Book 24, Dr. 11

OFFICE OF COUNTY ENGINEER
SEY CO. MINN.

Plan Survey

COUNTY ROAD "C2"

From Lexington To Victoria

Road Acc't. No.

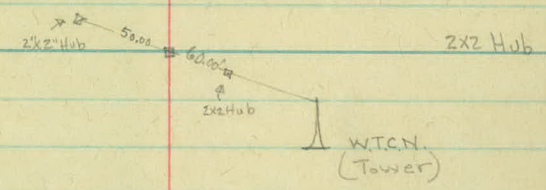
Date Filed 1-6-36 File 11

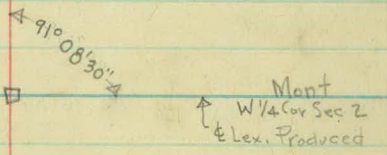
Alignment
Twp. Rd C²
Lex to Vict.

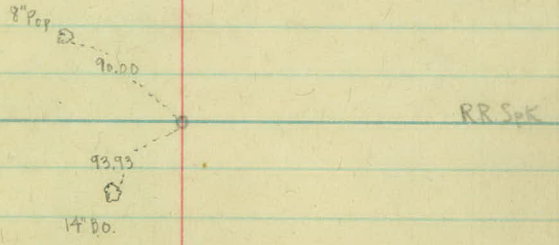
5+31.75 POT

2+49.24 POT

0+00 POT. ℄ Lexington Ave Beg. Prop. Cl


2"x2" Hub
50.00
60.00'
1x2 Hub
W.T.C.N.
(Tower)
2x2 Hub

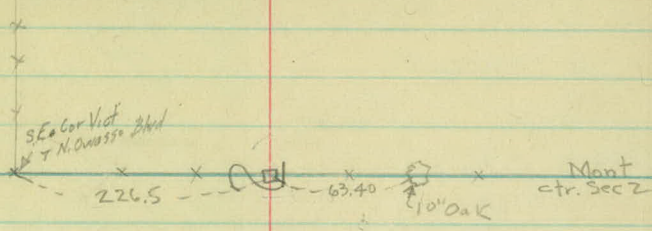

91°08'30"
Mont
W 1/4 Cor Sec 2
& Lex. Produced

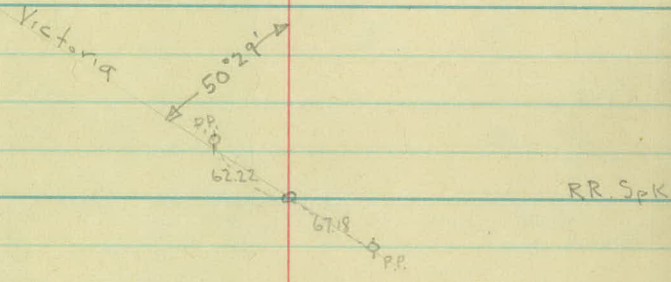

8" Pcp
90.00
RR Spk
93.93
14" Bo.

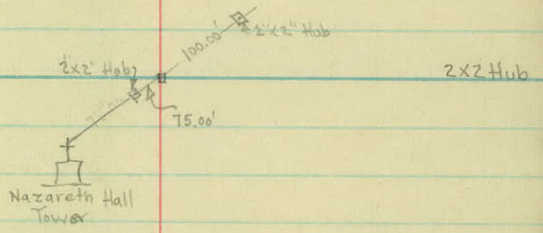
28+77.00 P.O.T.

26+51.00 P.O.T. & Victoria - End Prop. C^2

11+97.63 P.O.T.


