

B-32-211

Dr. 11 - Bk. 32

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

Tatum St

LINDIG ROAD

From Larpenteur Ave Co. Rd. A2

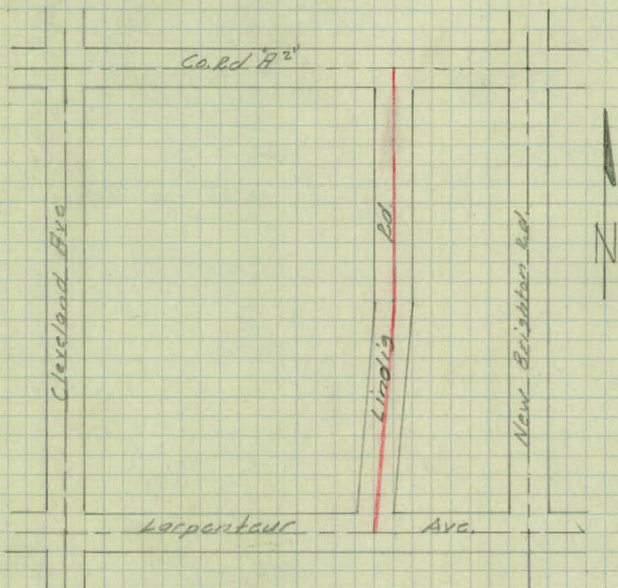
Road Acc't. No. R-54

Date Filed 12-23-38

File. _____

Rose Twp.

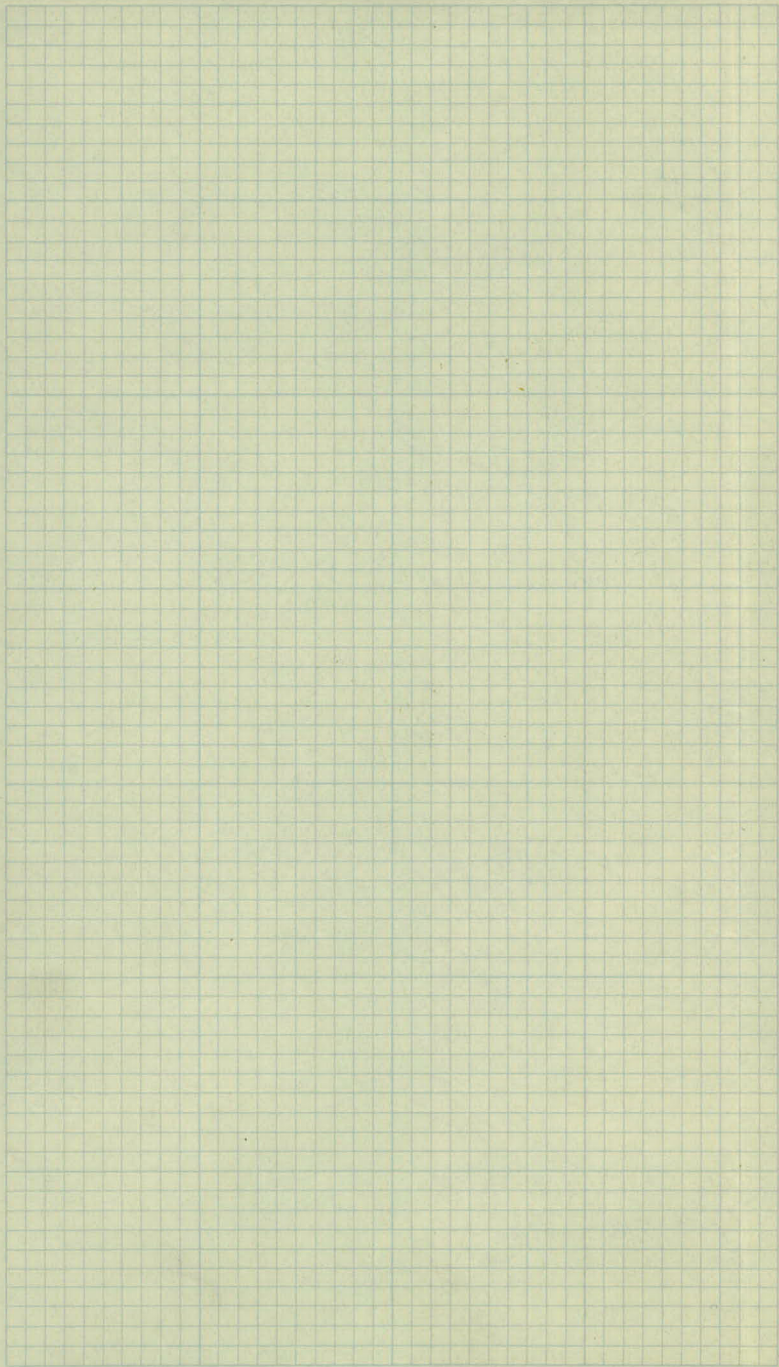
PLAN SURVEY
LINDIG RD.
Larperneur Ave. to Co. Rd. "A" 2nd



INDEX.

Align. - 1-2
Terra. - 3-5
Levels - 6-7
Sections - 8-14

10/18/38



1
Alignment.

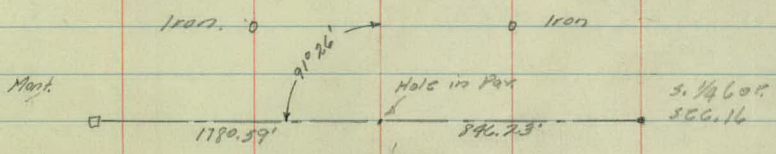
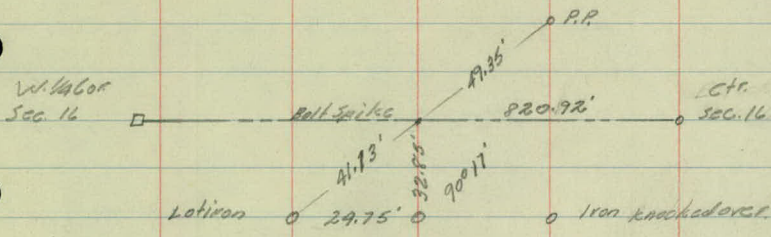
Sta	Point	ΔLt	ΔRt
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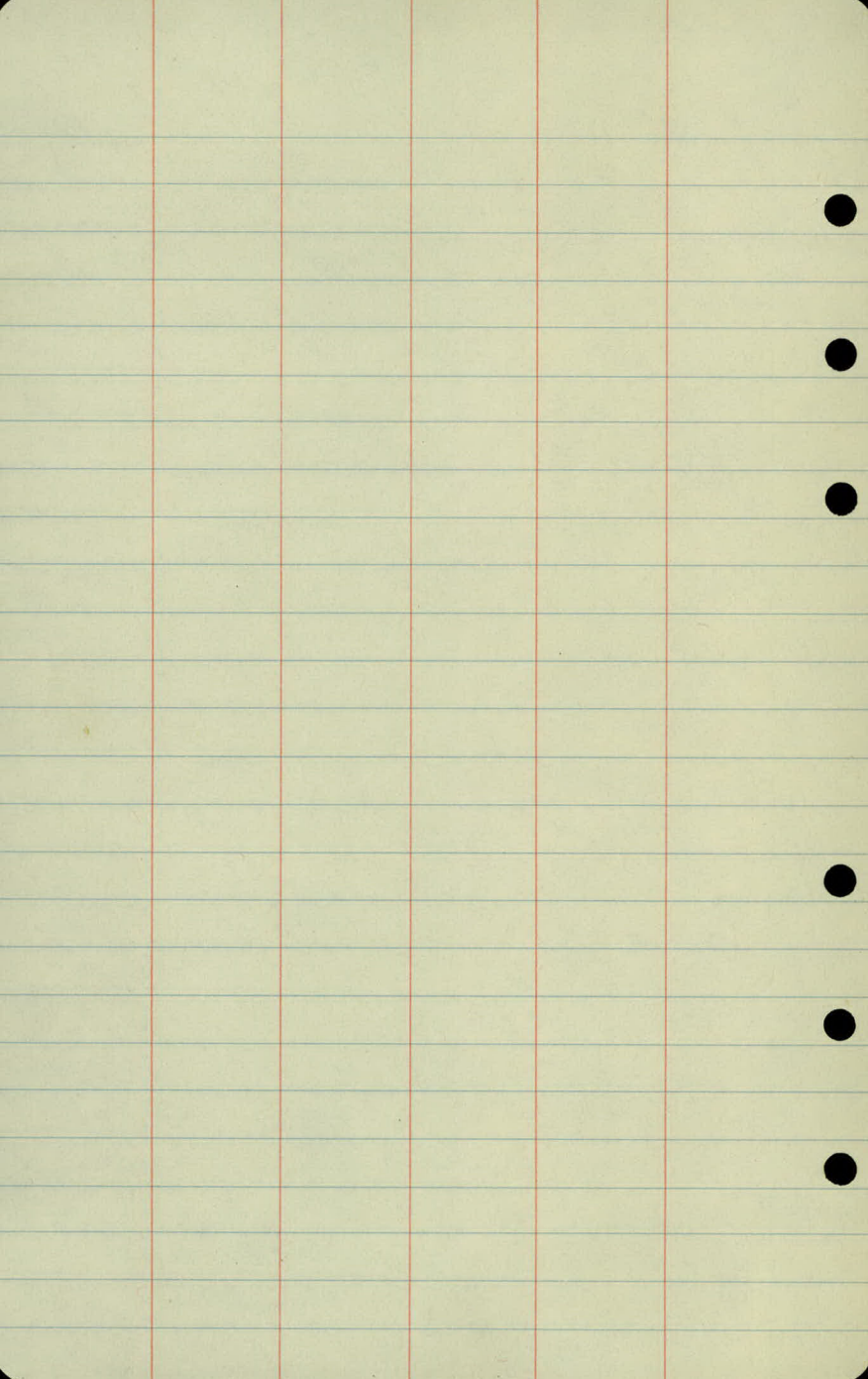
26	+34.25		
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19	+17.35	P.I.	1°07'
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0	100		
---	-----	--	--

