

Book #22, Dr. 11

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

_____ Plan _____ Survey

_____ DRAPER AVE. _____

From Hamline To Sedalia.

Road Acc't. No. R31

Date Filed Sept. 1935 File 11

8/29/35

X-Sections Draper Ave
Hamline Av. & Sedalia

Placed
to
Co. Board.
Sept. 16, 1935

Sta	+	π	-	Elev.
-----	---	-------	---	-------

B.M.	478	962.55 [✓]		957.77
------	-----	---------------------	--	--------

B.M.			9.18	953.37 [✓]
------	--	--	------	---------------------

B.M.	639	967.21 [✓]	173	960.82 [✓]
------	-----	---------------------	-----	---------------------

0		± Hamline		959.7
---	--	-----------	--	-------

+08				959.3
-----	--	--	--	-------

+15				958.6
-----	--	--	--	-------

+24				960.7
-----	--	--	--	-------

+30				964.5
-----	--	--	--	-------

+50				964.3
-----	--	--	--	-------

1				959.9
---	--	--	--	-------

S.E. Cor Conc. Steps NE. Cor A² r Hamline

Top Mont A² r Hamline

Spk in PP. 330' N of A² on Hamline

$$\begin{array}{r} 59.2 \\ 8.02 \\ \hline 100 \end{array} \quad \begin{array}{r} 7.71 \\ \hline 51 \end{array} \quad \begin{array}{r} 59.7 \\ 7.50 \\ \hline 51 \end{array} \quad \begin{array}{r} 58.9 \\ 8.30 \\ \hline 100 \end{array}$$
$$\begin{array}{r} 58.9 \\ 8.26 \\ \hline 100 \end{array} \quad \begin{array}{r} 8.18 \\ \hline 52 \end{array} \quad \begin{array}{r} 59.3 \\ 7.92 \\ \hline 53 \end{array} \quad \begin{array}{r} 58.6 \\ 8.20 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 58.5 \\ 8.7 \\ \hline 100 \end{array} \quad \begin{array}{r} 7.9 \\ \hline 52 \end{array} \quad \begin{array}{r} 58.6 \\ 8.6 \\ \hline 52 \end{array} \quad \begin{array}{r} 57.8 \\ 9.4 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 59.7 \\ 7.5 \\ \hline 100 \end{array} \quad \begin{array}{r} 7.9 \\ \hline 70 \end{array} \quad \begin{array}{r} 6.2 \\ \hline 36 \end{array} \quad \begin{array}{r} 60.7 \\ 6.5 \\ \hline 30 \end{array} \quad \begin{array}{r} 58.5 \\ 7.9 \\ \hline 67 \end{array} \quad \begin{array}{r} 8.7 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 62.8 \\ 4.4 \\ \hline 100 \end{array} \quad \begin{array}{r} 4.3 \\ \hline 75 \end{array} \quad \begin{array}{r} 3.7 \\ \hline 70 \end{array} \quad \begin{array}{r} 64.5 \\ 2.7 \\ \hline 29 \end{array} \quad \begin{array}{r} 3.4 \\ \hline 66 \end{array} \quad \begin{array}{r} 5.2 \\ \hline 100 \end{array} \quad \begin{array}{r} 6.5 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 62.2 \\ 5.0 \\ \hline 100 \end{array} \quad \begin{array}{r} 5.3 \\ \hline 80 \end{array} \quad \begin{array}{r} 5.1 \\ \hline 53 \end{array} \quad \begin{array}{r} 4.0 \\ \hline 71 \end{array} \quad \begin{array}{r} 64.3 \\ 2.9 \\ \hline 31 \end{array} \quad \begin{array}{r} 2.2 \\ \hline 62 \end{array} \quad \begin{array}{r} 2.0 \\ \hline 100 \end{array} \quad \begin{array}{r} 63.9 \\ 3.3 \\ \hline 100 \end{array}$$

$$\begin{array}{r} 58.8 \\ 8.4 \\ \hline 100 \end{array} \quad \begin{array}{r} 8.1 \\ \hline 78 \end{array} \quad \begin{array}{r} 7.8 \\ \hline 41 \end{array} \quad \begin{array}{r} 59.9 \\ 7.3 \\ \hline 42 \end{array} \quad \begin{array}{r} 5.7 \\ \hline 77 \end{array} \quad \begin{array}{r} 4.3 \\ \hline 100 \end{array} \quad \begin{array}{r} 62.7 \\ 4.5 \\ \hline 100 \end{array}$$

Sta

+

 π

-

Elev.

