

Bk.38 - Dr.11

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

_____ ELDRIDGE AVE _____

From _____ Cleveland Ave To 1/4 Mi. East _____

Road Acc't. No. R-15 _____

Filed 10-25-39

File _____

Plan Survey
~~Good Thru.~~

~~Lindig Property~~
Eldridge Ave
from Cleveland Ave. E.

8/18/39
R.O.P.
A.M.
L.C.
C.F.

Sta	Pt.	Angle Lt. Rt	Defl.
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13+15.83 P.O.T.

10+48.90 P.O.T.

0+00 E Cleveland Ave.

○

□

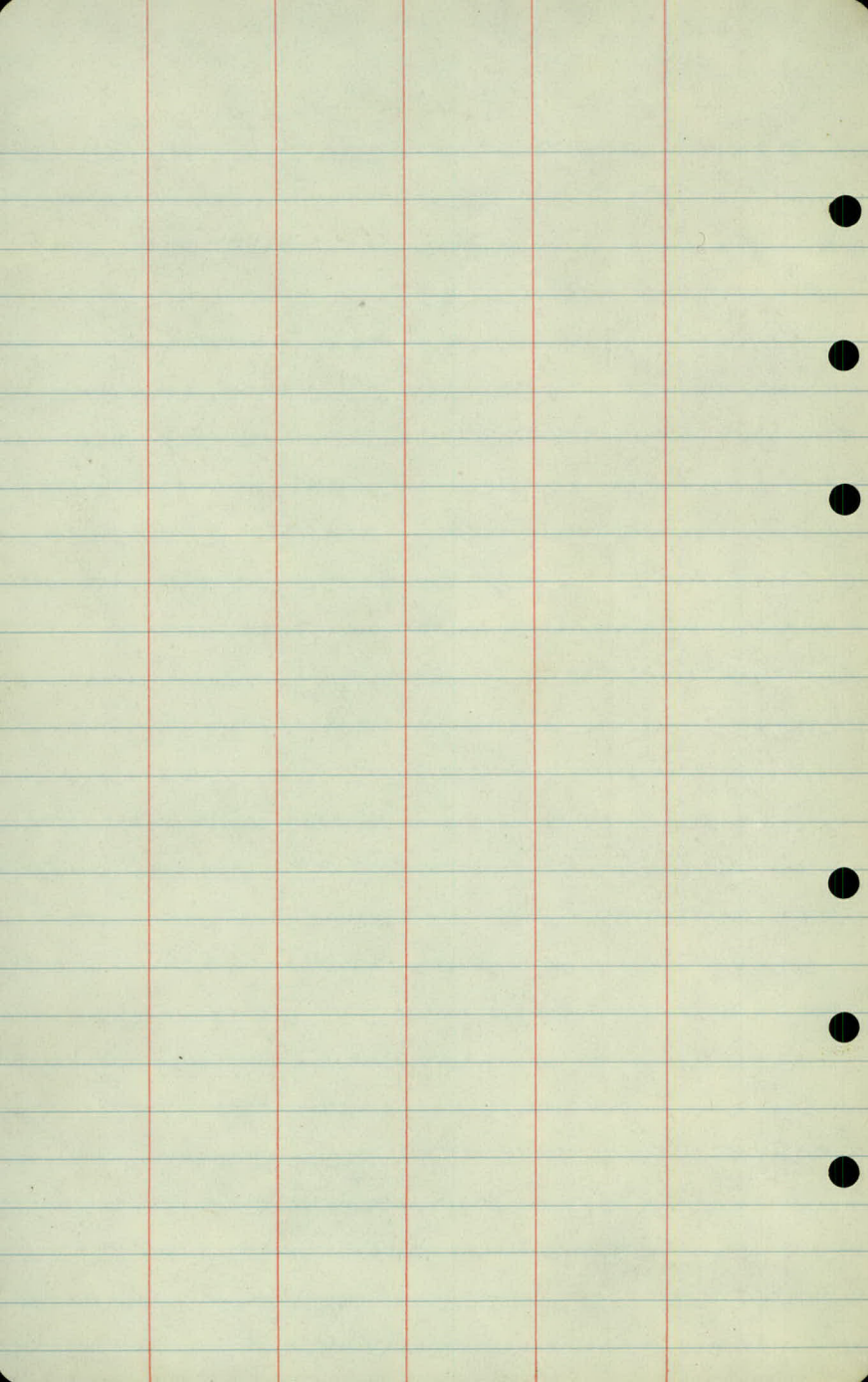
○

58.19

36.72

x second Iron
Fe Post from Cor.

○ Power Pole



Topography

6

5

4

3

2

1

0

+16 shldr xs 4

Pot Hole

+92 Pot Hole - 25-80

+52 Pot hole - 20-82

+56 Cor. Cult. 35'

Cultivated

+70 Cor. Gar. 78' 20'

+24 Cor. Ho - 58' 21' 26'

+87 P.P. - 20

Uncultivated

Uncultivated

+46 P.P. 19'

+92 Fe. Cor. 21'

Fe 22'

+73 P.P. - 19'

+65 A.P. 23'

+29 Fe. Cor. - 30'

Cleveland Ave. 22' B.T.

+ 29 Fc xs $\frac{1}{2}$.

13

12

11

10

9

8

7

Cultivated

x x x x x x x

Cultivated

Uncultivated

Uncultivated

+ 66 Cor. Cult. 35' —

17

16

15

14

Cross Sections.

Sta	+	π	-	Elev.
B.M.	3.67	976.96.		973.29
T.P.	3.23	972.35.	7.84	969.12.
B.M.	5.37		5.37	966.98.
0+00	E Cleveland		4.4	68.0.
+ 17			5.0	67.4.
+ 28			7.8	64.6.
+ 33	Special Ditch		10.5	61.9.
+ 50			8.4	64.0.
1			5.9	66.5.
+ 40			8.9	63.5.
2			10.0	62.4.
+ 50			9.8	62.6.
3			9.3	63.1.
+ 25			7.2	65.2.

Top Mon. Cleveland & "B"

Spike in P.P. S.W. Cor. Lindig Prop. Rd - Cleveland Ave

$$\begin{array}{r} 4.3 \\ 50 \end{array} \quad 4.4 \quad \begin{array}{r} 4.2 \\ 50 \end{array}$$

$$\begin{array}{r} 4.7 \\ 50 \end{array} \quad 5.0 \quad \begin{array}{r} 4.8 \\ 50 \end{array}$$

$$\begin{array}{r} 8.0 \\ 50 \end{array} \quad 7.8 \quad \begin{array}{r} 7.8 \\ 50 \end{array}$$

$$\begin{array}{r} 8.4 \\ 50 \end{array} \quad 10.5 \quad \begin{array}{r} 10.4 \\ 50 \end{array} \quad \begin{array}{r} 10.0 \\ 100 \end{array} \quad \begin{array}{r} 9.7 \\ 150 \end{array} \left(\begin{array}{l} \text{Pot hole} \\ 9.2 \end{array} \right)$$

$$\begin{array}{r} 7.6 \\ 50 \end{array} \quad 8.4 \quad \begin{array}{r} 8.4 \\ 24 \end{array} \quad \begin{array}{r} 7.7 \\ 50 \end{array}$$

$$\begin{array}{r} 8.4 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 12 \end{array} \quad 5.9 \quad \begin{array}{r} 4.3 \\ 20 \end{array} \quad \begin{array}{r} 3.7 \\ 50 \end{array}$$

$$\begin{array}{r} 10.2 \\ 50 \end{array} \quad \begin{array}{r} 9.8 \\ 24 \end{array} \quad 8.9 \quad \begin{array}{r} 7.4 \\ 16 \end{array} \quad \begin{array}{r} 5.8 \\ 35 \end{array} \quad \begin{array}{r} 3.8 \\ 50 \end{array}$$

$$\begin{array}{r} 10.3 \\ 50 \end{array} \quad \begin{array}{r} 10.0 \\ 23 \end{array} \quad 10.0 \quad \begin{array}{r} 9.2 \\ 21 \end{array} \quad \begin{array}{r} 7.3 \\ 50 \end{array}$$

$$\begin{array}{r} 10.1 \\ 50 \end{array} \quad \begin{array}{r} 10.0 \\ 30 \end{array} \quad 9.8 \quad \begin{array}{r} 9.3 \\ 21 \end{array} \quad \begin{array}{r} 7.5 \\ 50 \end{array}$$

$$\begin{array}{r} 9.8 \\ 50 \end{array} \quad 9.3 \quad \begin{array}{r} 8.0 \\ 22 \end{array} \quad \begin{array}{r} 7.0 \\ 31 \end{array} \quad \begin{array}{r} 6.0 \\ 50 \end{array}$$

$$\begin{array}{r} 8.5 \\ 50 \end{array} \quad \begin{array}{r} 8.0 \\ 15 \end{array} \quad 7.2 \quad \begin{array}{r} 5.9 \\ 22 \end{array} \quad \begin{array}{r} 3.7 \\ 50 \end{array}$$

