

D11-R33

Dr. 11 - Bk. 33

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

FOLWELL AVE. BURTON ST. & HOYT AVE.

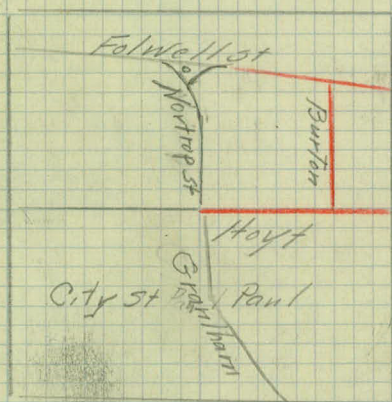
From UNIVERSITY & GROVE

Road Acc't. No. R-53-R-52-R44

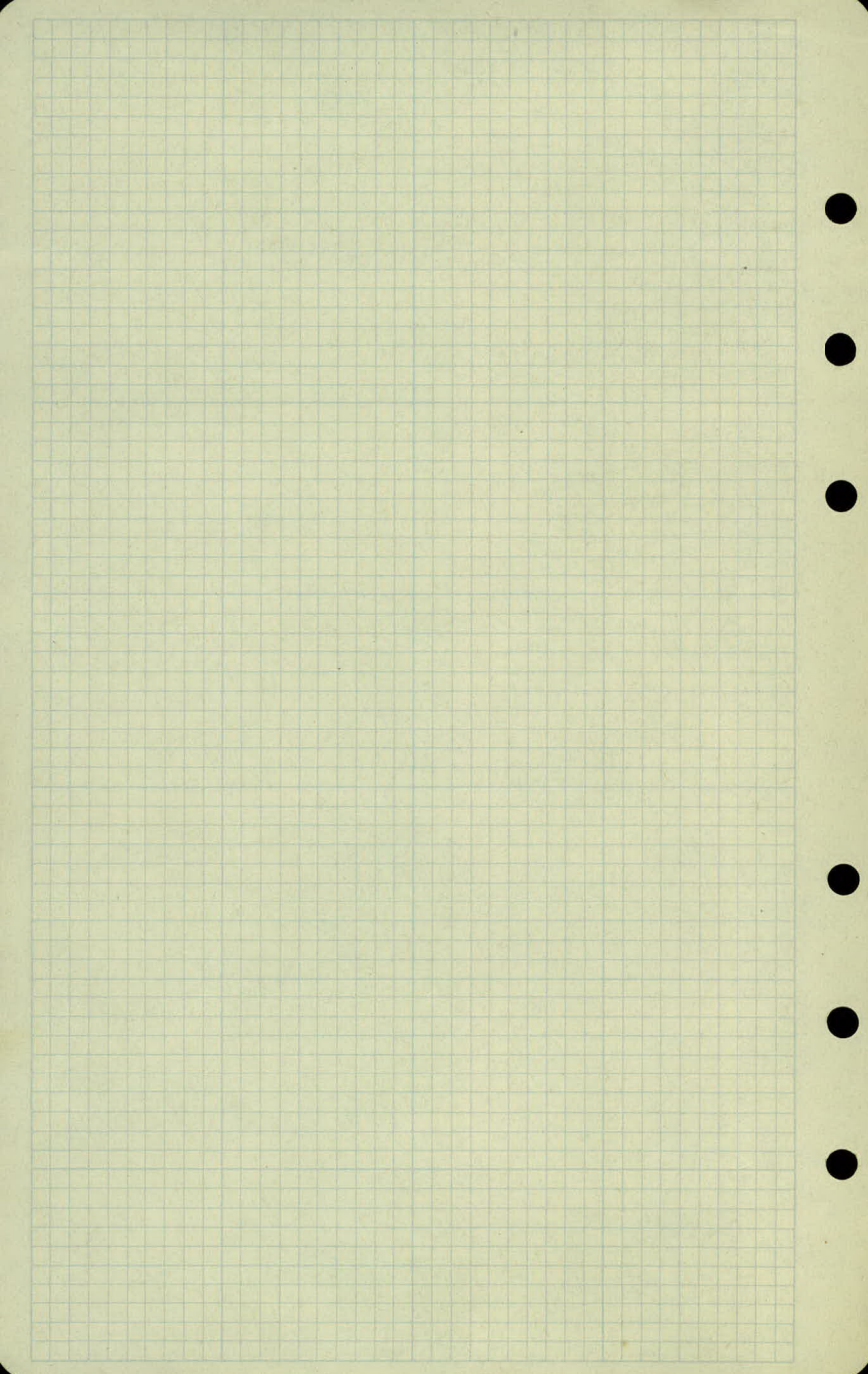
Date Filed 12-28-38

File

Streets In University Grove Folwell - Burton - Hoyt



Index	Pages
Alignment	1 to 10
Topog.	11 to 18
X Sections	18 to 27



Alignment
University Grove

Hoyt Ave
Burton St
Felwell St

Sta

$\Delta-Lt$ $\Delta-Rt$

4+98.93

P.I.

$90^{\circ}28'$

End Project

3+48.86 = P.I. $90^{\circ}00'$

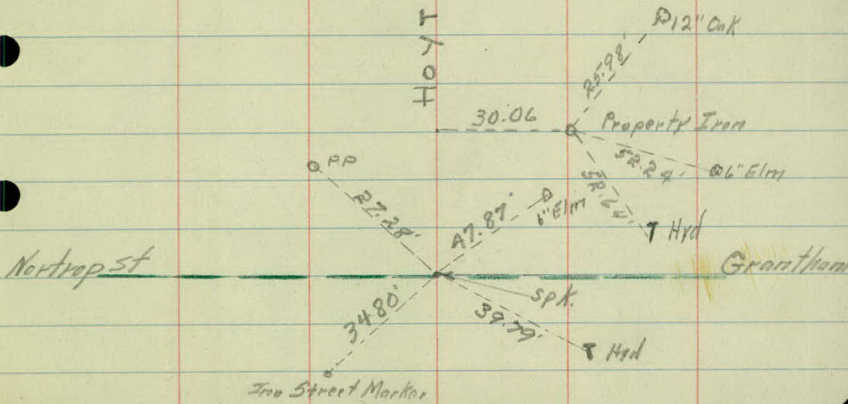
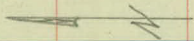
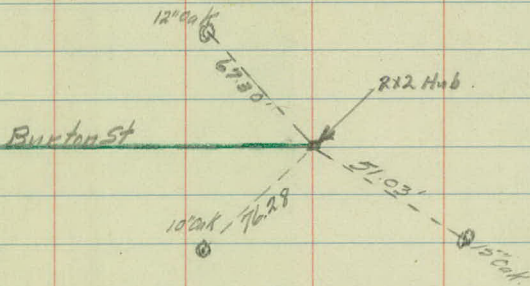
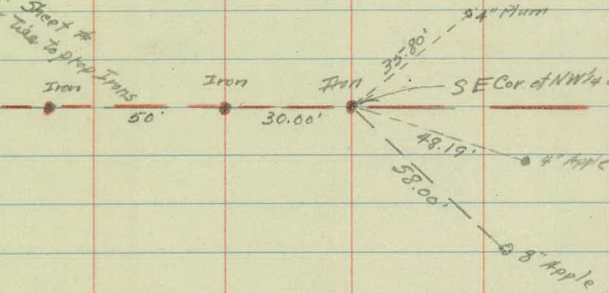
0+00 Δ Burton St

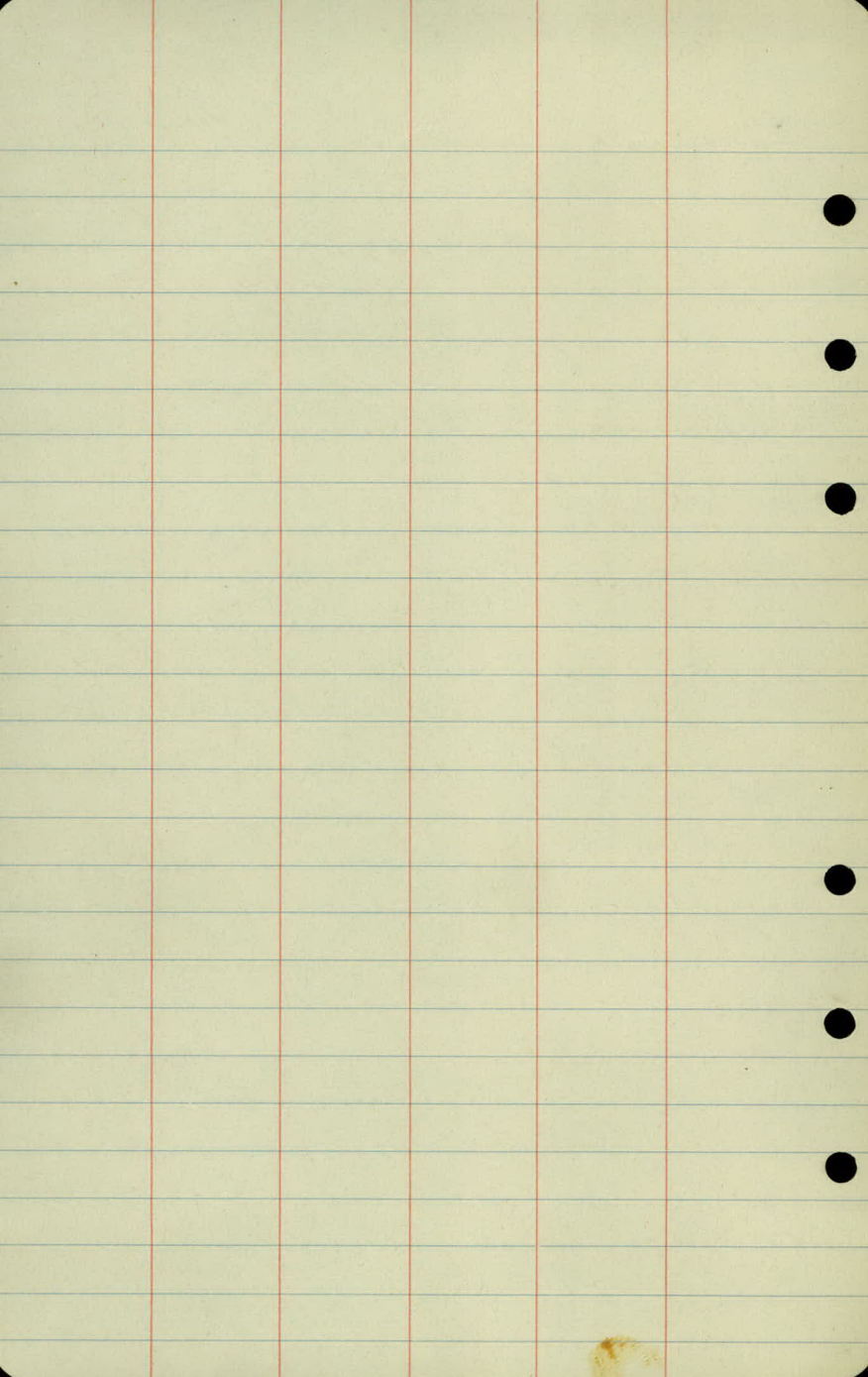
0+00

P.I.

