

Book #20, Dr. 11

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

..... PLAN Survey

MINNESOTA AVE.

From DALE ST. To RICE ST.

Road Acc't. No.

Date Filed

File 11

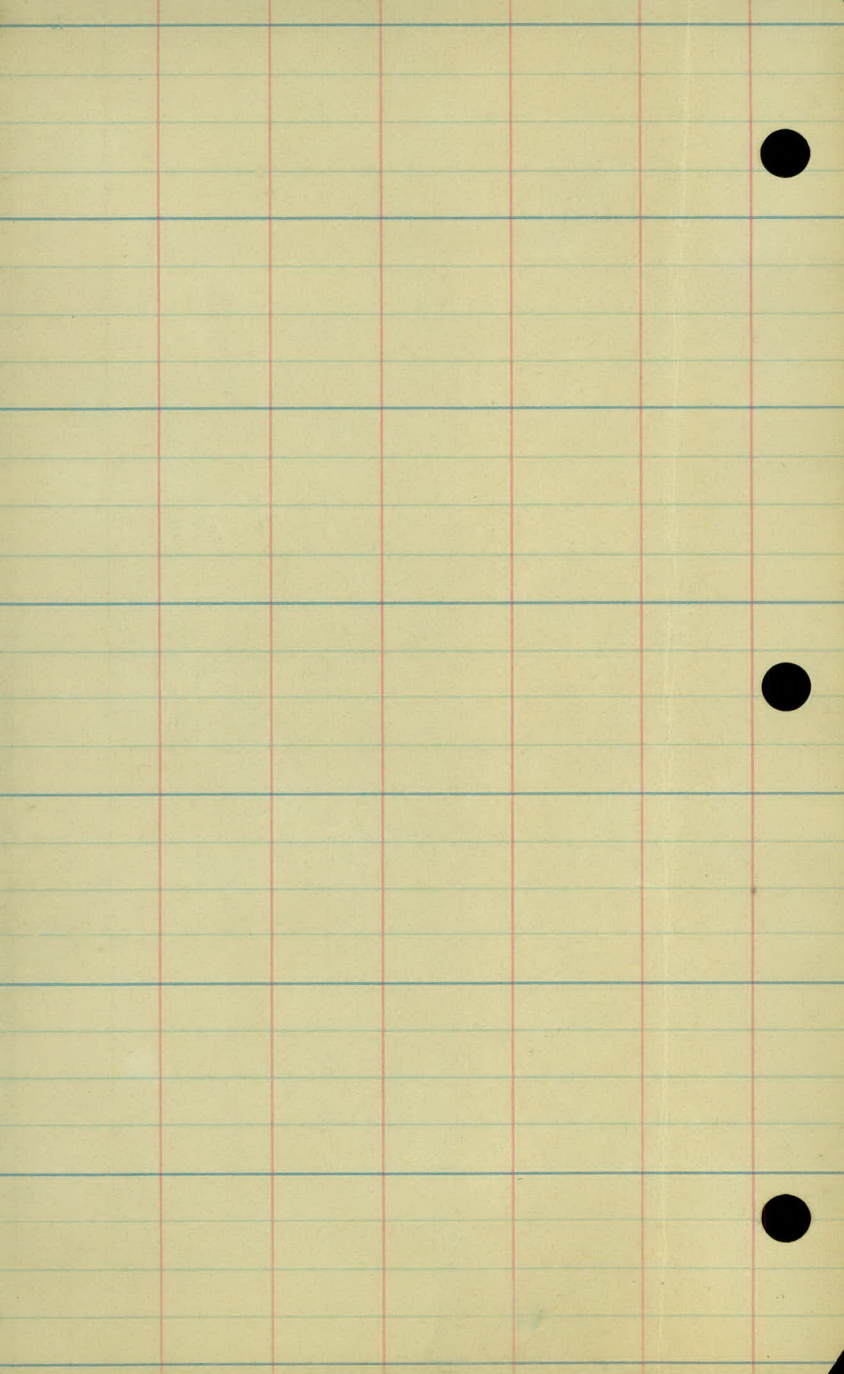
Plans Survey
Minnesota Avenue.
From Dale St. to Rice St.

Index.

Alignment	P. 1 to P. 3
Topography.	P. 4 to P. 12
Cross Sections.	P. 13 to P. 25

Plans
Complete
Aug. 8/1935

W. A. Carson
July 1935



Alignment

Sta.	Point	LT	Angle RT
------	-------	----	-------------

26+12.7	R1	0218'	
---------	----	-------	--

22+89.0	POT.		
---------	------	--	--

19+58.9	POT		
---------	-----	--	--

16+32.5	POT.		
---------	------	--	--

13+06.0	POT.		
---------	------	--	--

5+51.5	POT.		
--------	------	--	--

4+00	P.O.T.		
------	--------	--	--

0+00			
------	--	--	--

Mon.

Center
Sec. 12
T. 29. R. 23

1322.4
16 Rd. Sy.

89° 28'

E Western D.

(2)

Mon

33.1' I.P.

34.5' I.P.

31.5' I.P.

27.15' I.P.

44.6' I.P.

Forc'd

Cor. Ho.

62.54'

Spike

44.97'

T.P.

T.P.

54.70'

Spike

1315.09'

E Dale St.

37.6'

T.P.

Mon.

□

1315.09'

Mon.

□

S.W. Cor.
Sec. 12

July 3, 1935

W.H.C.
J.A.
L.B.H.

Sta.

Point

52+30.1

2 Rice.

48+18.3

P.O.T.

59+00

P.O.T.

38+77.83

P.O.T.

28+00

P.O.T.

3

Mon.

E

1315.82

Drilled Hole in Rove.

1315.82

Mon.

E

S.E. COR.
Sec. 12

P.P. O

41.53

31.73

O.P.P.

T.P. O

47.65

22.47

P.P.

33.35

40+47.5

Co. Rd. B.2

1 Door Ship
3 Nails Top 12' x 4' Post.
Car. Garage

34.21

Hub

T.P. O

54.75

Iron Pipe

32.62

33.3

38+42 (Anstrang)

33.2

1/P 34+37

33.2

34+32 Anstrang

29+42.5

I.P.

34.35

12" Oak

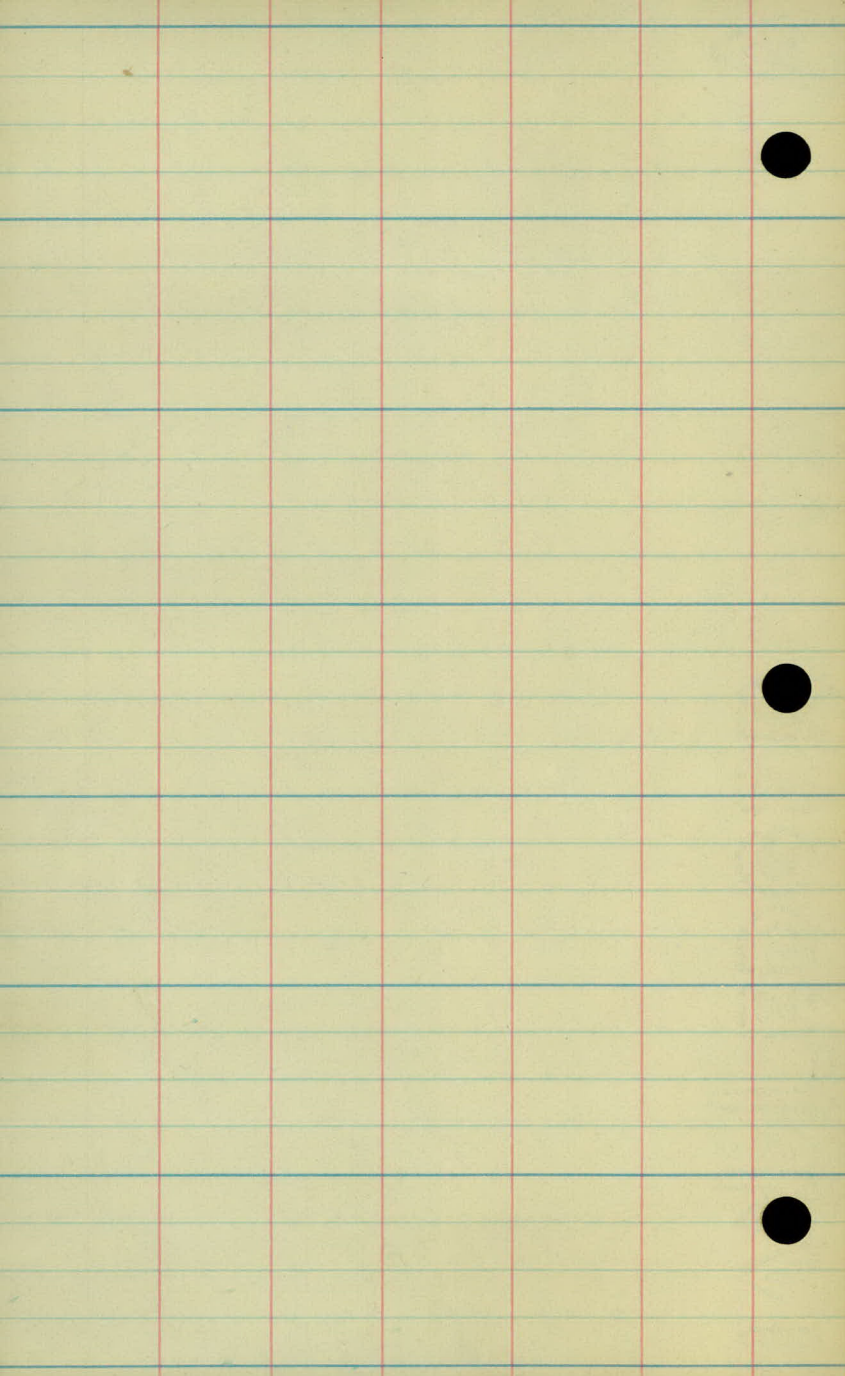
Bait Spike

49.92

50.44

10" Oak

Co. Rd. B.2



Topography

Sta.

5

4

3

2

1

oto

± Dale St.

Note:

Good Measurements are to edge of Travelled Road.
(Telephone & 2 Wires of Power on top.)

Rd. 9'

Rd. 10'

5

cult.

+62-FEN7

+22-R.R.-27

Cult

farm
Yard.

