

Book #2- Dr. 11

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN

Survey

CARL - SPRING ST.

Walnut St.

Pleasant St.

From Larpeur Ave.

To Summer St.

Road Acc't. No. R1 - R2

Date Filed 11-8-29

File Rose Twp.

PROJ. 29-R1

Transit Notes

E Carl St.
Rose Hill Twp.

Sept. 28, 1929.

Don Weber
M. A. Bedford
J. Bell

Walnut St to Pleasant St.

Sta.

 Δ Lt Δ Rt.

+99.21 P.T.

25°13'

+50

22°18.5'

6

19°22'

+50

16°25.5'

+100.44 P.I.

5

13°29'

+50

10°32.5'

4

7°35'

+50

4°39.5'

3

1°43'

+70.9 P.R.C.

0°00' 9°56'

+50

9°04'

2

6°58'

+153.24 P.I.

+50

4°53'

1

2°48'

+50

0°43'

+33 P.C.

0°00'

0+00

E Larpenleur Ave.

 $\Delta = 50.26$ Lt

D = 11°46'

T = 229.54

L = 428.31

P = 487.79

 $\Delta = 19.52$ Rt.

D = 8°21'

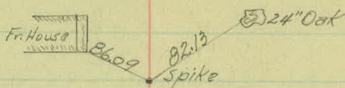
T = 120.24

L = 237.90

P = 669.79

686.79

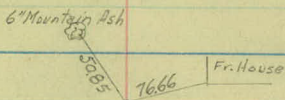
P.T.



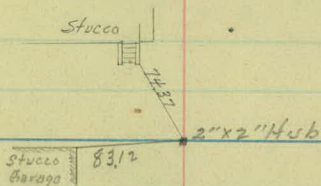
P.I.

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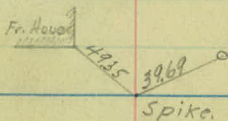
P.R.C.



P.I.



P.C.



Sta.

$\Delta L + \Delta R$

20 + 10.14 End of Project

16 + 13.12 P.O.T.

13 + 51.05 $\neq$ Spring St

+01.11 P.T. $10^{\circ}43'$

9 $10^{\circ}39'$

+50 $7^{\circ}30'$

+17.29 P.I.

8 $4^{\circ}21'$

+50 $1^{\circ}12'$

7 + 30.99 P.C. $0^{\circ}00'$

$\Delta = 21^{\circ}26'$
 $D = 12^{\circ}36'$
 $T = 86.3$
 $L = 170.12$
 $R = 455.65$

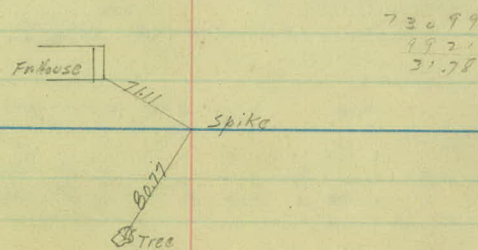
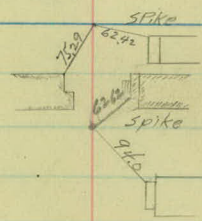
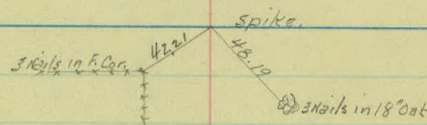
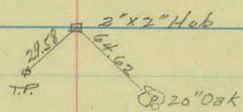
7

2166

5086

10.43

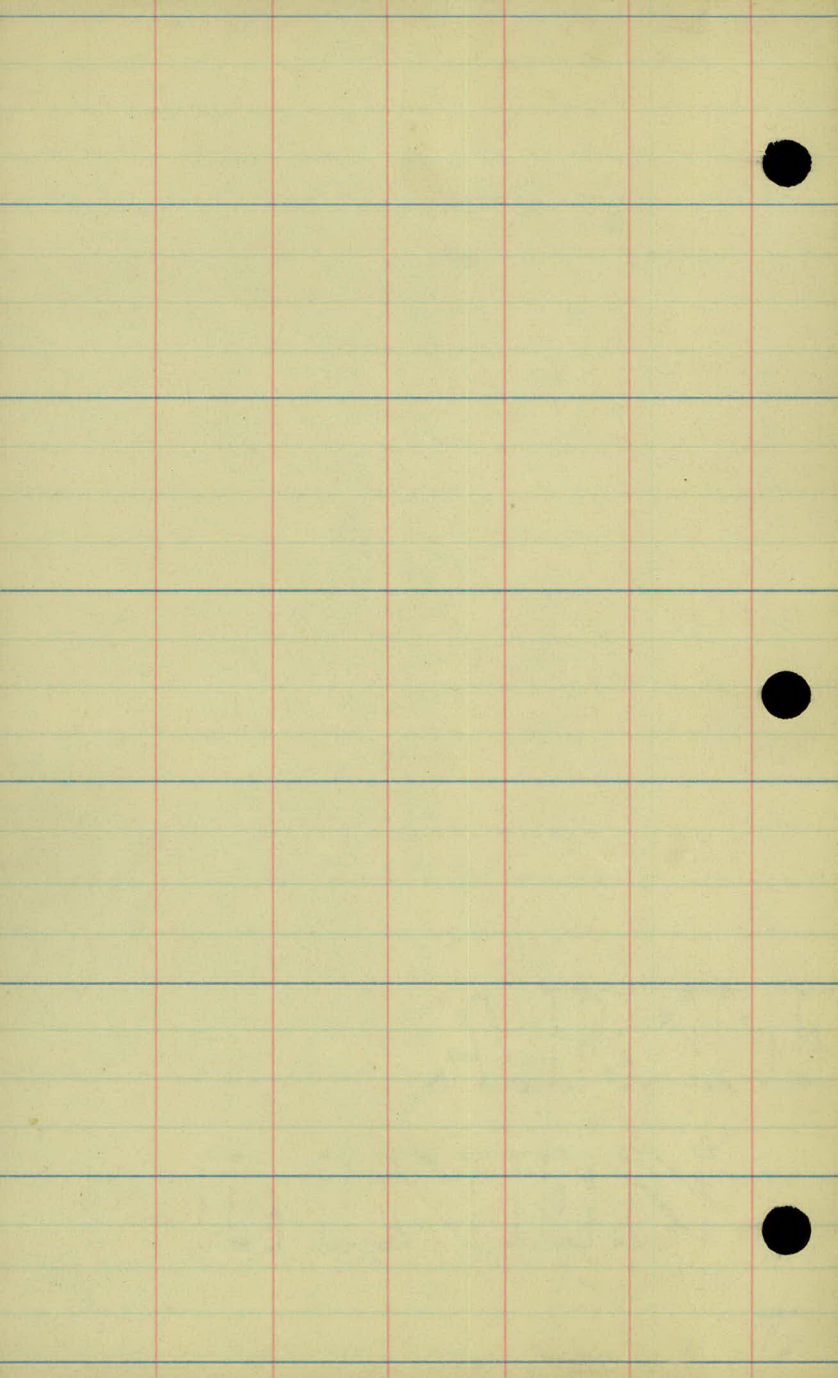
End



73099

9921

31.78



Topog. Notes

Carl St. Rose Twp.

2 Lapenteur Ave To 2 Summer St.

6

5

4

3

2

1

0+00

Larpenleur Ave.

L7

E

R7.

+50-20 Oak 27'

+48 P.P. 27'

13' 10'

+64-12 Oak 29'

+56-15 Oak 30'

+35-12 Oak 26'

200-400

Drive

11' 7'

+27-Lilac Adg. 23'

+23 P.P. 22'

+16

III

+43 Conc Steps 27'

10' 7'

+98 Pr. Dr.

+64 Pr. Dr.

+67 P.P. 22'

+56 Pr. Dr.

11' 7'

+64 Pr. Dr.

+86 Pr. Dr.

+73 Pr. Dr.

+44 P.P. 19'

+11 Gyp. Plc 20'

13' 13'

+70-Alley

+90 P.P. 20'

+77 Alley

+35 T.P. 30'

3' 15'

+34-Stop Sq. 10'

+58 P.P. 25'

+21 T.P. 27'

+10 Edge of Pavl

13

12

11

10

9

8

7

+72 R.H. 55.12
+72 P.R. 16

+91 = P.R. Dr.

+51.05 = E Spring

+30-13" x 36" C.M.

25 11.3

10'6"

+22 Conc. Walk 26'

III

10'8"

+02. P.R. 16

+77 - Conc. Wk. 27
+65 - P.Dr.

III

+45 P.R. Dr

+48.8" P.R. 12'

+37-6" P.R. 12'

9'6"

+73 P.R. Dr

III

9'6"

+03. P.R. 19'

+78 P.R. Dr.

+50 = End of Elms.

9'6"

+98 Conc. Step 20'

III

+97 = Row 4 Elms 1" thick 26'

+77 P.R. Dr.

+77 = 12" x 9' C.M. 15'

8'7"

+97 - P.R. 13'

I one

4'

20

19

18

17

16

15

14

47

PL.

(Finis)

402. P.P. 29'

75'

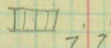
8' 5'

+ 87 P. Dr

+ 40-14'08k31'

+35 Pr. Dr.

+ 15 Conc. Steps 25'



+66-Pr. D.

424 P. Dr.

+86 Pr Dr
+80 F. Cor. 29'

+80 F. Cor. 29'



+53 P₁ Dr.