967.21

1+50

957.7

2

956.1

①

1.11

958.03

10.29

956.92

+50

~~961.5~~ 52.3

3

951.2

+50

951.8

4

953.4

+19

953.0

+50

951.2

56.6

 $\frac{10.6}{100}$ 76 - $\frac{10.8}{39}$

57.7

95

 $\frac{7.7}{35}$ $\frac{6.7}{62}$

60.3

 $\frac{6.9}{100}$

53.9

 $\frac{13.3}{100}$ $\frac{13.6}{59}$ $\frac{12.7}{30}$

56.1

11.1

 $\frac{9.0}{39}$ $\frac{8.3}{67}$ $\frac{8.8}{100}$

58.4

Top stake Sta 52.2

 $\frac{5.8}{100}$ $\frac{6.0}{73}$ $\frac{6.3}{38}$

52.3

5.7

 $\frac{4.2}{33}$ $\frac{3.0}{64}$ $\frac{2.6}{100}$

55.4



51.2

53.9

Lt 5.45

51.9

 $\frac{6.8}{33}$ $\frac{5.7}{65}$ $\frac{4.4}{100}$ $\frac{4.1}{42}$ $\frac{6.8}{81}$ $\frac{6.0}{100}$ $\frac{6.1}{100}$

53.0

 $\frac{5.0}{100}$ $\frac{4.4}{76}$ $\frac{5.5}{38}$

51.8

6.2

 $\frac{6.0}{63}$ $\frac{6.1}{100}$

51.9

51.5

 $\frac{6.5}{100}$ $\frac{6.1}{80}$ $\frac{5.7}{45}$

53.4

4.6

 $\frac{5.5}{51}$ $\frac{7.3}{100}$

50.7

50.6

 $\frac{7.4}{100}$ $\frac{6.8}{74}$ $\frac{6.2}{40}$

53.0

5.0

 $\frac{5.6}{46}$ $\frac{7.2}{82}$ $\frac{7.8}{100}$

50.2

49.8

 $\frac{8.2}{100}$ $\frac{7.6}{75}$ $\frac{7.3}{36}$

51.2

6.8

 $\frac{7.1}{47}$ $\frac{8.8}{100}$

49.2

Sta	+	-	Elev.
-----	---	---	-------

		958.03	
--	--	--------	--

5			948.3
---	--	--	-------

	+50		948.2
--	-----	--	-------

6			948.8
---	--	--	-------

	+50		947.9
--	-----	--	-------

7			948.3
---	--	--	-------

	+50		949.2
--	-----	--	-------

8			948.4
---	--	--	-------

0	3.70	949.51	12.22	945.81
---	------	--------	-------	--------

	+50		945.0
--	-----	--	-------

50.2

$\frac{7.8}{100}$	$\frac{7.8}{70}$	$\frac{8.8}{34}$	9.7	$\frac{10.1}{53}$	$\frac{10.4}{100}$
-------------------	------------------	------------------	-----	-------------------	--------------------

48.3

47.4

51.7

100 -	$\frac{6.3}{88}$	$\frac{7.4}{55}$	$\frac{8.9}{38}$	9.8	$\frac{10.6}{43}$	$\frac{10.5}{100}$
-------	------------------	------------------	------------------	-----	-------------------	--------------------

48.2

47.5

51.3

100 -	$\frac{6.7}{95}$	$\frac{7.5}{68}$	$\frac{8.6}{33}$	9.2	$\frac{10.3}{46}$	$\frac{10.7}{100}$
-------	------------------	------------------	------------------	-----	-------------------	--------------------

48.8

47.3

50.3

$\frac{7.7}{100}$	$\frac{8.0}{81}$	$\frac{9.0}{45}$	10.1	$\frac{10.8}{57}$	$\frac{11.0}{100}$
-------------------	------------------	------------------	------	-------------------	--------------------

47.9

47.0

50.5

$\frac{7.5}{100}$	$\frac{7.4}{66}$	$\frac{8.3}{33}$	9.7	$\frac{11.1}{54}$	$\frac{11.1}{100}$
-------------------	------------------	------------------	-----	-------------------	--------------------