$90^{\circ}00'$

See Sheet #
For Lake to prop. Irons





Alignement

Burton St.

Sta

$\Delta-Lt$ $\Delta-Rt$

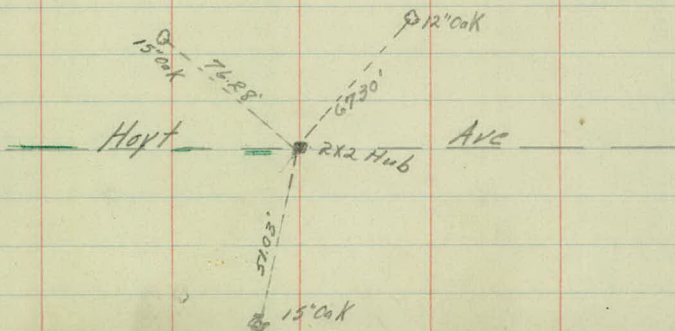
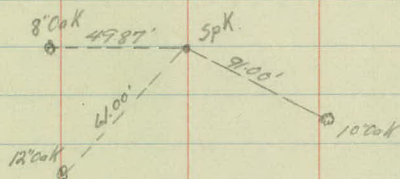
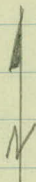
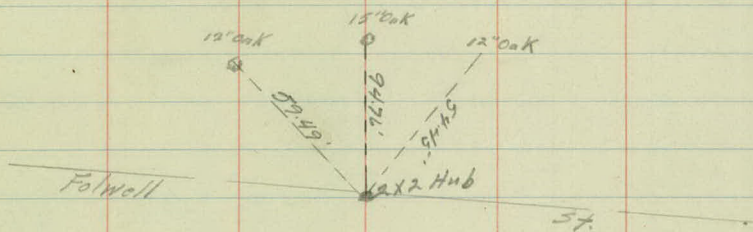
$4+96.84 =$ P.I. $86^{\circ}03'$

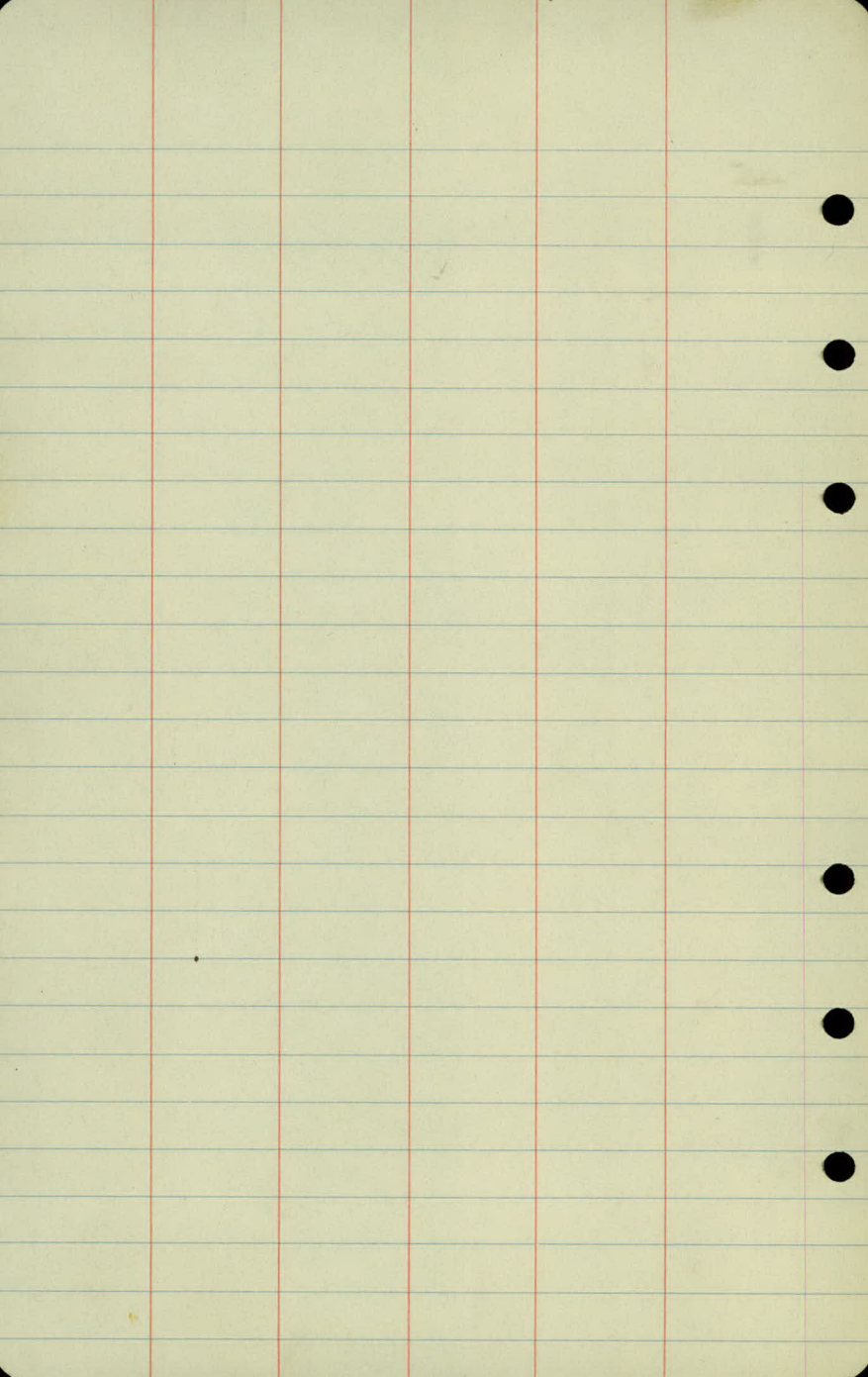
$4+47.59$ Folwe/1st

$2+72.65$ P.O.T

$0+00 =$ P.I.

$3+48.86$ Hoyt Ave





Alignment

Folwell St

Sta

Δ -Lt

Δ Rt

2+10.16

P.I

$0^{\circ}31'$

1+00

P.I

$0^{\circ}41'$

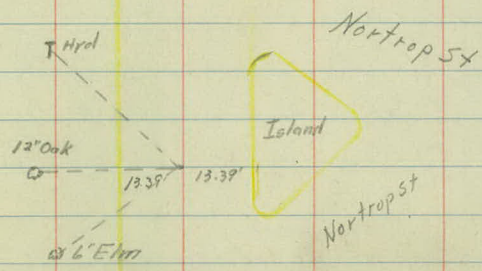
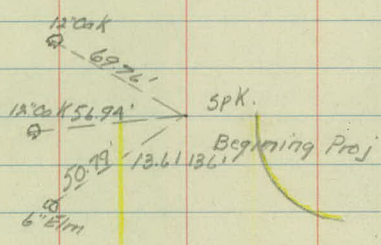
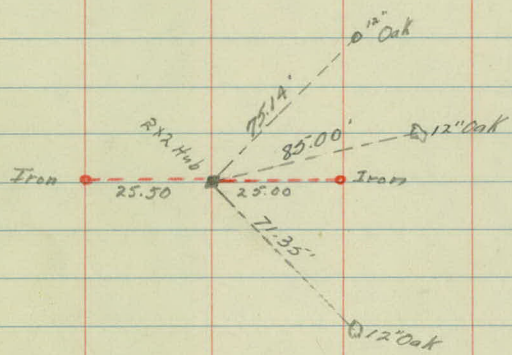
Est by splitting Imp

0+00

P.O.T.

Est. by using Present Imp.

See Sheet #7
For Ties to Irons



Sta

$\Delta-Lt$ $\Delta-Rt$

6+01.85

P.I

93°28'

Encl Project

4+47.59=

P.I

86°03'

4+96.84

2+91.80

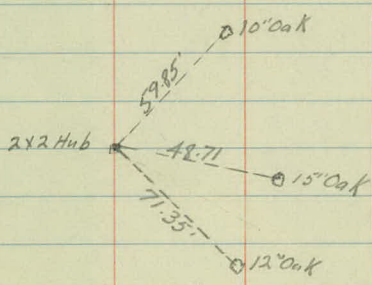
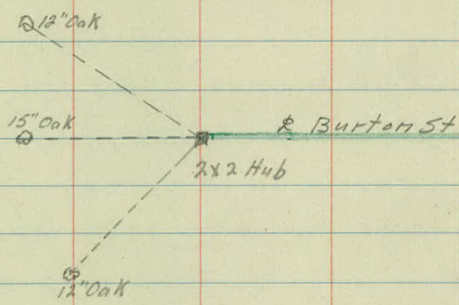
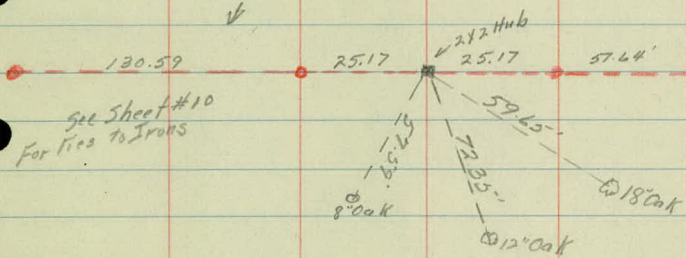
P.I

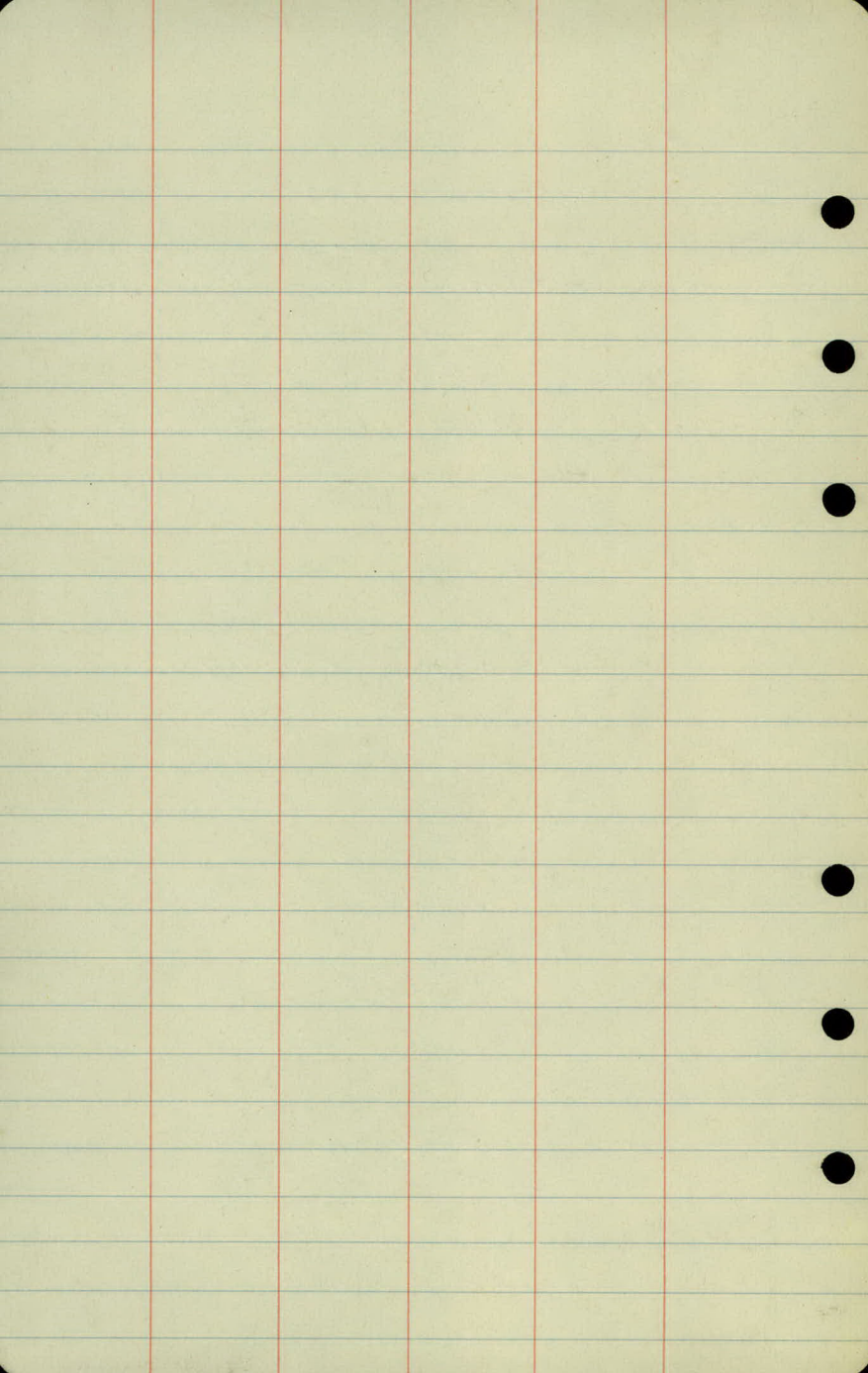
4°58'