+94-36" B.L. 33'
 +88-R.R. 22'
 +72-20" B.L. 34'
 +62-24" B.L. 34'
 +53-FEN7
 +40-24" B.L. 30'
 +28-20" B.L. 31'
 +1829-24" Bx E 1.36'

Rd. 8'

Rd. 10'

farm yard.

(F.P.)
+63-R.R.-26

Rd. 5'

+11-F. Cor. 24'
Rd. 12'

(T.O.)
+68-R.R. 26'
Rd. 5'

Rd. 13' F-24'

Rd. 5'

Rd. 12' - F. 26

Cultivated

Hay Meadow

(F.P.)
 +50-R.R. 26'
 +40-Rd. 4'
 +27-16 Sq. Sect. 21
 +10-B. Torvia.

+40-Rd. 15'
 +27-F. Cor. 28'

E. Dale St.

Torvia.

Sta.

12

11

10

9

8

7

6

+05-P.P. 2'
Rd. 12'
+91-E. 12" Vt. Culv.
16'

Rd. 8'
+93-E. 12" Vt. Culv. 16'
+96-3" Culv. 15' 6"

E. Culv. 13' 6"

E. Culv. 13' 6"

17 Rd. 11'

Rd. 8'

+47-P.P. 27'

11 Rd. 10'

Rd. 8'

10 Rd. 10'
+90-P.P. 27'

Rd. 9'

9 Rd. 10'

Rd. 9'

+34-P.P. 27'

8 Rd. 9'

Rd. 9'

cultivated

21' Surfacing

cultivated

7 Rd. 9'

Rd. 8'

+76-P.P. 27'

6

Sta.

19

18

17

16

15

14

13

177-RR 17'
173-10" Oak 22' 7

123-4" Tw. Oak 21'
117-Lilac 17'
19 3" Oak 31'
Rd. 9'
25.13' 100' 22'
181-Cor. H. 57'
170-Snowy Rd. 23'
161-Snowy Rd. 23'
140-4-2" Pl. Tree 31'
131-ENT
125-A & F Line 33'
116-A-F 43'
103-RR 17'
Rd. 10'

105-T. R. 27'
Rd. 11'

Rd. 12'

160-RR 27'

Rd. 11'

134-Force Line 37'
109-RR 27'

Rd. 10'

Rd. 11'

162-RR 27'

198-B. 12" V. 16'
182-ENT

155-Reg. Cul. 16'

Cult.

Farm Yard

Yard

Farm

Rd. 10'

Rd. 9' 22" F

Rd. 10' F-21'

Rd. 7'

102-F. Cor. 21'

26

25

24

23

22

21

20

+96.5" oak 27'

+60 Rd. 14'

+12.7c West. Ar. Survey

26

+90-1/2 Rd. 1/2 24'

+85 Rd. 12'

Note: See Western Ar.
Survey

+24-30" Cott s/p. 15'

25

Rd. 12'

24

Rd. 12'

+74-8" Pl. Tr. 30'

+38-4" Pl. 31'

+13-2" Pl. 25'

23

Rd. 10'

+73-36" Cott. 16'

+32-Int. Rd.

+09 24" Cott. 44'

22

Rd. 10'

+85-T.P. 27'

21

Rd. 10'

+50-T.P. 27'

20

Rd. 11'

Rd. 7

Timber 25'

+59-P.P. 15'

+60-Rd. 17'

+53-8" Oak 15'-Bay Tr.

+02-T.P. 15'

Rd. 11'

+95-8" oak 12'

+85-Rd. 8'

+ Rd. 7'

+01-6" Hf. 15'

+22-F.P. 14'

Rd. 8'

Rd. 10'

+49-12" oak 19'

+01-10" oak 21'

Rd. 9'

+92-P.P. 18'

+74-12" oak 33'

+59-10" oak 21'

+55-12" oak 32'

+50-8" oak 22'

+37-6" oak 21'

Rd. 10'

+81-10" oak 28'

Rd. 9'

Scattered Sp.

Cult.

Cult.

Cult.

33

32

31

30

29

28

27

Rd. 17'

76 S-E. Row Brush 20'

32

Rd. 16'

+90-T.P. 22'

32

Rd. 15'

+108-T.P. 21'

31

+70-Reg Row oak Brush 21'

30

+105-T.P. 21'
Rd. 14'

+90-10" oak 30'

+53-F. End

+17-F. L. 11 33'

+14-12" oak-32'

29

Rd. 12'

+96-10" oak 33'

+84-6" oak-31'

+75-6" oak-34'

+50-6" oak 31'

+20-12" oak 32'

+05-15" oak 31'

28

Rd. 14'

+75-15" oak 31'

+40-10" oak 33'

+23-12" oak 32'

+10-12" oak-31'

27

Rd. 2 9

+90-13" oak-27'

+82-R.A. 10

+67-12" oak 31'

+58-4-10" oak-31'

+43-8" oak 24'

+29-5" oak 20'

+70-4" oak 16'

+12-14" oak 27'

Rd. 3'

10-10

10-10

B-Trees

10-10

10-10

Rd. 4'

Timber 16'

8-Trees -

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

10-10

+43-R.P. 13'

+27-E. F. 19'

21.5' F-19'

Timber 19'

+44-Reg. Tree 16'

+40-Reg. F. 16

+10-8" oak-18'

Rd. 5'

+64-6" oak 17'

+37-14" oak-15'

+18-12" oak-12'

Rd. 7'

+99-F.P. 13'

5-oaks 1933

Posture scattered oak

Rd. 7' Timber 16'

+50-Timber 19'

40

39

38

37

36

35

34

Rd. 10

Rd. 0

10

+98-ENT LT.

(Row)
+84-End Oaks 30'

+1-10" oak-78' 1/2 Row.
Rd. 17'

+97-T.R. 24'
+86-6" oak-31'
+80-12" oak-28' +95-8" oak-31'
+77-8" oak-30'

+86-6" oak-29'
+43-6" oak-29'

+3-Ref. Wall-30'
+2-Cor. Gar. 38'

Rd. 18'
+91- Cor. Gar. 38'

+88- Cor. Wall 31'-43'
+51-T.R. 24'

+29-Stairs 25'
+25-End Stairs 20'

+24-Ref. Wall-34'-31'
+13-Ref. Wall-34'

+12- Cor. Gar.
Rd. 17'

+99- Cor. Gar. 35'

+15-T.R. 24'
+3-12" oak-32'
Rd. 16'

+73-10" oak-35'
+65-12" oak-34'
+28-12" oak-41'

+28- E. Culv. 75'
+28- ENT

+18-12" culv. 75' C.M.
Rd. 12' +18-10" oak-27'

+99-10" oak-27'
+88-12" oak-31'

+70-T.R. 24'
+69-6" B.E. 29'

+42-6" B.E. 26'

19' Rd. 1'

+34-T.R. 23'
+20-8" TW. 30'
+11-12" C.M. 2'-Rd. -18' Lt.

+56-ENT +56-12" x 14'-7'
C.M. Culv.

Rd. 1'

Rd. 0

+67-R.R. 12'
+36-8" C.M. 19'
+35-5" C.M. 21'
+28-10" C.M. 19'
+10-4" C.M. 22'
Rd. 4'

+72-4" C.M. 19'
+70-6" C.M. 15'
+65-E. Wall-15'
+92-12" C.M. 15'

+22- Cor. Shad.
+11- Cor. Shad. 74'
+08- Cor. Ht.

Rd. 0'

+92-Ref. Wall 15'
+80-ENT 10' x 27' C.M.
+72- Cor. Boring 76'

+59- Cor. Boring 76'

+30-P.R. 12'

Rd. 3'

+16-16" oak-12'

+27-Gr. Small B.E. 10'
+18-2-14" oak 33'

900

Gar.

Gar.

+66-6" Wall Ht.

12" W. 106'

74' A

11 Loc. Hedge.

116' Shad.

Yard.

Farm

Cult.

Cult.

47

46

45

44

43

42

41

+04-3-8" Oak 29'
Rd. 15'

Rd. 5'

11

+03-8" Oak-31
+75-Gr. 6-6" Oak-28'
+12-T.P. 23'

47 Rd. 15'

Rd. 5'

+84-4-6" Oak-27'
+85-6" Oak-28'

46 +10-6" Oak-30'
Rd. 15'

Rd. 3'

+16-E. Trees & Brush 19
+62 T.P. 23'

+77-P.P. 19'

+20-F. Ent

45 Rd. 16' Brush
20-34

Rd. 3'

+21-T.P. 23'

44 Rd. 16'

Rd. 3'

+42-P.P. 17'

43 Rd. 19'
Timber & Brush 25-35
+75-T.P. 24'

Rd. 3'

160

42 Rd. 21'
Timber & Brush 24-35'

+16-12" Oak-6'
Rd. 0'

+34-T.P. 24'

+05-Box Trees & Brush 23-39

+53-14" Oak-9'

41 +01-P.P. 11'

