

Dr 11 - Bk 34

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

COUNTY RD. C2

From Forest Lake Cut-off To New Brighton Rd.

Road Acc't. No. R-42

Date Filed 7-2-37

File

1
Levels

Co Rd C²⁴
at STA # 8 to 1350' East

7-6-43

HAW

AM

L.B.

Sta	+	Δ	-	Elev
B M	1.94	952.85		950.91
0+00		West End	24" ^{43.42} X 59" Conc.	

+59		East End	11" ^{42.45} X 4"	
-----	--	----------	---------------------------	--

+61				39.3
-----	--	--	--	------

1+00				40.5
------	--	--	--	------

+50				39.3
-----	--	--	--	------

2				38.9
---	--	--	--	------

+50				38.1
-----	--	--	--	------

3				37.5
---	--	--	--	------

T.P.	5.42	944.66	13.61	939.24
------	------	--------	-------	--------

+34		Δ pt		37.3
-----	--	-------------	--	------

+58		No End	24" X 48" ^{36.98}	
		3+50 C ^u X Drain		

+68		Shl Co Rd C ^u		40.7
-----	--	--------------------------	--	------

+98				40.6
-----	--	--	--	------

2
Ditch

Top Drill hole 0400 STH 8 + C²

Inv 9.43

10.40

13.6

124

Low spot

14.4

38.5

136

140

148

15.4

7.4

Inv

7.68

40

4.1

Sta	+	π	-	Elev
		44466		
4+06		So End	24" X 48' Conc	36.68
+50				36.6
5				36.4
+50				36.6
6				36.5
+50				36.6
7				36.6
+50				36.2
+64		West End Side Drain	18" X 20' CM	36.21
			(Poor Cond.)	
+84		East	" "	35.66
9				36.0
+50				35.9

3
Z
50 Ditch

In
7.98

8.1

8.3

8.1

8.2

8.1

8.1

8.5

In

8.45

In

9.00

8.7

8.8

Sta + π + Elev
94466

9+00 35.6

+50 35.6

+56 5.1 $\Delta p t$ 35.6

+58 50 End 18' 46' Conc 35.58

10 +64 50 Spl. Co Rd 6.2 38.3

+98 No Spl. Co Rd 6.2 38.1

10x04 35.7

+08 $\Delta p t$ 35.1
T.P 6.35 94372 7.29 93737

+50 35.0

+64 $\Delta p t$ 34.9

11 34.5

+36 $\Delta p t$ 34.0

4
S.Ditch

9.1

9.1

9.1

9.08

6.4

6.6

9.00

9.6

8.7

8.8

9.2

9.7

Sta	+	λ	-	Elev
-----	---	-----------	---	------

943.72

11+50				34.0
-------	--	--	--	------

12				32.8
----	--	--	--	------

+21				32.4
-----	--	--	--	------

+50				31.8
-----	--	--	--	------

13				31.4
----	--	--	--	------

+50				29.9
-----	--	--	--	------

B.M			5.27	938.45
-----	--	--	------	--------

5
£
Ditch No East

9.7

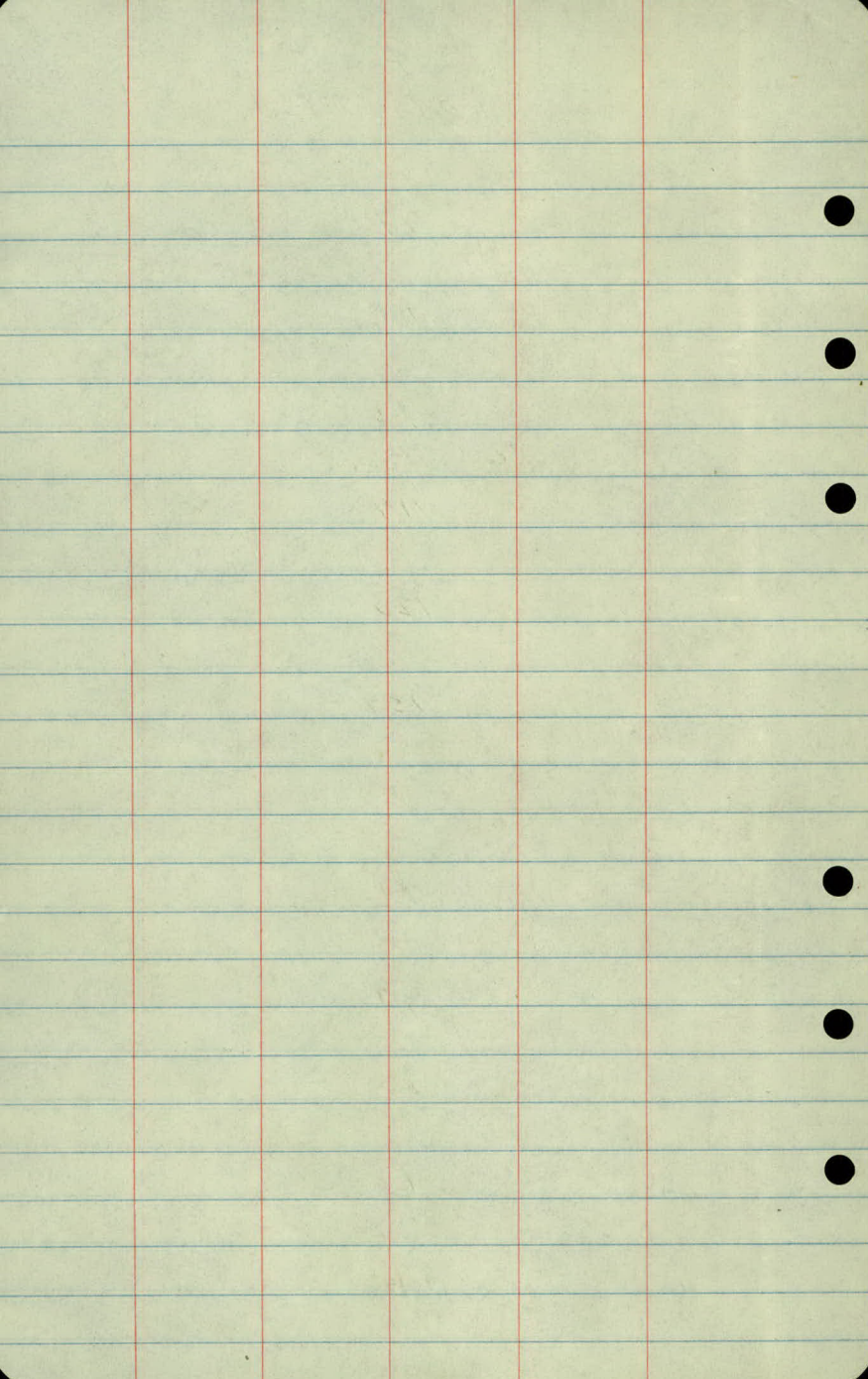
10.9

11.3

11.9

12.3

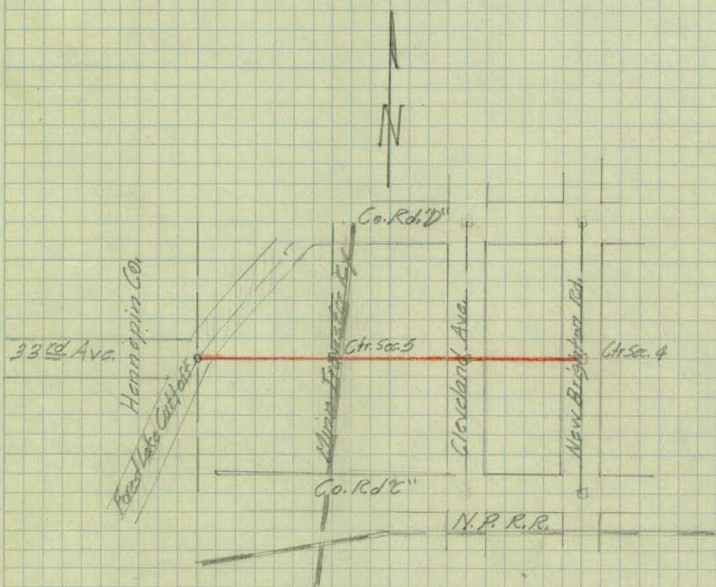
13.8



PLAN SURVEY

Co. Rd "C" 2"
from

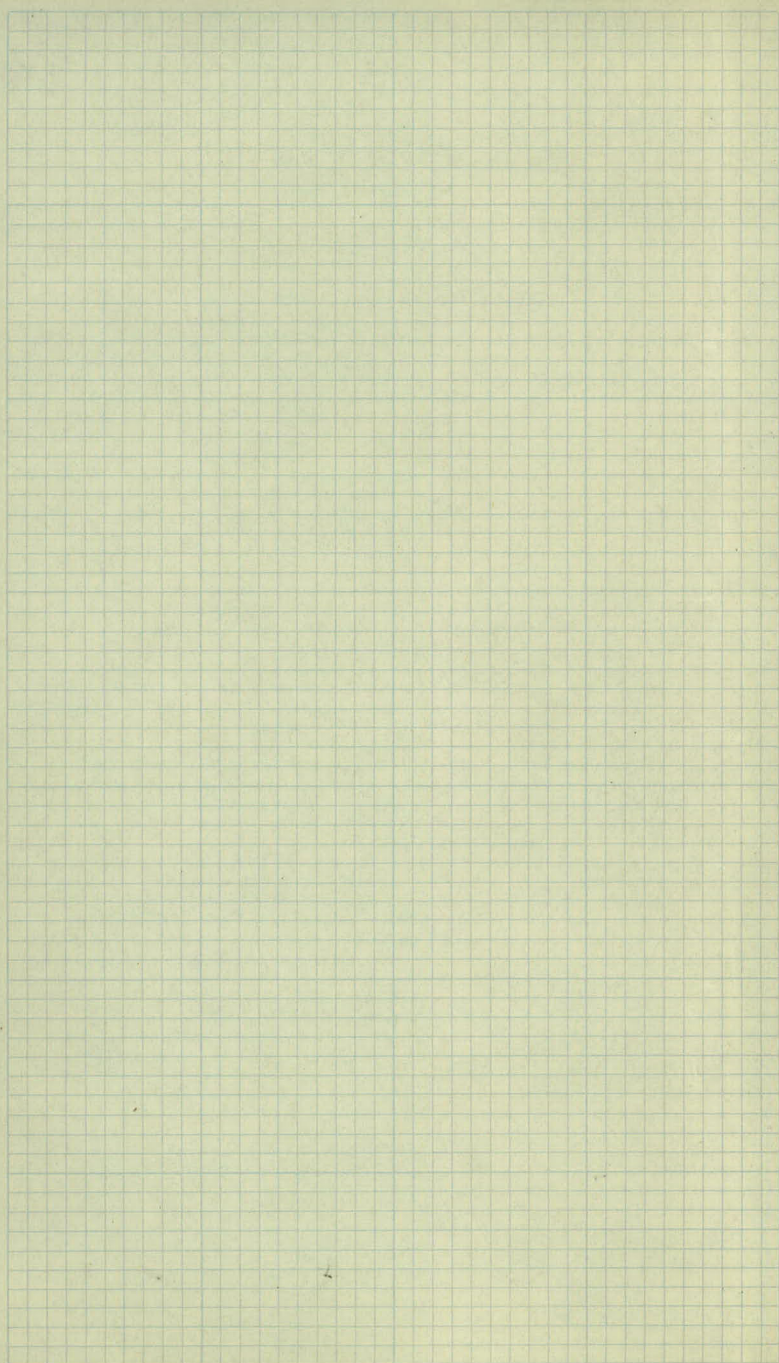
Forest Lake Cut-off to Cleveland Ave.



INDEX

- Align. - R1-3
- Topog. - 4-16
- Levels. - 17-18
- X Sections - 19-39

Minute Index.



Alignment

Sta	Point	ΔL	ΔR
-----	-------	------------	------------

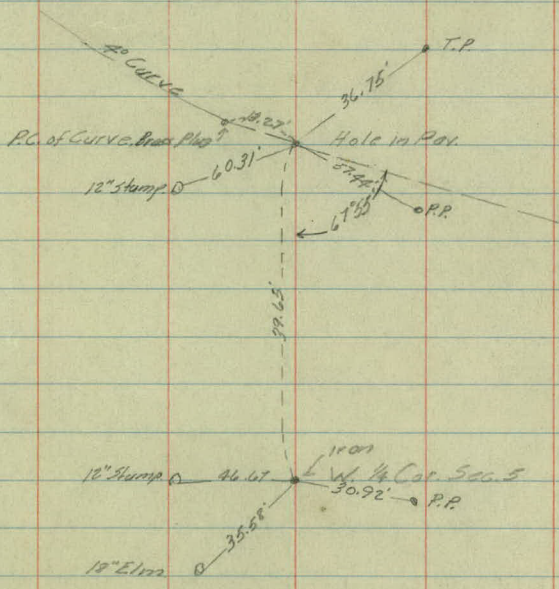
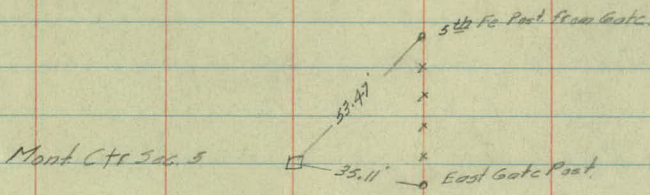
26+05.93	P.I.		
----------	------	--	--

		0°05'	
--	--	-------	--

0+00	= E Forest Lake Cutt Off		
------	--------------------------	--	--

12/27/97
 K.A.
 L.G.
 M.H.G.
 L.L.

2



Sta	Point	Δ Lt	Δ Rt
-----	-------	-------------	-------------

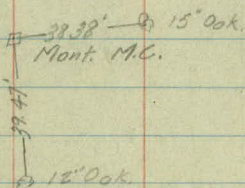
78+54.65	= E New Brighton Rd.		
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60+49.55	P.O.T.		
----------	--------	--	--

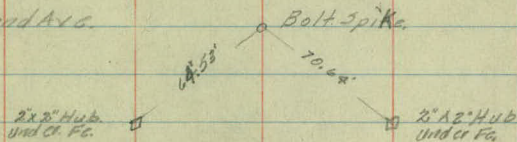
52+48.90		0°44'	
----------	--	-------	--

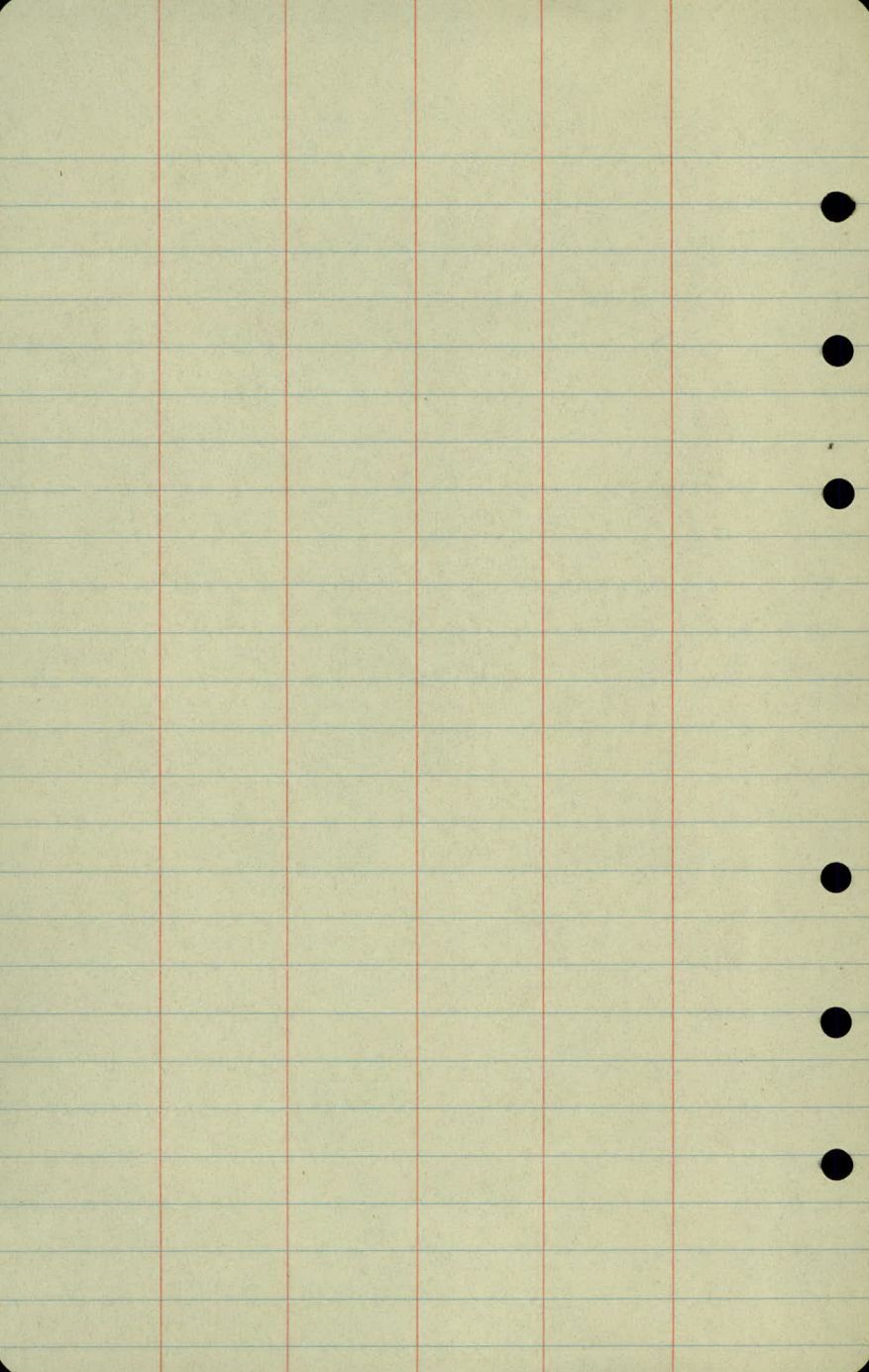
3
12/28/37

□ Mont. Ctr Sec. 4



= R. Cleveland Ave.





Topography

5

4

3

2

1

0/00

-1

12/28/37
K.P.
L.C.
M.J.G.
L.L.

Cult



+50 Trail Ditch 100

+45 Ditch 100

Cult

+50 End Low Tree 40

Trees 41



+30 T.P. 23'

Ridge Low Collars 40

+05 End of Core Cult 59'

Core

-28 End 18' C.M. 24'
-15' X 24' C.M.
-51 End 18' C.M. 15'

+44 End Core Cult 37'
+48 P.P. 30'

Black Top

12

11

10

9

8

7

6

Trail 34'

Trail 34'

Trail 31'

End Ditch 2'

Cult.

Cult.

Cult.

Cult.

+57-36" Stump 10'
+45 Trail X 8

Ditch 00

+35 Ditch 3'

Ditch 25'

Ditch 90'

19

18

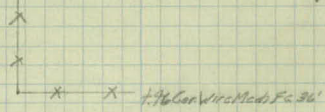
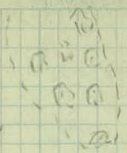
17

16

15

14

13



+30 Reg Woods 60'

+96 Con Wire Mesh Fa 36'

Trail 5' Cult.

Trail 4' Cult.

Trail 5'

Trail 5'

Trail 16' Cult.

Trail 31'

Trail 33'

26

25

24

23

22

21

20

+65 Beg Brush 5' Mt. Rt

+06' Fc. 21'

+006' Triple Oak, 15' x x x x

Fc. 21'

+95 2 1/4' Gato.

Cult.

Trail 3'

Trail 4'

Trail 5'

Cult.

Fc. 35'

+60 End Woods 90'

Trail 10'

Trail 8'

+37 High Voltage Line on 14" Poles X 5 ft.

+20 Tel. Line X 5 ft.

33 +07 High Voltage Line on Towers X 5 ft.

+82 R.R. Tel. Line X 5 ft.

+43.24 R.R. Tracks X 5 ft.

32

31

30

29

28

27

+57 Cfr. "H" Poles 15'

+36 T.P. 77'

+23 Cfr. of Tower 86'

+97 T.P. 53'

+97 Fe Cor. 2'

+77 19'

Minor Trans. Fe. Ry.

+94 Fe Lk. from R.

+70 End Brush on R.

+85 Cor. Wire Mesh Fe. 35'

+0089 Brush on R.

Cult.

Fe 35'

+0089 Brush on R.

Cult.

Brush 5'

Brush 5' Fe 35'

40

39

38

37

36

35

34

10

Fe. 00

00

Fe. 1'

1'

Fe 2'

2'

Fe. 2'

Cult

Cult

Cult

Cult

47

46

45

44

43

42

153 Fc. Cor.

Fc. 2'

Fc. 2'

Cult.

Wooded

134 Fc. Cor. & Beg Woods

Cult.

Cult.

00

00

54

53

52

51

50

49

48

Meadow

Fc 33'

Fc 33'

+82 Fc. Cor 33'

+59 Edge Black Top.

Cleveland Ave.
Black Top.

+39 Edge Bl. Top.

+17 Fc. Cor.

Cult.

Fc. 1'

Cult.

Fc. 1'

Fc. 1'

+95-16" Stump 14'
+90-18" Stump 29'

+85 End Woods

Cult.