S.E. Cor Viet
& N. Onondaga Blvd
226.5
63.40
10" Oak
Mont
ctr. Sec 2


Victoria
50°29'
P.P.
62.22
67.18
P.P.
RR. Spk

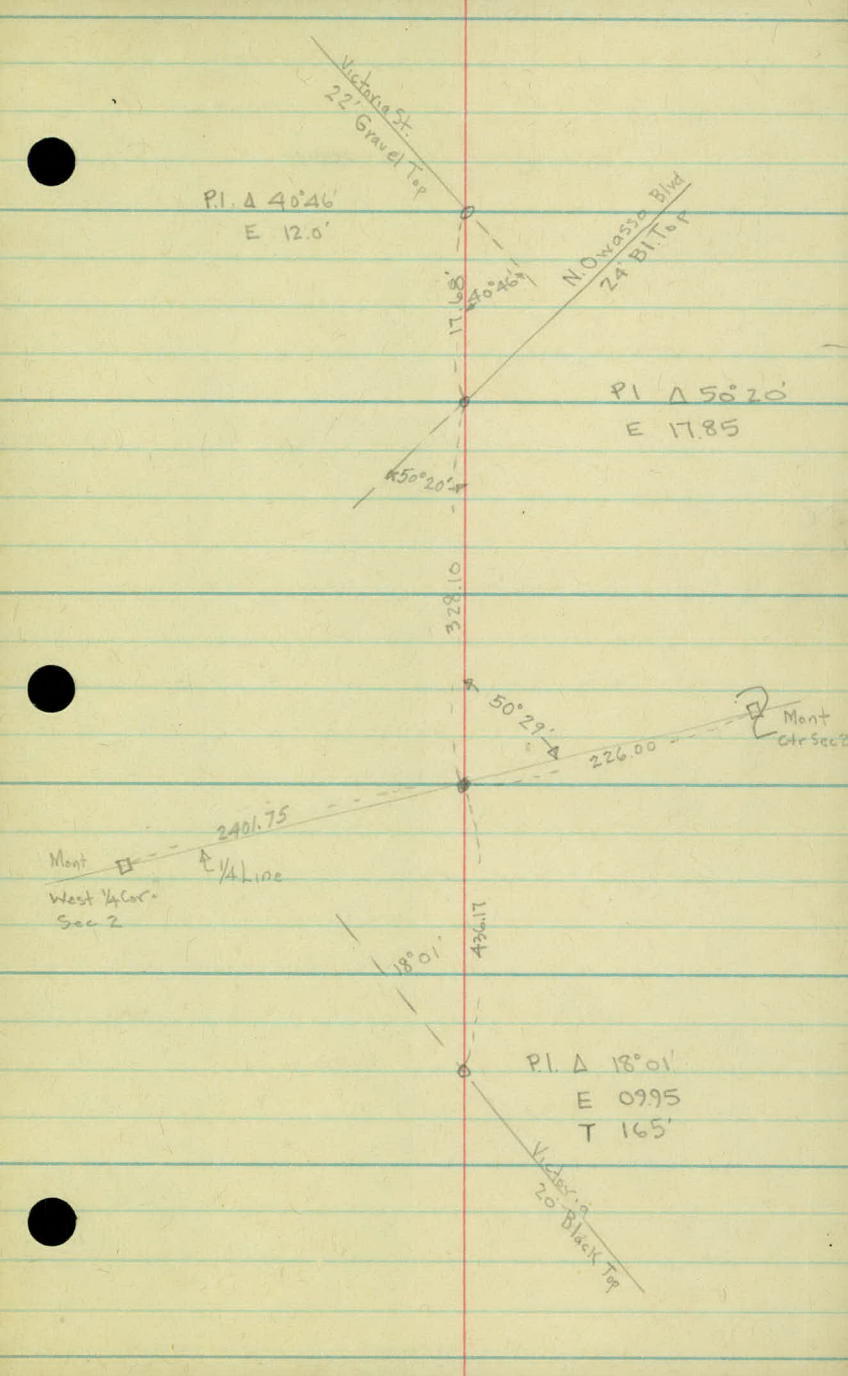

2"x2" Hub
100.00'
2"x2" Hub
2"x2" Hub
75.00'
Nazareth Hall
Tower

11/20/35

Trasit Location

Victoria St.