+47-12' Oct 22'

+29-10'08" 28'

400 Fence Cor 29' 77

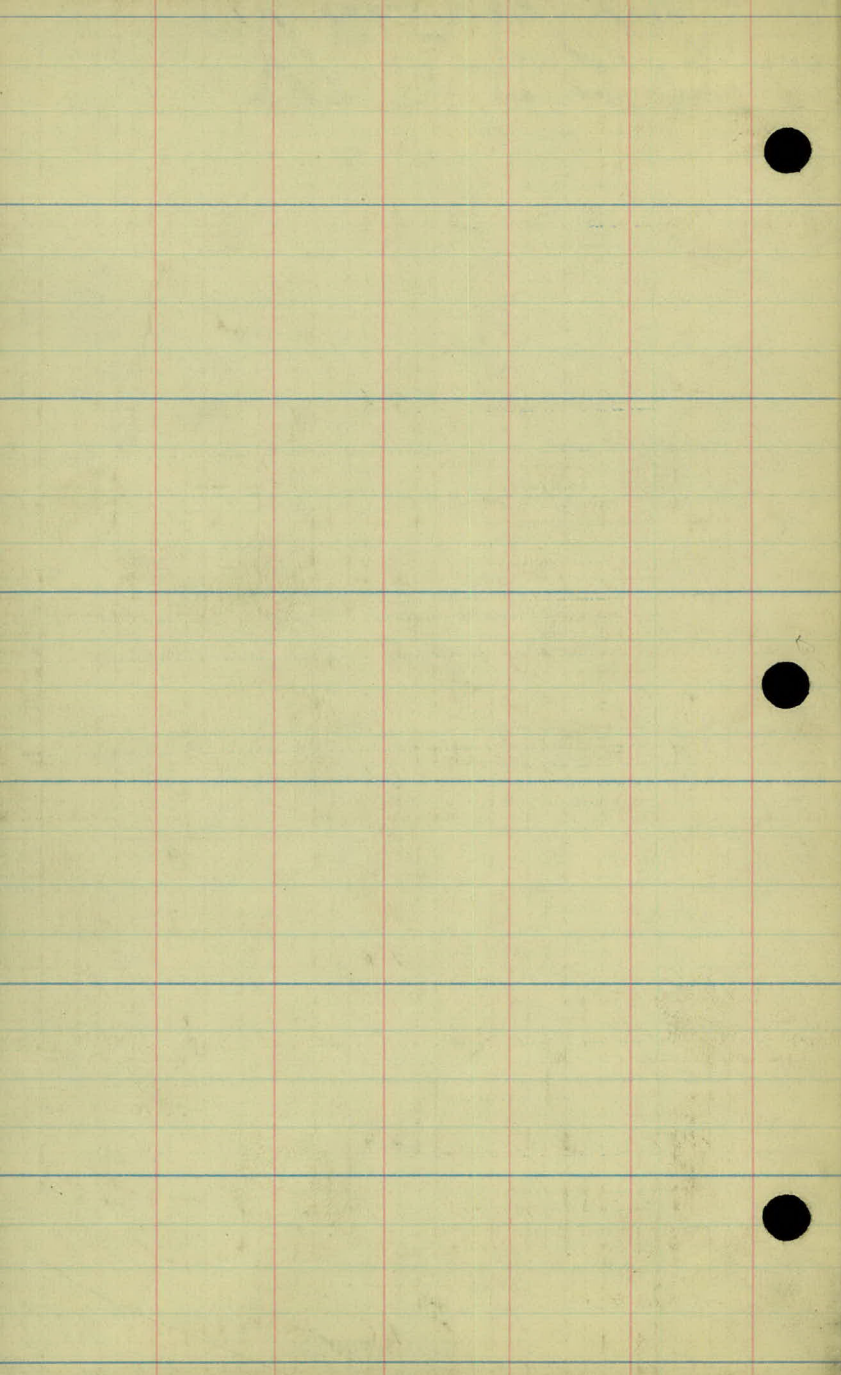
+98-15" Osk 20',

477-12" Oak 25

+16 Conc. Step 28'



5 9 6



Levels
and
X Sections
Carl St Rose Trp.

Sta	+	H.I.	-	Elev.
				326.22
	4.83	331.05		
	4.29	329.79	5.55	325.50
B.M.			3.00	326.79
T.P.	7.49	331.02	6.26	323.53
T.P.	1.92	329.65	3.29	327.73
B.M.			9.58	320.07
T.P.	5.54	324.75	10.44	319.21
B.M.	2.17	324.75	2.17	322.58
0+00		E Larp. Arc		21.8
+ 10		Edge Pav.		21.8
+ 16		Sh. Line.		21.7
+ 24		Ditch		21.4
+ 34				20.5
+ 41				20.1
+ 50				19.2
1				17.2
+ 50				17.3

Lt. Lt. Pt. Weber

Clear

Red Beaton

Tape Bell

Spike in Tree

Spike in 20" Oak 60' Lt Sta. 13+10

Nails in P.R. 15' Rt Sta. 8+00

No. Cor. lower Conc. Step 4+44 — 27' Rt.

Spike in P.R. #262 00-14-30' East.

$$\frac{3.5}{50} \quad 2.95 \quad \frac{2.2}{50}$$

$$\frac{3.5}{50} \quad 3.0 \quad \frac{2.1}{50}$$

$$\frac{3.1}{35} \quad \frac{3.9}{30} \quad \frac{2.7}{14} \quad 3.1 \quad \frac{3.0}{23} \quad \frac{2.8}{30} \quad \frac{2.5}{35}$$

$$\frac{5.1}{35} \quad \frac{4.8}{30} \quad \frac{4.4}{14} \quad 3.4 \quad \frac{3.8}{17} \quad \frac{3.5}{22} \quad \frac{4.3}{27} \quad \frac{4.2}{30} \quad \frac{4.0}{35}$$

$$\frac{4.2}{35} \quad \frac{4.2}{30} \quad \frac{4.9}{8} \quad 4.3 \quad \frac{5.0}{13} \quad \frac{4.8}{14} \quad \frac{5.1}{19} \quad \frac{3.9}{30}$$

$$\frac{4.3}{35} \quad \frac{5.8}{30} \quad \frac{9.7}{22} \quad \frac{7.6}{13} \quad \frac{5.4}{6} \quad 4.7 \quad \frac{5.3}{14} \quad \frac{7.0}{19} \quad \frac{5.0}{25} \quad \frac{3.1}{30}$$

$$\frac{3.5}{42} \quad \frac{9.3}{30} \quad \frac{4.3}{9} \quad \frac{5.7}{4} \quad 5.6 \quad \frac{5.6}{13} \quad \frac{7.3}{17} \quad \frac{7.6}{22} \quad \frac{4.3}{30} \quad \frac{4.3}{35}$$

$$\frac{7.7}{35} \quad \frac{8.2}{30} \quad \frac{8.8}{5} \quad \frac{7.8}{3} \quad 7.6 \quad \frac{7.5}{15} \quad \frac{8.8}{18} \quad \frac{9.0}{23} \quad \frac{5.8}{30} \quad \frac{5.3}{35}$$

$$\frac{8.3}{35} \quad \frac{8.3}{30} \quad \frac{8.4}{8} \quad \frac{7.7}{2} \quad 7.5 \quad \frac{7.5}{13} \quad \frac{8.4}{16} \quad \frac{8.8}{25} \quad \frac{7.5}{27} \quad \frac{7.2}{30} \quad \frac{6.6}{35}$$

Sta + H.I. - Elev.
324.75

2 18.3

+50 18.9

3 19.1

+50 19.4

4 19.7

T.P. 12.22 332.29 4.70 329.05 320.07 ✓

+50 20.8

5 22.2

+50 23.8

6 26.0

+50 27.8

+70 28.3

+86 apprx. to Lone St 28.6

L+

£

RT

 $\frac{4.7}{35} \frac{4.7}{30} \frac{5.1}{19} \frac{7.5}{15} \frac{6.9}{13} 6.5 \frac{6.9}{15} \frac{8.5}{16} \frac{8.5}{18} \frac{7.7}{19} \frac{8.1}{30} \frac{8.1}{30}$
 $\frac{4.6}{35} \frac{4.6}{30} \frac{5.0}{19} \frac{6.6}{18} \frac{6.3}{12} 5.9 \frac{6.3}{11} \frac{7.4}{13} \frac{7.4}{14} \frac{6.9}{15} \frac{7.4}{30} \frac{5.5}{35}$
 $\frac{4.1}{35} \frac{4.1}{30} \frac{4.2}{22} \frac{6.1}{19} \frac{6.0}{12} 5.7 \frac{6.1}{10} \frac{7.0}{11} \frac{7.0}{13} \frac{6.5}{15} \frac{6.4}{30} \frac{5.8}{35}$
 $\frac{4.6}{35} \frac{4.6}{30} \frac{5.1}{19} \frac{5.9}{18} 5.4 \frac{5.8}{10} \frac{6.5}{12} \frac{6.4}{30} \frac{4.2}{35}$
 $\frac{1.2}{35} \frac{2.2}{30} \frac{3.8}{22} \frac{3.8}{18} \frac{5.6}{14} 5.1 \frac{5.8}{9} \frac{6.0}{30} \frac{6.0}{30}$

No. cor conc. Step 27 RT St. 4+44

 $\frac{6.6}{35} \frac{7.2}{30} \frac{8.5}{22} \frac{9.0}{17} \frac{11.9}{13} 11.5 \frac{11.7}{8} \frac{13.1}{12} \frac{12.5}{27} \frac{11.2}{30} \frac{10.9}{35}$
 $\frac{5.7}{35} \frac{6.1}{30} \frac{7.9}{22} \frac{8.2}{18} \frac{11.2}{14} \frac{10.6}{10} 10.1 \frac{10.7}{7} \frac{11.7}{11} \frac{12.1}{26} \frac{11.2}{30} \frac{11.2}{35}$
 $\frac{5.7}{35} \frac{4.2}{30} \frac{5.0}{20} \frac{9.2}{14} 8.5 \frac{9.2}{8} \frac{9.7}{10} \frac{9.7}{13} \frac{8.6}{14} \frac{8.6}{30} \frac{8.6}{35}$
 $\frac{3.2}{35} \frac{3.2}{30} \frac{3.7}{21} \frac{7.5}{16} \frac{7.0}{12} 6.3 \frac{6.9}{11} \frac{7.6}{13} \frac{7.6}{15} \frac{6.7}{16} \frac{6.5}{30} \frac{6.5}{35}$
 $\frac{5.2}{35} \frac{3.2}{30} \frac{3.2}{19} \frac{5.1}{16} 4.5 \frac{5.1}{14} \frac{6.2}{19} \frac{6.3}{30} \frac{6.3}{35}$
 $\frac{2.4}{35} \frac{2.4}{30} \frac{2.5}{22} \frac{4.3}{19} 4.0 \frac{4.4}{5} \frac{5.4}{30} \frac{5.7}{35}$
 $\frac{2.4}{50} \frac{3.0}{25} 3.7 \frac{5.2}{25} \frac{6.1}{50}$

Sta	+	H.I.	-	Elev.
7		332.29 ✓		28.5
+50				28.2
8			4.56	27.7 ✓ 327.73
+50				27.1
9				26.8
T.P.	301	329.48 ✓	5.82	326.41 ✓
+50				26.4
10				26.2
+50				25.0
11				24.1
+50				23.8
12				23.2
+50				23.3
13				23.4