Fc 2'

61

60

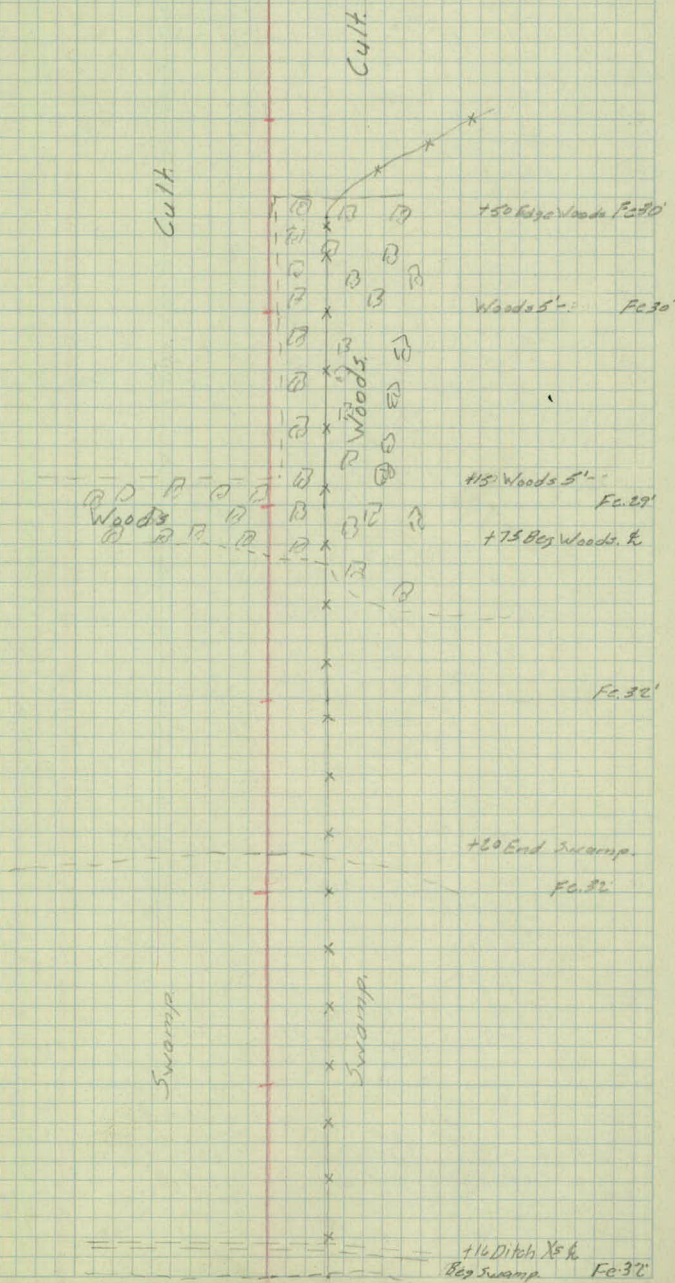
59

58

57

56

55



68

67

66

65

64

63

62

69400 = End Swamp

14

+21 Bag Fe 91'

Swamp

Swamp

+30 Trees 50-80'

Bag Swamp

+80 Trees 00

+65 Trees 00

+85 Fe 50'

+25 Fe 00

Cult.

Cult.

75

74

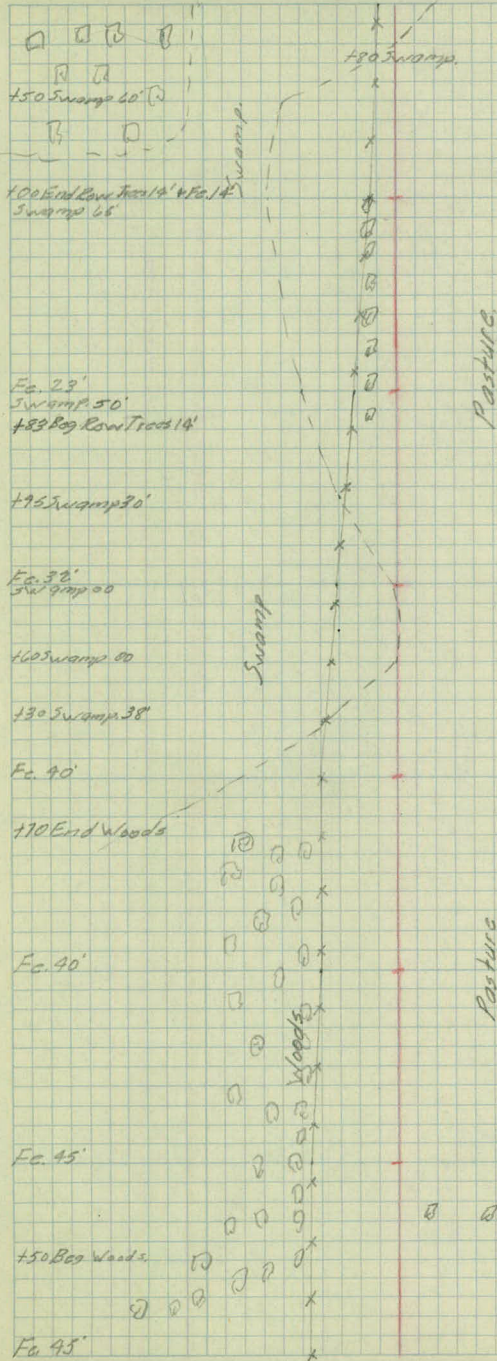
73

72

71

70

69

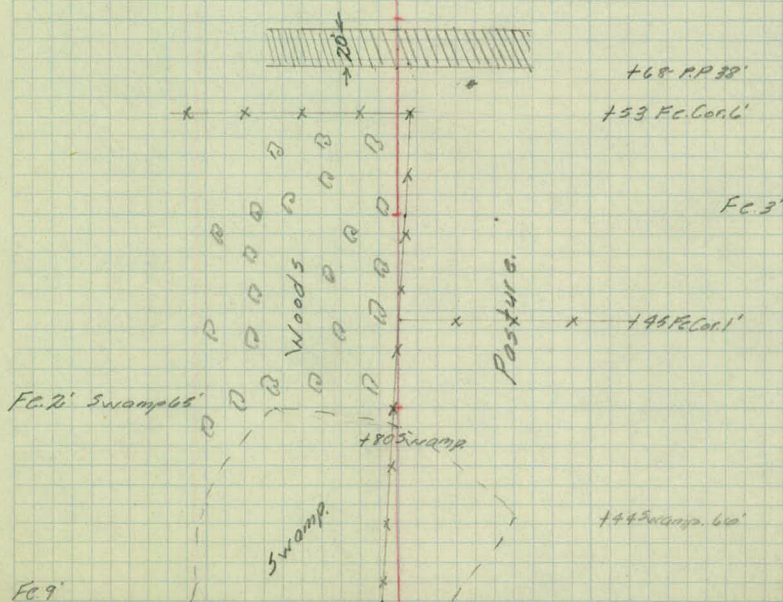


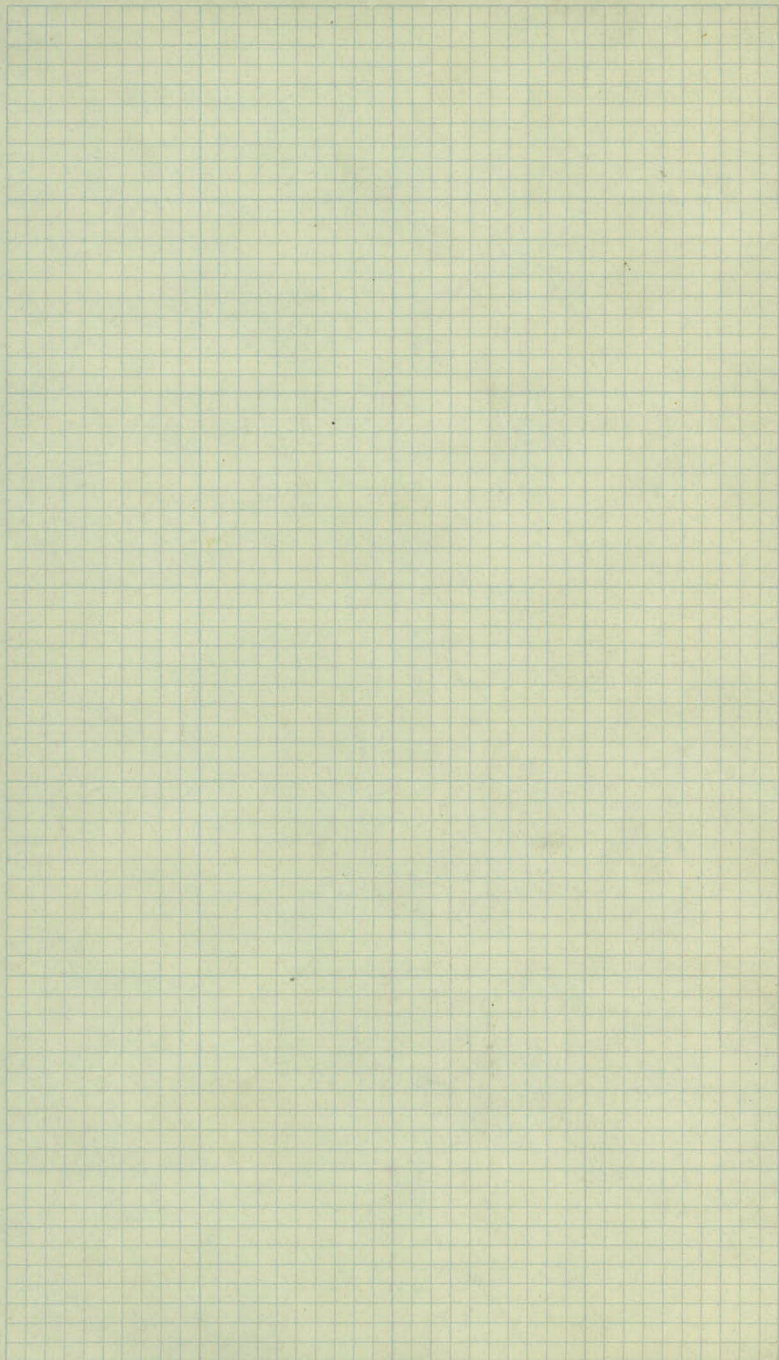
+84.65° to Pavement

78

77

76





Bench Levels

Sta	+	X	-	Elev.
B.M.	0.43	951.24		950.91
I.P.	4.70	948.98	7.06	944.28
I.P.	6.36	946.77	10.57	938.41
I.P.	7.56	952.22	2.11	994.66
B.M.	5.50	950.37	7.35	944.87
I.P.	0.37	938.11	12.63	937.74
I.P.	0.47	926.85	11.73	926.38
B.M.	8.72	923.02	12.55	914.20
I.P.	2.52	914.16	11.38	911.64
B.M.	6.81	920.33	0.64	913.52
I.P.	0.52	907.52	18.22	907.00
B.M.	4.74	907.52	4.74	902.78
I.P.	2.23	912.04	4.71	902.81
I.P.	13.72	925.08	0.68	911.36
B.M.	2.33	925.08	2.33	922.75
I.P.	1.63	913.32	13.27	911.69
I.P.	9.23	910.29	12.26	901.06
B.M.	12.67	922.95	0.01	910.23
I.P.	5.71	927.65	1.01	921.94
B.M.	5.44	932.16	0.93	926.72
I.P.	4.32	932.02	4.96	927.80
I.P.	4.02	925.69	7.33	924.69
I.P.	5.67	929.33	5.03	923.66
B.M.			3.62	925.71

Hole in Pine at 20

Top Corner Base Cor. E. Post Rt.

Spike in East H. Pole. 75' Lt 33+37

Spike in 15" Oak Co. Rt. sta 44+50

Top Bolt Spike Cleveland & "C"

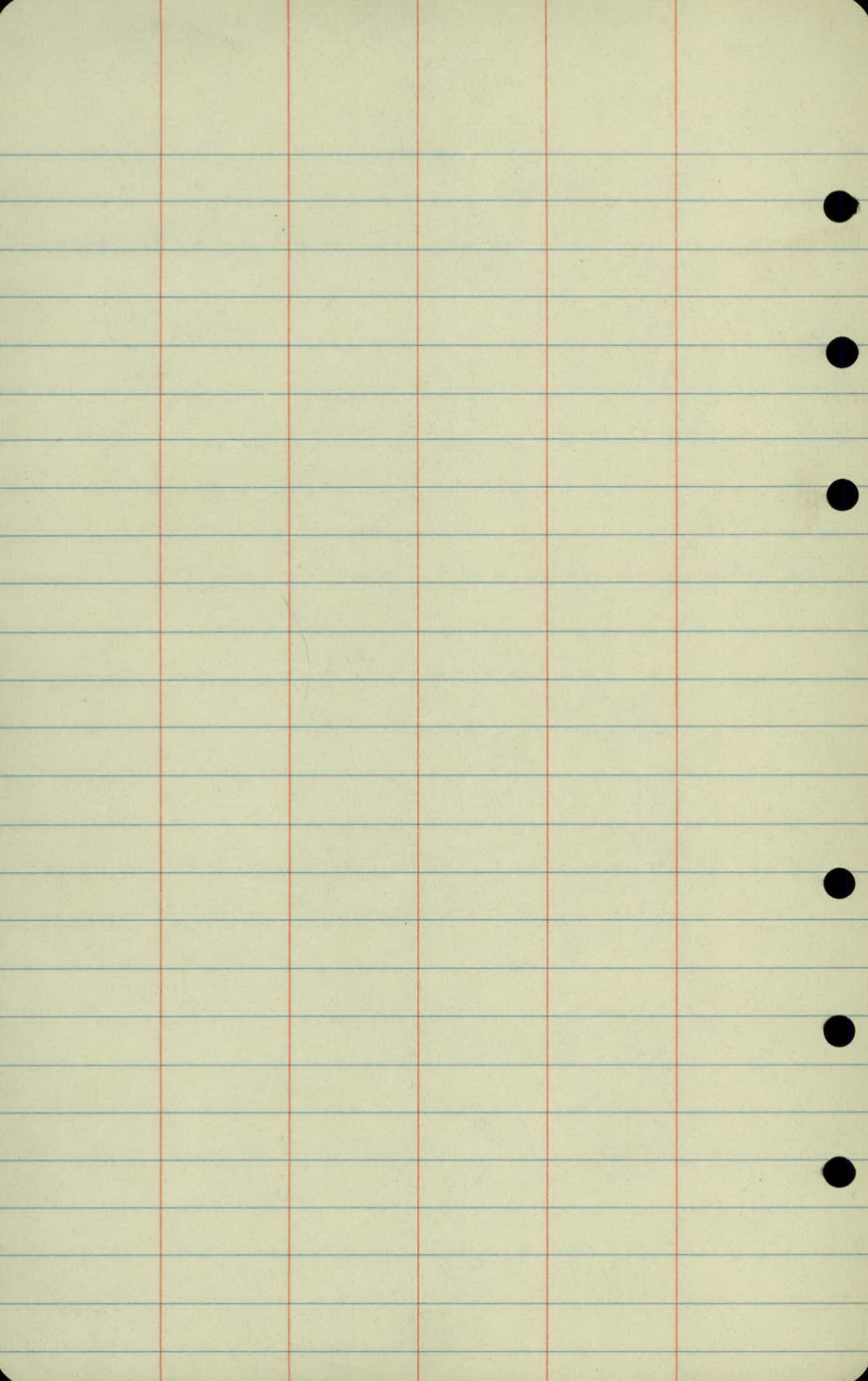
Top M.C. Mont.

Spike in 6" Poplar 55' Lt sta 69+55

Top Mont "C" & New Brighton Rd.

Top Mont. New Brighton Rd. So. of "C"

These levels run back ward from Co. Rd "C" & New Brighton Rd.



2/5/39

39

K. R.

L. B. H.

L. C.

M. J. G.

Rt.

Lt.

4

$\frac{133}{50}$

$\frac{411}{50}$

$\frac{110}{50}$

Top Mont New Brighton Rd & Co. Rd "C" 2"

Sta.

+

X

-

Elev.

CV

Center line Levels.

1/24/28

Sta.	+	π	-	Elev.
B.M.	0.43	951.34		950.91
0+00			0.4	50.9
+11.5			0.4	50.9
+19			1.1	50.2
+27			4.1	47.2
+40			4.7	46.6
+70			5.5	45.8
1+00			6.7	44.6
+50			7.9	43.4
2			9.5	41.8
+50			12.4	38.9
3			13.4	37.9

Sta	+	π	-	Elev.
3+50	951.34 [✓]	37.0	14.3	37.0
4		37.1	13.2	38.1
T.P.	11.18	950.45 [✓]	12.07	939.27 [✓]
+50			10.9	39.6
+80			7.6	42.9
5			5.9	44.6
+35			5.3	45.2
+70			4.9	45.6
6			4.9	45.6
+35			7.6	42.9
+80			12.3	38.2
7			13.2	37.3

Sta. + $\checkmark$ - Elev.

950.45

7+50

13.2

37.3

8

13.5

37.0

+50

14.0

36.5

9

13.5

37.0

+50

14.0

36.5

T.P.

3.91

942.77

11.59

938.86

10

4.8

38.0

+45

1.8

41.0

+70

1.1

41.7

11

3.6

39.2

+35

7.1

35.7

+75

8.1

34.7

Sta. + π - Elev.

942.77

12 9.5 33.3

+30 10.3 32.5

+75 5.6 37.2

13 1.9 40.9

T.P. 8.73 950.78 0.77 942.05

+30 7.8 43.0

+60 7.8 43.0

14 7.4 43.4

+50 8.2 42.6

15 9.2 41.6

+50 9.0 41.8

16 6.8 44.0

Sta.	+	+ 950.78	-	Elev.
16+40			3.0	47.8.
+60			3.5	47.3.
17			6.6	44.2.
+50			8.0	42.8.
18			7.6	43.2.
+50			9.7	41.1.
19			10.0	40.8.
+50			7.9	42.9.
B.M.	4.65	✓ 949.58	5.85	✓ 944.93
20			5.5	44.1.
+50			6.3	43.3.
21			5.8	43.8.

Sta.	+	Σ	-	Elev.
21+40		949.58	5.7	43.9.
+80			3.3	46.3.
22			2.8	46.8.
+38			2.9	46.7.
+67			2.9	46.7.
23			5.2	44.4.
+34			6.7	42.9.
+67			6.6	43.0.
24			7.8	41.8.
+50			10.2	39.4.
25			10.8	38.8.

Sta.	+	✓ K	-	Elev.
25+35		949.58	10.4	39.2.
+70			11.6	38.0.
26			12.4	37.2.
T.P.	4.90	✓ 941.54	12.94	✓ 936.64
+50			7.8	33.7.
27			9.4	32.1.
+50			10.8	30.7.
28			10.9	30.6.
+50			12.2	29.3.
29			12.8	28.7.
T.P.	0.58	✓ 930.47	11.65	✓ 929.89
+50			3.4	27.1.
30			4.7	25.8.
+50			7.0	23.5.
31			9.6	20.9.
T.P.	4.78	✓ 924.40	10.85	✓ 919.62
B.M.	7.61	✓ 921.91	10.10	✓ 914.30

Sta.	+	+	+	Elev.
	921.91	921.91		
32			3.8	18.1.
+10			4.6	17.3.
+14			7.5	14.4.
+17			7.5	14.4.
+22			3.9	18.0.
+29			3.6	18.3.
+40			2.7	19.2.
Top Tie			2.25	19.66.
Top Rail			1.80	20.11.
+53			2.6	19.3.
+60			5.8	16.1.
33			7.9	14.0.
+80			8.4	13.5.

Sta.	+	π	-	Elev.
		✓ 921.91		
34			7.6	14.3.
+50			6.3	15.6.
35			5.2	16.7.
+50			3.1	18.8.
36			0.6	21.3.
T.P.	2.01	✓ 923.77	0.15	✓ 921.76
+50			2.9	20.9.
37			5.8	18.0.
+50			9.9	13.9.
T.P.	0.62	✓ 911.33	13.06	✓ 910.71
38			1.8	09.5.
+50			3.4	07.9.
39			4.6	06.7.
+50			5.2	06.1.
40			5.3	06.0.
+50			5.0	06.3.
41			3.9	07.4.
+50			2.9	08.4.
42			2.8	08.5.
T.P.	6.85	✓ 916.43	1.75	✓ 909.58
+50			8.2	08.2.
43			7.5	08.9.
+50			6.3	10.1.

Sta.	+	π	-	Elev.
44		916.43 ✓	4.8	11.6 .
+50			3.4	13.0 .
T.P.	5.28	919.74 ✓	1.97	914.46 ✓
B.M.	6.22	919.74 ✓	6.22	913.52 ✓
45			6.8	12.9 .
+50			6.6	13.1 .
46			5.3	14.4 .
+50			2.8	16.9 .
47			2.0	17.7 .
+50			1.6	18.1 .
T.P.	1.66	921.01 ✓	0.39	919.35 ✓
48			4.2	16.8 .
+50			6.1	14.9 .
+80			9.7	11.3 .
49			12.5	08.5 .
T.P.	0.44	910.15 ✓	11.30	909.71 ✓
+50			5.2	05.0 .
50			7.3	02.9 .
+50			8.8	01.4 .
51			9.7	900.5 .
+50			10.4	899.8 .
52			10.6	899.6 .
+27			10.0	900.2 .
+32			8.4	01.8 .
+48.7			7.1	03.1 .