East Line of NW 1/4 of NE 1/4 Sec 20

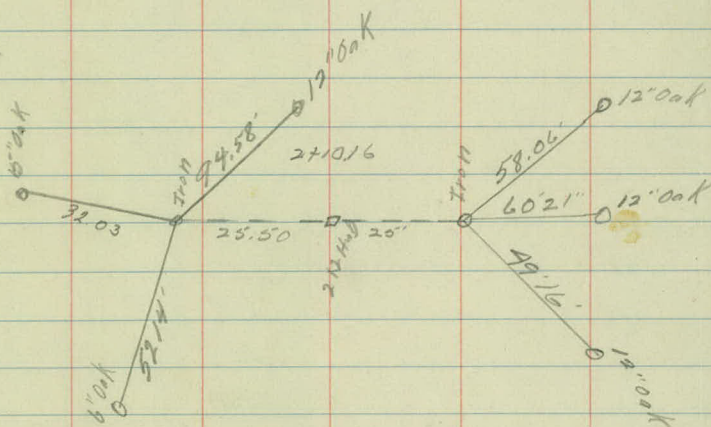


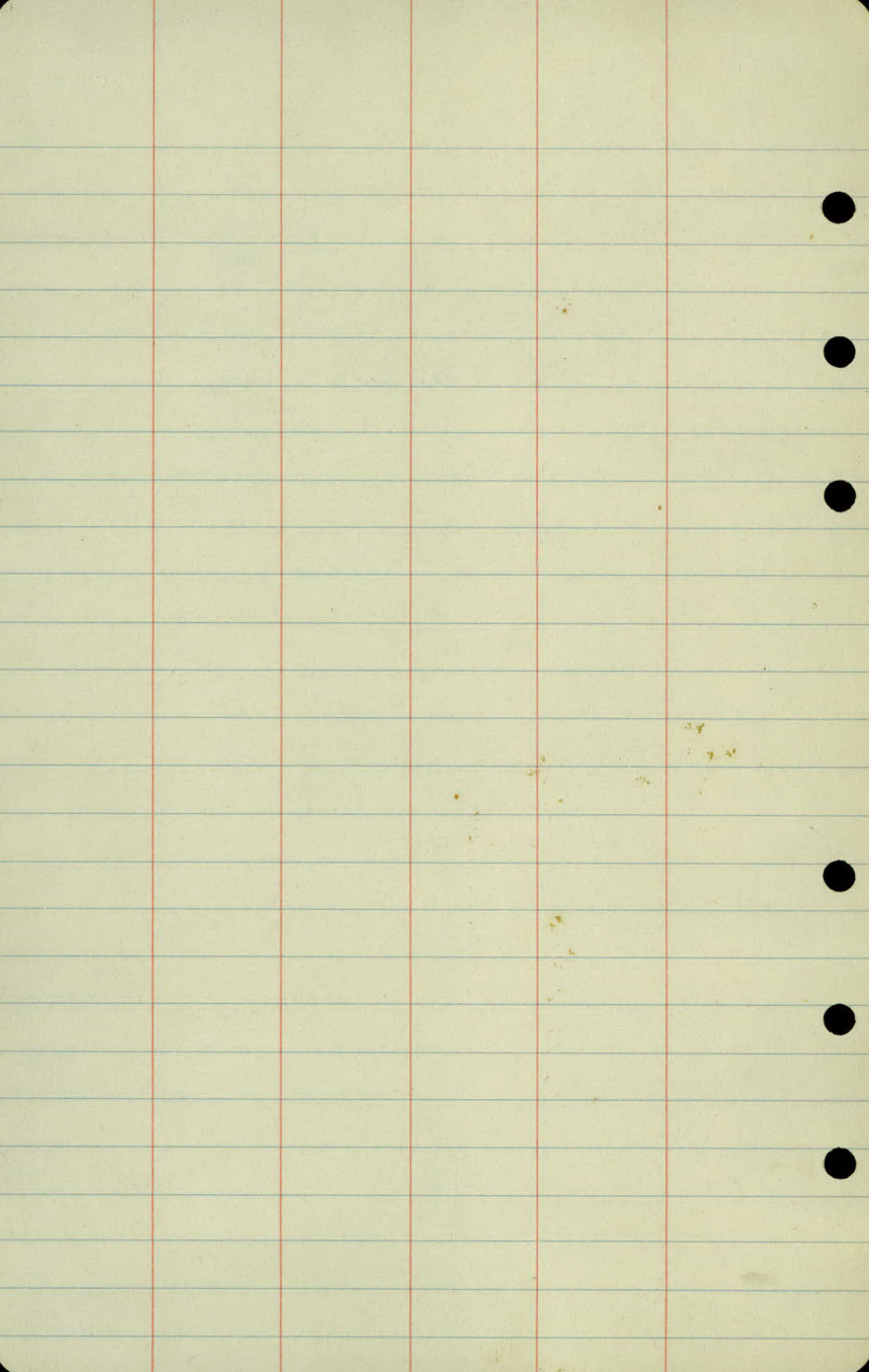
See Sheet #10
For Ties to Irons





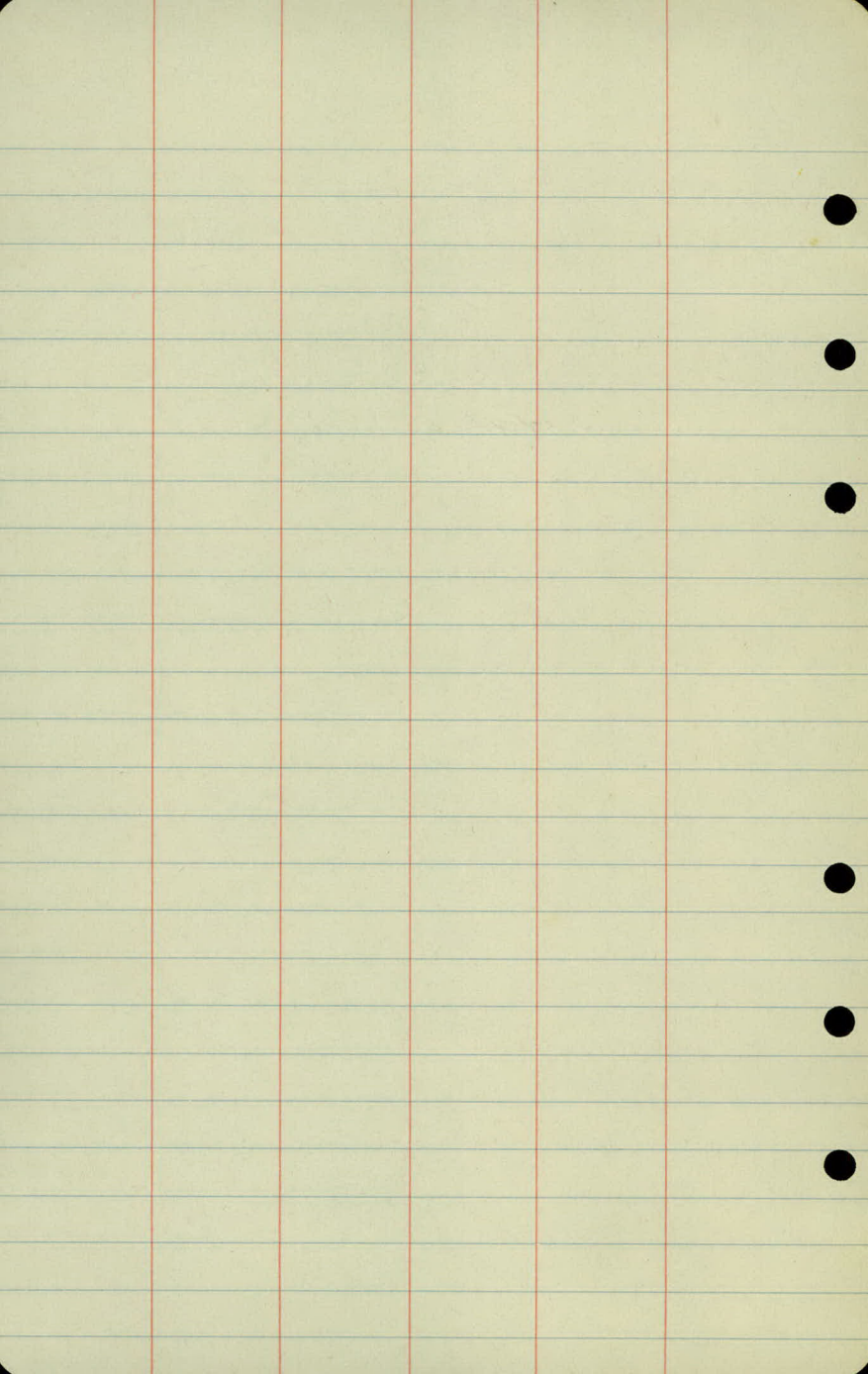
Ties to Irons Est. P.I Sta
2+10.16 Folwell St