K. A.
L. B. H.
L. C.
M. J. G.





Topography

5

4

3

105. S.W. Cor. Chicken Coop - 2.5'

2

+25 - Cor. S. head - 2.9' + Fee - 2.3'
+1.8 - Top Fe. - 2.3'

1

+93 - 3" Fee - 2.5' 199 - RM - 1.5'
+79 - 4" Apple - 2.4'
+72 - Thail - 2.1'
+66 - End Hedge - 1.6'
+58 - 4" Willow - 1.6'
+40 - 6" Pop - 1.6'
+26 - 4" Willow - 1.6'
+17 - 4" Tw. B. Hick - 1.6'
+08 - 3" Plum - 1.6'

196 S.W. Cor. Mo. - 8.4'

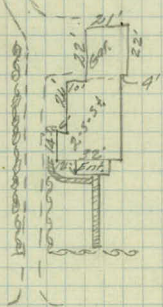
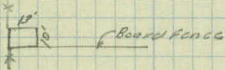
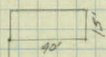
+99 - 6" Pop - 1.7'
+85 - 2" Plum Tr. - 1.7'
+73 - 6" Pop - 1.7'
+59 - Hedge - 1.7' Cor. Hedge - 3.1'
+30 - 2" End 2.6'

0 100

Cult

Cult

Trail 3'



126-3 Edge 81 Top.

26

7

2

7

6

16'

Cult.

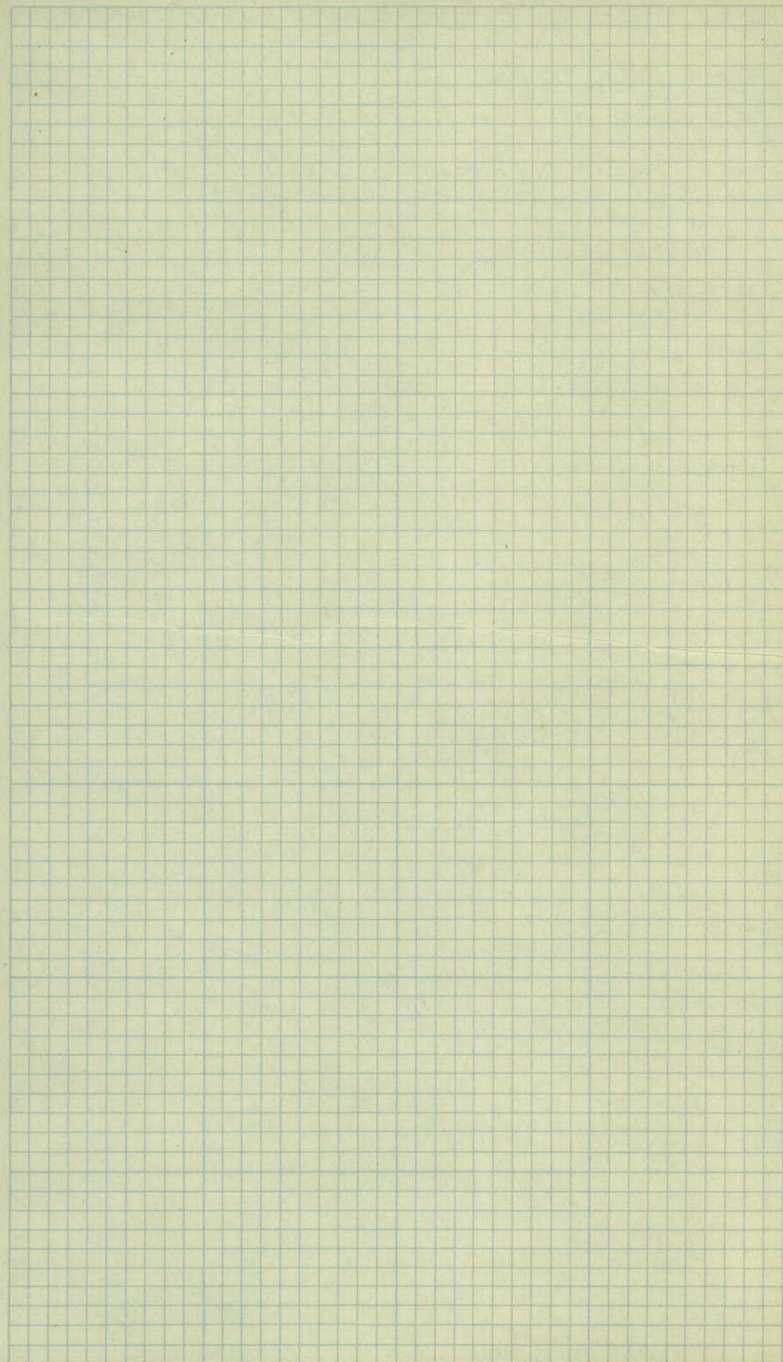
Cult.

Trail - 28'

7'

3

3



Bench Levels

Sta.	+	X	-	Elev.
B.M.	6.93	973.41		966.48
T.P.	7.55	977.98	2.98	970.43
B.M.	4.85	979.13	3.70	974.28
T.P.	6.18	980.37	4.94	974.19
T.P.	8.25	982.01	6.61	973.74
B.M.			3.17	978.54
T.P.	6.05	983.21	2.35	979.16
T.P.	12.84	993.09	4.96	980.25
B.M.			12.99	980.10