48.3

46.9

50.2

$\frac{7.8}{100}$	$\frac{7.2}{69}$	$\frac{7.4}{35}$	8.8	$\frac{10.5}{48}$	$\frac{10.5}{100}$
-------------------	------------------	------------------	-----	-------------------	--------------------

49.2

47.5

49.0

$\frac{9.0}{100}$	$\frac{9.3}{74}$	$\frac{9.0}{35}$	9.6	$\frac{10.8}{36}$	$\frac{11.0}{67}$	$\frac{10.6}{82}$	$\frac{11.0}{100}$
-------------------	------------------	------------------	-----	-------------------	-------------------	-------------------	--------------------

48.4

47.0

Top Stake Sta 8+50

46.8

$\frac{2.7}{100}$	$\frac{2.5}{72}$	$\frac{4.0}{38}$	15.3	$\frac{3.7}{47}$	$\frac{2.8}{100}$
-------------------	------------------	------------------	------	------------------	-------------------

45.0

46.7

Sta

+

K

-

Elev.

949.51

9

942.6

+50

941.3

10

941.5

+50

943.0

11

944.5

+50

943.3

12

942.4

+50

943.3

44.0

 $\frac{5.5}{100}$ $\frac{6.4}{72}$ $\frac{6.9}{43}$

42.6

 $\frac{6.1}{32}$ $\frac{5.2}{68}$

44.9

 $\frac{4.6}{100}$

42.2

 $\frac{7.3}{100}$ $\frac{7.9}{45}$

41.3

 $\frac{8.2}{46}$ $\frac{8.0}{46}$

42.3

 $\frac{7.2}{100}$

42.7

 $\frac{6.8}{100}$ $\frac{7.1}{88}$ $\frac{7.8}{42}$

41.5

 $\frac{8.0}{53}$ $\frac{7.6}{53}$

42.6

 $\frac{6.9}{100}$

44.2

 $\frac{5.3}{100}$ $\frac{5.2}{81}$ $\frac{6.0}{38}$

43.0

 $\frac{6.5}{32}$ $\frac{6.8}{32}$ $\frac{7.0}{65}$

42.0

 $\frac{7.5}{100}$

44.8

 $\frac{4.7}{100}$ $\frac{4.7}{32}$

44.5

 $\frac{5.0}{3}$ $\frac{4.7}{5}$ $\frac{6.1}{5}$ $\frac{6.9}{11}$ $\frac{6.1}{26}$

43.1

 $\frac{6.4}{50}$

43.7

 $\frac{5.8}{64}$

Hot Ho

Floor Conc Blk Ho E.I. = 94499

45.2

 $\frac{4.3}{100}$ $\frac{4.6}{83}$ $\frac{5.6}{35}$

43.3

 $\frac{6.2}{5}$ $\frac{6.3}{5}$ $\frac{7.1}{15}$ $\frac{7.4}{40}$ $\frac{6.5}{69}$

