

Book 14 Dr. 11

X

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

ELMER ST.

From McCarron's B.N. To Rice St.

Road Acc't. No.

Date Filed 3-13-34 File

34-R 28

Dec-1933

{ Don Weber
Dave Skooglund
Jim Bell
Dave Stearns

Transit Notes
and
X Sections
Elmer St.

34-R2B

18.15^m

$$26 + 17.45 = \text{Term Allow.}$$

$$22 + 71.0 \text{ P.O.T}$$

78

$$12 + 15.53 \text{ P.O.T}$$

55

$$14 + 41.45 \text{ P.O.T}$$

$$0 + 00$$

Co. 100

1473.0

L. Rice

29.60
Hole. 10

S. F.

N. E. Cor Sec 13-29-23

23.85

P. F.

Base
Fr. 40

61.25

62.92

Base Brn
3000

6" Am 10

43.30

44.58

26" 0

12" Elm.

76.15

31.15

14" GE.

320.7

88'

R. L. v. 100.0

427.3

27'

R. L. 19158.27

166.7017

18" 0

27.90

67.65

20" 0

B.M.	0.13	895.37 ✓		895.24 ✓
T.P.	1.87	885.54 ✓	11.70	883.67 ✓
B.M.			7.90	877.64 ✓
0+00				74.5

+33				77.5
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+46				78.5
-----	--	--	--	------

1 +00		✓ 5'		✓ 82.4
T.P.	11.94	895.61 ✓	1.87	883.67 ✓
+50				85.7

2				89.2
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+50		✓		✓ 92.8
B.M.	10.07	905.31 ✓	0.37	895.24 ✓

3				95.7
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+50				00.5
-----	--	--	--	------

4		✓		✓ 03.2
T.P.	13.43	916.57 ✓	2.17	903.14 ✓

3 +50				00.5
-------	--	--	--	------

4				03.2
---	--	--	--	------

12-19-33

Clear & cool

30°F

Lt.

L

Rt

spt in P.P. 11' Lt 2+45 = B.M. N.M. Parsons

21+54 - 41' Lt.

spt in 20" 0 35' Lt 0-02

9.2	10.4	13.0	11.7	11.4	12.1	12.7	12.1	12.4
35	17	14	10	11.0	11	17	20	23
76.3	75.1	72.5	73.8	74.1	73.4	72.7	73.4	73.1

7.8	8.2	9.7	8.4	8.4	9.2	9.7	9.0	8.2
35	16	14	11	9	17	20	21	35
77.7	77.3	75.8	77.1	77.1	76.3	75.8	76.5	77.3

3.8	5.0	6.6	8.8	7.8	8.2	8.8	7.8	6.5
35	23	17	14	11	16	20	21	35
81.7	80.5	78.9	76.7	77.7	77.3	76.7	77.7	79.0

2.0	2.0	3.2	3.8	3.1	4.4	3.5	2.2	2.2
35	24	12	10	9	22	23	31	35
83.2	83.5	82.3	81.7	82.4	81.1	81.0	83.3	83.3

10.1	9.8	10.6	10.0	10.7	9.7	10.8	9.4	7.3	7.5
35	27	28	18	10	10	23	25	33	50
85.5	85.8	85.0	85.6	84.9	85.9	84.8	86.2	88.3	88.1

5.8	4.4	4.7	7.3	6.4	7.2	3.6	3.6	2.2	2.4
35	26	13	9	10	22	26	29	33	35
89.8	91.2	90.9	86.3	89.2	88.4	92.0	92.0	93.4	93.8

over 41.

10	11.6	10.6	4.0.6	1.1	1.4	3.1	2.8	4.1	1.5	0.5	0.8
35	25	22	16	12	8	6	15	24	27	32	35
95.6	97.2	96.2	96.2	94.5	94.2	92.5	92.8	91.5	94.1	95.1	94.8

1.6	1.5	3.3	7.4	9.0	9.1	9.8	9.0	9.2	10.0	7.0	6.3
35	26	17	9	9	6	4	8	18	26	30	35
03.7	03.8	02.0	97.9	96.3	96.2	95.5	96.3	96.1	95.3	98.3	99.0

3.0	4.3	5.5	4.8	5.4	6.1
10	5	3	10	19	35
2.3	1.0	99.8	00.5	99.9	99.2

0.0	2.0	3.3	4.0	3.6	4.0	0.0
2.2	10	17	22	25	32	43
05.3	03.3	02.0	01.3	1.7	01.3	05.3

6.5	7.8
35	25
10.7	8.8

16.1

0.8	1.8	10.0
35	30	26
15.8	14.8	06.6

17.4

Sta. + H.I. ✓ - Elev.
916.57

4+50 04.8

5
T.P. 7.29 915.22 ✓ 8.64 ✓ 907.93 06.6
+50 08.2

6 09.2

+50 09.7

7 10.3

+50 12.1

8 12.0

+50
T.P. 7.39 919.92 ✓ 2.69 ✓ 912.53 11.6

9 12.3

+50 11.3

10 10.2

+50 09.6

Lt.

