

Dr. 11 - Bk. 29

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

CROSS ROADS COURT

NEAR

From

Larpenteur & Snelling

Holly Brook Court

Road Acc't. No.

Date Filed

File

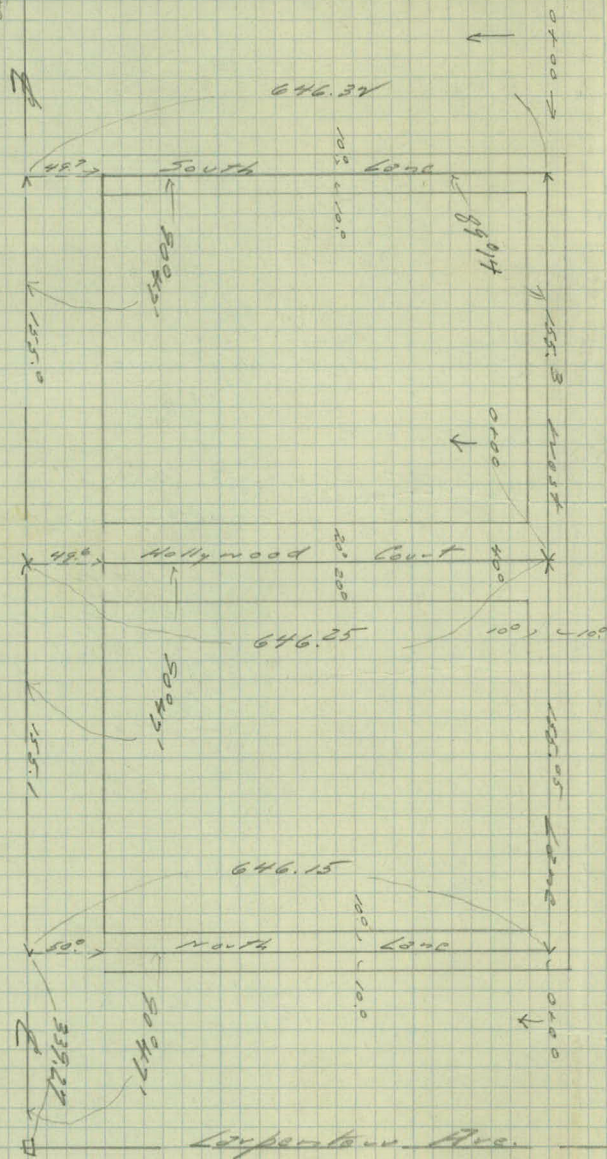
1

CROSS ROADS COURT

For Street Grades.

Street Layout based on
Existing Property Lines.

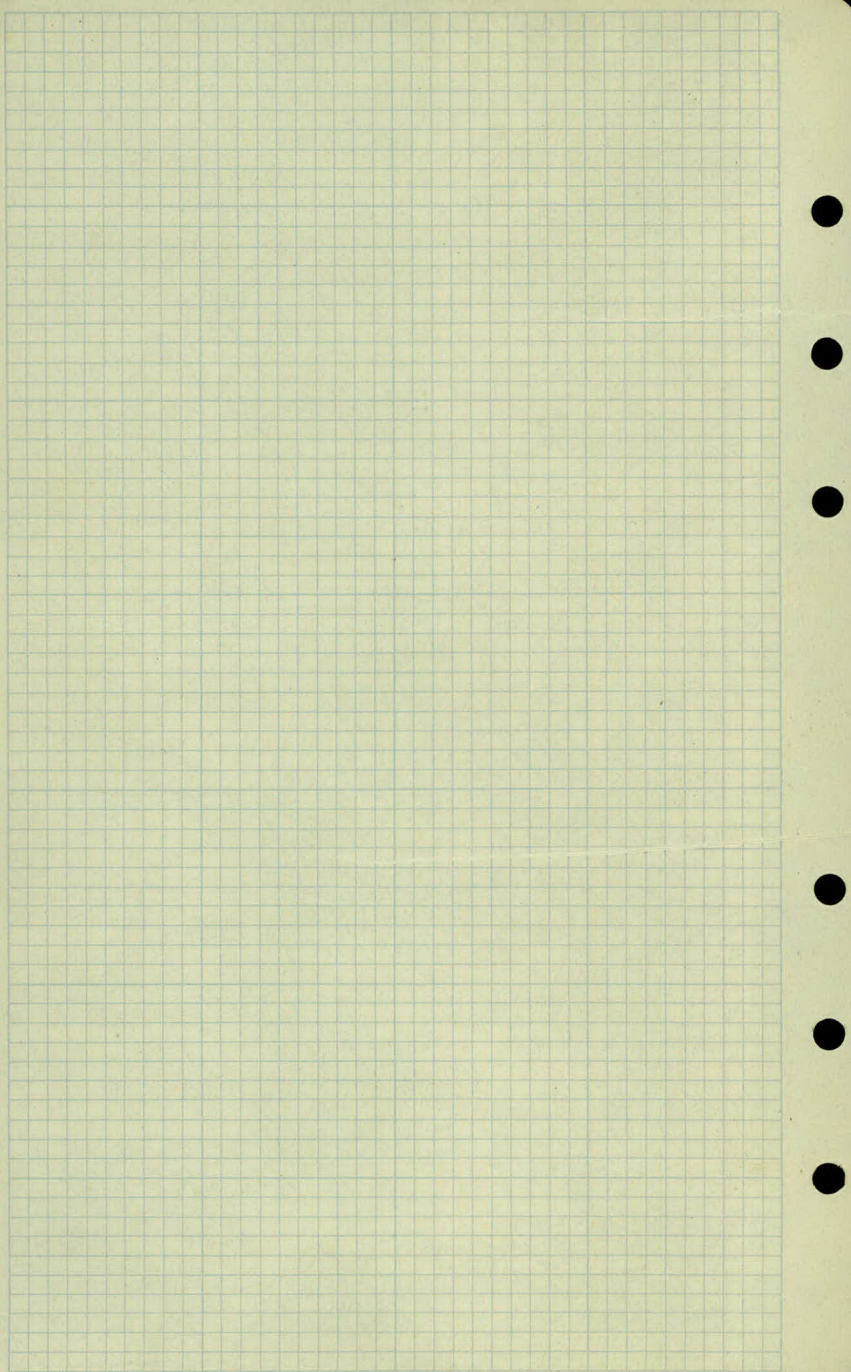
A. Bratager
H. Wiike
L. Goldberg
A. Moschter



North

John May

Cross Roads Court.



Hollywood Court.

Bratger
Witte
Goldberg
Moeschter

8/1/28

2

5

+91 Mock Orange Bush 12°

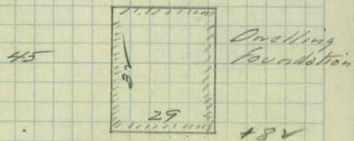
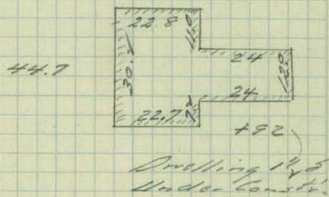
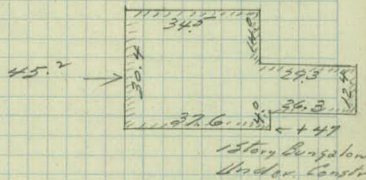
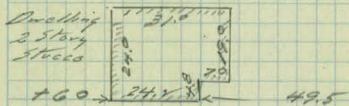
+75 Water shut off 20°

+60 Mock Orange Bush 12°

+51 Water shut off 14°

4

3



2

6+00

+60 Water Shut off 20.5

+64 Water Shut off 2.0

+04-Bush on 2 5' Dia.
5+00

40 ft. blacktop on concrete base.

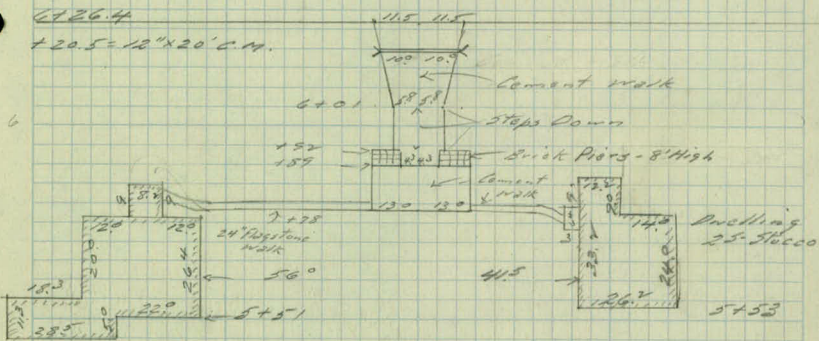
Drivelling
 2+46.25

Avenue

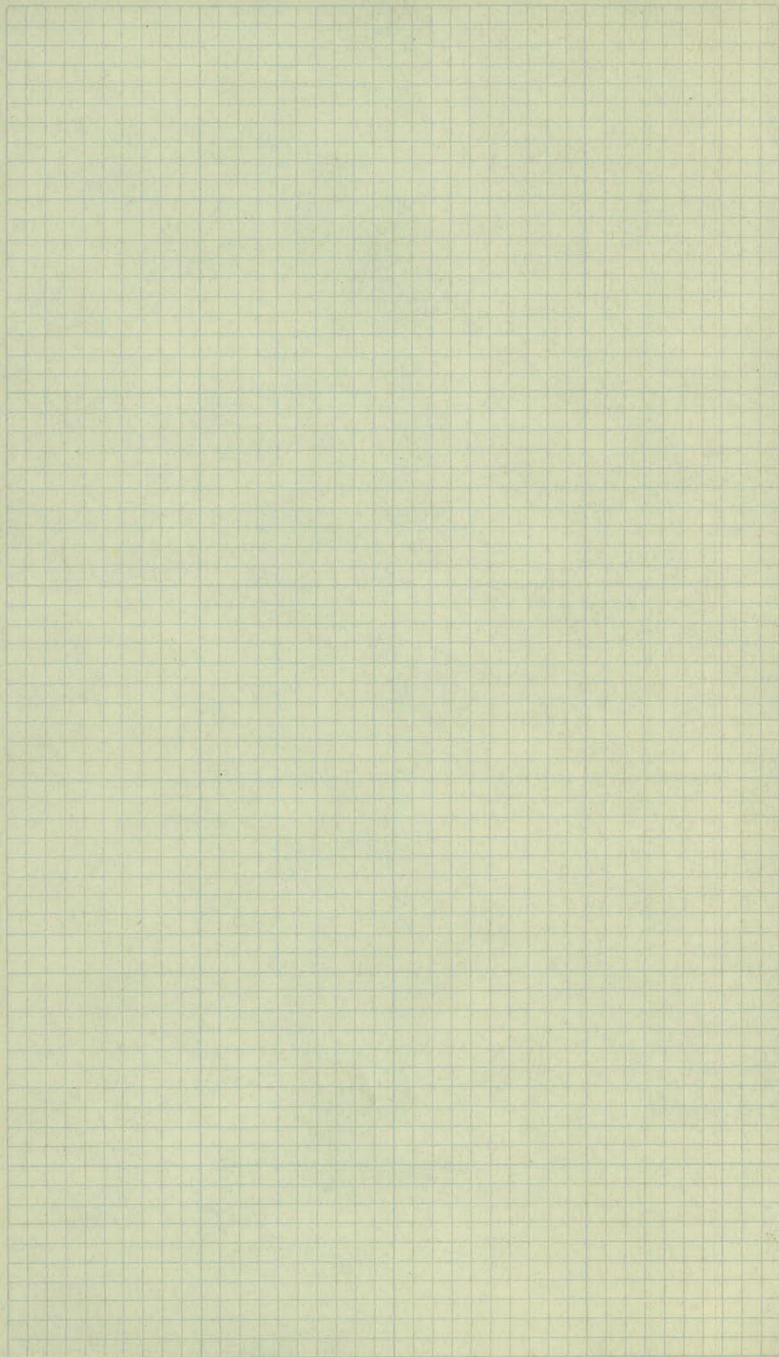


2+26.4

+20.5 = 12" x 20' C.M.



Drivelling
 25 foot frame



Hollywood Court.

6/1/38

Sta.	+	π	-	Elev.
------	---	-------	---	-------

B.M.	2.64	960.17 ✓		957.48 ✓
------	------	----------	--	----------

0-17				49.4
------	--	--	--	------

0-7				49.4
-----	--	--	--	------

0-5				48.0
-----	--	--	--	------

0+00				48.1
------	--	--	--	------

0+09				48.1
------	--	--	--	------

0+11				49.4
------	--	--	--	------

0+50				49.1
------	--	--	--	------

1+00				49.5
------	--	--	--	------

+50				50.6
-----	--	--	--	------

2+00				52.1
------	--	--	--	------

+50				53.6
-----	--	--	--	------

Lt.

L

Rt.

16

Top of water shut off 7' Rt. Sta. 5+64

$$\frac{10.7}{50}$$

$$\frac{10.5}{50}$$

$$\frac{10.0}{50}$$

$$\frac{10.7}{50}$$

$$\frac{10.5}{50}$$

$$\frac{10.0}{50}$$

$$\frac{10.5}{50}$$

$$\frac{10.5}{45}$$

$$\frac{12.2}{40}$$

$$\frac{12.1}{50}$$

$$\frac{11.3}{50}$$

$$\frac{10.5}{50}$$

$$\frac{10.5}{45}$$

$$\frac{12.2}{40}$$

$$\frac{11.0}{50}$$

$$\frac{11.1}{50}$$

$$\frac{10.5}{50}$$

$$\frac{10.5}{45}$$

$$\frac{12.2}{40}$$

$$\frac{11.0}{50}$$

$$\frac{11.1}{50}$$

$$\frac{10.3}{50}$$

$$\frac{10.7}{50}$$

$$\frac{10.6}{20}$$

$$\frac{11.4}{22}$$

$$\frac{11.5}{50}$$

$$\frac{11.3}{50}$$

$$\frac{11.0}{50}$$

$$\frac{10.7}{20}$$

$$\frac{12.2}{29}$$

$$\frac{11.7}{50}$$

$$\frac{10.9}{50}$$

$$\frac{10.6}{50}$$

$$\frac{10.5}{20}$$

$$\frac{10.9}{24}$$

$$\frac{11.7}{50}$$

$$\frac{9.9}{50}$$

$$\frac{9.5}{50}$$

$$\frac{9.5}{50}$$

$$\frac{8.3}{50}$$

$$\frac{8.6}{36}$$

$$\frac{8.0}{50}$$

$$\frac{8.6}{50}$$

$$\frac{6.5}{50}$$

$$\frac{7.0}{31}$$

$$\frac{6.5}{50}$$

$$\frac{7.1}{50}$$

Sta. + π - Elev.

960.17

3+00

953.8'

3+00 ±

+50

546

4+00

541'

4+00 ±

4+50

540'

+51

4+60 ±

4+75 ±

Lt.

E

Rt.

12

$$\frac{6.0}{50}$$

$$\frac{6.6}{15}$$

$$\frac{6.3}{1}$$

$$\frac{7.0}{21}$$

$$\frac{6.4}{45}$$

Top of Fdn. 45 Rt.

$$\frac{5.1}{1} \quad 955.02$$

$$\frac{5.0}{50}$$

$$\frac{5.5}{1}$$

$$\frac{6.2}{50}$$

$$\frac{5.4}{50}$$

$$\frac{6.0}{1}$$

$$\frac{6.4}{45}$$

{ Floor of Dwelling 45' Rt.
 { Cellar window sill
 { Top of Fdn.

$$\frac{4.65}{1} \quad 55.47$$

$$\frac{7.3}{1} \quad 52.82$$

$$\frac{5.5}{1} \quad 54.62$$

$$\frac{5.6}{50}$$

$$\frac{6.1}{1}$$

$$\frac{6.6}{10}$$

$$\frac{6.5}{46}$$

Water Shot off Corner Rt.

$$\frac{6.7}{1} \quad 58.42$$

Dwelling Rt. 46' Rt.

{ Top Fdn.
 { Cellar Window Sill
 { Floor
 { Present ground at entrance

$$\frac{5.6}{1} \quad 54.52$$

$$\frac{7.75}{1} \quad 52.87$$

$$\frac{5.0}{1} \quad 55.12$$

$$\frac{6.3}{1} \quad 53.82$$

Dwelling Lt.