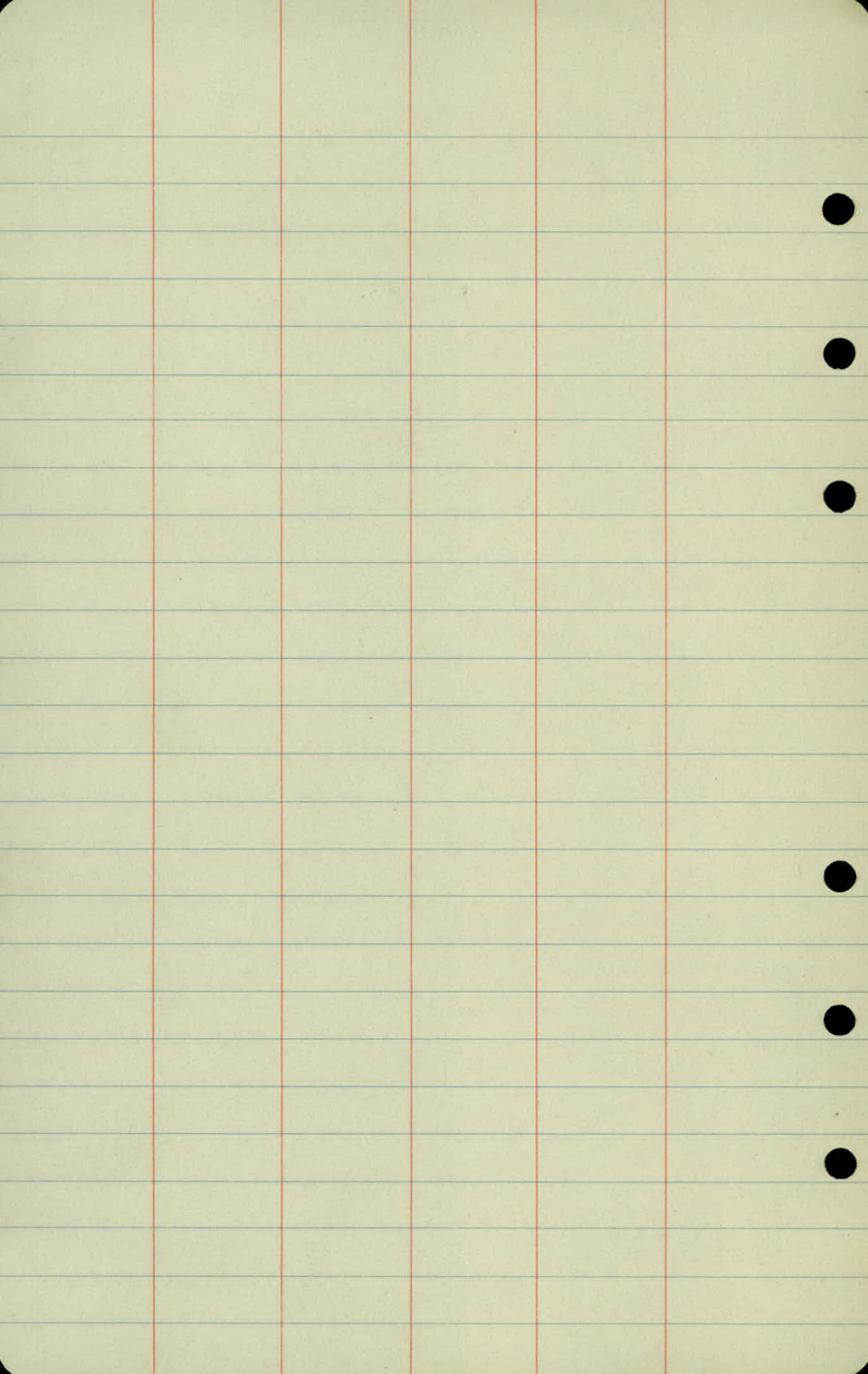
Descriptions

Top Bolt in Pav. & Larp & New Brighton Rd.

Top Hole in Pav 0+00

Top Iron Pipe 24.75' Lt sta 13+17.35

Spike in RR N.E. Cor. Co. Rd. 17² & Lindig Rd.



x sections

Sta	+	-	-	Elev
B.M.	7.56	974.04		966.48
I.P.	6.87	978.49	2.42	971.62
B.M.	4.42	978.70	4.20	974.29

0 100 74.28

+10 74.26

+22 74.1

+27 72.4

+31 72.5

+35 73.2

+50 73.4

1 73.5

+50 73.6

2 73.9

Lt

K

Rt

Top Bolt in Rev to Warp & New Brighton Rd

942 $\frac{403}{50}$ 994 $\frac{479}{50}$ $\frac{41}{50}$ 46 $\frac{49}{50}$ $\frac{58}{50}$ 63 $\frac{61}{14}$ $\frac{49}{17}$ $\frac{50}{38}$ $\frac{67}{41}$ $\frac{68}{50}$ $\frac{57}{50}$ 62 $\frac{65}{15}$ $\frac{50}{17}$ $\frac{50}{38}$ $\frac{67}{41}$ $\frac{69}{50}$ $\frac{51}{50}$ 55 $\frac{55}{19}$ $\frac{50}{17}$ $\frac{50}{38}$ $\frac{52}{41}$ $\frac{53}{50}$ $\frac{50}{50}$ $\frac{49}{23}$ 53 $\frac{56}{15}$ $\frac{48}{18}$ $\frac{51}{50}$ $\frac{49}{50}$ $\frac{49}{25}$ 52 $\frac{54}{19}$ $\frac{46}{18}$ $\frac{43}{30}$ $\frac{373}{32.5}$

W/4/16.

 $\frac{48}{50}$ $\frac{49}{24}$ 51 $\frac{52}{14}$ $\frac{45}{16}$ $\frac{42}{35}$ $\frac{47}{50}$ $\frac{46}{26}$ 48 $\frac{51}{20}$ $\frac{47}{24}$ $\frac{47}{50}$

Sta.	+	X	-	Elev
		978.70		
2	+50			74.1
3				74.4
T.P.	3.26	978.51	3.45	975.25
	+50			74.4
4				74.1
	+50			73.5
5				73.4
	+50			73.4
6				73.5
	+50			74.4
7				75.2
	+50			75.2
T.P.	3.42	979.36	2.57	975.94

Lt

L

Rt

$$\frac{44}{50} \quad \frac{44}{24} \quad \frac{46}{24} \quad \frac{50}{24} \quad L.O.$$

$$\frac{30}{50} \quad \frac{39}{25} \quad \frac{43}{24} \quad \frac{46}{24} \quad L.O.$$

$$\frac{37}{50} \quad \frac{37}{25} \quad \frac{41}{22} \quad \frac{39}{22} \quad \frac{40}{50}$$

$$\frac{44}{50} \quad \frac{44}{25} \quad \frac{44}{24} \quad \frac{40}{24} \quad \frac{36}{50}$$

$$\frac{51}{50} \quad \frac{52}{29} \quad \frac{50}{19} \quad \frac{47}{19} \quad \frac{35}{50}$$

$$\frac{53}{50} \quad \frac{53}{24} \quad \frac{51}{13} \quad \frac{52}{13} \quad \frac{36}{50}$$

$$\frac{50}{50} \quad \frac{52}{26} \quad \frac{51}{15} \quad \frac{51}{15} \quad \frac{36}{50}$$

$$\frac{47}{50} \quad \frac{50}{27} \quad \frac{50}{18} \quad \frac{49}{18} \quad \frac{39}{50}$$

$$\frac{37}{50} \quad \frac{40}{27} \quad \frac{41}{24} \quad \frac{40}{24} \quad \frac{36}{50}$$

$$\frac{27}{50} \quad \frac{32}{23} \quad \frac{33}{20} \quad \frac{32}{20} \quad \frac{30}{50}$$

$$\frac{24}{50} \quad \frac{28}{25} \quad \frac{33}{21} \quad \frac{31}{21} \quad \frac{31}{50}$$

	347	+	π	-	Elek
			717.36		
8					75.2
	+50				74.8
9					73.4
	+50				72.9
10					72.8
	+50				72.8
11					73.3
	+50				74.5
12					74.0
	+50				76.6
13					77.2
T.P.	7.28		986.11	0.53	978.83
			✓		✓
					978.84

L.H.