F

Rt

<u>1.2</u>	<u>5.0</u>	<u>6.0</u>	<u>10.4</u>	<u>12.0</u>	
35	26	18	14	10	11.8
15.4	11.6	10.6	06.2	04.6	

<u>12.2</u>	<u>7.5</u>	<u>7.2</u>
21	27	35
4.4	9.1	9.4

<u>5.0</u>	<u>7.0</u>	<u>9.0</u>	
35	21	14	100
11.1	9.6	7.6	

<u>9.8</u>	<u>11.0</u>	<u>11.0</u>	<u>9.0</u>	<u>8.6</u>
10	12	15	18	35
6.8	5.6	5.6	7.6	8.0

<u>4.2</u>	<u>5.1</u>	<u>6.0</u>	<u>7.7</u>	<u>8.0</u>	<u>7.0</u>	
35	32	22	21	18	15	7.0
11.0	10.1	9.2	7.5	7.2	8.2	

<u>6.8</u>	<u>7.5</u>	<u>8.5</u>	<u>8.6</u>	<u>7.0</u>	<u>8.2</u>
3	8	9	12	14	35
8.4	7.7	6.7	6.6	8.2	7.0

<u>4.5</u>	<u>6.0</u>	<u>7.0</u>	<u>6.2</u>	<u>5.8</u>	
35	22	20	13	6	60
10.7	9.2	8.2	9.0	9.4	

<u>7.5</u>	<u>7.7</u>	<u>6.4</u>	<u>8.5</u>	<u>10.8</u>
6	9	10	18	35
7.7	7.5	8.8	6.7	4.4

<u>6.3</u>	<u>5.8</u>	<u>6.8</u>	<u>5.5</u>	<u>5.8</u>	
35	26	19	13	8	55
8.9	9.4	8.4	9.7	9.9	

<u>5.8</u>	<u>7.3</u>	<u>7.3</u>	<u>6.0</u>	<u>7.8</u>	<u>9.5</u>
2	6	9	12	17	35
9.4	7.9	7.9	9.2	7.4	5.7

<u>5.7</u>	<u>5.5</u>	<u>6.3</u>	<u>5.0</u>	
35	25	21	17	49
09.5	09.7	08.9	10.2	

<u>6.9</u>	<u>6.1</u>	<u>7.5</u>
12	17	35
08.3	09.1	07.7

<u>3.8</u>	<u>3.8</u>	<u>4.8</u>	<u>4.8</u>	<u>3.3</u>	<u>3.5</u>	
35	27	25	20	12	3	31
11.4	11.4	10.4	10.4	11.9	11.7	

<u>5.0</u>	<u>2.5</u>	<u>5.0</u>
12	18	35
10.2	12.7	10.2

<u>2.2</u>	<u>3.2</u>	<u>4.2</u>	<u>4.2</u>	<u>3.2</u>	
35	26	25	20	12	32
13.0	12.0	11.0	11.0	12.0	

<u>5.0</u>	<u>3.0</u>	<u>4.4</u>
12	18	35
10.2	12.2	10.8

<u>1.7</u>	<u>2.8</u>	<u>3.8</u>	<u>3.2</u>	
35	24	21	12	36
13.5	12.4	11.4	12.0	

<u>3.1</u>	<u>5.0</u>	<u>3.3</u>	<u>5.3</u>
1	14	17	35
12.1	10.2	11.9	9.9

<u>6.2</u>	<u>7.1</u>	<u>8.4</u>	<u>7.4</u>	
25	35	21	11	7.6
13.7	12.8	11.5	12.5	

<u>7.7</u>	<u>9.3</u>	<u>7.6</u>	<u>8.7</u>	<u>9.7</u>
5	14	18	23	35
12.2	10.6	12.3	11.2	10.2

<u>5.7</u>	<u>7.2</u>	<u>8.4</u>	<u>7.7</u>	<u>7.5</u>	
35	25	21	17	9	8.6
14.2	12.7	11.5	12.2	12.4	

<u>8.1</u>	<u>10.2</u>	<u>8.4</u>	<u>9.5</u>	<u>10.5</u>
3	13	17	23	35
11.8	09.7	11.5	10.4	09.4

<u>7.0</u>	<u>10.0</u>	<u>9.7</u>	<u>9.3</u>	
35	21	17	8	9.7
12.9	9.9	10.2	10.0	

<u>9.5</u>	<u>10.0</u>	<u>11.0</u>	<u>9.3</u>	<u>10.3</u>	<u>10.7</u>
2	17	14	18	24	35
10.4	9.9	8.9	10.6	9.6	9.0

<u>6.8</u>	<u>7.0</u>	<u>10.0</u>	<u>10.0</u>	
35	33	21	9	10.3

<u>10.0</u>	<u>10.5</u>	<u>12.1</u>	<u>10.6</u>	<u>11.6</u>	<u>12.4</u>
2	7	14	18	24	35