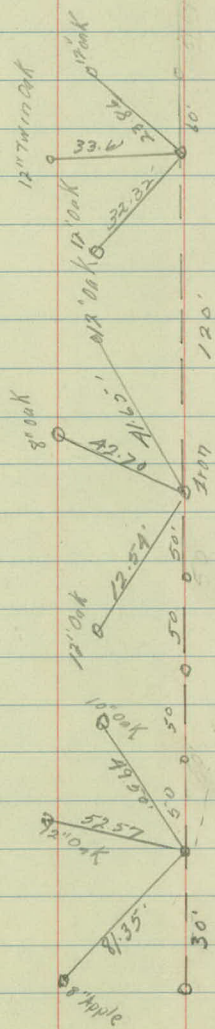




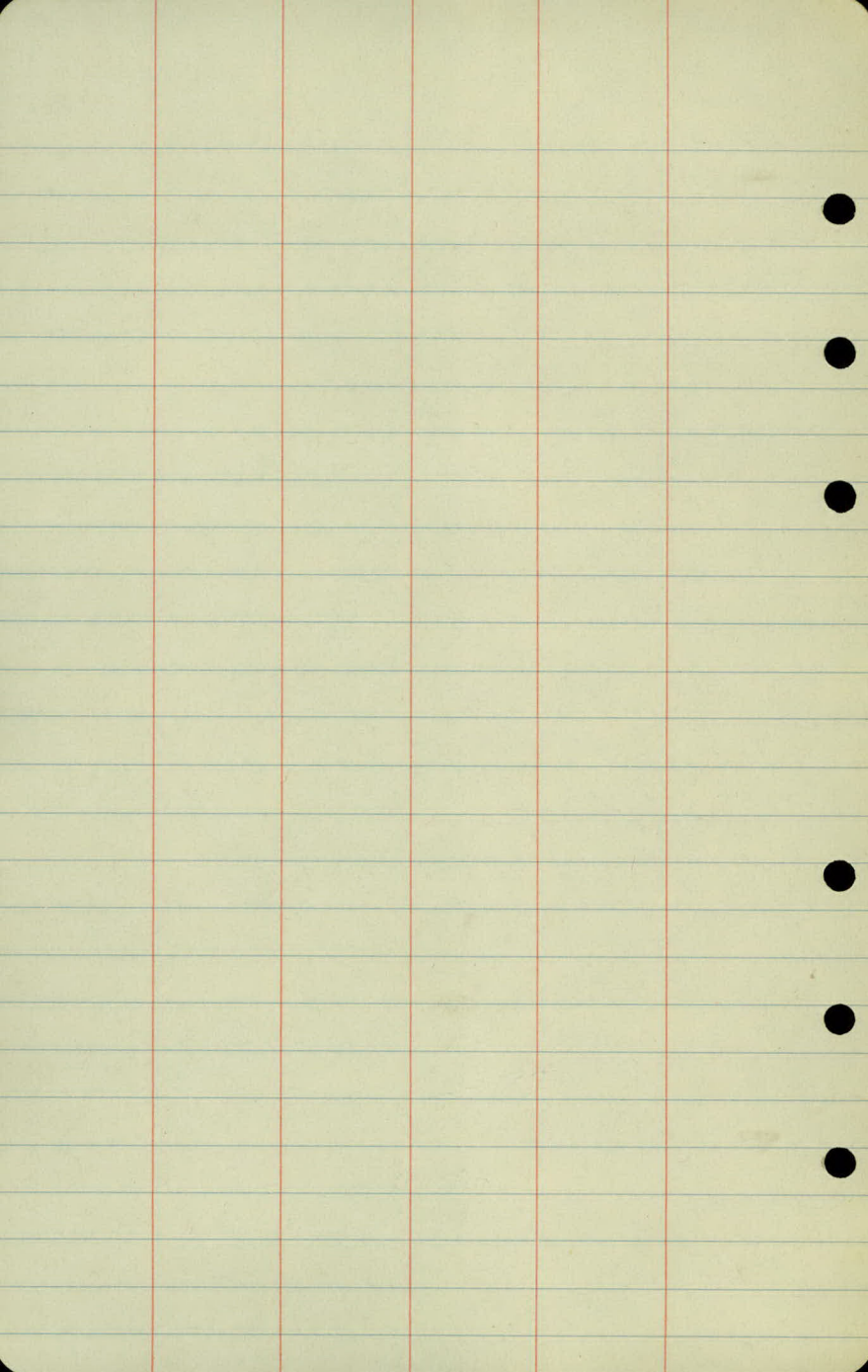
Ties to Trans

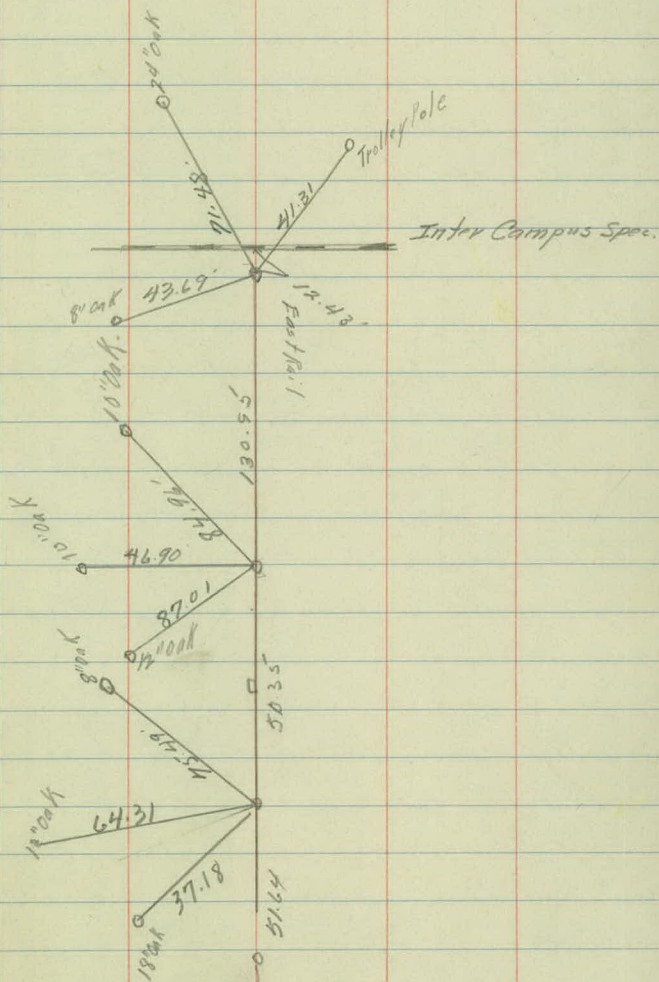
Eline of NW $\frac{1}{4}$ of NE $\frac{1}{4}$ Sec 20

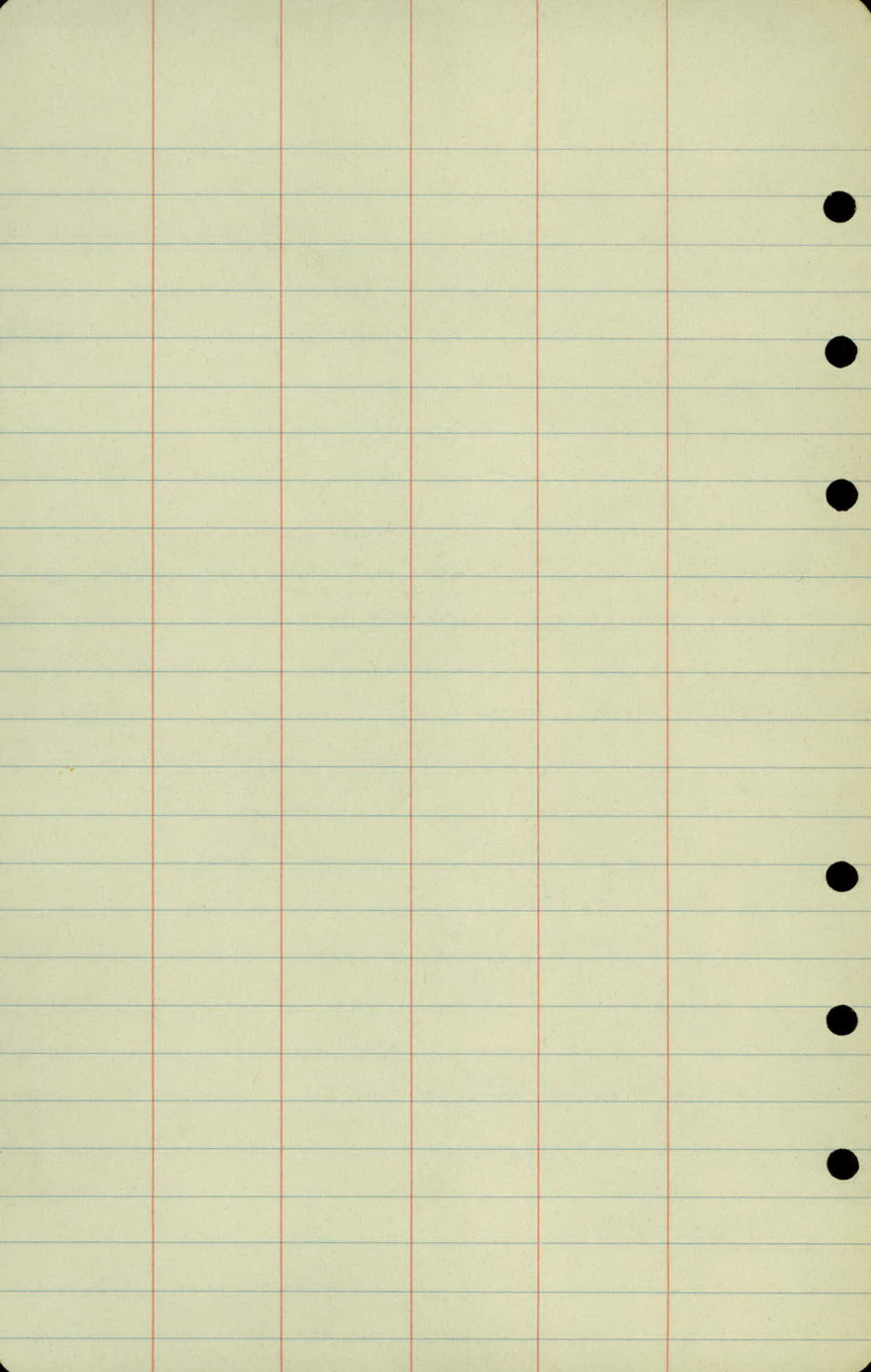




E Line $SE\frac{1}{4}$ of $NW\frac{1}{4}$ of $NE\frac{1}{4}$ sec 20







Topog
Hoyt St

5+00

+97 $\frac{P.P.}{24'}$

+99 $\frac{T.P.}{28'}$

+98 $\frac{\text{Small Fruit Trees}}{19'}$

+37 $\frac{6" Pop}{35'}$

+37 Orchard

+04 $\frac{6" Pop}{34'}$

+00 $\frac{6" Pop}{33'}$

+90 End Grading

+88 $\frac{10" Willow}{33'}$

4+00

+73 $\frac{P.P.}{23'}$

+20 $\frac{\text{End Oaks}}{40'}$

3+00

$\frac{Rd.}{7-4'}$

+75 $\frac{P.P.}{23'}$

+90 $\frac{\text{Shrub}}{28'}$

+20 $\frac{\text{Big Oaks}}{40'}$

+11 $\frac{\text{Row Fruit Trees}}{33'}$

2+00

$\frac{Rd.}{0-14'}$

+75 $\frac{P.P.}{22'5''}$

+05 $\frac{T.P.}{23'}$

+97 Alley

+87 $\frac{\text{End Wall}}{31'}$

+42 $\frac{\text{Big Rubble Wall}}{30.5'}$

1+00

$\frac{Rd.}{5-14'}$

+16 $\frac{6" Elm}{45'}$

+33 $\frac{\text{Big Yard}}{30'}$

+285 $\frac{\text{End Rd.}}{15'}$

+16 $\frac{P.P.}{16'}$

+24 $\frac{8" Elm}{42'}$

0+00

+14 $\frac{\text{Big Rd.}}{29.5'}$

+14 End 13 Top

+00 $\frac{M.H.}{33'}$

Note Curb is
2' Combination Curb
+ Gutter

Note M.H. has
Future opening
For Sewer On Hoyt St
Dead Ends Now

Cultivated

Yards

Scattered Oaks

Paul Trees

Yards

Gardens

Burton St

Scattered Oaks

overgrown with
Ragwort

Tree line 33'