A

R.H.

$$\frac{34}{50} \quad \frac{38}{25} \quad \frac{42}{25} \quad \frac{42}{25} \quad \frac{46}{50}$$

$$\frac{35}{50} \quad \frac{40}{25} \quad \frac{46}{28} \quad \frac{47}{28} \quad \frac{53}{50}$$

$$\frac{49}{50} \quad \frac{53}{26} \quad \frac{60}{29} \quad \frac{60}{29} \quad \frac{64}{50}$$

$$\frac{58}{50} \quad \frac{62}{26} \quad \frac{65}{25} \quad \frac{66}{25} \quad \frac{69}{50}$$

$$\frac{58}{50} \quad \frac{62}{26} \quad \frac{66}{28} \quad \frac{69}{28} \quad \frac{69}{50}$$

$$\frac{56}{50} \quad \frac{62}{30} \quad \frac{66}{23} \quad \frac{68}{23} \quad \frac{68}{50}$$

$$\frac{49}{50} \quad \frac{56}{26} \quad \frac{61}{28} \quad \frac{62}{28} \quad \frac{63}{50}$$

$$\frac{49}{50} \quad \frac{44}{26} \quad \frac{49}{29} \quad \frac{50}{29} \quad \frac{55}{50}$$

$$\frac{25}{50} \quad \frac{30}{28} \quad \frac{54}{26} \quad \frac{38}{26} \quad \frac{46}{50}$$

$$\frac{16}{50} \quad \frac{23}{23} \quad \frac{28}{23} \quad \frac{30}{23} \quad \frac{35}{50}$$

$$\frac{19}{50} \quad \frac{17}{27} \quad \frac{22}{26} \quad \frac{25}{26} \quad \frac{31}{50}$$

Tap Iron Pipe 24.75' 13' 17.35

Sta.	+	π	-	Elev.
		886.11		
13	+50			77.3
14				77.6
	+50			77.9
15				78.2
	+50			78.5
16				78.6
	+50			79.0
17				79.5
	+50			80.1
18				80.2
	+50			79.3

Lt

K

Rt

$$\frac{75}{50} \quad \frac{84}{24} \quad \frac{88}{25} \quad \frac{93}{50}$$

$$\frac{77}{50} \quad \frac{82}{26} \quad \frac{85}{28} \quad \frac{91}{50}$$

$$\frac{74}{50} \quad \frac{80}{26} \quad \frac{82}{23} \quad \frac{92}{50}$$

$$\frac{70}{50} \quad \frac{75}{26} \quad \frac{79}{28} \quad \frac{91}{50}$$

$$\frac{62}{50} \quad \frac{68}{24} \quad \frac{76}{26} \quad \frac{92}{50}$$

$$\frac{55}{50} \quad \frac{66}{26} \quad \frac{75}{25} \quad \frac{86}{50}$$

$$\frac{47}{50} \quad \frac{59}{26} \quad \frac{71}{23} \quad \frac{94}{50}$$

$$\frac{41}{50} \quad \frac{56}{24} \quad \frac{66}{27} \quad \frac{91}{50}$$

$$\frac{33}{50} \quad \frac{48}{24} \quad \frac{40}{22} \quad \frac{84}{50}$$

$$\frac{32}{50} \quad \frac{45}{30} \quad \frac{59}{26} \quad \frac{86}{50}$$

$$\frac{37}{50} \quad \frac{55}{26} \quad \frac{68}{23} \quad \frac{94}{50}$$

Sta	+	Δ	-	Elev.
		986.11		78
19				78.9
T.P.	8.05	987.67 ✓	649	779.62
+67				78.2
20				79.5
+50				80.9
21				81.6
+50				81.4
22				81.1
+50				81.5
23				83.1
T.P.	9.81	993.60 ✓	388	983.79
+50				85.4
24				88.3

44

4

24

$$\frac{43}{50} \quad \frac{59}{29} \quad \frac{72}{24} \quad \frac{89}{24} \quad \frac{96}{50}$$

$$\frac{70}{50} \quad \frac{84}{27} \quad \frac{75}{21} \quad \frac{101}{21} \quad \frac{107}{50}$$

$$\frac{55}{50} \quad \frac{71}{26} \quad \frac{82}{27} \quad \frac{93}{27} \quad \frac{106}{50}$$

$$\frac{48}{50} \quad \frac{59}{29} \quad \frac{68}{24} \quad \frac{79}{24} \quad \frac{92}{50}$$

$$\frac{48}{50} \quad \frac{54}{30} \quad \frac{61}{29} \quad \frac{72}{29} \quad \frac{81}{50}$$

$$\frac{54}{50} \quad \frac{59}{31} \quad \frac{63}{29} \quad \frac{73}{29} \quad \frac{78}{30}$$

$$\frac{52}{50} \quad \frac{61}{27} \quad \frac{66}{31} \quad \frac{73}{31} \quad \frac{75}{50}$$

$$\frac{46}{50} \quad \frac{56}{20} \quad \frac{62}{26} \quad \frac{69}{26} \quad \frac{73}{50}$$

$$\frac{52}{50} \quad \frac{40}{30} \quad \frac{46}{27} \quad \frac{53}{27} \quad \frac{60}{50}$$

$$\frac{21}{50} \quad \frac{80}{27} \quad \frac{82}{27} \quad \frac{80}{27} \quad \frac{99}{50}$$

$$\frac{50}{50} \quad \frac{53}{26} \quad \frac{53}{29} \quad \frac{59}{29} \quad \frac{61}{50}$$

3/2	+	π	-	Elev
		99860 ✓		

24	+30			90.5
----	-----	--	--	------

	+50			91.3
--	-----	--	--	------

	+75			89.6
--	-----	--	--	------

25				86.8
----	--	--	--	------

	+50			83.1
--	-----	--	--	------

26				80.7
----	--	--	--	------

	+19			80.4
--	-----	--	--	------

	+22			80.9
--	-----	--	--	------

13425				81.2
-------	--	--	--	------

B.M.		13.49	980.11 ✓	980.10
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L.L.

L.

R.H.

$$\frac{46}{50} \quad \frac{39}{29} \quad \frac{31}{28} \quad \frac{34}{28} \quad \frac{40}{50}$$

$$\frac{57}{50} \quad \frac{36}{22} \quad \frac{23}{29} \quad \frac{25}{29} \quad \frac{29}{50}$$

$$\frac{69}{50} \quad \frac{59}{24} \quad \frac{40}{7} \quad \frac{40}{7} \quad \frac{31}{29} \quad \frac{27}{50}$$

$$\frac{79}{50} \quad \frac{73}{21} \quad \frac{68}{25} \quad \frac{57}{25} \quad \frac{48}{50}$$

$$\frac{89}{50} \quad \frac{107}{29} \quad \frac{105}{25} \quad \frac{104}{25} \quad \frac{101}{50}$$

$$\frac{115}{50} \quad \frac{125}{50} \quad \frac{129}{25} \quad \frac{128}{25} \quad \frac{127}{50}$$

$$\frac{126}{50} \quad \frac{131}{29} \quad \frac{132}{24} \quad \frac{133}{24} \quad \frac{131}{50}$$

$$\frac{122}{50} \quad \frac{127}{25} \quad \frac{127}{26} \quad \frac{127}{26} \quad \frac{126}{50}$$