Sta. + H.I. ✓ - Elev
919.92

11 10.0

+50 ✓ 11.8

B.M. 4.87 915.05 915.06

12 14.0

+21 14.5

+68 12.8

13 11.1

+40 08.6

+70 06.8

14 ✓ 04.8

T.P. 4.20 910.49 13.63 906.29

14 04.8

+50 ✓ 01.2

T.P. 5.78 903.81 12.46 898.03

14+50 01.2

15 97.3

LEFT Δ RIGHT

$\frac{64}{35}$ $\frac{61}{33}$ $\frac{88}{28}$ $\frac{100}{11}$ $\frac{97}{9}$ 9.9 $\frac{96}{2}$ $\frac{105}{9}$ $\frac{120}{15}$ $\frac{108}{18}$ $\frac{131}{35}$

$\frac{44}{35}$ $\frac{68}{22}$ $\frac{81}{17}$ $\frac{74}{9}$ 8.1 $\frac{7.5}{4}$ $\frac{90}{15}$ $\frac{7.9}{19}$ $\frac{93}{24}$ $\frac{98}{35}$

Spk in App

$\frac{16}{35}$ $\frac{25}{26}$ $\frac{4.2}{23}$ $\frac{5.8}{17}$ $\frac{5.6}{10}$ 5.9 $\frac{5.4}{5}$ $\frac{6.5}{11}$ $\frac{6.5}{15}$ $\frac{3.8}{19}$ $\frac{4.6}{25}$ $\frac{5.0}{35}$

$\frac{0.5}{35}$ $\frac{24}{26}$ $\frac{48}{21}$ $\frac{57}{16}$ $\frac{5.3}{10}$ 5.4 $\frac{5.4}{5}$ $\frac{60}{15}$ $\frac{34}{19}$ $\frac{45}{24}$ $\frac{51}{35}$

$\frac{4.0}{35}$ $\frac{57}{29}$ $\frac{69}{10}$ 7.1 $\frac{7.6}{8}$ $\frac{86}{23}$ $\frac{86}{35}$

$\frac{33}{35}$ $\frac{8.1}{22}$ $\frac{76}{17}$ $\frac{86}{8}$ 8.8 $\frac{9.2}{7}$ $\frac{86}{8}$ $\frac{81}{14}$ $\frac{70}{19}$ $\frac{64}{35}$

$\frac{22}{45}$ $\frac{20}{39}$ $\frac{90}{28}$ $\frac{10.3}{14}$ $\frac{108}{12}$ 11.3 $\frac{11.6}{9}$ $\frac{131}{21}$ $\frac{11.6}{35}$

$\frac{2.2}{45}$ $\frac{22}{39}$ $\frac{47}{31}$ $\frac{12.8}{20}$ $\frac{12.3}{12}$ 13.1 $\frac{12.8}{8}$ $\frac{131}{18}$ $\frac{11.0}{20}$ $\frac{13.0}{35}$

$\frac{2.8}{40}$ $\frac{2.8}{38}$ $\frac{12.5}{24}$ (15.1)

$\frac{5.2}{13}$ 5.7 $\frac{5.7}{5}$ $\frac{5.2}{8}$ $\frac{6.7}{14}$ $\frac{11.0}{35}$

$\frac{0.0}{35}$ $\frac{14}{32}$ $\frac{81}{21}$ $\frac{92}{13}$ 9.3 $\frac{104}{6}$

(2.6)

$\frac{61}{13}$ $\frac{104}{35}$

$\frac{1.2}{35}$ $\frac{3.8}{25}$ $\frac{6.2}{22}$ $\frac{5.6}{15}$ $\frac{5.8}{4}$ 6.5 $\frac{8.8}{10}$ $\frac{12.2}{35}$

Sta + H.I. ✓ - Elev
903.81

+50 95.4

16 94.3

+50 94.1

17 94.1

+50 94.2

18 ✓ 95.2

T.R. 9.50 905.17 8.14 895.67

+50 96.5

19 97.2

+50 97.1

20 97.3

+50 98.5

21 ✓ 01.5

T.R. 12.10 915.45 1.82 903.35

+50 05.2

Severe cold wave on the way 12-19-33

LEFT ≠ RIGHT.

$$\frac{56}{35} \quad \frac{56}{30} \quad \frac{84}{23} \quad \frac{80}{19} \quad \frac{80}{4} \quad 84 \quad \frac{10.2}{10} \quad \frac{12.4}{35} \quad \frac{1}{1000}$$

$$\frac{66}{35} \quad \frac{70}{28} \quad \frac{95}{22} \quad \frac{90}{19} \quad 95 \quad \frac{11.4}{5} \quad \frac{12.6}{17} \quad \frac{12.6}{35} \quad \text{500000}$$

$$\frac{7.7}{35} \quad \frac{8.2}{29} \quad \frac{10.4}{23} \quad \frac{9.8}{13} \quad 9.7 \quad \frac{10.0}{3} \quad \frac{11.8}{7} \quad \frac{12.7}{20} \quad \frac{12.8}{35}$$