{ Bottom of steps @ entrance
 { Floor

$$\frac{5.4}{1} \quad 54.72$$

$$\frac{3.2}{1} \quad 56.82$$

Sta.	+	π ✓	-	Elev.
		960.12 ✓		

5+00				53.1 ✓
------	--	--	--	--------

T.P.	4.87	957.35 ✓	7.64	952.48 ✓
------	------	----------	------	----------

+50				52.7
-----	--	--	--	------

+60				
-----	--	--	--	--

+64				
-----	--	--	--	--

+89				52.1
-----	--	--	--	------

6+02 ✓				48.8
--------	--	--	--	------

6+12				48.7
------	--	--	--	------

6+20.5				48.6
--------	--	--	--	------

+22				48.6
-----	--	--	--	------

+26.4				48.7
-------	--	--	--	------

6+46.25				48.8
---------	--	--	--	------

Lt.

Q

Rt.

18

$$\frac{62}{50} \quad \frac{62}{44} \quad \frac{63}{14} \quad \frac{70}{14} \quad \frac{69}{6} \quad \frac{75}{11} \quad \frac{80}{41} \quad \frac{80}{50}$$

$$\frac{30}{50} \quad \frac{36}{23} \quad \frac{47}{11} \quad \frac{47}{11} \quad \frac{50}{11} \quad \frac{44}{20} \quad \frac{41}{42} \quad \frac{41}{50}$$

Water shut off Lt. $\frac{3.90}{53.45}$.

" " " Rt. $\frac{4.87}{52.48}$.

$$\frac{36}{20} \quad \frac{43}{21} \quad \frac{53}{14} \quad \frac{53}{14} \quad \frac{53}{14} \quad \frac{48}{23} \quad \frac{43}{42} \quad \frac{43}{50}$$

$$\frac{42}{20} \quad \frac{45}{24} \quad \frac{50}{9} \quad \frac{87}{5} \quad \frac{86}{5} \quad \frac{86}{5} \quad \frac{53}{10} \quad \frac{53}{50}$$

$$\frac{46}{50} \quad \frac{53}{13} \quad \frac{87}{8} \quad \frac{87}{9} \quad \frac{87}{9} \quad \frac{56}{16} \quad \frac{60}{50}$$

$$\frac{87}{50} \quad \frac{98}{10} \quad \frac{87}{10} \quad \frac{88}{10} \quad \frac{89}{10} \quad \frac{103}{10} \quad \frac{107}{50}$$

$$\frac{78}{50} \quad \frac{88}{50} \quad \frac{100}{50}$$

$$\frac{77}{50} \quad \frac{87}{50} \quad \frac{88}{50}$$

$$\frac{75}{50} \quad \frac{86}{50} \quad \frac{97}{50}$$

Sta. + K - Elev.

957.35

Sta. +

Sta. +

B.M.

4.87

957.48

957.45

Lt.

E

Rt.

19

Dwelling Lt.
Cellar Window Sill

2.8 54.55

Bottom of steps @ entrance
Floor.

2.84 54.5

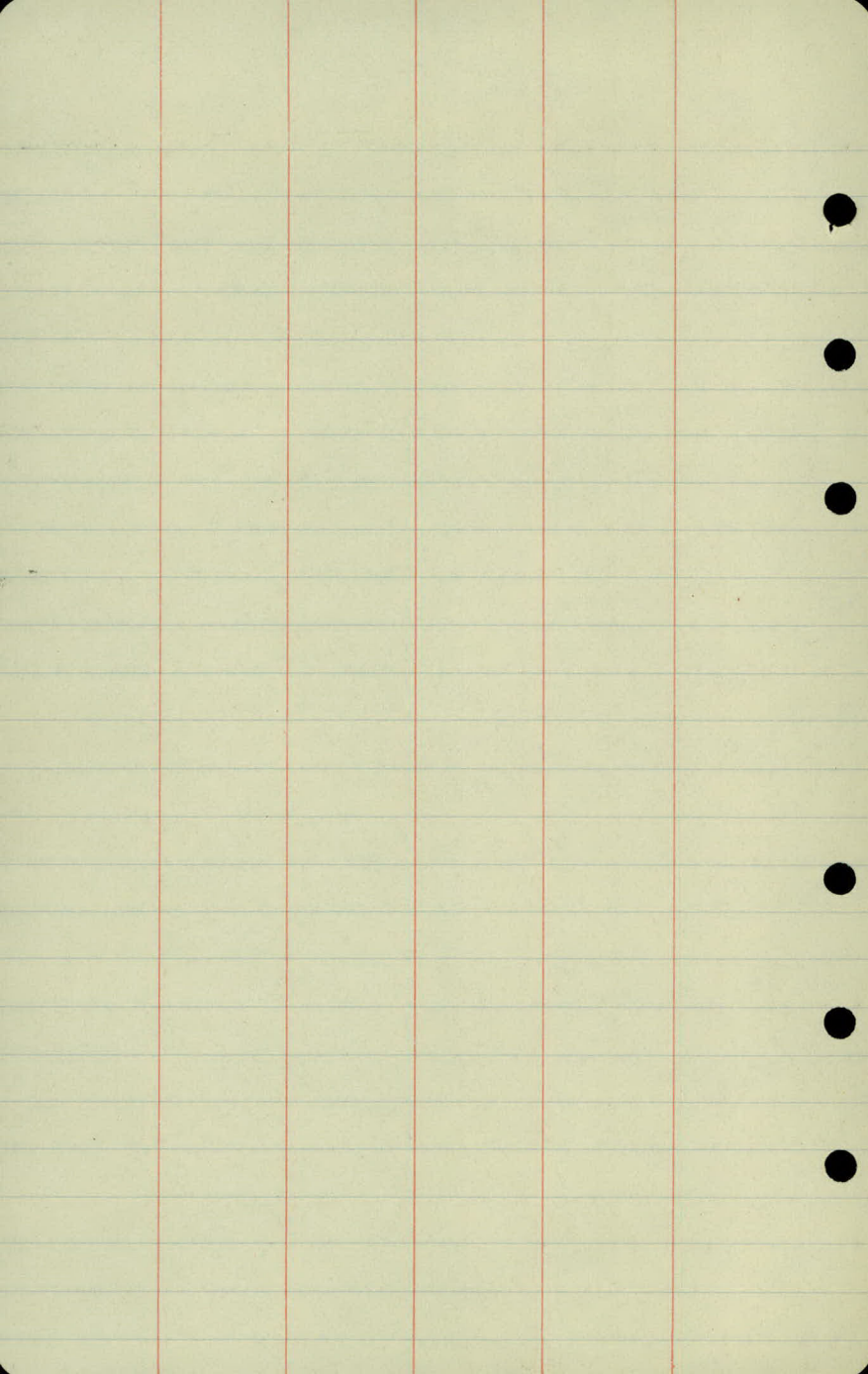
0.50 56.85

Dwelling Rt.

Bottom of entrance steps
Floor.

4.0 53.35

2.15 55.20



South Lane.

6

5

4

3

2

1

0+00

← North.

6

Snelling

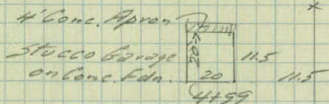
6+46.37

Ave.

6+26.5

+19 = 12" x 30" C.M.

+71 P.P. 9.0



+43 P.P. 9.0

+32 P.P. 9.0

+22 P.P. 9.0

+66 P.P. 9.0

6+26.5

6+11.0

Fence Correlates To Snelling

+20 = 24" Maple 7.5'

+88 = 30" Maple 7.0

+56 = 24" Stump 7.0

+24 = 24" Maple 7.0

+93 = 24" Maple 7.0

+80 = 30" Maple 6.5

Fencing
 { 48" W. W.
 2 B. W.
 Iron Posts @ 13'

2+81 = 20" Maple 6.0

2+42 = 24" Maple 7.5

2+11 = 30" Maple 7.0

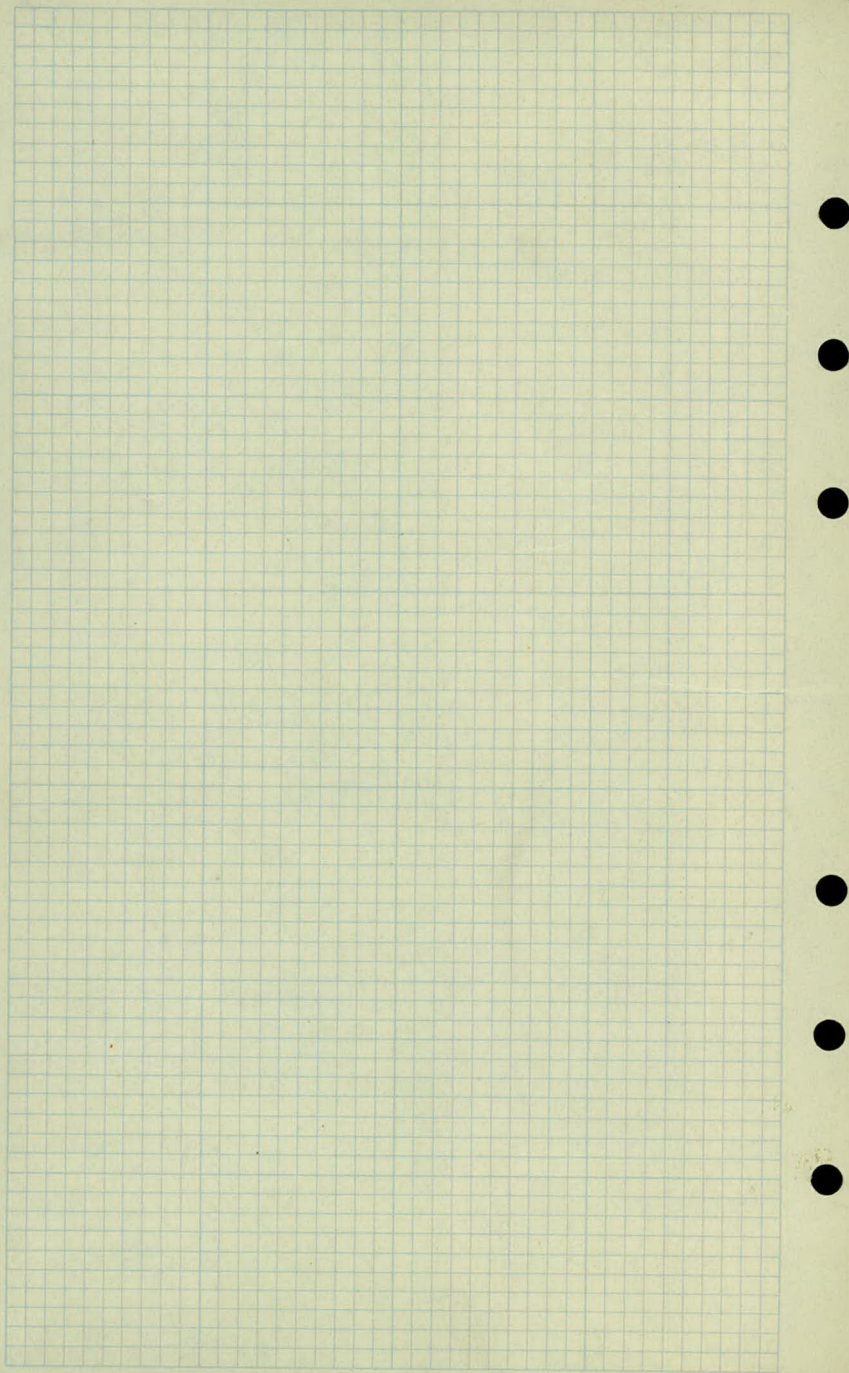
1+78 = 24" Maple 7.0

1+47 = 30" Maple 6.0

1+14 = 36" Maple 6.0

0+49 = 24" Maple 6.5

0+17 = 18" Maple 6.5



11
South Lane.

Cross Sections

H. Bratager

H. Witke

L. Goldberg

H. Moeschter

6/1/35

Sta.	+	π	-	Elev.
B.M.	0.70	957.34		956.64
B.M.	7.01	959.49	4.86	952.48
0+10				951.70
0+00				53.1
0+13				53.2
0+50				53.1
1+00				52.8
T.P.	4.63	958.34	5.78	953.71
1+50				52.7
2				52.5
+50				52.2
3+00				52.1
750				51.8

Lt.

E

Rt.

12

Top of Mon. Snelling & Carpenter Aves.

Top of Water Shut off 7' Rt. Sta 5+64 Hollywood Court

$$\frac{8.2}{50}$$

$$\frac{7.8}{11} \quad \frac{7.6}{14} \quad \frac{8.5}{50}$$

$$\frac{8.5}{50} \quad \frac{8.1}{16} \quad \frac{6.5}{10} \quad \frac{6.4}{5} \quad \frac{7.4}{11} \quad \frac{7.8}{50}$$

$$\frac{8.5}{50} \quad \frac{8.1}{17} \quad \frac{6.7}{13} \quad \frac{6.3}{2} \quad \frac{7.6}{5} \quad \frac{7.6}{11} \quad \frac{8.0}{50}$$

$$\frac{8.5}{50} \quad \frac{7.8}{17} \quad \frac{6.4}{14} \quad \frac{6.4}{3} \quad \frac{6.5}{6} \quad \frac{7.5}{11} \quad \frac{7.6}{50}$$

$$\frac{7.7}{50} \quad \frac{7.0}{16} \quad \frac{6.7}{11} \quad \frac{6.7}{50}$$

Nail in PP

$$\frac{6.2}{50} \quad \frac{5.2}{14} \quad \frac{5.8}{13} \quad \frac{5.6}{2} \quad \frac{5.1}{3} \quad \frac{5.2}{17} \quad \frac{6.0}{27} \quad \frac{6.2}{50}$$

$$\frac{5.5}{50} \quad \frac{5.0}{15} \quad \frac{6.1}{14} \quad \frac{5.7}{5} \quad \frac{5.8}{2} \quad \frac{5.5}{3} \quad \frac{4.8}{17} \quad \frac{5.1}{21} \quad \frac{5.6}{21} \quad \frac{6.5}{50}$$

$$\frac{5.1}{50} \quad \frac{5.2}{15} \quad \frac{6.1}{14} \quad \frac{6.1}{2} \quad \frac{5.9}{2} \quad \frac{5.1}{2} \quad \frac{5.4}{15} \quad \frac{5.7}{19} \quad \frac{6.3}{50}$$

$$\frac{5.3}{50} \quad \frac{5.6}{15} \quad \frac{6.3}{14} \quad \frac{6.2}{2} \quad \frac{6.2}{2} \quad \frac{5.1}{2} \quad \frac{5.3}{11} \quad \frac{5.6}{16} \quad \frac{7.3}{50}$$

$$\frac{4.5}{50} \quad \frac{5.7}{25} \quad \frac{6.5}{2} \quad \frac{6.4}{2} \quad \frac{5.6}{2} \quad \frac{6.0}{11} \quad \frac{6.6}{18} \quad \frac{8.4}{50}$$

Sta.	+	π ✓	-	Elev.
		958.34		

4+00				951.2
------	--	--	--	-------

4+10				
------	--	--	--	--

4+50				449.9
------	--	--	--	-------

4+59				
------	--	--	--	--

4+94				449.7
------	--	--	--	-------

5+00				449.7
------	--	--	--	-------

T.P.	1.10	954.81 ✓	4.63	953.71 ✓
5+09				

5+43				449.3
------	--	--	--	-------

6+00				446.6
------	--	--	--	-------

+14				446.0
-----	--	--	--	-------

+19				445.8
-----	--	--	--	-------

Lt.

£

Rt.

13

$\frac{5.2}{50}$	$\frac{6.8}{15}$	$\frac{7.2}{14}$	$\frac{7.1}{1}$	$\frac{7.0}{2}$	$\frac{6.3}{3}$	$\frac{6.8}{15}$	$\frac{7.4}{19}$	$\frac{9.5}{50}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

954.14
4.2

Floor of attached garage 60' Lt.

$\frac{6.5}{50}$	$\frac{5.6}{44}$	$\frac{6.8}{23}$	$\frac{7.6}{15}$	$\frac{8.2}{14}$	$\frac{8.0}{8}$	$\frac{8.4}{84}$	$\frac{7.9}{4}$	$\frac{8.2}{14}$	$\frac{8.4}{17}$	$\frac{8.9}{21}$	$\frac{10.6}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	-----------------	------------------	------------------	------------------	-------------------

952.94
5.4

Floor of attached garage 45' Lt.