53

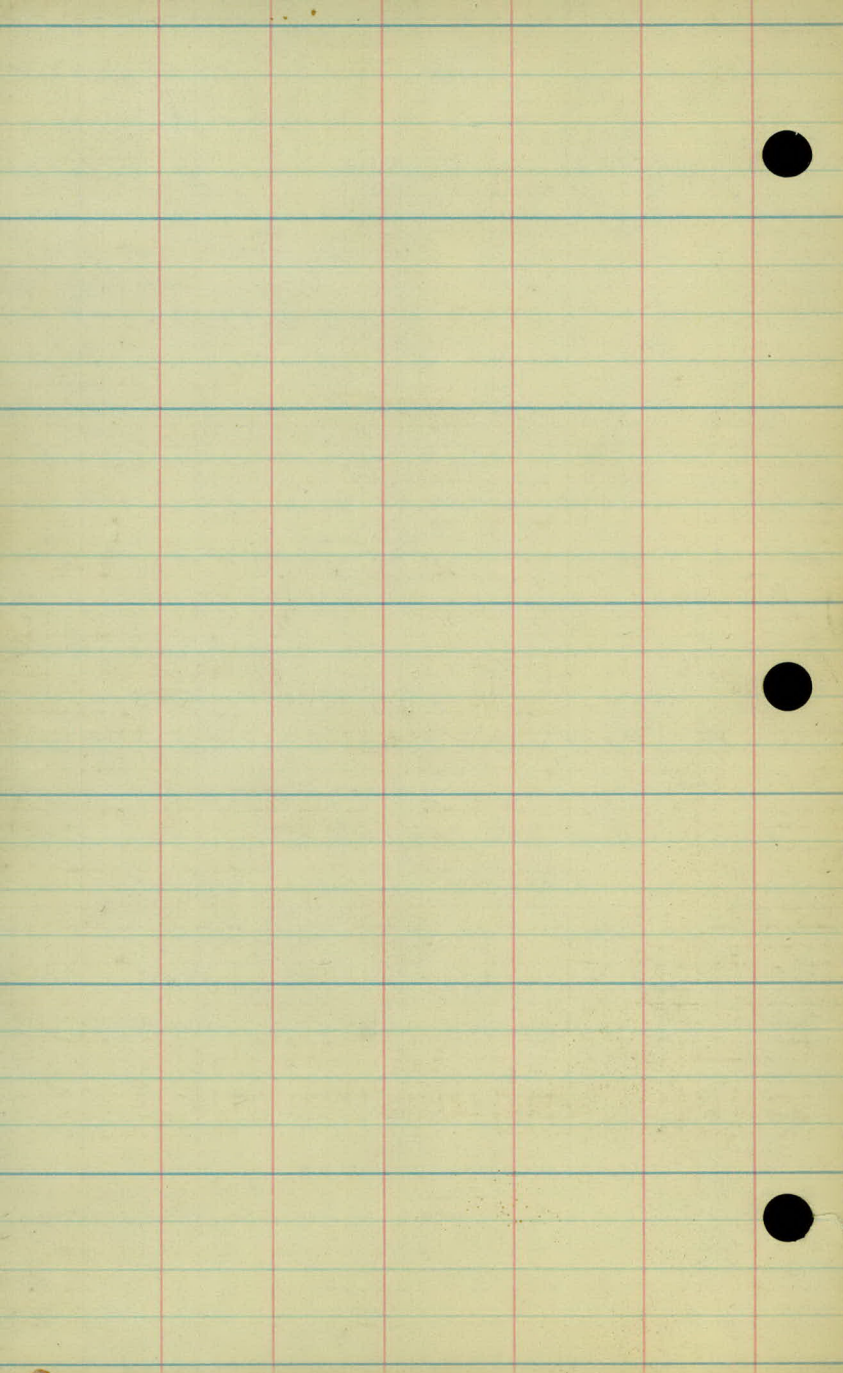
52

51

50

49

48



Cross Sections.
&
Check Levels.

(Co Rd 'B' Data is .26' lower)
than Main Ave. Data
5-26-41 -K.A.

Bench Levels.

Sta.	+ Western to Dale	π	-	Elev.
B.M.	0.02	981.32		981.30
	0.35	968.29	-13.38	967.94
	0.64	953.48	13.45	954.84
	3.25	945.01	13.72	941.76
B.M.	7.52	945.01	7.52	937.49
	6.05	948.33	2.73	942.28
	1.14	938.11	11.36	936.97
B.M.			6.30	931.81

Western to Rice

B.M.	11.35	992.65		981.30
	0.25	979.50	13.40	979.25
	10.41	985.71	4.20	975.30
B.M.	0.72	985.71	0.72	984.99
	0.00	976.28	9.43	976.28
	0.71	975.07	1.92	974.36
B.M.			13.43	961.64

Lt.

L

Rt.

14

R.R. Spike Top 30" Cott Stp. 13 Lt. Sta. 25+25

R.R. Spike 27' Lt. Sta. 13+05

^{P.R./c}
R.R. Spike 26 Lt. Sta. 0+50 N.E. Cor. Do/eo Ninth Ave.

Top Bott step E. end Lt. of Sta. 38+70

R.R. in R.P. 25' Rt 52+11

Sta.	+	T	-	Elev.
B.M.	5.75	937.56		931.81
0+0				
0+0 = E Dale St.				927.7
0+10	sh/dr.			27.5
0+14				27.4
0+25				28.0
0+60				29.3
1+0				31.2
+50				33.6
2+0				36.0
T.P.	11.87	948.86	0.57	936.99
+60				39.2
3+0				41.1
+50				43.1
4+0				44.0

Lt.

2

Rt.

15

W.H.C.

July 8, 35

B.P. Spike in B.P. 26' Lt. Sta. 0 to 50

29.8

25.5

 $\frac{6.5}{81}$

29.5

 $\frac{7.8}{50}$ $\frac{9.9}{50}$ $\frac{12.1}{50}$

25.0

 $\frac{14.4}{100}$ $\frac{8.1}{50}$ $\frac{9.0}{25}$ $\frac{10.1}{50}$ $\frac{11.4}{25}$ $\frac{12.6}{50}$

29.6

 $\frac{8.2}{50}$ $\frac{9.3}{25}$ $\frac{10.2}{50}$ $\frac{11.8}{25}$

24.9

 $\frac{12.7}{50}$

32.7

26.1

 $\frac{4.9}{50}$ $\frac{7.2}{25}$ $\frac{7.6}{18}$ $\frac{9.2}{14}$ $\frac{9.6}{50}$ $\frac{10.2}{14}$ $\frac{11.1}{19}$ $\frac{9.2}{25}$ $\frac{11.0}{39}$ $\frac{11.5}{50}$

31.6

26.5

 $\frac{6.0}{33}$ $\frac{6.4}{19}$ $\frac{8.4}{17}$ $\frac{8.4}{14}$ $\frac{7.9}{12}$ $\frac{8.3}{50}$ $\frac{8.2}{9}$ $\frac{8.5}{20}$ $\frac{10.2}{23}$ $\frac{11.2}{33}$

33.0

27.2

 $\frac{4.6}{33}$ $\frac{5.2}{18}$ $\frac{7.0}{16}$ $\frac{7.0}{14}$ $\frac{6.6}{11}$ $\frac{6.4}{50}$ $\frac{6.3}{5}$ $\frac{6.6}{19}$ $\frac{9.4}{23}$ $\frac{10.4}{33}$

35.0

29.5

 $\frac{2.6}{33}$ $\frac{3.3}{18}$ $\frac{4.9}{16}$ $\frac{4.4}{10}$ $\frac{4.0}{50}$ $\frac{4.5}{17}$ $\frac{6.4}{21}$ $\frac{7.1}{25}$ $\frac{8.1}{33}$

38.2

32.8

 $\frac{10.6}{33}$ $\frac{0.2}{17}$ $\frac{2.0}{15}$ $\frac{1.5}{10}$ $\frac{1.6}{50}$ $\frac{1.8}{18}$ $\frac{3.4}{22}$ $\frac{4.1}{27}$ $\frac{4.8}{33}$

41.0

37.8

 $\frac{7.9}{33}$ $\frac{8.1}{18}$ $\frac{9.8}{16}$ $\frac{9.8}{14}$ $\frac{9.4}{8}$ $\frac{10.3}{6}$ $\frac{9.7}{50}$ $\frac{9.4}{5}$ $\frac{9.7}{19}$ $\frac{10.4}{24}$ $\frac{11.1}{33}$

41.9

41.0

 $\frac{7.0}{33}$ $\frac{6.7}{17}$ $\frac{7.9}{14}$ $\frac{7.7}{7}$ $\frac{8.4}{6}$ $\frac{7.8}{50}$ $\frac{7.6}{5}$ $\frac{7.6}{15}$ $\frac{7.9}{18}$ $\frac{7.2}{20}$ $\frac{7.9}{28}$ $\frac{7.8}{33}$

42.7

43.2

 $\frac{6.2}{33}$ $\frac{6.1}{24}$ $\frac{6.2}{12}$ $\frac{5.8}{9}$ $\frac{6.3}{7}$ $\frac{5.8}{50}$ $\frac{5.7}{5}$ $\frac{6.0}{13}$ $\frac{5.5}{19}$ $\frac{5.2}{33}$

43.1

43.3

 $\frac{5.8}{33}$ $\frac{5.9}{12}$ $\frac{5.2}{9}$ $\frac{5.4}{7}$ $\frac{4.9}{50}$ $\frac{5.2}{11}$ $\frac{5.6}{17}$ $\frac{5.6}{33}$

Sta. + π - Elev.

948.86

4+50 944.2

5+0 43.9

+50 43.4

6+0 43.4

+50 43.6

7+0 43.4

T.P. 3.32 946.77 541 943.45

+50 42.8

8+0 42.4

+50 42.3

9+0 42.3

+50 41.8

10+0 41.6

42.9

 $\frac{6.0}{33}$ $\frac{5.6}{12}$ $\frac{5.1}{8}$ $\frac{4.7}{11}$ $\frac{5.1}{11}$ $\frac{4.8}{13}$

43.7

 $\frac{5.2}{33}$

42.5

 $\frac{6.4}{33}$ $\frac{5.6}{14}$ $\frac{5.2}{8}$ $\frac{5.0}{11}$ $\frac{5.5}{11}$ $\frac{5.9}{16}$ $\frac{5.2}{21}$

43.3

 $\frac{5.6}{33}$

41.4

 $\frac{7.5}{33}$ $\frac{6.9}{22}$ $\frac{5.4}{11}$ $\frac{6.1}{8}$ $\frac{5.5}{10}$ $\frac{5.8}{17}$ $\frac{6.7}{17}$

42.2

 $\frac{6.7}{33}$

41.8

 $\frac{7.1}{33}$ $\frac{6.6}{22}$ $\frac{5.8}{14}$ $\frac{5.2}{10}$ $\frac{5.9}{9}$ $\frac{5.5}{11}$ $\frac{5.9}{13}$ $\frac{5.4}{16}$ $\frac{5.9}{20}$ $\frac{7.1}{20}$

41.2

 $\frac{7.2}{33}$

42.7

 $\frac{6.2}{33}$ $\frac{5.2}{14}$ $\frac{4.9}{10}$ $\frac{5.4}{8}$ $\frac{5.3}{9}$ $\frac{5.8}{9}$ $\frac{5.3}{12}$ $\frac{5.8}{16}$ $\frac{6.6}{19}$

42.0

 $\frac{6.9}{33}$

43.2

 $\frac{5.7}{33}$ $\frac{5.5}{20}$ $\frac{4.8}{12}$ $\frac{5.8}{9}$ $\frac{5.5}{9}$ $\frac{5.7}{9}$ $\frac{5.3}{12}$ $\frac{5.8}{16}$ $\frac{6.5}{19}$

42.1

 $\frac{6.8}{33}$

41.7

 $\frac{5.1}{33}$ $\frac{4.5}{15}$ $\frac{3.9}{12}$ $\frac{4.3}{9}$ $\frac{4.0}{9}$ $\frac{4.2}{9}$ $\frac{3.9}{14}$ $\frac{4.8}{20}$

