

Book 13, Dr. 11

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

PLAN Survey

SUMMER ST. & LAKE ST.

From..... To.....

Road Acc't. No. 34-R10

Date Filed 1933 File.....

Summer Street
set R/W stakes

from Eustis to Fulham

X- Sections

34- R10

Summer St.

B.M. 2.38 987.18 954.80

0+00 E Pleasant St. 52.8-

+18 52.2-

+29 51.7-

+50 50.1-

1 50.4-

+50 49.7-

+80 49.0-

2 47.5-

+25 46.1-

+50 45.8-

T.P. 459 948.48 13.29 943.89

3 43.6-

+50 42.1-

+75 41.0-

Spk. in 24" Dak 100' Rt. 0+30

$\frac{2.8}{40}$	$\frac{3.3}{33}$	$\frac{5.9}{17}$	$\frac{6.3}{17}$	$\frac{5.8}{13}$	$\frac{4.6}{8}$	$\frac{4.2}{4.4}$	$\frac{3.6}{19}$	$\frac{3.6}{40}$
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$\frac{2.3}{40}$	$\frac{3.5}{29}$	$\frac{5.4}{19}$	$\frac{6.6}{18}$	$\frac{6.6}{16}$	$\frac{5.8}{15}$	$\frac{5.1}{10}$	$\frac{5.4}{5.0}$	$\frac{6.7}{7}$	$\frac{5.8}{12}$	$\frac{5.8}{40}$
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$\frac{2.3}{40}$	$\frac{3.2}{31}$	$\frac{5.7}{20}$	$\frac{6.6}{19}$	$\frac{6.6}{18}$	$\frac{6.0}{17}$	$\frac{5.2}{12}$	$\frac{5.1}{6}$	$\frac{6.8}{5.5}$	$\frac{6.8}{5}$	$\frac{6.1}{7}$	$\frac{5.4}{17}$	$\frac{5.4}{40}$
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$\frac{2.8}{40}$	$\frac{3.6}{32}$	$\frac{4.9}{25}$	$\frac{6.1}{21}$	$\frac{7.1}{20}$	$\frac{6.4}{19}$	$\frac{5.7}{16}$	$\frac{5.5}{11}$	$\frac{6.1}{2}$	$\frac{7.5}{7.1}$	$\frac{6.6}{2}$	$\frac{5.8}{4}$	$\frac{5.8}{40}$
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$\frac{3.2}{40}$	$\frac{4.1}{31}$	$\frac{5.2}{25}$	$\frac{7.5}{23}$	$\frac{7.5}{21}$	$\frac{6.7}{19}$	$\frac{6.3}{16}$	$\frac{6.1}{11}$	$\frac{8.0}{6.8}$	$\frac{7.7}{2}$	$\frac{8.4}{11}$	$\frac{7.8}{19}$	$\frac{7.8}{40}$
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$\frac{3.1}{40}$	$\frac{6.2}{20}$	$\frac{7.3}{14}$	$\frac{8.1}{14}$	$\frac{8.1}{12}$	$\frac{7.4}{10}$	$\frac{8.0}{7.5}$	$\frac{9.0}{6}$	$\frac{10.1}{11}$	$\frac{10.1}{40}$
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$\frac{3.4}{40}$	$\frac{4.6}{28}$	$\frac{6.3}{19}$	$\frac{7.6}{6}$	$\frac{9.4}{4}$	$\frac{8.3}{3}$	$\frac{8.9}{8.2}$	$\frac{9.4}{3}$	$\frac{10.1}{13}$	$\frac{10.8}{22}$	$\frac{10.8}{40}$
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$\frac{5.0}{40}$	$\frac{6.4}{34}$	$\frac{7.4}{14}$	$\frac{9.6}{3}$	$\frac{10.2}{1}$	$\frac{9.7}{9.7}$	$\frac{9.6}{7}$	$\frac{10.2}{16}$	$\frac{11.8}{21}$	$\frac{11.2}{23}$	$\frac{11.5}{40}$
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$\frac{8.4}{40}$	$\frac{10.1}{18}$	$\frac{9.8}{6}$	$\frac{10.9}{11.1}$	$\frac{10.5}{3}$	$\frac{10.9}{5}$	$\frac{11.5}{11}$	$\frac{12.3}{19}$	$\frac{11.9}{22}$	$\frac{11.6}{24}$	$\frac{11.6}{40}$
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$\frac{9.8}{40}$	$\frac{11.8}{10}$	$\frac{11.4}{11.4}$	$\frac{12.3}{3}$	$\frac{11.5}{8}$	$\frac{11.8}{21}$	$\frac{12.8}{24}$	$\frac{12.0}{26}$	$\frac{12.3}{40}$
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$\frac{4.0}{40}$	$\frac{4.5}{20}$	$\frac{5.4}{4}$	$\frac{5.1}{4.9}$	$\frac{5.0}{12}$	$\frac{5.2}{32}$	$\frac{5.2}{40}$
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$\frac{6.9}{40}$	$\frac{6.4}{20}$	$\frac{6.4}{6.4}$	$\frac{6.1}{6}$	$\frac{7.2}{20}$	$\frac{6.9}{40}$
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$\frac{8.8}{40}$	$\frac{8.1}{12}$	$\frac{7.5}{7.5}$	$\frac{6.8}{6}$	$\frac{6.3}{20}$	$\frac{7.3}{23}$	$\frac{6.8}{40}$
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✓
948.48