$\frac{6.0}{50}$	$\frac{7.0}{15}$	$\frac{8.5}{14}$	$\frac{8.6}{86}$	$\frac{9.0}{7}$	$\frac{9.5}{13}$	$\frac{10.6}{29}$	$\frac{11.5}{50}$
------------------	------------------	------------------	------------------	-----------------	------------------	-------------------	-------------------

$\frac{8.0}{50}$	$\frac{8.4}{14}$	$\frac{8.6}{86}$	$\frac{9.2}{11}$	$\frac{11.6}{50}$
------------------	------------------	------------------	------------------	-------------------

950.41
4.4

Floor of garage 17' Lt.

$\frac{4.7}{50}$	$\frac{5.1}{10}$	$\frac{5.5}{55}$	$\frac{5.8}{7}$	$\frac{6.3}{10}$	$\frac{6.7}{15}$	$\frac{8.7}{50}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------

$\frac{5.0}{50}$	$\frac{5.6}{10}$	$\frac{8.5}{8}$	$\frac{8.2}{8}$	$\frac{6.9}{10}$	$\frac{7.4}{16}$	$\frac{9.2}{50}$
------------------	------------------	-----------------	-----------------	------------------	------------------	------------------

$\frac{5.4}{50}$	$\frac{6.0}{16}$	$\frac{8.9}{9}$	$\frac{8.8}{8.8}$	$\frac{9.4}{9}$	$\frac{7.4}{13}$	$\frac{8.7}{36}$	$\frac{8.4}{50}$
------------------	------------------	-----------------	-------------------	-----------------	------------------	------------------	------------------

443.1
1.1

$\frac{8.4}{100}$	$\frac{9.5}{50}$	$\frac{12.4}{10.5}$	$\frac{8.1}{19}$	$\frac{9.0}{50}$	$\frac{9.7}{12}$	$\frac{14.2}{10.8}$	$\frac{11.3}{20}$	$\frac{13.0}{100}$
-------------------	------------------	---------------------	------------------	------------------	------------------	---------------------	-------------------	--------------------

44.01
1.1

Sta. + π - Elev.

954.81 ✓

6+22

945.6

+26

45.2

Edge Blacktop

6+46.32

45.5

Swelling Ar.

T.P.

6.41

960.12 ✓

1.10

953.71 ✓

B.M.

7.64

954.48 ✓

952.48

Lt.

E

Rt.

$$\frac{87}{50}$$

$$\frac{92}{50}$$

$$\frac{100}{13}$$

$$\frac{108}{50}$$

$$\frac{118}{100}$$

$$\frac{75}{100}$$

$$\frac{86}{50}$$

$$\frac{96}{50}$$

$$\frac{106}{50}$$

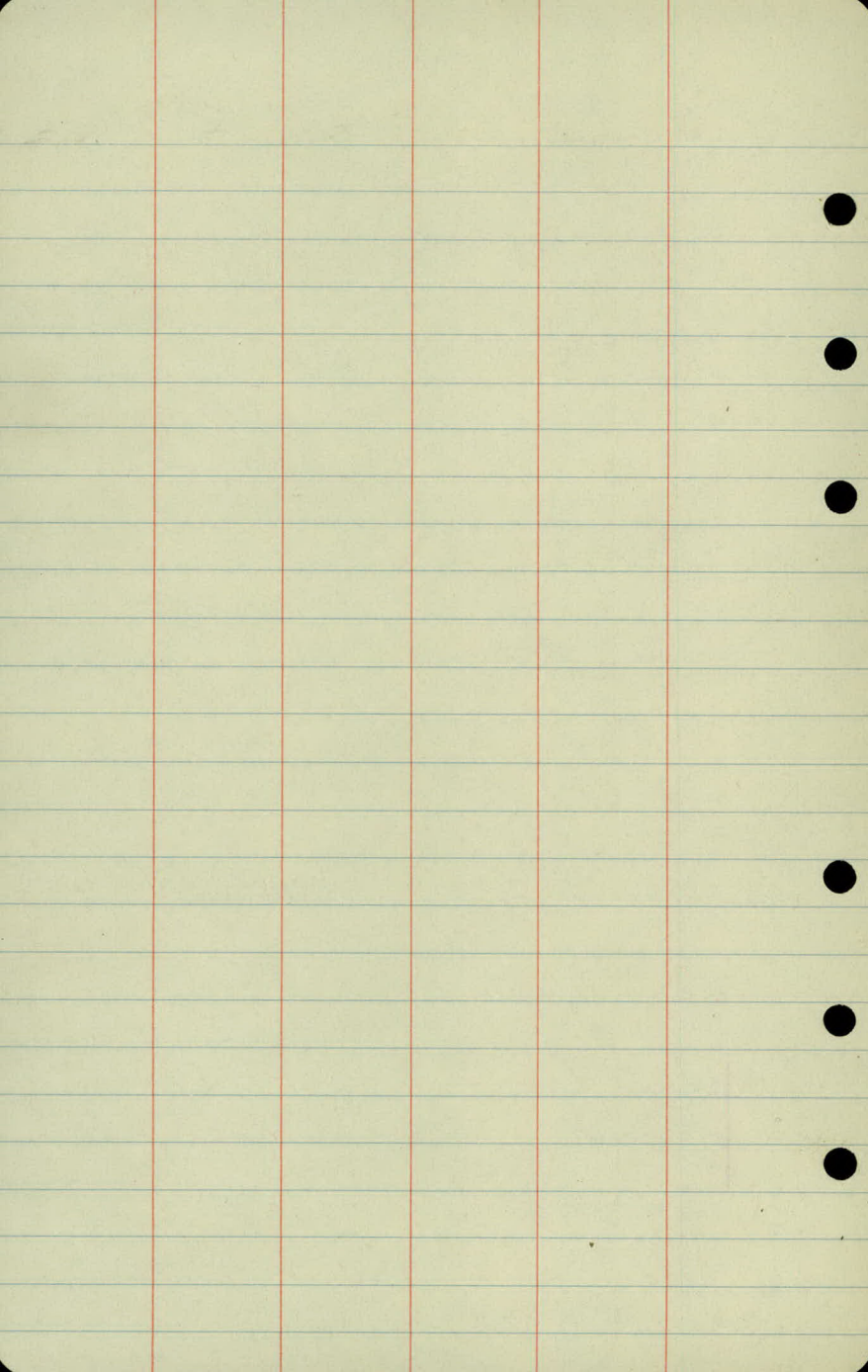
$$\frac{116}{100}$$

$$\frac{70}{100}$$

$$\frac{93}{50}$$

$$\frac{114}{100}$$

Top of water shot off 7' Rt. 5+64 Hollywood Court.



North Lane.

6

5

4

3

2

1

0

← North

8

6+46.7 of Snelling

6+26 Edge Blacktop

+18 = 15" x 24' C.M.
+14 End Fence 20.0

8.0
21

6+07 = 12" Oak 27.0
6+00 = 12" Oak 11.0

36" v. w.
Fencing

+25 T.P. 2.0
+27 P.P. 22.0

+51 = 10' Entry Drive
To Garage.

+22 = 18" Oak 11.0
+01 = 12" Oak 6.0

+24 Begin Fence 24.0
+14 End Hedge 27.0

12
20
Fu. Garage.

26. 415V

Scattered
Trees

6' Buckthorn Hedge

Snelling

Scattered

+34 Begin Hedge 28.0
+34 End Fg. 21.0

60" v. w.
Fencing

0+51 = 12" Maple 6.0

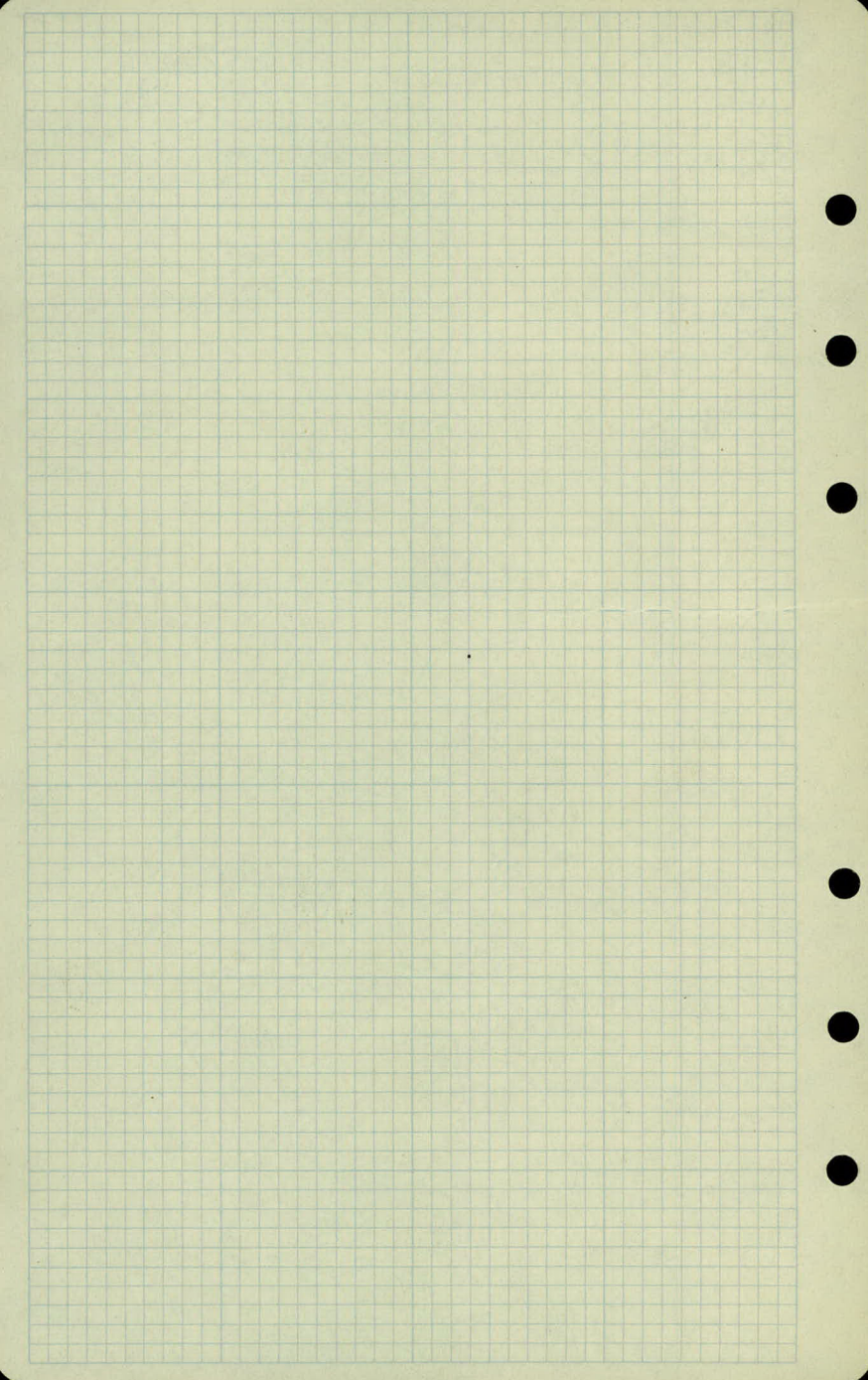
0+50 = 12" Maple 8.0

Brush

0+11 = 12" Maple 8.0

+05 = Frame Room

16.5 25



North Lane.

Sta.	+	π	-	Elev.
B.M.	7.68	960.16		952.48

0-20				950.00
------	--	--	--	--------

0+00				49.4
------	--	--	--	------

0+50				49.7
------	--	--	--	------

1+00				50.6
------	--	--	--	------

+50				51.4
-----	--	--	--	------

2+00				52.4
------	--	--	--	------

+50				53.6
-----	--	--	--	------

3+00				54.7
------	--	--	--	------

+50				56.1
-----	--	--	--	------

4+00				55.8
------	--	--	--	------

T.P.	2.11	957.93	4.34	955.87
				55.7

+50				
-----	--	--	--	--

+65				
-----	--	--	--	--

Lt.

E

Rt.

Top of water shut off 7' Rt. 5164 Hollywood Court.

$$\frac{10.2}{50}$$

$$\frac{10.2}{50}$$

$$\frac{10.7}{50}$$

$$\frac{10.4}{50}$$

$$\frac{10.4}{24}$$

$$\frac{10.6}{50}$$

$$\frac{10.8}{50}$$

$$\frac{10.3}{50}$$

$$\frac{10.3}{30}$$

$$\frac{10.5}{50}$$

$$\frac{10.5}{50}$$

$$\frac{8.8}{50}$$

$$\frac{9.2}{21}$$

$$\frac{9.6}{50}$$

$$\frac{10.3}{50}$$

$$\frac{8.0}{50}$$

$$\frac{8.2}{25}$$

$$\frac{8.8}{50}$$

$$\frac{8.7}{50}$$

$$\frac{6.5}{50}$$

$$\frac{7.0}{25}$$

$$\frac{7.8}{50}$$

$$\frac{7.7}{50}$$

$$\frac{5.4}{50}$$

$$\frac{5.9}{25}$$

$$\frac{6.6}{50}$$

$$\frac{6.4}{50}$$

$$\frac{4.9}{24}$$

$$\frac{5.5}{50}$$

$$\frac{5.8}{50}$$

$$\frac{3.6}{50}$$

$$\frac{3.8}{25}$$

$$\frac{4.1}{50}$$

$$\frac{4.5}{50}$$

$$\frac{3.9}{50}$$

$$\frac{3.9}{25}$$

$$\frac{4.4}{50}$$

$$\frac{4.7}{50}$$

$$\frac{1.9}{50}$$

$$\frac{1.9}{23}$$

$$\frac{2.2}{50}$$

$$\frac{3.2}{71}$$

gord

Floor of Garage Rt.

27 55.23.

Sta.	+	-	Elev.
		957.93	
5+00			954.6
+50	Sec. Box to Garage (attached) on lot.		53.8
6+00			53.1
+12			52.6
+18			52.3
+20			52.1
+26			51.9
6+46 ¹⁵			52.1
B.M.	1.29	956.64	956.64

Lt.