Lt

L

R4

$$\frac{2.5}{50} \quad \frac{3.3}{30} \quad \frac{3.5}{18} \quad 3.8 \quad \frac{4.6}{12} \quad \frac{5.6}{30} \quad \frac{6.0}{35}$$

$$\frac{1.9}{35} \quad \frac{2.3}{30} \quad \frac{2.3}{21} \quad \frac{3.7}{21} \quad \frac{4.7}{15} \quad \frac{4.0}{14} \quad 4.1 \quad \frac{4.5}{9} \quad \frac{5.1}{11} \quad \frac{5.9}{30} \quad \frac{6.0}{30}$$

$$\frac{2.4}{35} \quad \frac{2.6}{30} \quad \frac{3.2}{22} \quad \frac{5.6}{19} \quad \frac{5.8}{16} \quad \frac{5.1}{15} \quad \frac{5.1}{9} \quad 4.6 \quad \frac{5.7}{12} \quad \frac{5.9}{30} \quad \frac{5.9}{35}$$

P.R. 15' R1 Sta 8+00

$$\frac{2.6}{35} \quad \frac{2.6}{31} \quad \frac{4.2}{26} \quad \frac{3.9}{23} \quad \frac{6.1}{20} \quad 5.2 \quad \frac{6.0}{11} \quad \frac{7.3}{16} \quad \frac{6.5}{17} \quad \frac{6.6}{30} \quad \frac{6.6}{35}$$

$$\frac{2.8}{35} \quad \frac{2.8}{30} \quad \frac{4.4}{25} \quad \frac{4.4}{22} \quad \frac{6.0}{19} \quad \frac{6.0}{10} \quad 5.5 \quad \frac{6.7}{11} \quad \frac{8.0}{12} \quad \frac{7.5}{19} \quad \frac{7.4}{30+35}$$

$$\frac{0.3}{35} \quad \frac{0.3}{31} \quad \frac{2.3}{28} \quad \frac{2.8}{21} \quad \frac{4.0}{18} \quad \frac{4.0}{16} \quad \frac{3.5}{14} \quad 3.1 \quad \frac{3.8}{13} \quad \frac{5.7}{18} \quad \frac{4.8}{30} \quad \frac{4.7}{35}$$

$$\frac{1.4}{35} \quad \frac{1.4}{21} \quad \frac{4.2}{17} \quad \frac{4.2}{16} \quad \frac{3.5}{14} \quad 3.3 \quad \frac{3.8}{10} \quad \frac{4.8}{13} \quad \frac{5.5}{17} \quad \frac{4.4}{19} \quad \frac{5.3}{30} \quad \frac{5.3}{35}$$

$$\frac{1.3}{35} \quad \frac{1.7}{30} \quad \frac{3.6}{29} \quad \frac{4.1}{19} \quad \frac{4.9}{18} \quad 4.5 \quad \frac{5.2}{8} \quad \frac{6.2}{13} \quad \frac{6.6}{30} \quad \frac{6.6}{35}$$

$$\frac{3.8}{35} \quad \frac{4.1}{30} \quad \frac{5.1}{28} \quad \frac{5.8}{18} \quad 5.4 \quad \frac{6.4}{12} \quad \frac{6.4}{30} \quad \frac{6.4}{35}$$

$$\frac{4.8}{35} \quad \frac{4.6}{30} \quad \frac{5.0}{19} \quad \frac{6.2}{16} \quad 5.7 \quad \frac{6.9}{9} \quad \frac{6.0}{30} \quad \frac{5.8}{35}$$

$$\frac{4.9}{35} \quad \frac{5.5}{29} \quad \frac{6.0}{25} \quad \frac{6.0}{19} \quad \frac{7.0}{14} \quad 6.3 \quad \frac{7.5}{12} \quad \frac{7.2}{19} \quad \frac{5.7}{30} \quad \frac{5.5}{35}$$

$$\frac{6.2}{35} \quad \frac{6.4}{26} \quad \frac{7.4}{24} \quad \frac{7.4}{16} \quad \frac{6.5}{12} \quad 6.2 \quad \frac{6.7}{6} \quad \frac{7.9}{10} \quad \frac{5.4}{30} \quad \frac{5.5}{35}$$

$$\frac{4.3}{40} \quad \frac{4.6}{35} \quad \frac{7.2}{28} \quad \frac{7.4}{16} \quad \frac{6.6}{14} \quad 6.1 \quad \frac{6.6}{7} \quad \frac{7.9}{9} \quad \frac{5.8}{30} \quad \frac{5.7}{35}$$

			^{29.48} + H.I. ✓	-	Elev.	✓
B.M.	6.06	33285	2.69		326.79	
13						
+ 50	opp. E	→	Spring St.		23.9	
14					25.2	
+ 50					26.5	
15					27.4	
+ 50					28.1	
16					29.3	
+ 50					28.5	
17					25.9	
+ 50					24.1	
18					22.5	
T.P.	10.98	338.94 ✓	4.89		327.96 ✓	
16 + 18					28.9	
+ 21					28.9	

Lt # Pt.

Spike in 20'00k 60' Lt 54 13+10

$$\begin{array}{r} 6.3 \quad 8.9 \quad 9.0 \quad 11.2 \quad 12.0 \\ \hline 5.0 \quad 2.1 \quad \quad \quad 2.5 \quad 5.0 \end{array}$$

$$\begin{array}{r} 3.0 \quad 3.3 \quad 3.6 \quad 5.3 \quad 6.6 \quad 8.0 \quad 7.7 \quad 8.3 \quad 7.9 \quad 8.2 \quad 8.2 \\ \hline 3.5 \quad 3.0 \quad 2.8 \quad 2.7 \quad 1.8 \quad 1.4 \quad \quad \quad 7.0 \quad 7.2 \quad 3.0 \quad 3.5 \end{array}$$

$$\begin{array}{r} 1.0 \quad 1.4 \quad 5.2 \quad 5.8 \quad 6.9 \quad 6.4 \quad 7.5 \quad 6.6 \quad 8.4 \quad 8.7 \\ \hline 3.5 \quad 3.3 \quad 2.7 \quad 1.7 \quad 1.4 \quad \quad \quad 9 \quad 11 \quad 3.0 \quad 3.5 \end{array}$$

$$\begin{array}{r} 6.5 \quad 6.5 \quad 6.4 \quad 5.5 \quad 6.5 \quad 7.8 \quad 8.0 \\ \hline 3.5 \quad 3.0 \quad 1.1 \quad \quad \quad 7.0 \quad 3.0 \quad 3.5 \end{array}$$

$$\begin{array}{r} 4.5 \quad 4.5 \quad 4.4 \quad 5.3 \quad 4.8 \quad 6.2 \quad 7.5 \quad 7.9 \quad 8.1 \\ \hline 3.5 \quad 3.0 \quad 1.5 \quad 1.0 \quad \quad \quad 9 \quad 2.0 \quad 3.0 \quad 3.5 \end{array}$$

$$\begin{array}{r} 1.4 \quad 1.4 \quad 1.6 \quad 2.3 \quad 4.1 \quad 3.6 \quad 4.8 \quad 3.7 \quad 2.2 \quad 3.3 \quad 4.3 \\ \hline 3.5 \quad 3.0 \quad 2.0 \quad 1.4 \quad 1.1 \quad \quad \quad 7.1 \quad 7.2 \quad 1.7 \quad 3.0 \quad 3.5 \end{array}$$

$$\begin{array}{r} 4.4 \quad 5.3 \quad 5.8 \quad 6.5 \quad 6.1 \quad 6.1 \\ \hline 8 \quad 2.2 \quad 2.4 \quad 3.0 \quad 3.5 \end{array}$$

$$\begin{array}{r} 7.0 \quad 7.8 \quad 8.0 \quad 7.0 \quad 7.0 \\ \hline 7 \quad 3.0 \quad 3.1 \quad 3.5 \end{array}$$

$$\begin{array}{r} 6.6 \quad 6.9 \quad 7.3 \quad 9.4 \quad 8.8 \quad 9.8 \quad 9.7 \quad 9.5 \quad 9.5 \\ \hline 3.5 \quad 3.0 \quad 1.9 \quad 1.4 \quad \quad \quad 1.0 \quad 1.7 \quad 3.0 \quad 3.5 \end{array}$$

$$\begin{array}{r} 8.0 \quad 8.0 \quad 9.2 \quad 11.0 \quad 10.4 \quad 11.2 \quad 10.5 \quad 9.9 \quad 9.9 \\ \hline 3.5 \quad 3.2 \quad 3.0 \quad 1.5 \quad \quad \quad 1.0 \quad 7.8 \quad 3.0 \quad 3.5 \end{array}$$

$$\begin{array}{r} 7.0 \quad 7.2 \quad 8.3 \quad 10.4 \quad 10.00 \quad 10.1 \quad 8.5 \quad 7.8 \quad 8.4 \quad 8.9 \\ \hline 3.5 \quad 3.0 \quad 1.3 \quad 9 \quad \quad \quad 11 \quad 7.9 \quad 2.5 \quad 3.0 \quad 3.5 \end{array}$$

$$\begin{array}{r} 3.7 \quad 4.2 \quad 4.8 \quad 7.6 \quad 10.5 \quad 10.00 \quad 11.3 \quad 12.0 \quad 12.3 \\ \hline 3.5 \quad 3.0 \quad 1.8 \quad 1.7 \quad 9 \quad \quad \quad 11 \quad 2.0 \quad 3.5 \end{array}$$

Sta 16 + H.I. 338.94 - Elev.

+50

~~27.6~~

17

~~25.4~~

2.51 330.47 10.98 327.96

18+50

20.0

T.P. 1.73 321.48 10.72 319.75

19

17.2

+50

15.4

+81

Ditch Running E+W. 14.9

+90

present traveled R. 15.2
Summer st.

20

14.8

+101.4

End of Project. 15.2

B.M.