41.6

 $\frac{5.2}{33}$

41.4

 $\frac{5.4}{33}$ $\frac{5.6}{19}$ $\frac{4.6}{12}$ $\frac{5.0}{10}$ $\frac{4.4}{9}$ $\frac{4.5}{9}$ $\frac{4.9}{13}$ $\frac{5.4}{20}$

41.4

 $\frac{5.4}{33}$

41.4

 $\frac{5.4}{33}$ $\frac{5.6}{17}$ $\frac{4.5}{12}$ $\frac{4.9}{9}$ $\frac{4.5}{9}$ $\frac{4.7}{9}$ $\frac{4.6}{12}$ $\frac{5.3}{18}$

41.6

 $\frac{5.2}{33}$

41.6

 $\frac{5.2}{33}$ $\frac{5.8}{18}$ $\frac{4.7}{11}$ $\frac{5.0}{9}$ $\frac{4.5}{9}$ $\frac{4.9}{9}$ $\frac{4.9}{14}$

41.1

 $\frac{5.7}{33}$

41.3

 $\frac{5.5}{33}$ $\frac{5.9}{15}$ $\frac{5.4}{11}$ $\frac{5.5}{9}$ $\frac{5.0}{9}$ $\frac{5.1}{9}$ $\frac{4.9}{12}$ $\frac{5.7}{18}$

40.9

 $\frac{5.9}{33}$

41.0

 $\frac{5.8}{33}$ $\frac{6.0}{17}$ $\frac{5.7}{9}$ $\frac{5.2}{9}$ $\frac{5.5}{9}$ $\frac{5.3}{11}$

41.1

 $\frac{5.7}{33}$

Sta.	+	$\nearrow$	-	Elev.
		946.77		
10+50				941.4
11+0				41.1
+50				40.0
12+0				38.8
+60				38.1
B.M.	6.39	943.92	9.24	937.53
13+0				
12+92 & Culv.				
13+0				37.7
+30				37.6
+60				38.4
14+0				39.3
+50				39.9
15+0				40.7
T.P.	8.68	950.34	2.26	941.66

Lt.

E

Rt.

17

41.3

5.5

33

6.2

15

5.7

11

5.7

9

5.4

9

5.6

9

5.5

11

6.0

14

5.7

33

41.1

41.1

5.7

33

6.4

17

5.6

12

6.1

9

5.7

9

6.1

9

5.7

11

6.6

15

5.6

33

41.2

40.6

6.2

33

7.2

17

6.8

11

7.2

9

6.8

9

7.2

9

7.3

16

5.5

33

41.3

37.4

9.4

33

8.5

17

7.8

12

8.3

11

8.0

8

8.4

8

8.3

15

5.9

33

40.9

33.4

13.4

33

12.8

19

9.1

14

8.7

9

9.2

8

10.3

13

13.0

21

8.7

33

38.1

E.R. Spike in T.P. 27' Lt. Sta. 13405

Inlet of Culv 10.68

34.2

33

9.5

19

6.2

14

6.2

9

6.7

10

11.2

16

12.1

21

13.4

23

11.4

33

Outlet 12.30

32.5

36.7

7.2

33

7.4

20

8.5

18

8.5

15

6.1

12

6.3

9

6.9

9

15.2

22

17.8

28

17.8

24

14.8

26

14.8

40

29.1

39.6

4.3

33

4.4

20

7.7

16

5.4

12

5.5

9

6.0

10

13.0

20

13.7

25

16.5

37

20.9

47

22.7

48

22.7

52

22.7

58

(0.1)

27.4

41.6

2.3

33

7.8

26

4.0

18

5.4

16

4.4

14

4.6

10

5.0

10

13.7

23

14.5

33

29.4

42.4

1.5

33

2.7

22

4.6

16

4.1

14

4.0

10

4.4

10

13.2

24

12.6

33

31.3

42.4

1.5

33

1.8

28

3.0

17

3.4

14

3.2

10

3.7

12

7.2

16

8.4

23

9.7

33

34.2

Sta.	+	π	-	Elev.
		9303.4		
15+50				941.7
16+0				42.7
+50				44.1
17+0				45.5
+50				46.6
T.P.	9.10	958.05	1.39	948.95
18+0				48.3
+50				50.2
19+0				53.4
T.P.	12.13	969.84	0.34	957.71
+50				57.0
20+0				60.7
+50				63.8
T.P.	9.32	976.20	2.96	966.88
21+0				66.6

Lt.

d

Rt.