4

41.4

+50

43.3

5

44.5

T.P. 7.73 959.03 3.18 945.30

+50

43.8

+82

43.3

6

44.9

+25

49.2

+43

52.1

+50

48.3

+55

49.7

+69.68 £ Fulham St.

B.M.

0.72

952.31

✓ 50.5

952.31

$$\frac{9.6}{40} \quad \frac{8.4}{22} \quad 7.1 \quad \frac{6.6}{12} \quad \frac{6.3}{18} \quad \frac{6.9}{27} \quad \frac{6.6}{40}$$

$$\frac{8.5}{40} \quad \frac{6.9}{23} \quad \frac{6.4}{4} \quad \frac{5.3}{2} \quad 5.2 \quad \frac{5.2}{14} \quad \frac{4.8}{23} \quad \frac{5.4}{31} \quad \frac{4.6}{40}$$

$$\frac{8.2}{40} \quad \frac{5.6}{8} \quad \frac{4.0}{2} \quad 4.0 \quad \frac{3.3}{14} \quad \frac{2.5}{17} \quad \frac{2.1}{30} \quad \frac{1.5}{31} \quad \frac{0.7}{40}$$

$$\frac{14.0}{40} \quad \frac{11.8}{12} \quad \frac{10.9}{5} \quad 9.2 \quad \frac{7.0}{16} \quad \frac{4.6}{23} \quad \frac{4.3}{37} \quad \frac{3.4}{40}$$

$$\frac{14.0}{40} \quad \frac{12.6}{20} \quad \frac{11.0}{5} \quad 9.7 \quad \frac{6.4}{14} \quad \frac{3.5}{20} \quad \frac{3.4}{40}$$

$$\frac{13.0}{40} \quad \frac{12.1}{22} \quad \frac{10.3}{7} \quad 8.1 \quad \frac{6.1}{12} \quad \frac{3.4}{16} \quad \frac{2.9}{29} \quad \frac{2.0}{35} \quad H_0.$$

$$\frac{11.5}{40} \quad \frac{8.8}{21} \quad \frac{5.7}{6} \quad \frac{4.0}{2} \quad 3.8 \quad \frac{2.3}{28} \quad \frac{+1.0}{31} \quad \frac{+1.0}{35} \quad H_0.$$