$$\frac{88}{35} \quad \frac{91}{29} \quad \frac{100}{26} \quad \frac{97}{13} \quad 9.7 \quad \frac{9.7}{2} \quad \frac{12.2}{7} \quad \frac{12.6}{20} \quad \frac{12.7}{35}$$

$$\frac{10.8}{35} \quad \frac{10.8}{26} \quad \frac{9.6}{11} \quad 9.6 \quad \frac{9.8}{2} \quad \frac{11.6}{6} \quad \frac{12.6}{22} \quad \frac{12.8}{35}$$

$$\frac{100}{35} \quad \frac{10.5}{22} \quad \frac{8.5}{10} \quad 8.6 \quad \frac{8.8}{5} \quad \frac{10.2}{10} \quad \frac{12.0}{28} \quad \frac{12.4}{35}$$

$$\frac{10.7}{35} \quad \frac{10.8}{18} \quad \frac{8.4}{10} \quad 8.7 \quad \frac{8.7}{8} \quad \frac{9.2}{11} \quad \frac{8.5}{13} \quad \frac{8.3}{20} \quad \frac{10.1}{35}$$

$$\frac{7.7}{35} \quad \frac{7.7}{27} \quad \frac{10.5}{22} \quad \frac{10.2}{16} \quad \frac{8.6}{12} \quad 8.0 \quad \frac{8.2}{10} \quad \frac{8.7}{15} \quad \frac{8.4}{18} \quad \frac{9.2}{35}$$

$$\frac{10.3}{35} \quad \frac{10.1}{28} \quad \frac{10.3}{16} \quad \frac{8.5}{8} \quad 8.1 \quad \frac{8.8}{15} \quad \frac{8.7}{30} \quad \frac{8.0}{35}$$

$$\frac{11.6}{35} \quad \frac{10.2}{12} \quad \frac{7.8}{6} \quad 7.9 \quad \frac{7.9}{9} \quad \frac{9.0}{13} \quad \frac{9.1}{25} \quad \frac{6.4}{35} \quad \frac{6.4}{40}$$

$$\frac{9.4}{35} \quad \frac{8.7}{11} \quad \frac{6.5}{6} \quad 6.7 \quad \frac{6.7}{10} \quad \frac{7.6}{14} \quad \frac{8.1}{29} \quad \frac{7.2}{35} \quad \frac{7.2}{40}$$

$$\frac{4.8}{35} \quad \frac{5.3}{28} \quad \frac{4.0}{9} \quad \frac{3.4}{7} \quad 3.7 \quad \frac{4.3}{21} \quad \frac{3.7}{26} \quad \frac{3.7}{33} \quad \frac{3.1}{35} \quad \frac{3.1}{40}$$

$$\frac{10.1}{35} \quad \frac{9.1}{27} \quad \frac{9.0}{17} \quad \frac{10.2}{8} \quad 10.3 \quad \frac{10.0}{8} \quad \frac{9.8}{20} \quad \frac{10.1}{33} \quad \frac{9.2}{35}$$

Sta + H.I. ✓ - Elev.

915.45

22 08.0

+50 10.8

+71.0 11.7

23 11.4

+30 10.3

+75 08.2

24 ✓ ✓ 07.4

T.P. 533910.43 10.35 905.10

+20 06.8

+60 05.4

25 03.9

+50 00.7

+81 ✓ ✓ 98.5

B.M. 461 903.25 11.83 898.60 898.64

+86 98.0

LEFT $\neq$ RIGHT

$$\frac{25}{35} \frac{25}{30} \frac{36}{23} \frac{78}{9} \frac{74}{6} 7.5 \frac{75}{21} \frac{47}{33} \frac{47}{40}$$

$$\frac{16}{35} \frac{24}{30} \frac{44}{13} 47 \frac{50}{5} \frac{48}{13} \frac{51}{22} \frac{36}{27} \frac{38}{35}$$

$$\frac{17}{35} \frac{25}{26} \frac{30}{9} 38 \frac{42}{4} \frac{44}{13} \frac{50}{19} \frac{40}{24} \frac{38}{35}$$

$$\frac{0.5}{35} \frac{18}{15} \frac{43}{6} 41 \frac{41}{10} \frac{46}{13} \frac{46}{19} \frac{37}{21} \frac{43}{35}$$

$$\frac{0.1}{35} \frac{10}{26} \frac{28}{13} \frac{51}{6} 5.2 \frac{52}{16} \frac{30}{18} \frac{25}{26} \frac{31}{35}$$

$$\frac{45}{35} \frac{46}{27} \frac{56}{18} \frac{68}{8} \frac{74}{7} 73 \frac{73}{11} \frac{80}{19} \frac{94}{28} \frac{93}{35}$$

$$\frac{10.0}{35} \frac{10.3}{21} \frac{91}{12} \frac{81}{4} 81 \frac{81}{10} \frac{86}{12} \frac{109}{17} \frac{11.8}{35}$$