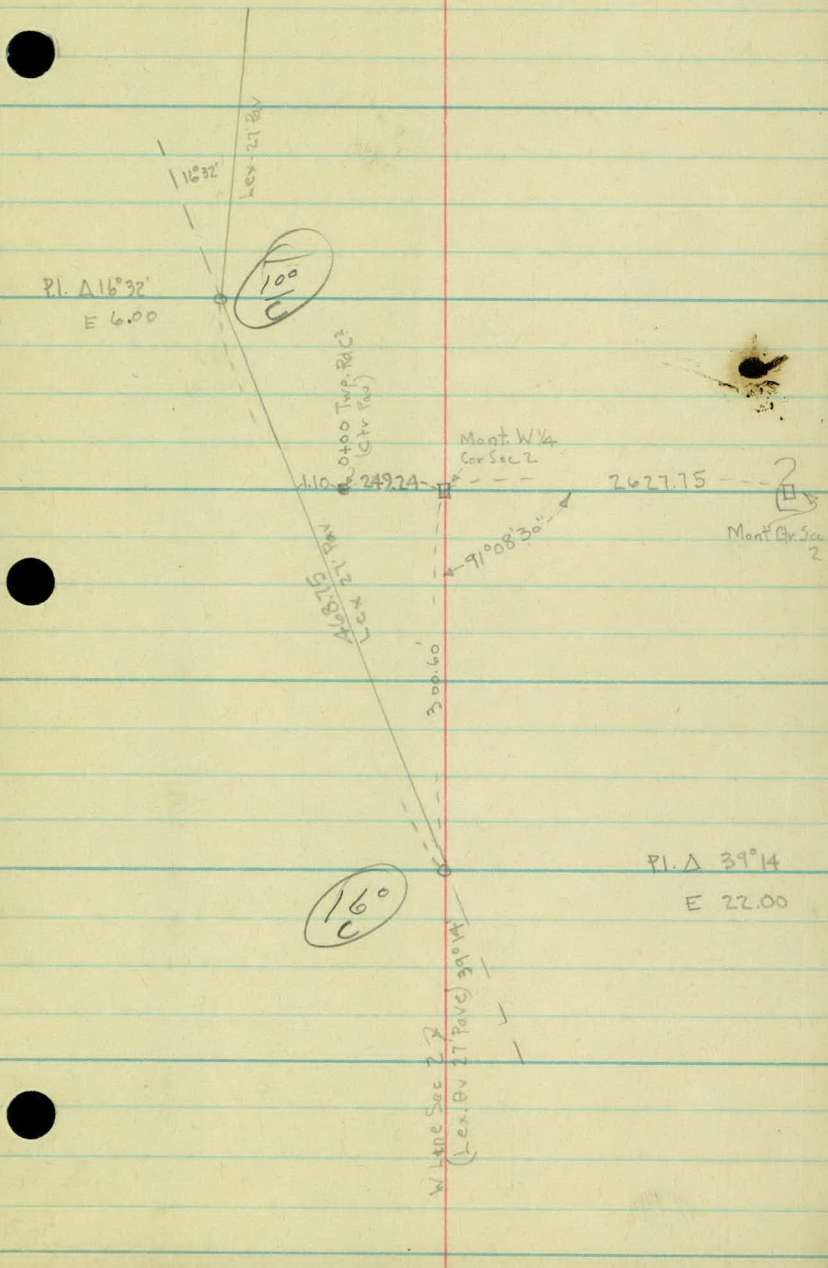
C.2


Victoria St.
22' Gravel Top
P.I. Δ 40°46'
E 12.0'
N. Owasso Blvd
24' Bit. Top
17.38'
40°46'
P.I Δ 50°20'
E 17.85
50°20'
328.10
50°29'
226.00
Mont
Ctr Sec 2
2401.75
Mont
West ¼ Cor.
Sec. 2
℄ ¼ Line
18°01'
436.17
P.I. Δ 18°01'
E 0995
T 165'
Victor...
20' Black Top

11/20/35

Transit Location

Lex. Over $C^{\frac{2}{-}}$


Lex. 27 Pav
16°32'
Pl. Δ 16°32'
E 6.00
10°
C
0400 Twp. Rd 2
(Ctr Pav)
1.10
249.24
Mont. W¼
Cor Sec 2
2627.75
Mont Ctr Sec 2
91°08'30"
Alley 21' Pav
300.60
16°
C
Pl. Δ 39°14
E 22.00
W Lane Sec 2
(Lexington Pave) 39°14'