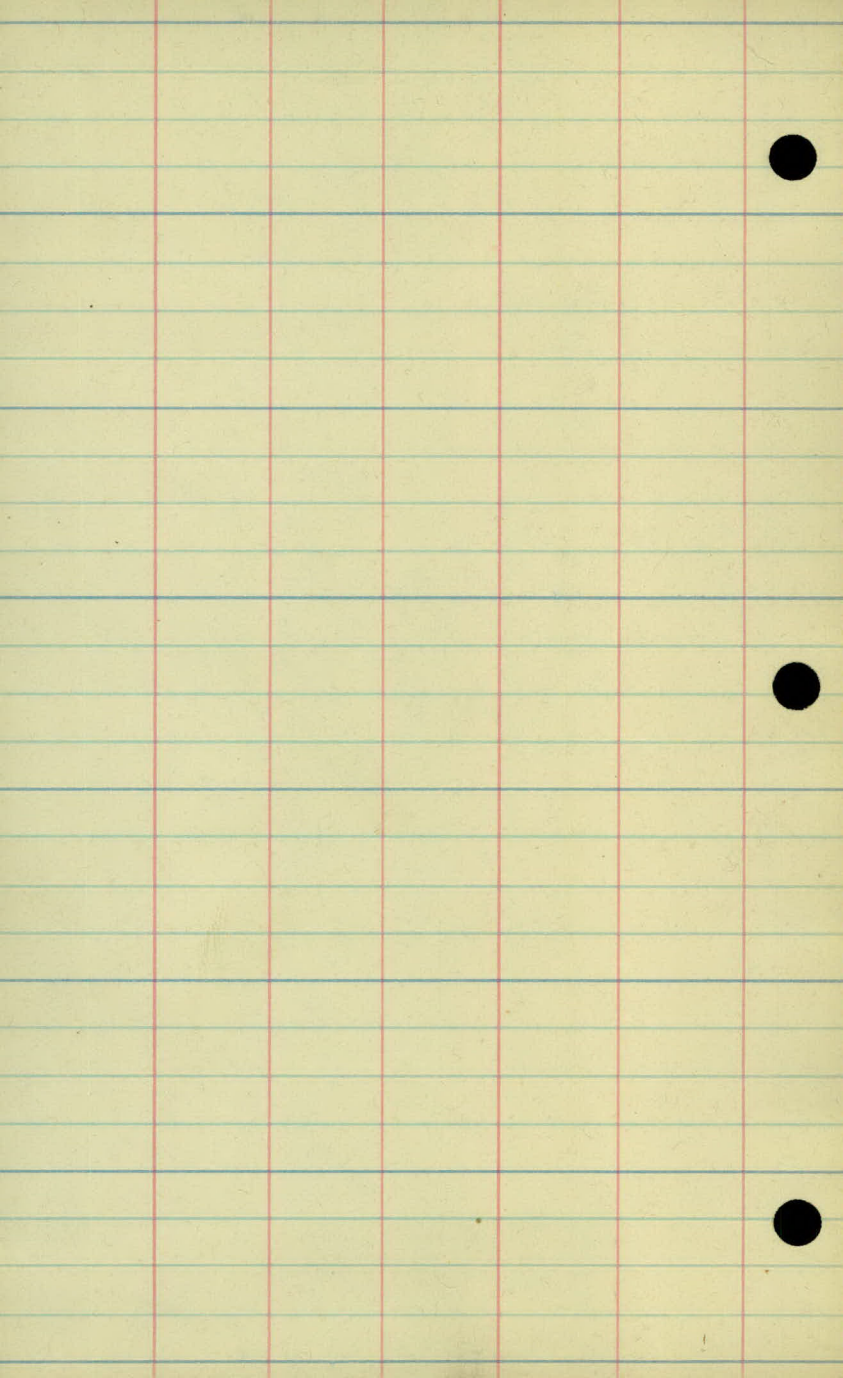
$$\frac{7.4}{40} \quad \frac{3.5}{12} \quad 0.9 \quad \frac{0.3}{7} \quad \frac{2.8}{11} \quad \frac{1.9}{27} \quad \frac{+2.0}{32} \quad \frac{+2.2}{40}$$

$$\frac{7.2}{40} \quad \frac{5.7}{22} \quad 4.7 \quad \frac{4.5}{10} \quad \frac{2.7}{12} \quad \frac{1.7}{33} \quad \frac{2.6}{37} \quad \frac{2.6}{40}$$

$$\frac{4.6}{40} \quad \frac{4.1}{22} \quad 3.3 \quad \frac{2.0}{22} \quad \frac{1.5}{40}$$

$$\frac{4.0}{40} \quad 2.5 \quad \frac{1.0}{40}$$

Spk. in 15" Oak N.E. Cor. Fulham + Summer Sts.



Alignment

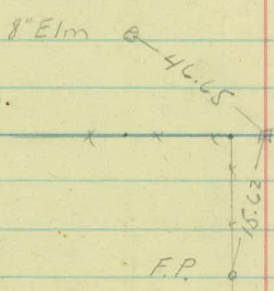
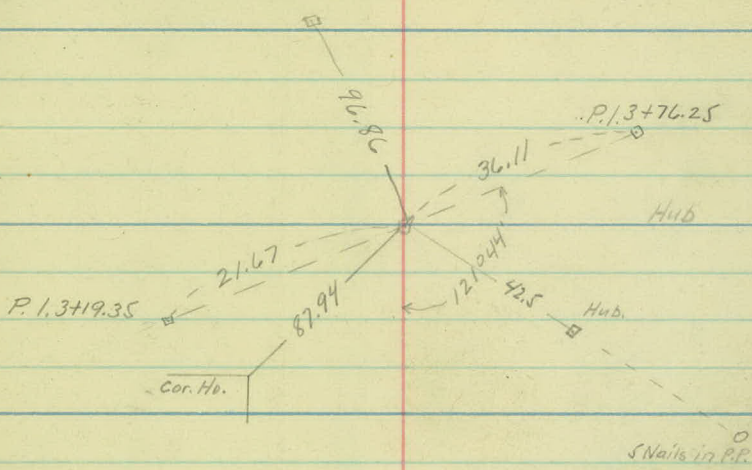
Lake St.