Sta.	+	π	-	Elev.
		972.35		
3 + 50			5.9	66.5
T.P.	6.87	977.66	1.56	970.79
4			6.1	71.6
+ 10			5.6	72.1
+ 50			5.0	72.7
+ 82			5.7	72.0
5 + 25			6.1	71.6
+ 50			6.0	71.7
6			5.4	72.3
+ 50			6.3	71.4
+ 70	Center P. of Hole	6.4		71.3
7			5.7	72.0
+ 50			2.5	75.2

$$\begin{array}{r} 7.3 \\ 50 \end{array} \quad \begin{array}{r} 6.9 \\ 14 \end{array} \quad \begin{array}{r} 4.0 \\ 17 \end{array} \quad \begin{array}{r} 0.0 \\ 50 \end{array}$$

$$\begin{array}{r} 10.9 \\ 50 \end{array} \quad \begin{array}{r} 7.5 \\ 18 \end{array} \quad \begin{array}{r} 10.2 \\ 16 \end{array} \quad \begin{array}{r} 8.8 \\ 12 \end{array} \quad \begin{array}{r} 6.1 \\ 22 \end{array} \quad \begin{array}{r} 2.5 \\ 34 \end{array} \quad \begin{array}{r} 1.8 \\ 50 \end{array}$$

$$\begin{array}{r} 7.3 \\ 50 \end{array} \quad \begin{array}{r} 10.4 \\ 34 \end{array} \quad \begin{array}{r} 9.0 \\ 18 \end{array} \quad \begin{array}{r} 9.8 \\ 16 \end{array} \quad \begin{array}{r} 9.2 \\ 14 \end{array} \quad \begin{array}{r} 4.3 \\ 2 \end{array} \quad \begin{array}{r} 2.3 \\ 21 \end{array} \quad \begin{array}{r} 1.8 \\ 31 \end{array} \quad \begin{array}{r} 3.4 \\ 50 \end{array}$$

$$\begin{array}{r} 6.5 \\ 50 \end{array} \quad \begin{array}{r} 6.2 \\ 43 \end{array} \quad \begin{array}{r} 8.6 \\ 35 \end{array} \quad \begin{array}{r} 7.3 \\ 18 \end{array} \quad \begin{array}{r} 8.1 \\ 16 \end{array} \quad \begin{array}{r} 7.0 \\ 14 \end{array} \quad \begin{array}{r} 5.9 \\ 8 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array} \quad \begin{array}{r} 3.6 \\ 10 \end{array} \quad \begin{array}{r} 4.2 \\ 23 \end{array} \quad \begin{array}{r} 5.0 \end{array}$$

$$\begin{array}{r} 5.7 \\ 50 \end{array} \quad \begin{array}{r} 7.1 \\ 20 \end{array} \quad \begin{array}{r} 7.9 \\ 17 \end{array} \quad \begin{array}{r} 6.9 \\ 12 \end{array} \quad \begin{array}{r} 5.7 \\ 50 \end{array} \quad \begin{array}{r} 4.6 \\ 20 \end{array} \quad \begin{array}{r} 3.7 \\ 35 \end{array} \quad \begin{array}{r} 3.4 \\ 50 \end{array}$$

$$\begin{array}{r} 3.7 \\ 50 \end{array} \quad \begin{array}{r} 3.8 \\ 22 \end{array} \quad \begin{array}{r} 6.9 \\ 19 \end{array} \quad \begin{array}{r} 6.4 \\ 15 \end{array} \quad \begin{array}{r} 6.1 \\ 19 \end{array} \quad \begin{array}{r} 5.7 \\ 19 \end{array} \quad \begin{array}{r} 4.8 \\ 31 \end{array} \quad \begin{array}{r} 3.6 \\ 50 \end{array}$$

$$\begin{array}{r} 2.1 \\ 50 \end{array} \quad \begin{array}{r} 5.4 \\ 20 \end{array} \quad \begin{array}{r} 6.1 \\ 16 \end{array} \quad \begin{array}{r} 5.6 \\ 15 \end{array} \quad \begin{array}{r} 6.2 \\ 19 \end{array} \quad \begin{array}{r} 5.6 \\ 50 \end{array}$$

$$\begin{array}{r} 2.4 \\ 50 \end{array} \quad \begin{array}{r} 4.5 \\ 22 \end{array} \quad \begin{array}{r} 5.3 \\ 14 \end{array} \quad \begin{array}{r} 5.0 \\ 8 \end{array} \quad \begin{array}{r} 5.4 \\ 18 \end{array} \quad \begin{array}{r} 6.0 \\ 18 \end{array} \quad \begin{array}{r} 6.1 \\ 50 \end{array}$$

$$\begin{array}{r} 3.5 \\ 50 \end{array} \quad \begin{array}{r} 4.4 \\ 13 \end{array} \quad \begin{array}{r} 5.8 \\ 5 \end{array} \quad \begin{array}{r} 6.3 \\ 8 \end{array} \quad \begin{array}{r} 7.1 \\ 17 \end{array} \quad \begin{array}{r} 7.4 \\ 17 \end{array} \quad \begin{array}{r} 7.6 \\ 38 \end{array} \quad \begin{array}{r} 7.5 \\ 50 \end{array}$$

$$\begin{array}{r} 3.0 \\ 50 \end{array} \quad \begin{array}{r} 4.4 \\ 7 \end{array} \quad \begin{array}{r} 7.0 \\ 6.4 \end{array} \quad \begin{array}{r} 7.3 \\ 10 \end{array} \quad \begin{array}{r} 7.8 \\ 18 \end{array} \quad \begin{array}{r} 8.0 \\ 32 \end{array} \quad \begin{array}{r} 5.0 \\ 50 \end{array}$$

$$\begin{array}{r} 1.9 \\ 50 \end{array} \quad \begin{array}{r} 3.5 \\ 13 \end{array} \quad \begin{array}{r} 5.1 \\ 17 \end{array} \quad \begin{array}{r} 7.0 \\ 17 \end{array} \quad \begin{array}{r} 7.5 \\ 50 \end{array}$$

$$\begin{array}{r} 0.7 \\ 50 \end{array} \quad \begin{array}{r} 1.9 \\ 16 \end{array} \quad \begin{array}{r} 2.5 \\ 22 \end{array} \quad \begin{array}{r} 3.7 \\ 22 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array}$$

Sta.	+	π	-	Elev.
		977.66		
8			3.7	74.0
T.P.	12.62	987.34	2.14	974.72
+50			12.6	74.7
9			10.3	77.0
+50			22	80.1
10			3.3	84.0
T.P.	8.02	992.85	2.51	984.83
+41			6.3	86.6
+90			12.4	80.5
11 + 26			15.4	77.5
T.P.				
+50			16.4	76.5
T.P.	1.22	981.29	12.78	980.07
11 + 26				77.5
+50				76.5
T 86			60	75.3

$$\frac{3.2}{50} \quad \frac{3.4}{16} \quad 3.7 \quad \frac{4.1}{21} \quad \frac{4.7}{50}$$

$$\frac{11.6}{50} \quad \frac{12.2}{18} \quad 12.6 \quad \frac{13.2}{24} \quad \frac{13.8}{50}$$

$$\frac{9.4}{50} \quad \frac{10.4}{20} \quad 10.3 \quad \frac{10.2}{10} \quad \frac{9.5}{20} \quad \frac{9.7}{50}$$

$$\frac{5.7}{50} \quad \frac{6.8}{17} \quad \frac{7.7}{10} \quad 7.2 \quad \frac{7.0}{14} \quad \frac{7.3}{28} \quad \frac{7.3}{50}$$

$$\frac{2.1}{50} \quad \frac{3.1}{16} \quad \frac{4.0}{6} \quad 3.3 \quad \frac{3.4}{15} \quad \frac{4.0}{24} \quad \frac{5.6}{50}$$

$$\frac{4.5}{50} \quad \frac{5.7}{8} \quad 6.3 \quad \frac{8.1}{17} \quad \frac{10.1}{29} \quad \frac{12.2}{50}$$

$$\frac{0.8}{60} \quad \frac{2.8}{32} \quad \frac{4.0}{17} \quad \frac{7.4}{9} \quad \frac{12.4}{3} \quad 12.4 \quad \frac{12.8}{6} \quad \frac{15.6}{25} \quad \frac{17.5}{50}$$

$$\frac{5.0}{61} \quad \frac{8.9}{50} \quad \frac{9.6}{35} \quad \frac{8.4}{25} \quad \frac{10.3}{18} \quad \frac{11.7}{11} \quad \frac{15.5}{6} \quad 15.4$$

$$\frac{9.2}{64} \quad \frac{9.4}{47} \quad \frac{6.9}{38} \quad \frac{6.0}{30} \quad \frac{13.8}{12} \quad \frac{16.4}{7} \quad 16.4$$

3.8

$$\frac{5.3}{17} \quad \frac{6.5}{24} \quad \frac{7.9}{50}$$

4.8

$$\frac{6.2}{13} \quad \frac{7.4}{25} \quad \frac{8.3}{50}$$

$$\frac{3.5}{50} \quad \frac{4.4}{41} \quad \frac{5.7}{8} \quad 6.0 \quad \frac{6.8}{13} \quad \frac{7.7}{23} \quad \frac{8.5}{50}$$

Sta	+	⌒	-	Elev.
-----	---	---	---	-------

981.29

12+25			5.2	76.1
-------	--	--	-----	------

+50			5.7	75.6
-----	--	--	-----	------

+85			7.9	73.4
-----	--	--	-----	------

13			8.5	72.8
----	--	--	-----	------

+15.83			9.2	72.1
--------	--	--	-----	------

B.M.	8.32		8.32	972.97
------	------	--	------	--------

T.P.	8.72	986.58	3.43	977.86
------	------	--------	------	--------

T.P.	3.98	978.71	11.85	974.73
------	------	--------	-------	--------

T.P.	1.93	975.71	4.93	973.78
------	------	--------	------	--------

B.M.			8.65	967.06
------	--	--	------	--------

Turn Around

$$\begin{array}{r} 5.3 \\ \hline 50 \end{array} \quad \begin{array}{r} 4.6 \\ \hline 13 \end{array} \quad \begin{array}{r} 5.4 \\ \hline 7 \end{array} \quad 5.2 \quad \begin{array}{r} 5.6 \\ \hline 12 \end{array} \quad \begin{array}{r} 6.9 \\ \hline 25 \end{array} \quad \begin{array}{r} 8.5 \\ \hline 50 \end{array}$$

$$\begin{array}{r} 6.3 \\ \hline 50 \end{array} \quad \begin{array}{r} 5.9 \\ \hline 15 \end{array} \quad 5.7 \quad \begin{array}{r} 6.3 \\ \hline 15 \end{array} \quad \begin{array}{r} 7.2 \\ \hline 28 \end{array} \quad \begin{array}{r} 9.0 \\ \hline 50 \end{array}$$