10x14 shed

Scattered Oaks

15' Alley

Orchard
+ Garden

City of St Paul

Yard

Boulevard

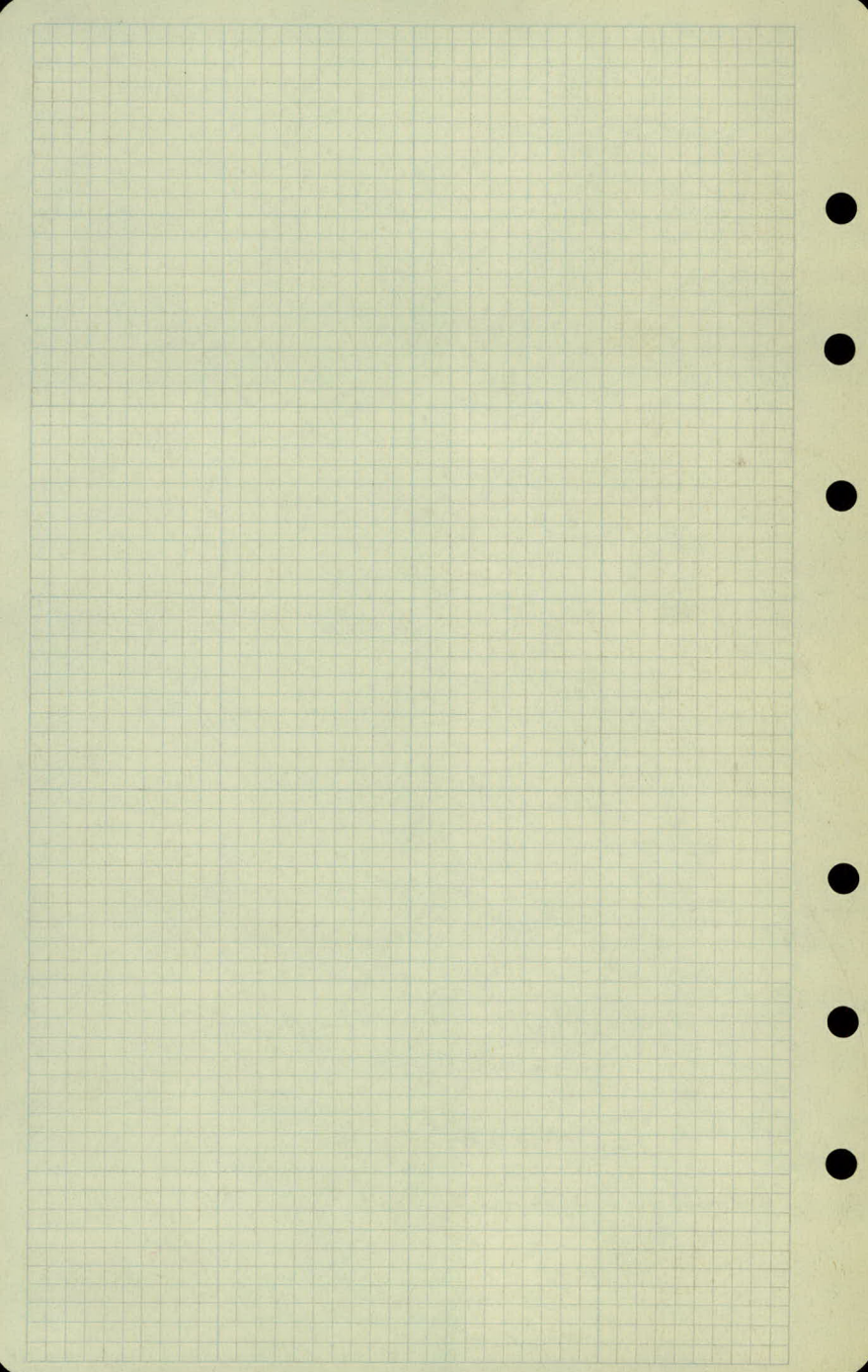
Black Top

5 1/2' Concrete

Granham St
Black Top

5.5' Concrete

Black Top



Topog
Burton ST.

5

4

3

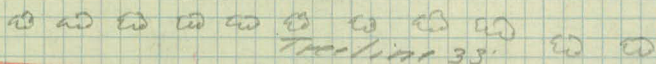
2

1

0+00 +40 $\frac{4\text{yd}}{16'}$

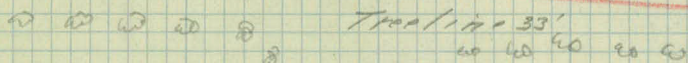
+43 Barricade
25'-25" 4" Iron Posts + 2"x10" Plank

Oaks



Tree line 33'

Folwell St



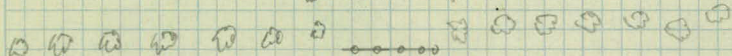
Tree line 33'

Scattered Oaks

Row overgrown with Poplar Brush

Tree line 33'