81.4

$$\frac{122}{50}$$

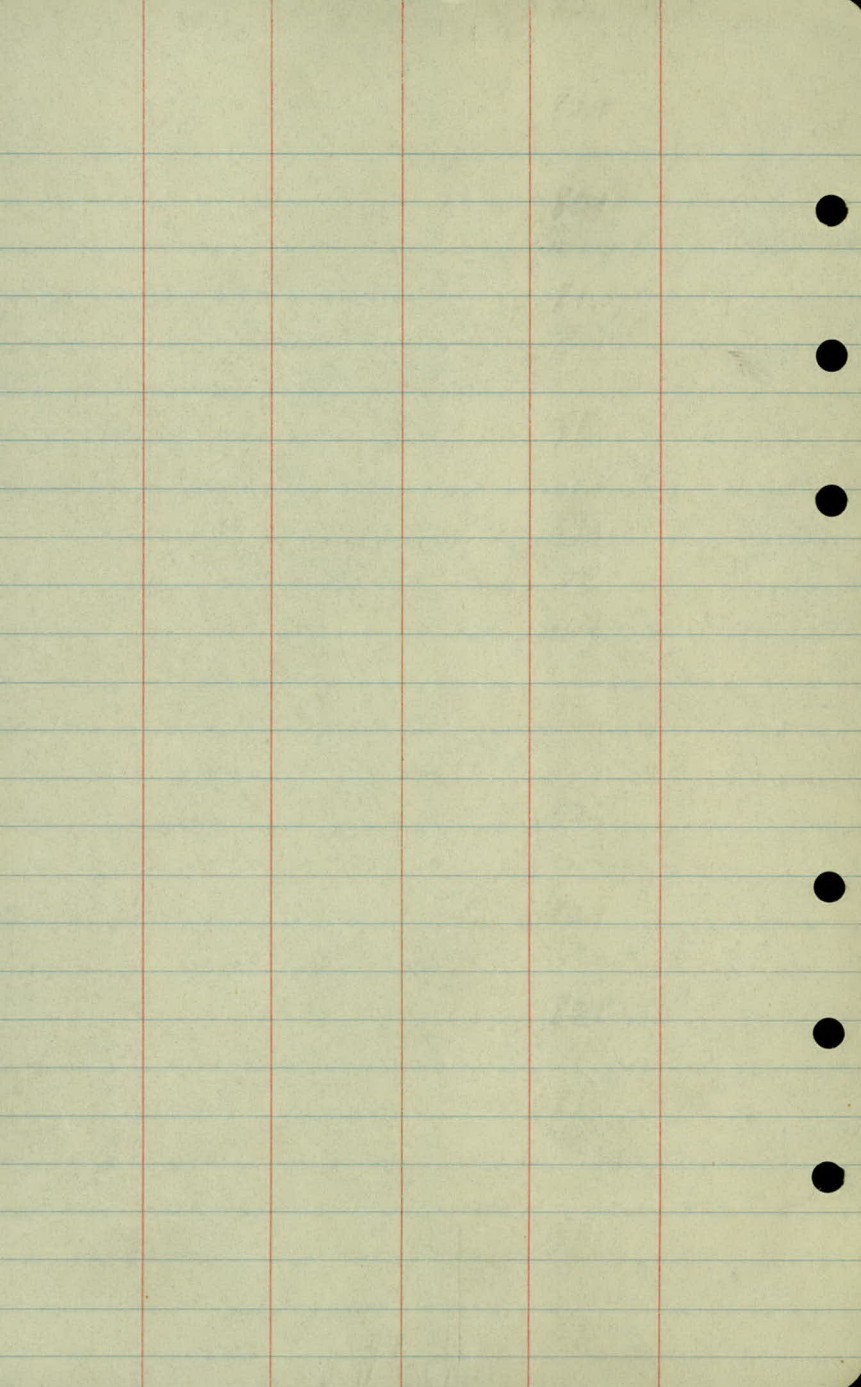
81.4

$$\frac{124}{50}$$

81.2

$$\frac{124}{50}$$

Spk. 172 PP N.E. Cor. Co. Rd. "D" 2" + Lindig Rd.



Lindig Road

Slope stakes from
Carpenter Av. to Co. Rd. A.2

7/38

26' Crown

15' Ditch

20' to Ditch Back Slope

Fills 3:1

Cuts 2:1

Use 4:1 Backslope Sts. 23 to 26+25

Sta	+	K	-	Grade
B.M.	4.93	979.21		974.28

+22				73.9
-----	--	--	--	------

+27				
-----	--	--	--	--

+31				
-----	--	--	--	--

+35				
-----	--	--	--	--

+50				73.9
-----	--	--	--	------

1+00				74.0
------	--	--	--	------

+50				74.1
-----	--	--	--	------

2				74.1
---	--	--	--	------

+50				74.2
-----	--	--	--	------

3				74.2
---	--	--	--	------

+50				74.3
-----	--	--	--	------

Lt.

E

Rt.

E Hole in Brooment

$$\begin{array}{r} 5.3 \\ 6.8 \end{array}$$

$$\begin{array}{r} 5.3 \\ DC1.1 \\ \hline 23.5 \end{array}$$

$$\begin{array}{r} 5.8 \\ FO.5 \end{array}$$

$$\begin{array}{r} 5.4 \\ DC1.4 \\ \hline 23.3 \end{array}$$

$$\begin{array}{r} 5.2 \\ 6.7 \end{array}$$

$$\begin{array}{r} 5.5 \\ DC1.2 \\ \hline 22.7 \end{array}$$

$$\begin{array}{r} 5.7 \\ FO.5 \end{array}$$

$$\begin{array}{r} 5.1 \\ DC1.6 \\ \hline 23.7 \end{array}$$

$$\begin{array}{r} 5.1 \\ 6.6 \end{array}$$

$$\begin{array}{r} 5.4 \\ DC1.2 \\ \hline 22.9 \end{array}$$

$$\begin{array}{r} 5.6 \\ FO.5 \end{array}$$

$$\begin{array}{r} 5.0 \\ DC1.6 \\ \hline 23.7 \end{array}$$

$$\begin{array}{r} 5.1 \\ 6.6 \end{array}$$

$$\begin{array}{r} 5.1 \\ DC1.5 \\ \hline 23.5 \end{array}$$

$$\begin{array}{r} 5.3 \\ FO.5 \end{array}$$

$$\begin{array}{r} 5.2 \\ DC1.4 \\ \hline 23.3 \end{array}$$

$$\begin{array}{r} 5.0 \\ 6.5 \end{array}$$

$$\begin{array}{r} 4.9 \\ DC1.6 \\ \hline 23.7 \end{array}$$

$$\begin{array}{r} 5.1 \\ FO.5 \end{array}$$

$$\begin{array}{r} 5.3 \\ DC1.2 \\ \hline 22.9 \end{array}$$

$$\begin{array}{r} 5.0 \\ 6.5 \end{array}$$

$$\begin{array}{r} 4.5 \\ DC2.0 \\ \hline 24.5 \end{array}$$

$$\begin{array}{r} 4.8 \\ CO.2 \end{array}$$

$$\begin{array}{r} 5.0 \\ DC1.5 \\ \hline 23.5 \end{array}$$

$$\begin{array}{r} 4.9 \\ 6.4 \end{array}$$

$$\begin{array}{r} 4.3 \\ DC2.2 \\ \hline 24.7 \end{array}$$

$$\begin{array}{r} 4.8 \\ CO.1 \end{array}$$

$$\begin{array}{r} 4.6 \\ DC1.8 \\ \hline 24.1 \end{array}$$

Sta.	+	K	-	Grade
		979.21		

4				74.3
---	--	--	--	------

+50				74.4
-----	--	--	--	------

5				74.4
---	--	--	--	------

T.P.	6.22	980.08	5.35	973.86
------	------	--------	------	--------

+50				74.5
-----	--	--	--	------

6				74.5
---	--	--	--	------

+50				74.6
-----	--	--	--	------

7				74.6
---	--	--	--	------

+50				74.7
-----	--	--	--	------

Lt.

E

Et.

4.9
6.4
$$\begin{array}{r} 5.3 \\ DC.1.1 \\ \hline 22.7 \end{array}$$

$$\begin{array}{r} 5.1 \\ F.0.2 \\ \hline \end{array}$$

$$\begin{array}{r} 4.6 \\ DC.1.8 \\ \hline 24.1 \end{array}$$
4.8
6.3
$$\begin{array}{r} 6.0 \\ DC.0.3 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 5.7 \\ F.0.9 \\ \hline \end{array}$$

$$\begin{array}{r} 5.4 \\ DC.0.9 \\ \hline 22.3 \end{array}$$
4.8
6.3
$$\begin{array}{r} 6.0 \\ DC.0.3 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 5.8 \\ F.1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 5.6 \\ DC.0.7 \\ \hline 21.9 \end{array}$$
5.6
7.1
$$\begin{array}{r} 6.8 \\ DC.0.3 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 6.6 \\ F.1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 6.5 \\ DC.0.6 \\ \hline 21.7 \end{array}$$
5.6
7.1
$$\begin{array}{r} 6.7 \\ DC.0.4 \\ \hline 21.3 \end{array}$$

$$\begin{array}{r} 6.6 \\ F.1.0 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ DC.1.7 \\ \hline 21.9 \end{array}$$
5.5
7.0
$$\begin{array}{r} 5.7 \\ DC.1.3 \\ \hline 22.1 \end{array}$$

$$\begin{array}{r} 5.6 \\ F.0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.5 \\ DC.1.5 \\ \hline 23.5 \end{array}$$
5.5
7.0
$$\begin{array}{r} 4.9 \\ DC.2.1 \\ \hline 24.7 \end{array}$$

$$\begin{array}{r} 4.9 \\ C.0.6 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ DC.2.1 \\ \hline 24.7 \end{array}$$
5.4
6.9
$$\begin{array}{r} 4.4 \\ DC.2.1 \\ \hline 24.7 \end{array}$$

$$\begin{array}{r} 4.9 \\ C.0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 4.7 \\ DC.2.2 \\ \hline 24.7 \end{array}$$

2/42471

Sta.	+	π	-	Grade
------	---	-------	---	-------

		980.08		
--	--	--------	--	--

8				74.8
---	--	--	--	------

+50				75.0
-----	--	--	--	------

9				75.3
---	--	--	--	------

+50				75.6
-----	--	--	--	------

10				75.9
----	--	--	--	------

+50				76.2
-----	--	--	--	------

11				76.5
----	--	--	--	------

T.P.	8.48	988.71	5.85	974.23
------	------	--------	------	--------

+50				76.8
-----	--	--	--	------

Lx.