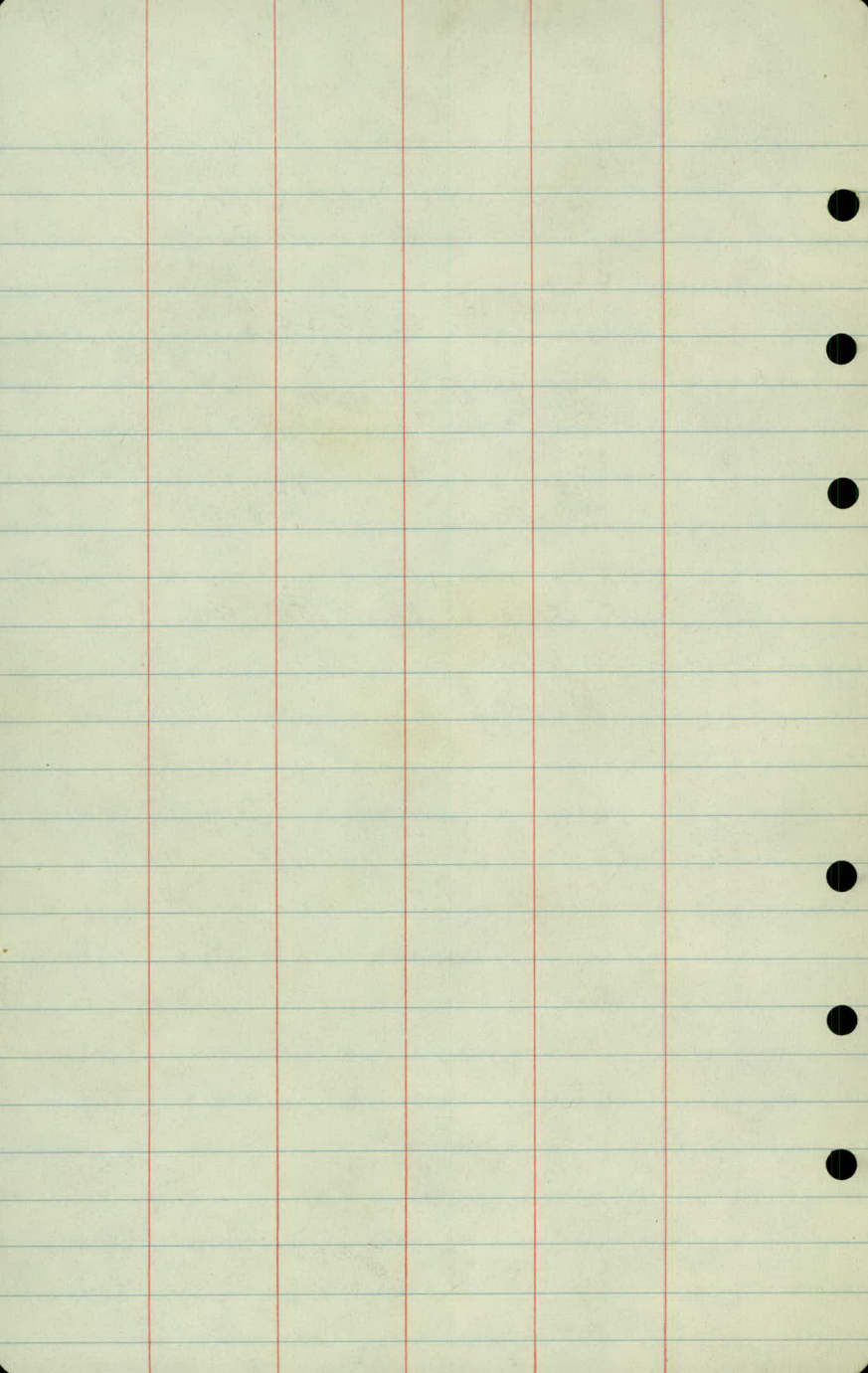
$$\begin{array}{r} 7.8 \\ \hline 75 \end{array} \quad \begin{array}{r} 7.6 \\ \hline 50 \end{array} \quad \begin{array}{r} 7.7 \\ \hline 10 \end{array} \quad \begin{array}{r} 8.1 \\ \hline 6 \end{array} \quad 7.9 \quad \begin{array}{r} 8.3 \\ \hline 18 \end{array} \quad \begin{array}{r} 10.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 10.1 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 7.3 \\ \hline 75 \end{array} \quad \begin{array}{r} 8.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 8.1 \\ \hline 24 \end{array} \quad 8.5 \quad \begin{array}{r} 8.8 \\ \hline 18 \end{array} \quad \begin{array}{r} 10.2 \\ \hline 50 \end{array} \quad \begin{array}{r} 10.2 \\ \hline 75 \end{array}$$

$$\begin{array}{r} 6.8 \\ \hline 75 \end{array} \quad \begin{array}{r} 8.0 \\ \hline 50 \end{array} \quad \begin{array}{r} 8.8 \\ \hline 31 \end{array} \quad \begin{array}{r} 8.9 \\ \hline 7 \end{array} \quad 9.2 \quad \begin{array}{r} 9.8 \\ \hline 15 \end{array} \quad \begin{array}{r} 10.4 \\ \hline 50 \end{array} \quad \begin{array}{r} 10.4 \\ \hline 75 \end{array}$$

Spike in 6" Birch 100' Rt. 13 + 25

Spike in P.P.



Ditch Survey

N.E. Cor. Cleveland & "B"

9/20/39 - 3 Pages

Party

R.R.

A.M.

L.G.

G.F.



24"x84" C.M.

273'

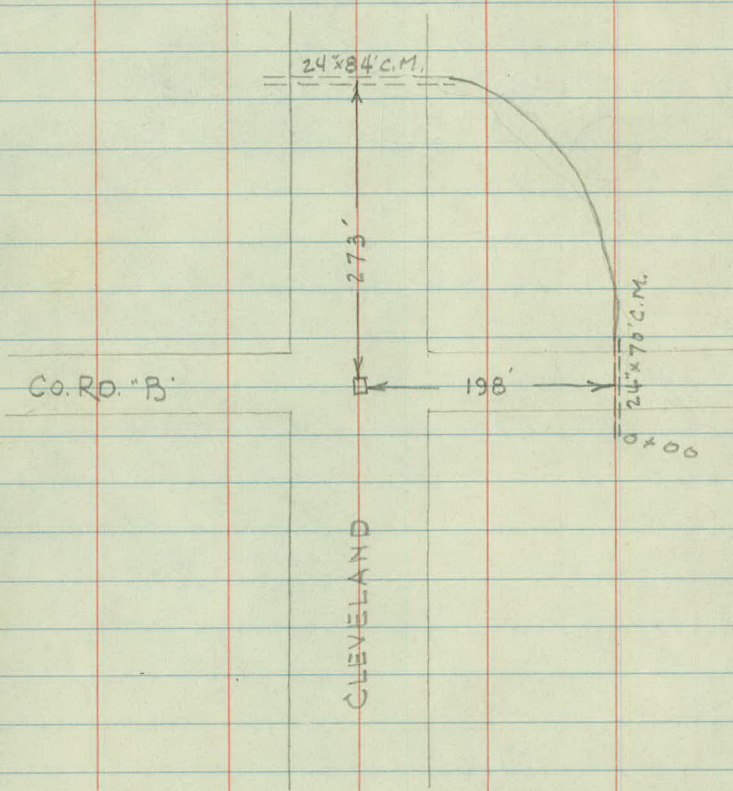
Co. Rd. "B"

198'

24"x70" C.M.

0'00"

CLEVELAND



Cross Sections
N.E. Cor. Cleveland & B.

Sta.	+	X	-	Elev.
B.M.	1.33	974.62	973.29	
0+00			13.39	61.23
+70			13.53	61.09
+70	Ditch		13.0	61.6
1+00			12.9	61.7
+50			13.1	61.5
2			13.0	61.6
+50			13.3	61.3
3			13.1	61.5
+50			13.4	61.2
+68	Ditch		13.7	60.9
+68			13.91	60.71
4+52			13.70	58.92
+52	Ditch		14.6	60.02
5	shot in Swamp.		16.0	58.6 W. side Cleveland
	Top water (9-20-39)		15.4	59.22

Top Mon. "B" & Cleveland

FL. S. End 24" x 70' C.M. under "B"

FL. N. End 24" x 70' C.M. under "B"

$\frac{11.9}{25}$ $\frac{11.5}{6}$ $\frac{11.2}{1}$ 12.9 $\frac{11.0}{1}$ $\frac{11.1}{8}$ $\frac{11.5}{25}$

$\frac{11.7}{25}$ $\frac{12.4}{7}$ $\frac{11.7}{1}$ 13.1 $\frac{12.2}{1}$ $\frac{12.6}{8}$ $\frac{12.8}{25}$

$\frac{12.2}{25}$ $\frac{12.5}{15}$ $\frac{12.2}{8}$ $\frac{12.1}{1}$ 13.0 $\frac{12.2}{1}$ $\frac{12.6}{8}$ $\frac{13.0}{25}$ $\frac{13.3}{35}$ ^{Low spot}

$\frac{10.8}{25}$ $\frac{11.5}{20}$ $\frac{12.0}{6}$ $\frac{11.6}{1}$ 13.3 $\frac{11.9}{1}$ $\frac{12.1}{6}$ $\frac{12.3}{15}$ $\frac{12.2}{25}$

$\frac{9.7}{25}$ $\frac{10.0}{11}$ $\frac{10.1}{4}$ 13.1 $\frac{11.4}{3}$ $\frac{9.9}{5}$ $\frac{10.3}{12}$ $\frac{10.0}{25}$

