.

Date Filed 6-11-41

File

PLAN SURVEY

COUNTY ROAD "B³"

from

Lexington Av.

to

Victoria St.

Index:

Alignment : 1-2

Topography : 3-7

Bench Levels : 8-9

Cross Sections 10-16

Party:

B.P.

A.M.

L.G.

C.F.

Survey Started - 1-8-41

" Completed - 1-10-41

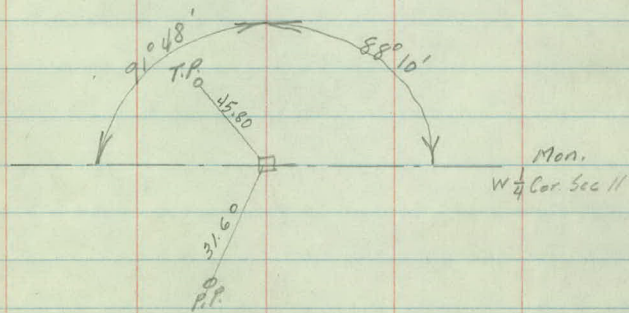
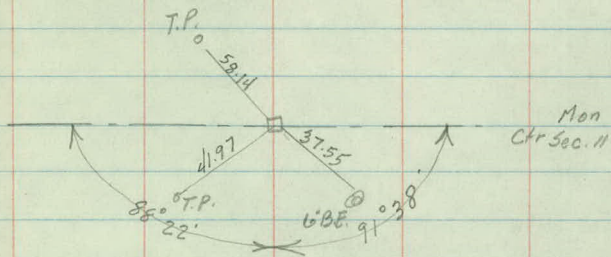
Rec'd in office 10/41 1093.

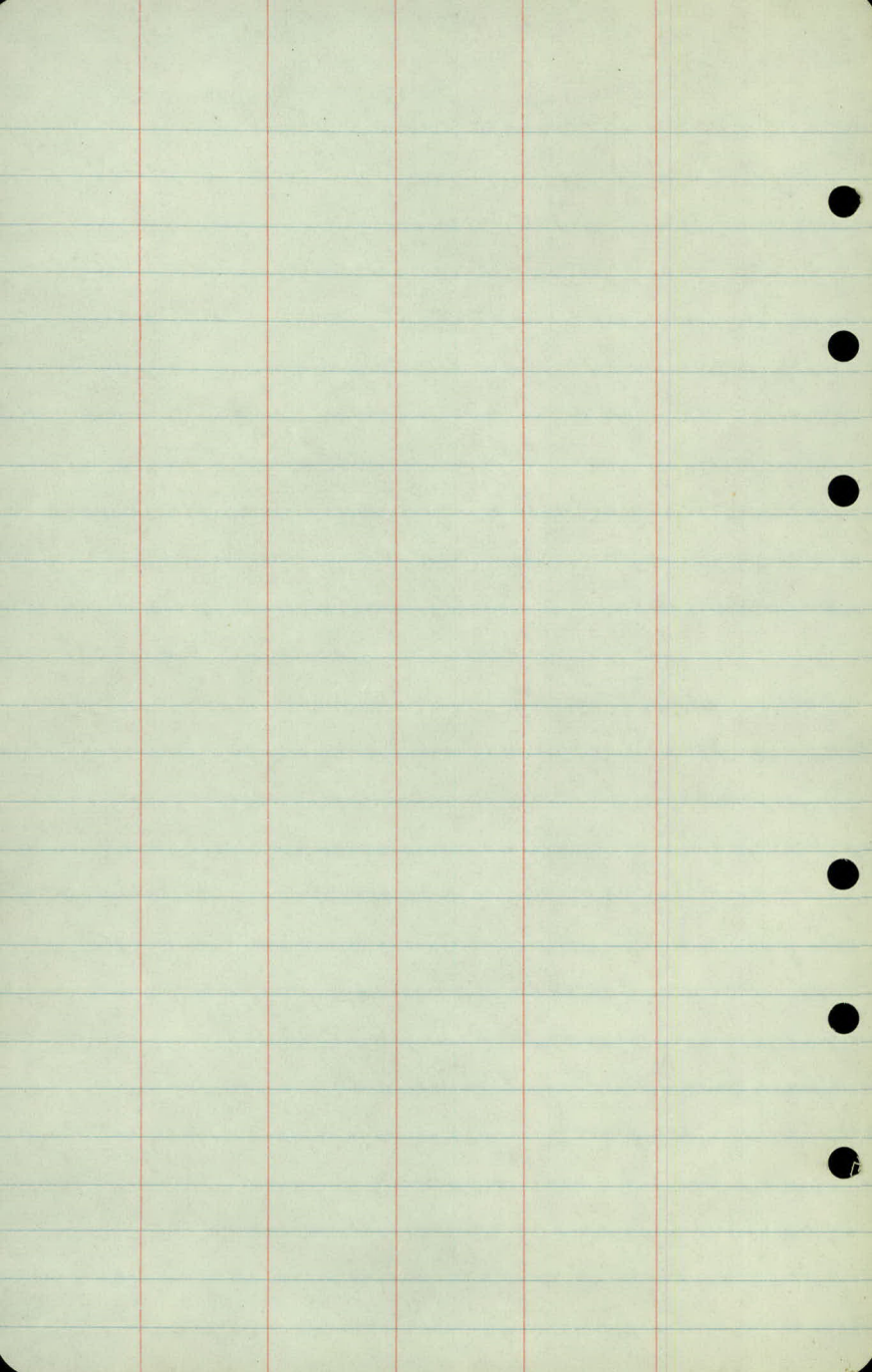
Plan Completer 5/19/41

Sta.	Pt.	Angle	Li.	Rt.	Date
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26+32.32	E Victoria				
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0+00	E Lexington				
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TOPOGRAPHY

Co. Rd. "B2"

from

Lexington Ave.

to

Victoria St.

E 8' Drive.

13'

+85 B.E.

+55 Stump

+54 Stump

+57 B.E.

+48 B.E.

+45 B.E.

+104 B.E. - d

15'

+180 Brush x 2 d

19

+71 B.E. d

+28 B.E. d

+76 B.E. d

+64 B.E. on d

+130 B.E. d

+16 B.E. on d

25'

+93 B.E. on d

+79 B.E. on d

+74 B.E. on d

+76 B.E. 11'

+91 B.E. 6'

Brush 1'

+36 Brush X 3 d

+27 Brush Lin. X 5 d

+13.5 Edge Pave. X 5 d

Brush 52'

- 13.5 Edge Pave. X 5 d

Brush 2'

Brush 6'

+75-2 BE 3-1'
 +66 BE 1'
 +64 BE 1'
 +30 BE 1'

+92 BE 1'
 +38 BE 1'
 +09 BE 1'

+82 Big Brush 3'

+82 Big Brush 7'

+99 BE 1'

+94 BE 1'
 +84 BE 1'
 +61 BE 2'
 +50 BE 1'
 +43 BE 1'
 +38 BE 2'
 +36 BE 2'
 +26 BE 3'

+04 BE 1'

+50 BE 1'
 +39 Fe. Cor. 8'
 +34 1'
 +02 BE 11'
 +90 BE 12'
 +89 BE 11'
 +83 BE 10'
 +68 BE 12'
 +61 BE 12'
 +54 BE 11'
 +46 BE 10'
 +46 Fe. Cor. 5'
 +38 BE 10'

+34 BE 0
 +16 BE 0
 +05 BE 6'
 +91 BE 5'
 +76 BE 5'
 +68 BE 5'

+46 10
 +127 T.P. 37'

+70 BE 1'
 +13 BE 6'
 +05 BE 6'
 +82 BE 6'
 +75 Oak 8'
 +68 30 Oaks 6-18-38
 +61 40 Oaks 7-26-35-40
 +54 25 Juniper 6-18
 +46 60 Oaks 10-19-27-37-44
 +39 12' Oak 55' 50"

LEXINGTON AVE.

28.5 mil
6

13

12

0

11

3'

10

7'

9

12

8

+06 BE. on E
15

7

10
+77 BE. on E

6

+39 BE on E

13

Cultivated

End Brush 1'

Brush 1'

Brush 2'

Cultivated

+11 Fc Cor. 18'
Brush 2'+17 Fc Cor. 19'
Brush 2'

Cultivated

End Brush 7'

Brush 5'

Brush 5'

Cultivated

Brush 5'

+6d B.E. 1'

Brush 6'

20

10'

19

9'

18

8'

17

1'

16

3'

15

2'

14

2'

13

0

Cultivated

Cultivated

27

E 8 Trail

26

+22 Edge of T. x 2
10'

25

9'

24

10'

23

10'

22

10

21

9'

20

10

+82 End Rod 16

+82 End Rod 12

CORDB

+46 Beg Rod 41

+46 Beg. Rod. 50

VICTORIA ST.

+057 P 32

+092 Ash. 5-28

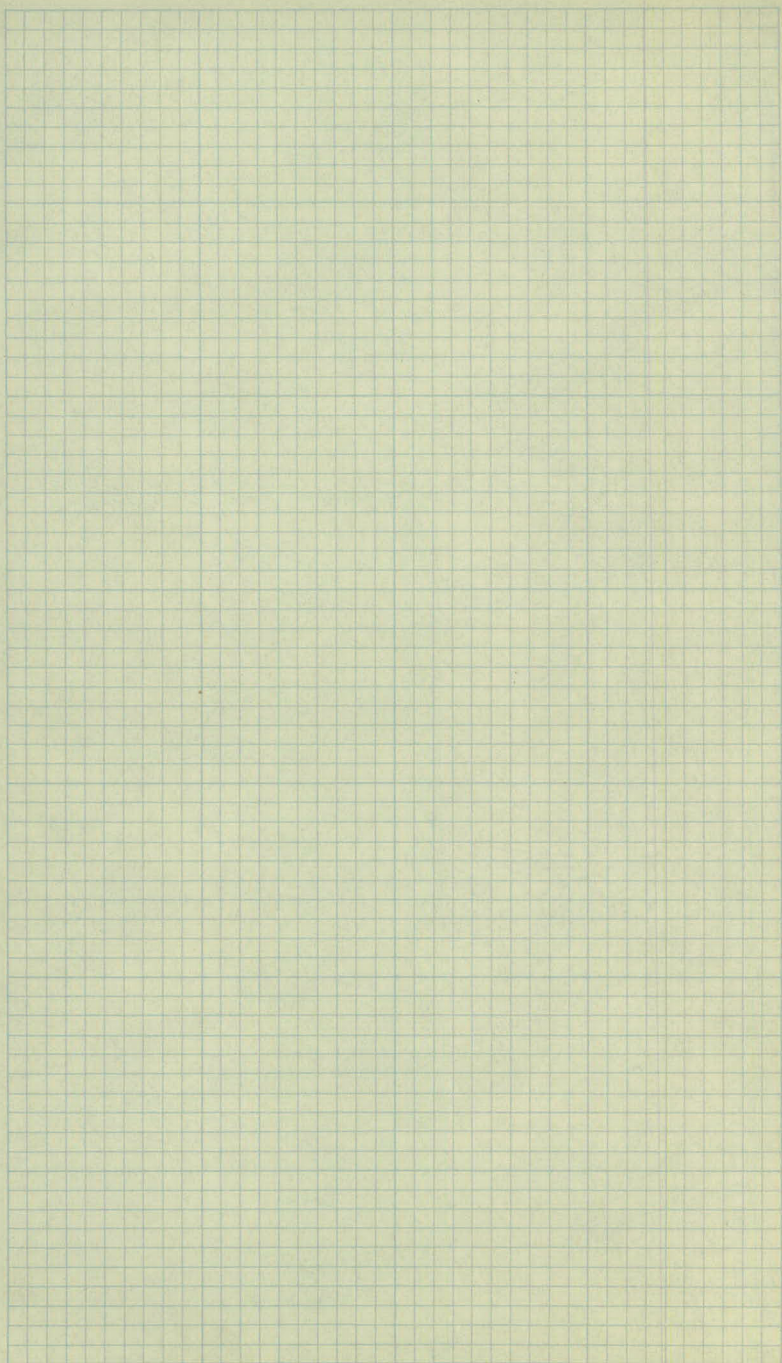
+10 Rasp. Cor. 0

Raspberries

+75 Rasp. Cor. 0

Cultivated

Cultivated



Correct sta. + ties at sta
8+2574.. on plansheet

BENCH LEVELS

Co. Rd. "B²"