Scattered Oaks

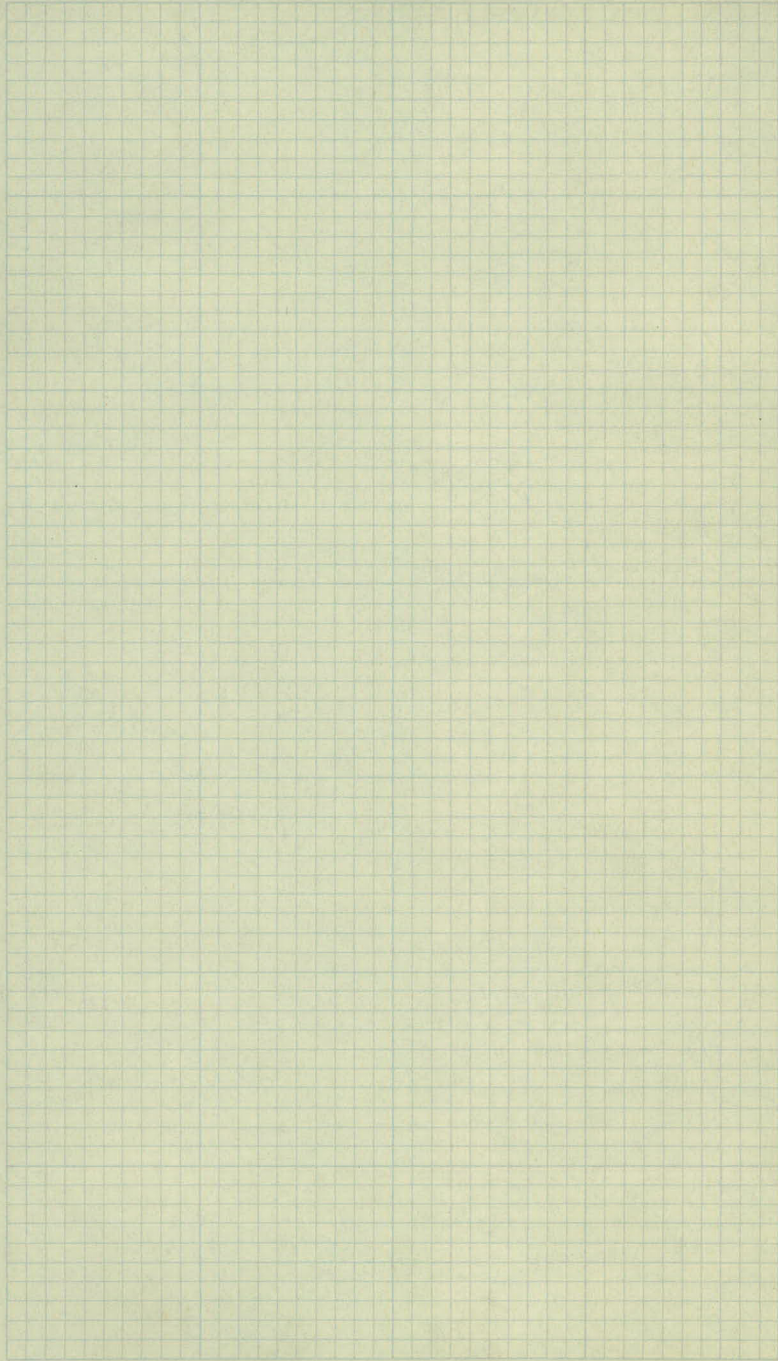


Tree line

Hoyt St

City limits

See Hoyt St Topog



Topog

Folwell St

6

+101 $\frac{P.P.}{16'}$
 +96 $\frac{Hycl.}{17'}$

+75 $\frac{Enil Oaks}{33'}$

5

4

3

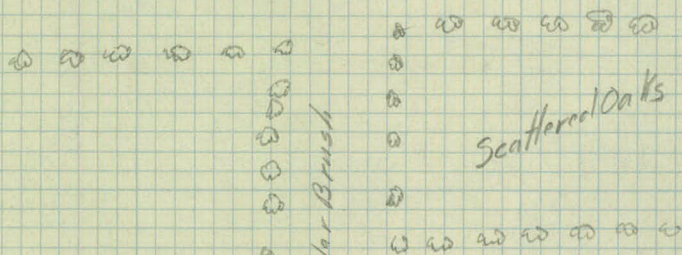
2

1

Enil Gutter Curbs + Walk +100 Barricade 4" Iron Post 72x10
 25'-25' Planks

0+00

Waste



Burton St

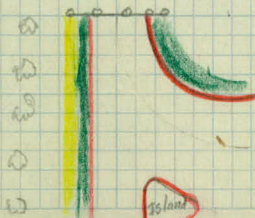
Scattered Onks

The 1st St

Overgrown with Poplar Bush

The 1st St

Scattered Onks



Note See Page 17
For Details
on Intersection

1+00

Walk
19.15

Curb
13.65

Curb
13.65

+92 $\frac{6" Elm}{17'}$

+93.5 $\frac{MH}{1.5'}$

+91 $\frac{6" Elm}{17'}$

+90 $\frac{Rad}{14.3}$

0+80

$\frac{Rad}{16.36}$

+70 $\frac{Rad}{20.5}$

0+60

$\frac{Rad}{28.6}$

+51 $\frac{6" Elm}{16.5'}$

+50 $\frac{Rad}{40.2}$

+45 $\frac{Rad}{58.3}$

0+40

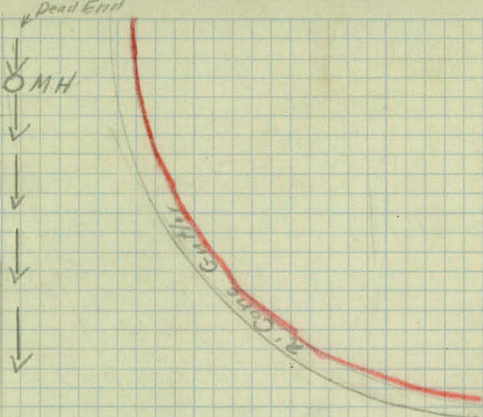
0+20

+11 $\frac{6" Elm}{17'}$

+07 $\frac{Hvil}{14.7}$

0+00 +02 $\frac{CB}{13.5}$

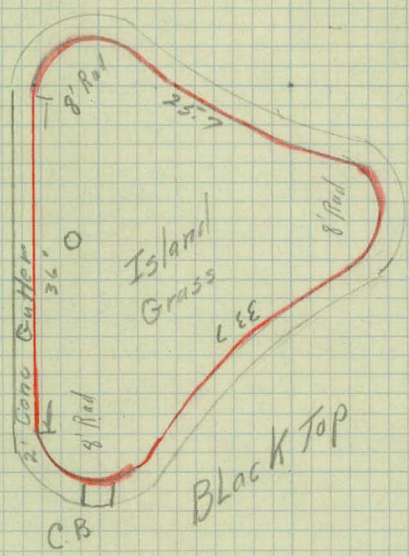
+04 $\frac{Ornamental Light}{17.0}$

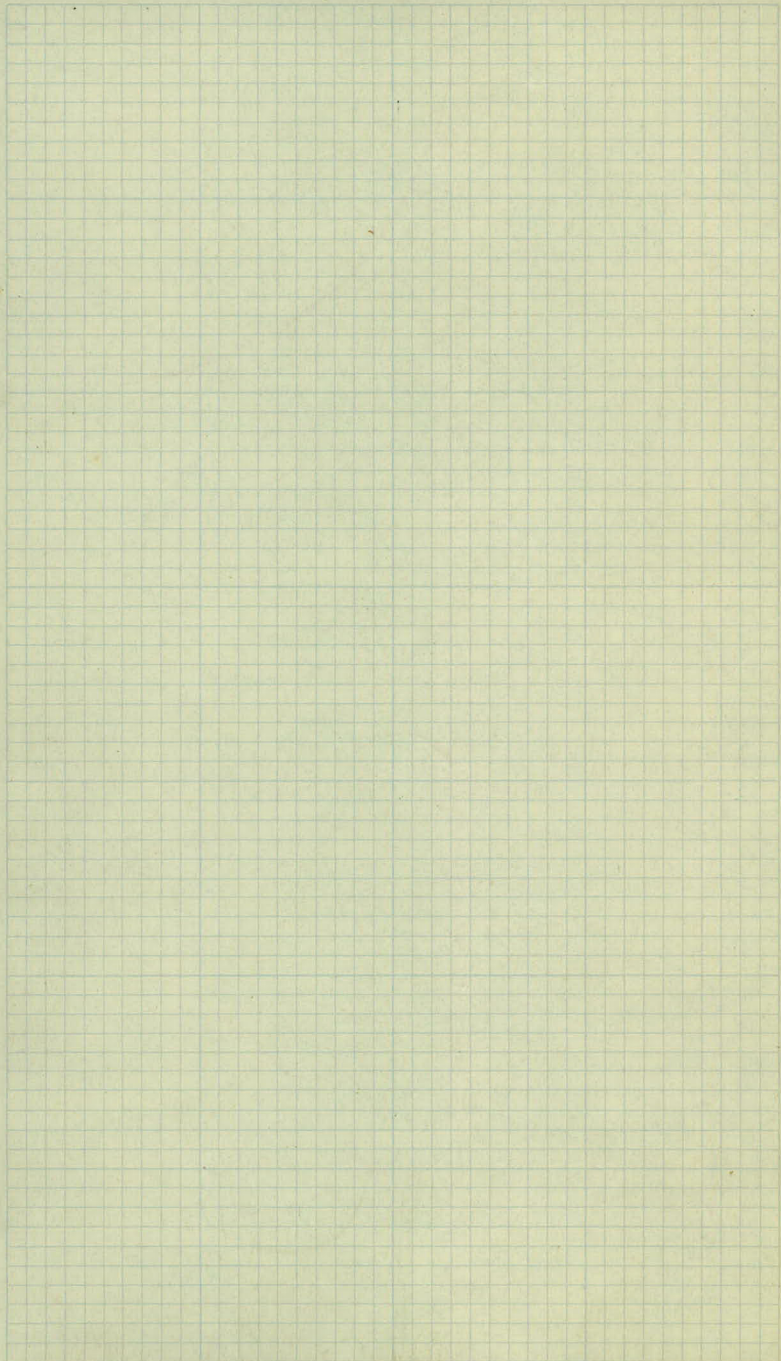


5.5' Conc Walk
 Bonjeram
 2' Conc Butte
 C.B.

Black Top

Black Top





Cross Sections
University Grove

Hoyt
Burton
Folwell St

Sta	+	Δ	-	Elev
B.M	338	29584		292.46

Profile Hoyt Ave West

0-13				290.3
------	--	--	--	-------

0-25				90.5
------	--	--	--	------

0-50				91.4
------	--	--	--	------

0-100				93.3
-------	--	--	--	------

0-150				95.5
-------	--	--	--	------

Lt.

X

Rt

Top of Hycl S.W. Cor Hart & Nortrop St

$$\frac{10.7}{100} \quad \frac{7.9}{50} \quad \frac{6.8}{33} \quad 5.5 \quad \frac{5.3}{13} \quad \frac{5.5}{25} \quad \frac{2.8}{50}$$

53

44

25

03

Sta	+	Δ	-	Elev
B.M	3.38	295.84		292.46

0+00				90.6
------	--	--	--	------

0+00	M.H	3 Ft Rt.		90.4
------	-----	----------	--	------

0+14		Gutter Line	Lt	90.3
------	--	-------------	----	------

0+14		Top of Curb	Lt	90.3
------	--	-------------	----	------

0+18				90.2
------	--	--	--	------

0+28				90.3
------	--	--	--	------

0+32				90.2
------	--	--	--	------

0+40				90.3
------	--	--	--	------

T.P	1226	304.72	3.38	292.46
-----	------	--------	------	--------

1+00				92.7
------	--	--	--	------

150				96.4
-----	--	--	--	------

+85				99.2
-----	--	--	--	------

+86				99.2
-----	--	--	--	------

LT E RT
 Top Hyl SW Cor Hoyt & Nortrop.

$$\frac{+5.0}{100} \quad \frac{8.0}{66} \quad \frac{2.1}{50} \quad \frac{4.6}{22} \quad 5.2 \quad \frac{6.9}{50} \quad \frac{9.5}{100} \quad \frac{12.3}{150}$$

$$5.4 \quad \frac{277.94}{17.9} \quad \text{Invert}$$

$$\frac{2.0}{50} \quad \frac{5.25}{27} \quad \frac{5.1}{22} \quad 5.5 \quad \frac{6.7}{30} \quad \frac{7.8}{50} \quad \frac{10.7}{100}$$

$$\frac{2.16}{50} \quad \frac{4.86}{27} \quad \frac{5.1}{22} \quad 5.5 \quad \frac{6.7}{30} \quad \frac{7.8}{50} \quad \frac{10.7}{100}$$

$$\frac{2.4}{50} \quad \frac{4.1}{33} \quad \frac{5.0}{18} \quad 5.6 \quad \frac{6.5}{27} \quad \frac{6.3}{29} \quad \frac{7.1}{50}$$

↑
 Curb Buried

$$\frac{2.0}{50} \quad \frac{4.4}{27} \quad \frac{4.95}{15} \quad \frac{5.3}{15} \quad 5.5 \quad \frac{6.0}{20} \quad \frac{6.9}{50}$$

Match Curb End. Rail

$$\frac{0.5}{50} \quad \frac{3.6}{30} \quad \frac{4.5}{26} \quad 5.6 \quad \frac{5.9}{27} \quad \frac{6.6}{50}$$

$$\frac{0.5}{50} \quad \frac{2.5}{34} \quad \frac{4.8}{29} \quad 5.5 \quad \frac{5.7}{29} \quad \frac{4.6}{36} \quad \frac{4.8}{50}$$

$$\frac{7.3}{50} \quad \frac{9.0}{34} \quad \frac{11.0}{30} \quad \frac{11.6}{16} \quad 12.0 \quad \frac{12.3}{16} \quad \frac{11.8}{29} \quad \frac{12.6}{32} \quad \frac{12.3}{50}$$

$$\frac{3.3}{50} \quad \frac{4.8}{34} \quad \frac{7.6}{30} \quad \frac{7.8}{15} \quad 8.3 \quad \frac{8.5}{14} \quad \frac{8.4}{24} \quad \frac{8.9}{31} \quad \frac{12.6}{31} \quad \frac{12.9}{50}$$

↑ Top Wall

$$\frac{6.2}{50} \quad \frac{6.2}{37} \quad \frac{4.6}{31} \quad \frac{5.8}{27} \quad \frac{5.7}{15} \quad \frac{5.5}{5} \quad 5.5 \quad \frac{5.1}{19} \quad \frac{6.3}{32} \quad \frac{10.4}{37} \quad \frac{12.3}{50}$$

$$\frac{6.2}{50} \quad \frac{6.2}{37} \quad \frac{4.6}{31} \quad \frac{5.8}{27} \quad \frac{5.7}{15} \quad \frac{5.5}{5} \quad 5.5 \quad \frac{5.5}{21} \quad \frac{6.2}{31} \quad \frac{7.4}{42} \quad \frac{9.2}{50}$$

Sta + T - Elev

304.72

1+96 Alley Rt 300.1

2+00 00.3

+30 01.5

T.P 9.20 310.80 3.12 301.60

+50 01.4

+80 00.8

3+00 00.1

+19 00.4

+24 00.4

+48.86 £ Barton 27.6

+85 00.8

T.P 3.09 303.75 10.14 300.66

+100 99.5

+27 95.7

L 2 R

$\frac{3.1}{50} \frac{5.5}{39} \frac{6.1}{23} \frac{5.1}{16} \frac{4.6}{4} 4.6 \frac{4.7}{15} \frac{5.2}{25} \frac{8.7}{50} \frac{11.9}{71} \frac{14.0}{84} \frac{17.4}{134}$

$\frac{0.0}{48} \frac{4.9}{39} \frac{6.2}{32} \frac{4.1}{27} \frac{5.0}{20} \frac{4.9}{11} 4.4 \frac{4.2}{14} \frac{4.2}{23} \frac{5.6}{30} \frac{9.3}{50}$