Ditch 2' Bottom Vertical Slopes

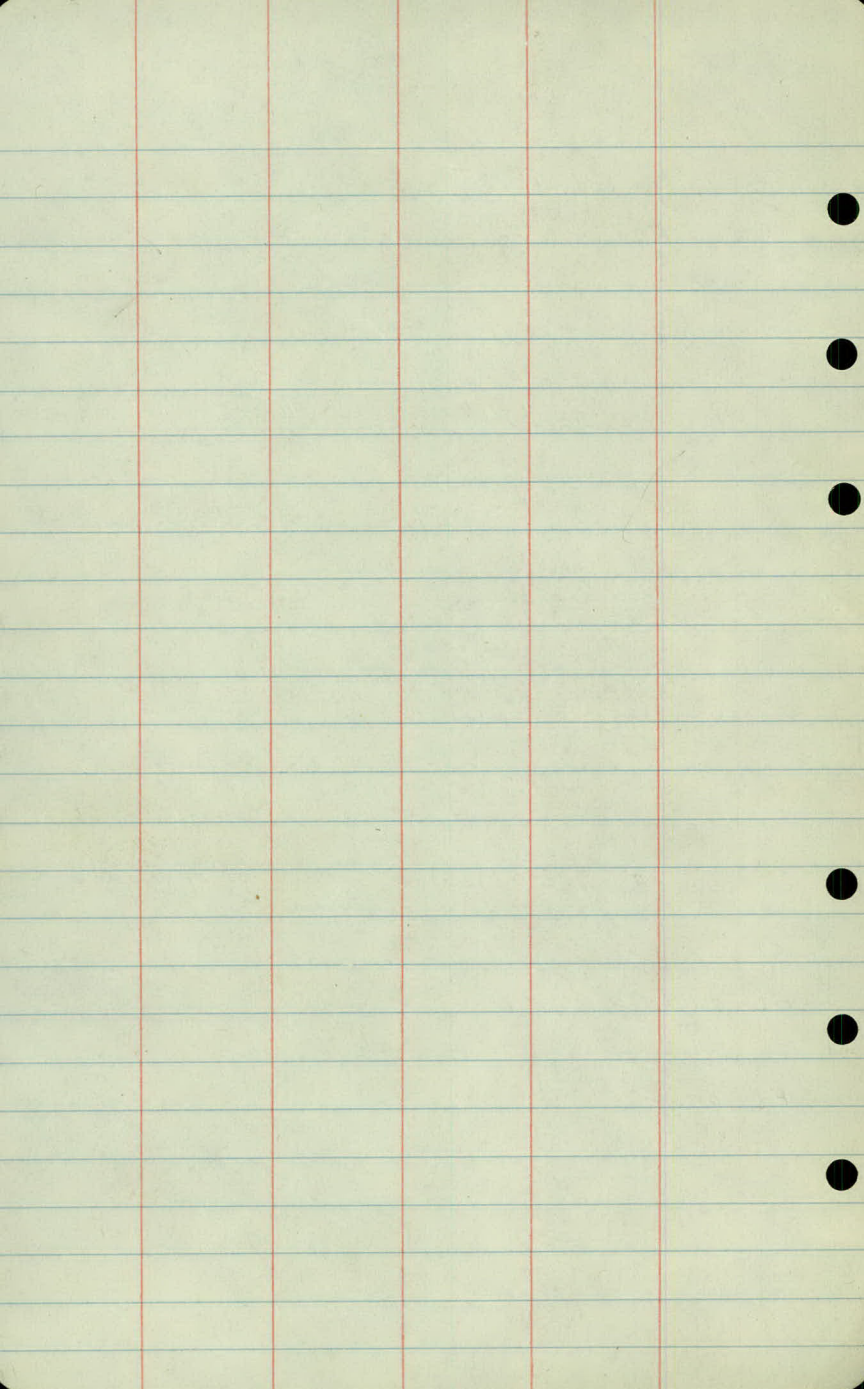
Note

Shldr. $\frac{7.1}{17}$ Toe $\frac{10.2}{12}$ $\frac{10.5}{9}$ $\frac{10.2}{5}$ 13.4 $\frac{11.2}{3}$ $\frac{10.6}{6}$ $\frac{9.0}{10}$ $\frac{9.5}{15}$ $\frac{9.3}{25}$

F.L. 24" x 84' C.M.

Under Cleveland.

F.L. 24" x 84' C.M.



Slope Stokes

Eldridge Ave

from Cleveland. 1315' EAST

staked- 10-6-39

Party:
R. P.
A. M.
L. G.
C. F.

5 pages.

Sta.	+	π	-	Elev.
B.M	4.13	971.11		966.98
0 + 28				67.3
+ 50				67.3
1				67.2
+ 40				67.1
2				67.1
+ 50				67.5
3				68.0
+ 25				68.5
+ 50				68.9
T.P.	10.80	977.66	4.25	966.86
4				69.9
+ 10				70.0
+ 50				70.7

Spike in P.P. S.W. Cor Cleveland & Eldridge

3.8 5.3	$\begin{array}{r} 6.1 \\ F2.3 \\ \hline 17.6 \end{array}$	$\begin{array}{r} 6.6 \\ F2.8 \\ \hline 18.2 \end{array}$	$\begin{array}{r} 6.4 \\ F2.6 \\ \hline 18.2 \end{array}$
3.8 5.3	$\begin{array}{r} 6.6 \\ F2.8 \\ \hline 18.6 \end{array}$	$\begin{array}{r} 7.5 \\ F3.7 \\ \hline 20.4 \end{array}$	$\begin{array}{r} 7.5 \\ F3.7 \\ \hline 20.4 \end{array}$
3.9 5.4	$\begin{array}{r} 6.2 \\ F2.3 \\ \hline 17.6 \end{array}$	$\begin{array}{r} 4.7 \\ F0.8 \\ \hline 24.8 \end{array}$	$\begin{array}{r} 3.0 \\ C0.9 \\ \hline 24.8 \end{array}$
4.0	$\begin{array}{r} 8.6 \\ F4.6 \\ \hline 22.2 \end{array}$	$\begin{array}{r} 7.7 \\ F3.7 \\ \hline 17.4 \end{array}$	$\begin{array}{r} 6.2 \\ F2.2 \\ \hline 17.4 \end{array}$
4.0	$\begin{array}{r} 8.8 \\ F4.8 \\ \hline 22.6 \end{array}$	$\begin{array}{r} 8.7 \\ F4.7 \\ \hline 21.2 \end{array}$	$\begin{array}{r} 8.1 \\ F4.1 \\ \hline 21.2 \end{array}$
3.6	$\begin{array}{r} 8.9 \\ F5.3 \\ \hline 23.6 \end{array}$	$\begin{array}{r} 8.7 \\ F5.1 \\ \hline 21.6 \end{array}$	$\begin{array}{r} 7.9 \\ F4.3 \\ \hline 21.6 \end{array}$
3.1	$\begin{array}{r} 8.5 \\ F5.4 \\ \hline 23.8 \end{array}$	$\begin{array}{r} 8.1 \\ F5.0 \\ \hline 20.4 \end{array}$	$\begin{array}{r} 6.8 \\ F3.7 \\ \hline 20.4 \end{array}$
2.6	$\begin{array}{r} 7.1 \\ F3.5 \\ \hline 20.0 \end{array}$	$\begin{array}{r} 5.9 \\ F3.3 \\ \hline 17.4 \end{array}$	$\begin{array}{r} 4.8 \\ F2.2 \\ \hline 17.4 \end{array}$
2.2	$\begin{array}{r} 5.7 \\ F3.5 \\ \hline 20 \end{array}$	$\begin{array}{r} 4.7 \\ F2.5 \\ \hline 23.0 \end{array}$	$\begin{array}{r} 2.2 \\ C0.0 \\ \hline 23.0 \end{array}$
7.8	$\begin{array}{r} 9.8 \\ F2.0 \\ \hline 17.0 \end{array}$	$\begin{array}{r} 6.1 \\ C1.7 \\ \hline 30 \end{array}$	$\begin{array}{r} 1.9 \\ C5.9 \\ \hline 30 \end{array}$
7.7	$\begin{array}{r} 9.0 \\ C0.2 \\ \hline 20.4 \end{array}$	$\begin{array}{r} 5.6 \\ C2.1 \\ \hline 30 \end{array}$	$\begin{array}{r} 1.8 \\ C5.9 \\ \hline 30 \end{array}$
7.0	$\begin{array}{r} 7.5 \\ C0.10 \\ \hline 22.0 \end{array}$	$\begin{array}{r} 5.1 \\ C1.9 \\ \hline 30 \end{array}$	$\begin{array}{r} 3.5 \\ C3.5 \\ \hline 30 \end{array}$

Sta.	+	π	-	Σ lev.
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977.66⁷

4+82

71.2

5 +25

71.9

+50

72.3

6

73.0

+50

73.7

+70

74.0

7

74.4

T.P

4.42

979.13

2.95

974.71

+50

75.1

8

75.8

+50

76.5

T.P

12.00

989.56⁶

1.57

977.56

9

77.2

6.5	$\begin{array}{r} 7.0 \\ DC 1.0 \\ \hline 22.0 \end{array}$	$\begin{array}{r} 5.8 \\ CO.7 \\ \hline \end{array}$	$\begin{array}{r} 4.1 \\ C 2.1 \\ \hline 27.8 \end{array}$
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5.8	$\begin{array}{r} 5.6 \\ CO.2 \\ \hline 23.4 \end{array}$	$\begin{array}{r} 6.2 \\ FO.4 \\ \hline \end{array}$	$\begin{array}{r} 3.2 \\ CO.6 \\ \hline 24.2 \end{array}$
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5.4	$\begin{array}{r} 4.9 \\ CO.5 \\ \hline 24.0 \end{array}$	$\begin{array}{r} 5.8 \\ FO.4 \\ \hline \end{array}$	$\begin{array}{r} 6.6 \\ DC 0.3 \\ \hline 20.6 \end{array}$
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4.7	$\begin{array}{r} 4.3 \\ CO.4 \\ \hline 23.8 \end{array}$	$\begin{array}{r} 5.3 \\ FO.6 \\ \hline \end{array}$	$\begin{array}{r} 6.2 \\ DC 0.0 \\ \hline 20.0 \end{array}$
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4.0	$\begin{array}{r} 4.2 \\ DC 1.3 \\ \hline 22.6 \end{array}$	$\begin{array}{r} 6.4 \\ F 2.4 \\ \hline \end{array}$	$\begin{array}{r} 7.4 \\ F 3.4 \\ \hline 19.8 \end{array}$
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3.7	$\begin{array}{r} 4.1 \\ DC 1.1 \\ \hline 22.2 \end{array}$	$\begin{array}{r} 6.5 \\ F 2.8 \\ \hline \end{array}$	$\begin{array}{r} 7.4 \\ F 3.7 \\ \hline 20.4 \end{array}$
-----	---	---	--

3.3	$\begin{array}{r} 3.5 \\ DC 1.3 \\ \hline 22.6 \end{array}$	$\begin{array}{r} 5.6 \\ F 2.3 \\ \hline \end{array}$	$\begin{array}{r} 6.9 \\ F 3.6 \\ \hline 20.2 \end{array}$
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Top Rock.