TOPOG
C²
LEX TO VICTORIA

4

3

+95-12" Tr
0

+74-3-15" Trs
2

+50 Sh. old Fill
40

+11 Sh old Fill
0-27

Sh. old Fill
6-15

3-8" Trs
19

2

+65-3-12" Trs
3

+76-6-8" Trs
0

+46-3-12" W. Trs
4

+33 Sh old Fill
25-0

+82-18" Tr
1

Sh. old Fill
26-4

1

+84 Steps
5

+35 T.P. - Sh old Fill
7 11-36

+58 End Culv - Ed Pav
28 43-84

+19 Ed Pav.
0

+10 End Culv
61

Ed Pav
31

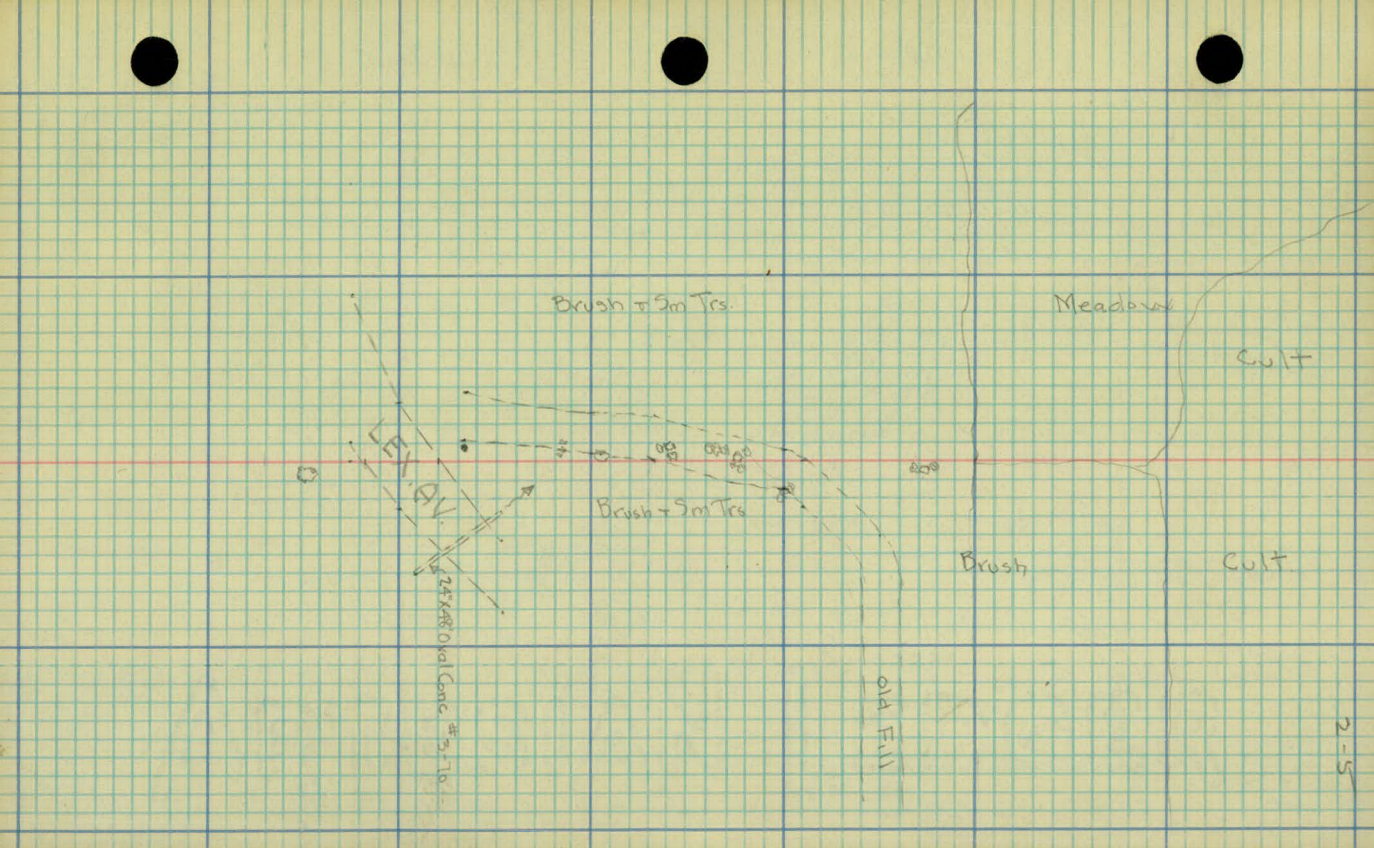
Ed Pav
26

0+00

-24 - Ed Pav
11-89

17 Ed Pav
0

45 Pipe - Tr
0 2


Brush + Sm Trs.
Meadow
Cult
Brush + Sm Trs.
Brush
Cult
Old Fill
24"x48" Oval Conc. #3 To
2-5