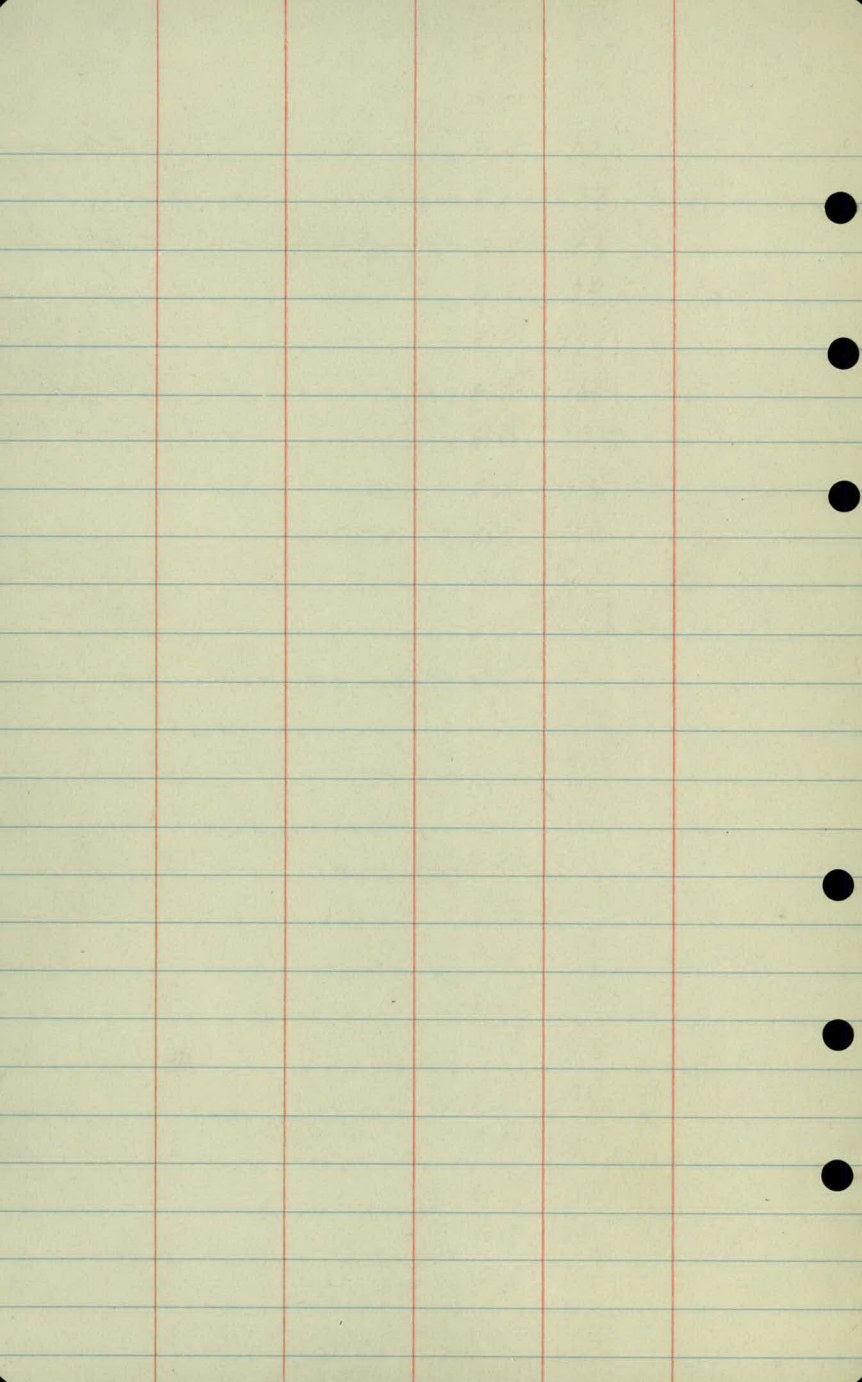
Sta.	+	π	-	Elev.
		910.15		
B.M.	2.28	905.06	7.37	902.78
52+64			2.7	02.4.
+70			5.1	900.0.
53			5.5	899.6.
54			5.5	99.6.
55			6.5	98.6.
+11			6.4	98.7.
+14			7.7	97.4.
+18			7.6	97.5.
+20			6.8	98.3.
+50			7.6	97.5.
56			8.1	97.0.
T.P.	10.65	908.89	6.87	898.24
+50			11.8	897.1.
57			10.9	98.0.
+50			9.2	99.7.
58			6.5	902.4.
+28			3.8	05.1.
+49			1.4	07.5.
+74			0.5	08.4.
T.P.	13.38	921.57	0.75	908.14
+80			9.5	12.0.
59			8.5	13.0.
+50			4.0	17.5.

Sta.	+	Σ	-	Elev.
		921.52		
T.P.	5.27	926.19	0.60	920.92
60			4.4	21.8.
B.M.	3.44	926.19	3.44	922.75
+50			3.9	22.3.
61			5.5	20.7.
+50			9.4	16.8.
62			12.3	13.9.
+50			12.3	13.9.
T.P.	0.47	913.53	13.13	913.06
63			1.6	11.9.
+22			2.0	11.5.
+28			4.0	09.5.
+50			6.9	06.6.
64			10.3	03.2.
65			12.5	01.0.
66			12.9	00.6.
T.P.	7.42	909.28	11.67	901.86
67			8.4	00.9.
68			8.1	01.2.
69			6.3	03.0.
+50			2.5	06.8.
T.P.	13.01	921.04	1.25	908.03
B.M.	10.76	921.04	10.76	910.28
+78			10.8	10.2.
+90			6.5	14.5.

Sta	+	π	-	Elev.
70		921.04	6.2	14.8
+21			3.4	17.6
+50			1.5	19.5
71			3.5	17.5
+50			7.3	13.7
72			9.3	11.7
+50			10.5	10.5
73			10.0	11.0
+50			7.8	13.2
74			5.3	15.7
T.P.	4.55	921.37	4.22	916.82
+35			5.7	15.7
75			7.7	13.7
+45			8.7	12.7
+65			10.6	10.8
76			12.5	08.9
+35			13.1	08.3
+78			11.6	09.8
77			9.3	12.1
+35			4.8	16.6
+58			4.0	17.4
78			2.2	19.2
T.P.	10.65	930.90	1.14	920.25

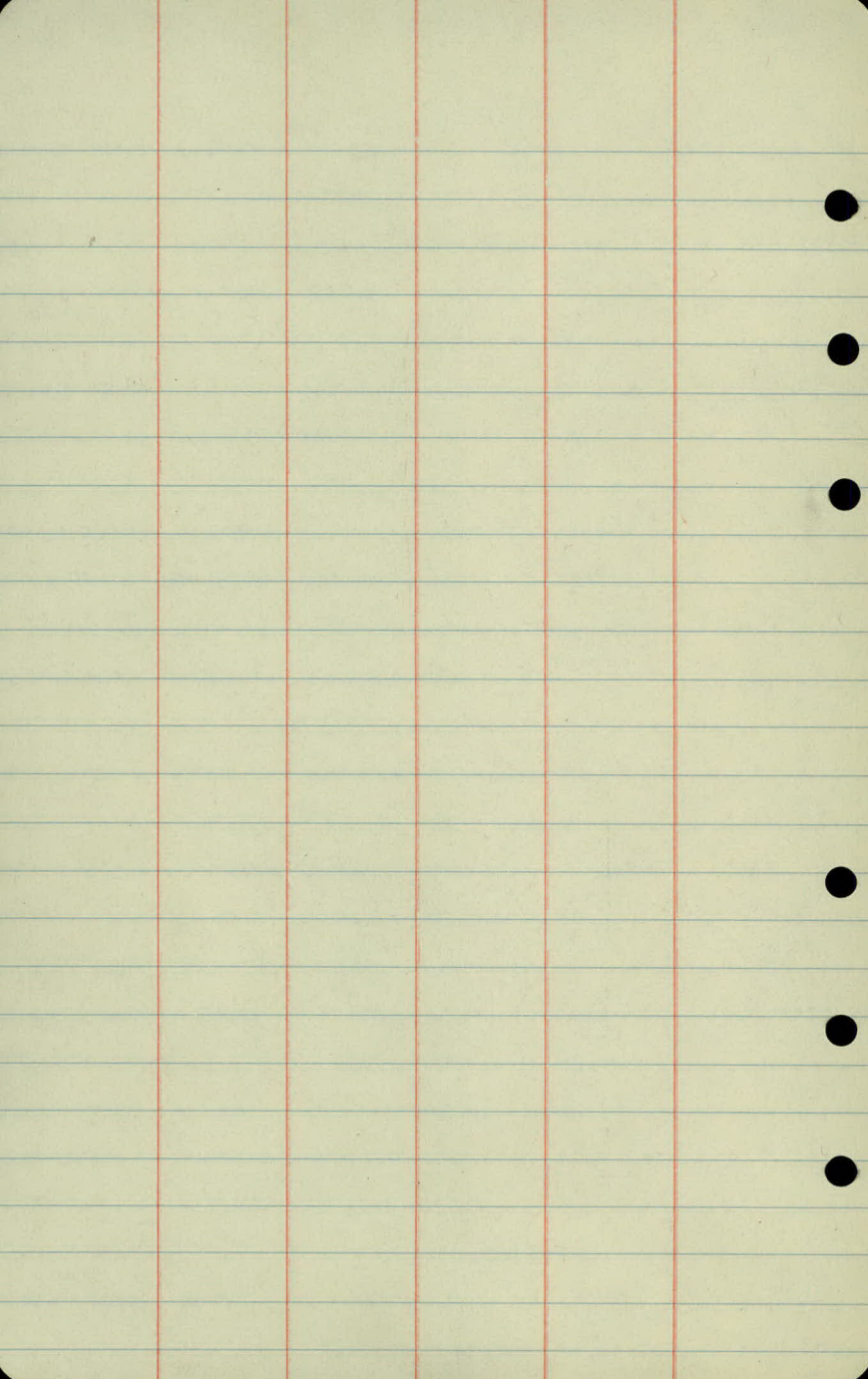
Sta.	+	π	-	Elev.
		930.90		
78+50			9.5	21.4.
+57			10.5	20.4.
+62			9.7	21.2.
+70			4.5	26.4.
+85			4.3	26.6.
B.M.			4.18	926.72

Note: See Bench levels for description of benches.



Clearance of overhead wires
above present ground line
on proposed C^Y road and at
the following locations

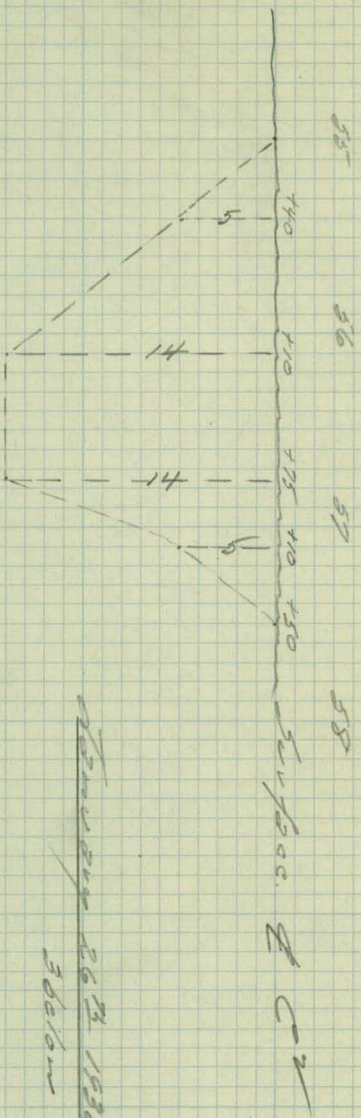
<u>Sta.</u>	<u>Description</u>	<u>Clearance</u>
32+70	Telegraph-3wires	18.4'
33+10	High Voltage-4"	39'
33+24	Telephone-4wires	23'
33+40	High Voltage 5"	35'
34+10	" " 5"	43'



Townsend 26th 1938
36 below.



No post here, $\frac{3}{8}$ " rod pushed thru soft clay to shore depths where firmer material was encountered soundings to 30' each side of it would be substantially the same.



These tests were made by pushing down a $\frac{3}{8}$ " rod to the depths as shown where a firmer material was encountered. The above depths represent probably 3 to 5' of foot with balance not soft clay, sandlings 30' each side of Φ would be substantially the same.

X Sections C²

Sta.	+	π	-	Elev.
B.M.	0.43	751.39		750.96
0+00				
+11.5				751.3
+19				50.2
+27				47.2
+40				46.6
+70				45.8
1				44.6
+50				43.4
2				41.8
+50				38.9
3				37.9

Lt.

K

Rt.

Hale in Pave sta 0100

$$\begin{array}{r} \text{Pav.} \\ 033 \\ \hline 35 \end{array} \quad \begin{array}{r} 00 \\ 50 \end{array}$$

$$\begin{array}{r} \text{Pav.} \\ 009 \\ \hline 1 \end{array}$$

$$\begin{array}{r} \text{Pav.} \\ 11 \\ \hline 215 \end{array} \quad \begin{array}{r} 11 \\ 17 \end{array} \quad \begin{array}{r} 34 \\ 17 \end{array} \quad \begin{array}{r} 40 \\ 50 \end{array} \quad \checkmark$$

$$\begin{array}{r} \text{Pav.} \\ 126 \\ \hline 33 \end{array} \quad \begin{array}{r} 11 \\ 12 \end{array} \quad \begin{array}{r} 41 \\ 33 \end{array} \quad \begin{array}{r} 49 \\ 33 \end{array}$$

$$\begin{array}{r} 13 \\ 42 \end{array} \quad \begin{array}{r} 35 \\ 29 \end{array} \quad \begin{array}{r} 47 \\ 33 \end{array} \quad \begin{array}{r} 53 \\ 33 \end{array}$$

$$\begin{array}{r} 49 \\ 33 \end{array} \quad \begin{array}{r} 55 \\ 33 \end{array} \quad \begin{array}{r} 57 \\ 33 \end{array}$$

$$\begin{array}{r} 57 \\ 33 \end{array} \quad \begin{array}{r} 56 \\ 16 \end{array} \quad \begin{array}{r} 67 \\ 22 \end{array} \quad \begin{array}{r} 57 \\ 22 \end{array} \quad \begin{array}{r} 56 \\ 33 \end{array}$$

$$\begin{array}{r} 81 \\ 33 \end{array} \quad \begin{array}{r} 85 \\ 27 \end{array} \quad \begin{array}{r} 79 \\ 16 \end{array} \quad \begin{array}{r} 68 \\ 16 \end{array} \quad \begin{array}{r} 67 \\ 33 \end{array}$$

$$\begin{array}{r} 101 \\ 33 \end{array} \quad \begin{array}{r} 85 \\ 33 \end{array} \quad \begin{array}{r} 82 \\ 33 \end{array}$$

$$\begin{array}{r} 126 \\ 33 \end{array} \quad \begin{array}{r} 124 \\ 14 \end{array} \quad \begin{array}{r} 120 \\ 14 \end{array} \quad \begin{array}{r} 107 \\ 33 \end{array}$$

$$\begin{array}{r} 139 \\ 33 \end{array} \quad \begin{array}{r} 134 \\ 33 \end{array} \quad \begin{array}{r} 129 \\ 33 \end{array}$$

Sta	+	Σ	-	Elcv
		751.87 34		
3	+50			37.0.
4				38.1.
T.P.	11.18	950.45 ✓	12.07 ✓	939.27 ✓
	+50			39.6.
	+80			42.9.
5				44.6.
	+85			45.2.
	+70			45.6.
6				45.6.
	+35			42.9.
	+80			38.2.
7				37.3.

Lt.

E.

Rt.

$$\frac{141}{33}$$

$$\frac{143}{4}$$

$$\frac{148}{4}$$

$$\frac{141}{6}$$

$$\frac{142}{33}$$

$$\frac{129}{33}$$

$$\frac{132}{33}$$

$$\frac{136}{33}$$

$$\frac{93}{33}$$

$$\frac{99}{12}$$

$$\frac{109}{33}$$

$$\frac{113}{33}$$

$$\frac{75}{33}$$

$$\frac{68}{6}$$

$$\frac{76}{33}$$

$$\frac{84}{33}$$

$$\frac{55}{33}$$

$$\frac{55}{7}$$

$$\frac{59}{33}$$

$$\frac{69}{33}$$

$$\frac{57}{33}$$

$$\frac{50}{11}$$

$$\frac{53}{33}$$

$$\frac{58}{23}$$

$$\frac{61}{33}$$

$$\frac{48}{33}$$

$$\frac{47}{11}$$

$$\frac{49}{33}$$

$$\frac{55}{18}$$

$$\frac{69}{33}$$

$$\frac{41}{33}$$

$$\frac{40}{14}$$

$$\frac{49}{33}$$

$$\frac{60}{17}$$

$$\frac{78}{33}$$

$$\frac{42}{33}$$

$$\frac{48}{18}$$

$$\frac{76}{33}$$

$$\frac{100}{25}$$

$$\frac{106}{33}$$

$$\frac{89}{33}$$

$$\frac{92}{21}$$

$$\frac{123}{33}$$

$$\frac{123}{30}$$

$$\frac{139}{33.0}$$

$$\frac{104}{33}$$

$$\frac{108}{25}$$

$$\frac{130}{13}$$

$$\frac{132}{33}$$

$$\frac{131}{12}$$

$$\frac{145}{15}$$

$$\frac{145}{31}$$

$$\frac{120}{37}$$

Sta	+	A	-	Elev
		950.45		
7	+50			37.3
8				37.0
	+50			36.5
9				37.0
	+50			36.5
I.P.	3.21	94277 ✓	11.59	92836 ✓
10				38.0
	+45			41.0
	+75			41.7
11				39.2
	+35			35.7
	+75			34.7

14

4

26

$$\frac{117}{33} \quad \frac{117}{21} \quad \frac{125}{13} \quad \frac{128}{2} \quad \frac{132}{3} \quad \frac{135}{5} \quad \frac{117}{6} \quad \frac{119}{33}$$

$$\frac{113}{33} \quad \frac{108}{20} \quad \frac{119}{2} \quad \frac{185}{2} \quad \frac{186}{2} \quad \frac{129}{2} \quad \frac{131}{25} \quad \frac{126}{33}$$

$$\frac{119}{33} \quad \frac{111}{23} \quad \frac{121}{16} \quad \frac{131}{3} \quad \frac{140}{1} \quad \frac{140}{2} \quad \frac{133}{2} \quad \frac{138}{33}$$

$$\frac{131}{33} \quad \frac{128}{25} \quad \frac{138}{15} \quad \frac{138}{4} \quad \frac{142}{2} \quad \frac{135}{13} \quad \frac{139}{13} \quad \frac{142}{33}$$

$$\frac{143}{33} \quad \frac{147}{15} \quad \frac{140}{2} \quad \frac{141}{11} \quad \frac{141}{33}$$

$$\frac{35}{33} \quad \frac{50}{26} \quad \frac{53}{16} \quad \frac{98}{33} \quad \frac{51}{33}$$

$$\frac{25}{33} \quad \frac{26}{28} \quad \frac{18}{2} \quad \frac{22}{33}$$

$$\frac{43}{33} \quad \frac{28}{22} \quad \frac{11}{2} \quad \frac{09}{33}$$

$$\frac{56}{33} \quad \frac{46}{24} \quad \frac{36}{2} \quad \frac{40}{33}$$

$$\frac{65}{33} \quad \frac{59}{24} \quad \frac{71}{2} \quad \frac{81}{21} \quad \frac{93}{33}$$

$$\frac{59}{33} \quad \frac{60}{23} \quad \frac{81}{2} \quad \frac{101}{19} \quad \frac{108}{33}$$

Sta	+	π	-	Elev
		942.77		
12				33.3
	+30			32.5
	+75			37.2
13				40.9
T.R	8.73	950.78 ✓	0.72	942.05 ✓
	+30			43.0
	+60			43.0
14				43.4
	+50			42.6
15				41.6
	+50			41.8
16				44.0

Lt

L

Rt

$$\frac{67}{33} \quad \frac{66}{30} \quad \frac{81}{13} \quad \frac{95}{10} \quad \frac{106}{10} \quad \frac{111}{33}$$

$$\frac{76}{33} \quad \frac{77}{28} \quad \frac{85}{20} \quad \frac{90}{15} \quad \frac{103}{16} \quad \frac{111}{16} \quad \frac{110}{33}$$

$$\frac{53}{33} \quad \frac{54}{28} \quad \frac{56}{19} \quad \frac{60}{19} \quad \frac{70}{33}$$

$$\frac{26}{35} \quad \frac{27}{29} \quad \frac{19}{12} \quad \frac{18}{10} \quad \frac{22}{10} \quad \frac{41}{33}$$

$$\frac{78}{33} \quad \frac{69}{14} \quad \frac{78}{18} \quad \frac{90}{18} \quad \frac{106}{33}$$

$$\frac{73}{33} \quad \frac{69}{19} \quad \frac{78}{33} \quad \frac{88}{33}$$

$$\frac{92}{33} \quad \frac{88}{25} \quad \frac{79}{13} \quad \frac{72}{13} \quad \frac{69}{20} \quad \frac{71}{33}$$

$$\frac{102}{33} \quad \frac{96}{23} \quad \frac{82}{33} \quad \frac{85}{33}$$

$$\frac{81}{33} \quad \frac{90}{21} \quad \frac{90}{12} \quad \frac{92}{22} \quad \frac{97}{22} \quad \frac{102}{33}$$

$$\frac{84}{33} \quad \frac{83}{15} \quad \frac{90}{24} \quad \frac{103}{24} \quad \frac{107}{33}$$

$$\frac{75}{33} \quad \frac{70}{11} \quad \frac{68}{5} \quad \frac{57}{5} \quad \frac{47}{33}$$

Sta	+	π	—	Elev.
		950.78		
16	+40			47.8
	+60			47.3
17				44.2
	+50			42.8
18				43.2
	+50			41.1
19				40.8
	+50			42.9
B.M.	4.65	949.58 ✓	5.85	944.93 ✓ 994.87
20				44.1
	+50			43.3
21				43.8

Lt.

K.

Rt.

$$\frac{66}{33} \quad \frac{50}{19} \quad \frac{41}{8} \quad \frac{30}{8} \quad \frac{17}{19} \quad \frac{18}{33}$$

$$\frac{67}{33} \quad \frac{48}{21} \quad \frac{43}{8} \quad \frac{35}{8} \quad \frac{30}{4} \quad \frac{21}{22} \quad \frac{22}{33}$$

$$\frac{80}{33} \quad \frac{69}{29} \quad \frac{67}{11} \quad \frac{66}{12} \quad \frac{64}{12} \quad \frac{56}{33}$$

$$\frac{66}{33} \quad \frac{69}{77} \quad \frac{80}{8} \quad \frac{80}{8} \quad \frac{84}{33}$$

$$\frac{45}{33} \quad \frac{50}{21} \quad \frac{66}{9} \quad \frac{76}{6} \quad \frac{83}{6} \quad \frac{91}{33}$$

$$\frac{69}{33} \quad \frac{75}{22} \quad \frac{90}{8} \quad \frac{97}{8} \quad \frac{91}{12} \quad \frac{89}{33}$$

$$\frac{103}{33} \quad \frac{99}{19} \quad \frac{100}{7} \quad \frac{90}{7} \quad \frac{76}{33}$$

$$\frac{102}{33} \quad \frac{85}{16} \quad \frac{79}{16} \quad \frac{61}{33}$$

$$\frac{67}{33} \quad \frac{61}{15} \quad \frac{60}{5} \quad \frac{55}{5} \quad \frac{41}{33}$$

$$\frac{67}{33} \quad \frac{63}{20} \quad \frac{66}{11} \quad \frac{63}{17} \quad \frac{53}{17} \quad \frac{37}{33}$$

$$\frac{53}{33} \quad \frac{54}{22} \quad \frac{57}{14} \quad \frac{58}{16} \quad \frac{50}{16} \quad \frac{23}{33}$$

Sta.	+	Δ	-	Elev.
		949.58		
21	+70			43.9
	+80			46.3
22				46.8
	+38			46.7
	+67			46.7
23				44.4
	+24			42.9
	+67			43.0
24				41.8
	+50			39.4
25				38.8

Lt.