$$\frac{6.5}{35} \frac{6.5}{27} \frac{57}{13} \frac{41}{9} 36 \frac{41}{9} \frac{62}{14} \frac{7.8}{35}$$

$$\frac{4.0}{35} \frac{5.7}{17} \frac{4.8}{13} 5.0 \frac{52}{5} \frac{46}{8} \frac{62}{15} \frac{6.8}{35}$$

$$\frac{6.4}{35} \frac{64}{31} \frac{53}{19} \frac{66}{13} 65 \frac{66}{5} \frac{6.0}{7} \frac{6.0}{12} \frac{41}{16} \frac{42}{22} \frac{35}{20}$$

$$\frac{74}{35} \frac{80}{28} \frac{88}{22} \frac{9.8}{19} 9.7 \frac{9.7}{2} \frac{9.0}{4} \frac{88}{11} \frac{45}{17} \frac{45}{32} \frac{1.8}{37}$$

$$\frac{9.3}{35} \frac{9.3}{30} \frac{11.6}{21} 11.9 \frac{11.5}{9} \frac{27}{25} \frac{30}{35}$$

3pk in G.P. Int Piece & Elmer St.

$$\frac{24}{35} \frac{26}{31} \frac{36}{27} \frac{48}{22} 53 \frac{53}{4} \frac{41}{8} \frac{20}{28} \frac{1.2}{35}$$

✓
903.25

25+95

£ Ditch

97.5

26

Top Shoulder

97.3

+174⁵
BM.

£ Rice St Pavement 97.20

461 898.64 ✓

(Finis 2:30 PM)