43.0

46.9

 $\frac{2.6}{100}$ $\frac{5.6}{61}$ $\frac{6.6}{32}$

42.4

 $\frac{7.1}{43}$ $\frac{7.3}{43}$

43.1

 $\frac{6.4}{69}$

46.6

 $\frac{2.9}{100}$ $\frac{4.7}{74}$ $\frac{5.6}{43}$

43.3

 $\frac{6.2}{45}$ $\frac{6.4}{45}$

44.2

 $\frac{5.3}{84}$

Sta	+	π	-	Elev.
		949.51		

12+86				945.8
-------	--	--	--	-------

+90	West Dt.	Seel		944.7
-----	----------	------	--	-------

+95	Shoulder			946.5
-----	----------	--	--	-------

13+04	$\pm$	Sedalia Grading		946.7
-------	-------	-----------------	--	-------

B.M.			5.38	944.13
------	--	--	------	--------

0	4.04	953.45	0.10	949.41
---	------	--------	------	--------

0	7.28	959.62	1.11	952.34
---	------	--------	------	--------

B.M.			1.84	
------	--	--	------	--

$$\begin{array}{r} 59.6 \\ 57.77 \\ \hline 1.85 \end{array}$$

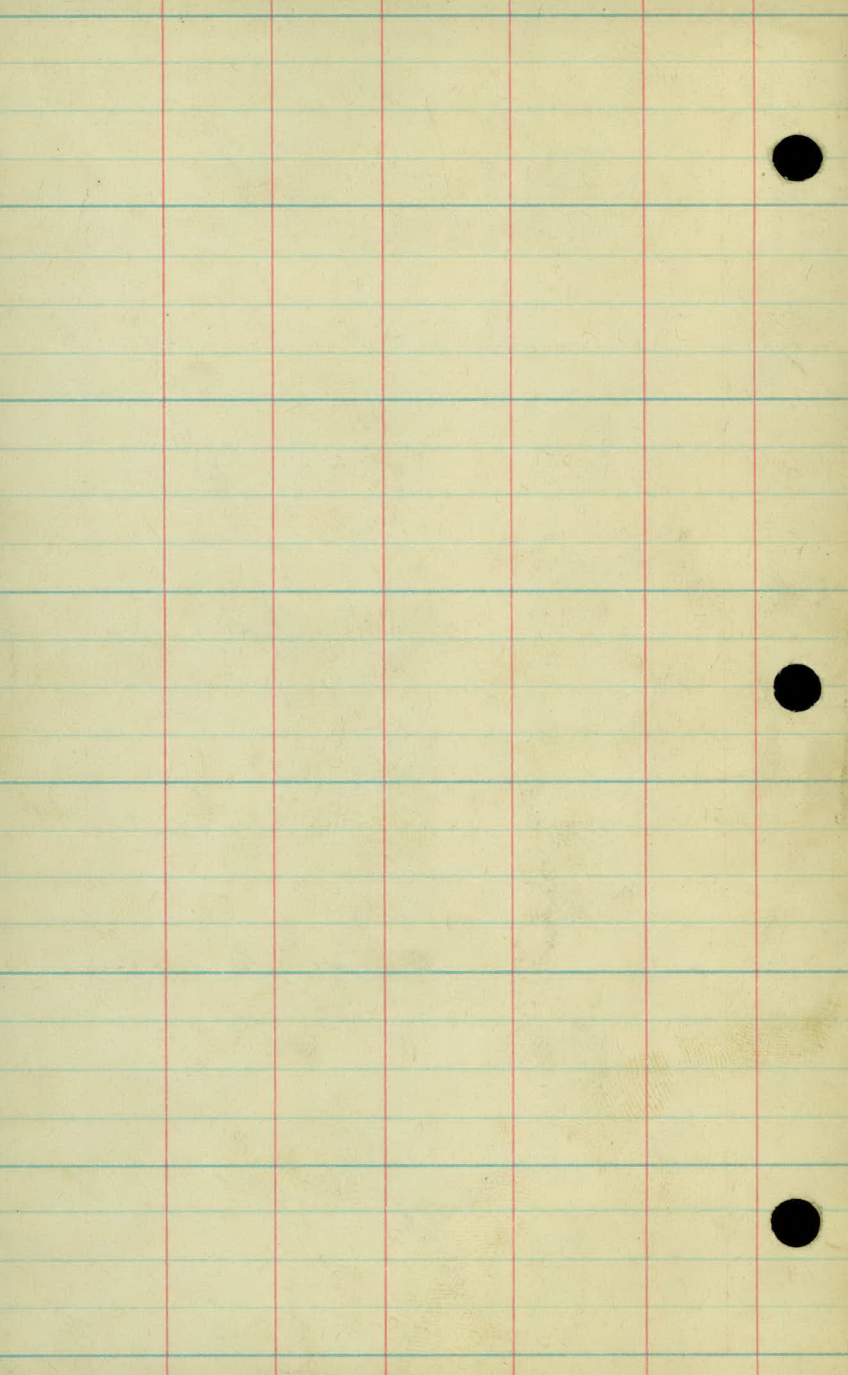
$$\begin{array}{r} 46.9 \\ 2.6 \quad 3.9 \quad 3.4 \quad 45.8 \quad 44.1 \\ 100 \quad 61 \quad 30 \quad 3.7 \quad 22 \quad 46 \quad 5.4 \\ 70 \end{array}$$

$$\begin{array}{r} 47.0 \\ 2.5 \quad 3.8 \quad 4.2 \quad 44.7 \quad F.L. \quad 44.1 \\ 100 \quad 58 \quad 22 \quad 4.8 \quad 5.7 \quad 5.3 \quad 5.4 \\ 27 \quad 45 \quad 81 \end{array}$$