¢

Rt

$$\frac{46}{33} \quad \frac{46}{24} \quad \frac{5.2}{15} \quad \frac{57}{33} \quad \frac{54}{33}$$

$$\frac{39}{33} \quad \frac{36}{31} \quad \frac{28}{17} \quad \frac{33}{33} \quad \frac{42}{24} \quad \frac{42}{33}$$

$$\frac{47}{33} \quad \frac{34}{19} \quad \frac{28}{6} \quad \frac{28}{6} \quad \frac{26}{33}$$

$$\frac{36}{33} \quad \frac{28}{14} \quad \frac{29}{33} \quad \frac{30}{33}$$

$$\frac{15}{33} \quad \frac{18}{12} \quad \frac{29}{33} \quad \frac{31}{33}$$

$$\frac{41}{33} \quad \frac{46}{12} \quad \frac{52}{5} \quad \frac{49}{5} \quad \frac{42}{33}$$

$$\frac{62}{33} \quad \frac{63}{19} \quad \frac{67}{33} \quad \frac{60}{33}$$

$$\frac{45}{33} \quad \frac{63}{8} \quad \frac{66}{8} \quad \frac{69}{33}$$

$$\frac{43}{33} \quad \frac{66}{18} \quad \frac{76}{8} \quad \frac{78}{33} \quad \frac{71}{33}$$

$$\frac{80}{33} \quad \frac{97}{17} \quad \frac{102}{13} \quad \frac{100}{13} \quad \frac{87}{33}$$

$$\frac{105}{33} \quad \frac{104}{10} \quad \frac{108}{6} \quad \frac{105}{6} \quad \frac{103}{33}$$

Sta	+	Σ	-	Elev.
		949.58		
25	+35			39.2
	+70			38.0
26				37.2
T.P.	4.90	941.54 ✓	12.94	936.64 ✓
	+50			33.7
27				32.1
	+50			30.7
28				30.6
	+50			29.3
29				28.7
T.P.	0.58	930.47 ✓	11.65	929.89 ✓
	+50			27.1

Lt.

C

Rt.

$$\frac{98}{33} \quad \frac{94}{11} \quad \frac{104}{33} \quad \frac{108}{33}$$

$$\frac{118}{33} \quad \frac{112}{11} \quad \frac{116}{33} \quad \frac{114}{33}$$

$$\frac{128}{33} \quad \frac{124}{33} \quad \frac{121}{14} \quad \frac{124}{33}$$

Top of Monument

$$\frac{75}{100} \quad \frac{76}{34} \quad \frac{78}{34} \quad \frac{87}{34}$$

$$\frac{93}{100} \quad \frac{91}{50} \quad \frac{97}{8} \quad \frac{89}{4} \quad \frac{94}{34} \quad \frac{96}{10} \quad \frac{105}{34}$$

$$\frac{94}{100} \quad \frac{96}{50} \quad \frac{101}{27} \quad \frac{108}{34} \quad \frac{115}{15} \quad \frac{120}{34}$$

$$\frac{107}{100} \quad \frac{106}{50} \quad \frac{109}{34} \quad \frac{118}{12} \quad \frac{128}{34}$$

$$\frac{120}{100} \quad \frac{115}{50} \quad \frac{120}{12} \quad \frac{122}{34} \quad \frac{130}{14} \quad \frac{136}{34}$$

$$\frac{120}{100} \quad \frac{125}{50} \quad \frac{128}{34} \quad \frac{133}{8} \quad \frac{141}{34}$$

$$\frac{21}{100} \quad \frac{29}{50} \quad \frac{34}{34} \quad \frac{47}{34}$$

Sta.	+	π	-	Elev.
30		930.47		25.8

+50				23.5
-----	--	--	--	------

31				20.9
----	--	--	--	------

T.P.	4.78	924.40	✓ 10.85	919.62 ✓
------	------	--------	---------	----------

B.M.	9.77	924.07	✓ 10.10	914.30 914.30
------	------	--------	---------	---

+50				18.9
-----	--	--	--	------

32				18.2
----	--	--	--	------

+16				14.8
-----	--	--	--	------

+23				18.0
-----	--	--	--	------

+90				19.6
-----	--	--	--	------

				920.03
--	--	--	--	--------

+51				19.6
-----	--	--	--	------

+65				15.4
-----	--	--	--	------

+75				15.0
-----	--	--	--	------

$$\begin{array}{r} \text{Lt.} \quad \quad \quad \text{Rt.} \\ \frac{3.6}{100} \quad \frac{4.6}{50} \quad \frac{5.7}{4} \quad \frac{4.7}{\cancel{4}} \quad \frac{6.1}{12} \quad \frac{6.3}{34} \end{array}$$

$$\frac{5.1}{100} \quad \frac{7.0}{50} \quad \frac{7.5}{3} \quad \frac{7.0}{\cancel{4}} \quad \frac{7.7}{6} \quad \frac{8.3}{13} \quad \frac{9.0}{34}$$

$$\frac{6.6}{100} \quad \frac{8.6}{50} \quad \frac{9.8}{3} \quad \frac{9.6}{\cancel{4}} \quad \frac{10.1}{6} \quad \frac{10.1}{15} \quad \frac{10.2}{34}$$

Spike in Tel. Pole 75' Lt. Sta. 33+37

$$\frac{4.7}{50} \quad \frac{4.9}{33} \quad \frac{5.2}{\cancel{33}} \quad \frac{1.3}{33}$$

$$\frac{5.8}{50} \quad \frac{6.1}{33} \quad \frac{5.9}{\cancel{33}} \quad \frac{5.7}{33}$$

$$\frac{10.1}{33} \quad \frac{9.8}{22} \quad \frac{9.3}{\cancel{12}} \quad \frac{8.2}{12} \quad \frac{5.7}{33}$$

$$\frac{10.0}{33} \quad \frac{9.5}{22} \quad \frac{6.1}{\cancel{33}} \quad \frac{5.0}{33}$$

$$\frac{6.3}{33} \quad \frac{4.8}{15} \quad \frac{4.5}{\cancel{33}} \quad \frac{4.4}{33}$$

~~44~~
Top Nail

$$\frac{4.7}{33} \quad \frac{4.5}{\cancel{7}} \quad \frac{4.6}{7} \quad \frac{7.6}{28} \quad \frac{7.8}{33}$$

$$\frac{5.0}{33} \quad \frac{8.4}{11} \quad \frac{8.6}{\cancel{19}} \quad \frac{8.3}{19} \quad \frac{8.5}{33}$$

$$\frac{8.4}{33} \quad \frac{9.2}{19} \quad \frac{9.1}{\cancel{14}} \quad \frac{8.9}{14} \quad \frac{9.0}{33}$$

Sta + π - Elev.

929.07

33

914.0

+50

13.6

34

14.3

+50

15.6

35

16.7

+50

18.8

36

21.4

+25

21.7

+50

21.1

37

18.0

+50

13.9

T.P.

0.45

913.98

10.54

913.53

Lt

E

Rt

$$\frac{59}{50} \quad \frac{43}{16} \quad \frac{41}{14} \quad \frac{47}{14} \quad \frac{51}{50}$$

$$\frac{55}{50} \quad \frac{57}{38} \quad \frac{58}{20} \quad \frac{59}{19} \quad \frac{64}{50}$$

$$\frac{67}{50} \quad \frac{71}{27} \quad \frac{72}{10} \quad \frac{72}{18} \quad \frac{76}{50}$$

$$\frac{77}{50} \quad \frac{80}{24} \quad \frac{78}{22} \quad \frac{81}{22} \quad \frac{86}{50}$$

$$\frac{77}{50} \quad \frac{81}{31} \quad \frac{78}{15} \quad \frac{79}{18} \quad \frac{82}{50}$$

$$\frac{77}{50} \quad \frac{77}{30} \quad \frac{76}{14} \quad \frac{77}{17} \quad \frac{83}{50}$$

$$\frac{65}{50} \quad \frac{67}{39} \quad \frac{65}{19} \quad \frac{65}{20} \quad \frac{73}{50}$$

$$\frac{52}{50} \quad \frac{55}{28} \quad \frac{57}{14} \quad \frac{55}{21} \quad \frac{65}{50}$$

$$\frac{49}{50} \quad \frac{51}{34} \quad \frac{51}{17} \quad \frac{54}{21} \quad \frac{68}{50}$$

$$\frac{49}{50} \quad \frac{51}{30} \quad \frac{51}{14} \quad \frac{57}{20} \quad \frac{66}{50}$$

$$\frac{45}{50} \quad \frac{47}{37} \quad \frac{47}{23} \quad \frac{47}{11} \quad \frac{53}{20} \quad \frac{68}{50}$$

Sta

+

 π

-

Elev

913.98

13 +50

910.2

44

11.6

+50

12.5

B.M.

9.85

923.82

0.45

912.53

913.52

45

13.0

+50

13.1

46

14.5

+50

16.8

47

17.7

+50

17.9

48

16.8

+50

14.9

T.P.

3.74

917.86

9.26

914.12

Lt

E

Rt

$$\frac{103}{33}$$

$$\frac{101}{19} \frac{96}{38} \frac{95}{38}$$

$$\frac{119}{35}$$

$$\frac{113}{22}$$

$$\frac{107}{16}$$

$$\frac{105}{3}$$

$$\frac{98}{3}$$

$$\frac{95}{33}$$

$$\frac{109}{33}$$

$$\frac{98}{4}$$

$$\frac{94}{4}$$

$$\frac{91}{33}$$

$$\frac{103}{33}$$

$$\frac{92}{6}$$

$$\frac{88}{5}$$

$$\frac{85}{4}$$

$$\frac{83}{4}$$

$$\frac{79}{33}$$

$$\frac{90}{33} \frac{81}{5} \frac{76}{4}$$

$$\frac{74}{5} \frac{74}{19} \frac{70}{19} \frac{74}{33}$$

L.O.

$$\frac{69}{38}$$

$$\frac{62}{16}$$

$$\frac{53}{19}$$

$$\frac{49}{19}$$

$$\frac{53}{38}$$

L.O.

$$\frac{43}{50}$$

$$\frac{40}{23}$$

$$\frac{36}{13}$$

$$\frac{27}{9}$$

$$\frac{31}{30}$$

$$\frac{29}{30}$$

$$\frac{45}{50}$$

$$\frac{38}{35} \frac{37}{43}$$

$$\frac{35}{27}$$

$$\frac{30}{12}$$

$$\frac{24}{8}$$

$$\frac{25}{31}$$

$$\frac{28}{31}$$

$$\frac{45}{50}$$

$$\frac{40}{50}$$

$$\frac{39}{24}$$

$$\frac{36}{11}$$

$$\frac{30}{7}$$

$$\frac{30}{24}$$

$$\frac{31}{50}$$

$$\frac{36}{50}$$

$$\frac{69}{50}$$

$$\frac{70}{30}$$

$$\frac{67}{14}$$

$$\frac{61}{8}$$

$$\frac{62}{29}$$

$$\frac{68}{29}$$

$$\frac{73}{50}$$

$$\frac{105}{50}$$

$$\frac{109}{24}$$

$$\frac{108}{14}$$

$$\frac{102}{10}$$

$$\frac{106}{27}$$

$$\frac{114}{27}$$

$$\frac{117}{50}$$

Sta	+	π	-	Elev.
		713.98		
38				909.6
	+50			08.1
39				06.8
	+50			06.2
40				06.1
	+50			06.3
41				07.5
	+50			08.5
42				08.6
	+50			08.7
43				08.7

Lt

4

Rt

$$\frac{34}{50} \quad \frac{37}{58} \quad \frac{38}{21} \quad \frac{38}{24} \quad \frac{50}{50} \quad \frac{5.7}{50}$$

$$\frac{21}{50} \quad \frac{28}{28} \quad \frac{24}{18} \quad \frac{35}{34} \quad \frac{40}{34} \quad \frac{41}{50}$$

$$\frac{11}{50} \quad \frac{13}{23} \quad \frac{28}{5} \quad \frac{16}{18} \quad \frac{22}{18} \quad \frac{24}{50}$$

Spt. 112 15" Oct Rt 44+50

$$\frac{89}{50} \quad \frac{94}{35} \quad \frac{95}{19} \quad \frac{94}{4} \quad \frac{104}{18} \quad \frac{111}{18} \quad \frac{120}{50}$$

$$\frac{75}{50} \quad \frac{82}{36} \quad \frac{26}{22} \quad \frac{84}{94} \quad \frac{103}{21} \quad \frac{112}{21} \quad \frac{115}{50}$$

$$\frac{62}{50} \quad \frac{74}{22} \quad \frac{74}{10} \quad \frac{80}{4} \quad \frac{89}{16} \quad \frac{96}{16} \quad \frac{98}{34} \quad \frac{94}{50}$$

$$\frac{47}{50} \quad \frac{53}{33} \quad \frac{55}{17} \quad \frac{58}{4} \quad \frac{66}{21} \quad \frac{76}{21} \quad \frac{77}{41} \quad \frac{76}{50}$$

$$\frac{38}{50} \quad \frac{48}{29} \quad \frac{44}{15} \quad \frac{48}{3} \quad \frac{57}{7} \quad \frac{62}{23} \quad \frac{74}{23} \quad \frac{81}{50}$$

$$\frac{45}{50} \quad \frac{76}{20} \quad \frac{45}{3} \quad \frac{55}{21} \quad \frac{70}{21} \quad \frac{98}{50}$$

$$\frac{56}{50} \quad \frac{62}{27} \quad \frac{61}{9} \quad \frac{57}{2} \quad \frac{66}{13} \quad \frac{72}{32} \quad \frac{95}{32} \quad \frac{16}{50}$$

$$\frac{92}{50} \quad \frac{93}{26} \quad \frac{92}{8} \quad \frac{84}{2} \quad \frac{85}{15} \quad \frac{102}{15} \quad \frac{118}{35} \quad \frac{148}{50}$$

Sta	+	X	-	Elev
		917.86		
48	+75			911.4
49				08.5
	+25			06.4
	+50			05.0
T.P	0.01	907.73 ✓	10.21	907.65 ✓
50				02.7
	+50			01.3
51				910.3
	+50			899.7
52				899.4
	+26			899.8
	+32			901.9

Lt.

E

Rt.

$$\frac{42}{30} \quad \frac{46}{28} \quad \frac{48}{8} \quad \frac{53}{3} \quad \frac{45}{12} \quad \frac{77}{32} \quad \frac{109}{50} \quad \frac{116}{50}$$

$$\frac{47}{50} \quad \frac{58}{30} \quad \frac{70}{13} \quad \frac{90}{3} \quad \frac{94}{12} \quad \frac{107}{32} \quad \frac{121}{50} \quad \frac{131}{50}$$

$$\frac{41}{50} \quad \frac{81}{36} \quad \frac{102}{17} \quad \frac{115}{13} \quad \frac{123}{33} \quad \frac{134}{33} \quad \frac{140}{50}$$

$$\frac{105}{50} \quad \frac{115}{37} \quad \frac{120}{16} \quad \frac{129}{16} \quad \frac{135}{33} \quad \frac{148}{33} \quad \frac{151}{50}$$

$$\frac{40}{50} \quad \frac{49}{35} \quad \frac{45}{16} \quad \frac{50}{14} \quad \frac{58}{32} \quad \frac{60}{32} \quad \frac{60}{50}$$

$$\frac{47}{50} \quad \frac{62}{34} \quad \frac{69}{13} \quad \frac{64}{14} \quad \frac{68}{35} \quad \frac{74}{35} \quad \frac{77}{50}$$

$$\frac{64}{30} \quad \frac{71}{24} \quad \frac{74}{11} \quad \frac{81}{50}$$

$$\frac{45}{50} \quad \frac{75}{23} \quad \frac{80}{18} \quad \frac{85}{50} \quad \frac{90}{50}$$

$$\frac{66}{50} \quad \frac{75}{23} \quad \frac{83}{11} \quad \frac{88}{50} \quad \frac{96}{50}$$

$$\frac{73}{50} \quad \frac{77}{23} \quad \frac{79}{20} \quad \frac{82}{50} \quad \frac{90}{50}$$

$$\frac{48}{50} \quad \frac{58}{50} \quad \frac{64}{50}$$

Sta.	+	Σ	-	Elev.
		907.73		
52 + 48.9	=	Cleveland Ave.		902.93
B.M.	4.96	907.73	4.96	902.77
+63				902.78
				02.4
+74				899.7
53				99.4
+50				99.6
54				99.5
+50				99.5
55				98.6
T.P.	12.52	912.24	8.01	899.72
+16	=	R. & Flow Line of Ditch		97.5
+50				97.7
56				97.2

Lt

L

Rt

$$\frac{41}{50}$$

$$\frac{48}{50}$$

$$\frac{53}{50}$$

Top Batt Spl. Elev. and 6' 2"

$$\frac{47}{50}$$

$$\frac{53}{50}$$

$$\frac{60}{50}$$

$$\frac{63}{50} \quad \frac{75}{20}$$

$$\frac{80}{50}$$

$$\frac{87}{22} \quad \frac{88}{50}$$

$$\frac{63}{50}$$

$$\frac{77}{20}$$

$$\frac{83}{50}$$

$$\frac{90}{33}$$

$$\frac{95}{50}$$

$$\frac{66}{50}$$

$$\frac{77}{19}$$

$$\frac{81}{50}$$

$$\frac{89}{32}$$

$$\frac{97}{50}$$

$$\frac{66}{50}$$

$$\frac{76}{23}$$

$$\frac{82}{50}$$

$$\frac{89}{32}$$

$$\frac{97}{50}$$

$$\frac{73}{50}$$

$$\frac{77}{24}$$

$$\frac{82}{50}$$

$$\frac{88}{32}$$

$$\frac{98}{50}$$

$$\frac{87}{50}$$

$$\frac{90}{23}$$

$$\frac{91}{50}$$

$$\frac{89}{32}$$

$$\frac{96}{50}$$

This section on
skew to R.

$$\left(\frac{148}{100} \quad \frac{147}{50} \quad \frac{147}{50} \quad \frac{153}{50} \quad \frac{160}{100} \right)$$

$$\frac{148}{50}$$

$$\frac{147}{28}$$

$$\frac{145}{50}$$

$$\frac{150}{33}$$

$$\frac{150}{50}$$

$$\frac{153}{50}$$

$$\frac{158}{32}$$

$$\frac{150}{50}$$

$$\frac{157}{33}$$

$$\frac{158}{50}$$

Sta.	+	π	-	Elev.
		912.24		
56	+50			897.1
57				98.1
	+50			99.7
58				902.1
	+43			06.8
	+59			07.5
	+72			08.0
	+82			12.5
T.P.	9.30	920.59 ✓	0.95	911.29 ✓
58	+72			908.0
	+82			12.5
59				13.0

Lt.

E

Rt.

$$\frac{156}{50} \quad \frac{152}{31} \quad \frac{151}{\quad} \quad \frac{160}{33} \quad \frac{134}{50}$$

$$\frac{142}{50} \quad \frac{142}{22} \quad \frac{141}{\quad} \quad \frac{147}{33} \quad \frac{143}{50}$$

$$\frac{132}{50} \quad \frac{129}{23} \quad \frac{125}{\quad} \quad \frac{123}{33} \quad \frac{120}{50}$$

$$\frac{105}{50} \quad \frac{104}{26} \quad \frac{98 \ 96 \ 92}{12 \ 32} \quad \frac{89}{50}$$

$$\frac{81}{50} \quad \frac{62}{19} \quad \frac{59}{\quad} \quad \frac{47}{13} \quad \frac{46}{32} \quad \frac{44}{50}$$

$$\frac{66}{50} \quad \frac{62}{39} \quad \frac{48}{15} \quad \frac{47}{\quad} \quad \frac{47}{32} \quad \frac{40}{50}$$

$$\frac{52}{50} \quad \frac{49}{24} \quad \frac{42}{\quad}$$

$$\frac{48}{30} \quad \frac{39}{19} \quad \frac{43}{\quad}$$

$$\textcircled{12.6} \quad \frac{77}{28} \quad \frac{67}{50}$$

$$\textcircled{8.1} \quad \frac{78}{14} \quad \frac{67}{32} \quad \frac{56}{50}$$

$$\frac{74}{50} \quad \frac{70}{41} \quad \frac{78}{18} \quad \frac{76}{\quad} \quad \frac{59}{13} \quad \frac{41}{30} \quad \frac{2.7}{50}$$

Sta	+	π	-	Elev.
		✓ 920.59		
59	+25			916.1
T.P.	8.92	✓ 926.23	3.28	✓ 917.31
	+68			19.4
60				21.8
	+90			22.5
	+70			21.8
B.M.	1.24	✓ 923.79	3.52	✓ 922.71 (922.75)
61				20.7
	+50			16.9
	+80			14.4
62				14.1
	+50			14.0
63				12.1
T.P.	0.90	✓ 914.01	10.88	✓ 913.11

2/4/38
slect.

34

Lt.