E

Cx.

$$\begin{array}{r} 5.3 \\ 6.8 \end{array}$$

$$\begin{array}{r} 4.5 \\ PG 23 \\ \hline 24.1 \end{array}$$

$$\begin{array}{r} 4.9 \\ F.0.4 \\ \hline \end{array}$$

$$\begin{array}{r} 4.8 \\ PG 20 \\ \hline 24.5 \end{array}$$

$$\begin{array}{r} 5.1 \\ 6.6 \end{array}$$

$$\begin{array}{r} 4.7 \\ PG 1.9 \\ \hline 24.3 \end{array}$$

$$\begin{array}{r} 5.2 \\ F.0.1 \\ \hline \end{array}$$

$$\begin{array}{r} 5.1 \\ PG 1.5 \\ \hline 23.1 \end{array}$$

$$\begin{array}{r} 4.8 \\ 6.3 \end{array}$$

$$\begin{array}{r} 6.1 \\ PG 0.2 \\ \hline 20.9 \end{array}$$

$$\begin{array}{r} 6.6 \\ F.1.8 \\ \hline \end{array}$$

$$\begin{array}{r} 6.4 \\ PG 0.00 \\ \hline 20.5 \end{array}$$

$$\begin{array}{r} 4.5 \\ 6.0 \end{array}$$

$$\begin{array}{r} 7.0 \\ F.2.5 \\ \hline 20.1 \end{array}$$

$$\begin{array}{r} 7.2 \\ F.2.7 \\ \hline \end{array}$$

$$\begin{array}{r} 7.3 \\ F.2.8 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 4.2 \\ 5.7 \end{array}$$

$$\begin{array}{r} 6.9 \\ F.2.3 \\ \hline 21.1 \end{array}$$

$$\begin{array}{r} 7.2 \\ F.3.0 \\ \hline \end{array}$$

$$\begin{array}{r} 7.4 \\ F.3.2 \\ \hline 22.5 \end{array}$$

$$\begin{array}{r} 3.9 \\ 5.4 \end{array}$$

$$\begin{array}{r} 7.0 \\ F.3.1 \\ \hline 22.3 \end{array}$$

$$\begin{array}{r} 7.3 \\ F.3.4 \\ \hline \end{array}$$

$$\begin{array}{r} 7.4 \\ F.3.5 \\ \hline 23.1 \end{array}$$

$$\begin{array}{r} 3.6 \\ 5.1 \end{array}$$

$$\begin{array}{r} 6.4 \\ F.2.8 \\ \hline 21.4 \end{array}$$

$$\begin{array}{r} 6.8 \\ F.3.2 \\ \hline \end{array}$$

$$\begin{array}{r} 6.8 \\ F.3.2 \\ \hline 22.6 \end{array}$$

$$\begin{array}{r} 5.9 \end{array}$$

$$\begin{array}{r} 8.0 \\ F.2.9 \\ \hline 19.1 \end{array}$$

$$\begin{array}{r} 8.3 \\ F.2.4 \\ \hline \end{array}$$

$$\begin{array}{r} 8.3 \\ F.2.4 \\ \hline 20.2 \end{array}$$

Sta. + π - Grade

982.71

12 77.1

+50 77.4

13 77.7

+50 78.0

14 78.3

B.M. 3.86 982.71 3.86 978.85 ^{OK} (978.84)

+50 78.6

15 78.9

+50 79.2

Lt.

E

Rt.

$$\begin{array}{r} 5.6 \\ 7.1 \end{array}$$

$$\begin{array}{r} 6.5 \\ DC.0.6 \\ 21.7 \end{array}$$

$$\begin{array}{r} 6.7 \\ F.1.1 \end{array}$$

$$\begin{array}{r} 7.0 \\ DC.0.1 \\ 20.7 \end{array}$$

$$\begin{array}{r} 5.3 \\ 6.8 \end{array}$$

$$\begin{array}{r} 5.7 \\ DC.1.1 \\ 22.7 \end{array}$$

$$\begin{array}{r} 6.1 \\ F.0.8 \end{array}$$

$$\begin{array}{r} 6.4 \\ DC.0.4 \\ 21.3 \end{array}$$

$$\begin{array}{r} 5.0 \\ 4.5 \end{array}$$

$$\begin{array}{r} 5.1 \\ DC.1.4 \\ 22.3 \end{array}$$

$$\begin{array}{r} 5.5 \\ F.0.5 \end{array}$$

$$\begin{array}{r} 5.8 \\ DC.0.7 \\ 21.9 \end{array}$$

$$\begin{array}{r} 4.7 \\ 6.2 \end{array}$$

$$\begin{array}{r} 4.9 \\ DC.1.3 \\ 23.1 \end{array}$$

$$\begin{array}{r} 5.4 \\ F.0.7 \end{array}$$

$$\begin{array}{r} 5.7 \\ DC.0.5 \\ 21.5 \end{array}$$

$$\begin{array}{r} 4.4 \\ 5.9 \end{array}$$

$$\begin{array}{r} 4.8 \\ DC.1.1 \\ 22.7 \end{array}$$

$$\begin{array}{r} 5.1 \\ F.0.7 \end{array}$$

$$\begin{array}{r} 5.5 \\ DC.0.4 \\ 21.3 \end{array}$$

Top of iron pipe 25' Lt 13+17

$$\begin{array}{r} 4.1 \\ 5.6 \end{array}$$

$$\begin{array}{r} 4.5 \\ DC.1.1 \\ 22.7 \end{array}$$

$$\begin{array}{r} 4.7 \\ F.0.6 \end{array}$$

$$\begin{array}{r} 5.3 \\ DC.0.3 \\ 21.1 \end{array}$$

$$\begin{array}{r} 3.8 \\ 5.3 \end{array}$$

$$\begin{array}{r} 4.4 \\ DC.1.1 \\ 22.7 \end{array}$$

$$\begin{array}{r} 4.4 \\ F.0.6 \end{array}$$

$$\begin{array}{r} 5.0 \\ DC.0.3 \\ 21.1 \end{array}$$

$$\begin{array}{r} 3.5 \\ 5.0 \end{array}$$

$$\begin{array}{r} 3.4 \\ DC.1.6 \\ 23.7 \end{array}$$

$$\begin{array}{r} 4.2 \\ F.0.7 \end{array}$$

$$\begin{array}{r} 4.9 \\ DC.0.1 \\ 20.7 \end{array}$$

Sta. + π - Grade

984.71

16 79.5

T.P. 5.84 985.21 3.34 979.37

+50 79.8

17 80.1

+50 80.4

18 80.7

+50 81.0

19 81.3

+67 81.7

4.