Q

Rt.

yard

$$\frac{32}{50}$$

$$\frac{30}{24}$$

$$\frac{33}{50}$$

$$\frac{37}{50}$$

yard

yard

$$\frac{37}{50}$$

$$\frac{41}{50}$$

Square Foot

$$\frac{32}{49}$$

$$54.73$$

$$\frac{44}{50}$$

$$\frac{44}{24}$$

$$\frac{48}{50}$$

$$\frac{44}{50}$$

yard

$$\frac{45}{50}$$

$$\frac{46}{27}$$

$$\frac{53}{50}$$

$$\frac{48}{50}$$

yard

$$51.63$$

$$51.33$$

$$50.93$$

$$\times \frac{1 \text{ in}}{6.3} \frac{36}{56}$$

$$\times \frac{1 \text{ in}}{6.6} \frac{5.4}{16}$$

$$\frac{56}{50}$$

$$\frac{58}{8}$$

$$\frac{1 \text{ in}}{7.0} \frac{20}{8}$$

$$\frac{82}{50}$$

Ditch

$$\frac{48}{50}$$

$$\frac{58}{50}$$

$$\frac{70}{50}$$

$$\frac{49}{50}$$

$$\frac{60}{50}$$

$$\frac{71}{50}$$

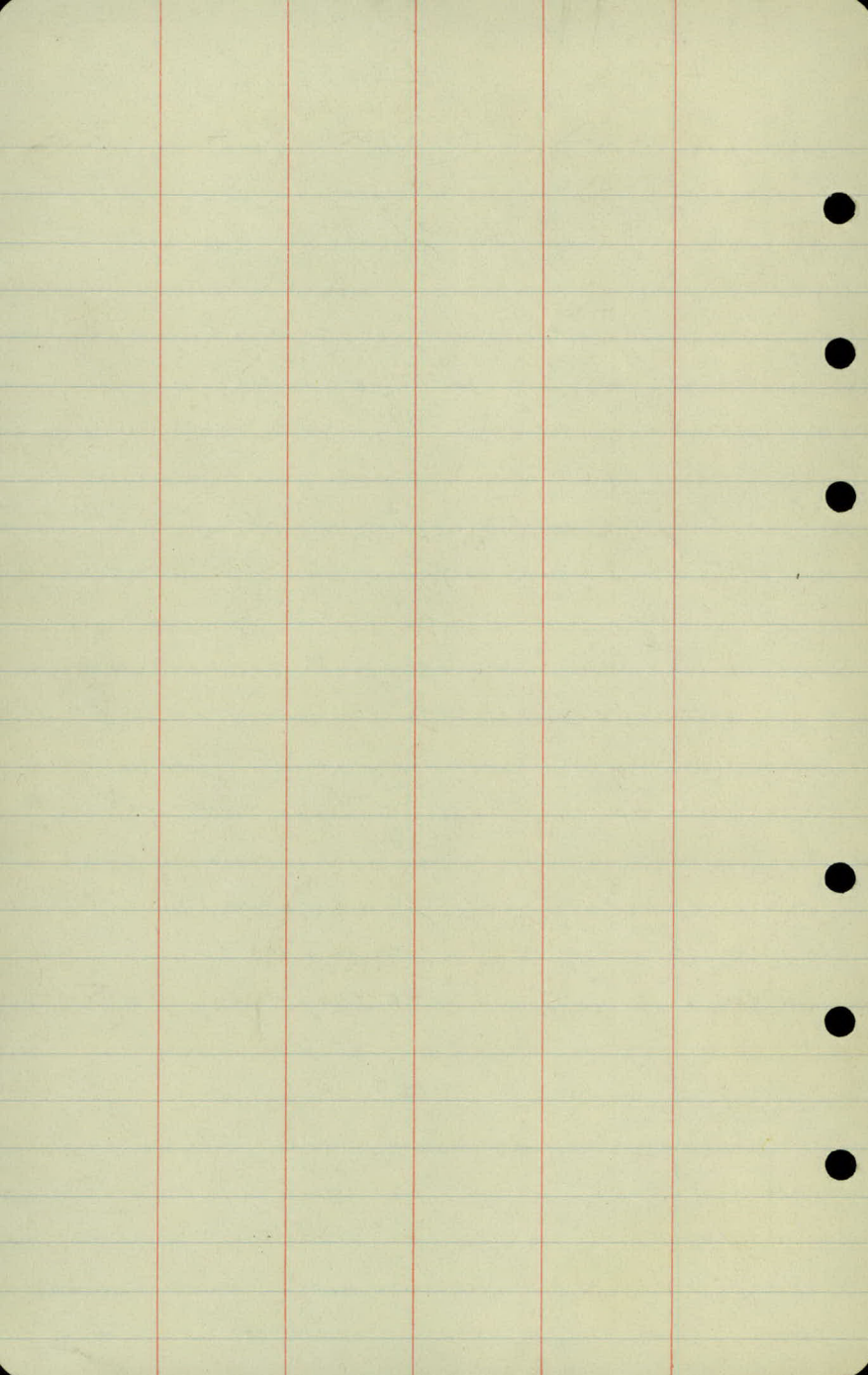
Blacktop

$$\frac{47}{50}$$

$$\frac{58}{50}$$

$$\frac{70}{50}$$

Top of Mon. Snelling & Carpenter



West Lane.

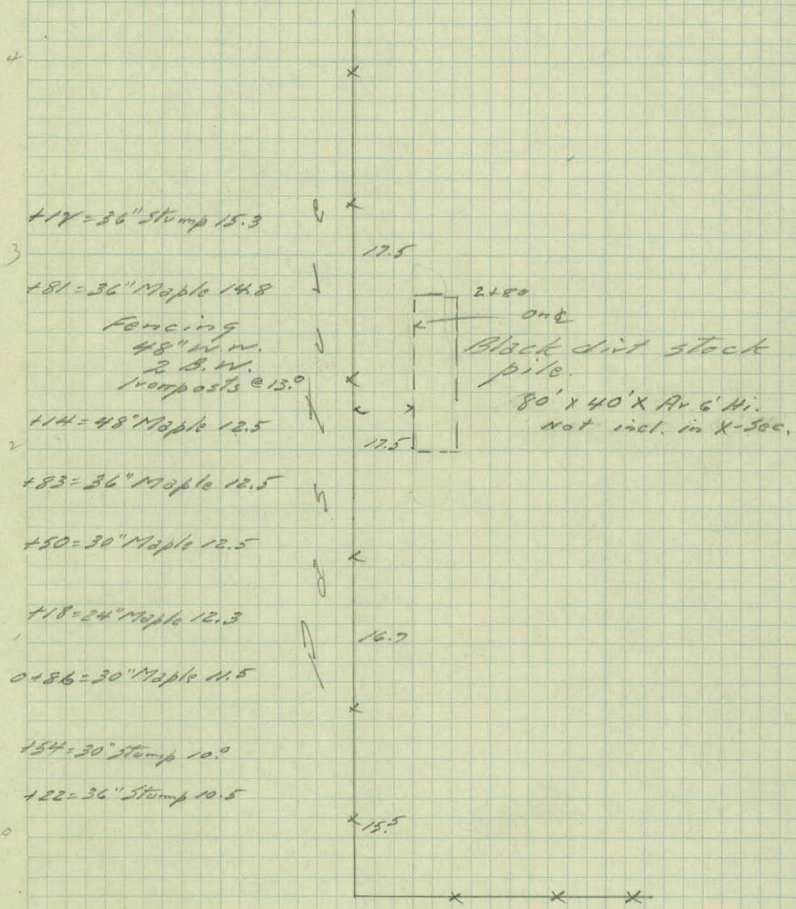
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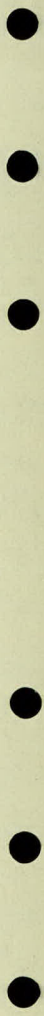
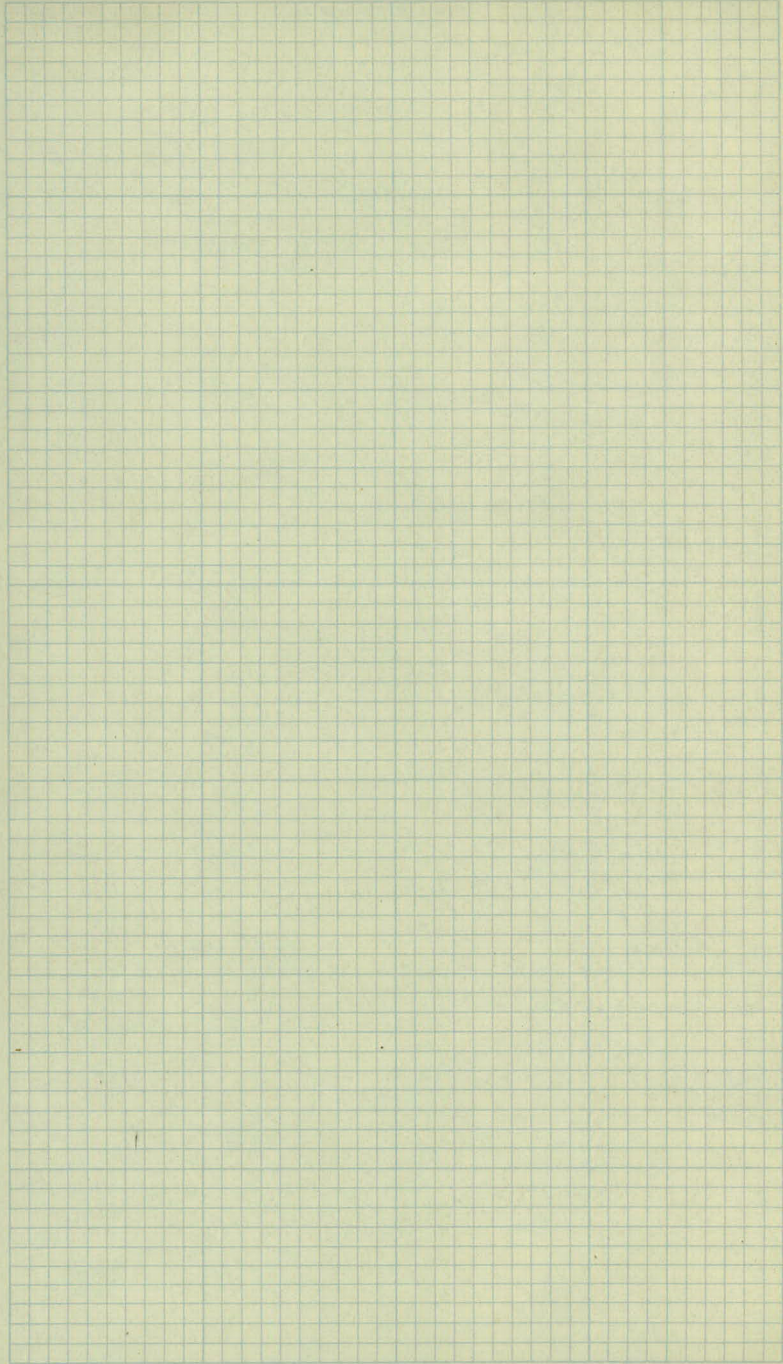
3

2

1

0+00





West Lane.

Sta.	+	π	-	Elev.
B.M.	7.68	960.16		952.48

0+00				953.2
------	--	--	--	-------

0+10				53.2
------	--	--	--	------

0+16				50.6
------	--	--	--	------

0+50				50.0
------	--	--	--	------

0+80				49.8
------	--	--	--	------

1+00				49.3
------	--	--	--	------

+35				48.7
-----	--	--	--	------

+40				48.6
-----	--	--	--	------

1+55.3				48.2
--------	--	--	--	------

+75				47.8
-----	--	--	--	------

+95				47.8
-----	--	--	--	------

Lt.

E

Rt.

21

Top of Water shut off 7' 124. 512. 5464

$$\frac{8.5}{50} \quad \frac{8.5}{15} \quad \frac{8.4}{6} \quad \frac{7.0}{3} \quad \cancel{7.0} \quad \frac{7.0}{50}$$

$$\frac{8.5}{50} \quad \frac{8.5}{15} \quad \frac{8.4}{6} \quad \frac{7.0}{3} \quad \cancel{7.0} \quad \frac{7.0}{50}$$

$$\frac{8.6}{50} \quad \frac{8.4}{15} \quad \frac{8.5}{7} \quad \frac{9.3}{6} \quad \cancel{9.6} \quad \frac{9.6}{10} \quad \frac{8.8}{10} \quad \frac{8.5}{50}$$

$$\frac{9.0}{50} \quad \frac{8.7}{16} \quad \frac{8.7}{8} \quad \frac{10.1}{6} \quad \cancel{10.2} \quad \frac{10.3}{9} \quad \frac{9.2}{11} \quad \frac{9.0}{50}$$

$$\frac{10.4}{50} \quad \frac{9.6}{26} \quad \frac{9.3}{16} \quad \frac{9.5}{9} \quad \frac{10.7}{7} \quad \cancel{10.4} \quad \frac{10.8}{9} \quad \frac{9.6}{11} \quad \frac{9.5}{50}$$

$$\frac{10.5}{50} \quad \frac{10.8}{40} \quad \frac{10.0}{17} \quad \frac{10.0}{7} \quad \frac{11.1}{6} \quad \cancel{10.9} \quad \frac{11.3}{9} \quad \frac{11.3}{50}$$

$$\frac{10.0}{50} \quad \frac{10.2}{30} \quad \frac{10.2}{17} \quad \frac{10.2}{9} \quad \frac{11.5}{7} \quad \cancel{11.5} \quad \frac{11.5}{8} \quad \frac{12.2}{43}$$

$$\frac{10.0}{50} \quad \frac{10.5}{30} \quad \frac{10.5}{17} \quad \frac{10.0}{10} \quad \frac{11.4}{8} \quad \cancel{11.6} \quad \frac{11.7}{9} \quad \frac{10.6}{10} \quad \frac{10.8}{50}$$

$$\frac{10.5}{50} \quad \frac{10.4}{45} \quad \frac{10.4}{17} \quad \frac{10.5}{7} \quad \frac{11.9}{6} \quad \cancel{11.0} \quad \frac{11.8}{10} \quad \frac{10.6}{11} \quad \frac{11.0}{50}$$

$$\frac{10.6}{50} \quad \frac{10.6}{18} \quad \frac{10.7}{9} \quad \frac{12.0}{6} \quad \cancel{12.4} \quad \frac{12.3}{5} \quad \frac{10.1}{8} \quad \frac{11.0}{50}$$

$$\frac{10.7}{50} \quad \frac{10.7}{18} \quad \frac{10.7}{9} \quad \frac{12.3}{7} \quad \cancel{12.4} \quad \frac{12.0}{8} \quad \frac{10.3}{10} \quad \frac{11.1}{50}$$

Sta. + π - Elev.

960.16

2+00

9/9.20

+50

4/9.5

3+00

4/9.7

3+10.³

4/9.6

B.M.

7.68 957.48

47.

2

24.