2

Rt.

$$\frac{56}{50} \frac{62}{28} \frac{55}{7} \frac{45}{11} \frac{27}{31} \frac{0.6}{50} \frac{+0.5}{50}$$

$$\frac{113}{50} \frac{10.9}{35} \frac{81}{10} \frac{68}{4} \frac{55}{33} \frac{32}{50} \frac{2.4}{50}$$

$$\frac{90}{50} \frac{6.2}{22} \frac{44}{7} \frac{36}{30} \frac{1.6}{30} \frac{2.3}{50}$$

$$\frac{81}{50} \frac{5.2}{22} \frac{45}{4} \frac{37}{12} \frac{37}{31} \frac{2.9}{50} \frac{2.9}{50}$$

$$\frac{7.3}{50} \frac{50}{20} \frac{44}{21} \frac{43}{50} \frac{3.9}{50}$$

Top M.C. Mount

$$\frac{5.2}{50} \frac{41}{28} \frac{33}{20} \frac{32}{20} \frac{2.8}{50}$$

$$\frac{8.0}{50} \frac{7.7}{33} \frac{7.8}{11} \frac{71}{19} \frac{6.7}{50} \frac{5.4}{50}$$

$$\frac{8.7}{50} \frac{9.5}{39} \frac{9.7}{19} \frac{96}{24} \frac{8.8}{50} \frac{8.1}{50}$$

$$\frac{8.3}{50} \frac{9.6}{24} \frac{9.9}{24} \frac{9.9}{24} \frac{9.1}{50}$$

$$\frac{7.4}{50} \frac{8.8}{25} \frac{10.0}{34} \frac{12.0}{50} \frac{11.4}{50}$$

$$\frac{9.5}{50} \frac{11.0}{26} \frac{11.9}{21} \frac{12.6}{21} \frac{13.5}{50}$$

Sta	+	X	-	Elev.
		✓ 914.01		
63	+21			911.9
	+27			08.3
	+60			05.9
64				03.3
	+50			01.7
65				01.2
	+50			900.9
66				900.7
T.P.	11.09	913.03 ✓	12.07	901.94 ✓
	+50			900.8
67				900.9
	+50			900.6

Lt.

2

Rt.

$$\frac{14}{50} \quad \frac{26}{19} \quad \frac{26}{6} \quad \frac{21}{22} \quad \frac{50}{22} \quad \frac{62}{50}$$

$$\frac{22}{50} \quad \frac{20}{37} \quad \frac{57}{25} \quad \frac{70}{25} \quad \frac{80}{50}$$

$$\frac{53}{30} \quad \frac{56}{45} \quad \frac{73}{20} \quad \frac{81}{24} \quad \frac{88}{24} \quad \frac{98}{50}$$

$$\frac{84}{50} \quad \frac{91}{35} \quad \frac{103}{15} \quad \frac{107}{25} \quad \frac{117}{25} \quad \frac{117}{50}$$

$$\frac{112}{50} \quad \frac{117}{23} \quad \frac{123}{20} \quad \frac{126}{20} \quad \frac{128}{50}$$

$$\frac{126}{50} \quad \frac{128}{23} \quad \frac{128}{25} \quad \frac{129}{25} \quad \frac{130}{50}$$

$$\frac{130}{50} \quad \frac{130}{25} \quad \frac{131}{25} \quad \frac{132}{25} \quad \frac{133}{50}$$

$$\frac{130}{50} \quad \frac{133}{50} \quad \frac{132}{50}$$

$$\frac{121}{50} \quad \frac{122}{50} \quad \frac{121}{50}$$

$$\frac{123}{50} \quad \frac{121}{50} \quad \frac{120}{50}$$

$$\frac{122}{50} \quad \frac{124}{50} \quad \frac{119}{50}$$

Sta	+	π ✓	-	Elev.
		913.03		
68				901.2
+65				01.6
69				03.1
+55				07.3
B.M.	2.79	913.07 ✓	2.79	910.24 (910.28)
+79				10.7
T.P.	11.27	923.01 ✓	1.33	911.74
+90				911.24
				14.7
70				15.0
+25				18.0
+55				19.4
71				17.7
+50				13.9

Lt

4

Rt

$$\frac{121}{50} \quad \frac{118}{50} \quad \frac{113}{23} \quad \frac{106}{50}$$

$$\frac{113}{50} \quad \frac{114}{50} \quad \frac{114}{50}$$

$$\frac{97}{50} \quad \frac{98}{25} \quad \frac{99}{26} \quad \frac{100}{50}$$

$$\frac{68}{50} \quad \frac{65}{18} \quad \frac{57}{27} \quad \frac{52}{50} \quad \frac{59}{50}$$

Spk. in 6" Pop. Lt. sta. 69+55

$$\frac{40}{50} \quad \frac{41}{32} \quad \frac{40}{14} \quad \frac{24}{30} \quad \frac{+12}{50} \quad \frac{+06}{50}$$

$$\frac{112}{50} \quad \frac{106}{28} \quad \frac{83}{22} \quad \frac{86}{22} \quad \frac{87}{50}$$

$$\frac{93}{50} \quad \frac{83}{37} \quad \frac{81}{17} \quad \frac{80}{22} \quad \frac{74}{22} \quad \frac{77}{50}$$

$$\frac{59}{50} \quad \frac{50}{41} \quad \frac{53}{21} \quad \frac{50}{27} \quad \frac{45}{27} \quad \frac{50}{50}$$

$$\frac{49}{50} \quad \frac{35}{40} \quad \frac{38}{33} \quad \frac{36}{26} \quad \frac{33}{26} \quad \frac{28}{50}$$

$$\frac{79}{50} \quad \frac{80}{44} \quad \frac{66}{36} \quad \frac{66}{20} \quad \frac{53}{23} \quad \frac{38}{23} \quad \frac{27}{50}$$

$$\frac{110}{50} \quad \frac{110}{41} \quad \frac{101}{32} \quad \frac{102}{20} \quad \frac{91}{24} \quad \frac{69}{41} \quad \frac{57}{50} \quad \frac{50}{50}$$

Sta + π ✓ - Elev
923.01

72 911.9

+60 10.5

73 11.0

+50 13.4

74 15.8

T.P. 6.18 923.13 6.06 916.95

+20 15.9

+50 15.0

75 13.7

+44 12.8

+61 11.0

76 09.1

Lt.

C

Rt.

$$\begin{array}{r} 12.6 \\ 50 \end{array} \quad \begin{array}{r} 12.0 \\ 32 \end{array} \quad \begin{array}{r} 11.4 \\ 23 \end{array} \quad \begin{array}{r} 11.1 \\ \hline \end{array} \quad \begin{array}{r} 9.7 \\ 24 \end{array} \quad \begin{array}{r} 8.0 \\ 50 \end{array}$$

$$\begin{array}{r} 14.1 \\ 50 \end{array} \quad \begin{array}{r} 13.8 \\ 37 \end{array} \quad \begin{array}{r} 13.5 \\ 17 \end{array} \quad \begin{array}{r} 12.5 \\ 30 \end{array} \quad \begin{array}{r} 11.8 \\ 50 \end{array} \quad \begin{array}{r} 10.9 \\ 50 \end{array}$$

$$\begin{array}{r} 14.0 \\ 50 \end{array} \quad \begin{array}{r} 13.4 \\ 32 \end{array} \quad \begin{array}{r} 13.3 \\ 21 \end{array} \quad \begin{array}{r} 12.0 \\ \hline \end{array} \quad \begin{array}{r} 11.1 \\ 28 \end{array} \quad \begin{array}{r} 9.6 \\ 50 \end{array}$$

$$\begin{array}{r} 13.4 \\ 50 \end{array} \quad \begin{array}{r} 13.3 \\ 43 \end{array} \quad \begin{array}{r} 12.6 \\ 29 \end{array} \quad \begin{array}{r} 10.6 \\ 16 \end{array} \quad \begin{array}{r} 9.6 \\ 22 \end{array} \quad \begin{array}{r} 7.3 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 50 \end{array}$$

$$\begin{array}{r} 13.0 \\ 50 \end{array} \quad \begin{array}{r} 12.1 \\ 33 \end{array} \quad \begin{array}{r} 8.3 \\ 16 \end{array} \quad \begin{array}{r} 7.2 \\ 22 \end{array} \quad \begin{array}{r} 5.5 \\ 50 \end{array} \quad \begin{array}{r} 3.7 \\ 50 \end{array}$$

$$\begin{array}{r} 13.0 \\ 50 \end{array} \quad \begin{array}{r} 11.8 \\ 31 \end{array} \quad \begin{array}{r} 8.5 \\ 16 \end{array} \quad \begin{array}{r} 7.2 \\ 22 \end{array} \quad \begin{array}{r} 5.2 \\ 22 \end{array} \quad \begin{array}{r} 3.3 \\ 50 \end{array}$$

$$\begin{array}{r} 12.9 \\ 50 \end{array} \quad \begin{array}{r} 12.0 \\ 35 \end{array} \quad \begin{array}{r} 9.3 \\ 15 \end{array} \quad \begin{array}{r} 8.1 \\ 28 \end{array} \quad \begin{array}{r} 6.0 \\ 50 \end{array} \quad \begin{array}{r} 4.0 \\ 50 \end{array}$$

$$\begin{array}{r} 12.3 \\ 50 \end{array} \quad \begin{array}{r} 11.9 \\ 39 \end{array} \quad \begin{array}{r} 10.8 \\ 20 \end{array} \quad \begin{array}{r} 9.8 \\ 10 \end{array} \quad \begin{array}{r} 9.4 \\ \hline \end{array} \quad \begin{array}{r} 8.1 \\ 25 \end{array} \quad \begin{array}{r} 6.1 \\ 50 \end{array}$$

$$\begin{array}{r} 12.9 \\ 50 \end{array} \quad \begin{array}{r} 12.6 \\ 34 \end{array} \quad \begin{array}{r} 12.0 \\ 14 \end{array} \quad \begin{array}{r} 11.2 \\ 4 \end{array} \quad \begin{array}{r} 10.3 \\ 22 \end{array} \quad \begin{array}{r} 9.6 \\ 22 \end{array} \quad \begin{array}{r} 7.7 \\ 50 \end{array}$$

$$\begin{array}{r} 13.4 \\ 50 \end{array} \quad \begin{array}{r} 13.5 \\ 28 \end{array} \quad \begin{array}{r} 12.6 \\ 10 \end{array} \quad \begin{array}{r} 12.1 \\ \hline \end{array} \quad \begin{array}{r} 9.8 \\ 15 \end{array} \quad \begin{array}{r} 9.4 \\ 34 \end{array} \quad \begin{array}{r} 8.2 \\ 50 \end{array}$$

$$\begin{array}{r} 14.4 \\ 50 \end{array} \quad \begin{array}{r} 14.2 \\ 26 \end{array} \quad \begin{array}{r} 14.0 \\ \hline \end{array} \quad \begin{array}{r} 13.2 \\ 26 \end{array} \quad \begin{array}{r} 10.6 \\ 45 \end{array} \quad \begin{array}{r} 10.3 \\ 50 \end{array}$$

Sta. + π / - ELEV
923.13

76 +32

918.6

+80

10.0

77

12.1

+45

17.3

T.P.

7.48

927.84

2.77

920.36

+70

17.9

78

19.3

+35

20.9

+53

21.0

+57

20.7

+60

20.8

+71

26.7

Lt.

4

Lt.

$$\frac{145}{50} \quad \frac{144}{25} \quad \frac{145}{25} \quad \frac{140}{30} \quad \frac{128}{50}$$

$$\frac{136}{50} \quad \frac{136}{22} \quad \frac{131}{22} \quad \frac{123}{22} \quad \frac{113}{50}$$

$$\frac{127}{50} \quad \frac{127}{24} \quad \frac{110}{25} \quad \frac{101}{25} \quad \frac{92}{50}$$

$$\frac{101}{50} \quad \frac{77}{28} \quad \frac{67}{13} \quad \frac{58}{25} \quad \frac{51}{25} \quad \frac{46}{30}$$

$$\frac{118}{50} \quad \frac{103}{33} \quad \frac{99}{25} \quad \frac{93}{9} \quad \frac{86}{30} \quad \frac{80}{50}$$

$$\frac{110}{50} \quad \frac{97}{21} \quad \frac{85}{16} \quad \frac{79}{16} \quad \frac{81}{33} \quad \frac{82}{50}$$

$$\frac{97}{50} \quad \frac{80}{34} \quad \frac{75}{14} \quad \frac{69}{14} \quad \frac{66}{34} \quad \frac{61}{50}$$

$$\frac{93}{50} \quad \frac{77}{25} \quad \frac{68}{25} \quad \frac{59}{25} \quad \frac{49}{50}$$

$$\frac{89}{50} \quad \frac{78}{25} \quad \frac{71}{25} \quad \frac{66}{25} \quad \frac{65}{50}$$

$$\frac{81}{50} \quad \frac{71}{25} \quad \frac{70}{25} \quad \frac{66}{25} \quad \frac{62}{50}$$

$$\frac{14}{50} \quad \frac{13}{25} \quad \frac{11}{25} \quad \frac{11}{25} \quad \frac{11}{50}$$

Sta + π / - Elev.

927.84 .

+84.65 = E Pavement

B.M.

1.11

926.73 926.727

"C"
Vic + to Rice

Co. Rd. "C"

Ditch Profiles R. & L.

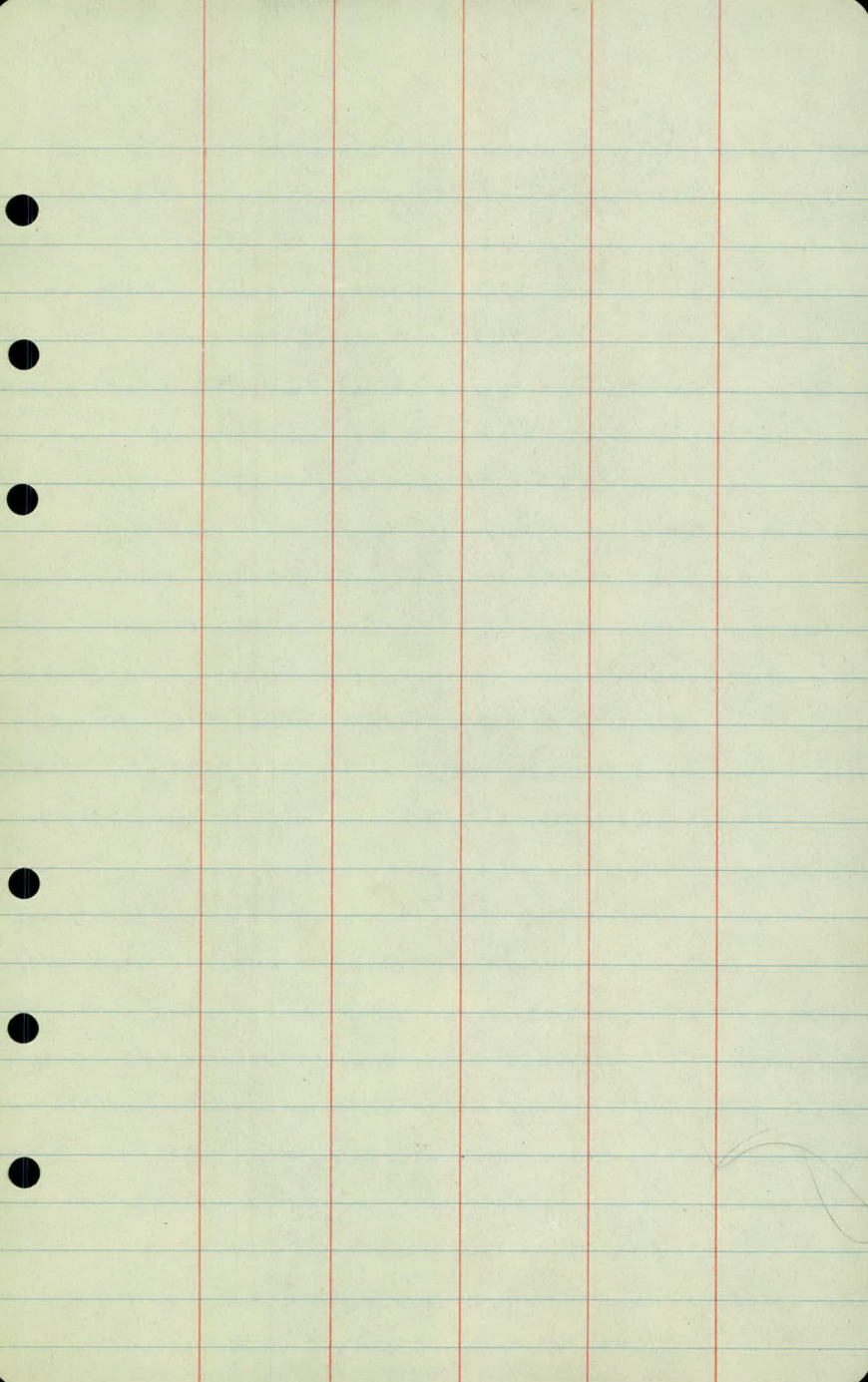
Intersection of Rice & Co Rd "C"
= 83 + 40.33

Rec'd 5/3/39.
Plotted 5/4/39 WJB.

Sta.	t	π	Lt.	Elev.	Rt.
B.M.	3.32	946.83	-	943.51	-
66		36.3	10.5	36.6	10.2
+12	FL	36.2	10.6		
+32		36.5	10.3		
+50		36.9	9.9	37.4	9.4
67		37.5	9.3	38.1	8.7
+50		38.8	8.0	39.0	7.8
68		40.1	6.7	40.5	6.3
+50		40.7	6.1	41.6	5.2
69		41.2	5.6	42.1	4.7
+50		41.3	5.5	43.2	3.6
70		41.2	5.6	43.0	3.8
+12	FL	41.0	5.8		
+32		41.0	5.8		
+50		41.3	5.5	43.1	3.7
71		41.4	5.4	43.6	6.2
+50		41.6	5.2	41.7	5.1
+93	FL	41.4	5.4		
72 + 01		41.4	5.4	39.6	7.2 Lower
+50		41.5	5.3	41.0	5.8
+67	FL	41.5	5.3		
+87		41.5	5.3		
73		41.9	4.9	42.2	4.6 42.2
+50		42.1	4.7	43.1	3.7 4.6
74		42.2	4.6	43.1	3.7 4.8 42.0

Spike in 18" Oak 150' Rt 67+35

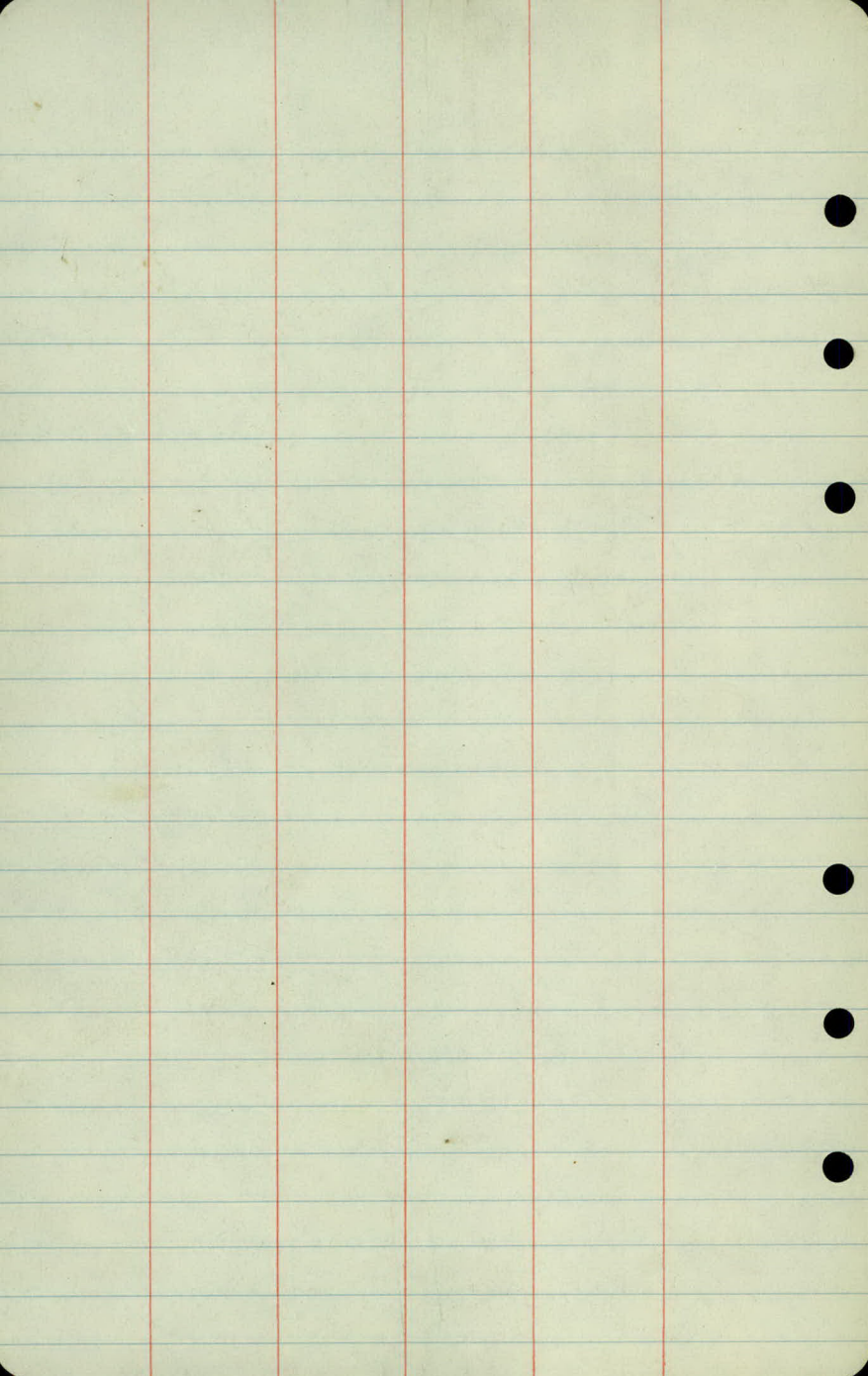
Sta	+	K	Lt -	Elev	Rt -
		946.83			
T.P.	6.35	951.68	1.50	945.33	42.0
74+50		42.5	9.2	42.5	9.2 9.7
75		42.3	9.4	42.5	9.2
+50		42.5	9.2	42.7	9.0 10.8 40.9
76		43.0	8.7	42.6	9.1 10.7
+50		43.4	8.3	43.8	7.9 41.0
+63	FL R			43.6	8.1
+83				44.4	7.3
+68	FL L	43.6	8.1		
+88		43.8	7.9		
77		44.0	7.7	44.7	7.0
+27	FL R			44.9	6.8
+47				45.0	6.7
+50		44.1	7.6		
78		44.2	7.5	45.0	6.7
+10	FL L	44.4	7.3		
+30		44.4	7.3		43.9
+50		44.4	7.3	44.1	7.6 7.8
79		44.6	7.1	44.5	7.2
+30	FL R			45.0	6.7
+50		44.5	7.2	44.9	6.8
80		44.4	7.3	44.9	6.8
+50		44.6	7.1	46.4	5.3
+60	FL R			46.6	5.1
+80				46.7	5.0



Sta	+	π	Lt. -	Elev	Rt. -
		951.68			
81		45.0	6.7	47.4	4.3
+16		45.3	6.4		
+41		46.0	5.7		45.9
+50		46.5	5.2	46.9	4.8 (5.8)
82		51.0	0.7	51.3	0.4
T.P	8.80	959.82	0.66	951.02	
B.M.			1.93	957.89	957.91

St+20-7.00 Drain tile Lead in from North
(Apparent Control Pt. of Ditch)

Top Mon Rice st. E Co. Rd. "C"



1
slope stakes

Co. Rd. "C"

Sta # 8 to New Brighton Rd.