2

8.

$$\begin{array}{r} 32 \\ 4.7 \end{array}$$

$$\begin{array}{r} 31 \\ DC16 \\ 23.7 \end{array}$$

$$\begin{array}{r} 4.0 \\ F0.8 \end{array}$$

$$\begin{array}{r} 49 \\ F17 \\ 18.1 \end{array}$$

$$\begin{array}{r} 5.4 \\ 6.9 \end{array}$$

$$\begin{array}{r} 52 \\ DC17.9 \\ 23.1 \end{array}$$

$$\begin{array}{r} 6.1 \\ F0.7 \end{array}$$

$$\begin{array}{r} 7.2 \\ F18 \\ 18.4 \end{array}$$

$$\begin{array}{r} 5.1 \\ 6.6 \end{array}$$

$$\begin{array}{r} 46 \\ DC20 \\ 24.1 \end{array}$$

$$\begin{array}{r} 5.6 \\ F0.5 \end{array}$$

$$\begin{array}{r} 6.1 \\ DC0.1 \\ 20.7 \end{array}$$

$$\begin{array}{r} RW \\ 24.7 \end{array}$$

$$\begin{array}{r} 4.8 \\ 6.3 \end{array}$$

$$\begin{array}{r} 39 \\ DC24 \\ 24.7 \end{array}$$

$$\begin{array}{r} 5.1 \\ F0.3 \end{array}$$

$$\begin{array}{r} 6.1 \\ DC0.7 \\ 20.9 \end{array}$$

$$\begin{array}{r} 4.5 \\ 6.0 \end{array}$$

$$\begin{array}{r} 38 \\ DC22 \\ 24.7 \end{array}$$

$$\begin{array}{r} 5.0 \\ F0.1 \end{array}$$

$$\begin{array}{r} 6.0 \\ F15 \\ 17.1 \end{array}$$

$$\begin{array}{r} 4.8 \\ 5.7 \end{array}$$

$$\begin{array}{r} 45 \\ DC12 \\ 22.9 \end{array}$$

$$\begin{array}{r} 5.9 \\ F1.7 \end{array}$$

$$\begin{array}{r} 7.0 \\ F.28 \\ 21.4 \end{array}$$

$$\begin{array}{r} 3.9 \\ 5.4 \end{array}$$

$$\begin{array}{r} 5.2 \\ DC0.2 \\ 20.9 \end{array}$$

$$\begin{array}{r} 6.3 \\ F.24 \end{array}$$

$$\begin{array}{r} 7.3 \\ F38 \\ 24.4 \end{array}$$

$$\begin{array}{r} 3.5 \\ 5.0 \end{array}$$

$$\begin{array}{r} 6.7 \\ F.27 \\ 21.1 \end{array}$$

$$\begin{array}{r} 7.0 \\ F.35 \end{array}$$

$$\begin{array}{r} 7.6 \\ F.41 \\ 24.7 \end{array}$$

Sta.	+	π	-	Grade.
		985.21		

20				81.9
----	--	--	--	------

+50				82.2
-----	--	--	--	------

21				82.5
----	--	--	--	------

+50				82.8
-----	--	--	--	------

T.P.	9.45	991.28	3.38	981.83
------	------	--------	------	--------

22				83.1
----	--	--	--	------

+50				83.4
-----	--	--	--	------

23				83.7
----	--	--	--	------

+50				84.0
-----	--	--	--	------

Elevation
 18.4 ft.

4161
 slopes

4.

2

et.

3.3
4.8

4.7
DCO¹
20.7

5.7
F.2.4

5.7
F.2.2
22.6

3.0
4.5

3.4
DCO¹
22.7

4.3
F.1.3

5.2
F.2.2
19.6

2.7
4.2

2.9
DCO¹
23.1

3.6
0.9

4.3
F.1.6
17.8

2.4
3.9

3.3
DCO²
21.7

3.8
F.1.4

4.4
F.2.0
19.0

8.2
9.7

7.6
DCO¹
20.7

10.2
F.2.0

10.5
F.2.3
19.9

7.9
9.4

9.3
DCO¹
20.7

9.8
F.1.9

10.2
F.2.3
19.9

7.6
9.1

2.8
DCO¹
25.7

8.2
F.0.6

8.7
DCO²
21.7

7.3
8.8

5.3
DCO¹
34.1

4.4
F.1.1
C

6.8
DCO²
18.0

Sta.	+	π	-	Grade
------	---	-------	---	-------

991.78

24

84.1

+30

84.0

T.P.

4.39

993.36

2.31

988.97

+50

83.9

+75

83.6

25

83.3

+50

82.3

26

81.2

+14

80.8

Exponent 24.84
4:1 Slopes

47.

2

47.

$$\begin{array}{r} 15 \\ 47 \quad 7.2 \\ 8.7 \end{array}$$

$$\begin{array}{r} 29 \\ 06.18 \\ 43.1 \end{array}$$

$$\begin{array}{r} 30 \\ 64.2 \end{array}$$

$$\begin{array}{r} 35 \\ 06.17 \\ 41.3 \end{array}$$

$$\begin{array}{r} 15 \\ 7.3 \\ 8.8 \end{array}$$

$$\begin{array}{r} 21 \\ 06.67 \\ 47.3 \end{array}$$

$$\begin{array}{r} 0.7 \\ 6.66 \end{array}$$

$$\begin{array}{r} 14 \\ 06.74 \\ 50.1 \end{array}$$

53

$$\begin{array}{r} 15 \\ 47 \quad 9.5 \\ 11.0 \end{array}$$

$$\begin{array}{r} 48 \\ 06.67 \\ 45.3 \end{array}$$

$$\begin{array}{r} 21 \\ 7.4 \end{array}$$

$$\begin{array}{r} 27 \\ 06.83 \\ 53.7 \end{array}$$

57

$$\begin{array}{r} 9.8 \\ 11.3 \end{array}$$

$$\begin{array}{r} 6.2 \\ 06.51 \\ 46.9 \end{array}$$

$$\begin{array}{r} 38 \\ 6.60 \end{array}$$

$$\begin{array}{r} 24 \\ 06.89 \\ 52.1 \end{array}$$

57

$$\begin{array}{r} 10.1 \\ 11.6 \end{array}$$

$$\begin{array}{r} 28 \\ 63.8 \\ 31.7 \end{array}$$

$$\begin{array}{r} 6.5 \\ 3.6 \end{array}$$

$$\begin{array}{r} 40 \\ 67.6 \\ 50.9 \end{array}$$

$$\begin{array}{r} 11.1 \\ 12.6 \end{array}$$

$$\begin{array}{r} 10.5 \\ 06.21 \\ 38.9 \end{array}$$

$$\begin{array}{r} 10.2 \\ 60.9 \end{array}$$

$$\begin{array}{r} 55 \\ 06.31 \\ 52.9 \end{array}$$

$$\begin{array}{r} 12.2 \\ 13.7 \end{array}$$

$$\begin{array}{r} 12.7 \\ 06.10 \\ 24.7 \end{array}$$

$$\begin{array}{r} 12.6 \\ 60.4 \end{array}$$

$$\begin{array}{r} 12.6 \\ 06.11 \\ 24.7 \end{array}$$

$$\begin{array}{r} 12.6 \\ 14.1 \end{array}$$

Sta. + K - Grade.

993.36

26+22

80.64

+34.25

81.2

B.M.

13.26 980.10 980.10

Lt.

£

Rt.

Spike in P.P.; N.E. Cor. A.² + Lindig Rd.

5/12

+

π

-

Grade

Slope Stakes
Lindig Rd.
Grade Revision

5 Pages

Sta	+	π	-	Grade
B.M.	0.24	979.08		978.84
8	+50			74.9
9				75.1
	+50			75.3
10				75.5
	+50			75.7
11				75.9
	+50			76.1
12				76.3
	+50			76.5
13				76.7
B.M.	3.54	984.32	0.24	978.84
	+50			76.9

1

Top Iron Pipe ^{24.75'} 25' Lt 13 + 17.35

$$\begin{array}{r} 7.5 \\ 253 \overline{) 10.9} \\ \underline{10.5} \\ 0.4 \end{array}$$

Sta.	+	π	-	Grade
		789.88		
14				77.1
	+50			77.3
15				77.5
	+50			77.7
16				77.9
	+50			78.1
17				78.3
	+50			78.5
18				78.7
	+50			78.9
T.P.	6.67	789.31	479	979.64
19				79.1

ht: 0.0 = 20.5
cut 06 = 29.5

1.7
2
34

2

Gr Rod

ht

ht

ht

$$7.3 \quad \frac{248}{+0.7} \quad \frac{68}{+0.6} \quad \frac{72}{+0.1/23.7}$$

$$7.1 \quad \frac{253}{+0.9} \quad \frac{64}{+0.7} \quad \frac{69}{+0.2/23.9}$$

$$6.9 \quad \frac{255}{+1.0} \quad \frac{61}{+0.8} \quad \frac{67}{+0.2/23.9}$$

$$6.7 \quad \frac{265}{+1.0} \quad \frac{59}{+0.8} \quad \frac{66}{+0.1/23.7}$$

$$6.5 \quad \frac{26.9}{+1.6} \quad \frac{57}{+0.8} \quad \frac{68}{+0.2/23.9}$$

$$6.3 \quad \frac{27.5}{+1.0} \quad \frac{55}{+1.0} \quad \frac{65}{+0.3/23.1}$$

$$6.1 \quad \frac{27.7}{+1.1} \quad \frac{58}{+1.3} \quad \frac{59}{+0.2/23.9}$$

$$5.9 \quad \frac{94}{+1.5} \quad \frac{54}{+0.5/24.5}$$

$$5.7 \quad \frac{28.5}{+1.5} \quad \frac{52}{+1.5} \quad \frac{53}{+0.4/24.3}$$

$$5.5 \quad \frac{27.1}{+1.8} \quad \frac{50}{+0.5} \quad \frac{62}{+0.2/22.1}$$

$$5.2 \quad \frac{25.5}{+1.0} \quad \frac{74}{-0.2} \quad \frac{85}{+0.2/20.9}$$

Sta

t

x

-

Grade

986.31

19

+67

79.5

20

79.7

+50

80.1

21

80.6

+50

81.2

22

81.7

+50

82.3

23

82.8

+50

83.4

T.P.