4.72 316.76

Lt

±

Rt

$$\frac{3.7}{35} \quad \frac{3.7}{30} \quad \frac{4.7}{20} \quad \frac{8.4}{19} \quad \frac{10.5}{14} \quad \frac{11.3}{9}$$

(10.4)

$$\frac{10.2}{35} \quad \frac{10.6}{30} \quad \frac{10.6}{21} \quad \frac{12.3}{20} \quad \frac{13.5}{12}$$

(13.0)

$$\frac{11.0}{35} \quad \frac{11.0}{30} \quad \frac{10.8}{18} \quad \frac{11.0}{8} \quad 10.5 \quad \frac{11.3}{6} \quad \frac{10.4}{21} \quad \frac{10.4}{35}$$

$$\frac{4.6}{35} \quad \frac{4.6}{30} \quad \frac{5.2}{26} \quad \frac{5.2}{15} \quad 4.3 \quad \frac{5.1}{6} \quad \frac{4.1}{11} \quad \frac{3.0}{30} \quad \frac{3.0}{35}$$

$$\frac{7.2}{35} \quad \frac{7.2}{30} \quad \frac{7.0}{17} \quad 6.1 \quad \frac{6.4}{12} \quad \frac{5.4}{28} \quad \frac{4.2}{33} \quad \frac{4.2}{35}$$

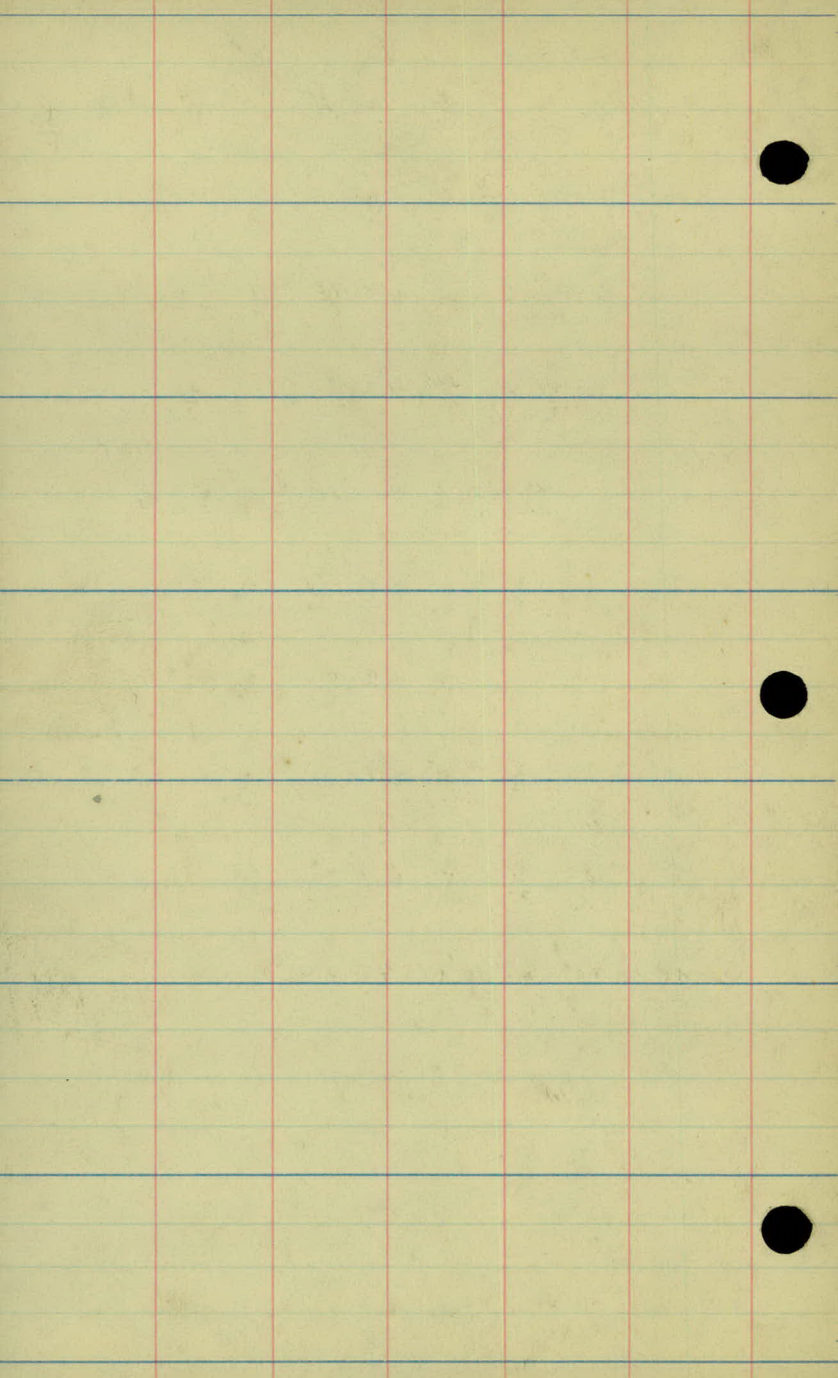
$$\frac{7.2}{50} \quad \frac{7.2}{25} \quad 6.6 \quad \frac{6.6}{25} \quad \frac{6.8}{50}$$

$$\frac{6.8}{50} \quad \frac{6.6}{25} \quad 6.3 \quad \frac{6.0}{25} \quad \frac{6.0}{50}$$

$$\frac{7.6}{50} \quad \frac{7.5}{25} \quad 6.7 \quad \frac{6.3}{25} \quad \frac{6.1}{50}$$

$$\frac{8.3}{50} \quad \frac{7.5}{35} \quad \frac{7.0}{20} \quad 6.4 \quad \frac{6.8}{25} \quad \frac{6.6}{50}$$

Spike in 20" Oak 30' Rt Sta. 19+50



Location Transit-Level
Notes.

Spring St
0+00 to 13+31.58 $\pm$ Pleasant

Larpenteur Ave to Summer St

Stn	+	H.I.	—	Elev.
				326.22
4.86		331.08		
4.53		330.03	5.58	325.50
6.75		334.38	2.40	327.63
			6.01	328.37
1.07		323.98	11.47	322.91
			4.50	319.48

13+31.58

6+50.79

650.79

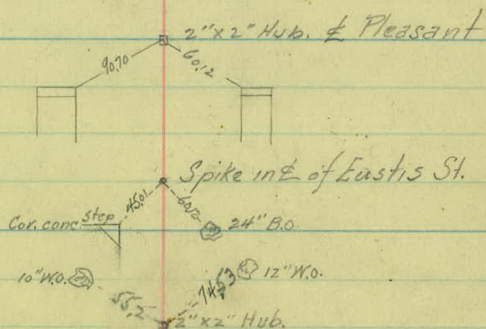
0+00

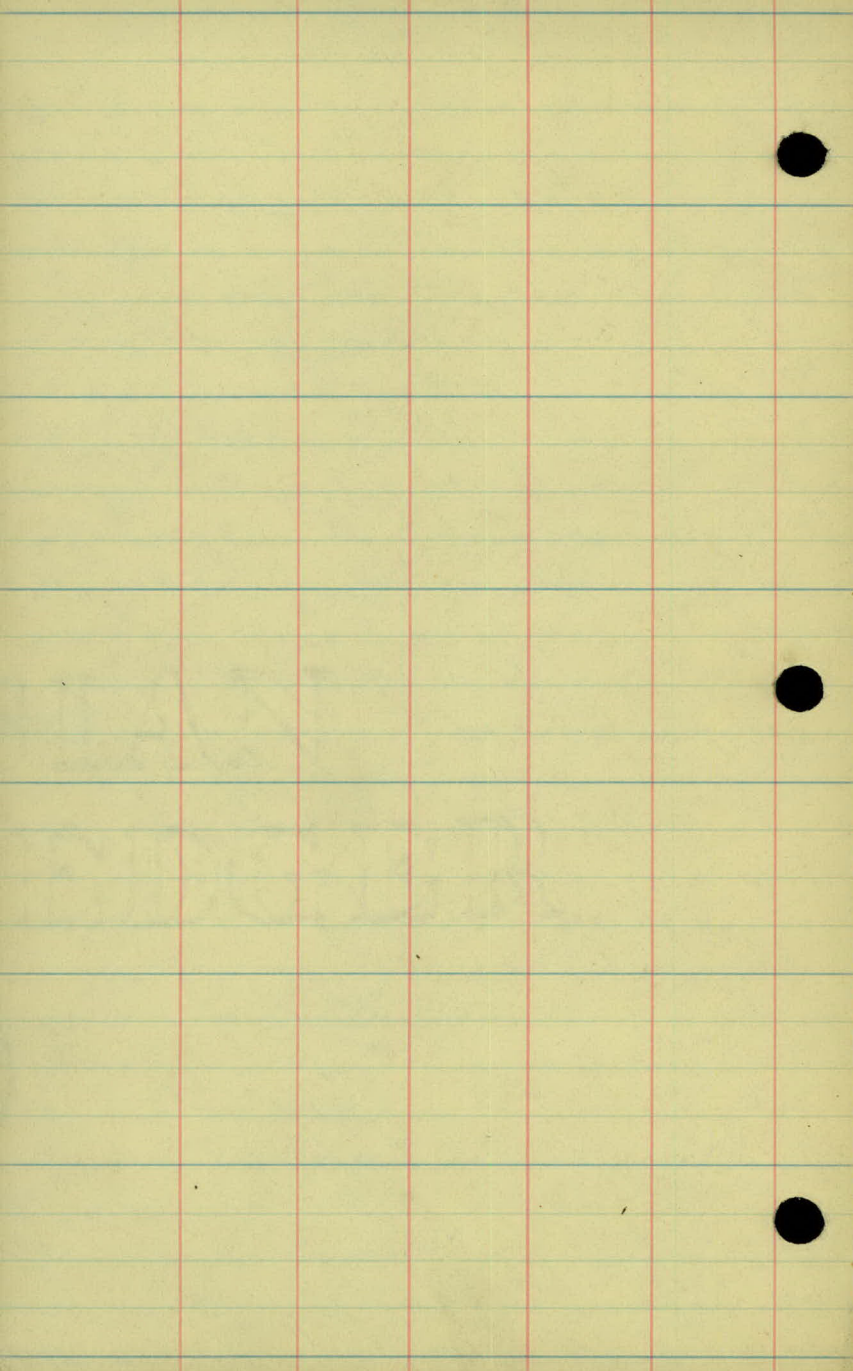
Spike in 12" Oak 500' So. Sta. 12+80.