$$\begin{array}{r} 48.7 \\ 0.8 \quad 1.7 \quad 2.3 \quad 46.5 \quad 45.4 \\ 100 \quad 70 \quad 34 \quad 3.0 \quad 3.5 \quad 4.0 \quad 4.1 \\ 21 \quad 58 \quad 100 \end{array}$$

$$\begin{array}{r} 49.1 \\ 0.4 \quad 1.4 \quad 2.0 \quad 46.7 \quad 45.5 \\ 100 \quad 70 \quad 42 \quad 2.8 \quad 3.4 \quad 3.7 \quad 4.0 \\ 35 \quad 79 \quad 100 \end{array}$$

Top Coal Chute Wall NE Cor on North Side Bldg Rt Sta



Purtell
8/29/35

Draper Ave Alignment

~~Mr. Pottier~~

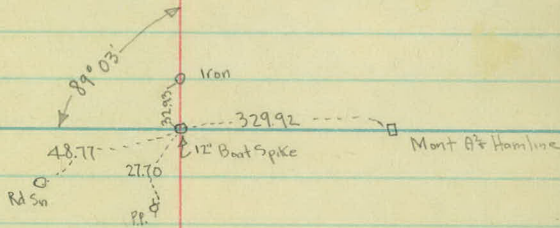
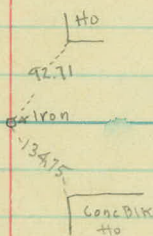
~~Hv. 3088~~