+01 House
178

+30 Shoulder
4

+1h Sn.
4

Cu H3

Cu H3

12' OIL TOP (OXFORD SS)

Cu H3

Cu H3

Trail
13-22

18

17

Trail
13-20

16

15

Trail
4-12

+60 Trail
6-15

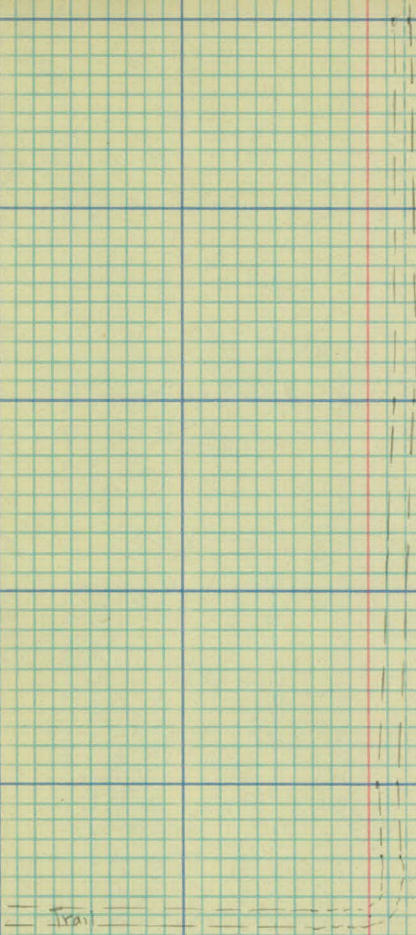
+30 Trail

14

+30 Wagon Trail

13

12


Trail

Ed Pav
53-83

+50 Ed. Rd
98-132
+26 Beg Brush
69-110
Trail
45-61

25

+50 Trail
10-19

24

Trail
7-15

23

Trail
9-16

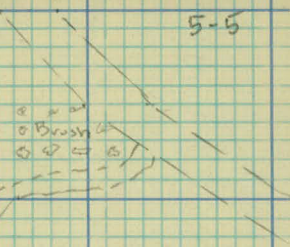
22

21

Trail
8-18

20

19



27

Ed. Pav
80 - 44

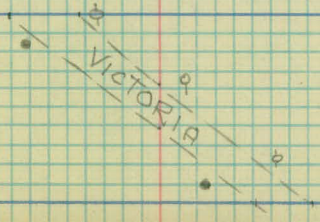
P.P.
35

+95 T.P.
71

+64 Ed Pav
0
+51 Ed Pav
0
+32 Ed Pav
0

+65 Rd Sw
11
+23 P.P.
62
+10 T.P
23

26


VICTORIA

11/14/35

Levels

Proposed Hwy. Co. Rd. C^2

Lexington to Victoria

Sta	+	π	−		
B.M.	1.42	911.75			910.33
⊙	2.10	903.51	10.34	901.41	
B.M.	11.76	912.77	2.50	901.01	
⊙	9.71	920.03	2.45	910.32	
⊙	13.36	932.80	0.59	919.44	
⊙	13.24	944.89	1.15	931.65	
⊙	6.54	950.67	0.76	944.13	
B.M.			0.29	950.38	
⊙	0.77	938.50	12.94	937.73	
⊙	0.61	925.78	13.33	925.17	
⊙	0.58	913.45	12.91	912.87	
⊙	0.72	901.99	12.18	901.27	

Spk. in 18" Oak W. Side School Yard @ Victoria & Co Rd "C"

Placed Spk in 12" W. Oak 20' W. of Victoria 275' S. of C²

Top Stake Sta 23+00

Top Stake Sta 13+00

Top Door Sill (W. Edge) House 200' Rt. Sta 11+00

Top Stake Sta 4+50

Sta	+	x	−	
		901.99		
B.M.			10.73	891.26
⊙	4.79	894.37	12.41	889.58
B.M.			3.84	890.53

Top Rock 10' Rt Sta 2+25

Top Stake Sta 2+00

SpK in 24" Oak 50' W. Sta 0+00

X-Sections

Twp. Rd C²

Lex. to Victoria

Sta	+	⊼	−		
BM.	3.84	894.37			890.53
0+00				89.12	
+23				88.1	
+29				85.6	
+50				84.5	
1+00				84.6	
+28				86.6	
+50				86.7	
2				88.8	