Lexington to Victoria

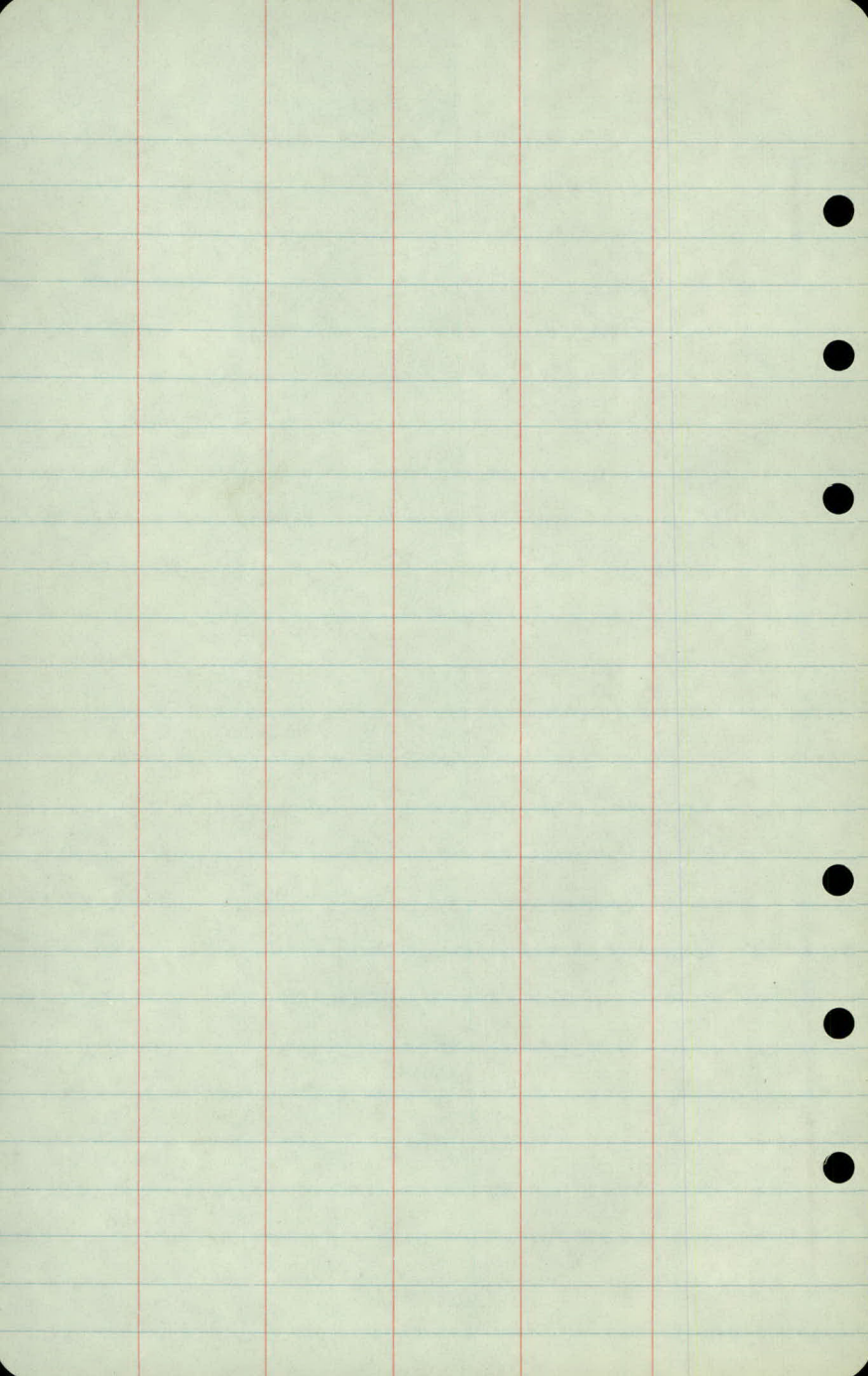
Pt.	+	π	-	Elev.
B.M.	539	946.69		944.30
	0.27	936.98	9.98	936.71
	1.88	926.37	12.49	924.49
	9.39	934.25	1.51	924.86
		949.27		926.70
B.M.	12.57	949.37	2.55	936.80
		949.98		945.63
	4.32	950.05	3.64	945.73
		51.54		47.53
	4.01	951.64	2.42	947.63
		96.62		44.80
	1.83	946.73	6.74	944.90
				46.37
B.M.	0.24	946.63	0.24	946.49
		46.58		34.64
	11.94	946.68	11.99	934.74
		52.44		42.90
	6.54	952.54	0.68	946.00
				43.76
B.M.			8.68	943.86

Top Iron. $\pm$ Lexington and Sharon

Top Mon $\pm$ Lexington and "B"

Top Iron 75' Bl 17+75

Top Mon $\pm$ Victoria and "B"



586E 10

CROSS SECTIONS

Co. Rd "B"

Lexington to Victoria

Sta.		Σ	-	Elev.
B.M.	11.12	947.82 947.92		36.70 936.80
0			11.2	36.70
+13.5			11.60	36.42
+1				
+18			11.4	36.4
+20			12.4	35.4
+29			12.5	35.3
+35			6.3	41.5
+42			6.9	40.9
+67			6.4	41.4
1			6.6	41.2
+50			6.0	41.8
2			5.0	42.8
I.P.	4.86	44.31 949.41	3.37	44.45 944.55
+50	4.86		5.4	43.9

Top Mon. & Lexington & B² (10+00)

$\frac{9.89}{50}$	$\frac{10.43}{25}$	$\frac{11.90}{25}$	$\frac{12.52}{50}$
	11.12		

$\frac{10.18}{50}$	$\frac{10.78}{25}$	$\frac{12.13}{25}$	$\frac{12.82}{50}$
	11.40		

$\frac{10.4}{50}$	$\frac{10.7}{25}$	$\frac{12.2}{25}$	$\frac{12.9}{50}$
	11.4		

$\frac{11.9}{50}$	$\frac{12.1}{25}$	$\frac{13.6}{25}$	$\frac{14.3}{50}$
	12.4		

$\frac{11.1}{50}$	$\frac{11.7}{25}$	$\frac{13.6}{25}$	$\frac{14.3}{50}$
	12.5		

$\frac{7.0}{37}$	$\frac{7.4}{26}$	$\frac{6.9}{14}$	$\frac{7.5}{6.3}$	$\frac{9.7}{13}$	$\frac{11.4}{35}$
					50

$\frac{4.6}{50}$	$\frac{5.6}{25}$	$\frac{7.1}{6.9}$	$\frac{8.7}{12}$	$\frac{11.4}{25}$
				50

$\frac{4.8}{50}$	$\frac{4.6}{25}$	$\frac{4.7}{11}$	$\frac{5.6}{3}$	$\frac{7.2}{6.4}$	$\frac{9.4}{7}$	$\frac{10.4}{28}$
						50

$\frac{5.2}{50}$	$\frac{5.2}{25}$	$\frac{5.3}{4}$	$\frac{8.8}{6.6}$	$\frac{9.5}{12}$	$\frac{11.0}{25}$
					50

$\frac{4.2}{50}$	$\frac{4.7}{25}$	$\frac{4.8}{8}$	$\frac{8.5}{6.0}$	$\frac{10.1}{22}$
				50

$\frac{4.2}{50}$	$\frac{4.2}{25}$	$\frac{4.8}{8}$	$\frac{7.5}{5.0}$	$\frac{9.5}{25}$
				50

$\frac{5.0}{50}$	$\frac{5.5}{25}$	$\frac{5.0}{12}$	$\frac{6.7}{5.4}$	$\frac{8.0}{9}$	$\frac{10.5}{25}$
					50

Sta.		+	—	Elev.
		49.31 949.41		
3			5.2	44.1
	+50		4.5	44.8
4			4.1	45.2
	+50		3.7	45.6
5			4.3	45.0
T.P.	3.68	49.34 949.44	3.65	45.66 945.76
	+50		4.8	44.5
6			4.6	44.7
	+50		4.8	44.5
7			4.6	44.7
	+50		4.4	44.9
8			4.1	45.2
	+50		4.2	45.1
T.P.	2.17	50.16 950.26	1.35	47.99 948.09

$$\begin{array}{r} 5.1 \\ 50 \end{array} \quad \begin{array}{r} 4.5 \\ 25 \end{array} \quad \begin{array}{r} 5.3 \\ 5.2 \end{array} \quad \begin{array}{r} 6.8 \\ 4 \end{array} \quad \begin{array}{r} 7.8 \\ 18 \end{array} \quad \begin{array}{r} 7.0 \\ 37 \end{array} \quad \begin{array}{r} 7.0 \\ 50 \end{array}$$

$$1 \quad \begin{array}{r} 4.7 \\ 50 \end{array} \quad \begin{array}{r} 4.9 \\ 25 \end{array} \quad \begin{array}{r} 4.8 \\ 4.5 \end{array} \quad \begin{array}{r} 5.8 \\ 7 \end{array} \quad \begin{array}{r} 6.9 \\ 28 \end{array} \quad \begin{array}{r} 6.9 \\ 50 \end{array}$$

$$\begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 5.0 \\ 25 \end{array} \quad \begin{array}{r} 4.0 \\ 4.1 \end{array} \quad \begin{array}{r} 5.5 \\ 7 \end{array} \quad \begin{array}{r} 6.7 \\ 25 \end{array} \quad \begin{array}{r} 6.7 \\ 50 \end{array}$$

$$\begin{array}{r} 4.9 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ 25 \end{array} \quad \begin{array}{r} 4.1 \\ 3.7 \end{array} \quad \begin{array}{r} 5.1 \\ 7 \end{array} \quad \begin{array}{r} 5.8 \\ 28 \end{array} \quad \begin{array}{r} 5.8 \\ 50 \end{array}$$

$$\begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 5.0 \\ 25 \end{array} \quad \begin{array}{r} 4.8 \\ 2 \end{array} \quad \begin{array}{r} 4.3 \\ 4.3 \end{array} \quad \begin{array}{r} 4.3 \\ 7 \end{array} \quad \begin{array}{r} 5.1 \\ 15 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 5.0 \\ 50 \end{array} \quad \begin{array}{r} 5.0 \\ 25 \end{array} \quad \begin{array}{r} 4.6 \\ 4.8 \end{array} \quad \begin{array}{r} 4.8 \\ 7 \end{array} \quad \begin{array}{r} 5.3 \\ 25 \end{array} \quad \begin{array}{r} 5.3 \\ 50 \end{array}$$

$$\begin{array}{r} 5.2 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 25 \end{array} \quad \begin{array}{r} 4.3 \\ 4.6 \end{array} \quad \begin{array}{r} 4.7 \\ 4 \end{array} \quad \begin{array}{r} 5.4 \\ 28 \end{array} \quad \begin{array}{r} 5.4 \\ 50 \end{array}$$

$$\begin{array}{r} 4.5 \\ 50 \end{array} \quad \begin{array}{r} 4.4 \\ 25 \end{array} \quad \begin{array}{r} 4.8 \\ 4.8 \end{array} \quad \begin{array}{r} 5.4 \\ 5 \end{array} \quad \begin{array}{r} 4.7 \\ 16 \end{array} \quad \begin{array}{r} 5.2 \\ 33 \end{array} \quad \begin{array}{r} 5.2 \\ 50 \end{array}$$

$$\begin{array}{r} 4.9 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ 25 \end{array} \quad \begin{array}{r} 4.6 \\ 4.6 \end{array} \quad \begin{array}{r} 4.7 \\ 6 \end{array} \quad \begin{array}{r} 5.2 \\ 29 \end{array} \quad \begin{array}{r} 5.3 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ 25 \end{array} \quad \begin{array}{r} 4.4 \\ 4.4 \end{array} \quad \begin{array}{r} 4.5 \\ 6 \end{array} \quad \begin{array}{r} 5.2 \\ 20 \end{array} \quad \begin{array}{r} 5.1 \\ 50 \end{array}$$

$$\begin{array}{r} 5.0 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ 25 \end{array} \quad \begin{array}{r} 4.8 \\ 4.8 \end{array} \quad \begin{array}{r} 4.5 \\ 8 \end{array} \quad \begin{array}{r} 4.8 \\ 27 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 5.0 \\ 50 \end{array} \quad \begin{array}{r} 4.3 \\ 25 \end{array} \quad \begin{array}{r} 4.3 \\ 4.3 \end{array} \quad \begin{array}{r} 4.7 \\ 7 \end{array} \quad \begin{array}{r} 4.7 \\ 34 \end{array} \quad \begin{array}{r} 4.8 \\ 50 \end{array}$$

Sta.	T	π	-	Elev.
		50.16 950.26		
9			48	45.4
+50			46	45.6
10			4.5	45.7
+50			4.5	45.7
11			4.2	46.0
+50			3.6	46.6
T.P.	5.51	52.59 952.69	3.08	47.08 947.18
12			5.9	46.7
+50			5.7	46.9
13			5.3	47.3
+43			6.0	46.6
+73			6.8	45.8
14			7.2	45.4

$$\frac{5.6}{50} \quad \frac{5.1}{25} \quad 4.8 \quad \frac{4.6}{6} \quad \frac{5.6}{19} \quad \frac{5.8}{50}$$

$$\frac{5.3}{50} \quad \frac{5.2}{25} \quad 4.6 \quad \frac{4.8}{7} \quad \frac{5.6}{23} \quad \frac{5.4}{50}$$

$$\frac{4.7}{50} \quad \frac{4.5}{36} \quad \frac{4.6}{18} \quad 4.5 \quad \frac{5.6}{26} \quad \frac{5.6}{50}$$

$$\frac{4.7}{50} \quad \frac{4.6}{25} \quad \frac{4.1}{12} \quad 4.5 \quad \frac{4.4}{9} \quad \frac{5.3}{16} \quad \frac{5.6}{50}$$

$$\frac{4.4}{50} \quad \frac{4.3}{25} \quad 4.2 \quad \frac{4.9}{13} \quad \frac{5.3}{27} \quad \frac{5.5}{50}$$

$$\frac{4.3}{50} \quad \frac{4.0}{26} \quad 3.7 \quad \frac{4.6}{8} \quad \frac{5.2}{10} \quad \frac{5.4}{25} \quad \frac{5.4}{50}$$

$$\frac{6.9}{50} \quad \frac{6.3}{25} \quad \frac{5.9}{5.9} \quad \frac{6.5}{13} \quad \frac{7.2}{30} \quad \frac{7.5}{50}$$

$$\frac{7.3}{50} \quad \frac{6.7}{25} \quad 5.7 \quad \frac{6.3}{13} \quad \frac{7.4}{27} \quad \frac{7.9}{50}$$

$$\frac{7.7}{50} \quad \frac{6.4}{25} \quad 5.3 \quad \frac{5.0}{12} \quad \frac{6.4}{15} \quad \frac{7.2}{30} \quad \frac{7.7}{50}$$

$$\frac{7.6}{50} \quad \frac{7.7}{25} \quad \frac{5.7}{6} \quad 6.0 \quad \frac{5.5}{13} \quad \frac{5.7}{16} \quad \frac{5.8}{37} \quad \frac{5.9}{50}$$

$$\frac{8.1}{50} \quad \frac{8.0}{22} \quad \frac{6.5}{4} \quad 6.8 \quad \frac{6.6}{6} \quad \frac{7.7}{25} \quad \frac{7.4}{50}$$

$$\frac{8.2}{50} \quad \frac{8.4}{38} \quad \frac{8.4}{25} \quad \frac{6.8}{5} \quad 7.2 \quad \frac{7.8}{25} \quad \frac{8.1}{50}$$