20 PAGES

Sta.	I	K	-	Grade
B.M.	0.35	951.26		(950.91)
0	400			950.91
	+14.5			50.9
	+19			50.8
	+27			50.6
	+40			50.5
	+70			49.8
1				49.1
	+50			47.4
2				45.3
	+50			43.2
3				41.7
T.P.	4.66	949.36	12.56	932.70

Cor. Rod.

Lt

R.

Rt

Held in Pav. R. 57.4. "64 Cor. Rod. 62"

1.5

$$26.2 / \begin{array}{r} 49 \\ -34 \end{array}$$

$$\begin{array}{r} 53 \\ -38 \end{array}$$

$$\begin{array}{r} 53 \\ -38 \end{array} / 26.4$$

2.2

$$25.2 / \begin{array}{r} 56 \\ -34 \end{array}$$

$$\begin{array}{r} 64 \\ -44 \end{array}$$

$$\begin{array}{r} 55 \\ -43 \end{array} / 24.8$$

3.9

$$27.9 / \begin{array}{r} 82 \\ -43 \end{array}$$

$$\begin{array}{r} 77 \\ -38 \end{array}$$

$$\begin{array}{r} 64 \\ -25 \end{array} / 22.5$$

6.0

$$26.1 / \begin{array}{r} 97 \\ -37 \end{array}$$

$$\begin{array}{r} 88 \\ -28 \end{array} / 23.9$$

8.1

$$27.6 / \begin{array}{r} 123 \\ -42 \end{array}$$

$$\begin{array}{r} 121 \\ -40 \end{array}$$

$$\begin{array}{r} 113 \\ -32 \end{array} / 20.6$$

9.6

$$26.4 / \begin{array}{r} 134 \\ -38 \end{array}$$

$$\begin{array}{r} 131 \\ -35 \end{array}$$

$$\begin{array}{r} 128 \\ -32 \end{array} / 24.6$$

Sta.	+	X	-	Grade
		748.36		
3	+50			40.7
4				40.2
	+50			40.0
T.P.	8.42	747.93	1.85	941.51
	+80			39.9
5				39.8
	+35			39.7
	+70			39.5
6				39.4
	+35			39.3
	+80			39.1
7				39.0

Geo. Rod

11

12

12

2.7	Cal V 69 29.1	$\begin{array}{r} 24.6 / 5.9 \\ -3.2 \end{array}$	$\begin{array}{r} 6.0 \\ -3.9 \end{array}$	$\begin{array}{r} 5.8 / 24.3 \\ -3.1 \end{array}$	Cal V 62 23.9
3.2		$\begin{array}{r} 20.4 / 6.0 \\ -1.8 \end{array}$	$\begin{array}{r} 5.1 \\ -1.9 \end{array}$	$\begin{array}{r} 5.4 / 21.6 \\ -2.2 \end{array}$	
3.4		$\begin{array}{r} 28.1 / 2.6 \\ -10.8 \end{array}$	$\begin{array}{r} 3.7 \\ -0.3 \end{array}$	$\begin{array}{r} 4.1 / 25.1 \\ -10.8 \end{array}$	
10.0		$\begin{array}{r} 32.9 / 6.8 \\ -13.2 \end{array}$	$\begin{array}{r} 6.8 \\ -13.2 \end{array}$	$\begin{array}{r} 7.6 / 31.3 \\ -12.9 \end{array}$	
10.1		$\begin{array}{r} 36.1 / 5.3 \\ -14.8 \end{array}$	$\begin{array}{r} 5.2 \\ -14.9 \end{array}$	$\begin{array}{r} 6.3 / 34.1 \\ -13.8 \end{array}$	
10.2		$\begin{array}{r} 36.7 / 5.1 \\ -15.1 \end{array}$	$\begin{array}{r} 4.5 \\ -15.7 \end{array}$	$\begin{array}{r} 5.5 / 35.9 \\ -14.7 \end{array}$	
10.4		$\begin{array}{r} 38.5 / 4.9 \\ -14.0 \end{array}$	$\begin{array}{r} 4.2 \\ -13.2 \end{array}$	$\begin{array}{r} 5.9 / 35.5 \\ -14.5 \end{array}$	
10.5		$\begin{array}{r} 40.9 / 3.3 \\ -17.2 \end{array}$	$\begin{array}{r} 4.9 \\ -14.2 \end{array}$	$\begin{array}{r} 7.4 / 32.7 \\ -13.1 \end{array}$	
10.6		$\begin{array}{r} 41.7 / 3.0 \\ -17.6 \end{array}$	$\begin{array}{r} 6.9 \\ -13.7 \end{array}$	$\begin{array}{r} 3.9 / 28.1 \\ -14.3 \end{array}$	
10.8		$\begin{array}{r} 32.3 / 7.9 \\ -12.9 \end{array}$	$\begin{array}{r} 11.8 \\ -11.0 \end{array}$	$\begin{array}{r} 11.7 / 24.7 \\ -13.0 \end{array}$	
10.9		$\begin{array}{r} 22.9 / 11.2 \\ -12.7 \end{array}$	$\begin{array}{r} 12.5 \\ -1.4 \end{array}$	$\begin{array}{r} 14.0 / 24.3 \\ -3.1 \end{array}$	

Sta	+	π	-	Grade
		747.93		
7	+50			38.8
8				38.6
	+50			38.5
9				38.4
T.P.	56.2	744.52	11.03	738.90
	+50			38.5
10				38.7
	+45			38.9
	+75			39.1
11				39.2
T.P.	3.02	741.72		738.90
	+35			39.4
	+75			39.6

Cor Rod.

Lk

R

RL

11.1

$$26.5 / \frac{11.1}{10.0}$$

$$\frac{12.7}{-1.6}$$

$$\frac{11.8}{208} / 25.1$$

11.3

$$28.5 / \frac{10.3}{10.0}$$

$$\frac{12.8}{-1.5}$$

$$\frac{12.6}{202} / 23.9$$

11.4

$$27.5 / \frac{10.9}{10.5}$$

$$\frac{13.8}{-2.1}$$

$$\frac{13.3}{-1.7} / 20.7$$

11.5

$$24.9 / \frac{12.3}{10.7}$$

$$\frac{13.3}{-1.8}$$

$$\frac{13.6}{-2.1} / 21.3$$

+ 22

(8.5)
Cul.(F.Kul.)
8.3

Top Slump.

6.0

$$22.5 / \frac{8.5}{-2.5}$$

$$\frac{8.2}{-2.2}$$

$$\frac{8.2}{-2.2} / 21.6$$

5.8

$$24.7 / \frac{6.7}{10.6}$$

$$\frac{6.4}{-0.6}$$

$$\frac{6.8}{205} / 24.5$$

5.6

$$28.1 / \frac{4.8}{10.8}$$

$$\frac{3.6}{+3.0}$$

$$\frac{3.8}{11.8} / 30.1$$

5.4

$$27.3 / \frac{5.0}{10.4}$$

$$\frac{2.8}{+2.6}$$

$$\frac{3.5}{209} / 32.3$$

5.3

$$24.3 / \frac{6.4}{10.4}$$

$$\frac{5.1}{10.0}$$

$$\frac{6.0}{208} / 25.1$$

Top Slump.

2.5

$$22.8 / \frac{5.1}{-2.6}$$

$$\frac{6.2}{-5.7}$$

$$\frac{8.1}{-5.6} / 31.8$$

2.3

$$23.1 / \frac{5.0}{-2.7}$$

$$\frac{7.1}{-4.8}$$

$$\frac{9.9}{-7.6} / 37.9$$

Step	t	A	-	Grade
		741.92		

12				39.7
----	--	--	--	------

+30				39.9
-----	--	--	--	------

+75				40.1
-----	--	--	--	------

13				40.2
----	--	--	--	------

T.P.	76.7	948.26	133	940.59
------	------	--------	-----	--------

+30				40.4
-----	--	--	--	------

+60				40.5
-----	--	--	--	------

14				40.7
----	--	--	--	------

+50				41.0
-----	--	--	--	------

15				41.2
----	--	--	--	------

+50				41.5
-----	--	--	--	------

16				41.7
----	--	--	--	------

T.P.	3.33	950.63	0.96	947.36
------	------	--------	------	--------

Gr. Rod

Lt

L

Lt

2.2

$$26.1 / \frac{59}{-37}$$

$$\frac{86}{-64}$$

$$\frac{10.2}{-80} / 39.0$$

2.0

$$29.1 / \frac{67}{-47}$$

$$\frac{92}{-72}$$

$$\frac{10.2}{-82} / 39.6$$

1.8

$$23.7 / \frac{47}{-27}$$

$$\frac{45}{-27}$$

$$\frac{52}{-34} / 25.2$$

1.7

$$25.7 / \frac{41}{-21}$$

$$\frac{0.9}{+0.8}$$

$$\frac{22}{+0.07} / 25.3$$

1.9

$$31.5 / \frac{59}{+25}$$

$$\frac{53}{+26}$$

$$\frac{74}{+0.5} / 27.5$$

1.8

$$32.7 / \frac{47}{+27}$$

$$\frac{52}{+26}$$

$$\frac{59}{+0.8} / 30.1$$

1.6

$$28.9 / \frac{69}{+12}$$

$$\frac{48}{+2.8}$$

$$\frac{46}{+3.0} / 32.5$$

2.3

$$26.9 / \frac{71}{+0.2}$$

$$\frac{54}{+1.7}$$

$$\frac{60}{+1.3} / 29.1$$

2.1

$$28.3 / \frac{62}{+0.9}$$

$$\frac{66}{+0.5}$$

$$\frac{75}{+1.1} / 25.7$$

6.8

$$28.5 / \frac{58}{+1.0}$$

$$\frac{64}{+0.4}$$

$$\frac{75}{+0.8} / 25.1$$

6.6

$$29.5 / \frac{51}{+1.5}$$

$$\frac{43}{+2.3}$$

$$\frac{16}{+5.0} / 36.5$$

Sta	+	π	-	Grade
		950.63		
16	+40			41.9
	+60			42.0
17				42.2
	+50			42.5
18				42.7
	+50			42.9
19				43.2
B.M.	5.71	950.58	5.71	944.92 (944.87)
	+50			43.5
20				43.7
	+50			44.0
21				44.2
I.P.	4.33	949.12	5.79	944.79

Cor. Rod. Lt. R. Rt.

$$8.7 \quad 30.9 / \begin{array}{r} 4.5 \\ 12.2 \end{array} \quad \begin{array}{r} 80 \\ 157 \end{array} \quad \begin{array}{r} 1.3 \\ 174 \end{array} / 1.3$$

$$8.6 \quad 31.1 / \begin{array}{r} 6.9 \\ 12.3 \end{array} \quad \begin{array}{r} 35 \\ 151 \end{array} \quad \begin{array}{r} 2.1 \\ 45 \end{array} / 37.5$$

$$8.4 \quad 28.7 / \begin{array}{r} 7.3 \\ 11.1 \end{array} \quad \begin{array}{r} 65 \\ 117 \end{array} \quad \begin{array}{r} 53 \\ 121 \end{array} / 32.7$$

$$8.1 \quad 29.5 / \begin{array}{r} 6.6 \\ 11.5 \end{array} \quad \begin{array}{r} 79 \\ 102 \end{array} \quad \begin{array}{r} 81 \\ 105 \end{array} / 26.5$$

$$7.9 \quad 33.5 / \begin{array}{r} 4.4 \\ 15.5 \end{array} \quad \begin{array}{r} 75 \\ 104 \end{array} \quad \begin{array}{r} 87 \\ 107 \end{array} / 24.9$$

$$7.7 \quad 27.1 / \begin{array}{r} 7.4 \\ 10.3 \end{array} \quad \begin{array}{r} 95 \\ 118 \end{array} \quad \begin{array}{r} 89 \\ 103 \end{array} / 24.1$$

$$7.4 \quad 22.8 / \begin{array}{r} 10.0 \\ 12.6 \end{array} \quad \begin{array}{r} 98 \\ 124 \end{array} \quad \begin{array}{r} 79 \\ 110 \end{array} / 25.5$$

Top Conc. Base Cor. Fg. Post 36' Rt. 17496

$$7.1 \quad 19.8 / \begin{array}{r} 8.7 \\ 11.6 \end{array} \quad \begin{array}{r} 87 \\ 106 \end{array} \quad \begin{array}{r} 61 \\ 110 \end{array} / 28.5$$

$$6.9 \quad 24.9 / \begin{array}{r} 7.7 \\ 10.7 \end{array} \quad \begin{array}{r} 67 \\ 102 \end{array} \quad \begin{array}{r} 55 \\ 114 \end{array} / 27.3$$

$$6.6 \quad 24.3 / \begin{array}{r} 7.7 \\ 10.4 \end{array} \quad \begin{array}{r} 73 \\ 107 \end{array} \quad \begin{array}{r} 51 \\ 115 \end{array} / 29.5$$

$$6.4 \quad 26.3 / \begin{array}{r} 6.5 \\ 10.4 \end{array} \quad \begin{array}{r} 68 \\ 104 \end{array} \quad \begin{array}{r} 46 \\ 118 \end{array} / 30.1$$

Sta	+	1	-	Grade
		949.12		
21	+40			44.3
	+80			44.3
22				44.2
	+38			43.9
	+67			43.5
23				43.1
	+34			42.4
	+67			41.7
24				40.9
	+50			39.6
T.P.	2.64	948.01	9.69	939.33
25				38.2

Cor Rod

Lt

R

Rt

$$4.8 \quad 28.1 / \frac{40}{10.8} \quad \frac{52}{-0.4} \quad \frac{52}{41/25.7}$$

$$4.8 \quad 28.1 / \frac{32}{11.6} \quad \frac{29}{+1.9} \quad \frac{37}{41/25.7}$$

$$4.9 \quad 28.1 / \frac{28}{11.1} \quad \frac{24}{+2.5} \quad \frac{23}{+2.4/31.7}$$

$$5.2 \quad 31.3 / \frac{28}{12.4} \quad \frac{25}{+2.7} \quad \frac{26}{+2.4/31.7}$$

$$5.4 \quad 35.7 / \frac{10}{11.6} \quad \frac{2.5}{13.1} \quad \frac{2.7}{+2.7/32.3}$$

$$6.0 \quad 30.9 / \frac{58}{12.2} \quad \frac{47}{11.3} \quad \frac{39}{+2.1/30.7}$$

$$6.7 \quad 28.1 / \frac{59}{10.8} \quad \frac{43}{10.4} \quad \frac{57}{110/88.5}$$

$$7.4 \quad 32.5 / \frac{39}{13.5} \quad \frac{42}{11.2} \quad \frac{46}{109/28.1}$$

$$8.2 \quad 35.3 / \frac{38}{14.4} \quad \frac{74}{10.8} \quad \frac{68}{114/29.3}$$

$$9.5 \quad 28.1 / \frac{82}{11.3} \quad \frac{22}{10.2} \quad \frac{82}{108/28.1}$$

R5/2.25

$$3.7 \quad 28.9 / \frac{27}{11.2} \quad \frac{31}{10.8} \quad \frac{30}{10.9/28.3}$$

Sta

+

x

-

Cascade

742.07

25 +35

17.3

+70

36.3

26

35.5

B.M.

5.51

742.15

5.51

736.56

(736.64)

+50

34.2

27

32.8

+50

31.5

28

30.1

+0.5

T.R.

1.35

732.70

10.80

731.25

+50

28.2

29

27.4

+50

26.1

30

24.7

Cor Rod.

Lt

4

Dist

4.8	$32.3 / 1.9$ $+2.9$	3.9 $+1.9$	8.2 $+6 / 27.7$
-----	------------------------	-----------------	----------------------

5.8	$29.9 / 4.1$ $+1.7$	4.2 $+1.6$	4.0 $+1.8 / 30.1$
-----	------------------------	-----------------	------------------------

6.7	$30.1 / 7.9$ $+1.8$	5.0 $+1.6$	5.3 $+1.4 / 29.3$
-----	------------------------	-----------------	------------------------

Top Mont 26105.93

8.0	$25.5 / 7.5$ $+1.0$	8.2 -0.2	9.0 $+0.5 / 29.5$
-----	------------------------	-----------------	------------------------

9.4	$25.5 / 7.9$ $+1.0$	9.8 -0.4	10.7 $+0.2 / 23.9$
-----	------------------------	-----------------	-------------------------

10.7	$26.1 / 7.9$ $+1.3$	11.6 -0.9	12.3 $+0.0 / 23.5$
------	------------------------	------------------	-------------------------

12.1	$27.7 / 11.5$ $+0.6$	11.4 $+0.7$	13.0 $+0.6 / 29.7$
------	-------------------------	------------------	-------------------------

3.9	$28.3 / 3.0$ $+0.7$	3.9 $+0.5$	4.5 $+0.9 / 25.3$
-----	------------------------	-----------------	------------------------

5.3	$29.5 / 3.5$ $+1.5$	4.0 $+1.3$	5.3 $+1.5 / 26.5$
-----	------------------------	-----------------	------------------------

6.6	$28.7 / 5.4$ $+1.2$	5.7 $+0.7$	6.9 $+0.2 / 25.9$
-----	------------------------	-----------------	------------------------

8.0	$27.9 / 7.3$ $+0.7$	7.1 $+0.9$	8.4 $+1.1 / 25.7$
-----	------------------------	-----------------	------------------------

Sta.	+	π	-	Grade	
		922.70			
30	+50			23.4	
31				22.3	-1.4
T.P.	2.37	924.16	10.91	921.79	
	+50			21.4	
31	+75			20.7	
		+15' 24" X 60' Culv.			
32	+16			20.4	
	+23			20.3	
	+40			20.0	
	+51			19.9	
	+65			19.7	
	+75			19.6	
33				19.2	
B.M.	10.55	924.85	7.80	914.36	914.30

Gr. Rod

Lt.

2

Lt.

9.3

$$26.3 / \frac{94}{10.7}$$

$$\frac{98}{10}$$

$$\frac{108}{15} / 9.5$$

10.4

$$24.3 / \frac{45}{20.7}$$

$$\frac{118}{1.7}$$

$$\frac{127}{23} / 2.9$$

2.8

$$21.9 / \frac{51}{23}$$

$$\frac{49}{-2.7}$$

$$\frac{45}{17} / 2.1$$

3.5

$$22.5 / \frac{60}{25}$$

$$\frac{59}{-2.4}$$

$$\frac{54}{-19} / 2.7$$

4.2

4.9

$$\frac{75}{3.2} / 24.6$$

4.5

$$27.0 / \frac{85}{40}$$

4.6

$$29.4 / \frac{94}{48}$$

$$\frac{91}{-4.5}$$

$$\frac{9.2}{-46} / 28.8$$

5.0

$$30.9 / \frac{103}{5.3}$$

$$\frac{103}{-5.3}$$

$$\frac{97}{-47} / 29.1$$

Spk. in East "H" Pole 75' Lt 33+37

Sta + π - E/cv

92485

33 +50

18.5

34

17.8

+50

17.1

35

16.4

+50

15.7

36

15.0

+25

14.6

+50

14.3

37

13.6

+50

12.9

T.P.

0.63

911.89

13.57

911.26

38

12.2

Gr Rod

Lt

R

Rt

$$6.4 \quad 330 / \begin{array}{r} 126 \\ -6.2 \end{array} \quad \begin{array}{r} 11.3 \\ -49 \end{array} \quad \begin{array}{r} 10.4 \\ -40 / 27.0 \end{array}$$

$$7.1 \quad 288 / \begin{array}{r} 117 \\ -46 \end{array} \quad \begin{array}{r} 10.6 \\ -35 \end{array} \quad \begin{array}{r} 10.3 \\ -3.2 / 28.6 \end{array}$$

$$7.8 \quad 240 / \begin{array}{r} 108 \\ -30 \end{array} \quad \begin{array}{r} 9.1 \\ -13 \end{array} \quad \begin{array}{r} 9.2 \\ -9.1 / 28.7 \end{array}$$

$$8.5 \quad 245 / \begin{array}{r} 95 \\ 1005 \end{array} \quad \begin{array}{r} 8.2 \\ 103 \end{array} \quad \begin{array}{r} 8.0 \\ 105 / 27.5 \end{array}$$

$$9.2 \quad 30.1 / \begin{array}{r} 74 \\ +1.8 \end{array} \quad \begin{array}{r} 6.0 \\ +3.2 \end{array} \quad \begin{array}{r} 6.2 \\ 15.0 / 32.5 \end{array}$$

$$9.9 \quad 36.3 / \begin{array}{r} 50 \\ +4.9 \end{array} \quad \begin{array}{r} 3.6 \\ 10.3 \end{array} \quad \begin{array}{r} 9.5 \\ 16.9 / 39.3 \end{array}$$

$$10.3 \quad 38.3 / \begin{array}{r} 44 \\ 75.9 \end{array} \quad \begin{array}{r} 3.3 \\ 17.0 \end{array} \quad \begin{array}{r} 3.4 \\ 16.9 / 40.3 \end{array}$$

$$10.6 \quad 37.9 / \begin{array}{r} 49 \\ 13.9 \end{array} \quad \begin{array}{r} 8.9 \\ 10.7 \end{array} \quad \begin{array}{r} 4.4 \\ 10.2 / 38.9 \end{array}$$

$$11.3 \quad 32.3 / \begin{array}{r} 85 \\ +2.8 \end{array} \quad \begin{array}{r} 6.9 \\ 14.4 \end{array} \quad \begin{array}{r} 7.8 \\ +3.5 / 33.5 \end{array}$$

$$12.0 \quad 26.1 / \begin{array}{r} 12.2 \\ 11.3 \end{array} \quad \begin{array}{r} 11.1 \\ 70.9 \end{array} \quad \begin{array}{r} 12.1 \\ 11.4 / 26.3 \end{array}$$

$$10.3 \quad 228 / \begin{array}{r} 23 \\ -26 \end{array} \quad \begin{array}{r} 2.1 \\ -26 \end{array} \quad \begin{array}{r} 2.9 \\ -3.2 / 24.6 \end{array}$$

Sta	+	π	-	Grade
		71189		
38	+50			11.5
39				10.8
	+50			10.2
40				09.7
	+50			09.5
41				09.3
	+50			09.4
42				09.6
	+50			09.9
43				10.2
T.P.	8.91	718.89	1.91	909.98
	+50			10.5

Gr. Rod.