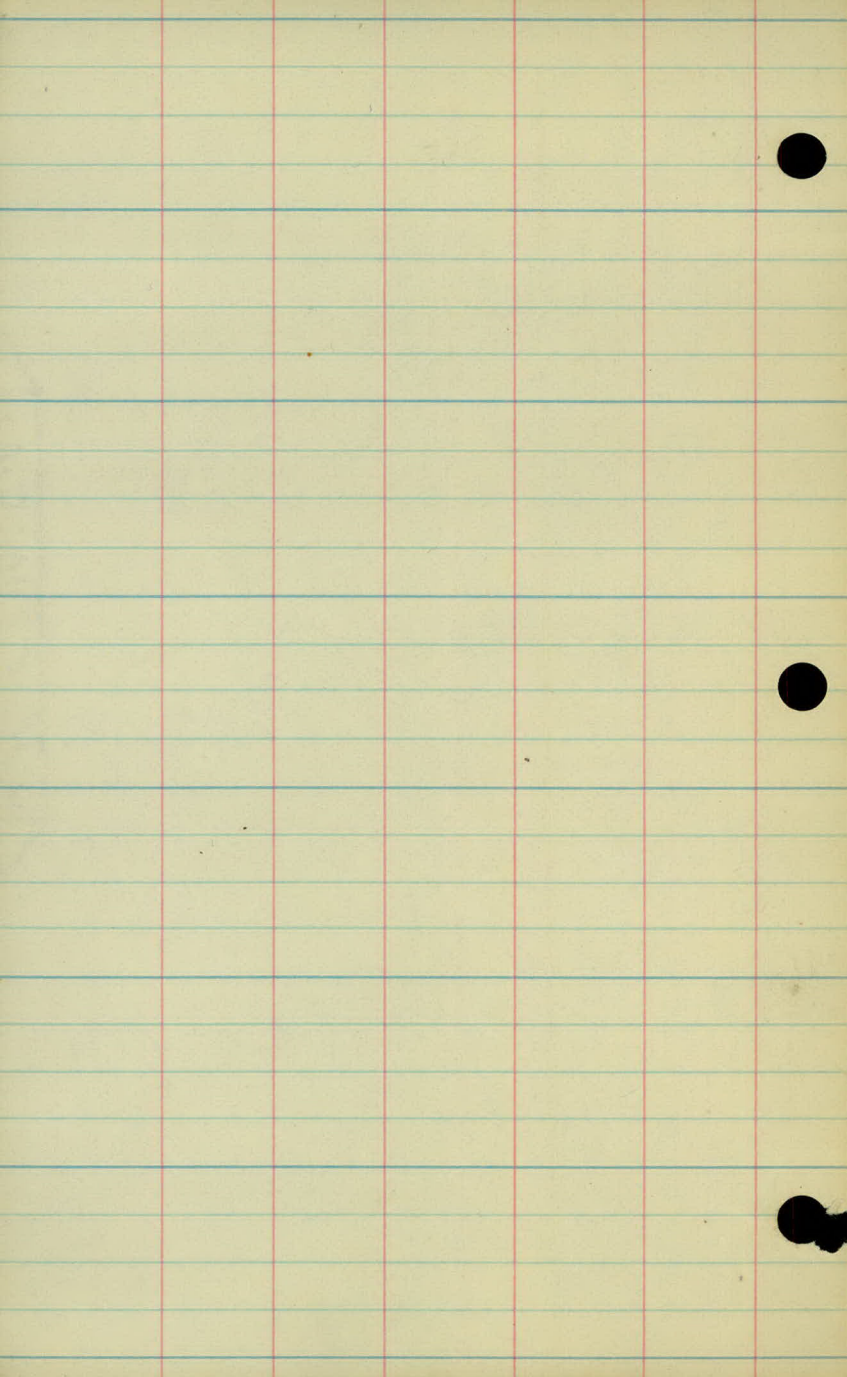
LEFT £ RIGHT

$\frac{5.8}{35}$ $\frac{6.1}{28}$ $\frac{5.6}{20}$ $\frac{4.8}{9}$ 58 $\frac{6.4}{9}$ $\frac{7.0}{25}$ $\frac{7.5}{35}$

$\frac{5.2}{35}$ $\frac{5.5}{18}$ $\frac{5.0}{9}$ 60 $\frac{6.4}{8}$ $\frac{6.1}{12}$ $\frac{6.7}{35}$

$\frac{4.85}{50}$ $\frac{5.4}{25}$ 60.5 $\frac{6.6}{25}$ $\frac{7.15}{50}$

Spk in G. P. Int. Rice St & Elmer St's.



Topog Notes
Elmer St.

5

4

3

2

1

0+00

+97-8-6" B.E. 30'

+72-3-6" B.E. 30'

+26-10" B.E. 31'

+06 Fld Ent

+87-20" B.E. 30'

+66-20" B.E. 28'

+44 Tw. 12" B.E. 28' +44 Beg F 28'

+39-8" B.E. 30'

OLD
Gravel
Pit

X+45

Light
clearing

+60 Guy P. 27'

X+60

{+38 Side Dr. Fld Ent}
12" x 20" Vit.

+11-3-6" O 17'

+96-6" O 18'

+77-10" O 17'

+45 P.P. 11'

+80-20" O 25'

+86 P.P. 12'

+21 Wester Ave
18" x 36" CM 8'

Cultivated

Cultivated



0 10 20 30 40 50 60 70 80 90 100

Yard

Garden
F 30'
F 29
F 28
Yard

+85 End lilacs 26'

+25 Beg. Row lilacs 22'

+21-4-4" O.H. 27'

+14-Pr. Dr. 14'

15" x 20" CM

+36-12" Maple 30'

+34 A.F. 38'

+34 P.P. 34'

+03-15" O 32'

+00-10" Tr. O 30'

+71-12" Linden 29'

+28-12" O 31'

+24-12" O 30'

+21-10" O 30'

+13-10" O 30'

+08-12" O 30'

+72-15" Tr. O 28'

+60-12" O 30'

+56-15" O 31'

+28-18" O 27'

+25 Rd Sq. 25'

+21-20" O 27'

+15-18" O 28'

+07-12" O 27'

+94-18" O 29'

+86-20" O 27'

+75-12" O 26'

+56-12" O 26'

+46-20" O 27'

+44-20" O 27'

+32-20" O 28'

+27 Beg. F 25'

+22 Side Dr. 12" x 20" CM 20'

+11-36" O 34'

11

10

9

8

7

6

+ 81-20" @ 28'

+ 51-10" Apple 32'

F29

+ 26-10" BE. 26'

+ 10 End Row Apple Trs 31'
F30

F30

F29

+ 42 Beg. Row 8" Apple Trs
15 Trees 30'

F30'

+ 45-6" @ 33'
+ 42-12" @ 32'
+ 32-12" @ 32'
+ 22-12" @ 30'
+ 18-8" @ 30'

F30'

Cultivated

+ 20 X

Yard
Barn 36'
18'

+ 95 End light
Clearing

+ 37 Beg. light
Clearing
+ 15 Cor. Barn 32'

Yard

17

16

15

14

13

12

+58 X Drain
10" X 14" 1/4"

+12 Fld Ent

F27



+45-12" Stump 4'

+27-12" Stump 8'

+12-15" Stump 4'

F27

Cult.

+17-15" Stump 4'

+83-15" Stump 22'

+75-15" Stump 20'
End F

+40-20" Stump 12'

F29

F19

+88-15" Ø 33'

+63-20" Ø 28'

+48-12" Ø 29'

+22-12" Ø 27'

F30'

F26'

+69-3-10" Ø 28'

F30'

+62 Fld Ent

+45-6" Apple 32'

+22-10" Apple 32'

Cult.

Cult

+69 Bag F23'

Wooded Area + Term. Swamp.

23

22

21

20

19

18

+93 F. Cor 25'

Swamp
X +75

+41 T.P. 21'

+60 Farm Ent

+72 R.P. 26'

+05 End F 35

Jard
X 05.

Cult

+53 Fld Ent

F30
Cult

+59 F. int 31'

X X X X

+38-3-6" Will 20'

+12-4-6" Wills 26'

F30

+92-6" Will 20'

+10/e

+57

Cult

F28

+41 Beg Cult.