Spike in 36" Cottonwood 20' East of 13+31.58

Top of Hyd. 30' Rt Sta. 6+30

Spike in 12" Oak 15' No. of Sta 0+00





9-20-29

Weber Beaton Bell

Topography.
Spring St

0400

To

13+31.58

6



5

4



3

2

1



0+00

+72 R.P. 9' Lt
 +64 = 12" x 46' C.M. 15' Lt + 25' Rt
 +50.79 E. El. 15' 1/2
 +35 = Cross Drain 12" x 45' C.M. = 21.3 Lt + 23.7 Rt
 +16 = Ctr 5' Wood Walk
 +16 Cor. 13' 1/2

+07 Cor. Cnc. Wk.
 +06 = End Fence
 +00 T.P. 21' Lt

+78 R.P. 18' Lt
 +09 Cor. Fence 22' Lt
 +03 = E. Fr. Drive

+94 = R.P. - 20' Lt
 +89 E. Alley
 +84 = 12" x 18' C.M.
 +79 T.P. = 21' Lt
 +77 = End of Fence

+28 Beg. Board Fence
 +20 = End of Berry Patch 24' Lt

+85 = T.P. 21' Lt
 +51 Road Spr. 16'
 +47 = R.P. 20' Lt
 +47 = Beg. Berry Patch 25'

+83 To 3405.
 Hedge 23' Rt

+71 R.P. + T.P.
 20' Rt
 Row of Live Bushes
 +20 To 39
 20' Lt

+82 = 24" Oak 22'
 Ger. Ent + 76
 +70 T.P. 28'
 +69 = R.P. 28'
 +53 Fr. Drive
 +25 = 24" Oak 26'

+99 = End of Fence 32'
 +94 = 18" Oak 24' Rt
 +47 Twin Apple 29' Rt
 +22 = E. Cond. Walk to School 27' Rt

+95 Beg. of Fence 31' Lt

+84 = T.P. - 24' Rt

+00 = 8" Cottonwood 18'

+27 = E. Malvern St app.
 6' = 12" x 14' C.M.

+40 = 12" x 16' C.M. 2' Rt

+60 = Guy Pole
 21'

+40 = 20" Oak 21' Rt

13

12

11

10

9

8

7

End. = Pleasant

+80 = 24" Oak 27
+67 = P.P. 22' Lt.

+93 = P.D. Drive
+93 = 30" Oak 32
+73 = T.P. 22' Lt.
+68 = P.P. 22' Lt.

+79 = P.D. Drive.

+64 Alley.

26' +37 End Gard.

26' +14 = Beg Garden

+70 = P.P. -22' +70 = P.P. 22'

+52 T.P. 21' +52 = T.P. 21'

+02 = P.D. Sq. 22

+89 = Carl's app.

+76 = P.P. 21' Lt.

+32 = End Garden 28'

+22 = T.P. 22' Lt.

+84 = 12" x 36" C.M.
+84 = 31" C.M. 21'

+32 = Beg Garden 28'

+32 = T.P. 21'

+23 = Alley

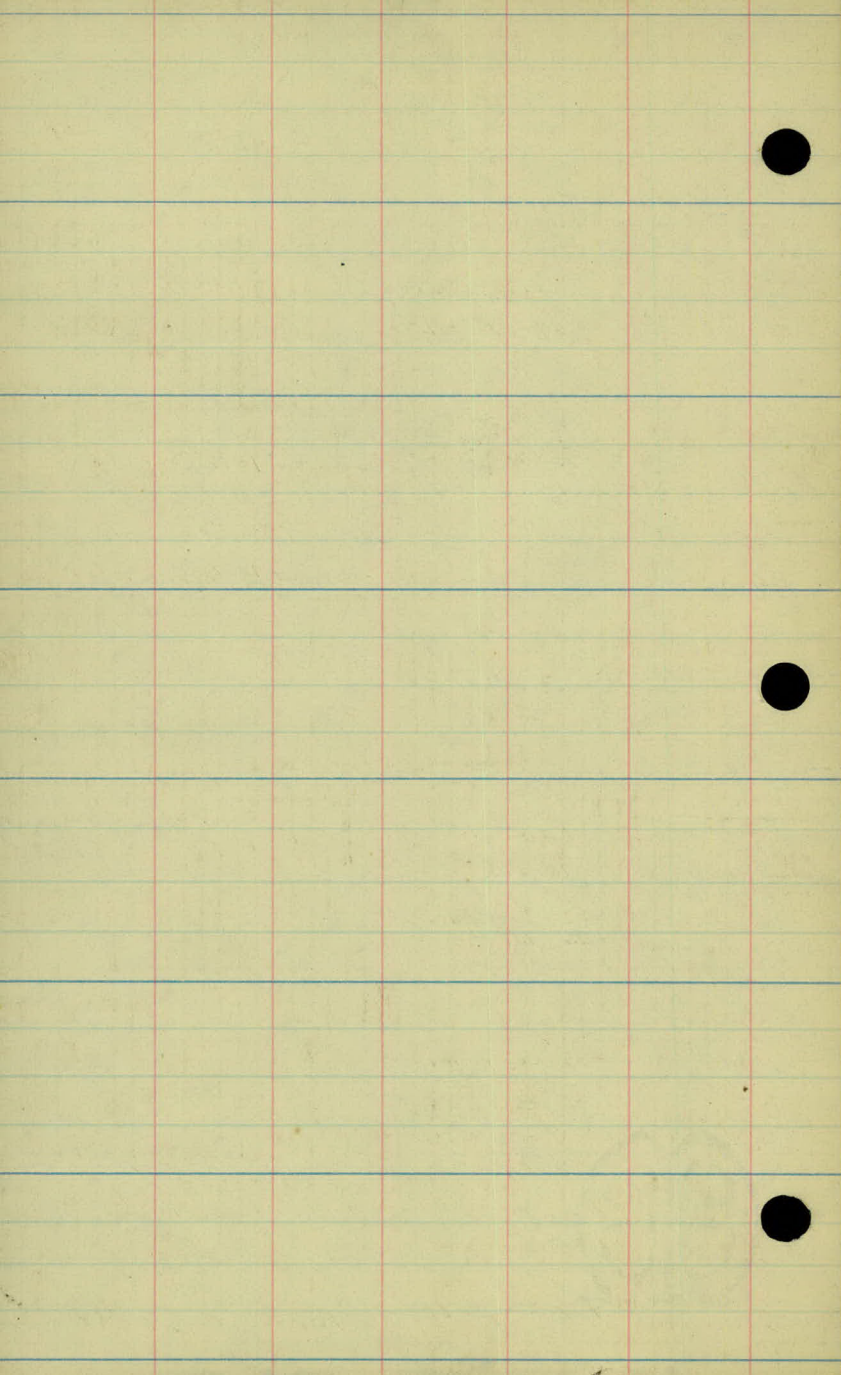
+12 = P.P. 21' Lt.

+09 } DBL Garage Ent

+99 }

+19 = T.P. 20' Lt.

+08 = 15' Oak 28' Rt.



X Weber
Beaton
Bell

X Section For
Spring St

Rose Twp.
9-19-1929

Sta + H.I. ✓ - Elev.
 3.16 322.64 319.48

0+00 311 17.9

+30 18.2

+50 17.8

1 17.8

+50 18.0

2 18.0

+50 17.9

3 Top Shoulder 17.8

+10 Toe " 17.9

+27 ± Malv. St 18.7

+43 Toe of Shoulder 18.4

+45 Top " " 18.4

4 20.4 ✓

T.P. 8.45 331.08 0.01 322.63 ✓

+50 23.2

✓ 25.1

+50 25.6

6+00 26.1

~~+21~~ ~~25.4~~

+25 25.4

+50.27 ± Eustis 24.9

~~+68~~ Toe of Slope on Lt only ~~25.7~~

~~+76~~ " " " " Rt " ~~26.0~~

+81 26.2

7 27.7 ✓

11.38 338.91 3.55 327.53 ✓

Lt E Rt.

Spike in 12" Oak 15' Lt Sta 0+00

	4.3	4.5	4.6	4.7	5.0	5.3	5.9	6.2	
	35	30	15		26	30	33	35	
3.7	4.0	3.9	4.7	4.9	4.4	5.0	5.9	6.0	6.1
35	30	25	20	8		4	18	30	35
2.0	3.6	3.6	4.7	4.4	4.8	5.1	5.9	6.3	6.3
	30	23	14	8		8	17	30	35
	35	37	4.0	5.0	4.8	5.0	5.6	6.0	6.0
	35	30	19	13		10	15	30	35
	3.7	4.0	4.6	4.6	4.3	5.2	5.2	4.8	4.8
	35	30	16		6	15	19	30	35
5.5	5.5	5.6	4.7	4.6	4.4	5.0	4.6	4.4	2.9
34	30	13	10		4	10	16	20	2.8
4.0	5.3	5.7	5.0	4.5	4.7	6.1	5.0	4.7	2.7
	30	11	9	4		2	4	11	15
									2.7
									1.7
									1.0
									4.0
4.0	5.2	5.3	5.7	5.0	4.8	4.7	5.7	5.7	4.9
	30	17	14	8		3	5	7	8
									11
									13
									19
									27
	5.1	5.0	5.0	4.7	5.0	4.3	4.1	3.9	
	35	30	10		10	24	30	37	
	4.6	4.2	3.9	3.5			2.7		
	30	23		15			5.0		
	5.0	4.8	4.5	4.2	4.1	3.5	3.5		
	35	30	18		17	30	35		
4.0	4.4	4.0	4.6	4.2	4.1	3.1	2.0		
	30	21	18		19	30	35		
4.6	2.1	1.3	2.0	2.4	2.2	1.9	1.7	0.5	0.0
33	30	21	6	4		8	15	19	30
									35

Ch. Coop 7.2 6.7 6.4 7.8 7.9 7.6 7.3 7.3 L.O.

Lo 4.0 4.5 6.3 6.6 5.9 6.0 6.7 6.6 6.1 School yard

35 35 3.8 5.6 5.5 5.6 6.3 6.1 5.8

35 30 13 10 10 12 14 30 35

Gro. Store

36 36 4.0 4.8 5.0 6.3 6.2 6.2 S.W. in front of Gro. Store

35 30 15 15 15 14 26 30 30

6.1 6.1 5.9 5.7 6.0 6.5 Same Slope

35 30 12 12 15 30 5.0

6.8 6.6 6.1 5.4

35 30 17 9 5.0 4.9 5.9 4.7 3.5 L.O.

4.7 4.7 5.7 3.7 3.4 4.4 2.9 2.5 L.O.