Lt.

R.

Rt.

$$0.4 \quad 249 \begin{array}{r} 37 \\ -23 \\ \hline \end{array} \quad \begin{array}{r} 37 \\ -33 \\ \hline 4 \end{array} \quad \begin{array}{r} 46 \\ -42 \\ \hline 27.6 \end{array}$$

$$1.1 \quad 270 \begin{array}{r} 51 \\ -40 \\ \hline \end{array} \quad \begin{array}{r} 51 \\ -40 \\ \hline 11 \end{array} \quad \begin{array}{r} 5.5 \\ -4.4 \\ \hline 28.2 \end{array}$$

$$1.7 \quad 270 \begin{array}{r} 57 \\ -40 \\ \hline \end{array} \quad \begin{array}{r} 57 \\ -40 \\ \hline 17 \end{array} \quad \begin{array}{r} 61 \\ -44 \\ \hline 28.2 \end{array}$$

$$2.2 \quad 264 \begin{array}{r} 40 \\ -38 \\ \hline \end{array} \quad \begin{array}{r} 58 \\ -36 \\ \hline 22 \end{array} \quad \begin{array}{r} 63 \\ -41 \\ \hline 27.3 \end{array}$$

$$2.4 \quad 240 \begin{array}{r} 54 \\ -30 \\ \hline \end{array} \quad \begin{array}{r} 57 \\ -33 \\ \hline 24 \end{array} \quad \begin{array}{r} 62 \\ -38 \\ \hline 26.4 \end{array}$$

$$2.6 \quad 210 \begin{array}{r} 46 \\ -20 \\ \hline \end{array} \quad \begin{array}{r} 45 \\ -19 \\ \hline 26 \end{array} \quad \begin{array}{r} 51 \\ -25 \\ \hline 22.7 \end{array}$$

$$2.5 \quad 243 \begin{array}{r} 36 \\ -09 \\ \hline \end{array} \quad \begin{array}{r} 35 \\ -10 \\ \hline 25 \end{array} \quad \begin{array}{r} 43 \\ -18 \\ \hline 20.4 \end{array}$$

$$2.3 \quad 247 \begin{array}{r} 32 \\ -16 \\ \hline \end{array} \quad \begin{array}{r} 34 \\ -11 \\ \hline 23 \end{array} \quad \begin{array}{r} 46 \\ -23 \\ \hline 21.9 \end{array}$$

$$2.0 \quad 243 \begin{array}{r} 31 \\ -04 \\ \hline \end{array} \quad \begin{array}{r} 38 \\ -18 \\ \hline 20 \end{array} \quad \begin{array}{r} 43 \\ -23 \\ \hline 21.9 \end{array}$$

$$1.7 \quad 247 \begin{array}{r} 26 \\ -06 \\ \hline \end{array} \quad \begin{array}{r} 31 \\ -14 \\ \hline 17 \end{array} \quad \begin{array}{r} 40 \\ -23 \\ \hline 21.9 \end{array}$$

$$8.4 \quad 259 \begin{array}{r} 87 \\ -02 \\ \hline \end{array} \quad \begin{array}{r} 87 \\ -03 \\ \hline 84 \end{array} \quad \begin{array}{r} 99 \\ -00 \\ \hline 23.5 \end{array}$$

Sta	+	x	-	Grade
		915.89		

44				10.8
----	--	--	--	------

+50				11.1
-----	--	--	--	------

B.M.				913.52
------	--	--	--	--------

45				11.4
----	--	--	--	------

+50				11.7
-----	--	--	--	------

46				12.0
----	--	--	--	------

T.P.	547	922.56	1.80	917.09
------	-----	--------	------	--------

+50				12.2
-----	--	--	--	------

47				12.0
----	--	--	--	------

+50				11.6
-----	--	--	--	------

48				10.9
----	--	--	--	------

+50				09.9
-----	--	--	--	------

+75				07.2
-----	--	--	--	------

T.P.	1.74	911.02	13.28	909.28
------	------	--------	-------	--------

Gr. Rod

Lt.

L

Rt.

8.1

$$28.1 / \frac{7.3}{12.8}$$

$$\frac{7.4}{12.7}$$

$$\frac{8.6}{12.19} / 25.5$$

7.8

$$29.7 / \frac{6.2}{11.6}$$

$$\frac{6.3}{11.5}$$

$$\frac{7.3}{10.5} / 27.5$$

3pk. in 15" 110' Rt. 44+50

7.5

$$31.7 / \frac{4.9}{12.6}$$

$$\frac{5.9}{11.6}$$

$$\frac{7.0}{10.5} / 27.5$$

Eos.

p

7.2

$$33.5 / \frac{3.7}{13.5}$$

$$\frac{5.8}{11.4}$$

$$\frac{6.9}{10.9} / 27.1$$

6.9

$$35.5 / \frac{2.9}{14.5}$$

$$\frac{4.0}{12.5}$$

$$\frac{3.1}{11.9} / 30.1$$

10.4

$$38.9 / \frac{4.2}{16.2}$$

$$\frac{5.7}{14.7}$$

$$\frac{6.9}{13.5} / 31.0$$

10.6

$$40.7 / \frac{3.5}{17.1}$$

$$\frac{4.9}{15.7}$$

$$\frac{6.9}{13.7} / 33.0$$

11.0

$$41.5 / \frac{3.5}{17.5}$$

$$\frac{4.8}{16.2}$$

$$\frac{7.4}{12.6} / 33.0$$

11.7

$$39.1 / \frac{3.4}{16.3}$$

$$\frac{5.0}{15.9}$$

$$\frac{8.2}{12.8} / 32.1$$

12.7

$$39.5 / \frac{3.7}{17.0}$$

$$\frac{8.0}{14.7}$$

$$\frac{10.8}{11.9} / 30.3$$

13.4

$$34.7 / \frac{3.3}{17.1}$$

$$\frac{11.0}{12.4}$$

$$\frac{14.4}{10.5} / 24.5$$

Sta. + x - Grade

711.02

49

086

+25

078

+50

071

50

058

+50

047

51

028

+50

032

52

$$\begin{array}{r} \text{L.t.} \\ 986.3 \\ \hline 285 \end{array}$$

Culv.

$$\begin{array}{r} \text{L.t.} \\ \text{Elev. 849.3} \\ \hline 25.5 \end{array}$$

028

+26

027

+32

026

+48.9

026

B.M.

8.26

902.76

902.78

Gr Rod.

Lt.

R.

Rt.

2.4

$$33.3 / \frac{71.0}{+34}$$

$$\frac{28}{-44}$$

$$\frac{44}{-20/21.0}$$

↑

Ess

3.2

$$26.7 / \frac{31}{+0.1}$$

$$\frac{46}{-14}$$

$$\frac{62}{-39/24.0}$$

3.9

$$23.7 / \frac{53}{+0.1}$$

$$\frac{61}{-22}$$

$$\frac{77}{-45/28.5}$$

5.2

$$22.8 / \frac{78}{-26}$$

$$\frac{83}{-31}$$

$$\frac{93}{-41/27.3}$$

6.3

$$25.5 / \frac{28}{-35}$$

$$\frac{99}{-36}$$

$$\frac{105}{-42/27.6}$$

7.2

$$24.7 / \frac{105}{-33}$$

$$\frac{108}{-36}$$

$$\frac{115}{-43/27.9}$$

7.8

$$24.3 / \frac{109}{-31}$$

$$\frac{113}{-35}$$

$$\frac{121}{-43/27.9}$$

8.2

$$23.1 / \frac{109}{-27}$$

$$\frac{115}{-33}$$

$$\frac{127}{-45/28.5}$$

1/6/39 Completed

Tap Bolt 3pk 6th Cleveland Arc & Gold's 2"

Sta.	+	X	-	Grade
B.M.	268	905.46		902.78

52	+63			902.4
----	-----	--	--	-------

	+74			02.3
--	-----	--	--	------

53				02.2
----	--	--	--	------

	+50			02.0
--	-----	--	--	------

54				01.8
----	--	--	--	------

	+50			01.6
--	-----	--	--	------

55				01.4
----	--	--	--	------

	+16			01.3
--	-----	--	--	------

	+50			01.2
--	-----	--	--	------

56				01.0
----	--	--	--	------

	+50			0.11
--	-----	--	--	------

Gr. Rod Lt. & Rt.

Top Bolt spt. Cleveland + Co. Rod "C"

3.1

26
52

3.3

$$21.0 / \frac{53}{-30}$$

$$\frac{60}{-27}$$

$$\frac{65}{-32} / 246$$

3.5

$$20.1 / \frac{52}{-17}$$

$$\frac{58}{-23}$$

$$\frac{64}{-29} / 22.7$$

3.7

$$20.1 / \frac{54}{-17}$$

$$\frac{57}{-22}$$

$$\frac{64}{-27} / 23.1$$

3.9

$$20.1 / \frac{56}{-17}$$

$$\frac{60}{-21}$$

$$\frac{67}{-28} / 23.4$$

4.1

$$22.5 / \frac{66}{-25}$$

$$\frac{67}{-24}$$

$$\frac{67}{-26} / 22.8$$

4.2

4.3

$$246 / \frac{75}{-32}$$

$$\frac{78}{-35}$$

$$\frac{74}{-31} / 243$$

4.5

$$258 / \frac{81}{-36}$$

$$\frac{79}{-34}$$

$$\frac{79}{-34} / 25.2$$

4.4

$$258 / \frac{80}{-36}$$

$$\frac{80}{-36}$$

$$\frac{80}{-36} / 25.8$$

Sta.	+	π	-	Grade
		905.46		
57				020
T.P.	1804	912.33	6.17	899.29
	+50			03.4
58				056
	+43			078
	+59			086
	+72			092
T.P.	1076	918.91	4.15	908.15
	+82			09.7
59				10.6
T.P.	832	925.71	1.52	917.39
	+35			12.4
	+68			13.8
60				14.7

Gr. Rod.

Lt.

E.

Rt.

3.5

$$264 / \begin{array}{r} 78 \\ -38 \end{array}$$

$$\begin{array}{r} 78 \\ -38 \end{array}$$

$$\begin{array}{r} 73 \\ -38 \\ \hline 264 \end{array}$$

8.7

$$270 / \begin{array}{r} 129 \\ -40 \end{array}$$

$$\begin{array}{r} 126 \\ -37 \end{array}$$

$$\begin{array}{r} 119 \\ -30 \\ \hline 240 \end{array}$$

6.7

$$264 / \begin{array}{r} 105 \\ -38 \end{array}$$

$$\begin{array}{r} 100 \\ -33 \end{array}$$

$$\begin{array}{r} 94 \\ -27 \\ \hline 231 \end{array}$$

4.5

$$213 / \begin{array}{r} 66 \\ -21 \end{array}$$

$$\begin{array}{r} 54 \\ -11 \end{array}$$

$$\begin{array}{r} 56 \\ -14 \\ \hline 263 \end{array}$$

3.7

$$235 / \begin{array}{r} 52 \\ -100 \end{array}$$

$$\begin{array}{r} 50 \\ -13 \end{array}$$

$$\begin{array}{r} 50 \\ -22 \\ \hline 291 \end{array}$$

(27) 2.1

$$201 / \begin{array}{r} 48 \\ +17 \end{array}$$

$$\begin{array}{r} 43 \\ -12 \end{array}$$

$$\begin{array}{r} +12 \\ +13 \\ \hline 300 \end{array}$$

2.2

$$325 / \begin{array}{r} 53 \\ +30 \end{array}$$

$$\begin{array}{r} 59 \\ +24 \end{array}$$

$$\begin{array}{r} 29 \\ +54 \\ \hline 300 \end{array}$$

13.3

$$307 / \begin{array}{r} 112 \\ +21 \end{array}$$

$$\begin{array}{r} 96 \\ +27 \end{array}$$

$$\begin{array}{r} 55 \\ +78 \\ \hline 300 \end{array}$$

11.9

$$301 / \begin{array}{r} 101 \\ +18 \end{array}$$

$$\begin{array}{r} 64 \\ +35 \end{array}$$

$$\begin{array}{r} 27 \\ +72 \\ \hline 300 \end{array}$$

11.0

$$343 / \begin{array}{r} 71 \\ +39 \end{array}$$

$$\begin{array}{r} 39 \\ +71 \end{array}$$

$$\begin{array}{r} 19 \\ +71 \\ \hline 300 \end{array}$$

Sta	+	π	-	Grade
		925.71		
60	+30			15.1
B.M.	2.27	925.02	7.72	922.79 922.75
	+70			13.2
61				14.7
	+50			13.2
	+80			12.1
62				11.4
	+50			09.6
T.P.	4.25	917.09	12.18	912.84
63				07.8
	+21			07.1
	+37			06.6
	+60			05.9

96
65

105

Gr. Rod.

LH

R

RH

$$10.6 \quad 389' / \begin{array}{r} 5.8 \\ +9.7 \end{array} \quad \begin{array}{r} 33 \\ +7.3 \end{array} \quad \begin{array}{r} 26 \\ +50 \end{array} / 30.0$$

Top Mark. 40+49.55

$$9.8 \quad 36.5' / \begin{array}{r} 48 \\ +50 \end{array} \quad \begin{array}{r} 32 \\ +66 \end{array} \quad \begin{array}{r} 28 \\ +70 \end{array} / 40.5'$$

$$10.3 \quad 36' / \begin{array}{r} 55 \\ +48 \end{array} \quad \begin{array}{r} 43 \\ +40 \end{array} \quad \begin{array}{r} 41 \\ +52 \end{array} / 38.9'$$

$$11.8 \quad 31.7' / \begin{array}{r} 72 \\ +26 \end{array} \quad \begin{array}{r} 85 \\ +33 \end{array} \quad \begin{array}{r} 73 \\ +75 \end{array} / 35.5'$$

$$12.9 \quad 30.7' / \begin{array}{r} 108 \\ +21 \end{array} \quad \begin{array}{r} 108 \\ +21 \end{array} \quad \begin{array}{r} 109 \\ +25 \end{array} / 31.5'$$

$$13.6 \quad 33.3' / \begin{array}{r} 102 \\ +34 \end{array} \quad \begin{array}{r} 111 \\ +25 \end{array} \quad \begin{array}{r} 112 \\ +27 \end{array} / 31.3'$$

$$15.4 \quad 39.5' / \begin{array}{r} 87 \\ +45 \end{array} \quad \begin{array}{r} 111 \\ +93 \end{array} \quad \begin{array}{r} 128 \\ +26 \end{array} / 31.7'$$

$$9.3 \quad 37.7' / \begin{array}{r} 57 \\ +56 \end{array} \quad \begin{array}{r} 51 \\ +92 \end{array} \quad \begin{array}{r} 62 \\ +31 \end{array} / 32.7'$$

$$10.0 \quad 35.3' / \begin{array}{r} 56 \\ +44 \end{array} \quad \begin{array}{r} 52 \\ +48 \end{array} \quad \begin{array}{r} 76 \\ +14 \end{array} / 29.3$$

$$10.5 \quad 35.3' / \begin{array}{r} 61 \\ +44 \end{array} \quad \begin{array}{r} 87 \\ +16 \end{array} \quad \begin{array}{r} 101 \\ +04 \end{array} / 27.3'$$

$$11.2 \quad 29.3' / \begin{array}{r} 98 \\ +14 \end{array} \quad \begin{array}{r} 113 \\ -01 \end{array} \quad \begin{array}{r} 119 \\ +08 \end{array} / 25.1$$

sta.	+	X	-	Grade	scrutings
		917.07			
64				051	
T.P.	425	908.26	1308	904.01	
+50				044	+ 0.3
65				042	+ 0.4
+50				041	+ 0.4
66				041	
+50				041	
67				041	
T.P.	10.53	913.00	579	902.47	
+50				041	+ 0.4
68				041	
+65				041	+ 0.4
69				043	
B.M.	2.69.79	912.97	269	910.31	(910.28)

Gr. Rod.

Lt.

R.

Rt.

$$120' \quad 243 \overline{) 131} \quad \begin{array}{r} 13.9 \\ -19 \\ \hline \end{array} \quad \begin{array}{r} 10.7 \\ -27 \\ \hline 23.1 \end{array}$$

$$36 \quad 22.2 \overline{) 40} \quad \begin{array}{r} 6.9 \\ -28 \\ \hline \end{array} \quad \begin{array}{r} 6.5 \\ -29 \\ \hline 23.7 \end{array}$$

$$38 \quad 261 \overline{) 37} \quad \begin{array}{r} 7.5 \\ -3.7 \\ \hline \end{array} \quad \begin{array}{r} 3.7 \\ -3.7 \\ \hline 26.1 \end{array}$$

$$38 \quad 264 \overline{) 38} \quad \begin{array}{r} 7.6 \\ -3.8 \\ \hline \end{array} \quad \begin{array}{r} 7.6 \\ -3.8 \\ \hline 26.4 \end{array}$$

$$3.8 \quad 285 \overline{) 45} \quad \begin{array}{r} 8.3 \\ -4.5 \\ \hline \end{array} \quad \begin{array}{r} 8.3 \\ -4.5 \\ \hline 28.5 \end{array}$$

$$3.8 \quad 287 \overline{) 46} \quad \begin{array}{r} 8.3 \\ -4.5 \\ \hline \end{array} \quad \begin{array}{r} 8.3 \\ -4.5 \\ \hline 28.5 \end{array}$$

$$3.8 \quad 274 \overline{) 42} \quad \begin{array}{r} 8.0 \\ -4.2 \\ \hline \end{array} \quad \begin{array}{r} 8.0 \\ -4.2 \\ \hline 27.6 \end{array}$$

$$3.5 \quad 285 \overline{) 45} \quad \begin{array}{r} 1.0 \\ -4.5 \\ \hline \end{array} \quad \begin{array}{r} 1.0 \\ -4.5 \\ \hline 28.5 \end{array}$$

$$3.5 \quad 267 \overline{) 39} \quad \begin{array}{r} 1.7 \\ -3.9 \\ \hline \end{array} \quad \begin{array}{r} 1.7 \\ -3.9 \\ \hline 26.6 \end{array}$$

$$3.5 \quad 228 \overline{) 41} \quad \begin{array}{r} 1.1 \\ -2.6 \\ \hline \end{array} \quad \begin{array}{r} 1.2 \\ -2.7 \\ \hline 23.1 \end{array}$$

$$3.7 \quad 245 \overline{) 80.5} \quad \begin{array}{r} 9.9 \\ -12 \\ \hline \end{array} \quad \begin{array}{r} 9.9 \\ -23 \\ \hline 24.1 \end{array}$$

spk in 6" Pap 35' Lt. 69+55

Sta	+	Σ	-	Grade
		912.97		
69	+55			021
	+79			057
I.P.	11.02	922.65	1.34	911.63
6	+90			060
70				062
	+25			070
	+55			081
71				096
	+50			110
72				120
	+60			128
73				132

Cor Rod.

L

K

Rt.

6.7

$$27.1 / \frac{46}{10.3}$$

$$\frac{57}{+1.2}$$

$$\frac{52}{+1.7/29.9}$$

6.3

$$29.3 / \frac{49}{+1.4}$$

$$\frac{27}{+3.6}$$

$$\frac{107}{170/10.5}$$

16.5

$$41.9 / \frac{8.7}{+1.7}$$

$$\frac{27}{+8.8}$$

$$\frac{79}{171/44.7}$$

15.7

$$46.9 / \frac{55}{+10.2}$$

$$\frac{47}{+1.0}$$

$$\frac{40}{111.7/49.9}$$

14.6

$$47.3 / \frac{4.2}{+10.4}$$

$$\frac{33}{+11.3}$$

$$\frac{24}{+12.2/50.9}$$

13.1

$$39.3 / \frac{6.7}{+6.4}$$

$$\frac{5.1}{+8.0}$$

$$\frac{25}{100/47.7}$$

11.7

$$29.9 / \frac{10.0}{+1.7}$$

$$\frac{88}{+2.7}$$

$$\frac{53}{16.4/57.5}$$

10.7

$$26.1 / \frac{11.7}{+1.3}$$

$$\frac{10.7}{-0.2}$$

$$\frac{9.0}{+1.7/29.9}$$

7.9

$$24.6 / \frac{13.1}{-3.2}$$

$$\frac{12.1}{-2.2}$$

$$\frac{11.5}{-1.6/19.8}$$

7.5

$$25.8 / \frac{13.1}{-3.6}$$

$$\frac{11.6}{-2.1}$$

$$\frac{11.0}{100/23.5}$$

Sta.	+	X	-	Grade
		922.65		
73	+50			13.7
I.P.	3.46	920.21	5.90	916.75
74				14.2
	+20			14.4
	+50			14.7
75				15.2
	+44			15.8
	+61			16.2
76				17.2
+32	$\frac{909.2}{39}$	Center Box	$\frac{910.5}{39}$	18.3
+80				20.3
77				21.2
I.P.	5.36	927.68	0.89	919.32

Gr. Road

Lk

R

Pt.