8.28

999.53

1.06

985.25

24

83.7

+30

83.7

$$20.00 = 20.5$$

$$20.40 = 20.5$$

$$20.40 = 20.5$$

Cor. Rod

Lt

Rt

Pt.

$$6.8 \quad 22.7 / \frac{7.2}{25.11} \quad \frac{80}{12} \quad \frac{8.6}{1.8} / 15.9$$

$$6.6 \quad 25.3 / \frac{5.7}{10.9} \quad \frac{6.9}{-0.3} \quad \frac{7.6}{2.05} / 21.5$$

$$6.2 \quad 26.5 / \frac{4.7}{11.5} \quad \frac{5.5}{10.7} \quad \frac{6.5}{2.12} / 22.9$$

$$5.7 \quad 26.5 / \frac{4.2}{11.5} \quad \frac{4.7}{11.0} \quad \frac{5.7}{10.0} / 23.5$$

$$5.1 \quad 28.9 / \frac{4.4}{10.7} \quad \frac{4.9}{-0.2} \quad \frac{5.6}{2.10} / 22.5$$

$$4.6 \quad 22.5 / \frac{4.6}{10.0} \quad \frac{5.2}{-0.6} \quad \frac{5.6}{2.05} / 26.5$$

$$4.0 \quad 23.8 / \frac{4.4}{10.0} \quad \frac{4.5}{-0.5} \quad \frac{5.1}{2.05} / 21.7$$

$$3.5 \quad 28.9 / \frac{2.9}{10.6} \quad \frac{3.2}{10.3} \quad \frac{4.9}{2.11} / 29.9$$

$$2.9 \quad 37.7 / \frac{0.1}{12.8} \quad \frac{0.8}{12.1} \quad \frac{1.7}{4.2} / 11.3$$

$$2.8 \quad 44.9 / \frac{5.2}{14.6} \quad \frac{5.2}{14.6} \quad \frac{5.7}{14.1} / 42.9$$

$$2.8 \quad 48.1 / \frac{4.4}{15.9} \quad \frac{2.9}{16.9} \quad \frac{3.6}{16.2} / 51.3$$

4:11 East Slopes

Sta	+	π	-	Grade
-----	---	-------	---	-------

792.53

24	+50	83.6
----	-----	------

175			834
-----	--	--	-----

25				83.1
----	--	--	--	------

150				82.3
-----	--	--	--	------

26				81.2
----	--	--	--	------

714				80.8
-----	--	--	--	------

122				80.67
-----	--	--	--	-------

B.M.	13.39	980.14	980.10
------	-------	--------	--------

Cor. Root

Lt.

Rt.

Rt.

9.9

$$457 / \frac{51}{198}$$

$$\frac{22}{177}$$

$$\frac{28}{21} / 54.9$$

10.1

$$41.7 / \frac{6.3}{158}$$

$$\frac{40}{161}$$

$$\frac{26}{25} / 56.5$$

10.4

$$36.9 / \frac{2.8}{126}$$

$$\frac{66}{158}$$

$$\frac{42}{162} / 51.3$$

11.2

$$28.9 / \frac{10.9}{106}$$

$$\frac{103}{109}$$

$$\frac{97}{115} / 32.5$$

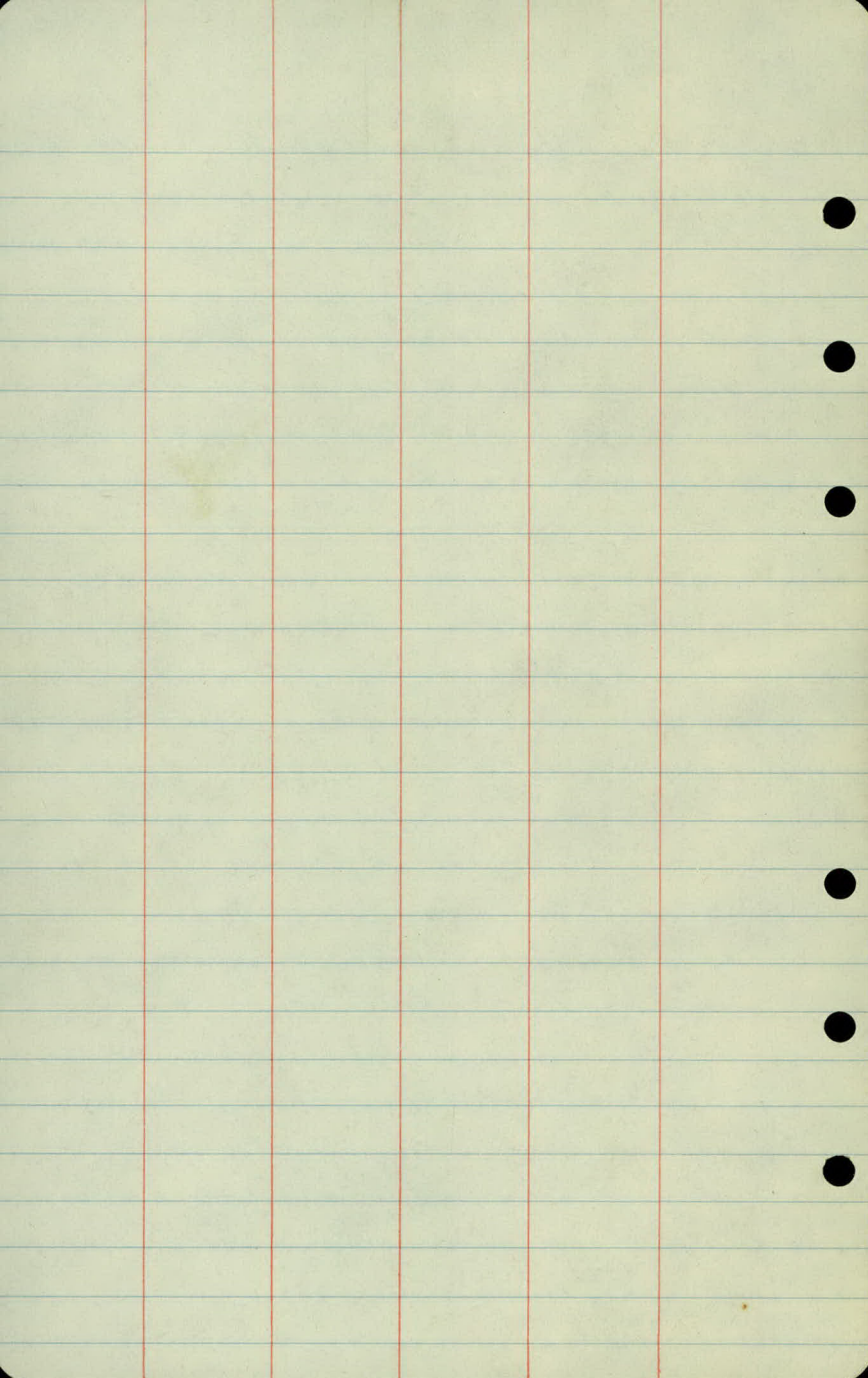
12.3

$$24.9 / \frac{12.7}{111}$$

$$\frac{128}{95}$$

$$\frac{12.7}{2.1} / 24.9$$

Spk. in PP. NE Cor "H²" + Lindig Rd



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