Sta.	t	Δ	-	Elev.	
		52.59 95269			
14+58			7.5	45.1	
T.P.	0.86	48.54 948.64	4.91	47.68 947.78	#15
15			3.8	44.7	
+50			3.8	44.7	
16			3.9	44.6	
+50			4.1	44.4	
17			4.6	43.9	
+50			5.1	43.4	
B.M.	2.13		2.13	946.41 946.51	946.32 946.49
18			6.1	42.4	
+50			8.4	40.1	
19			9.1	39.4	
+69			13.3	35.2	
T.P.	2.43	40.37 940.47	10.60	37.94 938.04	
20			5.8	34.6	

$$\begin{array}{r} 8.3 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 19 \end{array} \quad \begin{array}{r} 7.2 \\ 4 \end{array} \quad \begin{array}{r} 7.4 \\ 10 \end{array} \quad \begin{array}{r} 8.0 \\ 30 \end{array} \quad \begin{array}{r} 7.6 \\ 50 \end{array}$$

$$\begin{array}{r} 4.3 \\ 50 \end{array} \quad \begin{array}{r} 4.4 \\ 25 \end{array} \quad \begin{array}{r} 3.3 \\ 7 \end{array} \quad \begin{array}{r} 3.7 \\ 12 \end{array} \quad \begin{array}{r} 4.1 \\ 21 \end{array} \quad \begin{array}{r} 4.3 \\ 50 \end{array}$$

$$\begin{array}{r} 4.9 \\ 50 \end{array} \quad \begin{array}{r} 4.6 \\ 26 \end{array} \quad \begin{array}{r} 3.8 \\ 12 \end{array} \quad \begin{array}{r} 3.4 \\ 3 \end{array} \quad \begin{array}{r} 3.8 \\ 7 \end{array} \quad \begin{array}{r} 4.2 \\ 18 \end{array} \quad \begin{array}{r} 4.6 \\ 35 \end{array} \quad \begin{array}{r} 4.5 \\ 50 \end{array}$$

$$\begin{array}{r} 4.2 \\ 50 \end{array} \quad \begin{array}{r} 4.5 \\ 25 \end{array} \quad \begin{array}{r} 4.1 \\ 9 \end{array} \quad \begin{array}{r} 3.9 \\ 7 \end{array} \quad \begin{array}{r} 3.7 \\ 7 \end{array} \quad \begin{array}{r} 4.3 \\ 19 \end{array} \quad \begin{array}{r} 4.5 \\ 50 \end{array}$$

$$\begin{array}{r} 4.4 \\ 50 \end{array} \quad \begin{array}{r} 4.6 \\ 25 \end{array} \quad \begin{array}{r} 4.4 \\ 5 \end{array} \quad \begin{array}{r} 4.1 \\ 9 \end{array} \quad \begin{array}{r} 4.2 \\ 9 \end{array} \quad \begin{array}{r} 4.6 \\ 21 \end{array} \quad \begin{array}{r} 4.7 \\ 50 \end{array}$$

$$\begin{array}{r} 4.7 \\ 50 \end{array} \quad \begin{array}{r} 4.6 \\ 25 \end{array} \quad \begin{array}{r} 4.3 \\ 6 \end{array} \quad \begin{array}{r} 4.6 \\ 12 \end{array} \quad \begin{array}{r} 4.7 \\ 12 \end{array} \quad \begin{array}{r} 4.8 \\ 27 \end{array} \quad \begin{array}{r} 4.9 \\ 50 \end{array}$$

$$\begin{array}{r} 5.0 \\ 50 \end{array} \quad \begin{array}{r} 5.0 \\ 19 \end{array} \quad \begin{array}{r} 5.1 \\ 6 \end{array} \quad \begin{array}{r} 4.8 \\ 27 \end{array} \quad \begin{array}{r} 4.8 \\ 50 \end{array}$$

$$\begin{array}{r} 6.3 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 25 \end{array} \quad \begin{array}{r} 5.8 \\ 11 \end{array} \quad \begin{array}{r} 6.1 \\ 4 \end{array} \quad \begin{array}{r} 6.3 \\ 4 \end{array} \quad \begin{array}{r} 6.8 \\ 6 \end{array} \quad \begin{array}{r} 5.5 \\ 24 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

$$\begin{array}{r} 7.5 \\ 50 \end{array} \quad \begin{array}{r} 7.8 \\ 28 \end{array} \quad \begin{array}{r} 7.0 \\ 14 \end{array} \quad \begin{array}{r} 7.0 \\ 7 \end{array} \quad \begin{array}{r} 8.4 \\ 9 \end{array} \quad \begin{array}{r} 8.0 \\ 12 \end{array} \quad \begin{array}{r} 7.2 \\ 30 \end{array} \quad \begin{array}{r} 7.2 \\ 50 \end{array}$$

$$\begin{array}{r} 9.7 \\ 50 \end{array} \quad \begin{array}{r} 9.1 \\ 25 \end{array} \quad \begin{array}{r} 8.6 \\ 14 \end{array} \quad \begin{array}{r} 9.1 \\ 3 \end{array} \quad \begin{array}{r} 9.8 \\ 10 \end{array} \quad \begin{array}{r} 9.4 \\ 26 \end{array} \quad \begin{array}{r} 9.0 \\ 50 \end{array}$$

$$\begin{array}{r} 13.4 \\ 50 \end{array} \quad \begin{array}{r} 13.3 \\ 25 \end{array} \quad \begin{array}{r} 12.8 \\ 14 \end{array} \quad \begin{array}{r} 13.3 \\ 4 \end{array} \quad \begin{array}{r} 12.0 \\ 27 \end{array} \quad \begin{array}{r} 11.6 \\ 27 \end{array} \quad \begin{array}{r} 11.6 \\ 50 \end{array}$$

$$\begin{array}{r} 7.9 \\ 50 \end{array} \quad \begin{array}{r} 4.8 \\ 23 \end{array} \quad \begin{array}{r} 6.6 \\ 14 \end{array} \quad \begin{array}{r} 5.8 \\ 10 \end{array} \quad \begin{array}{r} 7.2 \\ 25 \end{array} \quad \begin{array}{r} 8.2 \\ 50 \end{array}$$

Sta.	+	π	-	Elev.
		40.37 940.47		
20+50			9.0	31.4
21			9.8	30.6
+50			9.2	31.2
22			6.8	33.6
+50			3.2	37.2
T.P.	12.26	50.14 950.24	2.49	37.88 937.98
23			10.4	39.7
+50			7.1	43.0
24			4.4	45.7
+50			3.1	47.0
25			3.1	47.0
+50			3.1	47.0
26			3.0	47.1

$$\begin{array}{r} 9.4 \\ 50 \end{array} \quad \begin{array}{r} 8.9 \\ 25 \end{array} \quad \begin{array}{r} 8.2 \\ 14 \end{array} \quad \begin{array}{r} 8.4 \\ 2 \end{array} \quad 9.0 \quad \begin{array}{r} 10.1 \\ 5 \end{array} \quad \begin{array}{r} 11.0 \\ 21 \end{array} \quad \begin{array}{r} 11.2 \\ 50 \end{array}$$

$$\begin{array}{r} 10.6 \\ 50 \end{array} \quad \begin{array}{r} 9.8 \\ 25 \end{array} \quad \begin{array}{r} 9.3 \\ 14 \end{array} \quad \begin{array}{r} 9.4 \\ 3 \end{array} \quad 9.8 \quad \begin{array}{r} 11.4 \\ 17 \end{array} \quad \begin{array}{r} 13.1 \\ 38 \end{array} \quad \begin{array}{r} 14.1 \\ 50 \end{array}$$

$$\begin{array}{r} 9.5 \\ 50 \end{array} \quad \begin{array}{r} 9.4 \\ 30 \end{array} \quad \begin{array}{r} 9.2 \\ 15 \end{array} \quad 9.2 \quad \begin{array}{r} 10.1 \\ 4 \end{array} \quad \begin{array}{r} 11.2 \\ 18 \end{array} \quad \begin{array}{r} 13.3 \\ 50 \end{array}$$

$$\begin{array}{r} 6.9 \\ 50 \end{array} \quad \begin{array}{r} 6.3 \\ 24 \end{array} \quad \begin{array}{r} 6.6 \\ 15 \end{array} \quad \begin{array}{r} 6.1 \\ 3 \end{array} \quad 6.8 \quad \begin{array}{r} 7.2 \\ 4 \end{array} \quad \begin{array}{r} 8.5 \\ 26 \end{array} \quad \begin{array}{r} 9.7 \\ 50 \end{array}$$

$$\begin{array}{r} 3.6 \\ 50 \end{array} \quad \begin{array}{r} 3.7 \\ 34 \end{array} \quad \begin{array}{r} 3.2 \\ 18 \end{array} \quad \begin{array}{r} 2.7 \\ 5 \end{array} \quad 3.2 \quad \begin{array}{r} 4.2 \\ 7 \end{array} \quad \begin{array}{r} 5.1 \\ 25 \end{array} \quad \begin{array}{r} 6.2 \\ 50 \end{array}$$

$$\begin{array}{r} 10.4 \\ 50 \end{array} \quad \begin{array}{r} 10.2 \\ 25 \end{array} \quad \begin{array}{r} 9.3 \\ 14 \end{array} \quad \begin{array}{r} 9.3 \\ 4 \end{array} \quad 10.4 \quad \begin{array}{r} 11.5 \\ 16 \end{array} \quad \begin{array}{r} 12.2 \\ 37 \end{array} \quad \begin{array}{r} 12.7 \\ 50 \end{array}$$

$$\begin{array}{r} 7.6 \\ 50 \end{array} \quad \begin{array}{r} 7.6 \\ 30 \end{array} \quad \begin{array}{r} 6.9 \\ 17 \end{array} \quad \begin{array}{r} 6.0 \\ 4 \end{array} \quad 7.1 \quad \begin{array}{r} 8.6 \\ 18 \end{array} \quad \begin{array}{r} 9.4 \\ 35 \end{array} \quad \begin{array}{r} 9.9 \\ 50 \end{array}$$

$$\begin{array}{r} 6.3 \\ 50 \end{array} \quad \begin{array}{r} 5.8 \\ 25 \end{array} \quad \begin{array}{r} 4.3 \\ 16 \end{array} \quad \begin{array}{r} 3.7 \\ 3 \end{array} \quad 4.4 \quad \begin{array}{r} 4.9 \\ 4 \end{array} \quad \begin{array}{r} 6.0 \\ 26 \end{array} \quad \begin{array}{r} 6.8 \\ 50 \end{array}$$

$$\begin{array}{r} 5.5 \\ 50 \end{array} \quad \begin{array}{r} 4.7 \\ 25 \end{array} \quad \begin{array}{r} 3.6 \\ 16 \end{array} \quad \begin{array}{r} 2.5 \\ 3 \end{array} \quad 3.1 \quad \begin{array}{r} 3.7 \\ 4 \end{array} \quad \begin{array}{r} 4.6 \\ 28 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 5.9 \\ 50 \end{array} \quad \begin{array}{r} 4.3 \\ 26 \end{array} \quad \begin{array}{r} 3.2 \\ 16 \end{array} \quad \begin{array}{r} 2.5 \\ 5 \end{array} \quad 3.1 \quad \begin{array}{r} 4.0 \\ 27 \end{array} \quad \begin{array}{r} 4.4 \\ 50 \end{array}$$

$$\begin{array}{r} 4.8 \\ 50 \end{array} \quad \begin{array}{r} 4.3 \\ 23 \end{array} \quad \begin{array}{r} 3.2 \\ 15 \end{array} \quad \begin{array}{r} 2.7 \\ 3 \end{array} \quad 3.1 \quad \begin{array}{r} 4.2 \\ 29 \end{array} \quad \begin{array}{r} 4.4 \\ 50 \end{array}$$

$$\begin{array}{r} 4.4 \\ 50 \end{array} \quad \begin{array}{r} 3.6 \\ 20 \end{array} \quad 3.0 \quad \begin{array}{r} 3.4 \\ 25 \end{array} \quad \begin{array}{r} 3.5 \\ 50 \end{array}$$

Sta.	+	π	-	Elev.
		50.14 950.24		

26 + 08

2.7

47.4

+15

6.5

43.6

+19

6.7

43.4

+32.32

6.4

43.7

B.M.