Spk in 24" B. Oak 50' W. Sta 0+00

8.4/100 8.6/89 7.9/59 53- 9.0/46 6.4/34 El? 6.05/27 5.25 E.R. 4.74/18 4.8/21 6.8/27 7.3/34 9.0/41 9.2/50 8.2/54 6.8/100

7.9/92 9.0/87 9.3/70 - 9.2/52 7.2/40 7.9/35 6.4/16 6.8/11 8.3/7 8.4/4 6.3 E.R. 5.91/5 ℄ 5.24/26 E.R. 4.95/46 5.2/56 8.5/69 8.2/88 6.9/92-100

7.5/98 9.2/110

(oval) F.L. 24" Conc. W. End 8.98

#3-70 " " " E. 9.86

48' long

8.8

9.8/120 10.8/90 9.8/62 10.0/38 7.5/33 7.9/30 8.0/17 6.8/11 9.6/3 9.9 9.0/21 6.1/27 E.R. 5.79/33 ℄ 5.02/53 E.R. 4.76/73 4.9/79 7.6/86 8.0/100

7.6/100 7.2/92 60- 10.2/32 7.8/27 8.0/19 7.5/6 9.8 10.2/28 10.0/47 9.5/71 Sh? 4.8/93 E.R. 4.11/100

7.8

8.2/100 10.2/42 10.4/27 7.1/18 8.0/7 7.7 10.3/7 10.6/100

9.5/100 10.4/14 6.0/6 5.6 5.3/14 9.9/28 10.3/100

Sta	+	⊼	−	
		894.37		
.2 + 12				88.7
+25				84.6
+50				84.4
B.M.	11.22	896.39	9.20	885.17
+71				84.6
3				84.9
+70				87.6
4				90.9
0	12.32	908.12	0.59	895.80

3-10
908.12
901.27
6.85

5.7

$\frac{10.6}{100}$ $\frac{10.7}{28}$ $\frac{10.2}{5}$ 9.8 $\frac{5.5}{8.33}$ $\frac{10.0}{46}$ $\frac{10.4}{100}$

$\frac{11.0}{100}$ $\frac{10.6}{49}$ $\frac{10.3}{27}$ 10.0 $\frac{9.8}{20}$ $\frac{5.0}{42}$ $\frac{2.7}{100}$

Top Mont. W ¼ Cor Sec. 2. 11/14/35

$\frac{13.0}{100}$ $\frac{12.5}{31}$ 11.8 $\frac{10.4}{56}$ $\frac{8.7}{100}$

$\frac{12.8}{100}$ $\frac{12.7}{37}$ 11.5 $\frac{10.2}{32}$ $\frac{7.9}{100}$

$\frac{12.5}{100}$ $\frac{11.3}{27}$ 8.8 $\frac{8.1}{14}$ $\frac{5.9}{45}$ $\frac{0.9}{100}$

$\frac{12.1}{100}$ $\frac{10.7}{37}$ $\frac{5.6}{5}$ 5.5 $\frac{4.9}{10}$ $\frac{0.3}{48}$ $\frac{+5.6}{100}$

Sta	+	=	−	
		908.12		
4+50				01.2
⊙	12.19	919.91	0.40	907.72
5				13.4
⊙	9.26	928.46	0.71	919.20
+32				19.1
6				21.1
+30				20.6
7				24.1
+70	Place 24" Culvert			20.5

$\frac{22.5}{100}$ $\frac{20.7}{92}$ $\frac{13.7}{80}$ $\frac{9.3}{43}$ $\frac{7.2}{19}$ $\frac{4}{7}$ 6.9 $\frac{4.3}{19}$ $\frac{1.7}{41}$ $\frac{00}{80}$ $\frac{+6.1}{100}$

Top Stake Sta 44+75

$\frac{55.}{150}$ $\frac{25.2}{100}$ $\frac{22.5}{84}$ $\frac{13.4}{34}$ $\frac{9.9}{21}$ $\frac{7.7}{7}$ 6.5 $\frac{1.1}{41}$ $\frac{+4.4}{85}$ $\frac{+4.9}{100}$

$\frac{55.}{225}$ $\frac{29.0}{100}$ $\frac{21.6}{46}$ $\frac{13.0}{17}$ $\frac{9.6}{3}$ 9.4 $\frac{2.0}{71}$ $\frac{1.3}{100}$