$$\frac{10.7}{50}$$

$$\frac{10.7}{18}$$

$$\frac{11.0}{50}$$

$$\frac{11.0}{50}$$

$$\frac{10.7}{50}$$

$$\frac{10.7}{19}$$

$$\frac{10.7}{50}$$

$$\frac{10.8}{50}$$

$$\frac{10.5}{50}$$

$$\frac{10.5}{20}$$

$$\frac{10.5}{50}$$

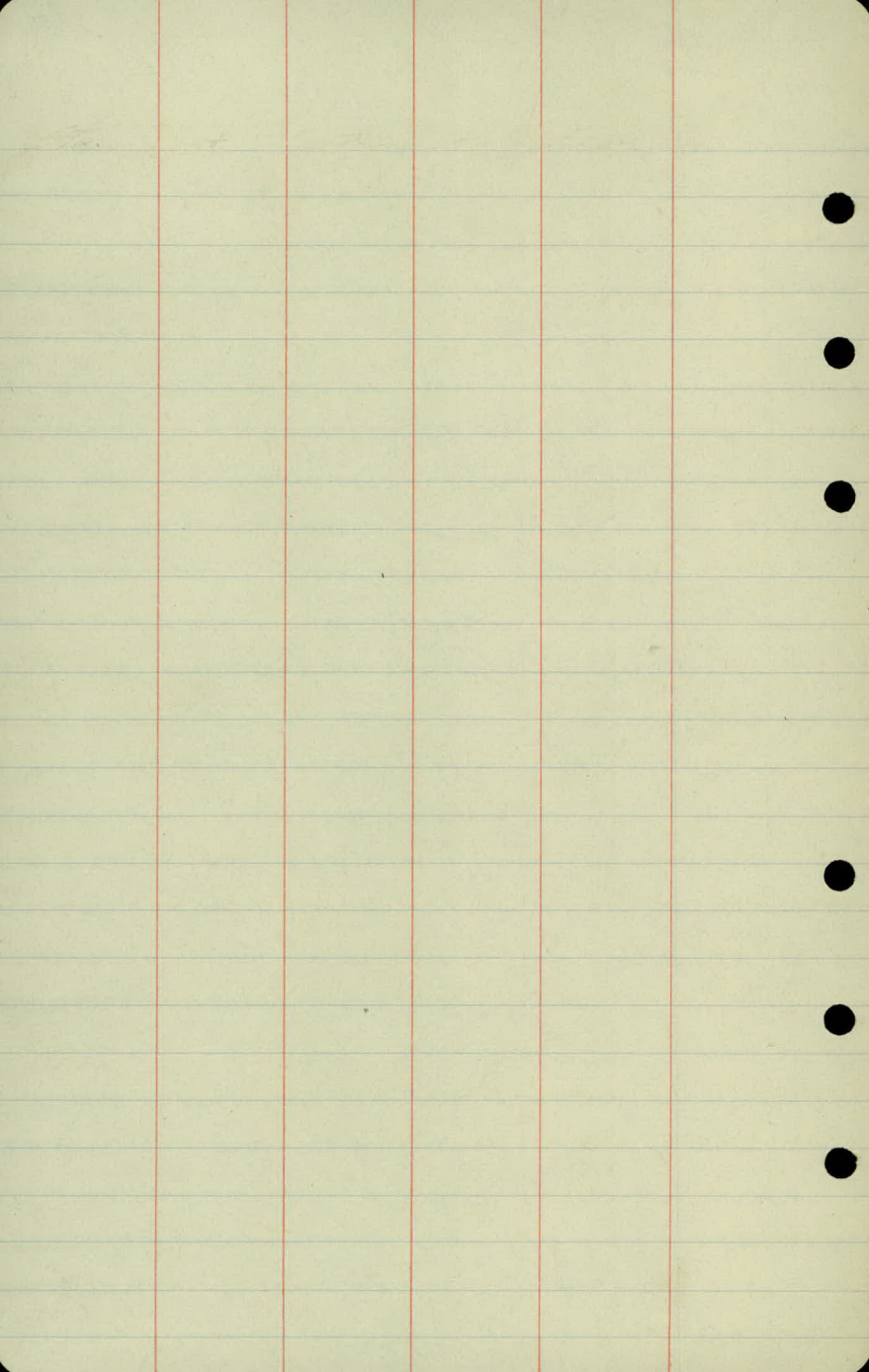
$$\frac{10.4}{50}$$

$$\frac{10.3}{50}$$

$$\frac{10.3}{20}$$

$$\frac{10.6}{50}$$

$$\frac{10.5}{50}$$



Slope Stokes

North Lane

Cross Roads Court

Sta	+	π	-	Elev
B.M.	9.49	960.39		950.90
		53		5.67 956.57

0				51.0
---	--	--	--	------

+50				51.1
-----	--	--	--	------

1				51.2
---	--	--	--	------

+50				51.4
-----	--	--	--	------

2				52.1
---	--	--	--	------

+50				53.5
-----	--	--	--	------

3				54.9
---	--	--	--	------

+50				55.7
-----	--	--	--	------

4				55.8
---	--	--	--	------

+50				55.3
-----	--	--	--	------

5				54.4
---	--	--	--	------

+50				53.3
-----	--	--	--	------

Grade Rod

Hollywood Ca

Top Water Shut Off. 5' Lt Sta 0+40

8.9

$\frac{8.9}{8}$

$\frac{8.9}{8}$

8.8

$\frac{8.8}{8}$

$\frac{8.8}{8}$

8.7

$\frac{8.7}{8}$

$\frac{8.7}{8}$

8.5

$\frac{8.5}{8}$

$\frac{8.5}{8}$

7.8

$\frac{7.8}{8}$

$\frac{7.8}{8}$

6.4

$\frac{6.4}{8}$

$\frac{6.4}{8}$

5.0

$\frac{5.0}{8}$

$\frac{5.0}{8}$

4.2

$\frac{4.2}{8}$

$\frac{4.2}{8}$

4.1

$\frac{4.1}{8}$

$\frac{4.1}{8}$

4.6

$\frac{4.6}{8}$

$\frac{4.6}{8}$

5.5

$\frac{5.5}{8}$

$\frac{5.5}{8}$

6.6

$\frac{6.6}{8}$

$\frac{6.6}{8}$

560

+

 π

-

Elev.

960.39⁴

6

52.2

+12

52.0

+18

51.8

+20

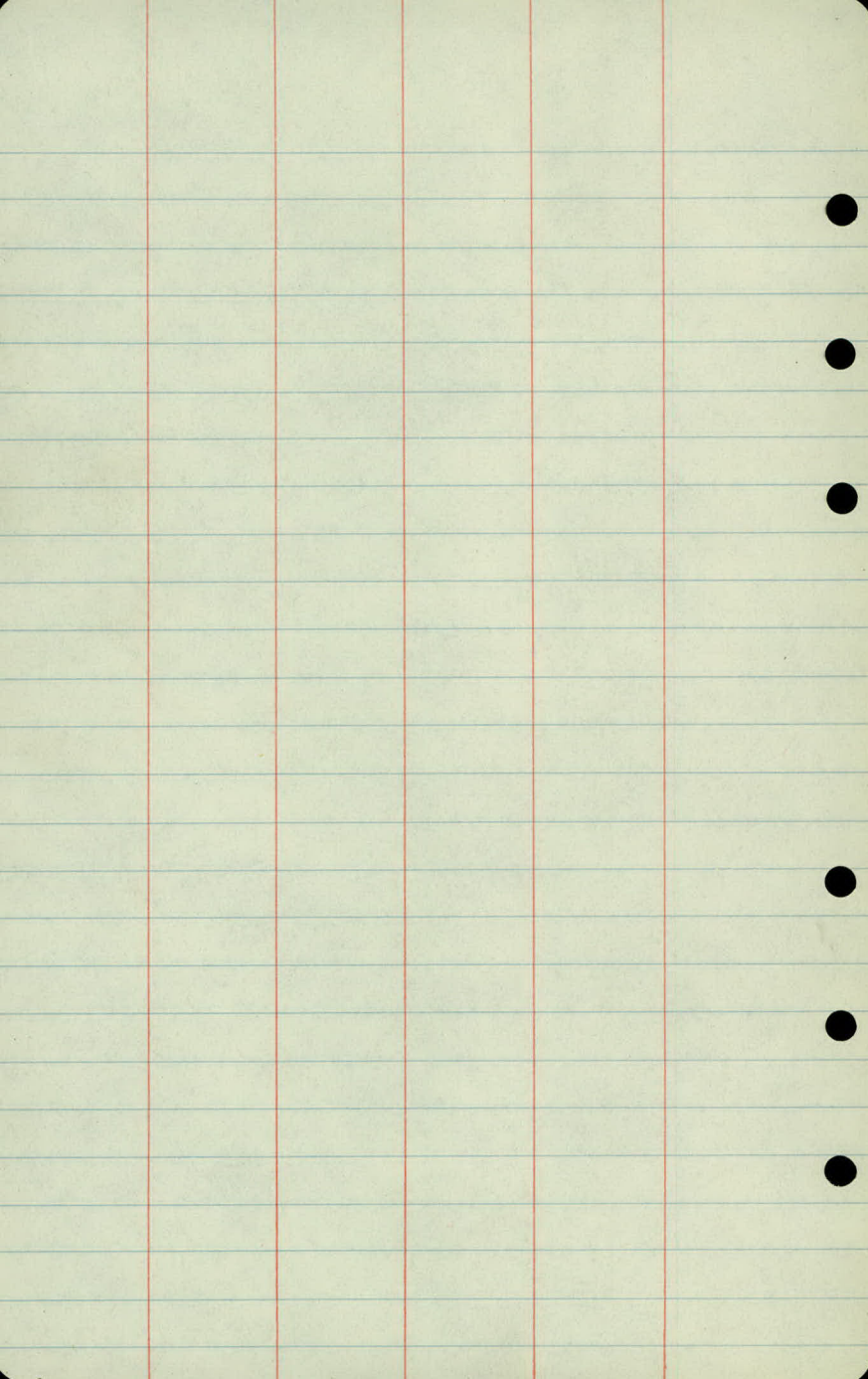
51.8

+22

9.7

$\frac{6.7}{8}$ Down 1.0

$\frac{6.7}{8}$ Down 1.0



Slope Stakes

South Lane

Sta	+	π	-	Elev
B.M.	7.14	958.04 ^{7.5}		950.90

0				52.5
---	--	--	--	------

+13				52.5
-----	--	--	--	------

+50				52.4
-----	--	--	--	------

1				52.2
---	--	--	--	------

+50				52.1
-----	--	--	--	------

2				52.0
---	--	--	--	------

+50				51.9
-----	--	--	--	------

3				51.7
---	--	--	--	------

+50				51.6
-----	--	--	--	------

4				51.3
---	--	--	--	------

+50				50.2
-----	--	--	--	------

T.P	4.66	955.40 ^{4.9}	7.30	950.74
-----	------	-----------------------	------	--------

+94				49.5
-----	--	--	--	------

Top Water Shut Off 5'lt 0+40 Holly Grt

5.1

$\frac{6.1}{8}$ Fill 1.0

$\frac{6.1}{8}$ Fill 1.0

5.3

$\frac{5.3}{8}$

$\frac{5.3}{8}$

5.4

$\frac{5.4}{8}$

$\frac{4.4}{8}$ Down 1.0

5.5

$\frac{5.5}{8}$

$\frac{4.5}{8}$ Down 1.0

5.6

$\frac{5.6}{8}$

$\frac{4.6}{8}$ Down 1.0

5.8

$\frac{4.8}{8}$ Down 1.0

$\frac{4.8}{8}$ Down 1.0

5.9

$\frac{4.9}{8}$ Down 1.0

$\frac{4.9}{8}$ Down 1.0

6.2

$\frac{6.2}{8}$

$\frac{6.2}{8}$

7.3

$\frac{7.3}{8}$

$\frac{7.3}{8}$

5.4

$\frac{4.4}{8}$ Down 1.0

$\frac{5.4}{8}$

Sta	+	π	-	Elev
-----	---	-------	---	------

		⁴⁹ 955.40		
--	--	-------------------------	--	--

5				49.5
---	--	--	--	------

+43				48.9 ³
-----	--	--	--	-------------------

6				46.5
---	--	--	--	------

+14				45.7
-----	--	--	--	------

+19				45.4
-----	--	--	--	------

+22				45.2
-----	--	--	--	------

BM		2.90		952.50
----	--	------	--	--------

5.4

$\frac{4.4}{8}$ Down 1.0

$\frac{6.4}{8}$ Fill 1.0

6.0

$\frac{5.0}{8}$ Down 1.0

$\frac{6.0}{8}$

8.4

$\frac{7.4}{8}$ Down 1.0

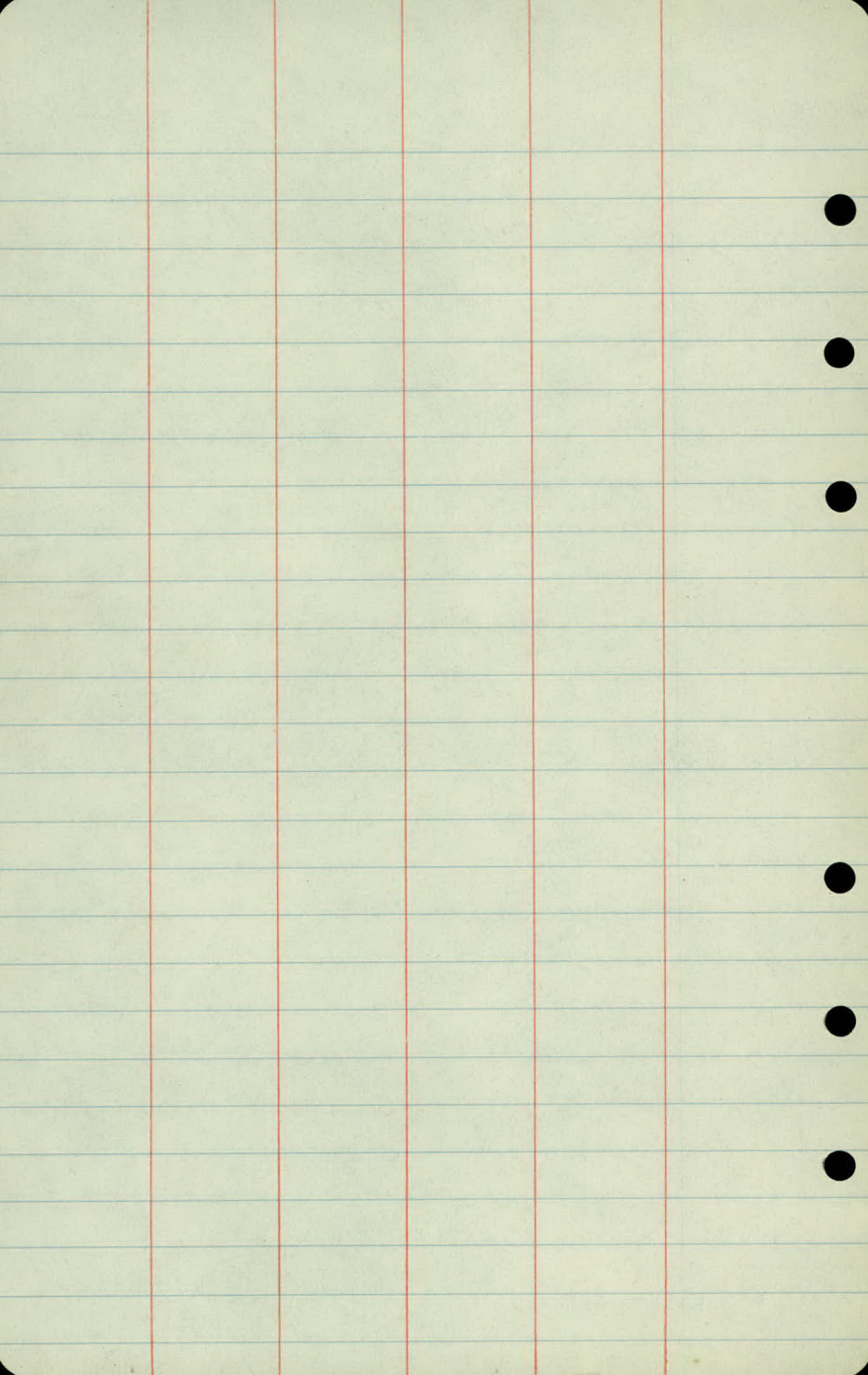
$\frac{8.4}{8}$

9.2

$\frac{9.2}{8}$

$\frac{9.2}{8}$

Top Water Shut Off 7' Rt 5+64 Holly. Crt.



Slope stakes

West Lane

Sta	+	π	-	Elev	
B.M.	4.91	955.81		950.90	
0				52.5 ⁰	
- +10				51.9 ⁰ 52.4	
- +16				1.8 52.3	
+50				51.9 ⁰	
- +80				51.5 ⁰	
1				51.3 ⁰	
+35				1.5 51.0	
- +40				50.9 ¹	—
+55.3				50.8 ³	—
- +75				50.8 ₃	.
+95				50.8	—
2				50.8	