4.1	$\begin{array}{r} 3.0 \\ CO 1.1 \\ \hline 25.2 \end{array}$	$\begin{array}{r} 4.0 \\ CO.1 \\ \hline \end{array}$	$\begin{array}{r} 5.2 \\ DC 0.4 \\ \hline 20.8 \end{array}$
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3.3	$\begin{array}{r} 4.8 \\ DC 0.0 \\ \hline 20.0 \end{array}$	$\begin{array}{r} 5.2 \\ F 1.9 \\ \hline \end{array}$	$\begin{array}{r} 5.5 \\ F 2.2 \\ \hline 17.4 \end{array}$
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2.6	$\begin{array}{r} 4.0 \\ DC 0.1 \\ \hline 20.2 \end{array}$	$\begin{array}{r} 4.5 \\ F 1.9 \\ \hline \end{array}$	$\begin{array}{r} 4.7 \\ F 2.1 \\ \hline 17.2 \end{array}$
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Stake Sta 9000

12.4	$\begin{array}{r} 12.8 \\ DC 1.1 \\ \hline 28.9 \end{array}$	$\begin{array}{r} 13.6 \\ F 0.2 \\ \hline \end{array}$	$\begin{array}{r} 11.7 \\ CO.7 \\ \hline 24.4 \end{array}$
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Sta	+	π	-	Elev.
		989.56		
9+50				77.9
10				78.4
+41				78.5
T.P.	6.16	993.73	1.99	987.57
+90				78.2
11 +26				77.7
+50				77.3
T.P.	0.48	981.35	12.86	980.87
+86				77.6
12 +25				75.8
+50				75.3
+85				74.6

11.7

$$\begin{array}{r} 8.8 \\ C2.9 \\ \hline 28.8 \end{array}$$

$$\begin{array}{r} 7.5 \\ C2.2 \\ \hline \end{array}$$

$$\begin{array}{r} 9.2 \\ C2.5 \\ \hline 28.0 \end{array}$$

11.2

$$\begin{array}{r} 5.5 \\ C5.7 \\ \hline 34.4 \end{array}$$

$$\begin{array}{r} 5.6 \\ C5.6 \\ \hline \end{array}$$

$$\begin{array}{r} 6.3 \\ C4.9 \\ \hline 30 \end{array}$$

11.1

$$\begin{array}{r} 4.5 \\ C9.6 \\ \hline 42.2 \end{array}$$

$$\begin{array}{r} 3.1 \\ C8.0 \\ \hline \end{array}$$

$$\begin{array}{r} 6.9 \\ C4.2 \\ \hline 30 \end{array}$$

15.5

$$\begin{array}{r} 2.6 \\ C12.9 \\ \hline 48.8 \end{array}$$

$$\begin{array}{r} 13.3 \\ C2.2 \\ \hline \end{array}$$

$$\begin{array}{r} 15.9 \\ DC1.1 \\ \hline 22.2 \end{array}$$

16.0

$$\begin{array}{r} 10.3 \\ C5.7 \\ \hline 34.4 \end{array}$$

$$\begin{array}{r} 16.2 \\ F0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 17.9 \\ F1.9 \\ \hline 16.8 \end{array}$$

16.4

$$\begin{array}{r} 8.6 \\ C9.8 \\ \hline 38.6 \end{array}$$

$$\begin{array}{r} 17.4 \\ F1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 19.2 \\ F2.8 \\ \hline 18.6 \end{array}$$

3.8

$$\begin{array}{r} 5.0 \\ DC0.3 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 6.2 \\ F2.4 \\ \hline \end{array}$$

$$\begin{array}{r} 7.3 \\ F3.5 \\ \hline 20.0 \end{array}$$

5.6

$$\begin{array}{r} 5.3 \\ C0.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 5.2 \\ C0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ DC0.6 \\ \hline 21.2 \end{array}$$

6.1

$$\begin{array}{r} 6.3 \\ DC1.3 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 5.9 \\ C0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.8 \\ DC0.8 \\ \hline 21.6 \end{array}$$

6.8

$$\begin{array}{r} 7.6 \\ F0.8 \\ \hline 60.0 \end{array}$$

$$\begin{array}{r} 8.0 \\ DC0.3 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 8.1 \\ F1.3 \\ \hline \end{array}$$

$$\begin{array}{r} 8.3 \\ DC0.0 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 10.3 \\ F3.5 \\ \hline 60.0 \end{array}$$

Sta + π — Elev.

981.35⁴

13

74.3

+15.83

13 M.

8.43

972.92

972.97

7.1

$$\begin{array}{r} 7.7 \\ F0.6 \\ \hline 60 \end{array}$$

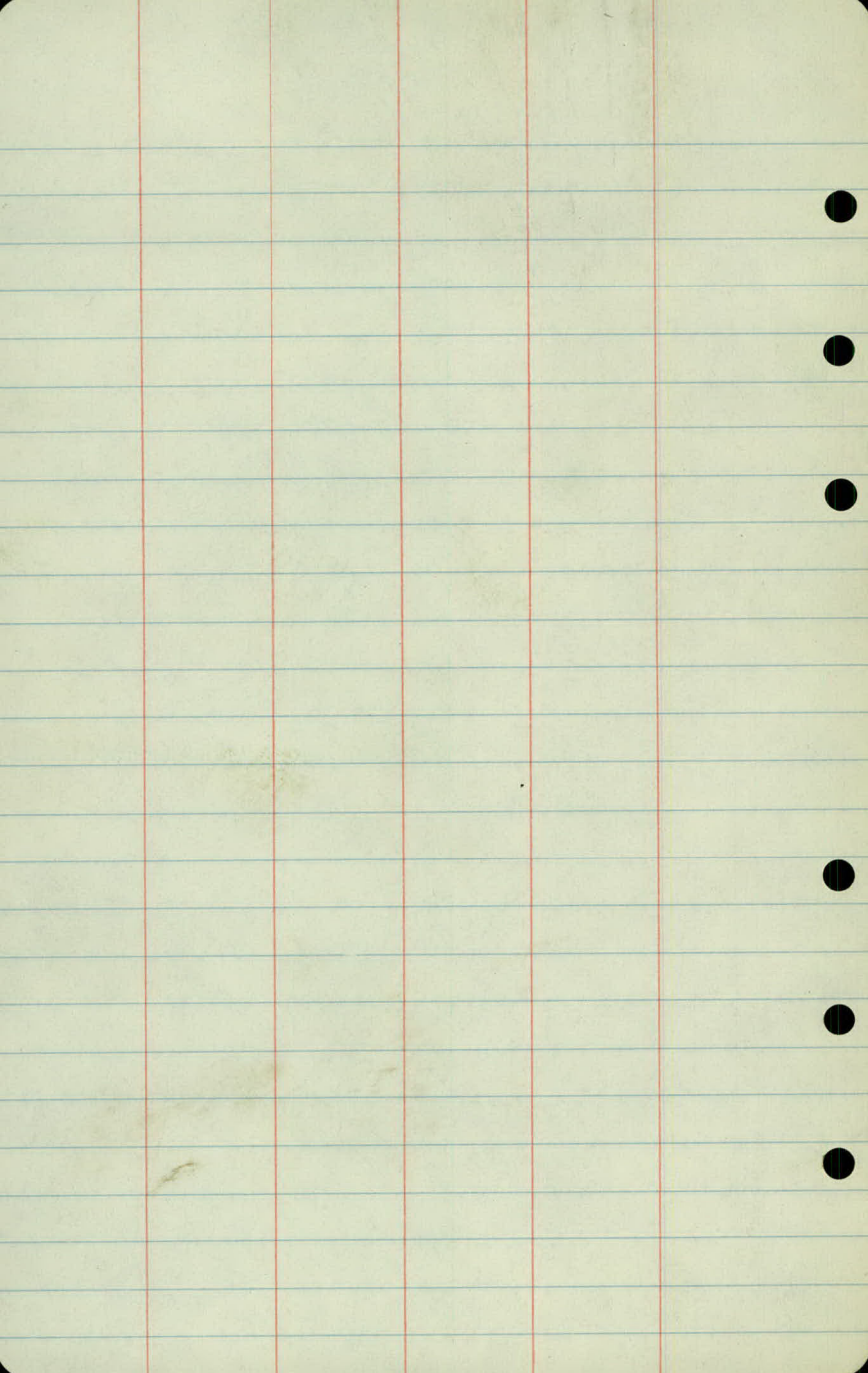
$$\begin{array}{r} 8.6 \\ F1.5 \\ \hline \end{array}$$

$$\begin{array}{r} 10.4 \\ F3.3 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 7.6 \\ F0.5 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 10.7 \\ F3.6 \\ \hline 60 \end{array}$$

Spike 6" Birch 100' Rt. 13+25.