6.39

43.75

943.76

943.85

943.86

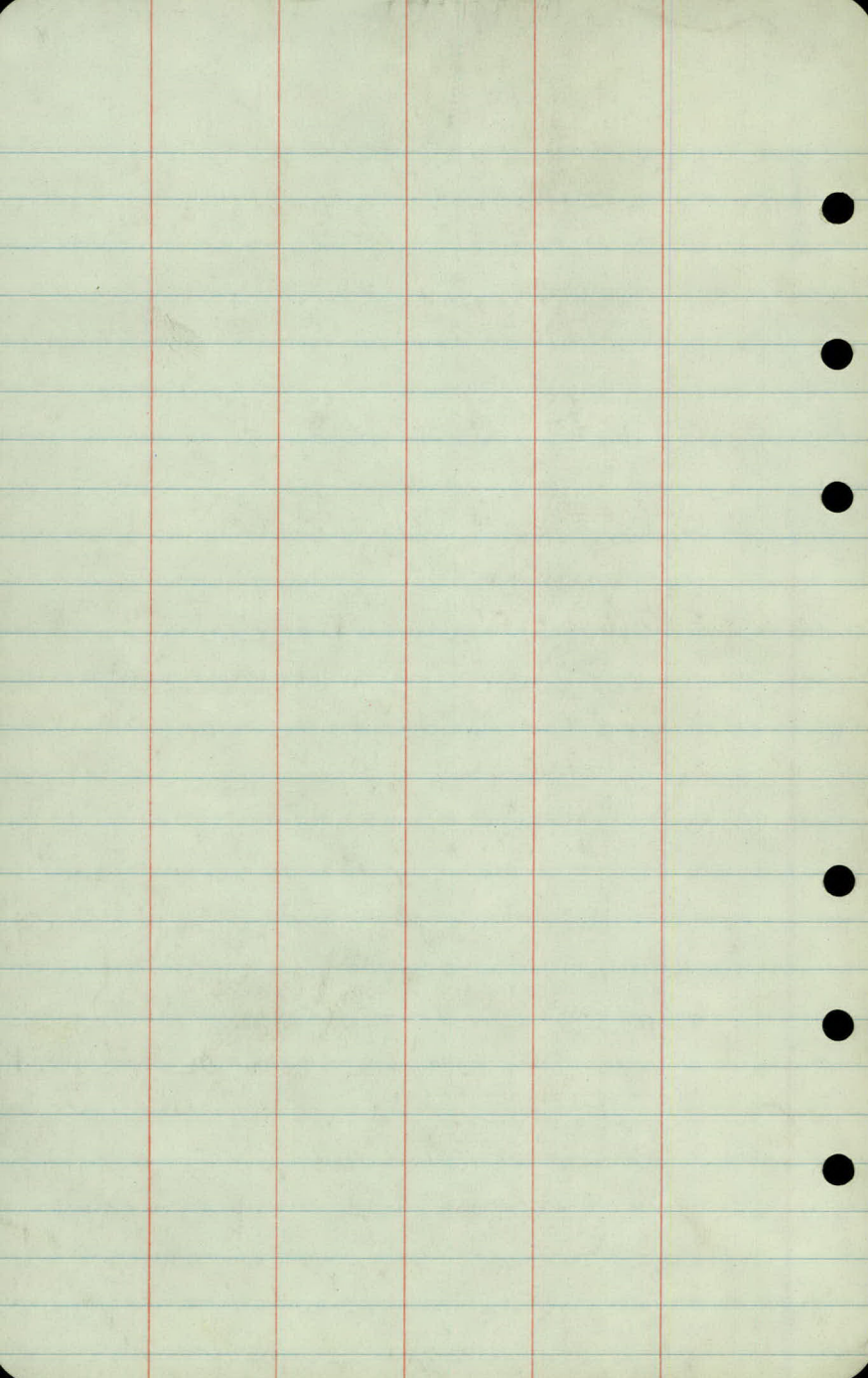
$\frac{4.1}{50}$ $\frac{3.7}{25}$ $\frac{3.7}{17}$ $\frac{5.0}{15}$ $\frac{4.6}{7}$ $\frac{3.3}{25}$ $\frac{3.1}{80}$
 2.7

$\frac{7.7}{50}$ $\frac{7.0}{25}$ 6.5 $\frac{6.3}{25}$ $\frac{6.2}{50}$

$\frac{8.1}{50}$ $\frac{7.2}{25}$ 6.7 $\frac{6.6}{25}$ $\frac{6.3}{50}$

$\frac{7.7}{50}$ $\frac{6.9}{25}$ 6.4 $\frac{6.1}{25}$ $\frac{6.0}{50}$

Top Mon. & Victoria + B³.



Profile Levels

Co Rd "B²"

Fulham to 300' East
Long Lake Rd

Rec'd. 8-20-51
R.C.

8-17-51 HAW
AM
MB
T.W

Drawn Up.

Sta	+	Δ	-	Elev
B.M	944	946.44		937.20
T.P	2.94	941.07	8.51	938.13
	6.19	941.55	5.71	935.36
B.M	8.67	941.55	8.67	932.88
0+00	Cons Sec 8-29-23			32.9

+50				32.1
-----	--	--	--	------

1				31.7
---	--	--	--	------

+50				29.4
-----	--	--	--	------

2				29.4
---	--	--	--	------

+50				32.8
-----	--	--	--	------

3				37.7
---	--	--	--	------

4

Top Iron West Line Line Longlake Rd + 4 B²

Top Mon 4 Sec 8-29-23

8.7

9.5

9.9

12.2

12.2

88

39

Sta

+

K

-

Elev.

941.55

3+50

34.3

4

36.5

+50

38.5

5

38.2

+50

38.7

T.P.

5.80

945.70

1.65

939.90

6

37.9

+50

36.7

7

37.4

2

13

51

31

34

29

78

90

83

Sta + Δ - Elev

945.70

7+50

36.8

8

36.2

T.P. 12.40 949.07 9.03 936.67

+50

37.1

9

39.1

+50

41.0

10

41.7

+50

41.5

11

44.3

~~2~~

89

9.5

120

10.0

81

74

7.1

4.8

Sta	+	π	-	Elev
		949.07		

11	+50			43.4
----	-----	--	--	------

12				36.3
----	--	--	--	------

B.M	6.21	943.41	11.88	937.19	937.20
-----	------	--------	-------	--------	--------

	+50			31.3
--	-----	--	--	------

13				30.8
----	--	--	--	------

	+50			34.0
--	-----	--	--	------

14				38.9
----	--	--	--	------

	+25			43.4
--	-----	--	--	------

	+50			50.9
--	-----	--	--	------

2

57

128

Top Iron

12.1

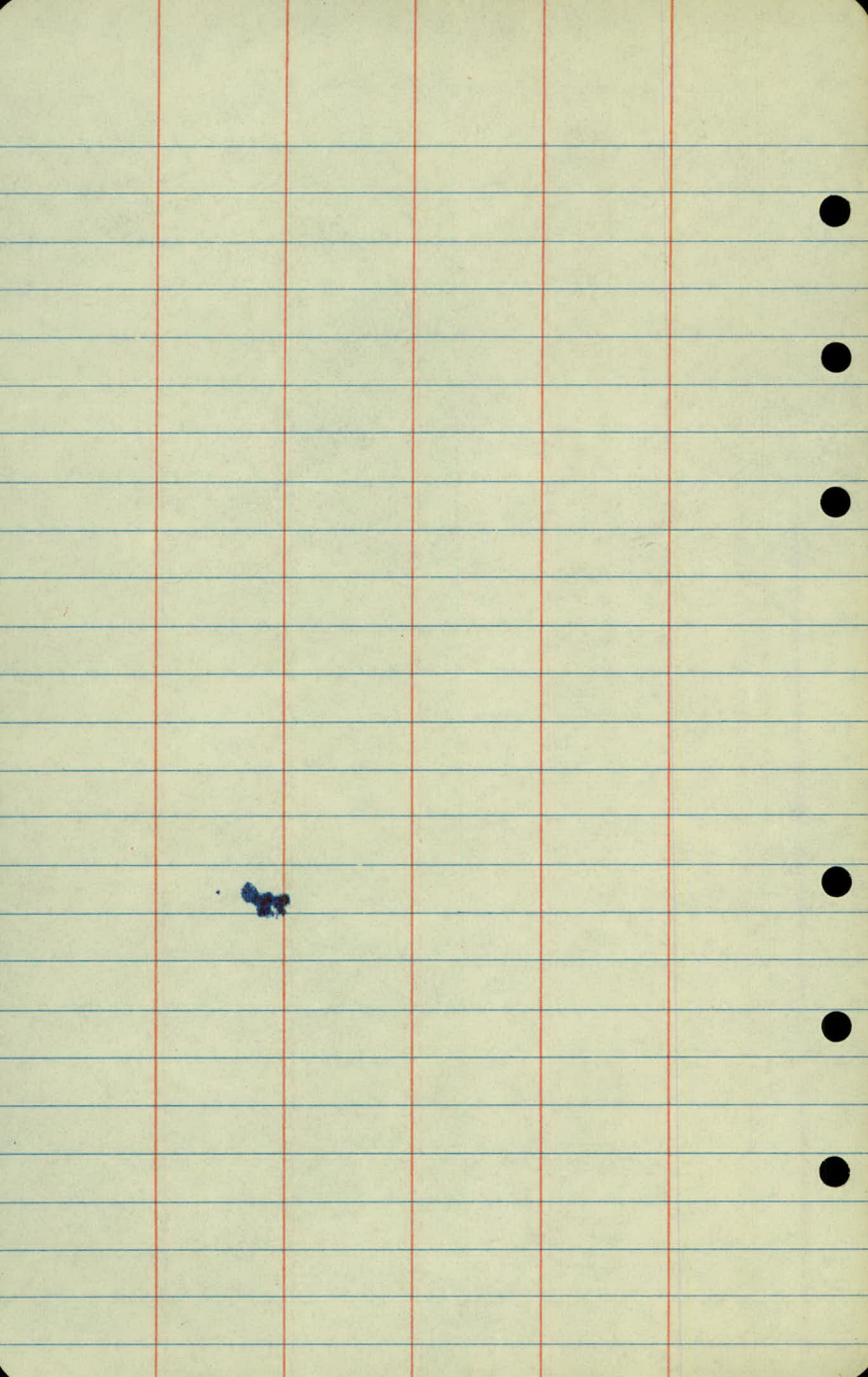
12.6

94

4.5

0.6

+7.5



1
B²

Victoria to Dale

X-sections

7/2/53

also

6/24/54

starto

drawn up

8-11-53

A.G.

Sta	+	π	-	Elev
BM	5.92	944.04		938.12

0+00

+10

+18

+27

+32 18" SCP With CM Extensions

+50

+50

26 June 1953

FK
AM
MMe
PM

2

Lt

L

Rt

Top Mant. Cen. Sec. II

38.2
12.3 10.6 8.8 7.0 6.6 6.1 5.8 5.6 5.5 5.3 5.3 5.2 5.2
200 150 100 50 38 15 10 38 50 100 150 200

38.5
7.3 6.5 5.7 5.5 5.4 5.3 5.5
50 31 11 10 28 50

38.6
8.0 7.2 5.6 5.4 5.3 5.9 5.8 5.5
50 34 11 11 34 40 50

38.9
4.7 4.3 7.3 6.6 5.3 5.1 5.2 5.9 5.6 4.2 4.8
50 35 28 23 10 12 24 30 39 50

35.7
8.34
22
FL 18" CM

36.4
7.63
23
FL 18" CM

39.2
5.3 5.2 5.1 6.9 5.5 5.3 4.8 5.3 5.5 6.1 6.1 4.0 4.1
50 40 30 22 16 11 12 19 23 27 33 50

39.5
4.9 4.9 4.9 7.0 7.0 5.3 5.0 4.5 4.9 5.1 6.6 6.6 4.6 4.8 5.1
50 38 28 23 20 15 11 10 19 24 26 30 38 50

39.6
4.6 3.9 3.7 6.6 6.6 5.3 5.0 4.4 4.9 5.1 6.6 6.6 4.4 5.0 5.2
50 35 29 24 21 15 10 10 16 22 24 29 41 50

Sta + X - Elev

944.04

2

+50

+50

+72

+72

3

3

+50

BM

5.98

944.10

938.12

Lt

R

Rt

39.5

5.5 5.3 4.9 6.9 6.9 5.4 5.1 4.5 4.9 5.3 7.0 7.0 5.1 5.7 6.0
 50 41 27 23 21 14 10 11 14 22 25 29 36 50

39.5

6.3 6.3 6.1 5.4 7.0 7.0 4.5 4.8 5.1 6.3 5.8 6.5
 50 38 32 27 22 20 11 15 21 29 38

5.2 5.0
 14 10

6.7
 50

39.6

5.2 6.5 6.5 5.2 4.9 4.4 4.7 5.0 5.9 6.0 6.3 6.7
 26 22 19 14 10 11 16 20 29 40 50

5.0 4.9
 50 39

39.7

4.4 4.6 5.0 6.4 6.4 4.3 4.6 4.8 5.8 5.8 6.6
 50 36 25 23 20 11 15 23 31 50

5.1 4.8
 16 11

39.8

4.6 4.7
 50 35

4.6 4.2
 11

4.5
 11

4.6 5.8 6.2 6.6
 16 24 37 50

Top Mont. Cent Sec. II

Sta + π - Elev
944.10

4

+50

✓✓

5

+50

6

+08

+50

Lt

L

Rt

39.8

5.0	5.4	5.1	6.1	5.2	4.9	4.3	4.7	4.9	6.2	5.6	6.5	7.0
50	33	24	18-21	15	11		11	16	22	28	40	50

39.1

5.6	6.0	6.0	6.8	5.1	4.9	4.4	4.7	4.9	6.6	6.7	7.2	7.4
50	33	25	22-20	16	11		10	16	21-25	27	40	50

39.6

6.2	6.7	6.5	7.0	5.5	5.0	4.5	4.9	5.3	6.7	6.8	6.6	7.1	7.8
50	39	29	23-21	17	12		10	18	22	27	30	37	50

39.5

6.8	6.5	5.7	6.3	5.0	5.0	4.6	4.8	5.1	5.5	7.1	7.3	7.1	8.4
50	37	28	23-20	17	12		7	11	15	23	27	29	42

39.6

5.4	5.5	6.3	5.6	5.1	4.7	4.5	4.6	5.2	5.5	7.3	7.6
32	28	23-21	19	15	8		6	14	18	30	50