Holly-

Top Water Shut Off 5' Lt Sta 0+40

3.8

$\frac{3.8}{8}$

$\frac{3.8}{8}$

~~3.9~~

4.0

4.4

$\frac{4.4}{8}$

$\frac{4.4}{8}$

~~4.5~~

5.0

$\frac{5.0}{8}$

$\frac{5.0}{8}$

5.3

$\frac{5.3}{8}$

$\frac{5.3}{8}$

~~5.4~~

~~5.5~~

5.5

$\frac{5.5}{8}$

$\frac{5.5}{8}$

✓

5.5

$\frac{5.5}{8}$

$\frac{5.5}{8}$

Sta.	+	π	-	Elev.
------	---	-------	---	-------

		955.81		
--	--	--------	--	--

2 + 50				
--------	--	--	--	--

				50.9 ⁴
--	--	--	--	-------------------

3				
---	--	--	--	--

				51.0 ^{0.5}
--	--	--	--	---------------------

+ 10.3				
--------	--	--	--	--

				51.0 ^{0.5}
--	--	--	--	---------------------

5.4

$$\frac{5.4}{8}$$

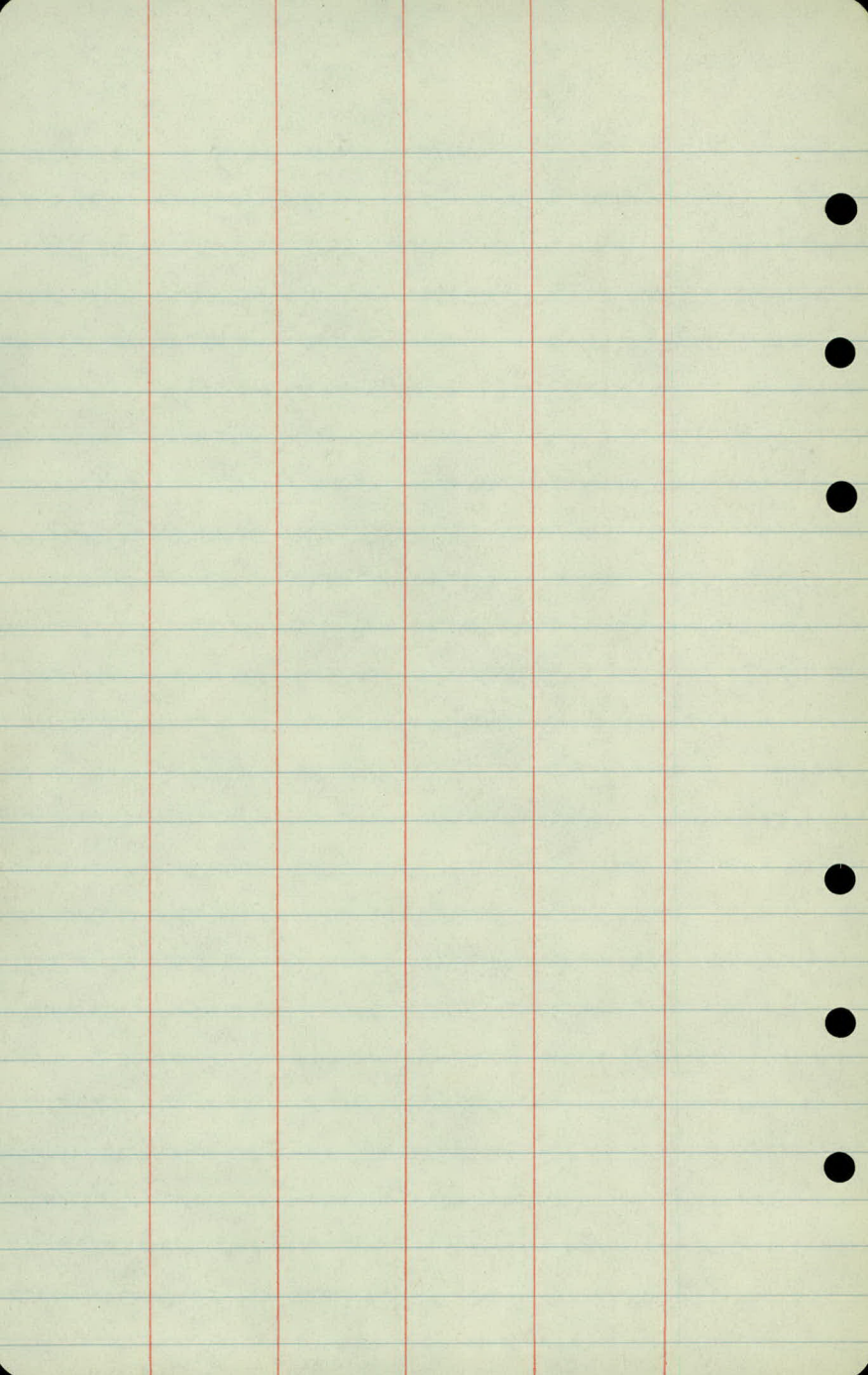
$$\frac{5.4}{8}$$

5.3

$$\frac{5.3}{8}$$

$$\frac{5.3}{8}$$

5.3



Slope Stakes

Holly Wood Court

Sta	+	π	-	Elev.
B.M.	6.94	959.42		952.48

0				50.8
---	--	--	--	------

+09				50.8
-----	--	--	--	------

+11				50.8
-----	--	--	--	------

+50				50.9
-----	--	--	--	------

1				51.0
---	--	--	--	------

+50				51.2
-----	--	--	--	------

2				51.9
---	--	--	--	------

+50				53.0
-----	--	--	--	------

3				53.8
---	--	--	--	------

+50				54.2
-----	--	--	--	------

4				54.0
---	--	--	--	------

+50				53.5
-----	--	--	--	------

Top Water shut Off 7' RT 5+64

— 8.6

— 8.6

— 8.6

8.5

$$\frac{8.5}{13}$$

$$\frac{8.5}{13}$$

8.4

$$\frac{8.4}{13}$$

$$\frac{8.4}{13}$$

8.2

$$\frac{8.2}{13}$$

$$\frac{8.2}{13}$$

7.5

$$\frac{7.5}{13}$$

$$\frac{7.5}{13}$$

6.4

$$\frac{6.4}{13}$$

$$\frac{6.4}{13}$$

5.6

$$\frac{5.6}{13}$$

$$\frac{5.6}{13}$$

5.2

$$\frac{5.2}{13}$$

$$\frac{5.2}{13}$$

5.4

$$\frac{4.4}{13} \text{ Down 1.0}$$

$$\frac{5.4}{13}$$

5.9

$$\frac{4.9}{13} \text{ Down 1.0}$$

$$\frac{5.9}{13}$$

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		959.42		
--	--	--------	--	--