35 30 19 15 17 19 30

71.1=338.91
 4.0 6.6 6.6 7.8 5.6 5.8 5.0 4.9 5.9 4.7 3.5 L.O.
 35 30 22 17 9 5.0 4.9 5.9 4.7 3.5 L.O.
 4.0 4.7 4.7 5.7 3.7 3.4 4.4 2.9 2.5 L.O.
 35 30 19 15 17 19 30

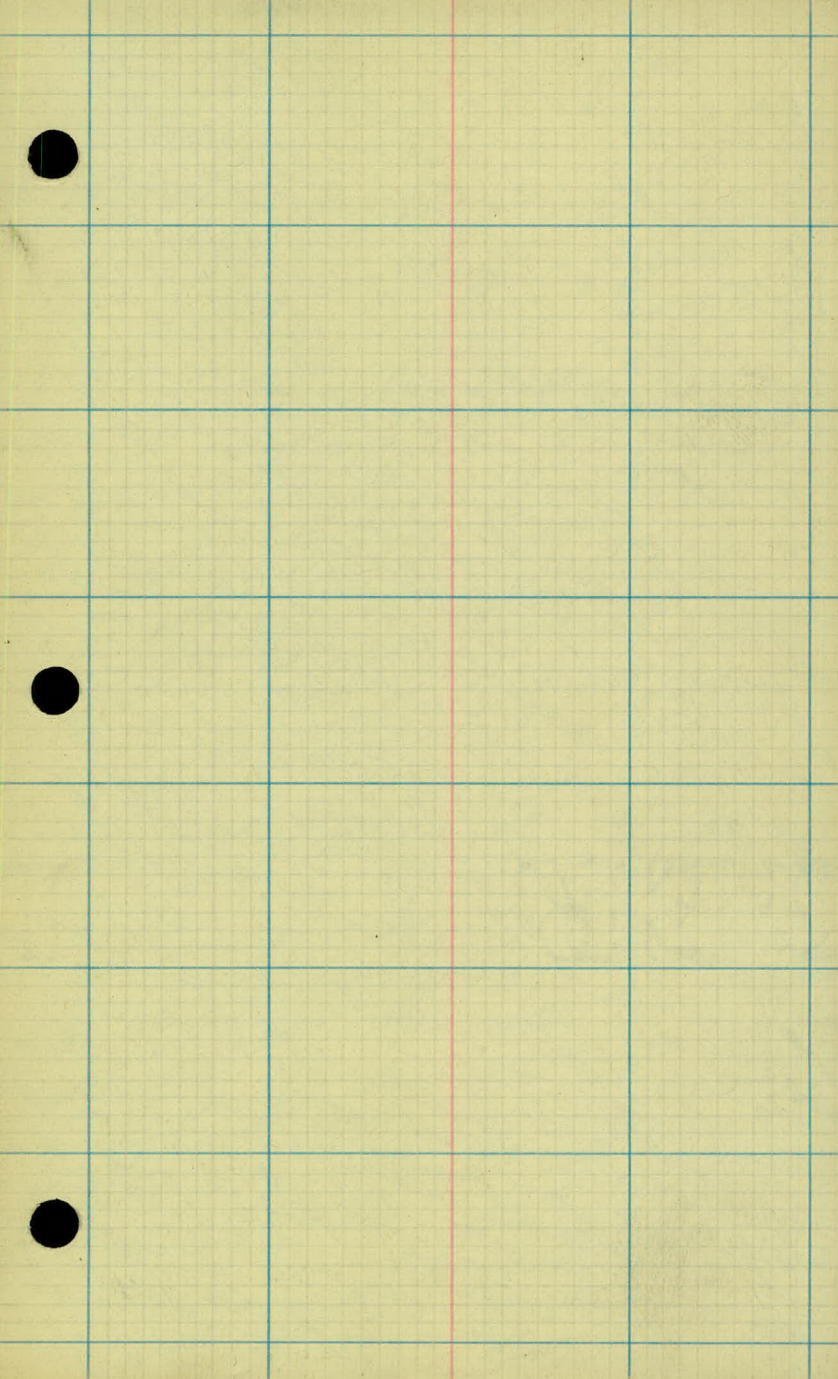
(2.7)
 (11.2)

Spike in 12 Oct

Lt

4

Pt.



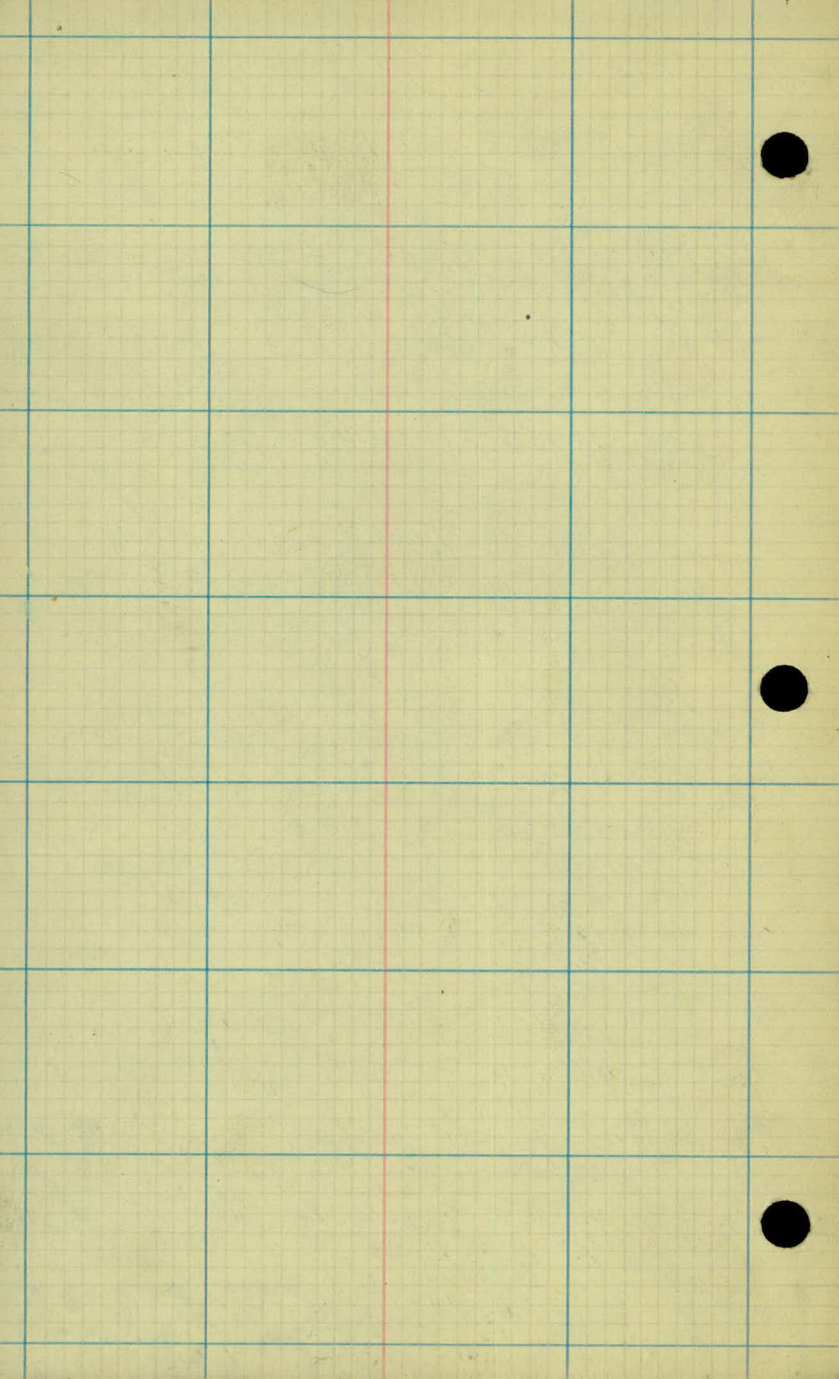
Sta.	+	H.I.	-	Elev.
7.50				29.56
+25		338.91		29.5
+50				30.6
8				31.6
+27				32.9
+50				32.3
+68				32.0
9				29.4
T.P.	158	329.20	11.29	327.62
+50				25.6
+64				Ditch on Rt Top of Slope on Lt 24.4
+79				Toe of Slope Lt Top Shoulder on Rt 23.8
+89				Carl St 24.1
+97				Top of Shoulder 23.3
10+02				Toe of Slope on Rt + Top of Slope Lt 22.7
50				20.6
11				20.8
+50				23.9
+71				24.5
12				23.6
+50				22.1
13				25.7
+030				Top of Slope on Rt only 25.5
+081				Toe of Slope Rt + Top of Slope Lt 24.5
+13				" " Lt 24.0
+31				Pleasant 25.1
				3.71 325.49

14 E 77.

1.8	1.8	2.3	2.8	9.0	9.4	9.3	9.6	9.6	
35	30	24	18	15		10	30	35	
1.0	1.4	1.4	1.7	4.6	5.0	8.2	8.3	8.1	7.8
35	30	25	32	18	15	10	26	30	35
4.2	4.2	4.3	6.5	6.5	7.5	7.3	6.5	6.2	
35	30	26	25	22	17		30	35	
			5.0	5.1	5.8	6.0	7.0	7.3	
			35	30	16		18	30	35
L.O.			4.7	5.3	6.3	6.6	7.2	7.7	11.0
			28	20	18		17	27	30
4.0	4.0	5.1	6.4	6.6	6.9	7.7	8.9	11.0	11.0
35	30	20	15	8		13	26	30	35
3.7	4.0	4.8	6.6	9.1	9.5	9.4	8.2	8.9	11.8
35	30	20	16	8		9	17	23	27

7.15	7.12	0.6	2.9	3.6	3.7	3.5	4.5	3.7	3.7
35	29	18	14		19	26	30	35	40
0.2	0.6	1.0	4.0	4.8	5.7	7.1	7.1	7.6	
35	20	28	15		18	19	30	35	
	4.6	4.8	5.2	5.4	5.8	5.9	5.9	5.9	L.O.
	35	30	18		17	30	35		
	4.0	4.6	5.1	5.6	5.6	5.6			
	35	25		25	30				
4.9	5.0	5.5	5.7	6.3	5.8	6.1	6.1		
35	30	18		10	15	30	35		
4.2	4.2	5.0	6.0	6.5	6.5	7.6	8.2	7.9	7.8
35	30	16	15		7	13	27	30	35
L.O.	5.4	6.6	8.2	8.6	8.8	8.1	5.9	5.9	L.O. House
	33	30	19		11	20	26	30	
L.O.	6.0	6.6	7.9	8.4	8.5	7.7	6.3	5.8	L.O.
	35	32	29		12	18	24	30	
5.8	5.9	6.0	6.2	5.3	5.1	4.7	= Garage Floor.		
35	30	31	16		16	32			
	4.6	5.6	6.0	4.7	3.6	3.4	L.O.		
	35	30	13		10	30			
4.7	4.7	5.9	6.3	5.6	4.6	3.9	3.0	3.0	L.O.
35	31	16	7		14	22	24	30	
7.5	7.8	7.3	6.1	7.1	7.3	6.0	2.6	L.O. House	
35	30	20	7		13	24	32		
4.2	5.3	5.5	5.4	5.6	3.5	2.7	2.3	3.0	2.4
30	30	27	21	4		2	18	22	30
					3.7	2.6	2.3	3.0	2.6
						2	18	31	30
4.5	4.5	4.2	4.1	4.7	4.8	4.7			
35	30	20	21		15	35			
5.3	5.3	5.2	4.7	5.2					
35	30	23	14						
4.9	4.4	4.1	3.9	3.7					
			25	30					

Spike in 36° C.W. 20° E of End of Proj.