$\frac{22.0}{140}$ $\frac{23.0}{100}$ $\frac{21.8}{90}$ $\frac{13.0}{32}$ 7.4 $\frac{3.0}{68}$ $\frac{3.2}{100}$

$\frac{23.0}{150}$ $\frac{21.2}{100}$ $\frac{10.8}{35}$ 7.9 $\frac{5.0}{64}$ $\frac{5.5}{100}$ $\frac{5.7}{130}$

$\frac{55.}{150}$ $\frac{17.9}{100}$ $\frac{13.1}{78}$ $\frac{6.1}{36}$ 4.4 $\frac{4.8}{22}$ $\frac{7.0}{68}$ $\frac{7.2}{100}$ $\frac{6.5}{150}$

$\frac{19.8}{100}$ $\frac{13.7}{59}$ $\frac{9.1}{8}$ 8.0 $\frac{7.4}{61}$ $\frac{6.6}{100}$

Sta	+	x	−	
		928.46		
8				20.7
9				26.2
⊙	13.38	940.16	1.68	926.78
+11	Shoulder Rt			27.2
+20	E Oxford St Rt			27.6
+33	Shoulder			27.7
+38				27.6
10				28.7
+35				31.1

19.8/100 12.4/43 7.8 5.9/36 2.8/100

15.6/100 12.2/85 8.0/61 4.6/33 2.3 1.6/58 +1.0/100

Top Iron Sta 9+06

24.2/100 21.0/80 15.0/25 13.0 9.7/61 7.0/100

27.0/100 22.0/80 15.5/24 12.6 12.6/4 8.5/70 7.4/100

27.5/100 23.0/83 19.6/61 15.7/28 12.5 12.3/3 11.9/24 9.0/70 6.7/100

25.5/100 19.3/61 16.0/32 12.6 11.0/4.6 8.8/86 7.7/100

25.0/100 19.7/61 15.0/38 11.5 10.6/12 3.1/58 00/100

24.0/100 22.3/86 18.3/64 9.1 8.0/10 1.0/53 00/67 +0.5/100

Sta	+	π	−		
		940.16			
11				35.8	
⊙	6.59	944.21	2.54	937.62	
+50				37.1	
12				37.6	
+40				36.0	
13				31.2	
⊙	0.04	931.69	12.57	931.64	931.65
+50				27.3	
14				25.7	

6-10 93.65
12.56

15.3/100 7.9/57 7.5/25 4.4 3.4/12 00/52 +1.8/100

Top Stk Sta 11+97.63

17.4/100 12.1/63 9.7/46 8.2/30 7.1 6.2/15 2.5/55 0.6/72 +3.3/100

16.7/100 9.6/63 7.2/38 6.6 6.4/13 2.8/51 00/82 +2.6/100

16.1/100 10.9/65 8.8/39 8.2 8.8/8-12 5.3/100

17.7/100 14.8/65 13.4/33 13.0 13.0/3 14.0/6 12.8/16 9.8/53 9.0/100

Top Stake Sta. 13+00

9.4/100 6.2/64 4.9/35 5.0/12 4.4 3.7/3 2.9/44 0.5/57 +3.8/100

17.3/100 14.5/62 11.0/27 6.0 4.7/5 4.2/20 +4.6/80 +6.9/100

St				
		931.69		
14+47				24.1
+65				24.5
15				24.5
⊙	4.02	928.31	7.40	924.29
+6.5				22.9
16				18.5
⊙	5.05	924.01	9.35	918.96
17				13.6
18				13.8

19.5 / 100 17.5 / 65 13.2 / 29 9.2 / 10 7.6 6.0 / 4 1.3 / 53 +4.0 / 100

19.8 / 100 12.5 / 58 7.6 / 7 7.2 7.0 / 2 5.3 / 4 4.6 / 15 1.1 / 51 +4.0 / 100

22.8 / 100 16.2 / 42 8.2 / 6 7.2 7.1 / 2 5.4 / 4 5.1 / 12 .00 / 48 +6.5 / 100

Top Iron Sta. 15+63

22.0 / 100 8.3 / 18 7.3 / 2 5.4 4.1 / 3 3.3 / 15 .00 / 34 +6.8 +8.0 / 75 / 100

22.1 / 100 13.0 / 28 10.0 / 6 9.8 9.0 / 3 6.6 / 9 6.5 / 18 +5.7 / 90 +7.0 / 100

21.5 / 100 21.0 / 89 20.7 / 84 10.4 10.3 / 1 8.2 / 6 6.4 / 9 5.4 / 13 3.9 / 41 1.1 / 86 +4.8 / 115