18

42.6

35.6

$$\begin{array}{r} 7.7 \\ 33 \end{array}$$

$$\begin{array}{r} 8.9 \\ 17 \end{array}$$

$$\begin{array}{r} 8.7 \\ 12 \end{array}$$

$$\begin{array}{r} 8.6 \\ - \end{array}$$

$$\begin{array}{r} 9.2 \\ 11 \end{array}$$

$$\begin{array}{r} 12.6 \\ 17 \end{array}$$

$$\begin{array}{r} 13.6 \\ 23 \end{array}$$

$$\begin{array}{r} 14.7 \\ 33 \end{array}$$

43.2

35.3

$$\begin{array}{r} 7.1 \\ 33 \end{array}$$

$$\begin{array}{r} 7.8 \\ 19 \end{array}$$

$$\begin{array}{r} 7.5 \\ 14 \end{array}$$

$$\begin{array}{r} 7.4 \\ - \end{array}$$

$$\begin{array}{r} 8.1 \\ 12 \end{array}$$

$$\begin{array}{r} 13.0 \\ 20 \end{array}$$

$$\begin{array}{r} 13.8 \\ 23 \end{array}$$

$$\begin{array}{r} 15.0 \\ 33 \end{array}$$

46.6

37.0

$$\begin{array}{r} 3.7 \\ 33 \end{array}$$

$$\begin{array}{r} 5.3 \\ 22 \end{array}$$

$$\begin{array}{r} 6.7 \\ 20 \end{array}$$

$$\begin{array}{r} 6.4 \\ 15 \end{array}$$

$$\begin{array}{r} 6.2 \\ - \end{array}$$

$$\begin{array}{r} 6.5 \\ 11 \end{array}$$

$$\begin{array}{r} 11.3 \\ 18 \end{array}$$

$$\begin{array}{r} 12.0 \\ 23 \end{array}$$

$$\begin{array}{r} 13.3 \\ 33 \end{array}$$

48.1

39.6

$$\begin{array}{r} 2.2 \\ 33 \end{array}$$

$$\begin{array}{r} 4.2 \\ 23 \end{array}$$

$$\begin{array}{r} 5.6 \\ 19 \end{array}$$

$$\begin{array}{r} 5.0 \\ 12 \end{array}$$

$$\begin{array}{r} 4.8 \\ - \end{array}$$

$$\begin{array}{r} 5.4 \\ 14 \end{array}$$

$$\begin{array}{r} 9.1 \\ 21 \end{array}$$

$$\begin{array}{r} 10.7 \\ 33 \end{array}$$

50.4

42.7

$$\begin{array}{r} 10.1 \\ 33 \end{array}$$

$$\begin{array}{r} 14 \\ 25 \end{array}$$

$$\begin{array}{r} 4.3 \\ 20 \end{array}$$

$$\begin{array}{r} 4.4 \\ 17 \end{array}$$

$$\begin{array}{r} 3.7 \\ 14 \end{array}$$

$$\begin{array}{r} 3.7 \\ - \end{array}$$

$$\begin{array}{r} 4.4 \\ 12 \end{array}$$

$$\begin{array}{r} 5.2 \\ 16 \end{array}$$

$$\begin{array}{r} 4.7 \\ 21 \end{array}$$

$$\begin{array}{r} 6.6 \\ 23 \end{array}$$

$$\begin{array}{r} 8.0 \\ 33 \end{array}$$

53.2

42.7

$$\begin{array}{r} 4.9 \\ 33 \end{array}$$

$$\begin{array}{r} 7.3 \\ 23 \end{array}$$

$$\begin{array}{r} 10.2 \\ 19 \end{array}$$

$$\begin{array}{r} 10.1 \\ 11 \end{array}$$

$$\begin{array}{r} 9.8 \\ - \end{array}$$

$$\begin{array}{r} 10.5 \\ 11 \end{array}$$

$$\begin{array}{r} 14.1 \\ 19 \end{array}$$

$$\begin{array}{r} 15.4 \\ 33 \end{array}$$

54.9

45.3

$$\begin{array}{r} 3.2 \\ 33 \end{array}$$

$$\begin{array}{r} 4.9 \\ 25 \end{array}$$

$$\begin{array}{r} 7.8 \\ 17 \end{array}$$

$$\begin{array}{r} 7.6 \\ 12 \end{array}$$

$$\begin{array}{r} 7.9 \\ - \end{array}$$

$$\begin{array}{r} 8.6 \\ 11 \end{array}$$

$$\begin{array}{r} 10.5 \\ 15 \end{array}$$

$$\begin{array}{r} 11.8 \\ 21 \end{array}$$

$$\begin{array}{r} 12.8 \\ 33 \end{array}$$

58.1

50.8

$$\begin{array}{r} 0.0 \\ 33 \end{array}$$

$$\begin{array}{r} 2.0 \\ 23 \end{array}$$

$$\begin{array}{r} 4.1 \\ 18 \end{array}$$

$$\begin{array}{r} 5.0 \\ 17 \end{array}$$

$$\begin{array}{r} 5.1 \\ 11 \end{array}$$

$$\begin{array}{r} 4.7 \\ - \end{array}$$

$$\begin{array}{r} 5.0 \\ 12 \end{array}$$

$$\begin{array}{r} 5.8 \\ 15 \end{array}$$

$$\begin{array}{r} 7.3 \\ 33 \end{array}$$

61.7

57.1

$$\begin{array}{r} 8.1 \\ 33 \end{array}$$

$$\begin{array}{r} 18.9 \\ 27 \end{array}$$

$$\begin{array}{r} 12.4 \\ 16.5 \end{array}$$

$$\begin{array}{r} 13.5 \\ 16 \end{array}$$

$$\begin{array}{r} 13.0 \\ 12 \end{array}$$

$$\begin{array}{r} 12.8 \\ - \end{array}$$

$$\begin{array}{r} 13.2 \\ 11 \end{array}$$

$$\begin{array}{r} 13.8 \\ 12 \end{array}$$

$$\begin{array}{r} 12.1 \\ 17 \end{array}$$

$$\begin{array}{r} 12.7 \\ 33 \end{array}$$

68.0

63.5

$$\begin{array}{r} 2.8 \\ 33 \end{array}$$

$$\begin{array}{r} 3.8 \\ 29 \end{array}$$

$$\begin{array}{r} 8.3 \\ 17 \end{array}$$

$$\begin{array}{r} 9.9 \\ 16 \end{array}$$

$$\begin{array}{r} 9.4 \\ 10 \end{array}$$

$$\begin{array}{r} 9.1 \\ - \end{array}$$

$$\begin{array}{r} 9.5 \\ 9 \end{array}$$

$$\begin{array}{r} 9.8 \\ 12 \end{array}$$

$$\begin{array}{r} 8.2 \\ 16 \end{array}$$

$$\begin{array}{r} 5.8 \\ 21 \end{array}$$

$$\begin{array}{r} 6.3 \\ 33 \end{array}$$

70.3

69.3

$$\begin{array}{r} 10.5 \\ 40 \end{array}$$

$$\begin{array}{r} 10.5 \\ 31 \end{array}$$

$$\begin{array}{r} 3.4 \\ 21 \end{array}$$

$$\begin{array}{r} 6.6 \\ 14 \end{array}$$

$$\begin{array}{r} 6.6 \\ 13 \end{array}$$

$$\begin{array}{r} 6.3 \\ 12 \end{array}$$

$$\begin{array}{r} 6.0 \\ - \end{array}$$

$$\begin{array}{r} 6.5 \\ 10 \end{array}$$

$$\begin{array}{r} 6.8 \\ 12 \end{array}$$

$$\begin{array}{r} 5.6 \\ 14 \end{array}$$

$$\begin{array}{r} 1.0 \\ 22 \end{array}$$

71.8

70.9

$$\begin{array}{r} 4.4 \\ 33 \end{array}$$

$$\begin{array}{r} 5.1 \\ 28 \end{array}$$

$$\begin{array}{r} 8.0 \\ 19 \end{array}$$

$$\begin{array}{r} 10.2 \\ 15 \end{array}$$

$$\begin{array}{r} 10.0 \\ 16.0 \end{array}$$

$$\begin{array}{r} 9.6 \\ - \end{array}$$

$$\begin{array}{r} 10.1 \\ 10 \end{array}$$

$$\begin{array}{r} 10.5 \\ 12 \end{array}$$

$$\begin{array}{r} 9.5 \\ 15 \end{array}$$

$$\begin{array}{r} 5.3 \\ 22 \end{array}$$

$$\begin{array}{r} 5.3 \\ 33 \end{array}$$

S_4	$+$	π	$-$	$E/ev.$	
		976.20			
21+50				969.1	
22+0				71.1	
+50				72.4	
23+0				73.8	
T.P.	8.73	984.56	0.37		975.83
+50				75.7	
+85				76.8	
24+0				77.3	
+50				79.0	
25+0				80.8	
B.M.			3.22		981.34
+50				83.2	}
B.M.	10.81	992.11			
+85				84.6	
26+0				85.2	

47.

2

Rt.

72.9

3.3	4.3	6.5	7.8	7.6	7.1	7.5	8.0	6.9	7.8
33	26	20	14	12		10	14	19	33

70.5

5.7	6.4	5.4	5.1	5.5	6.0	5.7	5.8
<u>33</u>	<u>18</u>	<u>10</u>		<u>11</u>	<u>14</u>	<u>20</u>	<u>35</u>

70.9

$$\begin{array}{r} 5.3 \\ \underline{33} \end{array} \quad \begin{array}{r} 5.5 \\ \underline{27} \end{array} \quad \begin{array}{r} 4.3 \\ \underline{11} \end{array} \quad \begin{array}{r} 3.8 \\ \underline{1} \end{array} \quad \begin{array}{r} 4.3 \\ \underline{10} \end{array} \quad \begin{array}{r} 6.2 \\ \underline{16} \end{array} \quad \begin{array}{r} 5.6 \\ \underline{33} \end{array}$$

74.4

$\frac{1.8}{33}$	$\frac{2.8}{22}$	$\frac{4.2}{18}$	$\frac{4.2}{16}$	$\frac{2.7}{10}$	$\frac{2.4}{10}$	$\frac{3.1}{18}$	$\frac{6.3}{18}$	$\frac{7.9}{23}$
------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

77.7

<u>6.9</u>	<u>8.7</u>	<u>10.2</u>	<u>9.0</u>	<u>8.9</u>	<u>9.9</u>	<u>12.7</u>	<u>15.4</u>
33	21	16	13		10	15	33

78.6

6.0	7.7	9.3	9.3	7.9	7.8	8.7	11.1	12.6	14.8
33	21	17	16	12		9	13	18	33

17.1

7.5	89	98	9.8	7.3	7.3	8.1	10.8	12.8	14.6
<u>33</u>	<u>20</u>	<u>18</u>	<u>17</u>	<u>13</u>		<u>8</u>	<u>12</u>	<u>21</u>	<u>33</u>

75.3

$\frac{9.3}{33}$	$\frac{9.8}{22}$	$\frac{9.2}{17}$	$\frac{6.2}{12}$	$\frac{5.6}{7}$	$\frac{6.1}{7}$	$\frac{11.3}{14}$	$\frac{12.3}{10}$	$\frac{13.4}{33}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-------------------	-------------------	-------------------

76.0

$$\begin{array}{r} 86 \\ 33 \end{array} \quad \begin{array}{r} 85 \\ 26 \end{array} \quad \begin{array}{r} 76 \\ 17 \end{array} \quad \begin{array}{r} 40 \\ 12 \end{array} \quad \begin{array}{r} 38 \\ 8 \end{array} \quad \begin{array}{r} 43 \\ 15 \end{array} \quad \begin{array}{r} 87 \\ 33 \end{array} \quad \begin{array}{r} 109 \\ 33 \end{array}$$

41.9

$\frac{27}{33}$	$\frac{33}{22}$	$\frac{33}{17}$	$\frac{20}{13}$	$\frac{14}{19}$	$\frac{20}{15}$	$\frac{51}{15}$	$\frac{76}{32}$
-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------	-----------------

Spike Top 30' Co H. Sep.

856 $\begin{array}{r} 6.5 \\ 33 \end{array}$ $\begin{array}{r} 6.0 \\ 76 \end{array}$ $\begin{array}{r} 7.6 \\ 19 \end{array}$ $\begin{array}{r} 7.8 \\ 11 \end{array}$ $\begin{array}{r} 7.5 \\ 10 \end{array}$ $\begin{array}{r} 7.9 \\ 12 \end{array}$ $\begin{array}{r} 8.6 \\ 23 \end{array}$ $\begin{array}{r} 11.0 \\ 23 \end{array}$ $\begin{array}{r} 12.7 \\ 33 \end{array}$

86.4

$$\begin{array}{r} 5.7 \\ 33 \end{array} \quad \begin{array}{r} 6.6 \\ 21 \end{array} \quad \begin{array}{r} 7.3 \\ 18 \end{array} \quad \begin{array}{r} 6.9 \\ 14 \end{array} \quad \begin{array}{r} 7.6 \\ 20 \end{array} \quad \begin{array}{r} 8.8 \\ 33 \end{array} \quad \begin{array}{r} 11.0 \\ 33 \end{array}$$

Sta.	+	A	-	Elev.
		992.11		
26+12.7				85.5
+33				86.4
+47				86.9
+70				87.4
27+0				88.1
+35				88.8
	2.80	992.23	2.68	989.43
28+0				89.3
+50				89.8
29+0				87.3
+30				86.6
+60				85.5
30+0				83.8
T.P.	1.65	984.57	9.31	982.92

Lt.

E

Rt.

86.5

$$\frac{56}{33}$$

$$\frac{58}{22}$$

$$\frac{67}{13}$$

66

$$\frac{82}{22}$$

$$\frac{95}{33}$$

85.2

$$\frac{69}{33}$$

$$\frac{69}{28}$$

$$\frac{54}{23}$$

$$\frac{59}{16}$$

$$\frac{57}{-}$$

$$\frac{64}{10}$$

83.9

$$\frac{82}{33}$$

$$\frac{200+1340}{-}$$

Note:

 See
Western
Ave - S. 100

91.1

$$\frac{+45}{50}$$

$$\frac{+42}{26}$$

$$\frac{35}{26}$$

$$\frac{55}{20}$$

$$\frac{55}{13}$$

52

$$\frac{67}{13}$$

$$\frac{71}{20}$$

83.8

$$\frac{83}{33}$$

93.6

$$\frac{+62}{50}$$

$$\frac{+62}{40}$$

$$\frac{0.0}{29}$$

$$\frac{45}{21}$$

$$\frac{51}{13}$$

47

$$\frac{54}{8}$$

$$\frac{52}{13}$$

$$\frac{25}{17}$$

$$\frac{40}{26}$$

86.7

$$\frac{54}{33}$$

93.2

$$\frac{+50}{50}$$

$$\frac{+51}{39}$$

$$\frac{+45}{26}$$

$$\frac{0.0}{28}$$

$$\frac{34}{21}$$

$$\frac{44}{13}$$

$$\frac{40}{-}$$

$$\frac{46}{8}$$

$$\frac{47}{13}$$

$$\frac{48}{15}$$

$$\frac{51}{18}$$

84.8

$$\frac{73}{33}$$

92.3

$$\frac{+35}{50}$$

$$\frac{+35}{38}$$

$$\frac{+0.2}{24}$$

$$\frac{31}{20}$$

$$\frac{35}{15}$$

$$\frac{3.3}{-}$$

$$\frac{40}{9}$$

$$\frac{43}{12}$$

$$\frac{36}{14}$$

$$\frac{46}{22}$$

86.0

$$\frac{61}{33}$$

92.8

$$\frac{+20}{50}$$

$$\frac{+20}{36}$$

$$\frac{+3.5}{27}$$

$$\frac{1.0}{23}$$

$$\frac{27}{20}$$

$$\frac{3.0}{14}$$

$$\frac{26}{7}$$

$$\frac{29}{-}$$

$$\frac{3.6}{8}$$

$$\frac{40}{10}$$

$$\frac{2.2}{14}$$

87.4

$$\frac{48}{33}$$

92.0

$$\frac{+20}{50}$$

$$\frac{+20}{41}$$

$$\frac{+3.2}{35}$$

$$\frac{+2.0}{29}$$

$$\frac{0.0}{26}$$

$$\frac{3.1}{21}$$

$$\frac{3.7}{14}$$

$$\frac{3.3}{7}$$

34

$$\frac{40}{8}$$

$$\frac{43}{10}$$

$$\frac{3.6}{12}$$

$$\frac{5.2}{21}$$

85.5

$$\frac{67}{33}$$

91.4

$$\frac{0.8}{33}$$

$$\frac{23}{29}$$

$$\frac{3.6}{23}$$

$$\frac{49}{18}$$

$$\frac{5.1}{14}$$

$$\frac{48}{8}$$

44

$$\frac{54}{8}$$

$$\frac{6.1}{12}$$

$$\frac{7.3}{22}$$

84.3

$$\frac{7.9}{33}$$

88.2

$$\frac{40}{33}$$

$$\frac{46}{26}$$

$$\frac{6.0}{19}$$

$$\frac{59}{14}$$

$$\frac{56}{-}$$

$$\frac{6.0}{8}$$

$$\frac{8.0}{11}$$

$$\frac{8.6}{13}$$

$$\frac{9.4}{18}$$

81.9

$$\frac{103}{33}$$

86.7

$$\frac{5.5}{33}$$

$$\frac{6.1}{27}$$

$$\frac{7.0}{13}$$

$$\frac{67}{-}$$

$$\frac{7.1}{7}$$

$$\frac{9.6}{13}$$

$$\frac{10.8}{20}$$

80.9

$$\frac{11.3}{33}$$

88.0

$$\frac{4.2}{40}$$

$$\frac{4.6}{35}$$

$$\frac{7.5}{27}$$

$$\frac{8.9}{13}$$

84

$$\frac{86}{10}$$

$$\frac{10.1}{20}$$

81.5

$$\frac{10.7}{33}$$

Sta.	+	T	-	Elev.
		984.57		
30+50				82.0
31+0				80.2
+50				78.5
32+0				76.6
T.P.	2.48	977.49	9.56	975.01
+50				74.8
33+0				73.3
+45				71.8
34+0				70.9
T.P.	6.11	977.02	6.58	970.91
+40				70.6
35+0				70.4
+40				72.1
36+0				73.7
T.P.	11.12	985.67	2.47	974.55

Lt.

±

Rt.

21

85.5

81.7

139	0.2	2.8	3.0	26	2.9	3.3	1.5	2.0	29
33	24	19	14		7	9	12	24	33

84.2

79.6

0.4	2.0	4.5	4.7	4.4	4.6	5.2	3.6	4.6	5.0
33	73	19	14		7	11	15	29	33

81.7

65.9

29	4.0	6.3	6.5	6.1	6.4	7.1	7.2	8.7
33	20	21	1.6		5	9	17	33

79.4 5.2

72.6

15.2	6.1	8.3	8.2	2.7	8.0	8.2	9.0	10.0	10.8	12.0
33	26	21	1.6	5		6	8	13	21	33

75.5

71.4

2.0	2.7	3.5	3.5	2.6	2.4	2.7	4.0	5.1	6.1
33	25	23	21	18	8		7	9	20

74.2

70.5

33	40	48	53	53	42	40	4.2	4.4	6.3	6.7	7.4
33	28	24	22	21	18	9		5	10	20	33

71.6

67.8

59	5.8	5.9	5.3	5.5	5.7	5.9	7.2	8.6	9.7
33	29	21	18	53		3	6	18	33

70.3

64.5

7.2	7.4	6.3	6.4	6.6	6.6	10.8	13.0
33	21	18	6		2	8	33

70.5

61.8

6.5	6.8	6.2	6.1	6.4	6.4	10.9	12.8	15.7
33	21	19	9		2	7	17	33

34+11

Culv

7.50						8.75	
70.5							60.7
6.5	6.5	5.5	5.4	4.6	13.1	16.6	17.3
33	23	20	11		9	23	33

70.2

60.8

6.8	6.9	4.8	4.5	4.9	13.5	15.4	16.2
33	24	20	12		12	20	33

73.0

66.3

4.0	4.6	3.1	2.9	3.3	3.3	6.1	8.2	10.7
33	23	20	11		3	8	15	33

W₁
top end c.m. Culv. Lt. 34+11 36+15

Sta.	+	T	-	Elev.	
		985.67			
36+50				75.4	
37				77.0	
+50				79.3	
38				81.0	
B.M.	3.40	988.39	0.65		985.02 984.99
+50				82.3	
39				82.8	
+17				82.7	
+50				82.0	
40+0				80.3	
T.P.	1.90	999.77	10.52		977.87
+45				78.2	
41+0				75.0	
+45				73.0	
T.P.	2.89	994.70	7.96		991.81

Lt. 1 2 Rt.

77.6

70.9

$\frac{81}{33}$	$\frac{99}{27}$	$\frac{104}{24}$	$\frac{104}{21}$	$\frac{98}{17}$	$\frac{97}{9}$	$\frac{103}{5}$	$\frac{104}{5}$	$\frac{123}{11}$	$\frac{136}{24}$	$\frac{148}{30}$
-----------------	-----------------	------------------	------------------	-----------------	----------------	-----------------	-----------------	------------------	------------------	------------------

79.1

72.7

$\frac{6.6}{33}$	$\frac{8.2}{22}$	$\frac{8.5}{17}$	$\frac{8.3}{9}$	$\frac{8.7}{6}$	$\frac{9.3}{8}$	$\frac{10.0}{8}$	$\frac{10.0}{9}$	$\frac{9.4}{13}$	$\frac{8.6}{13}$	$\frac{10.9}{13}$	$\frac{13.0}{33}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------	-------------------	-------------------

84.6

$\frac{0.5}{40}$	$\frac{10}{33}$	$\frac{6.2}{24}$	$\frac{6.2}{18}$	$\frac{5.8}{9}$	$\frac{6.4}{2}$	$\frac{6.7}{2}$	$\frac{7.5}{9}$	$\frac{7.5}{10}$	$\frac{6.8}{11}$	$\frac{6.3}{14}$	$\frac{6.1}{14}$	$\frac{6.7}{15}$	$\frac{7.4}{15}$	$\frac{7.9}{28}$
------------------	-----------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------	------------------	------------------	------------------

85.5

81.5 76.9

$\frac{7.0}{40}$	$\frac{0.2}{33}$	$\frac{3.4}{20}$	$\frac{4.5}{18}$	$\frac{4.3}{10}$	$\frac{4.7}{5}$	$\frac{4.9}{5}$	$\frac{5.0}{10}$	$\frac{2.1}{15}$	$\frac{3.2}{21}$	$\frac{4.2}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------	------------------

Top Bottom Step E. end.

Lt. Sta. 38+70

85.6

$\frac{87.5}{33}$	$\frac{0.9}{30}$	$\frac{0.9}{30}$	$\frac{4.0}{30}$	$\frac{5.0}{21}$	$\frac{5.6}{11}$	$\frac{6.1}{7}$	$\frac{6.0}{12}$	$\frac{4.6}{12}$	$\frac{1.2}{17}$	$\frac{1.4}{25}$	$\frac{2.8}{33}$
-------------------	------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

84.6

86.0

$\frac{3.8}{33}$	$\frac{5.0}{18}$	$\frac{5.0}{10}$	$\frac{5.6}{8}$	$\frac{5.5}{15}$	$\frac{4.1}{15}$	$\frac{1.5}{24}$	$\frac{2.4}{33}$
------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------

88.4

85.1

$\frac{150}{50}$	$\frac{150}{40}$	$\frac{0.0}{32}$	$\frac{5.0}{23}$	$\frac{5.5}{18}$	$\frac{5.3}{9}$	$\frac{5.7}{10}$	$\frac{4.9}{15}$	$\frac{1.7}{15}$	$\frac{2.2}{25}$	$\frac{3.3}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	------------------	------------------	------------------	------------------	------------------

90.3

82.1

$\frac{184}{50}$	$\frac{183}{34}$	$\frac{6.3}{23}$	$\frac{6.0}{9}$	$\frac{6.4}{5}$	$\frac{5.9}{5}$	$\frac{5.7}{15}$	$\frac{6.3}{33}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------

85.1

77.4

$\frac{3.3}{40}$	$\frac{3.3}{30}$	$\frac{8.3}{22}$	$\frac{7.7}{11}$	$\frac{8.1}{6}$	$\frac{8.2}{6}$	$\frac{8.1}{13}$	$\frac{9.3}{24}$	$\frac{11.0}{33}$
------------------	------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	-------------------

79.4

72.9

$\frac{11.2}{33}$	$\frac{11.0}{30}$	$\frac{1.6}{23}$	$\frac{1.4}{21}$	$\frac{1.1}{10}$	$\frac{1.6}{4}$	$\frac{1.8}{6}$	$\frac{2.8}{6}$	$\frac{2.8}{7}$	$\frac{1.9}{8}$	$\frac{4.0}{14}$	$\frac{5.7}{28}$	$\frac{6.9}{33}$
-------------------	-------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

76.0

67.6

$\frac{7.8}{33}$	$\frac{4.2}{22}$	$\frac{4.0}{10}$	$\frac{4.8}{5}$	$\frac{4.8}{6}$	$\frac{7.0}{6}$	$\frac{8.4}{11}$	$\frac{12.1}{33}$
------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	-------------------

69.7

64.9

$\frac{10.1}{33}$	$\frac{6.0}{22}$	$\frac{6.0}{11}$	$\frac{6.8}{4}$	$\frac{8.4}{13}$	$\frac{14.7}{13}$	$\frac{14.9}{33}$
-------------------	------------------	------------------	-----------------	------------------	-------------------	-------------------

Sta.	+	T	-	Elev.
		994.70		
42 to				70.7
+45				70.0
+60				69.7
43				69.3
+50				69.2
44				69.6
+50				70.0
T.P	8.15	999.84	3.01	991.69
45				70.9
+35				72.0
+65				72.8
46				73.5
+30				74.1

Lt.

E

Rt.

65.5

6.12

9.2

9.2

3.1

2.9

4.0

4.0

13.0

60.6

14.1

33

33

30

21

10.