6.1	6.5
35	50

39.6

6.5	5.6	6.0	5.3	5.9	6.1	4.5	4.9	5.6	7.0	7.5	6.4
50	37	33	33	27	21		10	20	27	39	50

4.6	5.1
7	14

39.1

5.2	5.2	6.1	6.6	5.2	4.7	4.4	4.5	4.9	6.0	6.7	4.8	4.7
33	30	24	23-21	16	9		6	14	23	34	50	75

5.6	6.2
33	50

Sta	+	T	-	Elev
		944.10		

7+00

T.P.	4.96	944.65	4.41	939.69
------	------	--------	------	--------

+24

+50

8

+25

+50

+84

conc. Ent. 15' Wide

9

Lt

♀

Rt

39.9

✓

5.7 5.0 4.2 5.0 6.0 5.0 4.4 4.2 4.5 5.4 6.0 5.7 6.4
50 35 33 28 21 16 9 9 19 25 29 50

40.2

✓

4.6 5.2 5.6 6.5 5.2 4.8 4.5 4.7 5.3 6.3 6.1 5.2
32 30 25 22-19 15 9 7 15 24 37 50
4.5 6.1
34 50

40.3

✓

5.9 5.1 4.2 4.1 5.2 6.3 4.4 4.6 4.9 5.6 6.2 5.7 4.9 4.4
50 40 35 31 28 22-20 7 14 22 31 37 50 40.2
Mo. 44 74

Rt side

4.6 5.1 40.4
8 15

Lt. side

5.0 5.4 5.8 5.4 4.9 4.5 4.3 4.5 4.8 6.0 5.2 4.9 3.8 4.1
75 50 33 23 15 8 9 15 20-22 25 30 32 34

40.4

5.4 4.7
50 34

5.6 5.0 4.7 4.0 4.3 5.8 4.9 4.3 4.5 4.9 4.8 5.4 5.4 5.1
50 40 34 34 30 22-20 16 8 14 21 28 37 50

4.5 40.4
8

40.2

3.8 4.3 5.0 6.0 5.0 4.6 4.3 4.5 4.9 5.4 5.2 4.9 4.2
(31 30 25 22-20 15 8 8 14 23 34 50 77

3.8 4.5 5.1 5.3
33 33 42 50

40.6
4.60
43

40.3

✓

5.2 5.0 4.0 4.4 3.7 4.5 6.2 4.4 4.6 5.0 5.3 5.2 5.0 5.2
50 41 36 33 33 29 23 8 15 25 37 50 100

4.6 5.1 6.2
8 15 20

Sta + π - Elev

944.65

9+ 27

conc. Ent. 8' wide

+ 50

+ 92

T. P. 3.82 944.26 4.21 940.44

10

+ 50

+ 58

conc. Ent. 8' wide

11

Lt

A

Rt

39.99
4.66
43

40.5

40.5
40.0

3.6 3.9 4.4 5.9 4.9 4.5 4.2 4.4 4.8 5.2 5.3 5.1 4.6 4.0
32 30 26 21-19 13 8 7 14 18 21 34 50 74

4.4 4.0 5.1
32 36 50

40.5

✓ 4.7
93

5.0 4.3 3.7 3.9 3.2 5.8 4.2 4.3 4.7 5.3 5.1 5.0 4.8
50 40 35 32 32 23 7 13 24 33 50 75

4.5 4.9 5.8
9 15 21

40.5

39.8

3.0 2.7 4.2 5.3 4.3 4.0 3.8 3.9 4.3 5.2 4.5 4.4 ✓
32 31 26 22-20 13 8 7 14 25 39 50

3.6 4.3 4.5
32 45 50

40.5

40.0

4.76
40.0

4.9 4.3 3.9 3.3 3.6 5.6 3.8 4.0 4.6 4.7 4.3 3.6 2.5
50 40 33 33 28 24 7 16 26 36 50 74

4.1 4.5 5.4
7 16 22

40.93
3.82
43

40.4

40.3

✓

6.1 4.1 4.8 5.7 4.8 4.3 3.9 4.1 4.7 4.0 3.73 3.65
50 32 27 21-23 15 9 7 15 28 43 50

sta + Δ - Elev
944.26

11 +50

+86

12

+50

+92

13

+13 Approx & N. Grotto st

+27

Lt.

E

Rt.

40.2

39.3

41.26

H.O.

6.4 5.7 5.1 5.0 4.5 5.7 4.1 4.3 4.8 5.4 5.0 3.8 3.0
50 40 33 29 24-22 18) 7 14 21 30 50 74

4.4
8

4.8
13

40.1

✓

5.5 5.7 6.5 5.2 5.0 4.4 4.2 4.3 4.7 5.4 5.6 5.4 5.1 4.5
32 27 23-20 16 14 8 6 14 20 27 39 50 100

7.0
50

40.1

✓

7.2 5.5 6.4 5.1 4.6 4.2 4.4 4.7 5.8 5.7 5.2 4.4
50 32 24-21 16 9 7 13 20 29 50 100

39.9 46
8

✓ 39.56
H.O.

7.3 5.6 6.5 5.3 4.9 4.4 5.0 7.4 6.3 5.3 5.0 4.7
50 30 23-20 16 9 15 22-24 29 39 50 74

39.7

7.6 7.2 6.1 6.4 5.5 4.9 4.6 4.9 5.5 7.1 7.2 5 7.1 6.3 5.9
50 41 33 24-22 17 9 8 15 21 22 23 32 50

F.L. 15"
C.M.
W. End.

39.6

✓

7.5 7.0 6.0 6.3 5.4 4.9 4.7 4.9 5.6 6.1 6.4
50 41 31 23-21 15 7 8 20 33 50

39.6

✓

6.0 5.1 6.1 5.9 5.1 4.7 4.9 5.3 5.5 5.8 5.7 5.7
50 30 23-21 18 10 8 26 50 100 150 200

39.6

5.5 5.7 5.5 6.3 5.4 4.9 4.7 4.9 5.5 6.2 6.4
50 38 29 23-20 14 6 8 22 39 50

✓

Sta + π - Elev

944.26

13 + 32

+ 50

14

+ 50

B.M. 4.05 943.84 4.47 939.79

+ 57

side walk Lt.

15

+ 39

side walk Lt. & House

+ 50

16

+ 07

side walk Lt.

Lt

L

Rt

39.5

6.2	5.9	6.4	5.5	5.0	4.8	5.0	5.6	7.20	6.1	6.3	6.0	✓
50	31	23-20	14	9		8	14	22	29	37	50	

31.00
7.20
22
Fl. 15'
E. End
C. 111.

39.6

6.0	5.8	6.0	6.5	5.5	5.0	4.7	5.0	5.3	6.3	6.8	6.7	✓
50	37	28	23-20	14	9		8	16	24	34	50	

39.5

5.3	6.1	6.4	7.0	5.6	5.1	4.8	4.9	5.2	5.7	6.5	6.8	6.8	✓
50	36	26	23-20	15	9		6	12	18	24	36	50	

Ho.
3.9
73

39.5

4.5	5.6	6.4	6.9	7.2	5.6	5.1	4.8	5.0	5.3	6.3	6.3	6.0	✓
23	50	36	27	23-20	14	9		8	14	24	37	50	

Ho.

S. E. Cor. of lower step Ho⁴ 729 w. B²

5.28

39.4

43

6.4	6.3	6.3	6.2	5.4	4.8	4.4	4.5	4.5	4.8	4.8	✓
50	39	28	22-20	15	8		7	17	30	50	

Ho.

5.3

5.88

73

39.3

6.2	6.6	6.9	7.0	5.3	4.8	4.5	4.7	5.0	6.1	6.1	4.6	4.0	✓
50	34	25	22-20	15	9		7	13	21	24	29	50	

Ho.
3.4
81

39.4

5.3	5.8	6.3	6.6	5.1	4.8	4.4	4.7	4.9	5.1	4.9	✓
73	50	32	22-20	15	8		7	20	33	50	

5.72

43

Sta + π - Elev

943.84

16 +50

+75

Ho. & side walk ht. 4' wide

17

+29

+33

+50

8

+50

T.P. 5.10 942.93 6.01 937.83

19 ✓

Lt

E

Rt.

39.3

5.8	5.6	6.2	5.5	5.0	4.5	4.7	5.1	5.8	5.9	5.8	✓
50	28	23-20	15	8		8	14	23	34	50	

5.70	5.3
43	73

39.1

6.0	5.9	6.6	5.9	5.1	4.7	4.8	5.2	5.8	5.9	✓
50	34	24-21	17	10		6	13	22	50	

39.2

5.2	5.9	6.0	6.5	5.4	4.7	4.6	4.8	5.3	5.9	6.3	6.1	✓
73	50	28	23-20	14	6		6	15	22	34	50	

39.2

Duplicate + 29 on Lt.					4.6	4.9	5.3	5.5	5.7	5.4	✓
						8	16	26	38	50	

39.3

5.8	6.2	6.9	5.3	4.7	4.5	4.8	5.5	6.6	5.4	5.1	5.2
50	28	23-20	14	7		6	15	23-25	30	39	50

39.4

5.9	5.6	5.5	7.2	5.3	4.7	4.4	4.7	5.2	6.7	5.2	5.1	5.0
50	40	32	24-21	15	7		8	15	22-25	31	42	50

39.3

6.1	6.0	7.3	5.5	4.9	4.5	4.7	5.3	6.8	5.1	5.2
50	30	25-22	16	8		8	15	23-27	33	50

39.1

5.5	5.3	6.5	4.8	4.1	3.8	4.0	4.6	6.1	5.0	4.2
50	30	25-22	16	8		7	14	23-25	36	50

Sta + π - Elev

942.93

19 + 50

+82

+97

W. End 15" C.M. Culv.

20

+18

Approx $\pm$ St. Alban St.

+33

+37

+56

Lt.

♀

Rt

39.0

✓

6.1 5.9 6.7 4.7 4.3 3.9 4.2 4.8 6.4 5.1 4.8 4.2 3.2
50 30 25-22 14 8 7 16 24-27 31. 39 50 73

140

38.8

✓

6.5 5.9 7.0 5.0 4.5 4.1 4.4 5.0 6.3 5.1 4.6
50 33 27-24 16 7 7 16 23-26 30 50

21.38
6.45 = F.L.
25

38.7

✓

4.8 4.6 4.8 4.6 4.2 4.5 4.8 5.2 5.6 5.1
50 30 17 9 8 16 25 36 50

38.5

✓

4.2 4.5 5.1 4.9 4.8 4.4 4.4 4.7 4.9 5.5 6.4 7.2
150 100 50 31 13 6 10 27 50 100 150

38.6

✓

6.0 4.9 4.6 4.3 4.5 5.1 5.0 5.0 5.3
50 20 8 8 15 25 38 50

38.6

35.92

✓

5.6 4.8 4.5 4.8 4.6 4.3 4.5 5.4 (7.01) 5.9 5.5
50 38 26 16 8 7 18 26 36 50
F.A. E. End 15" C.M.

38.1

5.7 4.5 4.6 5.0 4.7 4.8 4.6 5.2 6.5 5.2 5.6 5.6
50 35 23 13 9 9 17 24-27 35 42 50

Sta	+	π	-	Elev
-----	---	-------	---	------

942.93

20 + 64

21

+50

22

+50

23

+50

T.P.	6.92	942.83	7.02	935.91
------	------	--------	------	--------

24

Lt

F

Rt

38.6

✓

5.9	6.3	7.1	5.3	4.8	4.3	4.5	5.0	6.7	5.7	5.4
50	35	24-22	15	8		8	16	24-27	31	50

38.6

✓

5.7	5.7	6.8	7.1	5.2	4.6	4.3	4.6	5.1	6.7	5.5	5.4
50	39	29	24-21	14	6		8	16	24-27	32	50

Ho
6.0
74

38.5

6.1	5.6	6.1	6.8	5.3	4.8	4.4	4.5	4.9	6.7	5.2	5.2
50	38	33	24-21	15	9		7	12	24-27	32	50

38.5

✓

6.1	5.9	6.8	5.2	4.7	4.4	4.6	5.2	7.0	5.0	4.8
50	31	25-22	15	7		8	15	25-28	33	50

38.4

✓

7.1	6.4	6.2	6.6	5.3	5.0	4.5	4.7	5.1	6.3	3.8	3.1
50	39	32	24-21	13	9		7	13	24-28	34	50

38.3

✓

7.5	6.8	7.4	5.6	5.0	4.6	5.0	5.6	6.3	4.0	3.5	3.3
50	33	25-22	15	9		9	18	25-28	33	38	50

38.3

✓

7.6	7.1	7.3	5.5	5.1	4.6	4.8	5.4	6.7	4.2	3.4
50	35	25-22	14	8		7	16	25-28	35	50

38.3

✓

7.6	7.0	7.0	5.5	4.8	4.5	4.7	5.3	6.6	4.3	3.5
50	32	23-21	15	7		8	16	25-28	34	50

Sta + π - Elev.