5				53.1
---	--	--	--	------

+50				51.8
-----	--	--	--	------

+89				50.1
-----	--	--	--	------

6+02				49.5
------	--	--	--	------

+12				49.0
-----	--	--	--	------

B.M.		8.52		950.90
------	--	------	--	--------

6.3

$$\frac{5.3}{13}$$

Down 1.0

$$\frac{6.3}{13}$$

7.6

$$\frac{6.6}{13}$$

Down 1.0

$$\frac{6.6}{13}$$

Down 1.0

9.3

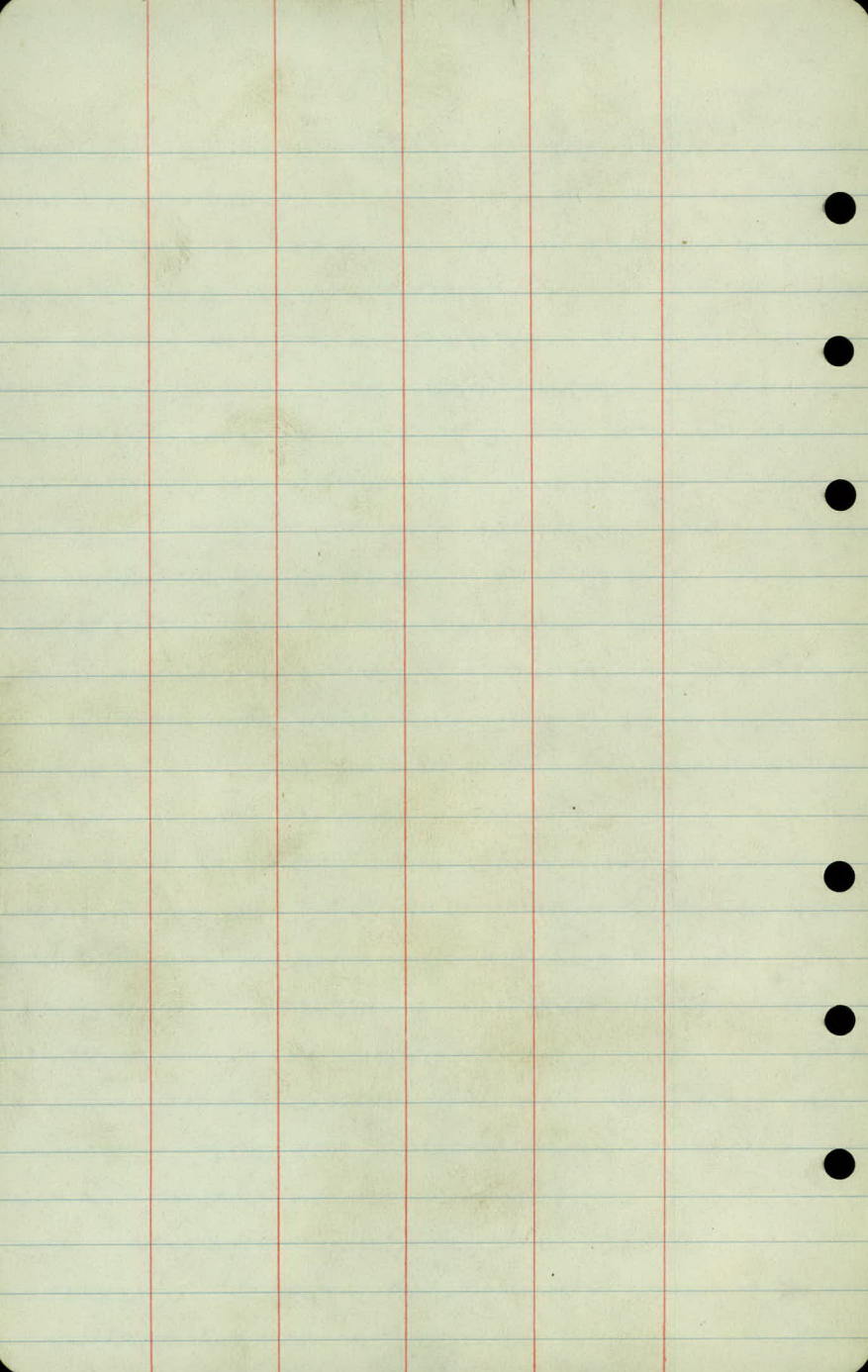
$$\frac{7.3}{13}$$

Down 2.0

$$\frac{7.3}{13}$$

Down 2.0

Top shut off 5' Lt 0.40



\$10000 Stakes

Hollywood Court

B.M. 6.48 ^{59.}958.96 952.48

0 +50 50.9 8.1

1 51.0 8.0

+50 51.2 7.8

2 51.9 7.1

+50 53.0 6.0

3 53.8 5.2

+50 54.2 4.8

4 54.0 5.0

+50 53.5 5.5

5 53.1 5.9

+50 51.8 7.2

+89. 50.1 8.9

L

R

Top Water Shutoff 7' Rt 5+64

$$\frac{8.1}{13}$$

$$\frac{8.1}{13}$$

$$\frac{8.0}{13}$$

$$\frac{8.0}{13}$$

$$\frac{7.8}{13}$$

$$\frac{7.8}{13}$$

$$\frac{7.1}{13}$$

$$\frac{7.1}{13}$$

$$\frac{6.0}{13}$$

$$\frac{6.0}{13}$$

$$\frac{5.2}{13}$$

$$\frac{5.2}{13}$$

$$\frac{4.8}{13}$$

$$\frac{4.8}{13}$$

$$\frac{5.0}{13}$$

$$\frac{5.0}{13}$$

$$\frac{4.5}{\frac{6.10}{13}}$$

$$\frac{5.5}{13}$$

$$\frac{4.9}{\frac{6.10}{13}}$$

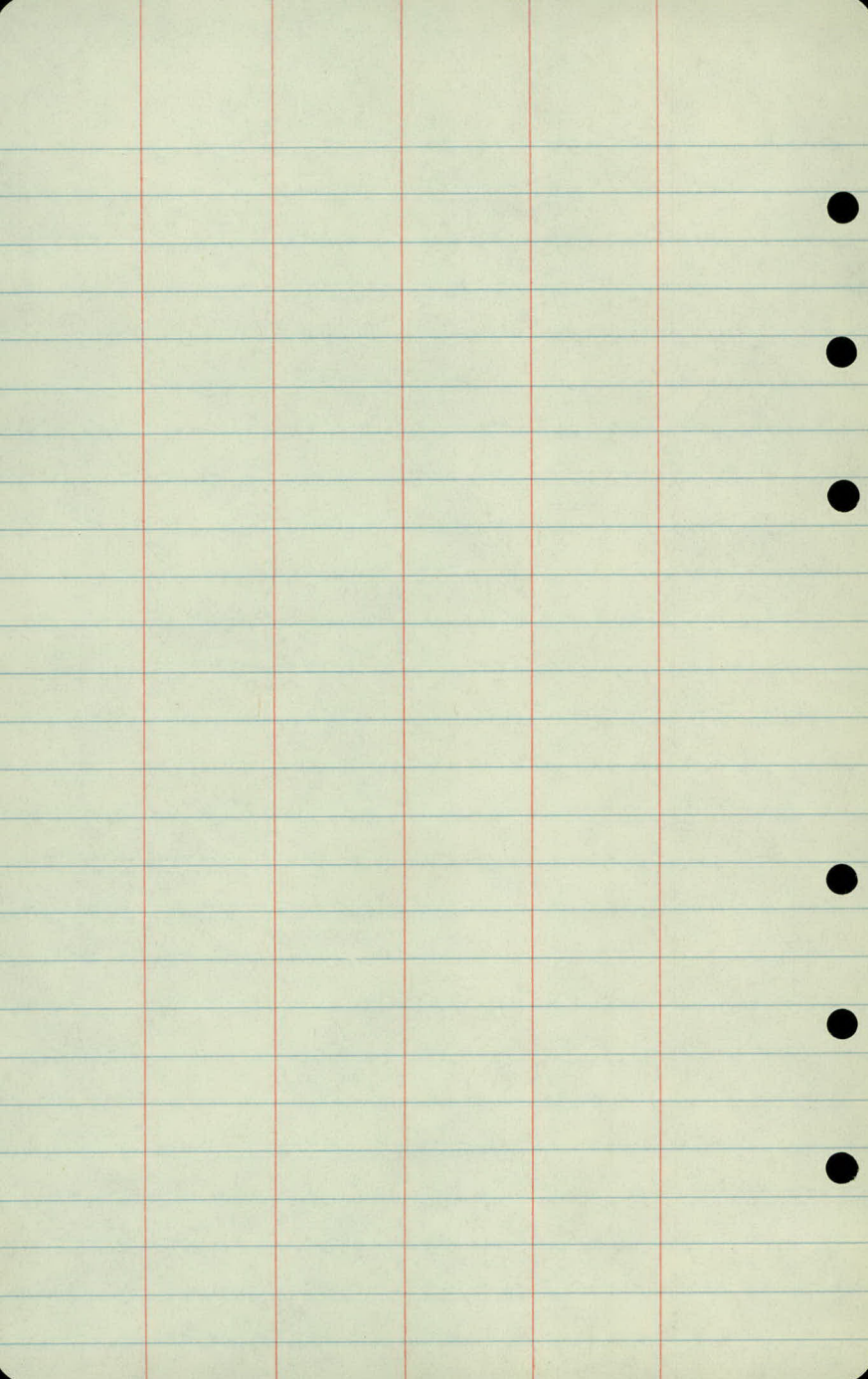
$$\frac{5.7}{13}$$

$$\frac{6.2}{\frac{6.10}{13}}$$

$$\frac{6.2}{\frac{6.10}{13}}$$

$$\frac{6.9}{\frac{6.20}{13}}$$

$$\frac{6.9}{\frac{6.20}{13}}$$



Slope Stakes

South Lane

B.M. 6.46 958.94 952.48

~~0 + 0.0~~

~~53.0~~
~~52.5~~

5.9

~~+13~~

~~53.0~~
~~52.5~~

+50

52.9
52.4

6.0

1

52.7
52.2

6.2

+50

52.6
52.1

6.3

2

52.5
52.0

6.4

+50

52.4
51.9

6.5

T.P. 4.48 956.95 6.47

51.0
952.47

3

52.2
51.7

4.8

+50

52.1
51.6

4.9

4

51.8
51.3

5.2

+50

50.7
50.2

6.3

Top water shut off 7' RL 5+64 Holly

3

1

$$\frac{6.0}{8}$$

$$\frac{6.0}{8}$$

$$\frac{6.2}{8}$$

$$\frac{6.2}{8}$$

$$\frac{6.3}{8}$$

$$\frac{5.3}{8}$$

$$\frac{C.1.0}{8}$$

$$\frac{6.4}{8}$$

$$\frac{5.4}{8}$$

$$\frac{C.1.0}{8}$$

$$\frac{6.5}{8}$$

$$\frac{5.5}{8}$$

$$\frac{C.1.0}{8}$$

$$\frac{4.8}{8}$$

$$\frac{3.8}{8}$$

$$\frac{C.1.0}{8}$$

$$\frac{4.9}{8}$$

$$\frac{3.9}{8}$$

$$\frac{C.1.0}{8}$$

$$\frac{5.2}{8}$$

$$\frac{5.2}{8}$$

$$\frac{6.3}{8}$$

$$\frac{6.3}{8}$$

⁷⁰
956.95

4 + 94

50.0
~~49.5~~

7.0

5

50.0
~~49.5~~

7.0

+ 43

49.4
~~48.9~~

7.6

6

47.0
~~46.5~~

10.0

Lt

Rt

$$\frac{7.0}{8}$$

$$\frac{7.0}{8}$$

$$\frac{7.0}{8}$$

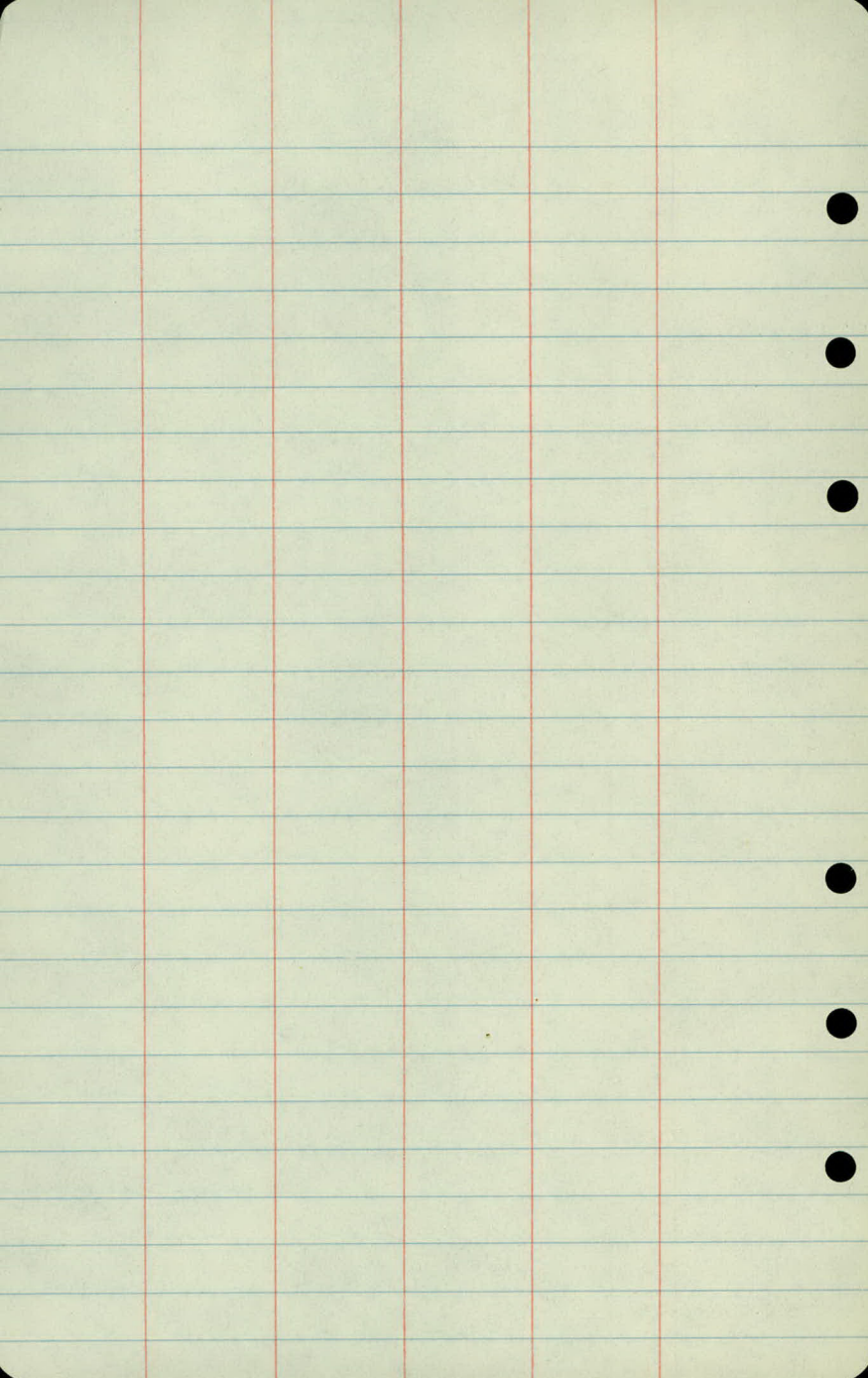
$$\frac{7.0}{8}$$

$$\frac{7.6}{8}$$

$$\frac{7.6}{8}$$

$$\frac{10.0}{8}$$

$$\frac{10.0}{8}$$



(C)
Slope Stakes

North Lane

B.M.	4 .47	956.95	952.48	
	3.26	^{59.0} 958.97	1.24	955.71
0			51.5 51.0	7.5
+50			51.6 51.1	7.4
1			51.7 51.2	7.3
+50			51.9 51.4	7.1
2			52.6 52.1	6.4
+50			54.0 53.5	5.0
3			55.4 54.9	3.6
+50			56.2 55.7	2.8
4			56.3 55.8	2.7
+50			55.8 55.3	3.2
5			54.9 54.4	4.1

Lt.

Rt.

Top water. Shut off 7' Rt. 5464 Holly.

$$\frac{7.4}{8}$$

$$\frac{7.4}{8}$$

$$\frac{7.3}{8}$$

$$\frac{7.3}{8}$$

$$\frac{7.1}{8}$$

$$\frac{7.1}{8}$$

$$\frac{6.4}{8}$$

$$\frac{6.4}{8}$$

$$\frac{5.0}{8}$$

$$\frac{5.0}{8}$$

$$\frac{3.6}{8}$$

$$\frac{3.6}{8}$$

$$\frac{2.9}{8}$$

$$\frac{2.8}{8}$$

$$\frac{2.7}{8}$$

$$\frac{2.7}{8}$$

$$\frac{3.2}{8}$$

$$\frac{3.2}{8}$$

$$\frac{4.1}{8}$$

$$\frac{4.1}{8}$$

958.97

5+50

53.8
~~53.3~~

5.2

6

52.5
~~52.2~~

6.5

+12

+18

+20

T.P.	6.19	959.96	'	5.20	953.77
B.M.	7.45	959.93	7.45	952.51	952.48
B.M.			2.51	957.42	

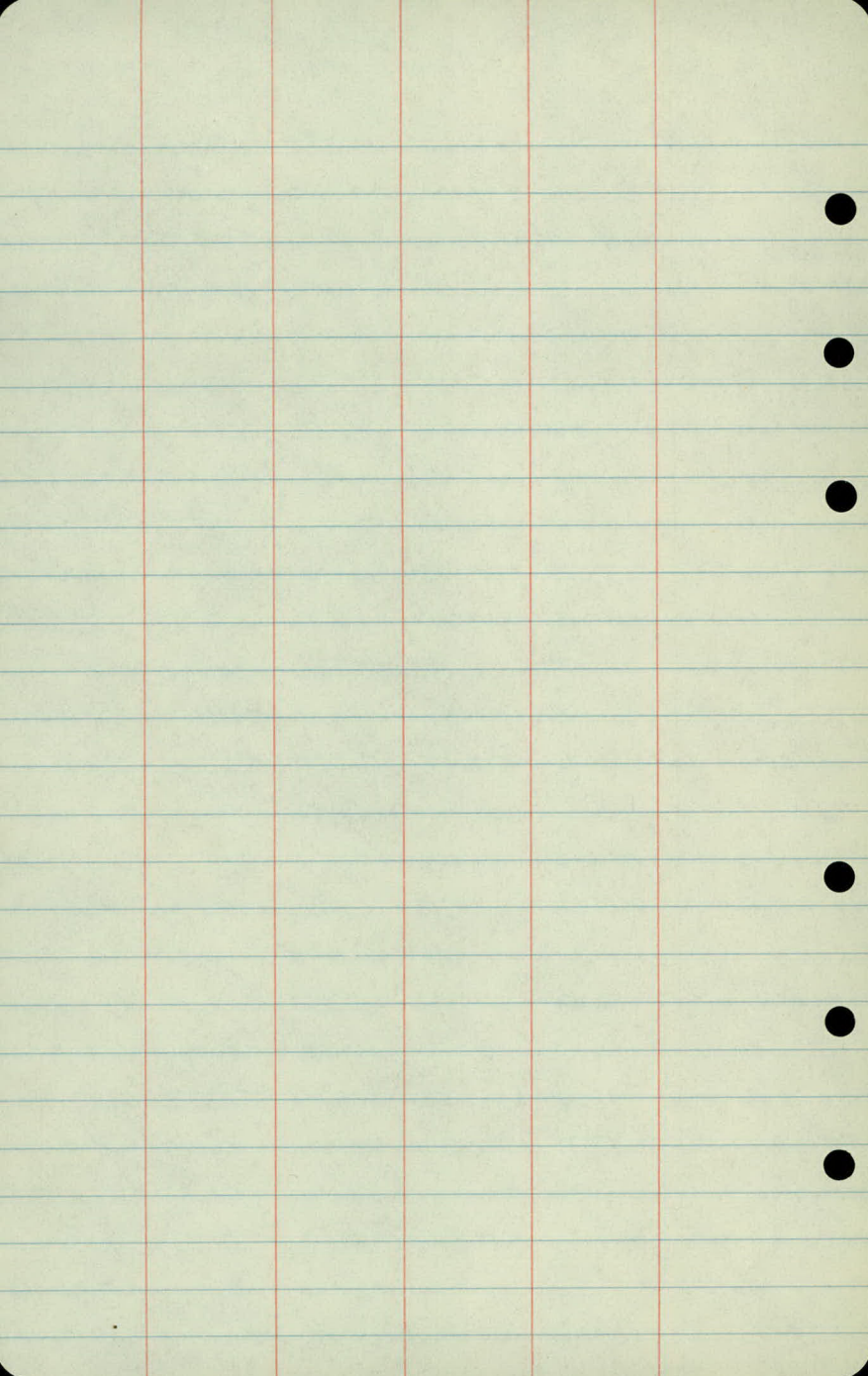
$$\frac{5.1}{8}$$

$$\frac{5.2}{8}$$

$$\frac{5.5}{6.10}$$

$$\frac{5.5}{6.10}$$

Top Water Shut Off 7' RT 5+64 (Hollywood Court)
Top W. Cor. Top step Lt 3+60 (Hollywood Court)



Slope Stakes

West Lane

B.M.	1.31	958.73		957.42	
T.P.	4.41	956.24	6.90	951.83	
0+00				52.0 52.5	4.2
				51.4 51.9	4.8
				50.8 51.3	5.4
				50.5 51.0	5.7
				50.3 50.8	5.9
				50.3 50.8	5.9
				50.4 50.9	5.8
				50.5 51.0	5.7
3					

Top W. Cor Top Step Lt. 3160 C40114)

$$\frac{4.2}{8}$$

$$\frac{4.2}{8}$$

$$\frac{4.8}{8}$$

$$\frac{4.8}{8}$$

$$\frac{5.4}{8}$$

$$\frac{5.4}{8}$$

$$\frac{5.7}{8}$$

$$\frac{5.7}{8}$$

$$\frac{5.7}{8}$$

$$\frac{5.7}{8}$$

$$\frac{5.9}{8}$$

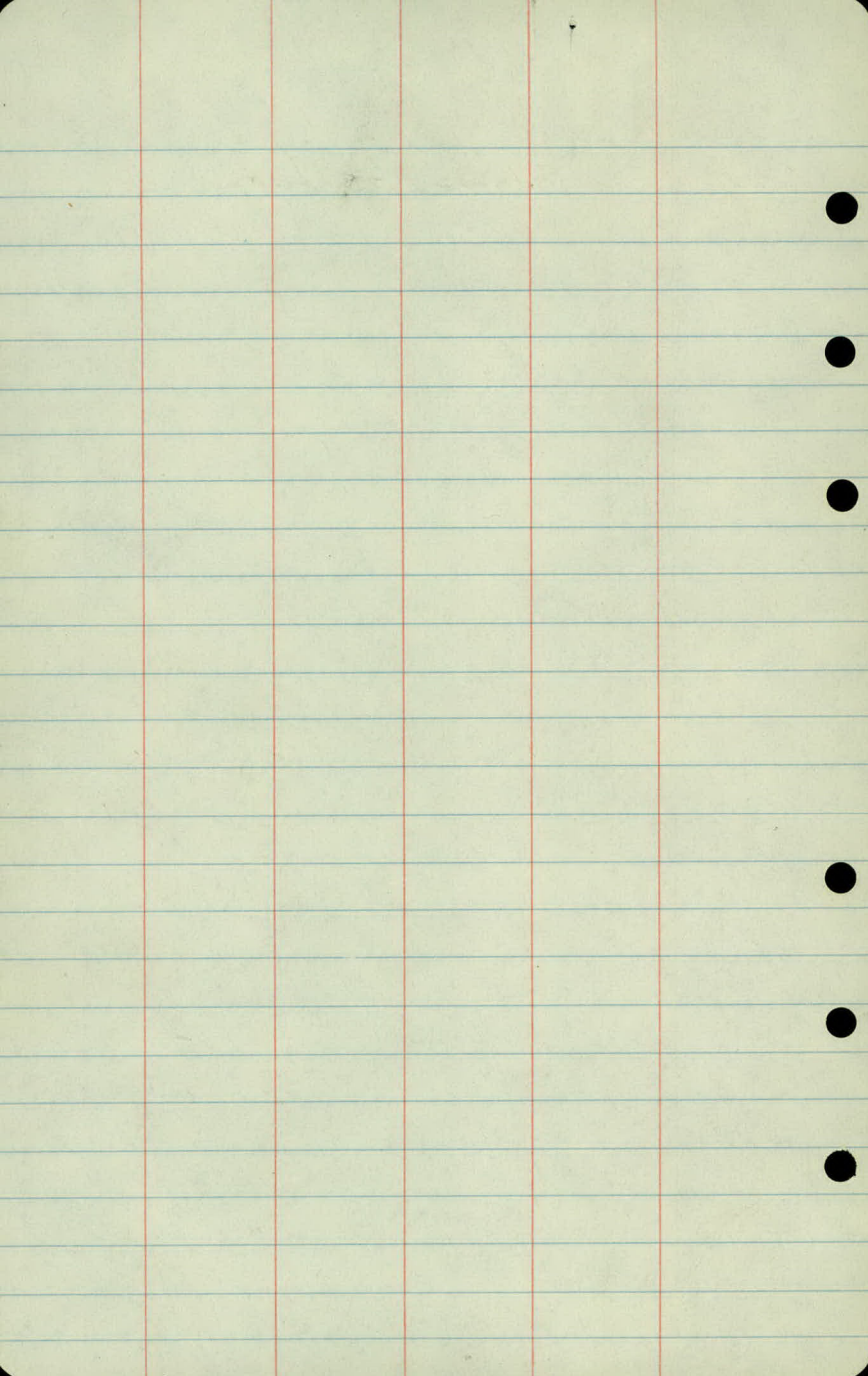
$$\frac{5.9}{8}$$

$$\frac{5.8}{8}$$

$$\frac{5.8}{8}$$

$$\frac{5.7}{8}$$

$$\frac{5.7}{8}$$



X Sections

Hollywood Court

Index

West Lane

North Lane

1 to 3

3 to 6

Rec'd. 6/28/51

drawn up.