2

15.0

69.2

63.5

5.5

5.5

7.0

4.7

4.2

4.7

5.1

8.2

10.5

11.2

33

31

25

20

9

3

9

22

33

70.2

67.7

4.5

6.6

6.9

5.0

4.6

5.0

5.4

7.6

8.3

7.0

7.0

33

27

22

19

19

4

8

12

19

33

68.1

68.4

6.6

7.0

8.3

7.4

5.4

5.0

5.4

5.7

6.7

8.0

6.9

5.6

6.3

33

30

26

22

19

9

5

8

12

15

24

33

65.7

67.2

7.0

8.9

5.6

5.3

5.5

6.0

8.0

8.9

7.5

7.5

33

26

18

8

6

11

14

21

33

66.7

69.2

8.0

8.2

5.2

4.9

5.1

5.0

6.2

5.2

5.5

33

29

18

8

7

15

22

33

68.2

67.8

6.5

6.9

4.6

4.4

4.7

4.9

6.8

6.9

6.2

6.9

33

26

17

7

7

12

19

22

33

72.2

65.9

7.6

8.3

8.4

8.9

9.2

11.3

12.8

13.9

33

19

6

6

12

23

33

72.8

65.3

7.0

7.5

7.9

7.5

7.8

8.3

12.4

14.1

14.5

33

27

19

7

6

12

23

33

74.4

67.5

5.4

5.8

6.5

7.1

6.8

7.0

7.2

10.1

10.0

12.3

33

28

22

17

7

7

14

19

33

80.1

71.7

10.3

0.2

6.3

6.4

6.0

6.3

6.5

6.8

5.7

8.1

33

31

25

25

6

7

14

20

33

83.3

73.3

13.1

13.3

5.7

6.0

5.6

5.7

6.0

6.0

6.6

5.2

6.5

40

33.5

26

16

6

6

11

15

21

33

Sta. + π - Elev.

979.84

46+70

74.9

47+0

74.9

+50

74.6

48+0

74.2

T.P.

3.17

977.52

5.49

974.35

+50

74.0

49+0

73.7

+40

73.0

50+0

71.4

+50

69.2

51+0

66.2

T.P.

2.14

968.48

11.18

966.34

+50

63.9

+85

61.6

L1.

2

R1-

24

81.0

2nd

72.5

$\frac{7.25}{40}$	$\frac{7.12}{30}$	$\frac{4.0}{25}$	$\frac{5.0}{16}$	$\frac{4.7}{6}$	4.9	$\frac{5.1}{7}$	$\frac{6.2}{17}$	$\frac{5.3}{21}$	$\frac{7.3}{33}$
-------------------	-------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------	------------------

78.1

71.1

$\frac{1.7}{33}$	$\frac{4.4}{22}$	$\frac{4.7}{17}$	$\frac{4.6}{5}$	4.9	$\frac{5.3}{7}$	$\frac{6.4}{14}$	$\frac{7.5}{23}$	$\frac{8.7}{33}$
------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------	------------------

76.3

72.1

$\frac{3.5}{34}$	$\frac{5.0}{31}$	$\frac{5.4}{22}$	$\frac{5.3}{16}$	$\frac{5.0}{6}$	$\frac{5.2}{7}$	$\frac{5.5}{7}$	$\frac{6.2}{17}$	$\frac{7.1}{21}$	$\frac{7.7}{33}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

75.1

70.6

$\frac{4.7}{33}$	$\frac{4.7}{26}$	$\frac{5.8}{23}$	$\frac{5.6}{17}$	$\frac{5.4}{6}$	5.6	$\frac{5.8}{7}$	$\frac{8.2}{26}$	$\frac{8.6}{23}$	$\frac{9.2}{33}$
------------------	------------------	------------------	------------------	-----------------	-----	-----------------	------------------	------------------	------------------

76.3

68.3

$\frac{1.2}{33}$	$\frac{1.2}{27}$	$\frac{3.2}{21}$	$\frac{3.2}{16}$	$\frac{3.2}{9}$	$\frac{3.5}{6}$	$\frac{3.9}{6}$	$\frac{8.7}{17}$	$\frac{9.2}{33}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------

77.5

70.1

$\frac{0.0}{33}$	$\frac{0.7}{28}$	$\frac{2.6}{23}$	$\frac{3.8}{19}$	$\frac{3.5}{15}$	$\frac{3.4}{8}$	$\frac{3.8}{9}$	$\frac{4.2}{9}$	$\frac{5.7}{14}$	$\frac{5.7}{16}$	$\frac{5.3}{18}$	$\frac{7.4}{33}$
------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------	------------------

76.4

71.8

$\frac{1.0}{33}$	$\frac{1.6}{25}$	$\frac{4.9}{20}$	$\frac{4.9}{19}$	$\frac{4.5}{18}$	$\frac{4.6}{16}$	$\frac{4.5}{9}$	$\frac{4.8}{5}$	$\frac{4.6}{9}$	$\frac{5.4}{16}$	$\frac{2.6}{20}$	$\frac{5.7}{33}$
------------------	------------------	------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

72.9

72.0

$\frac{4.6}{33}$	$\frac{4.6}{26}$	$\frac{8.0}{21.5}$	$\frac{8.0}{19}$	$\frac{6.3}{16}$	$\frac{6.1}{7}$	$\frac{6.5}{7}$	$\frac{6.5}{16}$	$\frac{7.3}{20}$	$\frac{5.5}{33}$
------------------	------------------	--------------------	------------------	------------------	-----------------	-----------------	------------------	------------------	------------------

68.0

73.8

$\frac{9.5}{33}$	$\frac{8.6}{22}$	$\frac{9.0}{20}$	$\frac{9.0}{17}$	8.3	$\frac{8.6}{9}$	$\frac{8.4}{12}$	$\frac{9.5}{16}$	$\frac{9.5}{17}$	$\frac{9.1}{19}$	$\frac{4.0}{27}$	$\frac{3.7}{33}$
------------------	------------------	------------------	------------------	-----	-----------------	------------------	------------------	------------------	------------------	------------------	------------------

65.2

69.9

$\frac{12.3}{33}$	$\frac{11.5}{23}$	$\frac{11.5}{18}$	$\frac{11.0}{8}$	$\frac{11.3}{7}$	$\frac{11.6}{6}$	$\frac{11.2}{16}$	$\frac{8.1}{25}$	$\frac{7.6}{33}$
-------------------	-------------------	-------------------	------------------	------------------	------------------	-------------------	------------------	------------------

63.1

66.5

$\frac{5.4}{33}$	$\frac{4.4}{30}$	$\frac{4.6}{23}$	$\frac{5.0}{20}$	$\frac{4.5}{8}$	$\frac{4.6}{6}$	$\frac{5.0}{6}$	$\frac{5.5}{18}$	$\frac{2.1}{28}$	$\frac{2.0}{33}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

58.2

63.5

$\frac{10.8}{33}$	$\frac{7.7}{21}$	$\frac{6.7}{8}$	$\frac{6.9}{7}$	$\frac{7.3}{9}$	$\frac{7.8}{15}$	$\frac{6.8}{27}$	$\frac{5.0}{33}$
-------------------	------------------	-----------------	-----------------	-----------------	------------------	------------------	------------------

Sta.

+

1

-

Elev.

968.48

52+0

60.8

+18.2 West Edge Pave.

59.79

52+30.1

59.96

6.83

961.65 $\frac{8}{3}$ 961.64

L.

L

Rt.

25

57.9

$$\begin{array}{r} 106 \\ 33 \end{array}$$

$$\begin{array}{r} 79 \\ 23 \end{array}$$

$$\begin{array}{r} 76 \\ 12 \end{array}$$

7.7

$$\begin{array}{r} 76 \\ 12 \end{array}$$

$$\begin{array}{r} 9.2 \\ 25 \end{array}$$

$$\begin{array}{r} 9.7 \\ 33 \end{array}$$

58.8

60.8

$$\begin{array}{r} 7.73 \\ 50 \end{array}$$

$$\begin{array}{r} 8.21 \\ 25 \end{array}$$

8.69

$$\begin{array}{r} 9.22 \\ 25 \end{array}$$

58.8

$$\begin{array}{r} 9.67 \\ 50 \end{array}$$

60.9

$$\begin{array}{r} 7.60 \\ 50 \end{array}$$

$$\begin{array}{r} 8.06 \\ 25 \end{array}$$

8.52

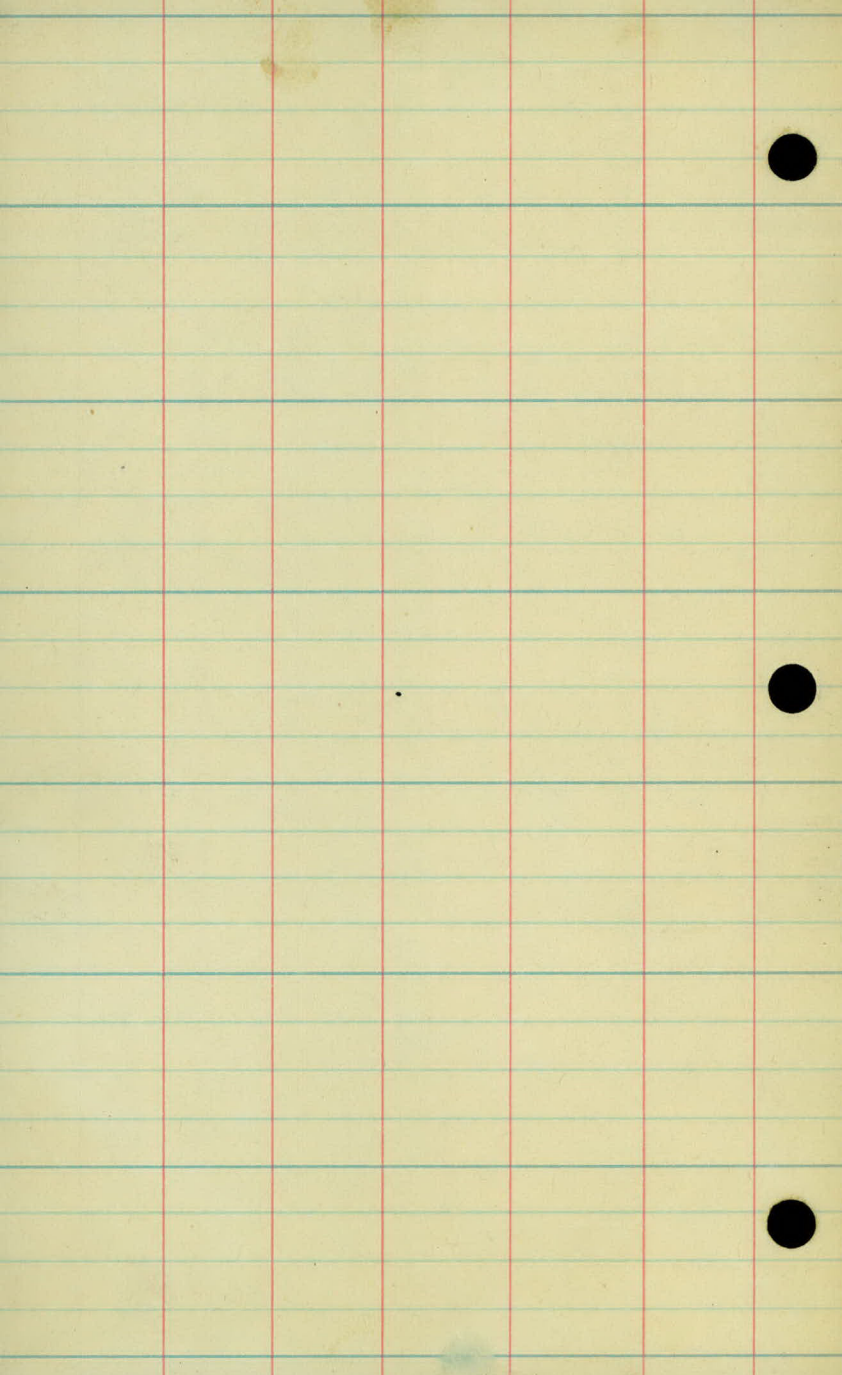
$$\begin{array}{r} 9.06 \\ 25 \end{array}$$