942.83

24 +50

25

+20

House Lt. 62'

+50

+92

X Drain 18" X 40 S.C.P

26

+07

+14

Lt

E

Rt

38.3

✓

7.4	7.1	7.2	5.4	4.8	4.5	4.8	5.2	6.7	4.0	4.4
50	34	25-22	14	7		7	14	25-28	33	50

38.2

✓

5.7	5.9	6.6	5.6	5.0	4.6	4.7	5.1	5.5	6.4	4.0	4.3
50	34	25-22	15	8		6	13	21	27-29	35	50

5.9

62

38.1

✓

5.6	5.6	6.9	5.9	5.1	4.7	4.8	5.0	6.9	6.6	4.5	5.2
50	35	25-22	16	8		8	16	25-28	32	36	50

34.8

4.9
9 38.3

34.9

5.9	5.6	7.6	(7.95)	5.8	4.5	4.7	5.7	(7.86)	7.1	6.6	5.6
50	35	26-24	(20 F.L.)	18		9	19	(20 F.L.)	27	32	36

38.3

5.7
50

✓

6.5	6.2	7.3	6.1	5.5	4.8	4.5		4.6	5.4	6.8	5.9	5.7
50	39	32-28	26	19	8			9	21	32	37	50

38.3

7.2	6.8	5.9	5.3	4.8	4.5	4.6	5.2	5.7	5.3	✓
50	35	30	20	9		10	28	38	50	

38.3

✓

5.7	5.5	4.7	4.5		4.6	4.9	5.0
50	32	9			13	28	50

Sta + $\bar{A}$ - Elev

942.83

26 + 25 Approx $\frac{1}{2}$ Mile St

B.M.			5.95	936.88	937.20
------	--	--	------	--------	--------

T.P.	7.93	943.40	7.36	935.47	
------	------	--------	------	--------	--

B.M.	4.56	944.31	3.65	939.75	
------	------	--------	------	--------	--

T.P.	4.05	944.32	4.04	940.27	
------	------	--------	------	--------	--

B.M.			6.26	938.06	938.12
------	--	--	------	--------	--------

Lt

C

Rt

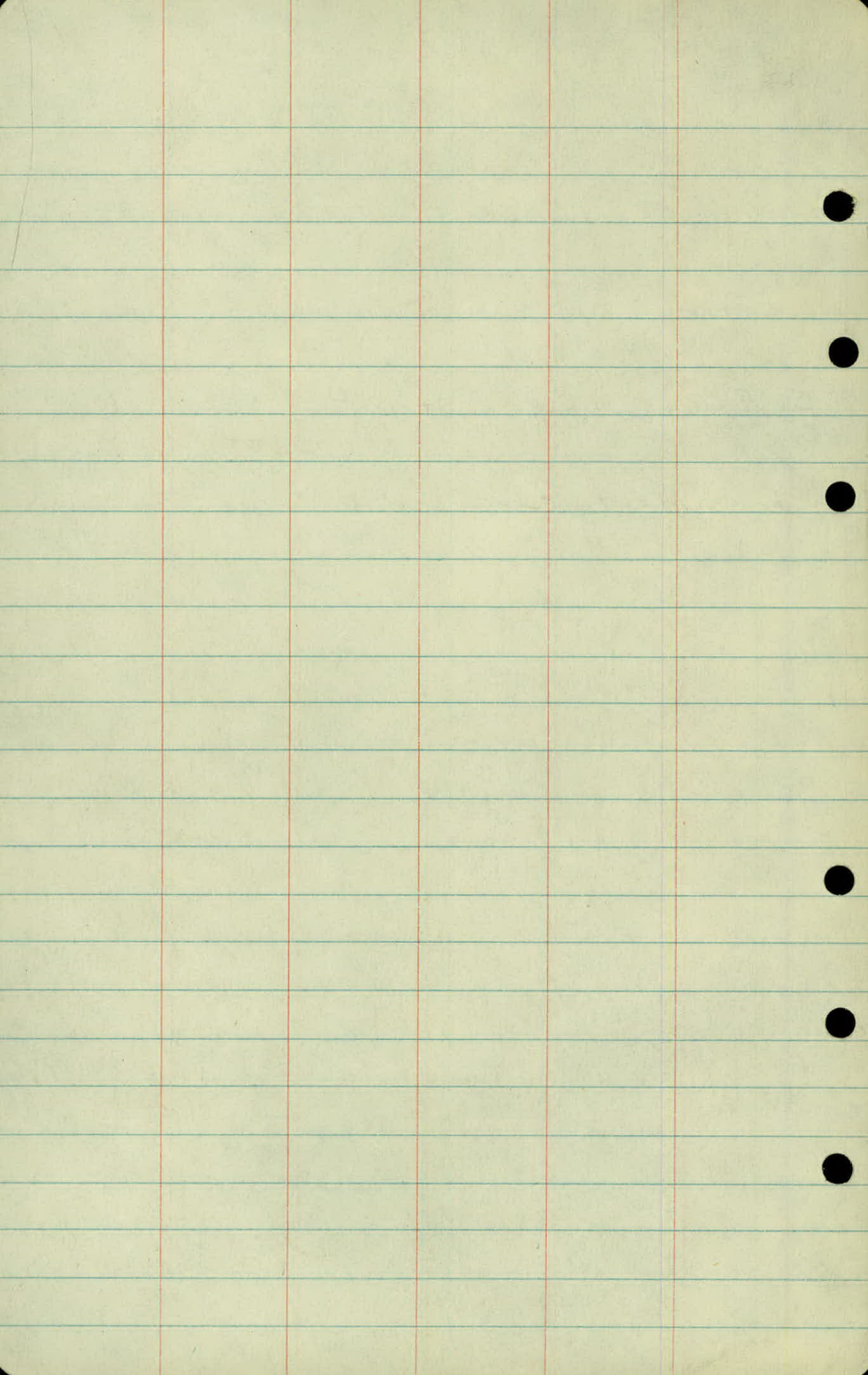
38.1

6.2	5.8	5.5	5.1	4.7	4.7	4.8	4.2	3.8
150	100	50	25		25	50	100	150

spike in p.p. N.W. Cor. Dale & B²

S.E. Cor. Lower step Ho. # 729 w. "B"²

Top Mont. cent. sec. 11



1
"B2" Victoria to Date

New x-Sections Left.

Sta 13 to 21

4 pages

Rid

6/24/54

Sta + π - Elev

BM 3.86 943.61 939.75

14

+55 Walk

15

+38 Walk

16

+04 Walk

FK
AM
EG

June 23, 1954

2

L Rd.

S.E. Cor Lower step Ho #729 Co Rd 82¹¹

38.1 38.3 37.9 37.4 38.4 38.9 39.4

4.9 5.3 5.7 6.2 5.2 4.7 4.2 ✓

44 35 27 23 18 12

38.56

5.05

44

Walk

37.3 37.3 37.6 38.1 39.4

6.3 6.3 6.0 4.9 4.2 ✓

50 35 24 12

37.96

5.65

44

38.1 37.6 37.3 38.3 38.8 39.4

5.5 6.0 6.3 5.3 4.8 4.2 ✓

50 33 23 17 11

38.10

5.51

43

Sta + π - Elev

943.61

16 + 74 Walk

17

+ 47 Walk

18

19

T.P. 2.91 942.95 3.57 940.04

+ 50 Ho

+ 73

Lt

L

38

38.11

5.50

44

37.8

37.7

37.4

38.4

38.8

39.2

5.8 5.9 6.2 5.2 4.8 4.4 ✓
 50 27 24 18 10

38.13

37.8

37.5

36.9

38.6

39.2

5.8 5.8 6.1 6.7 5.0 4.4 ✓
 43 35 28 24 15
 Walk

37.9

38.3

36.6

36.6

37.7

38.8

39.4

5.7 5.3 7.0 7.0 5.9 4.8 4.2 ✓
 50 33 26 23 20 12

37.2 37.8

37.6

36.5

36.5

38.1

38.5

39.2

6.4 5.8 6.0 7.1 7.1 5.3 5.1 4.4 ✓
 47 45 30 26 23 16 12

37.1

36.8

36.8

37.0

36.7

37.5

38.2

38.9

6.2 6.2 6.0 6.3 5.3 4.8 4.1 ✓
 40 50 28 21 18 11

Sta + x - Elev

942.95

7.00
6.50

20

+20 $\pm$ St. Albans

+50

+75

No Change Beyond

21

TP 2.03 940.98 4.00 938.95 36.88.

25790

527.20

FL No. End 18" SCP 6.13

at Dale St

14

2

37.4	38.0	38.0	37.7	38.3	38.8
56	50	50	53	47	42
50	30	20	16	11	

36.0	36.5	37.5	38.2	38.7
70	65	55	48	43
125	100	50	11	

37.1	37.3	37.7	37.7	38.2	38.7
59	57	53	53	48	43
50	39	30	19	10	

37.1	36.9	36.0	36.1	37.6	38.1	38.7
59	61	70	69	54	49	43
50	37	30	22	15	12	

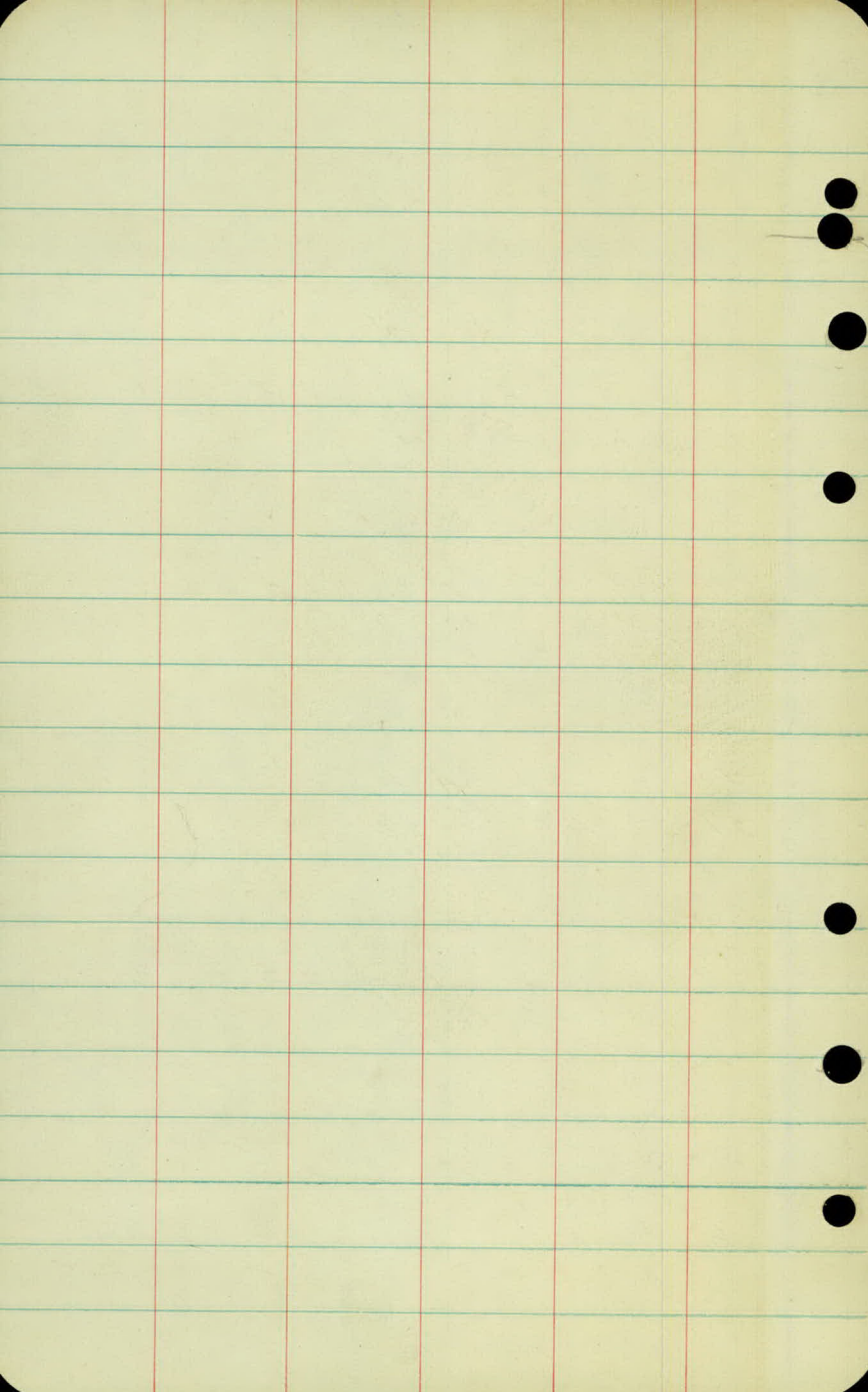
37.7	37.3	36.6	36.1	35.7	37.3	36.0	38.7
583	576	64	69	73	57	50	43
Walk 61	50	32	27	23	15	11	

34.85

6.13
N. End

34.96

6.02
S End



KP
JS

15 MAY 1961
WINDY 45°

1.

CO. RD. B2

GROTTO TO DALE

DITCH ELEVATIONS

9 (PAGES)

STA	+	π	-	ELEV
-----	---	-------	---	------

BM	2.99	102.99		
----	------	--------	--	--

100.0

0+00

2.99

+31

+51

1+00

+50

15 MAY 1961

2,

LT

~~E~~

RT

TOP ROAD ~~E~~ B₂ & GROTTO

~~E~~ B₂ AT GROTTO

97.58

00.0

5.41

3.0

23

FL 12" CM (W.)

97.41

00.0

5.58

3.0

23

FL 12" CM (E.)

97.9

99.9

5.1

3.1

23

97.9

99.9

5.3

3.1

STA	+	π	-	ELEV.
-----	---	-------	---	-------

102.99				
--------	--	--	--	--

1455				
------	--	--	--	--

1473				
------	--	--	--	--

1484				
------	--	--	--	--

2404				
------	--	--	--	--

450				
-----	--	--	--	--

LT

~~LT~~

RT

97.51

99.9

5.48 (w)

3.1

23

FL 12" CM

97.23

99.9

5.76 (E)

3.1

23

FL 12" CM

97.34

99.9

5.45

3.1

23

FL 12" CM (w)

97.23

99.8

5.76

3.2

23

FL 12" CM (E)

97.9

99.8

5.1

3.2

23

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		102.99		
--	--	--------	--	--

3+00				
------	--	--	--	--

+11				
-----	--	--	--	--

+31				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

15 MAY 1961

4.