Sta	+	Δ	-	Elev
B.M	0.11	958.16		958.05
	2.76	955.49	5.43	952.73

0+10	No Line So Lane	51.5
------	-----------------	------

+43	Conc Slab Rt
-----	--------------

+50	509
-----	-----

+75	507
-----	-----

1	505
---	-----

+36	So Prop line Hollywood Court ⁵⁰⁴
-----	---

+56	50.2
-----	------

Lt

2

Rt

2

Top Hyd Snelling & Long

$$\begin{array}{r} 46 \\ 15 \end{array}$$

$$\begin{array}{r} 40 \\ 7 \end{array}$$

40

$$\begin{array}{r} 3.8 \\ 12 \end{array}$$

$$\begin{array}{r} 3.8 \\ 21 \end{array}$$

$$\begin{array}{r} 440 \\ 10 \end{array}$$

$$\begin{array}{r} 46 \ 47 \ 46 \\ 15 \ 6 \end{array}$$

$$\begin{array}{r} 47 \\ 9 \end{array}$$

$$\begin{array}{r} 440 \\ 12 \end{array}$$

$$\begin{array}{r} 430 \\ 20 \end{array}$$

$$\begin{array}{r} 55 \ 55 \ 50 \ 48 \ 48 \ 44 \\ 16 \ 11 \ 6 \ 8 \ 20 \end{array}$$

$$\begin{array}{r} 5.7 \ 5.3 \ 5.0 \ 5.0 \ 46 \\ 13 \ 7 \ 9 \ 20 \end{array}$$

$$\begin{array}{r} 61 \ 55 \ 51 \ 51 \ 53 \ 49 \\ 16 \ 8 \ 11 \ 19 \ 20 \end{array}$$

$$\begin{array}{r} 60 \ 55 \ 53 \ 50 \ 49 \ 48 \\ 16 \ 10 \ 11 \ 22 \ 75 \end{array}$$

Sta + π - Elev

955.49

1+76 No time ⁵⁰¹ Hollywood Court

2

50.0

+17 Conc slab 121

+25

49.9

+50

49.9

+75

50.1

3

50.1

+10

★

R1

3

60	62	55	54	51	5.5	5.0	✓
16	10	3		9	17	20	

64	64	57	55	56	57	50	46	✓
16	12	4		7	12	13	19	

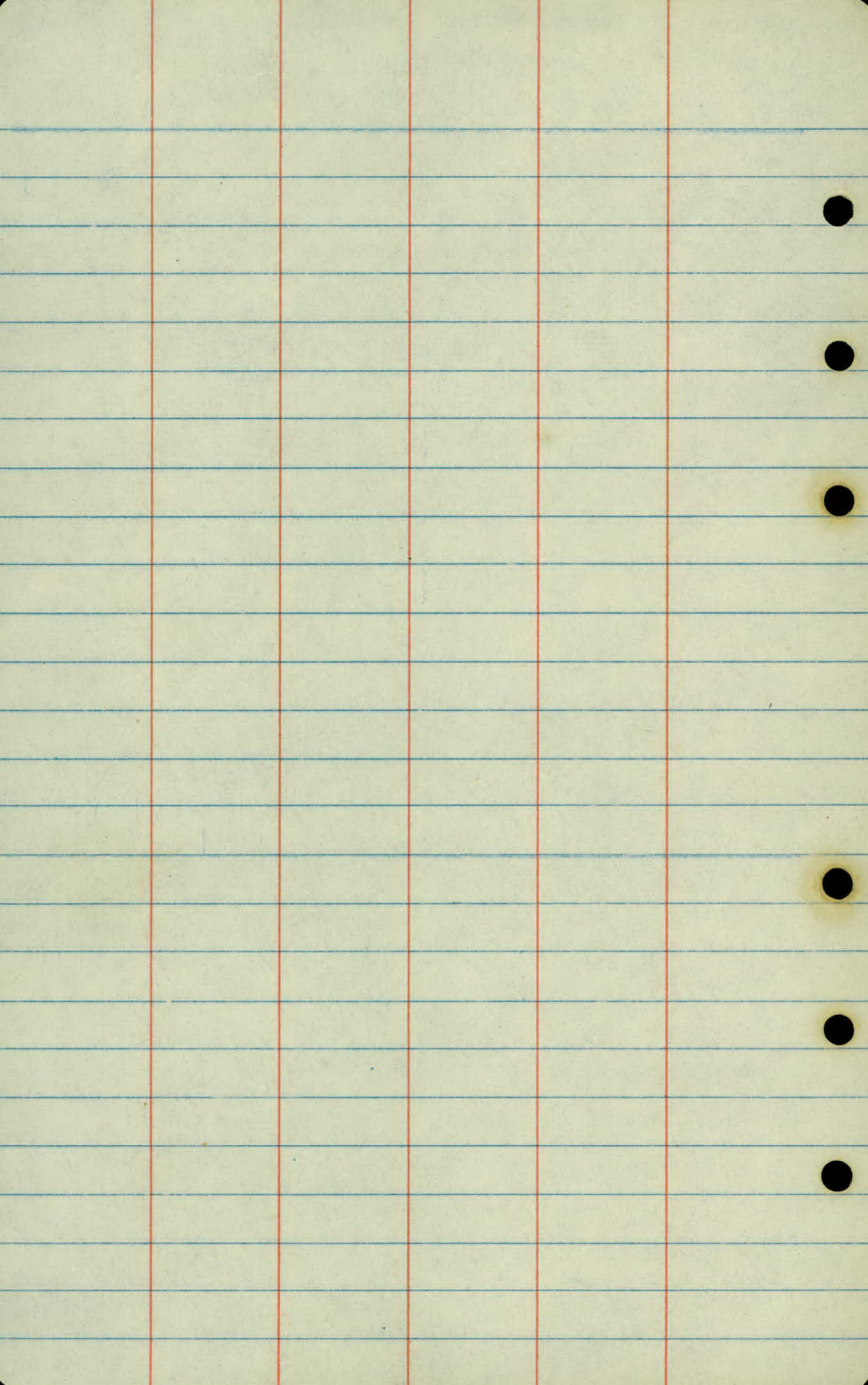
493	410	✓
<u>125</u>	19	

62	59	56	55	486	434	✓
17	7		9	12	19	

63	59	56	5.5	54	48	✓
18	8		6	10	13	

61	58	54	5.3	55	5.3	49	✓
16	10		5	10	13	15	

59	57	54	51	49	5.3	✓
19	10		9	12	23	



Additional X Section

West Lane - Hollywood Court

6-28-51

As phoned in by H.A.W.

W.J.B.

Sta.	+	Σ	-	Elev.
B.M.	4.67	955.97		951.30

1+76				50.1
------	--	--	--	------

2+00				50.0
------	--	--	--	------

+25				49.9
-----	--	--	--	------

+50				49.9
-----	--	--	--	------

+75				50.1
-----	--	--	--	------

3 +00				50.1
-------	--	--	--	------

1 +00		at &	Ditch Lt.	
-------	--	------	-----------	--

1 +36		&	" Lt.	
-------	--	---	-------	--

1 +50		&	" Lt.	
-------	--	---	-------	--

£

$$\frac{7.1}{50} \quad \frac{7.0}{21} \quad 5.9 \quad \checkmark$$

$$\frac{7.0}{50} \quad \frac{7.0}{20} \quad 6.0 \quad \checkmark$$

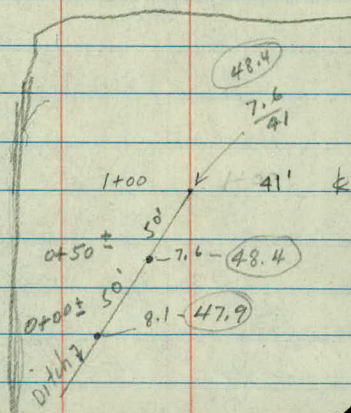
$$\frac{6.9}{50} \quad \frac{7.0}{32} \quad \frac{7.1}{20} \quad 6.1 \quad \checkmark$$

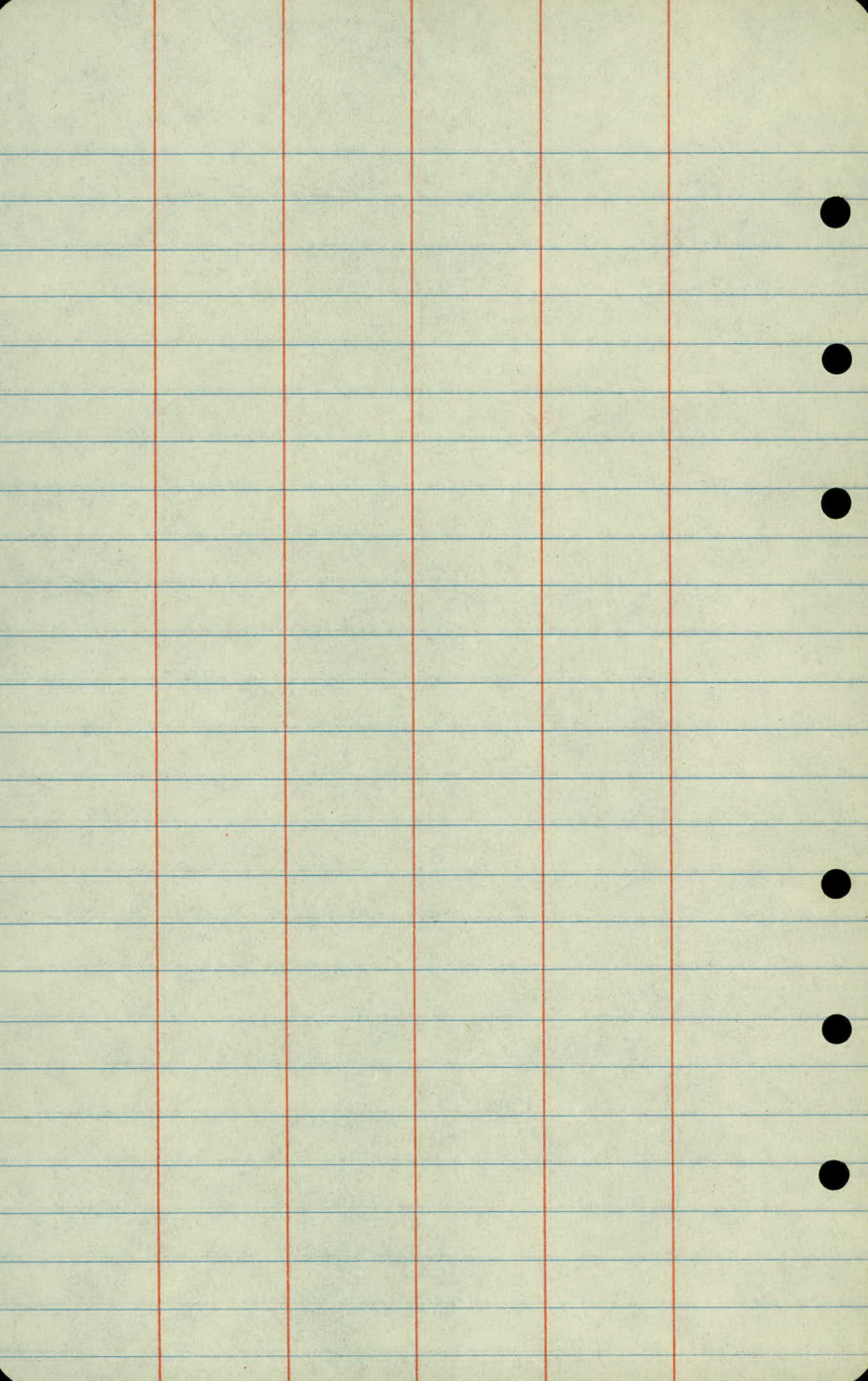
$$\frac{6.8}{50} \quad \frac{6.9}{39} \quad \frac{7.2}{21} \quad 6.1 \quad \checkmark$$

$$\frac{6.8}{50} \quad \frac{6.9}{33} \quad \frac{7.0}{22} \quad 5.9 \quad \checkmark$$

$$\frac{6.7}{50} \quad \frac{6.8}{29} \quad \frac{7.0}{21} \quad 5.9 \quad \checkmark$$

$$\begin{array}{r} 48.4 \\ \frac{7.6}{41} \\ \hline 48.6 \\ \frac{7.4}{33} \\ \hline 48.7 \\ \frac{7.3}{30} \end{array} \quad \checkmark$$





North Lane

Sta + π - Elev
955.49

0+20 49.0

0+19 49.9

0+00 50.1

+20 50.6

+50 51.0

+81 Beg Wall/Lt 51.1

+ 51.3

+50 51.5

L1

2

R1

65
10

65

65
20

60
10

56

60
20

48
11

53
9

54

54
15

✓

4.7
10

5.4
9

5.2
6

49

50
8

53
13

49
15

✓

44
10

49
8

45

46
4

45
11

✓

Wall

419
10

46
10

45
8

44

44
4

41
6

44
8

44
12

✓

Wall

3.9
10

4.2
10

4.2

44
6

4.3
9

4.3
12

✓

Wall

Gar Floor

325
10

38
10

39
8

40

40
7

35
13

336
18

✓

Sta + Δ - Elev

95549

2

52.2

+50

535

535

P.M.

B.M.

4.19

951.30

L

R+

Wall

253
103.2
1035
6

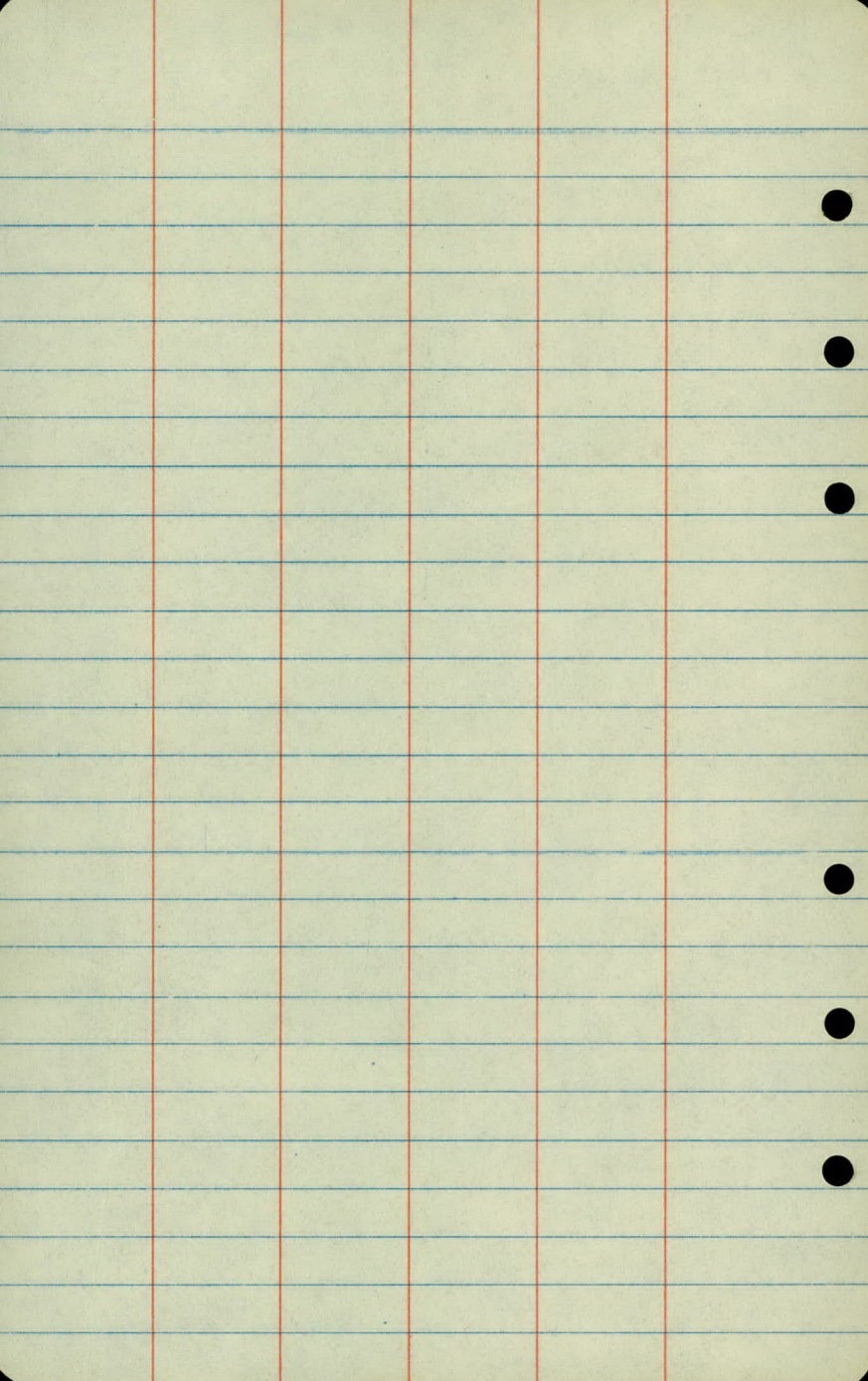
3.3

36 29
8 101.73
102.1
1022
7

20

21
62.1
10

End Cone Wall 10' L 0+81 North Lane



Additional
X Sections

West Lane Hollywood Court.

6-28-51

HAW

AM

LC

MB

Sta	+	π	-	Elev
B.M	467	955.97	955.97	957.30

1+76

2

+25

+50

+75

3

+10.

L+

Z

7

7.1	7.0	5.9
50 ✓	21 ✓	✓

7.0	7.0	6.0
50 ✓	20 ✓	

6.7	7.0	7.1	6.1
50	32	20	

6.8	6.9	7.2	6.1
50	39	21 ✓	✓

6.8	6.9	7.0	5.9
50 ✓	33	22	

6.7	6.8	7.0	5.9
50	29	21	

1400

1400

1436

2

$$\begin{array}{r} 8.1 \\ 7.6 \\ \hline \end{array}$$

$$\begin{array}{r} 7.6 \\ 4.1 \end{array}$$

5.5

$$\begin{array}{r} 7.3 \\ 3.0 \end{array}$$

$$\begin{array}{r} 7.4 \\ 3.3 \\ \checkmark \end{array}$$