+86 End Cult

Waste

+59-20" O 27'

F28

Cult

Swamp

+174⁵ End Proj.

26

25

24

Rice ST.

700 PP. 16'

+ 9.5 x Dr.
15" x 27 CM +

+64-3-15th 29

+ 45-15" Tw. @ 30'

+85 F Cor 28'
+79 End Row Trs 31

+ 79 End Row Trs 31

$$\frac{25}{25} \cdot \frac{1}{1}$$

+02 T.P. 20' F26

+53 BCG Row 9-8" B.E. 328

+27-6 "B.E. 31'

Cult

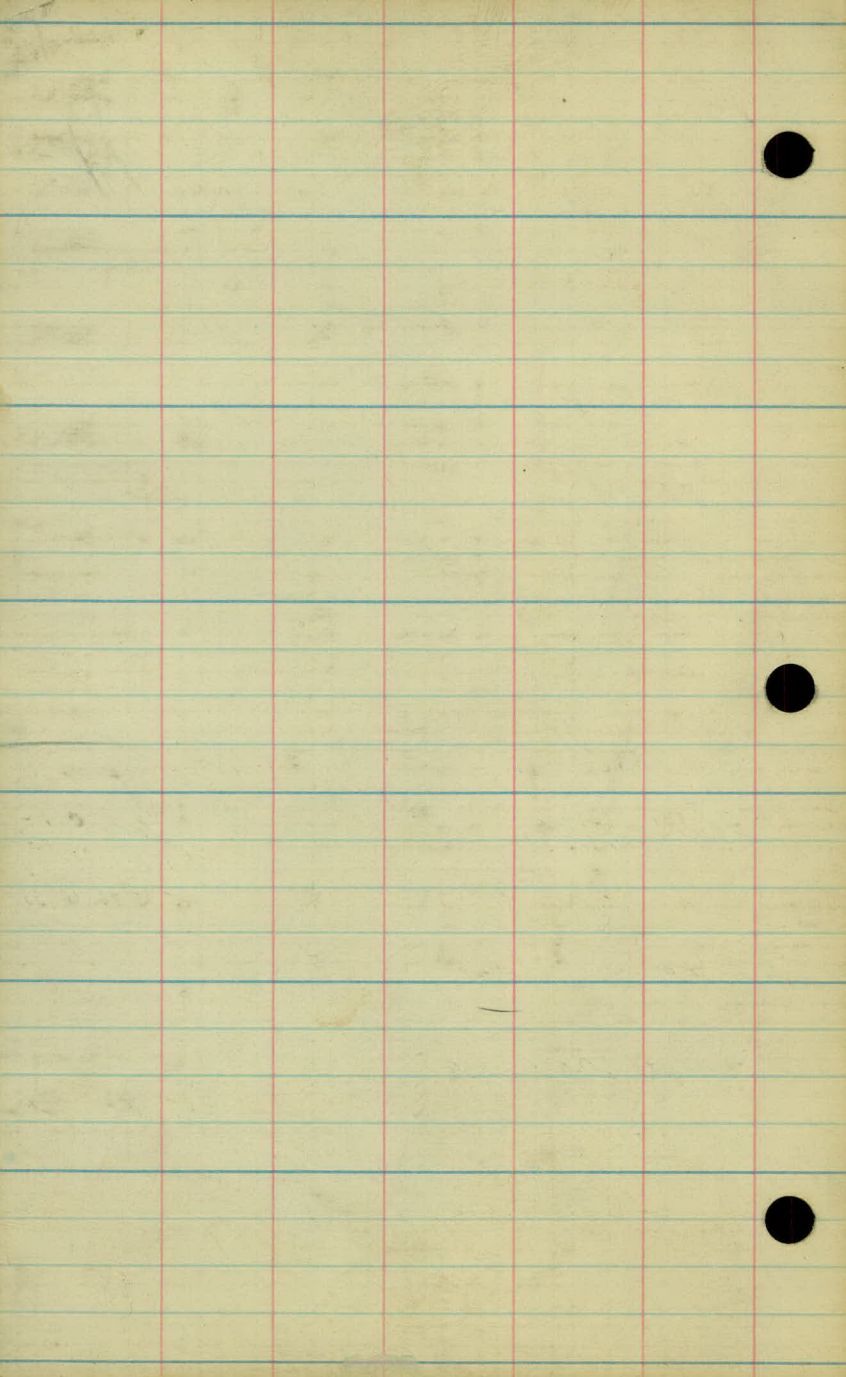
$\angle 70^\circ$

+37 P.P. 21

Y 125

Yard.

Swamp



Plans in Hand

3/29/34

ELMER ST.

Carley
Graham

0+21 Lt. Rem. + Replace ✓ X

0+22 Rt. Rem. + Replace ^{2.} X

1+50 to 2+00 (Clear +
Grub 1) 2.