SPRING ST.

9/24/29

O.R.V.K.
W.S.M.

✓ 1+53 - L^t - P-12"X20' C.M. ✓

✓ 1+76 - L^t - " " ✓

✓ 2+40 - R^t - Rem. & rep. ✓

✓ 1+00 to 2+00 - Cl. & Gr. 2 T.

3+45 - L^t - Rep. 12"X14' from 3+06 ✓

3+06 - Remove - P-12"X36' C.M.

3+43 - P-12"X36' C.M.

4+89 - L^t - Rem. & rep. 12 yds. (Exc. for drive. ✓)

5+03 - L^t - P-12"X20' C.M. 15 yds.

4+90 - R^t - P-12"X20' C.M. 12 yds.

6+35 and 6+64 - O.K. ✓

✓ 4+00 to 5+00 - Cl. & Gr. 2 T. ✓

7+99¹⁰ - R^t - 8+09¹⁰ - R^t - 8+23¹⁰ - L^t. No culv. req.

11+50 R^t - P-12"X20'

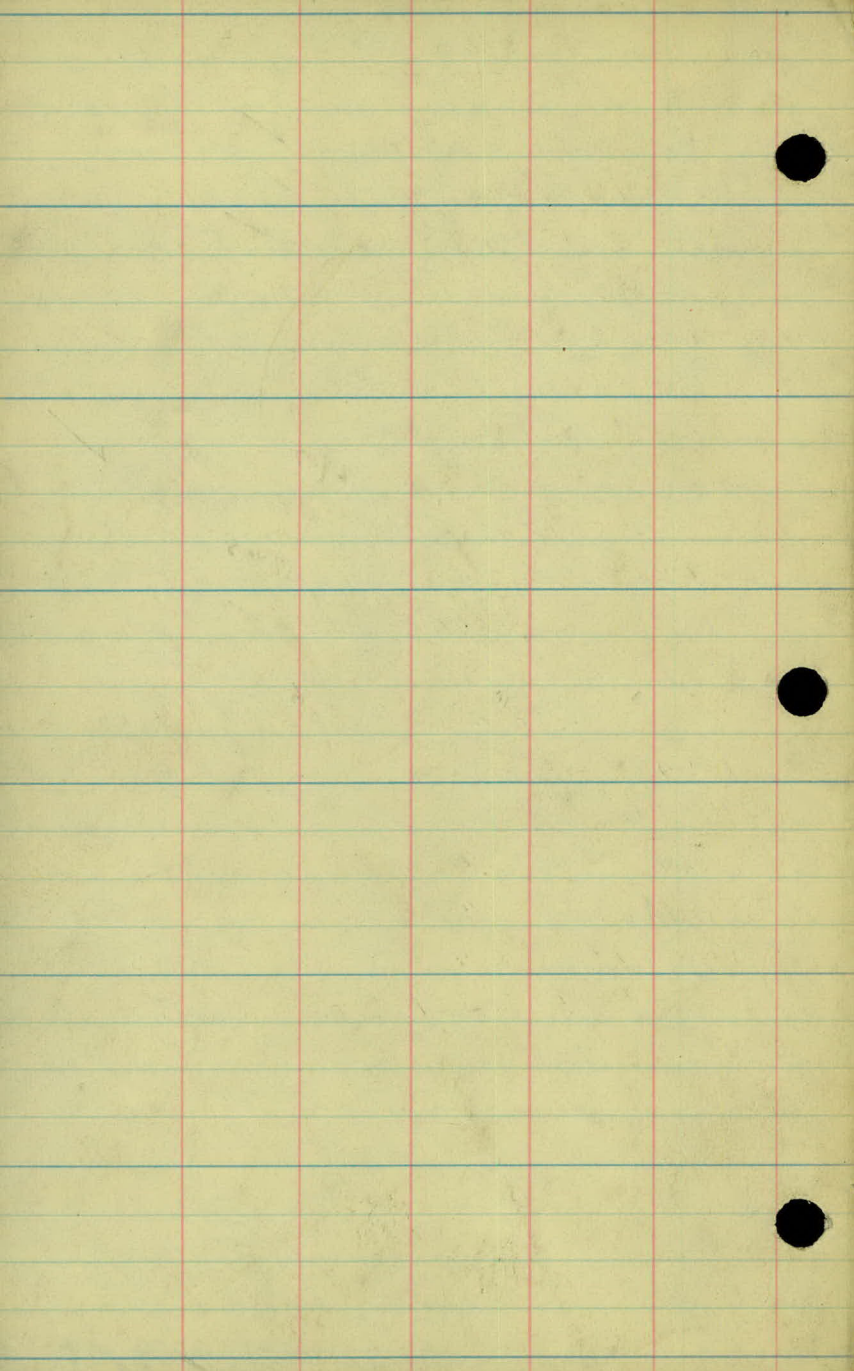
11+64 " "

11+79 " "

11+93 L^t "

11+64 L^t "

✓ 11+00 to 13+00 - Cl. 2 T. Gr. 3 T.



29-R1

#1 = 13 +

'H.

0.0 To 1.0 = Comp. yellow Clay.
1.0 To 7.0' = Sand & " "
7' = Hard Pan

#2

#3

0.0 To 3' = Sand & yellow Clay.
3 To 3.5 = Hard Pan

#4

0.0 To 1.0' yellow Clay.
1 To 3.5 Black Loam
3.5 " 17 yellow Clay & Sand.
17 " 19 Sand & Gravel.
19 " 23? Black Gumbo.

#5

0.0 To 7' Gr. & Sand.
7 To 11' Fine sand.
11 " 12 Clay very little sand
12 To 13.6 + Sand & Gravel.

St. 1/2

#1
#2
#3

Spring

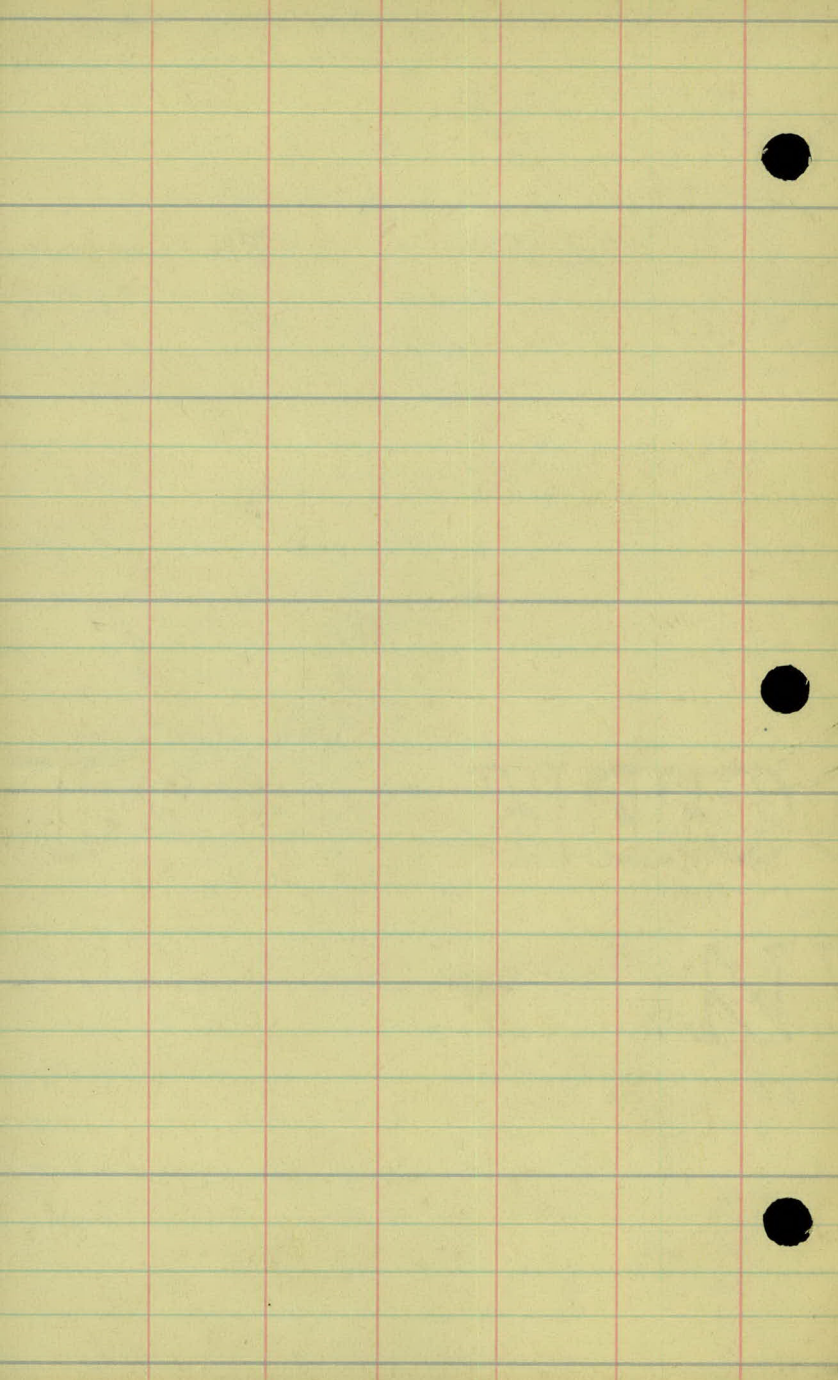
St.