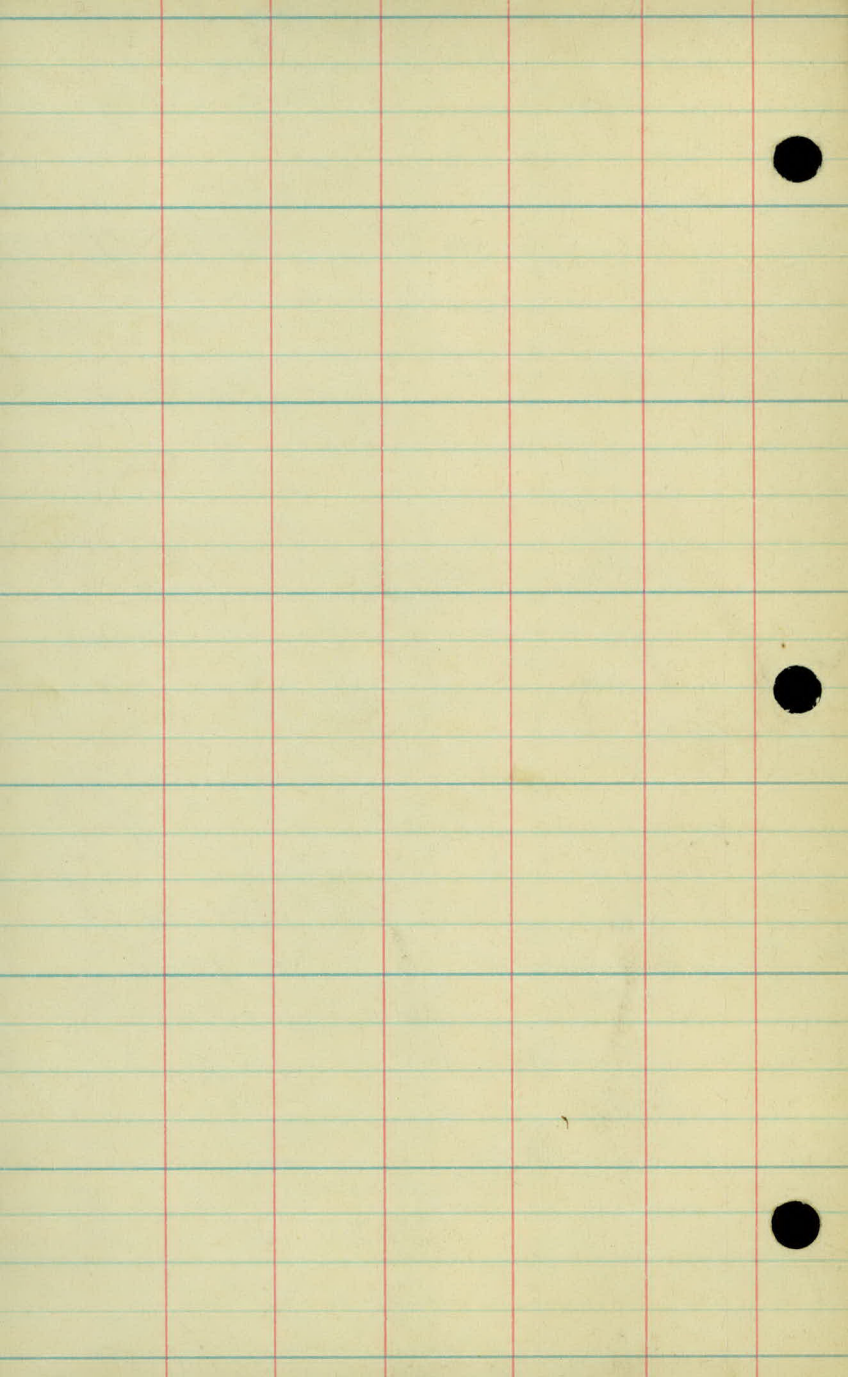
~~To be called
when plan
is complete~~

12 + 09.28

0 + 00

E Hamline Ave





1-3
8/30/35

TOPOGRAPHY
DRAPER STREET
HAMLINE TO SEDALIA

5

4

3

2

1

0+00

cult.

cult.

Hamline Ave

18" Black Top

φ

+96 Shoulder Sedalia (New Grading)

+46 Cor Ho
87

+90 Hot H. Cor
69

12

11

+51 Cor Bldg
31

10

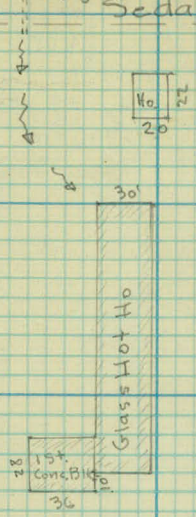
9

8

7

+75 Po. Line X's
79 - 43

6



Cultivated

Cultivated

+14 Shoulder Sedalia

+054 Sedalia 10" X 26' CM
27

DRAPER AVE.

Slope Stakes.

5 Pages

Sta.	+	-	Grade
B.M.	5.15	965.97	960.82

0	+00		59.3
---	-----	--	------

	+30		59.1
--	-----	--	------

1			57.8
---	--	--	------

	+50		56.4
--	-----	--	------

2			59.7
---	--	--	------

T.P.	1.60	957.29	10.28	955.69
------	------	--------	-------	--------

	+50		53.0
--	-----	--	------

3			51.5
---	--	--	------

	+50		50.4
--	-----	--	------

4			49.5
---	--	--	------

	+19		49.3
--	-----	--	------

	+50		48.9
--	-----	--	------

Cut 0.0 = 260
 20. 00 = 21.5

1

Rod Lt R Rt

Spr in PP Vd of 0 to 100.

4.5

6.9 40.1 / $\frac{2.2}{+4.7}$ $\frac{5.5}{+1.4}$ $\frac{2.6}{+4.3/38.9}$

8.2 30.8 / $\frac{6.6}{+1.6}$ $\frac{6.5}{+1.7}$ $\frac{4.4}{+3.5/37.4}$

9.6 27.5 / $\frac{9.1}{+1.5}$ $\frac{8.3}{+1.3}$ $\frac{6.3}{+3.3/35.9}$

11.3 24.5 / $\frac{11.8}{+1.0}$ $\frac{9.4}{+1.9}$ $\frac{8.4}{+2.9/34.7}$

4.3 21.5 / $\frac{5.8}{+0.0}$ $\frac{5.2}{-0.9}$ $\frac{4.0}{+0.3/26.9}$

5.7 25.4 / $\frac{6.0}{+1.3}$ $\frac{5.0}{+0.8/28.4}$

6.7 31.7 / $\frac{5.0}{+1.9}$ $\frac{5.4}{+1.5}$ $\frac{5.1}{+1.8/31.4}$

7.8 35.3 / $\frac{4.7}{+1.1}$ $\frac{7.2}{+3.6}$ $\frac{4.1}{+2.7/37.1}$

8.0 34.4 / $\frac{5.2}{+2.8}$ $\frac{4.7}{+3.3}$ $\frac{4.4}{+3.6/36.8}$

8.4 32.6 / $\frac{6.2}{+2.2}$ $\frac{6.1}{+2.3}$ $\frac{6.1}{+2.3/32.9}$

Sta.	+	X	-	Grade
		957.29		
5				48.4
+50				48.0
6				47.7
+50				47.5
7				47.2
T.P.	3.41	951.79	8.91	748.38
+50				46.7
8				46.0
+50				45.1
9				44.1
+50				43.3
				194 41.4
10				10.3 43.0 41.5