ELDRIDGE ROAD

Slope Stakes
from Cleveland 1316' East

5/2/40

R. P.
A. M.
L. G.
C. F.

Sta.	+	π	-	Elev.
B.M.	4.88	971.86	971.86	166.98
0 + 00	± Cleveland			

+28				67.3	4.6
-----	--	--	--	------	-----

+50				67.3	4.6
-----	--	--	--	------	-----

1				67.2	4.7
---	--	--	--	------	-----

+40				67.1	4.8
-----	--	--	--	------	-----

2				67.1	4.8
---	--	--	--	------	-----

+50				67.5	4.4
-----	--	--	--	------	-----

3				68.0	3.9
---	--	--	--	------	-----

+50				68.9	3.0
-----	--	--	--	------	-----

T.P.	7.00	978.32	0.54	971.32	
------	------	--------	------	--------	--

4				69.9	8.4
---	--	--	--	------	-----

+10				70.0	8.2
-----	--	--	--	------	-----

+50				70.7	7.6
-----	--	--	--	------	-----

3p k₁ P.P. S.W. Cor Cleveland.

$$\begin{array}{r} 6.9 \\ F2.3 \\ \hline 17.6 \end{array}$$

$$\begin{array}{r} 7.3 \\ F2.7 \\ \hline 18.4 \end{array}$$

$$\begin{array}{r} 7.0 \\ F2.2 \\ \hline 17.6 \end{array}$$

$$\begin{array}{r} 9.4 \\ F4.6 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 7.6 \\ F4.8 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 9.7 \\ F5.3 \\ \hline 23.6 \end{array}$$

$$\begin{array}{r} 9.3 \\ F5.4 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 6.5 \\ F3.5 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 10.4 \\ F2.0 \\ \hline 17.0 \end{array}$$

$$\begin{array}{r} 9.6 \\ DC0.2 \\ \hline 40.4 \end{array}$$

$$\begin{array}{r} 8.6 \\ DC1.0 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 7.2 \\ F2.6 \\ \hline 18.2 \end{array}$$

$$\begin{array}{r} 8.3 \\ F3.7 \\ \hline 20.4 \end{array}$$

$$\begin{array}{r} 3.8 \\ C0.9 \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} 7.0 \\ F2.2 \\ \hline 17.4 \end{array}$$

$$\begin{array}{r} 8.9 \\ F4.1 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} 8.7 \\ F4.3 \\ \hline 21.6 \end{array}$$

$$\begin{array}{r} 7.6 \\ F3.7 \\ \hline 20.4 \end{array}$$

$$\begin{array}{r} 3.0 \\ C0.0 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 2.5 \\ C5.9 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 2.4 \\ C5.9 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 4.1 \\ C3.5 \\ \hline 30 \end{array}$$

Sta	+	+	-	Elev.	
				978.35	
4+82				71.2	7.1
5+25				71.9	6.4
+50				72.3	6.0
6				73.0	5.3
+50				73.7	4.6
+70				74.0	4.3
7				74.4	3.9
+50				75.1	3.2
8				75.8	2.5
+50				76.5	1.8
T.P.	11.62	98 6.47 ⁵	3.47	974.85	
9				77.2	9.3
+50				77.9	8.6

$$\begin{array}{r} 7.6 \\ DC 1.0 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 6.2 \\ CO 1.2 \\ \hline 23.4 \end{array}$$

$$\begin{array}{r} 5.5 \\ CO 1.5 \\ \hline 24.0 \end{array}$$

$$\begin{array}{r} 4.9 \\ CO 1.4 \\ \hline 23.8 \end{array}$$

$$\begin{array}{r} 4.8 \\ DC 1.0 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 4.7 \\ DC 1.1 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 4.3 \\ DC 1.1 \\ \hline 22.2 \end{array}$$

$$\begin{array}{r} 2.3 \\ CO 1.9 \\ \hline 24.8 \end{array}$$

$$\begin{array}{r} 4.0 \\ DC 2.3 \\ \hline 20.0 \end{array}$$

$$\begin{array}{r} 3.2 \\ DC 0.1 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 9.7 \\ DC 1.1 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 5.7 \\ CO 1.9 \\ \hline 28.8 \end{array}$$

$$\begin{array}{r} 4.7 \\ CO 2.4 \\ \hline 27.8 \end{array}$$

$$\begin{array}{r} 5.8 \\ CO 1.6 \\ \hline 24.2 \end{array}$$

$$\begin{array}{r} 7.4 \\ DC 0.1 \\ \hline 20.2 \end{array}$$

$$\begin{array}{r} 6.8 \\ DC 0.0 \\ \hline 23.0 \end{array}$$

$$\begin{array}{r} 8.2 \\ F 3.4 \\ \hline 19.8 \end{array}$$

$$\begin{array}{r} 8.3 \\ F 4.0 \\ \hline 21.0 \end{array}$$

$$\begin{array}{r} 7.7 \\ F 3.8 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 4.3 \\ DC 0.4 \\ \hline 20.8 \end{array}$$

$$\begin{array}{r} 4.7 \\ F 2.2 \\ \hline 17.4 \end{array}$$

$$\begin{array}{r} 3.9 \\ F 2.1 \\ \hline 17.2 \end{array}$$

$$\begin{array}{r} 8.6 \\ CO 1.7 \\ \hline 24.4 \end{array}$$

$$\begin{array}{r} 6.1 \\ CO 2.5 \\ \hline 28.0 \end{array}$$

Sta.	+	Σ	-	Elev.	
		986.47 ⁵			
10+00				78.4	8.1
T.P.	7.23	991.90	1.80	984.67	
+41				78.5	13.4
+90				78.2	13.7
11+26				77.7	14.2
+50				77.3	14.6
T.P.	0.91	980.71	12.10	979.80	
+86		980.71 7.29		76.6	41
12+25				75.8	4.9
+50				75.3	5.4
+85				74.6	6.1
13				74.3	6.4
+15.83					
			7.79	972.92	(972.97)

$$\begin{array}{r} 2.4 \\ C 5.7 \\ \hline 34.4 \end{array}$$

$$\begin{array}{r} 3.8 \\ C 9.6 \\ \hline 42.2 \end{array}$$

$$\begin{array}{r} 0.8 \\ C 12.9 \\ \hline 48.8 \end{array}$$

$$\begin{array}{r} 8.5 \\ C 5.7 \\ \hline 34.4 \end{array}$$

$$\begin{array}{r} 6.8 \\ C 7.8 \\ \hline 38.6 \end{array}$$

$$\begin{array}{r} 4.4 \\ DC 12 \\ \hline 22.4 \end{array}$$

$$\begin{array}{r} 4.6 \\ C 0.3 \\ \hline 33.6 \end{array}$$

$$\begin{array}{r} 5.4 \\ DC 1.3 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 7.3 \\ DC 0.3 \\ \hline 30.6 \end{array}$$

$$\begin{array}{r} 3.2 \\ C 4.9 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 9.2 \\ C 4.2 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 14.1 \\ DC 1.1 \\ \hline 32.2 \end{array}$$

$$\begin{array}{r} 16.1 \\ F 1.9 \\ \hline 16.8 \end{array}$$

$$\begin{array}{r} 17.4 \\ F 2.8 \\ \hline 18.6 \end{array}$$

$$\begin{array}{r} 6.6 \\ F 2.5 \\ \hline 18 \end{array}$$

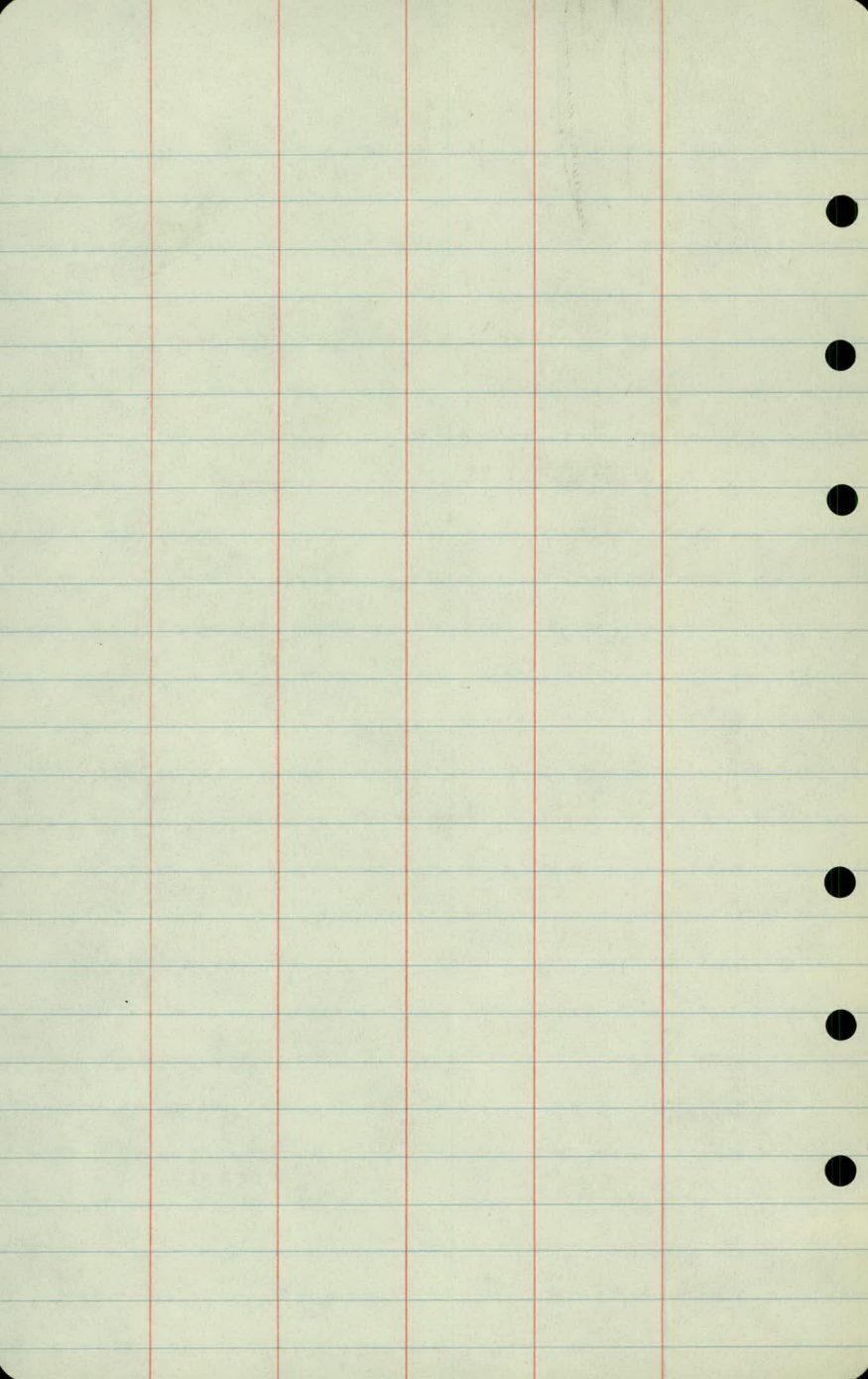
$$\begin{array}{r} 5.8 \\ DC 0.6 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} 4.3 \\ DC 0.6 \\ \hline 21.2 \end{array}$$

$$\begin{array}{r} 7.6 \\ DC 0.0 \\ \hline 20 \end{array}$$

$$\begin{array}{r} F 3.0 \\ \hline 60 \end{array}$$

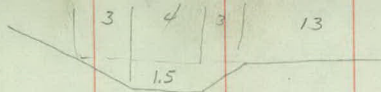
Spt 6 Birch 100' Rt 13+25



Eldridge Rd.