20.8 / 100 18.6 / 36 16.8 / 68 10.6 / 5 10.2 9.3 / 4 6.0 / 13 3.0 / 53 .00 / 74 .55 / 100

Sta	+	⊼	−			
		924.01				
18+20				13.8		
19				12.5		
+45				12.1		
20				12.0		
21				13.1		
22				12.2		
+60				11.5		
⊙	0.60	913.57	11.04	912.97		
✓			32.5	910.32	910.32	

S.S.= Same Slope

3.5 / 100 | 18.3 / 30 | 11.8 / 43 | 10.3 / 3 | 10.2 | 9.6 / 3 | 7.2 / 7 | 5.9 / 12 | 5.0 / 25 | 2.5 / 66 | S.S. / 100

11.2 / 100 | 11.0 / 89 | 13.8 / 38 | 12.0 / 9 | 11.5 | 11.3 / 4 | 9.6 / 9 | 8.8 / 21 | 00 / 82 | +2.5 / 100

9.5 / 100 | 9.2 / 85 | 12.8 / 38 | 11.9 | 11.3 / 6 | 11.0 / 15 | 10.0 / 29 | 7.2 / 70 | 3.8 / 100

9.5 / 100 – 87 | 11.0 / 40 | 12.0 / 13 | 12.0 | 11.4 / 9 | 11.3 / 16 | 10.6 / 20 | 9.0 / 73 | 5.7 / 100

10.6 / 100 | 9.9 / 88 | 10.2 / 69 | 10.3 / 12 | 10.9 | 10.6 / 7 | 10.1 / 8-18 | 8.6 / 100

12.9 / 100 | 12.0 / 83 | 11.7 / 7 | 11.8 | 10.9 / 10 | 10.4 / 18-33 | 10.7 / 100

12.0 / 100 | 11.8 / 86 | 13.2 / 58 | 12.2 / 13 | 12.5 | 11.8 / 7 | 11.9 / 19 | 13.0 / 34 | 15.1 / 59 | 15.4 / 100

Top Stake Sta 22+00

Top Stake Sta 23+00

Sta	+	±	−	
		913.57		
23				09.8
+75				07.2
24				07.0
+40				07.8
25				07.7
26				10.9
+25				10.4
+33				07.2

901.01 BM
9-10

2.9/100 2.3/83 3.8/63 3.1/37 3.3/5 3.8 3.7/8-15 6.3/61 6.4/100

4.0/100 3.6/88 4.5/74 5.9/34 6.4 6.3/5 6.7/14 8.4/61 6.0/100

3.2/100 3.0/89 4.1/74 6.3/18 6.6 6.5/6 6.7/15 7.8/42-56 7.3/75 6.8/100

3.3/100 2.8/86 3.7/73 5.0/24 5.8 5.4/7 4.9/12 5.7/20 6.7/36 11.3/66 10.5/88 11.0/100

5.6/100 4.8/32 5.9 5.6/9 6.6/16 8.1/47 11.3/100

Dif ER Eff
2.0/100 0.4/81 1.6/31 2.7 2.6/7 2.0/12 1.7/31 7.5/42 82 8.3/51 69
7.6/101 9.8/77 Dif 7.4/87 ER

Dif E.R. Eff ER Dif
2.6/100 0.8/80 1.8/30 3.2 6.3/8 7.2/16 6.9/33 7.5/48 8.1/56 4.4/65 6.2/100

6.4

		913.57			
26 + 38	Edge Road			07.0	
26 + 51.0	& Victoria St.			907.64	
B.M.	2.10	903.11	12.56	901.01	901.01
⊙	10.18	911.60	1.69	901.42	
B.M.			1.27	910.33	910.33

901.41
10-70

6.56

			Dtf	ER		E.R.	Dtf		
2.5/100	1.0/85	2.8/28	5.7/25	6.08/15	5.93	6.70/16	7.0/24	3.5/32	6.1/100

5pK in 18" W.Oak W.Side School #24 Yard