LT

~~E~~

RT

99.7

5.3

99.7

3.3

99.38

5.61

23

FL 12" CM (W)

99.8

3.2

99.35

5.64

23

FL 12" CM (E)

99.7

3.3

99.9

5.1

99.7

3.3

99.82

5.17

23

TOP M-1

99.6

3.4

STA	+	π	-	ELEV.
-----	---	---	---	-------

		102.99		
--	--	--------	--	--

3486				
------	--	--	--	--

4400				
------	--	--	--	--

420				
-----	--	--	--	--

BM		2.99	100.00	
----	--	------	--------	--

15 MAY 1961

5.

LT

~~E~~

RT

97.09

99.6

5.90

3.4

23

FL 12" CM (W)

99.7

3.3

97.07

99.7

5.92

3.3

23

FL 12" CM

TOP ROAD ~~E~~ B2 & GROTTO

STA	+	π	-	ELEV.
-----	---	-------	---	-------

337		103.37		
-----	--	--------	--	--

				100.0
--	--	--	--	-------

0+00				
------	--	--	--	--

3+75				
------	--	--	--	--

+86				
-----	--	--	--	--

4+20				
------	--	--	--	--

+50				
-----	--	--	--	--

+64				
-----	--	--	--	--

LT

E

RT

6.

TOP ROAD BZ E' GROTTO

98.9

100.0

4.5

3.4

23

97.78

5.59

23

TOP MH

97.03

6.34

23

FL 12" CM (W)

97.10

6.37

23

FL 12" CM (E)

97.17

5.7

23

97.22

6.15

23

FL 12" CM (W)

99.8

3.6

99.9

3.5

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		103.37		
--	--	--------	--	--

4+83				
------	--	--	--	--

5+00				
------	--	--	--	--

+32				
-----	--	--	--	--

+78				
-----	--	--	--	--

6				
---	--	--	--	--

+50				
-----	--	--	--	--

LT

~~E~~

RT

91.35
6.02
23
FL 12" CM (E)

99.9
3.5

91.7
5.7
23

99.9
3.5

96.83
6.54
23
FL 12" CM (W)

99.9
3.5

96.44
6.93
23
FL 12" CM (E)

99.7
3.7

91.5
5.9

99.5
3.9

91.5
5.9

99.5
3.9

STA	+	π	-	ELEV
-----	---	-------	---	------

		103.37		
--	--	--------	--	--

6+86				
------	--	--	--	--

7+10	±	ST. ALBANS		
------	---	------------	--	--

7+24				
------	--	--	--	--

8+06				
------	--	--	--	--

+26				
-----	--	--	--	--

8+56				
------	--	--	--	--

LT

~~E~~

RT

8.

97.11

6.26

23

FL 15" CM (W)

98.1

5.0

23

99.1

96.1

6.66

23

FL 15" CM (E)

96.12

6.95

23

FL 15" CM (W)

96.17

6.90

23

FL 15" CM (E)

96.19

6.88

23

FL 15" CM (W)

99.3

4.1

99.2

4.2

99.1

4.3

STA	+	π	-	ELEV
		103.37		
8+76				
9+00				
9+25				
+45				
10+03				
+23				
BM			3.37	100.00 100.00

LT

~~4~~

RT

9.

96.53

99.1

6.84

4.3

23

FL 15" CM (E)

97.5

99.1

5.9

4.3

23

96.8

6.55

23

FL 15" CM (W)

96.39

6.98

23

FL 15" CM (E)

96.01

7.36

23

FL 15" CM (W)

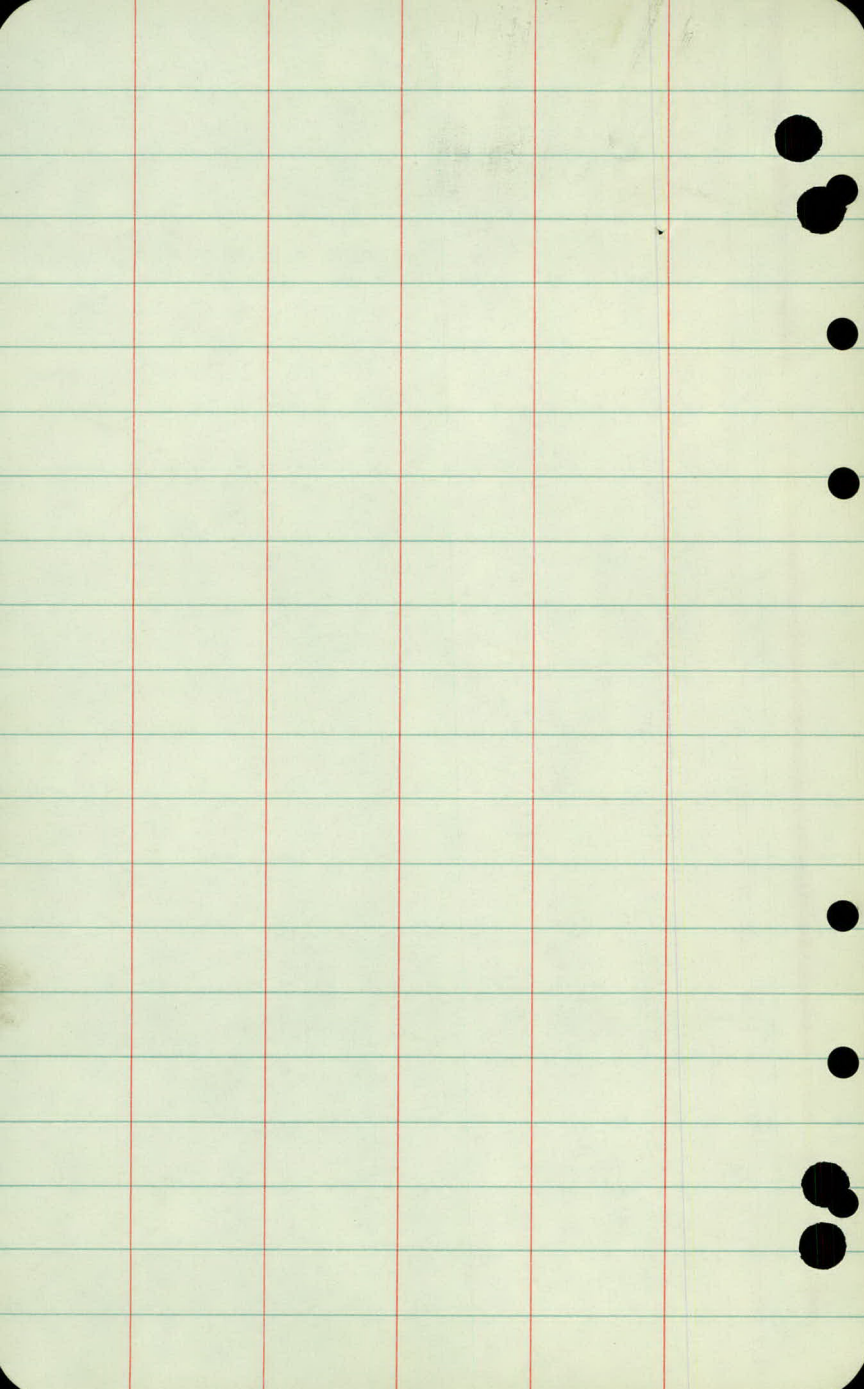
96.12

7.25

23

FL 15" CM (E)

TOP OF R-5 (GROSS)



12 JUNE 1962

Co. RD B2

VICTORIA TO GROTTO



$0700 = \frac{1}{2}$ VICTORIA : B2

VICTORIA

GROTTA

STA	+	π	-	ELEV.
BM	4.45	104.45		100.00
1+00				
✓				
2+00				
✓				
3+00				
+25				
+50				
4+00				

12 JUNE 1962

LT

£

RT

£ VICTORIA AND B²

101.4

3.1

101.4

3.1

101.5

3.0.

. 24.0.

100.5

4.0

101.6

2.9

101.6

2.9

100.7

3.8

101.5

3.0

100.4

4.1

STA + π - ELEV

104.45

4+50

LOT FROM STA
4+40⁺ TO 5+17⁺ ON
RT IS BEING FILLED.

5+00

+17 = PROPERTY LINE H/O # 808

+50

12 JUNE 1962

Lf

E

Rf

101.4

3.1

24.0

100.1

4.4

101.3

3.2

99.9

4.6

101.3

3.2

99.3

5.3

101.2

3.3

99.5

5.0

STA	+	π	-	ELEV
-----	---	-------	---	------

		104.45		
--	--	--------	--	--

6+00				
------	--	--	--	--

✓				
---	--	--	--	--

+18	=	W. END 12" CM		
-----	---	---------------	--	--

✓				
---	--	--	--	--

+38	=	E. END 12" CM		
-----	---	---------------	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

7+00				
------	--	--	--	--

+22	=	W END 12" CM		
-----	---	--------------	--	--

+42	=	E. END 12" CM		
-----	---	---------------	--	--

BM				
----	--	--	--	--

		4.45		
--	--	------	--	--

			100.00	
--	--	--	--------	--

				100.00
--	--	--	--	--------

12 JUNE 1962

101.3
3.2 - 24.0
99.5
5.0

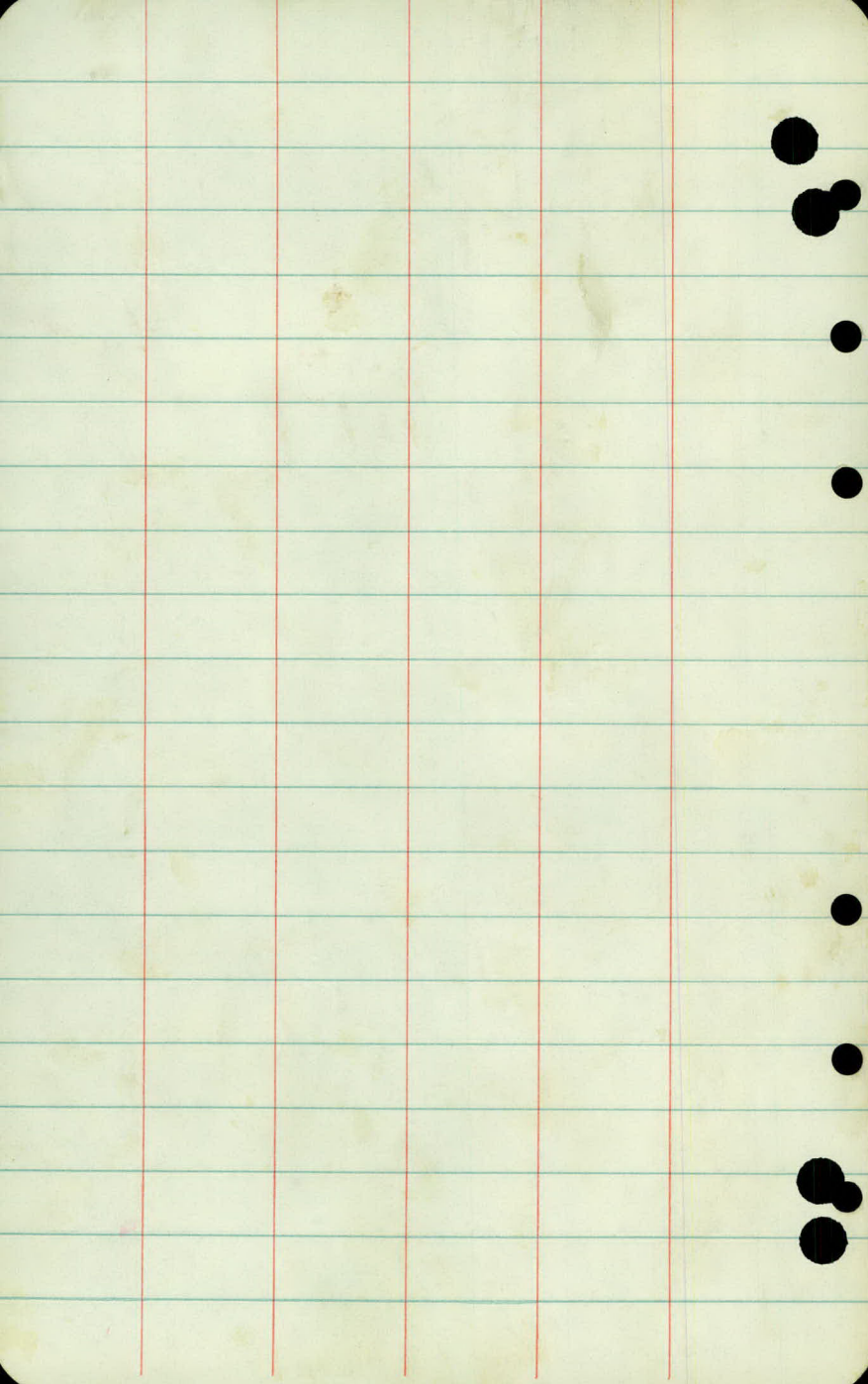
101.3
3.2
101.4
3.1
99.39
5.06
99.34
5.11