#4

Cesspools
24' Deep

Alley

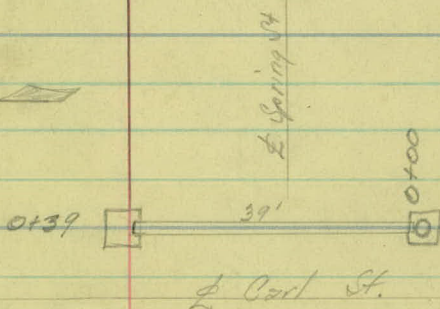
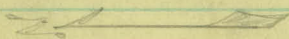
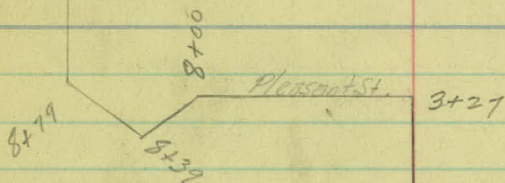
Carl

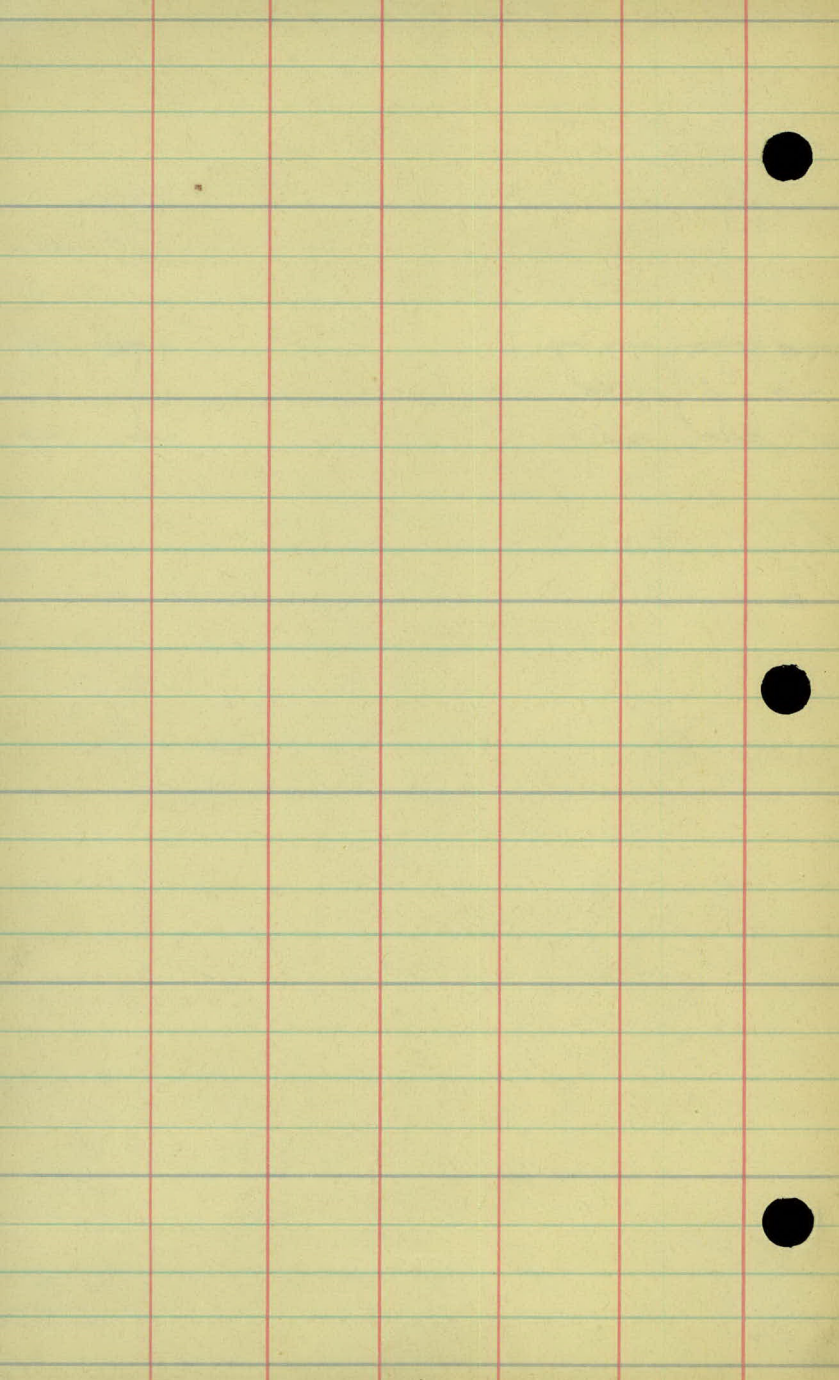


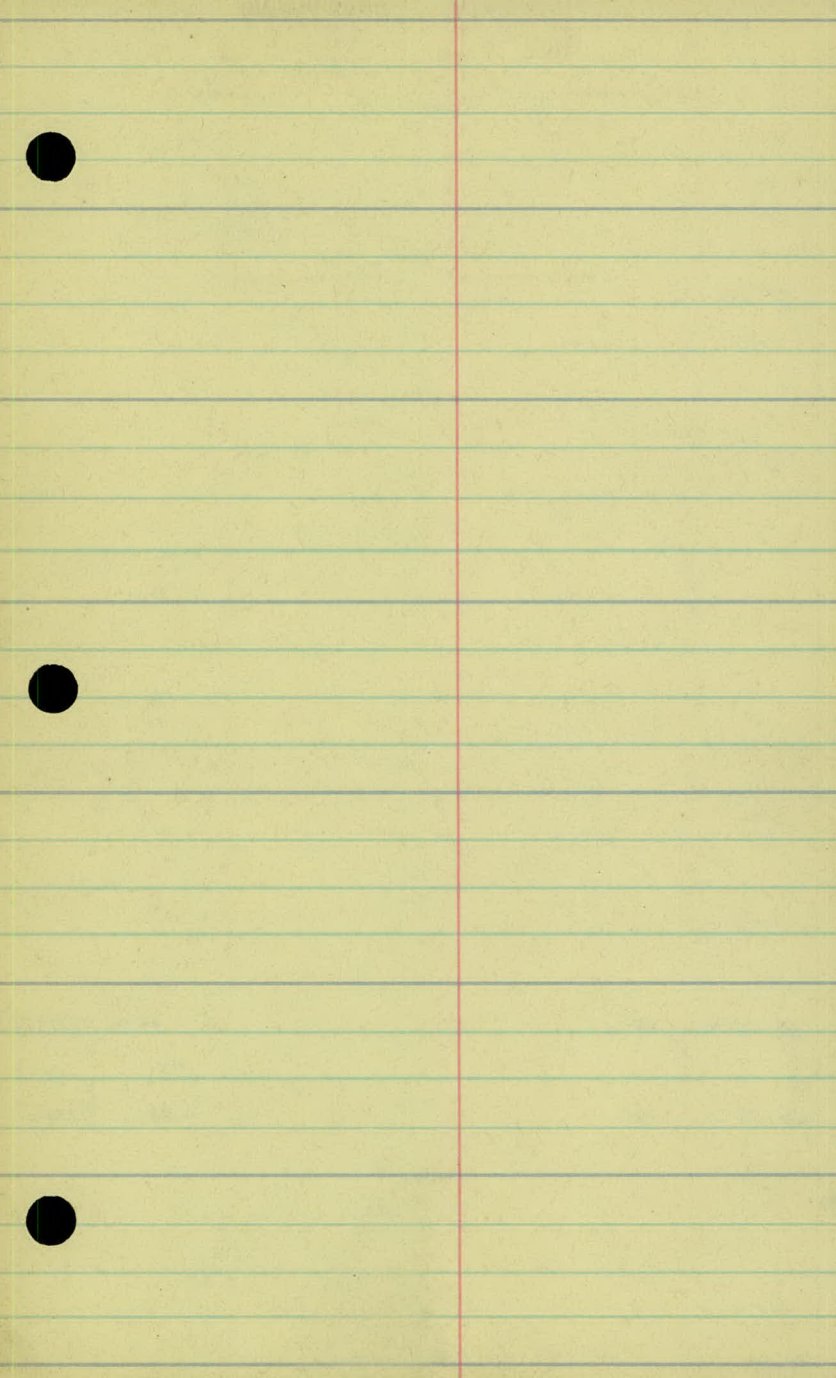
11+80

29-R1

North Side Summer







	+	H.I.	-	Red.	Elev
B.M.	3.52	103.52			100.00 Assumed
0+00				10.3	93.20
+15				5.6	97.90
+38				6.6	96.90
+50				6.4	97.10
1+00				6.2	97.30
+04.0				6.22	97.30
+24				6.18	97.34
+50				6.3	97.20
+62				6.35	97.20
+82				5.95	97.55
+98				6.15	97.35
2+18				5.95	97.55
+50				5.7	97.8
3				5.4	98.1
+27				4.1	99.4
T.P.	2.02	102.02	3.52		100.00
+50				4.0	98.0
4				5.5	96.5
+50				6.8	95.2
+53				7.1	94.9
+73				7.7	94.3
5				8.3	93.7
+50				9.9	92.1
+65				10.55	91.47
+85				11.85	90.17
6				12.4	90.6

= So. End X Drain
E Spring St.
Gutter No. side of Spring St.

{ Side Drain 12" x 20' C.M. }
{ " " " " }

{ Side Drain 12" x 20' C.M. }
{ Side Drain 12" x 20' C.M. }

△ Pt. at Pleasant Ave. (N.W. Cor.)

{ Side Drain 12" x 20' C.M. }

{ Side Drain 12" x 20' C.M. }

		10202		Pod.	Elev.
T.P.	210	92.31	11.81		90.21
6+50				4.0	88.3
+55				4.4	87.9
+75				4.85	87.46
7				5.3	87.0
+37				5.9	86.4
+51				6.2	86.1
8				6.7	85.6
+39				7.5	84.8
+79				8.9	83.4
				8.5	83.8
				8.45	83.86
9				8.5	83.8
+50				8.8	83.5
10				9.6	82.7
+41				11.15	81.16
+59				11.55	80.76
T.P.	1.94	83.75	10.50		81.81
11				4.4	79.35
+80				7.6	76.15
B.M.			1.94		81.81

{ 12" x 20' CM. } side Dr.

12" x 14' CM. } side Dr.

W. end of Proposed X Drain

E. " " " " "

{ W. end of present X Dr. in place }
 { E. " " " " " 15" x 40' CM. }

{ 12" x 18' CM. } side Dr.

End of Proj

East end of side Drain Sta. 10+59