Slope Stakes
for Grade Change

B.M.	10.82	983.79		972.97	
13 + 15.83				72.4	11.4
13				72.9	10.9
+85				73.4	10.4
+50				74.5	9.3
12 125				75.3	8.5
11 + 86				76.6	7.2
+50				77.7	6.1
T.P.	13.30	99.3.21	3.88	979.91	
11 + 26		15.5		78.4	14.8
10 + 90				79.1	14.1
+41				79.4	13.8
10				79.1	14.1
+50				78.0	15.2
T.P.	+0.05	980.98	12.28	980.93	



Spike 6" Birch 100' Rt. 13+25

$$\begin{array}{r} 10.0 \\ C 1.4 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 11.7 \\ F 0.3 \\ \hline \end{array}$$

$$\begin{array}{r} 13.0 \\ F 1.6 \\ \hline 60 \end{array}$$

X

$$\begin{array}{r} 10.0 \\ C 0.4 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 10.4 \\ C 0.0 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 10.4 \\ F 0.0 \\ \hline \end{array}$$

$$\begin{array}{r} 10.4 \\ C 0.0 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 12.7 \\ F 2.3 \\ \hline 60 \end{array}$$

$$\begin{array}{r} 8.8 \\ C 0.5 \\ \hline 24 \end{array}$$

$$\begin{array}{r} 8.4 \\ C 0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 7.2 \\ C 0.1 \\ \hline 23 \end{array}$$

$$\begin{array}{r} 7.7 \\ C 0.8 \\ \hline 24.6 \end{array}$$

$$\begin{array}{r} 7.9 \\ C 0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 9.0 \\ D 1.0 \\ \hline 22.0 \end{array}$$

$$\begin{array}{r} 7.3 \\ D 1.4 \\ \hline 22.8 \end{array}$$

$$\begin{array}{r} 8.6 \\ F 1.4 \\ \hline \end{array}$$

$$\begin{array}{r} 9.9 \\ F 2.7 \\ \hline 18.4 \end{array}$$

$$\begin{array}{r} 11.6 \\ C 2.7 \\ \hline 38.4 \end{array}$$

$$\begin{array}{r} 7.1 \\ F 1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 9.3 \\ F 3.2 \\ \hline 19.4 \end{array}$$

$$\begin{array}{r} 9.5 \\ C 5.3 \\ \hline 33.6 \end{array}$$

$$\begin{array}{r} 15.2 \\ F 0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 18.0 \\ F 3.2 \\ \hline 18.4 \end{array}$$

$$\begin{array}{r} 2.0 \\ C 12.1 \\ \hline 47.2 \end{array}$$

$$\begin{array}{r} 11.2 \\ C 2.9 \\ \hline \end{array}$$

$$\begin{array}{r} 15.3 \\ D 0.3 \\ \hline 20.6 \end{array}$$

$$\begin{array}{r} 5.1 \\ C 8.7 \\ \hline 40.4 \end{array}$$

$$\begin{array}{r} 7.7 \\ C 6.1 \\ \hline \end{array}$$

$$\begin{array}{r} 10.5 \\ C 3.3 \\ \hline 29.6 \end{array}$$

$$\begin{array}{r} 9.8 \\ C 5.1 \\ \hline 39.2 \end{array}$$

$$\begin{array}{r} 10.3 \\ C 3.8 \\ \hline \end{array}$$

$$\begin{array}{r} 9.9 \\ C 4.2 \\ \hline 30 \end{array}$$

$$\begin{array}{r} 12.4 \\ C 2.8 \\ \hline 28.6 \end{array}$$

$$\begin{array}{r} 13.2 \\ C 2.0 \\ \hline \end{array}$$

$$\begin{array}{r} 12.8 \\ C 2.4 \\ \hline 27.8 \end{array}$$

^{1.0}
980.98

9

76.7

4.3

150

75.7

5.3

8

74.9

6.1

+50

74.4

6.6

7

74.0

7.0

+70

73.7

7.3

+50

73.5

7.5

B.M.

14.00

966.98

6

73.0

+50

72.3

~~111~~

5 +25

71.9

4 + 82

71.2

$\frac{4.2}{C0.1}$	$\frac{4.0}{C0.3}$	$\frac{3.1}{C1.2}$
23.2		25.4

$\frac{5.7}{DC1.1}$	$\frac{6.4}{F1.1}$	$\frac{6.7}{DC0.1}$
22.2		20.2

$\frac{6.7}{DC0.9}$	$\frac{7.1}{F1.0}$	$\frac{7.4}{DC0.2}$
21.8		20.4

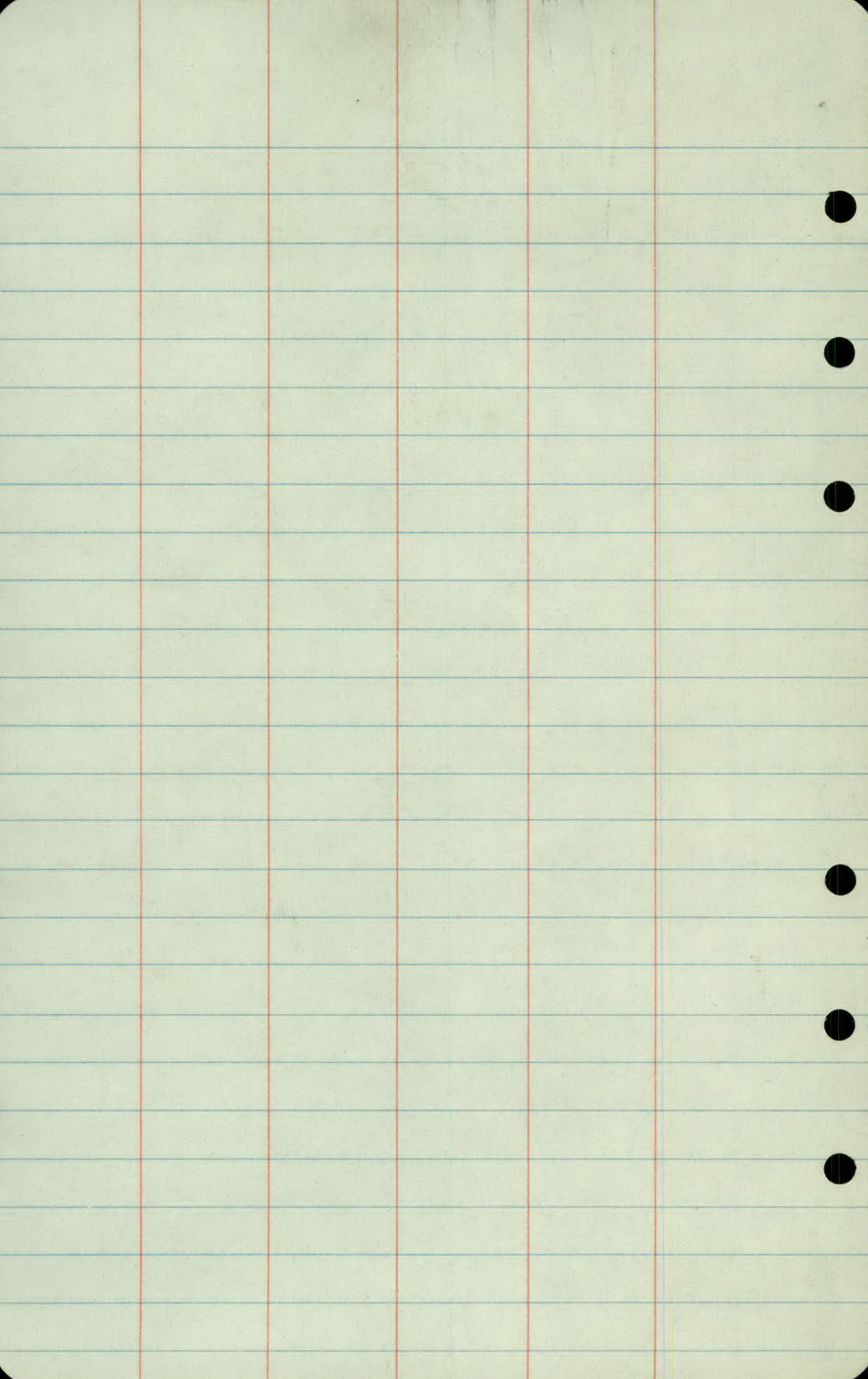
$\frac{4.9}{C1.7}$	$\frac{5.8}{C0.8}$	$\frac{7.0}{DC1.1}$
26.4		22.2

$\frac{7.0}{C0.0}$	$\frac{9.0}{F2.0}$	$\frac{10.3}{F3.3}$
23.0		19.6

$\frac{7.8}{DC1.0}$	$\frac{9.8}{F2.5}$	$\frac{10.8}{F3.5}$
22.0		20.0

$\frac{9.7}{F2.2}$	$\frac{10.7}{F3.2}$
	19.4

Spike P.P S.W. Cor. Edridge Rd - Cleveland



Feldri 991

Graden

6-25-51

HAW
HM
MB
LC

Sta	+	π	-	Elev	P.G.R
BM	645	962.88		956.43	
3+50				54.6	

4				54.9	
---	--	--	--	------	--

+50				55.4	
-----	--	--	--	------	--

5				56.1	
---	--	--	--	------	--

+50				56.9	
-----	--	--	--	------	--

				57.1	
6				57.8	

+50				58.0	
-----	--	--	--	------	--

7				60.0	
---	--	--	--	------	--

G. Rod

● 549

8.0

● 55.2

76

5

● 55.7

71

56.4

64

57.2

56

● 58.1

47

● 59.2

3.6

● 60.5

23

$$\begin{array}{r}
 15 \\
 11.5 \\
 \hline
 19 \quad 215 \\
 19 \\
 \hline
 209
 \end{array}$$

$$\begin{array}{r}
 18.5 \\
 14 \\
 \hline
 7 \\
 72 \\
 8 \\
 \hline
 159
 \end{array}$$

1206 04

Profile Levels

Eldridge Ave

Hamlin to Fernwood

Red.
6-22-51

R.C.