Elev	+	X	-	Grade.
------	---	---	---	--------

B.M.	2.74	963.36		960.82
------	------	--------	--	--------

T.P.	2.92	954.58	11.90	951.66
------	------	--------	-------	--------

5				48.6
---	--	--	--	------

+50				48.5
-----	--	--	--	------

6				48.7
---	--	--	--	------

+50				49.0
-----	--	--	--	------

7				49.1
---	--	--	--	------

+50				48.7
-----	--	--	--	------

8				47.9
---	--	--	--	------

+50				46.6
-----	--	--	--	------

9				45.3
---	--	--	--	------

+50				44.3	41.4
-----	--	--	--	------	------

T.P.	6.93	949.05	12.46	942.12	
------	------	--------	-------	--------	--

10				43.8	7.6 41.5
----	--	--	--	------	-------------

Lat.	Long.	Alt.	Dist.
Spt in P.P. W/ 0400			
6.0	$28.1 / 5.9$ 10.7	7.2 -1.2	6.8 $R.07 / 22.6$
6.1	$28.4 / 5.3$ 10.8	7.1 -1.0	7.2 $R.09 / 22.7$
5.9	$28.1 / 5.0$ 10.9	5.6 $+0.3$	6.1 $R.13 / 22.4$
5.6	$28.5 / 6.1$ $R.10$	6.6 -1.0	6.9 $R.08 / 22.1$
5.5	$27.2 / 5.1$ 10.7	6.2 -0.1	6.9 $R.01 / 21.8$
5.9	$31.4 / 4.1$ 11.8	5.4 $+0.5$	6.3 $R.11 / 24.8$
6.7	$30.2 / 5.3$ 11.4	5.9 $+0.8$	7.1 $R.11 / 24.8$
8.0	$25.9 / 9.2$ $R.03$	9.5 -1.5	9.2 $R.03 / 22.4$
9.2	$21.1 / 11.9$ -2.7	12.0 -2.8	11.5 $-2.3 / 19.9$
10.3	$25.4 / 13.1$ $R.00$ $21.4 / 13.1$ -2.8	13.2 -2.9	13.0 $-2.7 / 21.1$ 13.1 $R.00 / 25.1$
5.3	$24.8 / 7.3$ $R.03$	7.3 -2.1	7.6 -2.3 7.5 -2.2 7.5 $R.01 / 24.8$

Sta	+	π	-	Grade	
		949.05			
10	+50			43.5	7.5 41.6
T.P.					
B.M.			405	945.00	945.04
					7.4 41.7
11				43.7	
T.P.		948.89			
	+50			44.2	418
12				44.9	41.9
	+50			45.6	
	+86			46.1	
B.M.			3.85	945.04	

C. Rod

Lt

R

Rt

5.6	$289 / 5.6$ 18.19	5.6 0.0	61 -0.5	5.0 -0.6	50 $18.25 / 30.0$
-----	------------------------	----------------	----------------	-----------------	------------------------

Top. N. End. Ent. Culv.

5.4	$22 / 4.3$ 18.21	43 $+1.1$	45 $+0.9$	55 -0.1	55 $18.19 / 28.7$
-----	-----------------------	----------------	----------------	----------------	------------------------

4.7	$30 / 50$ 18.21	50 -0.3	55 -0.8	65 -1.0	65 $18.06 / 26.0$
-----	----------------------	----------------	----------------	----------------	------------------------

4.0	$29.0 / 60$ 18.10	60 -2.0	64 -2.4	65 -2.5	65 $18.05 / 27.5$
-----	------------------------	----------------	----------------	----------------	------------------------

3.3	$19.6 / 55$ -2.2		60 -2.7		61 $-2.8 / 21.4$
-----	-----------------------	--	----------------	--	-----------------------

2.8	$260 / 2.8$ $+0.0$		3.3 -0.5		46 $-1.8 / 18.4$
-----	-----------------------	--	-----------------	--	-----------------------