2.0

$$22.7 / \frac{11.9}{-2.9}$$

$$\frac{9.8}{-0.3}$$

$$\frac{4.1}{+2.9/32.5'}$$

4.0

$$22.3 / \frac{7.5}{-4.0}$$

$$\frac{4.5}{+1.5}$$

$$\frac{1.8}{+2.2/34.9'}$$

5.8

$$22.4 / \frac{7.8}{-4.0}$$

$$\frac{4.3}{+1.5}$$

$$\frac{1.5}{+2.3/35.1'}$$

5.5

$$22.1 / \frac{8.2}{-2.7}$$

$$\frac{5.8}{+1.1}$$

$$\frac{3.1}{+2.4/31.3'}$$

5.0

$$22.9 / \frac{8.3}{-3.3}$$

$$\frac{6.4}{-1.4}$$

$$\frac{5.2}{+1.3/26.1'}$$

4.4

$$31.5 / \frac{9.9}{-5.5}$$

$$\frac{7.4}{-2.0}$$

$$\frac{6.7}{-2.3/21.7'}$$

4.0

$$35.4 / \frac{10.8}{-6.8}$$

$$\frac{7.1}{-5.1}$$

$$\frac{7.1}{-5.1/24.3'}$$

3.0

$$40.2 / \frac{11.4}{-8.4}$$

$$\frac{11.0}{-8.0}$$

$$\frac{9.5}{-6.5/24.5'}$$

1.9

$$43.8 / \frac{11.5}{-9.6}$$

$$\frac{11.3}{-9.4}$$

$$\frac{10.5}{-8.6/20.8'}$$

10.1

$$42.7 / \frac{10.8}{-1.9}$$

$$\frac{10.3}{-10.4}$$

$$\frac{8.7}{-8.8/41.4'}$$

11.0

$$48.9 / \frac{10.3}{-11.3}$$

$$\frac{8.2}{-9.2}$$

$$\frac{7.1}{-8.1/37.3'}$$

sta. + π - Grands

927.68

77 +95 22.2

+70 24.2

78 25.1

+35 26.0

+53 26.3

+57 26.3

+60 26.4

+71 26.5

+89.65 26.7

B.M. 0.97 726.71

926.72

Gr. Bed

Lt

R

Rt

$$\frac{4.5}{10.1}$$

9.5

$$41.1 / \frac{15.2}{-2.7}$$

$$\frac{103}{-58}$$

$$\frac{9.7}{-5.2/30.6}$$

3.5

$$37.2 / \frac{10.9}{-7.4}$$

$$\frac{9.7}{-4.2}$$

$$\frac{8.5}{-5.0/30.0}$$

2.6

$$38.1 / \frac{10.8}{-7.7}$$

$$\frac{8.5}{-5.7}$$

$$\frac{8.0}{-5.7/31.2}$$

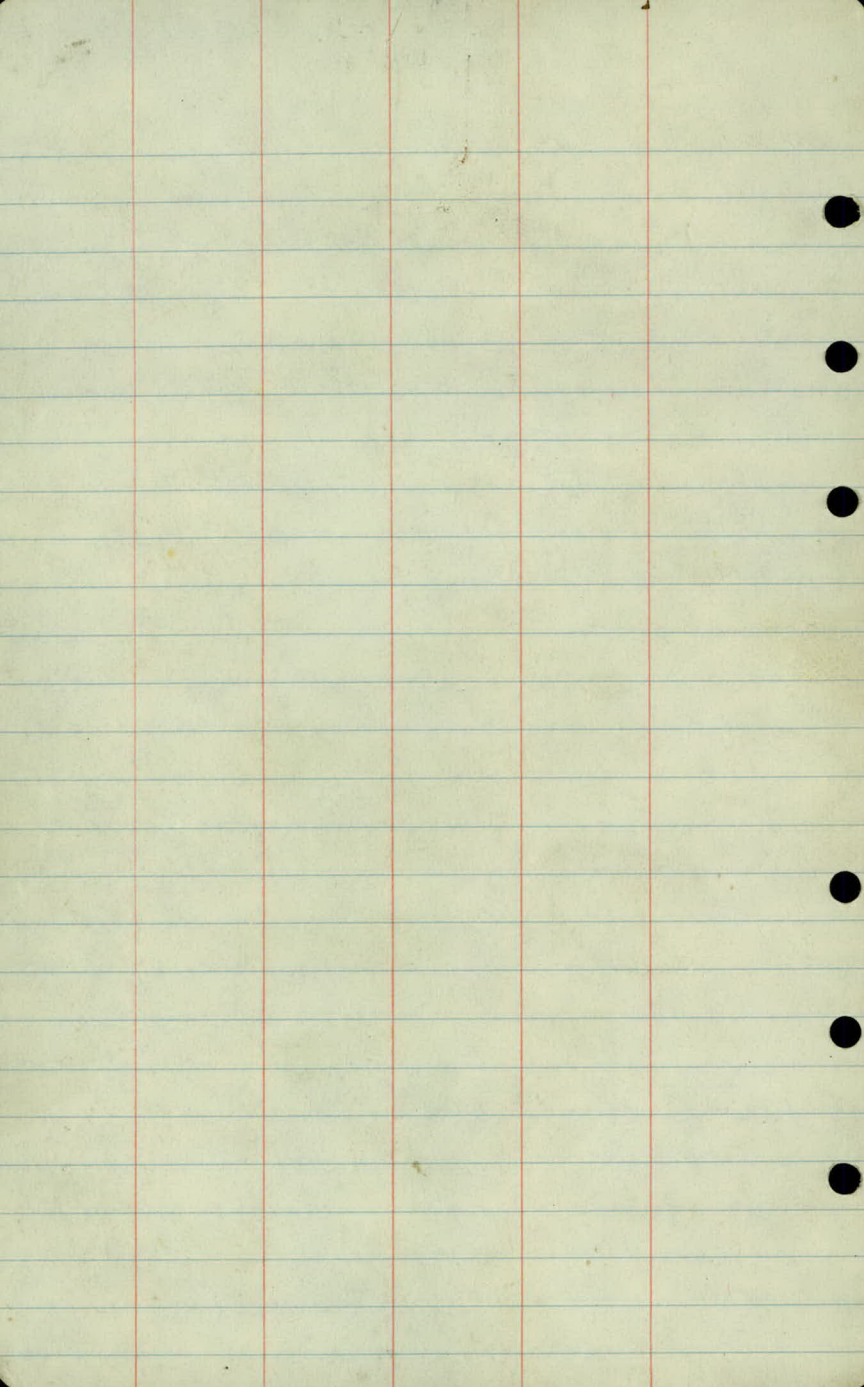
1.7

$$36.6 / \frac{7.1}{-7.2}$$

$$\frac{6.8}{-5.7}$$

$$\frac{6.5}{-1.7/25.4}$$

Top Mont. 78+84.65



Align

Drainage Co Rd Cr

Index	Pages	3-5-43
Align	1 to 3	HAW
X Section	3 to 7	AM
Topog	7 to 9	LC
		C.F
		LL

Noted

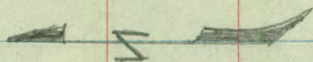
Sta Pt ΔLt ΔRt.

11+00 P.O.T

5+72³⁰ P.O.T

0+00 P.O.T

Description



2"x2" Hub

21'

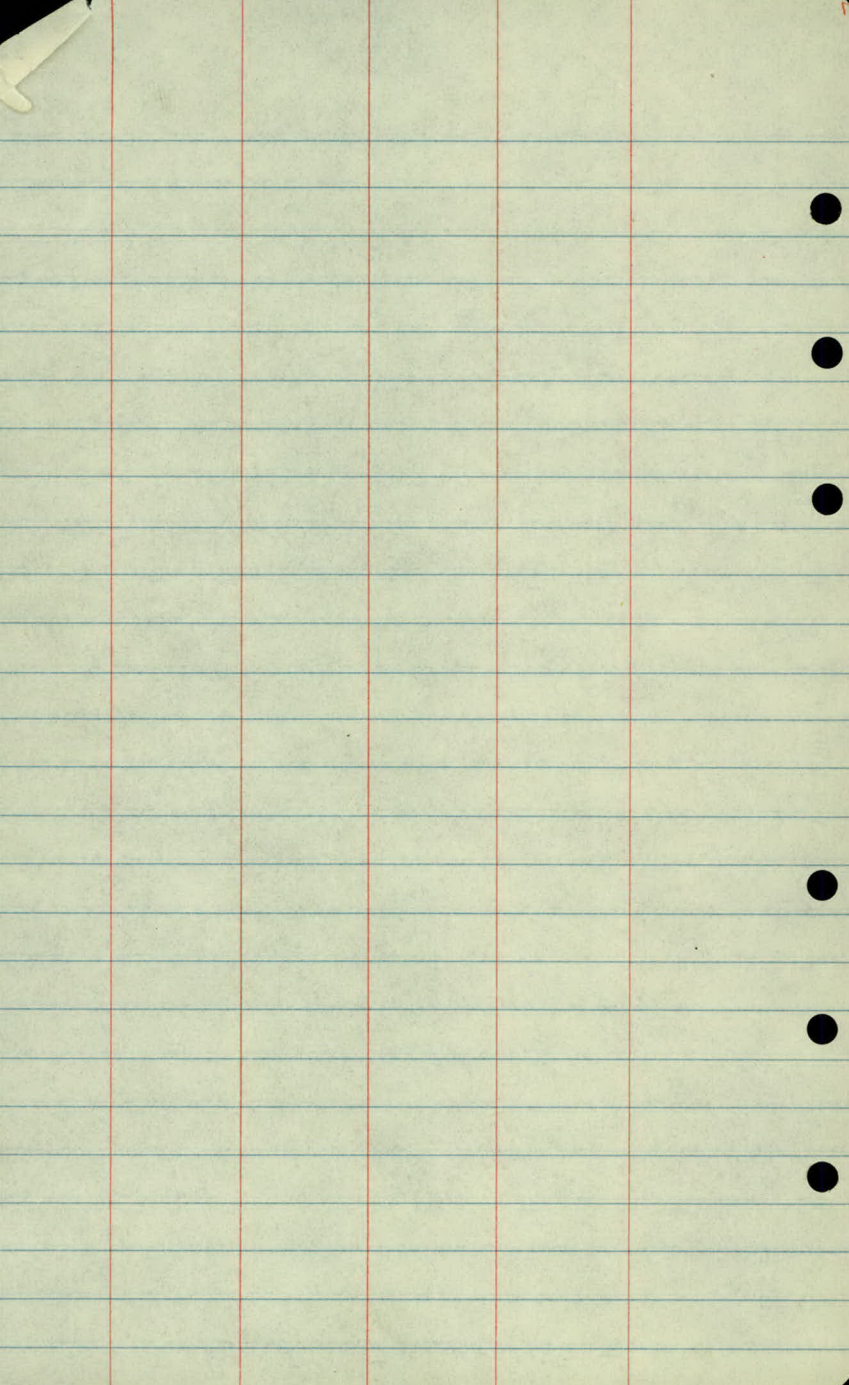
ACES 5004
E 1/4 NW 1/4 Sec 4
Co Rd 22

Drill hole over
36" CM. Culv

21'

265'43'

West 1/4 Sec 4



X sections

Drainage Co Rd "C"

Sta	+	Δ	-	Elev
B.M	3.64	906.98		903.34
0+00				00.2
+50				99.3
1				99.1
+50				98.8
2				01.0
+50				01.7
T.P	11.38	916.28	2.08	904.90
3				04.3
+50				07.6
+67				08.7
+75				09.0
4				09.5
B.M	6.86	921.97	1.17	915.11
+50				11.9

Lt K R1

Spk in PP S.F. Cor Cleve + "02"

97.1 → $\frac{99}{33}$ $\frac{99}{3}$ 68 $\frac{5.3}{6}$ $\frac{5.0}{21}$ $\frac{5.3}{37}$

97.0

$\frac{10.0}{21}$ $\frac{9.7}{8}$ $\frac{8.3}{3}$ 77 $\frac{5.4}{6}$ $\frac{5.2}{21}$ $\frac{5.6}{35}$

96.8

$\frac{10.2}{28}$ $\frac{9.9}{8}$ 77 $\frac{5.7}{6}$ $\frac{5.3}{21}$ $\frac{5.5}{35}$

97.2

$\frac{9.8}{24}$ $\frac{9.0}{5}$ 82 $\frac{5.3}{6}$ $\frac{4.9}{21}$ $\frac{4.7}{28}$ $\frac{4.8}{36}$

99.5

$\frac{8.5}{31}$ $\frac{8.6}{8}$ 60 $\frac{4.0}{6}$ $\frac{3.4}{17}$ $\frac{3.3}{27}$ $\frac{4.0}{36}$

99.8

$\frac{7.2}{25}$ $\frac{6.2}{10}$ $\frac{5.4}{3}$ 5.3 $\frac{2.6}{6}$ $\frac{1.9}{18}$ $\frac{1.9}{29}$ $\frac{2.4}{36}$

02.2

$\frac{14.1}{26}$ $\frac{13.5}{7}$ 120 $\frac{10.0}{6}$ $\frac{9.5}{20}$ $\frac{9.6}{30}$ $\frac{9.7}{36}$

07.0

$\frac{9.3}{23}$ $\frac{9.0}{10}$ 8.7 $\frac{7.9}{6}$ $\frac{7.6}{18}$ $\frac{7.5}{30}$ $\frac{7.7}{36}$

08.2

$\frac{8.1}{25}$ $\frac{8.1}{7}$ 7.6 $\frac{7.2}{6}$ $\frac{6.8}{18}$ $\frac{6.7}{26}$ $\frac{7.0}{37}$

08.9

$\frac{3.0}{24}$ $\frac{3.6}{12}$ $\frac{7.4}{3}$ $\frac{7.4}{4}$ 43 $\frac{6.7}{6}$ $\frac{6.5}{22}$ $\frac{6.7}{35}$

$\frac{1.2}{27}$ $\frac{2.6}{11}$ $\frac{6.3}{4}$ 68 $\frac{5.7}{4}$ $\frac{5.3}{20}$ $\frac{5.7}{35}$

Spk in Twin Oak 26.41 sta 3+95

$\frac{6.9}{24}$ $\frac{4.5}{10}$ $\frac{10.0}{3}$ 101 $\frac{9.7}{4}$ $\frac{9.2}{12}$ $\frac{9.1}{24}$ $\frac{9.2}{33}$

Sta	+	π	-	Elev
		921.97		
5				12.7 .
+50				13.6 .
6				12.4 .
+50				11.2 .
7				09.5 .
+50				07.3 .
T.P	5.27	914.28	12.96	909.01
8				06.4 .
+50				04.8 .
9				03.8 .
+50				03.1 .
10				02.4 .
11				03.3 .

Lt

✱

Rt

$$\frac{44}{28} \quad \frac{33}{14} \quad \frac{73}{3} \quad 9.3 \quad \frac{73}{3} \quad \frac{86}{5} \quad \frac{82}{13} \quad \frac{81}{22}$$

$$\frac{31}{25} \quad \frac{1.8}{14} \quad \frac{8.4}{3} \quad 8.4 \quad \frac{8.5}{5} \quad \frac{8.1}{15} \quad \frac{8.1}{25} \quad \frac{8.4}{33}$$

$$\frac{46}{25} \quad \frac{40}{14} \quad \frac{9.6}{3} \quad 9.6 \quad \frac{9.6}{3} \quad \frac{8.7}{6} \quad \frac{8.5}{23} \quad \frac{8.5}{33}$$

$$\frac{7.2}{25} \quad \frac{7.5}{9} \quad \frac{10.9}{3} \quad 10.8 \quad \frac{10.1}{6} \quad \frac{9.8}{18} \quad \frac{10.0}{26}$$

$$\frac{6.5}{25} \quad \frac{6.7}{15} \quad \frac{12.5}{3} \quad 12.5 \quad \frac{12.5}{3} \quad \frac{11.7}{6} \quad \frac{11.1}{22} \quad \frac{11.4}{35}$$

$$\frac{6.7}{25} \quad \frac{7.2}{16} \quad \frac{14.1}{3} \quad 14.7 \quad \frac{14.7}{3} \quad \frac{13.2}{6} \quad \frac{12.9}{22} \quad \frac{13.2}{35}$$

$$\frac{1.9}{25} \quad \frac{2.4}{16} \quad \frac{7.9}{3} \quad 7.9 \quad \frac{7.9}{3} \quad \frac{7.1}{5} \quad \frac{6.7}{20} \quad \frac{7.0}{34}$$

$$\frac{7.0}{19} \quad \frac{7.8}{7} \quad \frac{7.3}{3} \quad 9.5 \quad \frac{8.5}{3} \quad \frac{8.0}{20} \quad \frac{8.5}{34}$$

$$\frac{10.6}{16} \quad 10.5 \quad \frac{10.0}{3} \quad \frac{8.8}{6} \quad \frac{8.4}{20} \quad \frac{8.8}{24}$$

901.9 → Low Spot

$$\frac{12.4}{26} \quad 11.2$$

906.57

→ 77.1

→ W.S

3/5/43

$$\frac{13.4}{26} \quad 11.9$$

Low spot
14.0

900.3

11.0

900.6

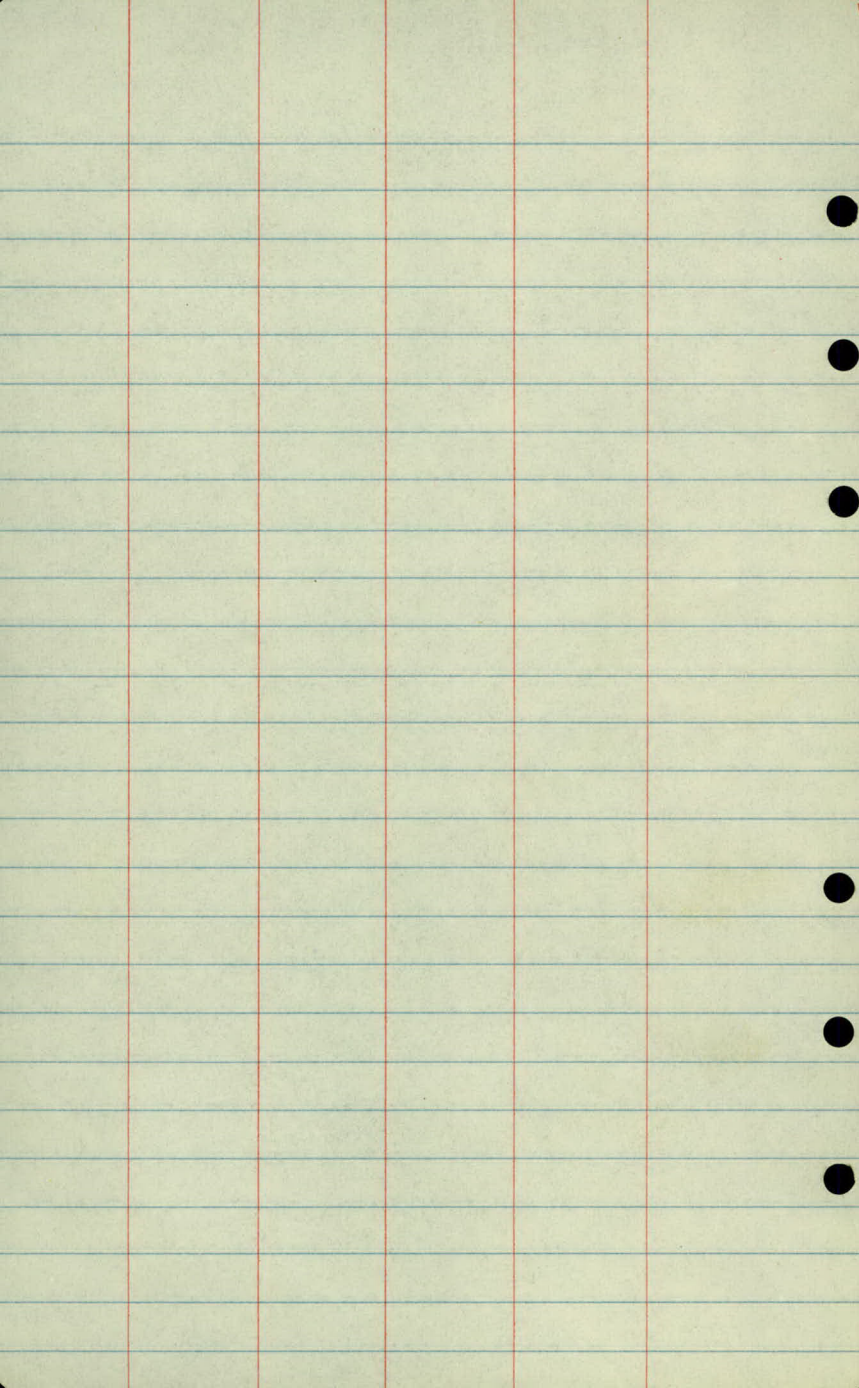
Low spot

13.7

Sta	+	π	-	Elev
		914.28		
T.P	1.21	914.59	0.90	913.38
	2.66	906.73	10.52	904.07
B.M			3.41	903.32 903.34

2

SpK in Arc Lt Polc S.E. Cor Cleve YB²



Topography

Co Rd "C²"

From 255' E. of Cleva to 1100' East.

6

+40 * Ent.

5

4

3

2

1

0

Rd 5' & 35'

Cultivated

Rd 5' & 35'

+100 End Woods 17

Rd 5' & 35'

1000
1000
1000

+150 Beg Woods 14' & 200'

Rd 5' & 35'

+50 End Lake 13' & 250'

Lake 9'

Rd 5' & 35'

Lake 9'

Lake Wilson

Rd 5' & 35'

+100 End 36" Culv 3'

(36" x 48" CM)

Rd 6' & 39'
+100 End 36" Culv
45

11

10

9

8

100 Edge Water hole

7

6