101.4
3.1
99.4
5.1

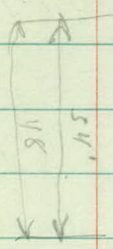
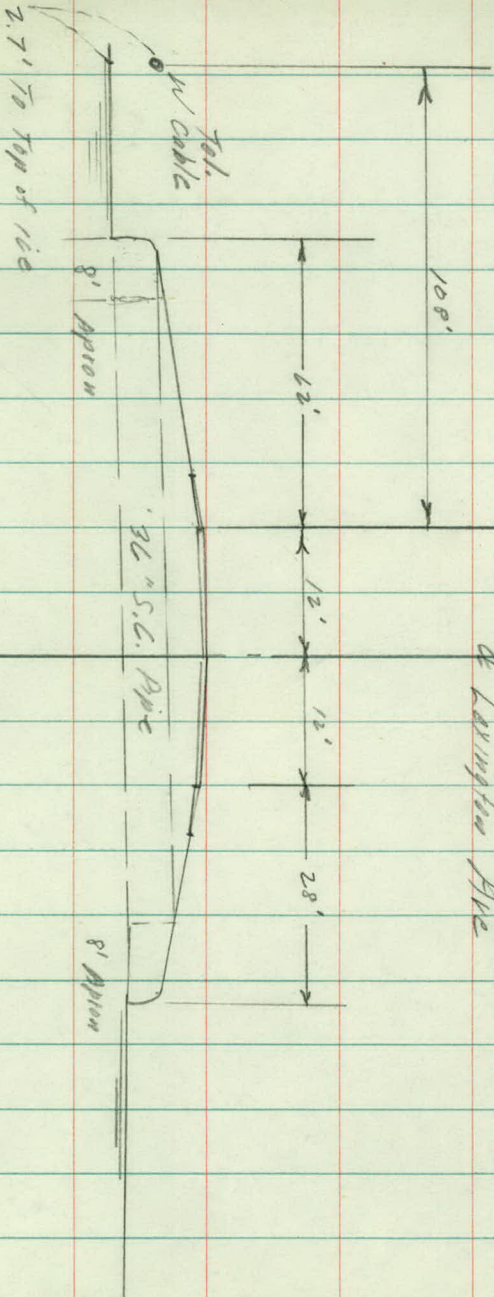
101.7
2.8
101.9
2.6
99.9
4.6
99.77
4.68

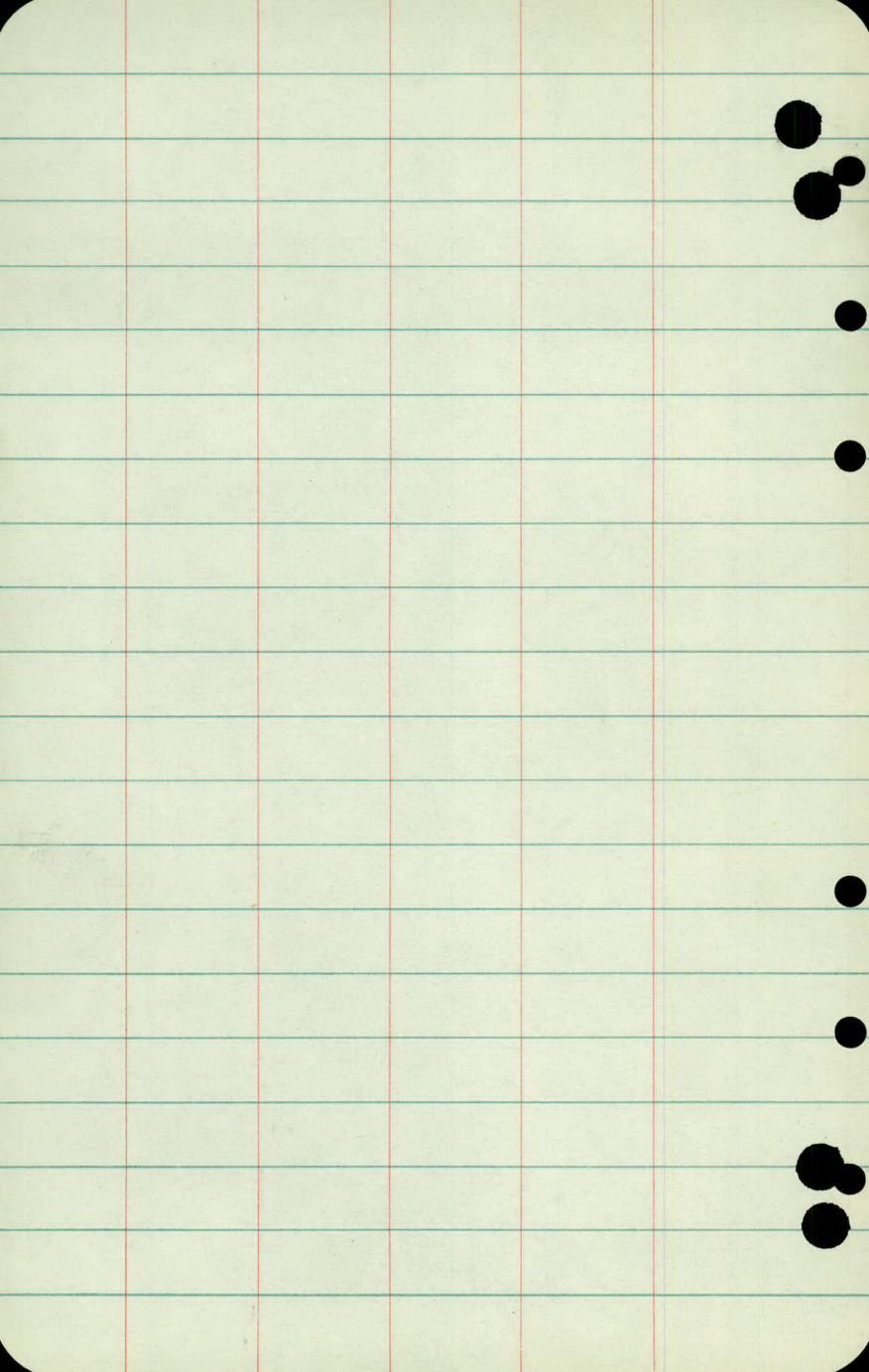
102.0
2.5
99.85
4.60

£ VICTORIA £ B²



2 Larington Ave

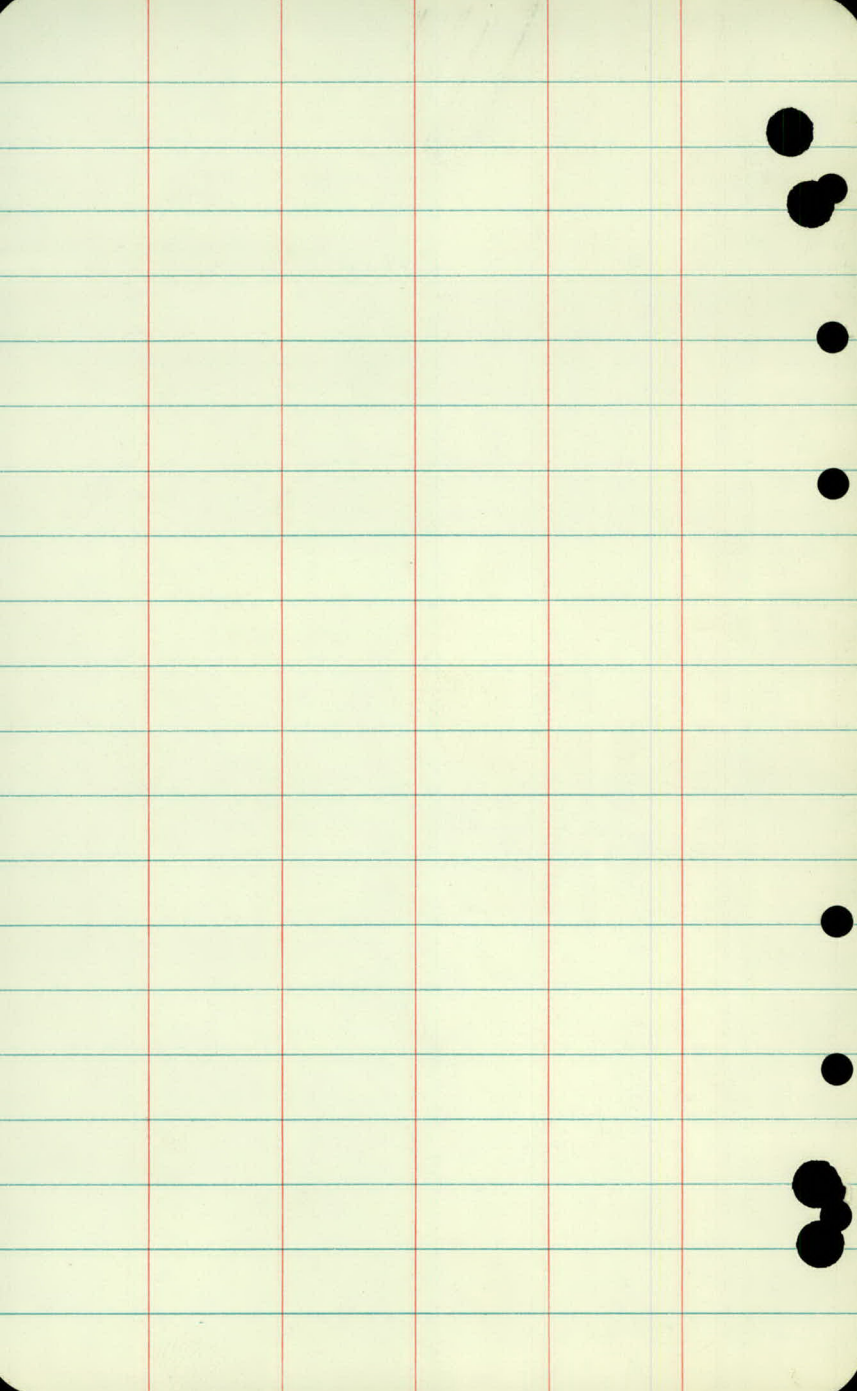




East
By New Brighton Rd

Drain at East Edge of Garage

1.5	1.3	1.5
2.6	2.4	2.6
3.4	3.2	3.5
4.0	3.9	4.1
4.4	4.3	4.4
4.9	4.6	4.9
5.1	4.8	5.1
5.2	5.0	5.2
S. Side 5.3	5.2	5.4 N. Side
5.4	5.4	5.6
5.6	5.4	5.7
5.6 at side 5.4 Drains	5.8	
← 5.6	5.3	5.7
5.5	5.1	5.5
5.4 T sign	4.8	5.4
5.1	4.6	5.1
4.9	4.4	4.8
4.6	4.2	4.7
4.3	4.0	4.4
4.2	3.8	4.3
	West	



Sept. 14, 1964

1

C. Rd B² Profile

Victoria to Dale

DRAINAGE

5 pages

Sta + π - Elev.

BM 4.72 943.54

938.82

BM 2.09 941.45

0+00 $\pm$ Victoria 38.0
5.5

+45 39.1
4.4

39.4

4.1

39.5

4.0

39.5

4.0

39.5

4.0

39.6

3.9

39.8

3.7

39.7

3.8

39.6

3.9

BM 2.33 944.12 1.75 941.79

39.5

4.6

FK
WS
GB
RP

Sept. 14, 1964

2

Rt

2

Spike in PP SE Cor. Victoria + B²

Top Hyd SE Cor. Victoria + B²

24 Rt

38.1

5.4

38.2

5.3

38.3

5.2

39.1

4.44

Yard Rt = 39.0
4.5

38.7

4.8

4.8

38.6

4.9

33'

Ent

38.8

4.7

38.5

5.0

38.5

5.0

38.8

4.7

33

Ent

Top Hyd Between Ho^{#s} 816 and 824

38.1

6.0

37.7

6.4

Kow Spot
Between House
23

Sta + π - Elev

944.12

5+50

39.5
4.6

6

39.5
4.6

+25

+50

39.7
4.4

7

39.9
4.2

+50

40.2
3.9

8

40.3
3.8

BM 3.58 945.35 2.35 941.77

+50

40.25
5.1

+80

9

40.25
5.1

+50

40.45
4.9

Sept 14, 1964
23 RT 3

39.15
6.2

39.25
6.1

63
33

39.55 Conc Ent
5.8 43

39.65
5.7

39.95
5.4

40.15
5.2

Top Hyd Between Ho # 7824 Ho # 790 B2

39.05
63

59
33

39.15
6.2 Conc Ent
5.44 43

38.95
64

Sta + π $\frac{L}{-}$ Elev.

945.35

10

40.45

4.9

+50

40.45

4.9

11

40.35

5.0

+50

40.15

5.2

1

12

40.05

5.3

+50

39.85

5.5

13

39.55

5.8

BM 3.03 943.67 4.71 940.64

BM 3.20 940.47 940.51

Sept 14, 1964 4
 Lt 22 Rt Rt 33 Rt

37.37
 6.3 6.0

37.59
 6.1 5.02
 Conc, Ent
 44

37.87
 5.8 5.0
 Ent

37.37
 6.3 5.8

37.17
 6.5 6.8

36.97
 6.7 6.6

10.8 9.1 8.4 7.5 6.6 6.3 6.7 6.9 7.1 7.1
 91 68 54 32 18 25 39 69 91 97
 Top Hyd SW. Cor. Grotto & Co Rd B2

NE Cor, Lower Step Ho #748 Grandview

Sta	Victoria	B ² → North	Elev
BM	1.04	939.86	938.82
0+00	± B ²	38.06 1.8	
0+40		37.16 2.7	
+78		35.86 4.0	
1		34.96 4.9	
+50		33.26 6.6	
2+09		31.16 8.7	
+50		29.36 10.5	
3	S. Side Sextant	26.86 13.0	
BM	1.28	928.13	13.01 926.85
+50	N. Side	23.53 4.6	
4+52		16.63 11.5	
BM		11.59	916.54

Sept. 14, 1964

E Side 5

Spike in P.P. SE Cor Victoria & B2

2.4
MH
27

2.7
³⁰
Bit Ent

48 28
18 33

6.9 4.7
18 33

9.0 8.68
20 30

11.1 9.7
19 33

13.7 13.2
21 33

Top Hyd NE Cor Sextant & Victoria

5.1 43
25 33

Top Hyd N.W. Cor. Transit & Victoria
11.6 11.08
21 Conc Ent
26