6-20-51

HAW

LC

MB

AM

drawn up.

Sta	+	π	-	Elev
B.M	12.84	963.39		950.55
B.M	5.83	962.26	6.96	956.43
0+00	R	Hamlin Ave		56.8.

+33				55.8
-----	--	--	--	------

+65				54.5
-----	--	--	--	------

1				53.5
---	--	--	--	------

+50				53.1
-----	--	--	--	------

2				53.1
---	--	--	--	------

+50				53.1
-----	--	--	--	------

3				52.8
---	--	--	--	------

Lt

L

Pt

U.S.G.S 911 251' W x 285 S of Hamlin & B"
 Spk 17 Ave Lt Pole SW Cor Hamlin & Eldridge

^{57.1}
 52
 60

5.5

^{56.1}
 62
 50

56.7

56.2

55.8

55.3

56
7041
30

65

45
3070
60

56.5

56.1

53.1

53.4

58
6042
30

78

72
3089
60

56.2

55.3

51.4

51.4

61
6070
30

88

109
30109
60

56.0

54.7

51.1

50.8

63
6076
30

92

112
30115
60

54.3

53.9

52.2

52.1

80
6084
30

92

101
30102
60

53.7

52.7

53.5

53.6

86
6096
30

92

88
3087
60

50.9

51.4

53.2

52.7

114
60107
30

95

91
3096
60

Sta	+	Δ	-	Elev
-----	---	----------	---	------

962.22

+50

52.9

4

53.3

+50

54.8

5

56.8

+50

58.0

6

58.8

+50

59.5

T.P

3.57

963.41

2.42

959.84

7

59.7

Lt

Z

Rt

50.8

51.4

51.1

50.6

115

109

94

112

117

60

30

30

60

50.5

50.5

50.8

50.5

118

118

90

115

118

60

30

30

60

54.2

55.7

54.8

54.7

54.3

81

66

75

76

80

60

30

30

60

55.7

56.9

56.5

56.8

66

54

55

58

55

60

30

30

60

56.6

57.1

55.8

54.5

57

52

43

65

78

60

30

30

60

57.6

58.7

57.4

55.1

47

36

35

49

72

60

30

30

60

57.9

58.9

59.7

58.1

44

34

28

26

42

60

30

30

60

59.9

59.6

59.4

59.4

35

38

37

40

40

60

30

30

60

Sta + Δ - Elev

9634'

7+24

Conc Walk Rt

+50

59.7

8

59.3

+11

Conc Walk Rt

+50

58.7

9

57.5

+50

56.3

10

55.4

Lt

L

Pt

59.6
Grat Ho Lt
31.8

59.33
408
30

59.5 59.5
39 39 37
40 30

59.5 Elev
Orlat Ho
39 59.5
40

58.4 58.8
5.2 46 41
41 30

59.3 59.5 Elev at Ho
41 39
30 40

59.25
416
30

59.2 60.8
42 26 47
60 30

58.6 58.8
48 46
30 40

58.8 58.8
46 46 5.9
60 30

55.4 52.8
8.0 106
30 40

57.7 57.7
5.7 5.7 71
60 30

53.3 52.1
101 11.3
30 60

Grat Ho 57.1 56.1
63 73 80
60 30

54.1 52.5
93 10.9
30 40

Sta + π - Elev
963.41

10+50 54.3

11 53.1

+50 52.5

12 52.3

+50 51.8

13 51.5

+18 Δ FernWood 51.8

+50 51.9

14

L1

L2

R1

54.8

55.0

53.0

50.1

86

84

91

104

13.3

60

30

30

60

51.9

52.1

51.4

50.3

115

113

103

120

131

60

30

30

60

50.0

50.3

50.4

50.2

134

131

109

130

13.2

60

30

30

60

50.4

51.0

51.7

50.7

130

124

111

11.7

127

60

30

30

60

50.1

49.9

50.9

49.9

13.3

135

116

125

135

60

30

30

60

51.7

51.3

50.7

50.5

11.7

121

119

127

129

60

30

30

60

52.0

51.2

114

116

122

60

11.5

Sta

+

π

-

Elev

963.41

14

51.6

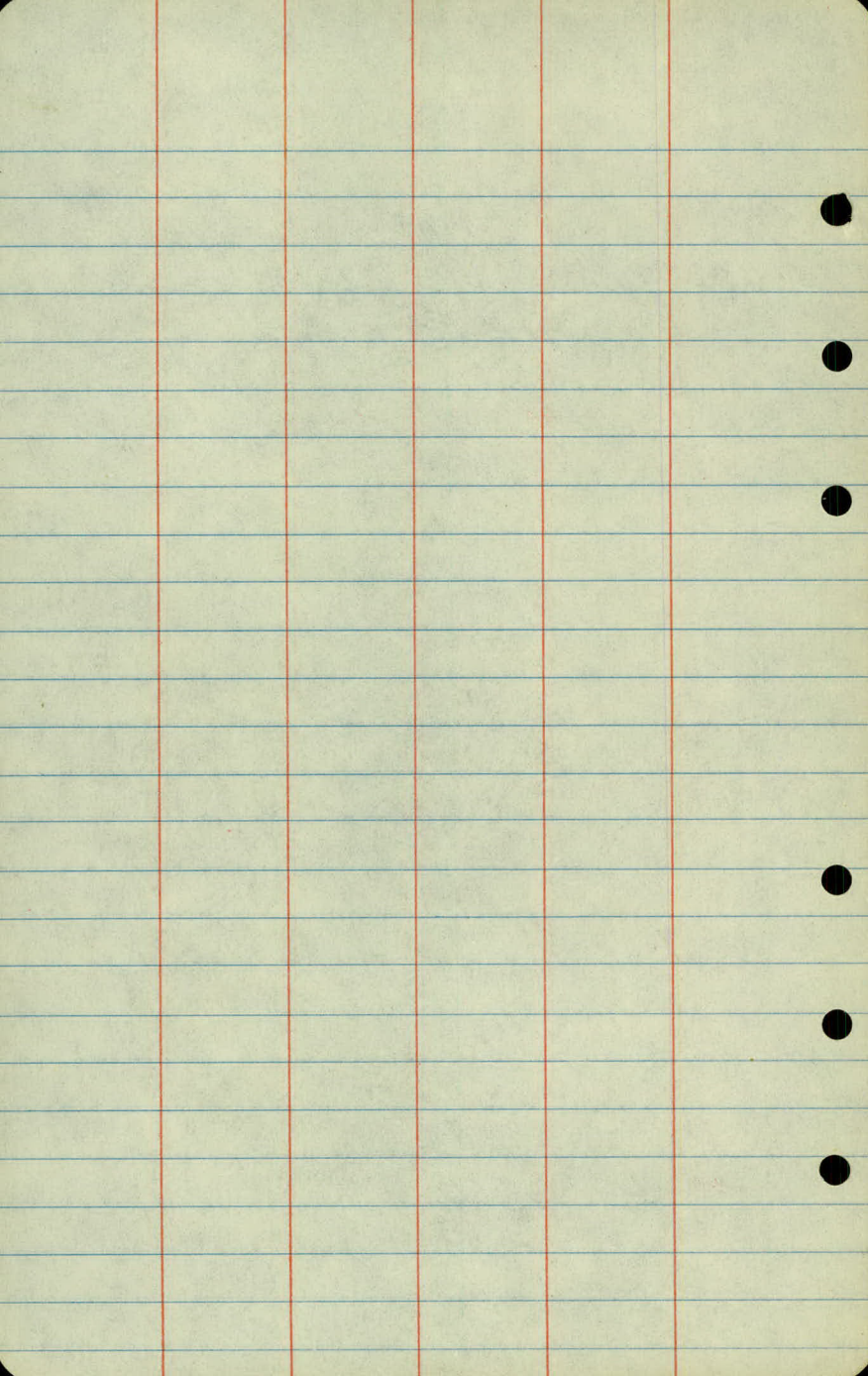
B.M

8.93 954.48

2

11.8

S.W. Cor. Bott. Stop Hs. #1215 N.E. Cor
Eldridge & Fernwood



Check Profiles

Eldridge Ave
(As Graded)

10-18-51

ITAW

L.C.

M.B.

Rec'd. 10-19-51

Sta	+	X	-	Elev
B.M	6.07	962.50		956.43

0+00	±	Ham/iny	56.9
------	---	---------	------

+33			55.9
-----	--	--	------

+65			55.6
-----	--	--	------

1			55.0
---	--	--	------

+50			54.4
-----	--	--	------

2			54.4
---	--	--	------

+50			54.2
-----	--	--	------

3			54.1
---	--	--	------

~~2~~

SpK in P.P. 3. W Co ✓ Hamline Y5/dr. 8/2

5.6

6.6

6.9

7.5

8.1

8.1

8.3

8.4

Sta t π - π

962.50

3 + 50

54.3

↓

54.6

+ 50

55.1

5

55.9

+ 50

56.4

6

56.9

+ 50

57.1

7

57.3

8

82

79

74

66

61

56

54

52

Sta + Δ - Elev

962.50

7+50

57.4

8

57.3

7+50

56.8

9

56.2

7+50

55.5

10

54.6

7+50

53.7

11

52.9

±

5.1

5.2

5.7

6.3

7.0

7.9

8.8

9.6

Sta + Δ - Elev

962.50

11450

52.5

12

52.3

750

51.9

785

51.5

13

51.6

~~2~~

10.0

10.2 ✓

10.6

11.0

10.9