$\frac{13.0}{50} \frac{5.2}{00} \frac{2.7}{41} \frac{2.8}{36} \frac{4.0}{27} \frac{4.5}{24} \frac{3.8}{18} \frac{3.8}{13} 3.2 \frac{3.3}{20} \frac{2.5}{33} \frac{6.4}{46} \frac{2.8}{50}$

$\frac{4.1}{50} \frac{4.1}{40} \frac{6.7}{36} \frac{8.6}{30} 9.1 \frac{9.4}{24} \frac{5.6}{29} \frac{7.4}{44} \frac{8.6}{50}$

$\frac{4.6}{50} \frac{3.3}{38} \frac{9.2}{30} 10.0 \frac{10.0}{23} \frac{6.5}{27} \frac{5.4}{50}$

$\frac{4.8}{50} \frac{6.1}{38} \frac{9.6}{29} 10.7 \frac{10.4}{26} \frac{8.8}{28} \frac{8.5}{41} \frac{7.8}{50}$

$\frac{4.6}{50} \frac{3.9}{38} \frac{10.0}{29} 10.4 \frac{10.0}{24} \frac{10.5}{50}$

$\frac{8.6}{50} \frac{10.0}{32} 10.4 \frac{10.8}{27} \frac{11.4}{50}$

$\frac{9.3}{50} 10.2 \frac{10.1}{20} \frac{10.6}{25} \frac{11.6}{32} \frac{13.2}{50}$

$\frac{9.5}{50} \frac{9.8}{31} 10.0 \frac{10.3}{13} \frac{11.7}{29} \frac{13.6}{50}$

Top of Hub 0+00 & Burton

$\frac{2.7}{50} \frac{4.3}{37} \frac{5.3}{26} 4.3 \frac{5.1}{25} \frac{6.5}{34} \frac{7.7}{50}$

$\frac{2.5}{50} \frac{4.7}{37} \frac{5.6}{31} 8.1 \frac{8.5}{8} \frac{7.5}{15} \frac{8.4}{26} \frac{9.2}{28} \frac{10.3}{50}$

Sta + π - Elev

303.75

4+39

294.7

+80

94.6

+98.93

94.7

5+25

96.1

T.P.

3.09

300.66

Lt £ Pt

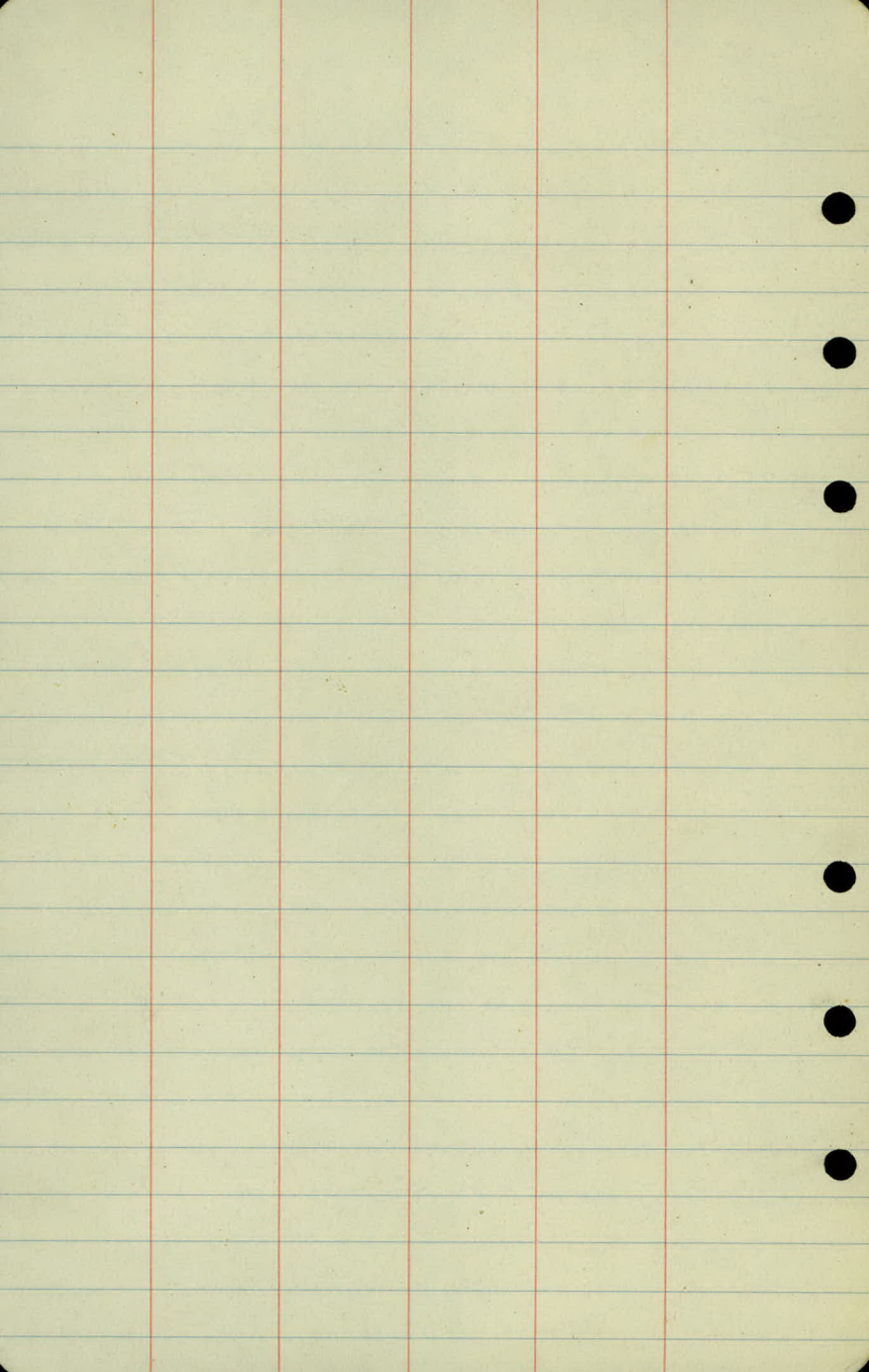
$$\frac{3.0}{50} \quad \frac{7.7}{20} \quad 9.1 \quad \frac{10.0}{15} \quad \frac{10.3}{25} \quad \frac{11.1}{20}$$

$$\frac{4.8}{30} \quad \frac{5.9}{77} \quad \frac{9.4}{13} \quad 9.2 \quad \frac{9.1}{15} \quad \frac{9.8}{22} \quad \frac{11.3}{41} \quad \frac{11.3}{50}$$

$$\frac{4.2}{50} \quad \frac{7.2}{21} \quad \frac{8.4}{4} \quad 9.1 \quad \frac{9.5}{14} \quad \frac{10.4}{35} \quad \frac{10.4}{50}$$

$$\frac{2.1}{50} \quad \frac{5.4}{21} \quad \frac{7.5}{2} \quad 7.7 \quad \frac{8.7}{16} \quad \frac{10.0}{50}$$

Top Hub 0x00 & Burton



Cross Sections
Burton St

Sta	+	π	-	Elv
T.P	13.56	314.22 ✓		300.66 ✓
B.M	7.46	314.22 ✓	7.46	304.76 ✓

0+00 300.6

0+31 01.1

0+37 01.2

0+50 01.6

1+00 04.7

+40 06.9

+75 08.2

2+00 09.2

+30 10.5

T.P 9.49 319.86 ✓ 3.85 310.37 ✓

+72 11.8

3+00 12.3

LT & RT

Top of Hub & Burton
Top of Hyl NW Cor Burton & Hoyt

13.6

$\frac{128}{50}$ $\frac{132}{29}$ $\frac{133}{18}$ $\frac{131}{13.1}$ $\frac{130}{24}$ $\frac{124}{27}$ $\frac{138}{37}$ $\frac{15.3}{50}$

$\frac{9.5}{50}$ $\frac{9.2}{35}$ $\frac{13.1}{28}$ $\frac{13.1}{12}$ $\frac{13.0}{18.0}$ $\frac{13.0}{21}$ $\frac{12.2}{25}$ $\frac{13.5}{35}$ $\frac{15.0}{50}$

$\frac{8.1}{50}$ $\frac{8.2}{34}$ $\frac{12.4}{27}$ $\frac{12.5}{18}$ $\frac{12.6}{12.6}$ $\frac{12.7}{14}$ $\frac{12.6}{23}$ $\frac{11.9}{28}$ $\frac{12.8}{32}$ $\frac{13.1}{50}$

$\frac{7.7}{50}$ $\frac{7.7}{34}$ $\frac{8.2}{24}$ $\frac{9.4}{16}$ $\frac{9.5}{9.5}$ $\frac{9.2}{24}$ $\frac{6.7}{30}$ $\frac{5.2}{50}$

$\frac{3.2}{50}$ $\frac{3.0}{44}$ $\frac{5.0}{36}$ $\frac{6.4}{31}$ $\frac{7.0}{26}$ $\frac{6.9}{13}$ $\frac{7.3}{7.3}$ $\frac{7.5}{10}$ $\frac{7.3}{25}$ $\frac{6.6}{30}$ $\frac{3.7}{37}$ $\frac{3.0}{50}$

$\frac{5.1}{50}$ $\frac{5.7}{29}$ $\frac{6.5}{8}$ $\frac{6.0}{6.0}$ $\frac{6.1}{15}$ $\frac{6.0}{40}$ $\frac{6.5}{50}$

$\frac{5.0}{50}$ $\frac{4.0}{14}$ $\frac{4.0}{6}$ $\frac{4.6}{5}$ $\frac{5.0}{5.0}$ $\frac{5.5}{19}$ $\frac{5.4}{36}$ $\frac{6.0}{50}$

$\frac{3.6}{50}$ $\frac{2.6}{27}$ $\frac{3.5}{22}$ $\frac{3.2}{5}$ $\frac{3.7}{3.7}$ $\frac{4.2}{23}$ $\frac{3.6}{30}$ $\frac{2.8}{34}$ $\frac{4.1}{42}$ $\frac{4.3}{50}$

$\frac{6.8}{50}$ $\frac{6.0}{30}$ $\frac{8.4}{26}$ $\frac{8.0}{9}$ $\frac{8.1}{8.1}$ $\frac{7.8}{26}$ $\frac{3.9}{35}$ $\frac{4.2}{50}$

$\frac{6.6}{50}$ $\frac{5.8}{31}$ $\frac{7.5}{26}$ $\frac{7.8}{22}$ $\frac{7.6}{7.6}$ $\frac{7.5}{29}$ $\frac{4.1}{37}$ $\frac{4.0}{50}$

Sta + π - Ekv

319.86

3 + 50

311.1

+ 85

09.3

4 + 20

08.5

+ 30

08.1

+ 64

07.2

+ 69

07.3

+ 96.84

$\pm$ Folwell

06.8

T.P

13.64

321.75

11.75

308.11

B.M.