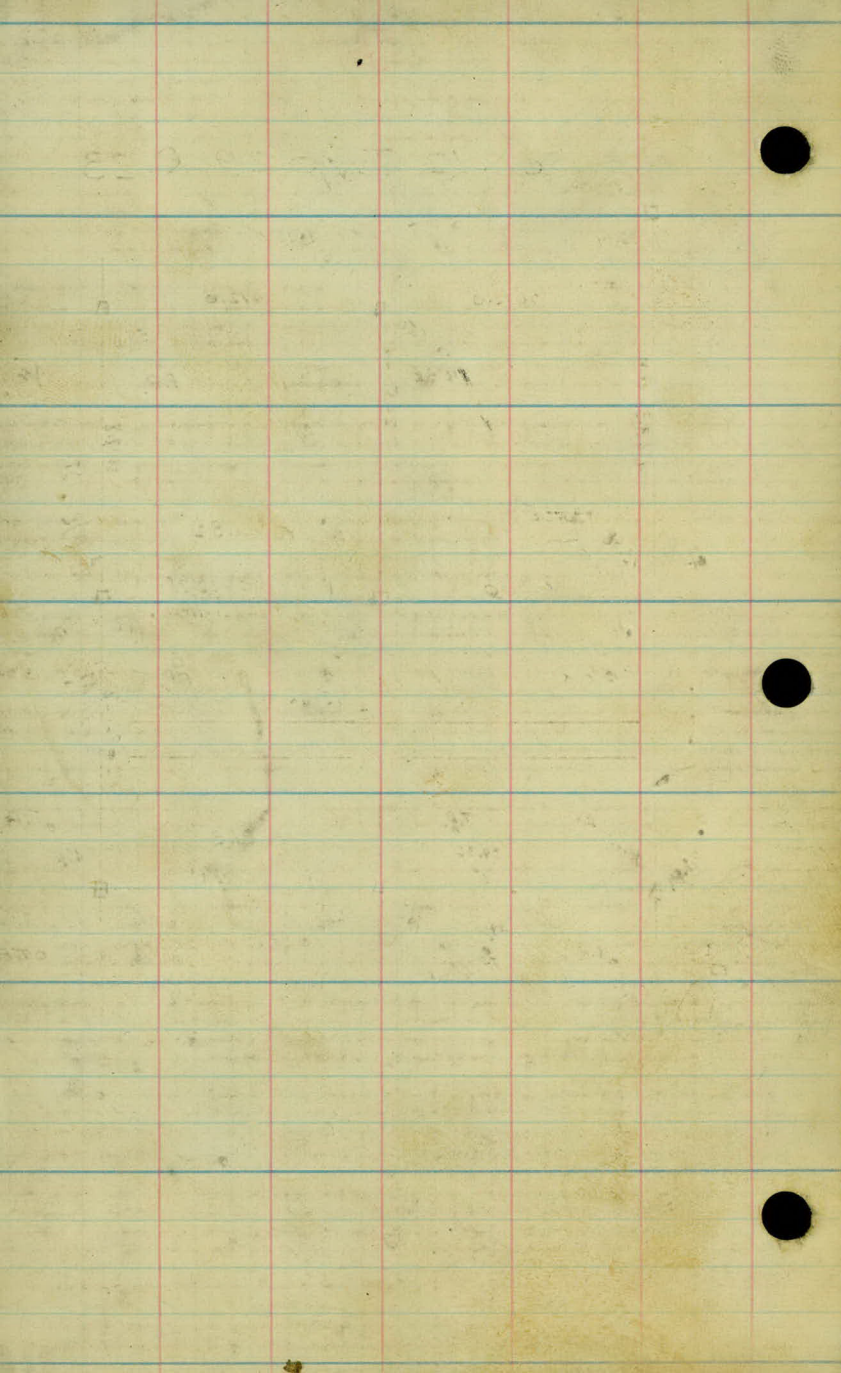
58.9

$$\begin{array}{r} 9.56 \\ 50 \end{array}$$

R.R. in R.R. 25' Rt. 52+11

$$\begin{array}{r} 42 \\ 24 \\ 18 \end{array}$$





Max + Igglekay's Cedar
 of Out Ldts

G. 50 km

33
 757.68
 494.34
 33

131802 - E. Side Western
 from 13-mi

no 44.56
 1318.02

1326.54

1337.2
 1318.02

2655.22 Rec.
 no 44.56 Rec.
 no 44.80 - Meas.

1337.2
 1318.02
 2655.22

660
 677.2

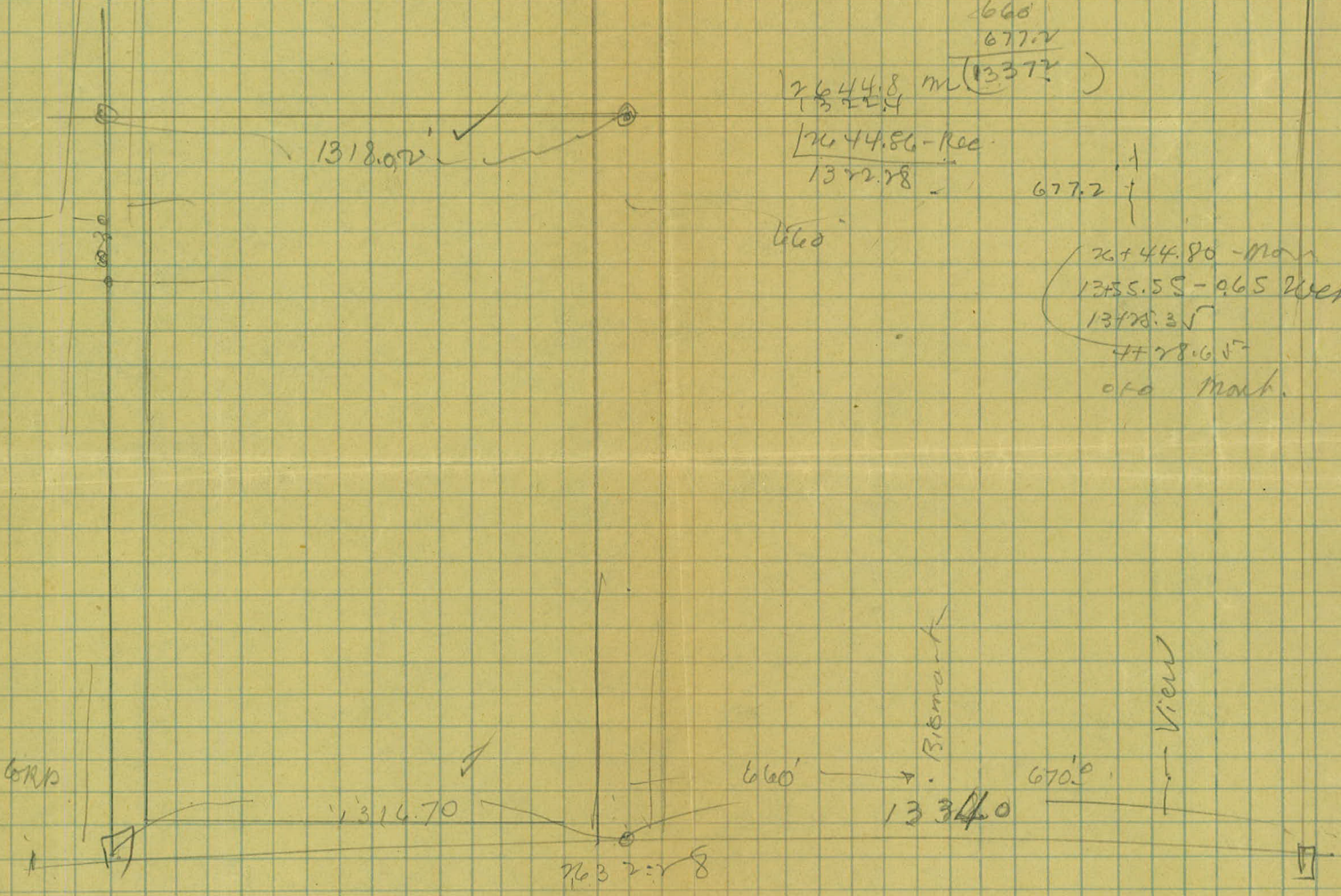
2644.8 m (1337.2)

no 44.86 - Rec.
 1322.28

677.2

660

no 44.80 - man
 1355.55 - 965 West
 13428.35
 4428.65
 old Mont.



660

1314.70

660

1334.0

670.0

2632.28

1330
 1316.7

2646.7 = Rec.
 no 32.28 Rec.
 no 31.47
 2631.64

1316.70
 338
 2654.70

660
 670
 1330

1316.70
 1326.0
 2657.70

Rico 74

man 76

33.0
405.9
438.9
405.9
33

1316.7

444.34
757.68
66.

1318.02

13418.35
13 12 85
12.50

1328.25
1324
2.92

99607%

1322.4

Western Ave

(1318.02 = Req.)
1312.85

(Req. 2655.22)
(Meas. 2644.80)

66°
677.4
(1337.2 = Req.)
1331.95

1331.95
1312.85
2644.80

Co. Rd. 13

Minnesota Ave

Co. Rd. 13

1582
9.21
6.61

(1316.7)
1309.21

R.D. 21.10

22°
4154

2646.7 = Req.

(1330.03) Req.
1322.43

Rice St.

2631.64 Meas

994309%

1309.21
1322.43
2631.64