3+38 Lt. Rem. + pl. ^{12x20} 15x20 C.M. X

2+50 to 3+50 Clear 5 Grub 8 ^{Note: Void}

5+06 Lt. Pl. ^{12x20} 15x20 C.M. X

5+14 ^{Rt.} Rem. + Rep. X

7+20 Rt. Pl. 15x20 CM X

10+50 Ch. Drainage X

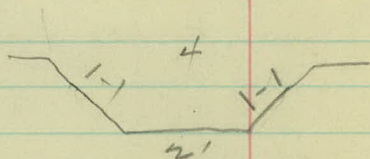
12+62 Rt. No cul. reqd.

12+62 Lt. Pl. 15x20 CM

17+50
~~16+50~~ Pl. 24" P3

17+12 Lt. No cul. reqd.

400
15 yd. ex.



ELMER ST. CONTD,

20+50 ck. Drainage

21+53 Lt. Pl. 15x20 CM

22+60 Lt. No cul. reqd.

25+95 Remove - No cul. reqd.

2+50 to 6+50

Clear 20

Grub 28

5+50 - 6+00 Clear & Grub 5

6+50 - 7 Clear & Grub 5

~~10+25 Lt. No cul. reqd.~~

11+50 - 12 Clear & Grub 1

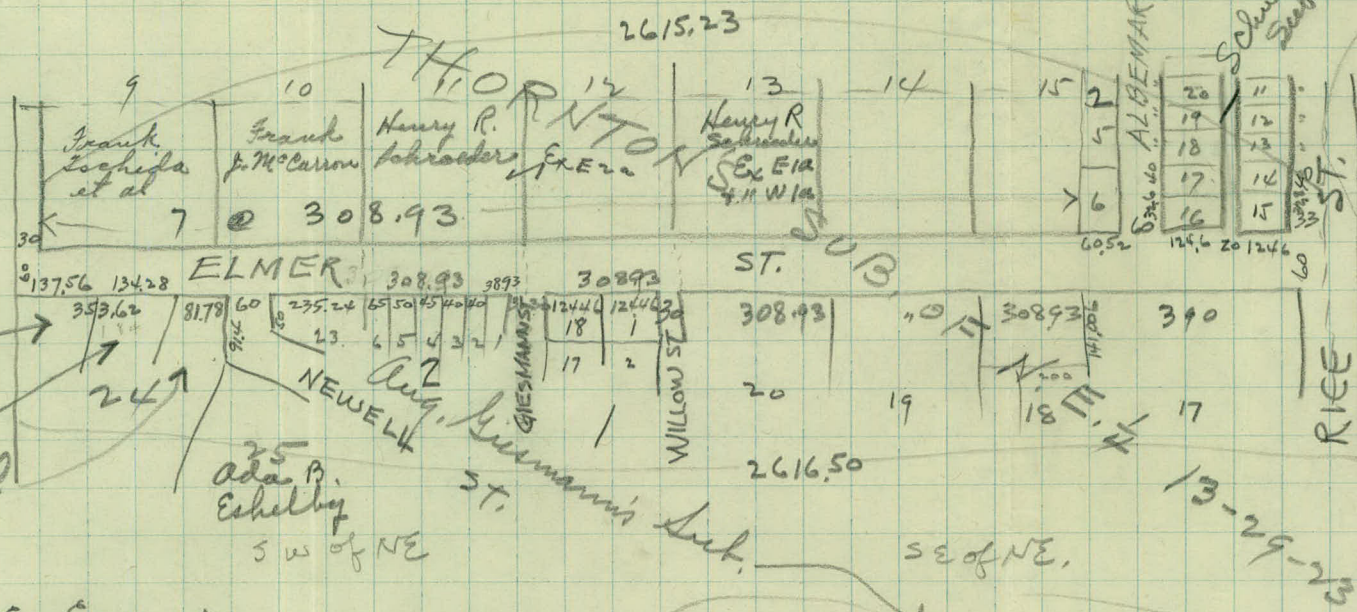
13+50 - 15+00 Cr. G. 67

14+50 - 15 Rt. clear 1

19+50 - 20+50 Lt. Q. ~~2.5~~ 5

NW of NE

NE of NE



Armin H. Albrecht
Clara A. Albrecht
Alma H. Voll

Henry R. Schroeder Ex. E. 2a 12
Henry Schroeder E. 2a of 12 + W. 1 of 13
Henry R. Schroeder Ex. E. 1a + Ex. W. 1a 13
Henry Schroeder E. 1a of 13 + all of 1K

Rose Eschida 15

Fred Brunk 17

Joseph + Katherine Platzgen N. 141.006' of 18

Louisa Conzelman Ex. 2a to School Dist. #29

School Dist. #29 1/2 a. in

John P. Kill

Lemmie V. Rodecker

Elmer St.

7 (2163.51
309.07

$$\begin{array}{r} 214736 \\ \hline 8947 \end{array} =$$

~~8947~~

2314119 ✓
38

4 8 0 5
8756 m ✓
✓

879,365,472 ✓
38

~~28~~