3.38

318.37

318.34

LT * RT

$\frac{7.8}{50}$ $\frac{8.4}{22}$ $\frac{8.6}{12}$ $\frac{8.3}{8}$ 8.8 $\frac{9.1}{10}$ $\frac{9.0}{19}$ $\frac{8.8}{25}$ $\frac{7.1}{31}$ $\frac{8.1}{50}$

$\frac{8.3}{50}$ $\frac{9.3}{27}$ $\frac{10.0}{24}$ $\frac{10.0}{11}$ 10.6 $\frac{10.8}{12}$ $\frac{11.1}{20}$ $\frac{10.8}{22}$ $\frac{10.2}{27}$ $\frac{10.7}{35}$ $\frac{11.0}{50}$

$\frac{8.2}{50}$ $\frac{8.7}{30}$ $\frac{10.8}{25}$ $\frac{11.1}{12}$ $\frac{10.7}{14}$ $\frac{11.5}{20}$ $\frac{10.0}{30}$ $\frac{10.3}{30}$

$\frac{7.3}{50}$ $\frac{7.1}{34}$ $\frac{11.7}{26}$ $\frac{11.8}{13}$ 11.8 $\frac{12.2}{18}$ $\frac{12.0}{25}$ $\frac{7.8}{35}$ $\frac{9.1}{50}$

$\frac{7.7}{50}$ $\frac{7.8}{43}$ $\frac{10.5}{40}$ $\frac{12.1}{33}$ $\frac{12.6}{14}$ 12.7 $\frac{12.7}{14}$ $\frac{13.4}{28}$ $\frac{8.0}{38}$ $\frac{9.5}{50}$

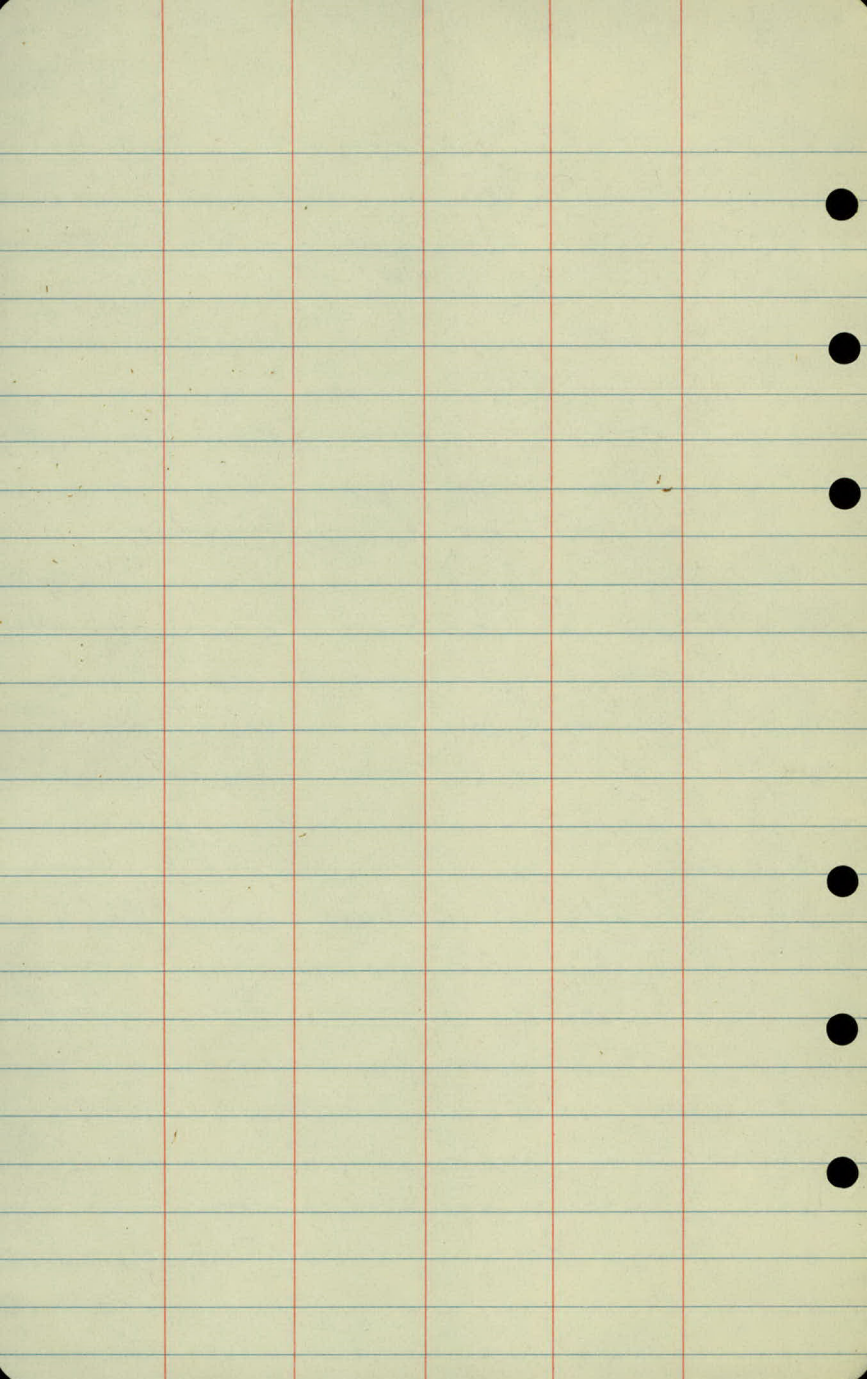
$\frac{11.1}{50}$ $\frac{10.9}{40}$ $\frac{12.3}{29}$ $\frac{12.7}{12}$ 12.6 $\frac{12.7}{11}$ $\frac{13.8}{27}$ $\frac{15.2}{50}$

$\frac{11.4}{50}$

13.1

$\frac{15.3}{50}$

Top Hyd Folwell & Nortrop



X sections
Folwell St

	+	π	-	Elv
B.M	3.55	321.89		318.34
				14.6

0+00

0+50

16.3

+93

1+00

1+00

16.9

+50

+50

16.9

2+00

15.9

+50

14.7

3

13.0

T.P

2.99

316.49

8.39

313.00

+50

11.1

4

08.2

+08

07.8

+20

07.6

LT & PT

6.95 TopCurb $\frac{7.28}{13.4}$ 7.82 $\frac{7.25}{11.5}$ 7.3 $\frac{7.68}{11.5}$ $\frac{7.79}{13.4}$ $\frac{7.32}{13.4}$ curb
Walk Gutter

5.48 TopCurb $\frac{5.65}{12.5}$ $\frac{6.14}{13.5}$ $\frac{5.94}{11.5}$ 5.6 $\frac{5.6}{15}$ $\frac{6.38}{34}$ $\frac{6.58}{36}$ $\frac{6.10}{36}$ TopCurb
Sidewalk Gutter

M.H 4.85 14.65 to Thurst

$\frac{2.7}{35}$ $\frac{4.8}{29}$ $\frac{4.65}{25}$ $\frac{4.72}{20}$ $\frac{4.85}{14}$ $\frac{5.29}{14}$ $\frac{5.14}{12}$ 5.0 $\frac{5.18}{12}$ $\frac{5.30}{14}$ $\frac{4.84}{14}$ $\frac{4.9}{29}$ $\frac{1.2}{35}$ $\frac{2.0}{50}$

$\frac{1.2}{50}$

$\frac{0.2}{50}$ $\frac{1.1}{37}$ $\frac{3.3}{34}$ $\frac{4.6}{28}$ $\frac{4.8}{12}$ 5.0 $\frac{5.2}{10}$ $\frac{4.6}{33}$ $\frac{3.1}{37}$ $\frac{2.7}{50}$

$\frac{6.9}{50}$ $\frac{5.7}{28}$ $\frac{6.3}{25}$ 6.0 $\frac{5.8}{11}$ $\frac{5.1}{28}$ $\frac{4.6}{50}$

$\frac{5.2}{50}$ $\frac{5.2}{35}$ $\frac{7.2}{28}$ $\frac{6.6}{6}$ 7.2 $\frac{6.6}{9}$ $\frac{6.4}{12}$ $\frac{6.3}{25}$ $\frac{5.8}{29}$ $\frac{4.5}{50}$

$\frac{10.4}{50}$ $\frac{9.1}{43}$ $\frac{6.4}{28}$ $\frac{8.6}{21}$ 8.9 $\frac{9.1}{12}$ $\frac{8.8}{25}$ $\frac{6.0}{30}$ $\frac{6.7}{50}$

$\frac{6.3}{50}$ $\frac{2.7}{30}$ $\frac{5.6}{22}$ $\frac{5.9}{13}$ 5.4 $\frac{5.8}{13}$ $\frac{5.4}{25}$ $\frac{2.7}{30}$ $\frac{2.7}{50}$

$\frac{9.0}{50}$ $\frac{6.2}{29}$ $\frac{7.9}{24}$ 8.3 $\frac{8.1}{10}$ $\frac{7.8}{25}$ $\frac{4.5}{32}$ $\frac{4.0}{50}$

$\frac{8.7}{50}$ $\frac{6.5}{30}$ $\frac{8.5}{24}$ 8.7 $\frac{7.9}{26}$ $\frac{4.5}{32}$ $\frac{4.0}{50}$

$\frac{8.7}{50}$ $\frac{7.2}{28}$ $\frac{9.1}{22}$ 8.9 $\frac{8.9}{14}$ $\frac{8.4}{50}$

Sta + T - Elev

316.49

4+38

306.8

+70

05.8

+80

05.4

5

04.3

B.M. 4.81 308.83 12.47 304.02

+50

02.4

+80

01.3

6+01.85

End Project 300.6

+25

299.8

B.M. 4.81 308.83 4.81 304.02

13.76 320.47 2.12 306.71

2.13 318.34 318.34

L+ E Rt

$$\frac{104}{50} \quad \frac{8.7}{29} \quad \frac{9.6}{23} \quad 9.7 \quad \frac{9.4}{24} \quad \frac{8.8}{50}$$

$$\frac{11.4}{50} \quad \frac{11.2}{19} \quad \frac{10.5}{6} \quad 10.7 \quad \frac{10.1}{36} \quad \frac{9.3}{50}$$

$$\frac{12.3}{50} \quad \frac{11.7}{26} \quad 11.1 \quad \frac{11.0}{19} \quad \frac{10.3}{26} \quad \frac{5.1}{39} \quad \frac{4.8}{50}$$

$$\frac{13.2}{50} \quad \frac{12.3}{13} \quad \frac{11.8}{5} \quad 12.0 \quad \frac{11.7}{24} \quad \frac{6.5}{32} \quad \frac{5.2}{50}$$

Top Hyd NW^{Cor} Folwell + E line of NW^{1/4} of NE^{1/4}

$$\frac{7.8}{50} \quad \frac{5.7}{26} \quad \frac{6.8}{24} \quad 6.4 \quad \frac{6.6}{27} \quad \frac{3.4}{34} \quad \frac{3.0}{50}$$

$$\frac{7.3}{50} \quad \frac{6.4}{26} \quad \frac{7.8}{23} \quad 7.5 \quad \frac{8.0}{31} \quad \frac{8.2}{50}$$

$$\frac{7.4}{50} \quad \frac{7.2}{25} \quad 8.2 \quad \frac{9.0}{25} \quad \frac{9.6}{50}$$

$$\frac{7.5}{50} \quad \frac{8.0}{25} \quad 9.0 \quad \frac{9.7}{20} \quad \frac{10.2}{50}$$

Top Hyd Folwell + End Project

Top Hyd Folwell + Northrop