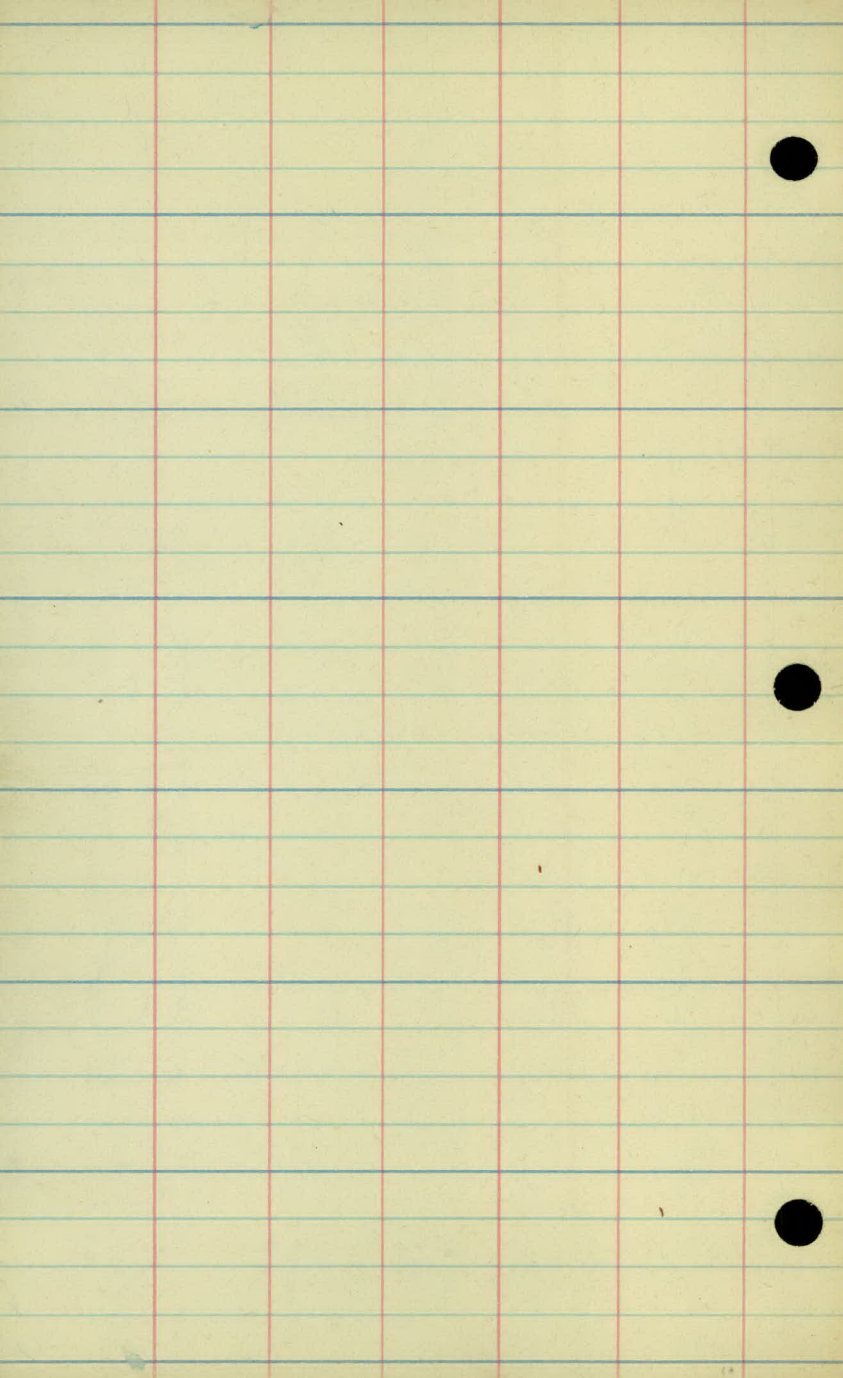
34-R10

6+39.88 @ Summer St.

0+00 @ Spring St.

Hub @ F. Cor.





Topog.
34-R10
Lake St.

7

6

5

4

3

2

1

0700

+37-F. 35'

+96-T. 32'

+27-T. 25'

Yard

Yard

Cult.

Cult.

+81-T. 20'

+70-T. 20'

+69-T. 20'

+47-T. 25'

+05-12"X14' C.M. 18'

+95-T. 28'

+80-T. 28'

Cult.

+77-F.G. 20'

+09-F. Int. 23'

Yard

Berries

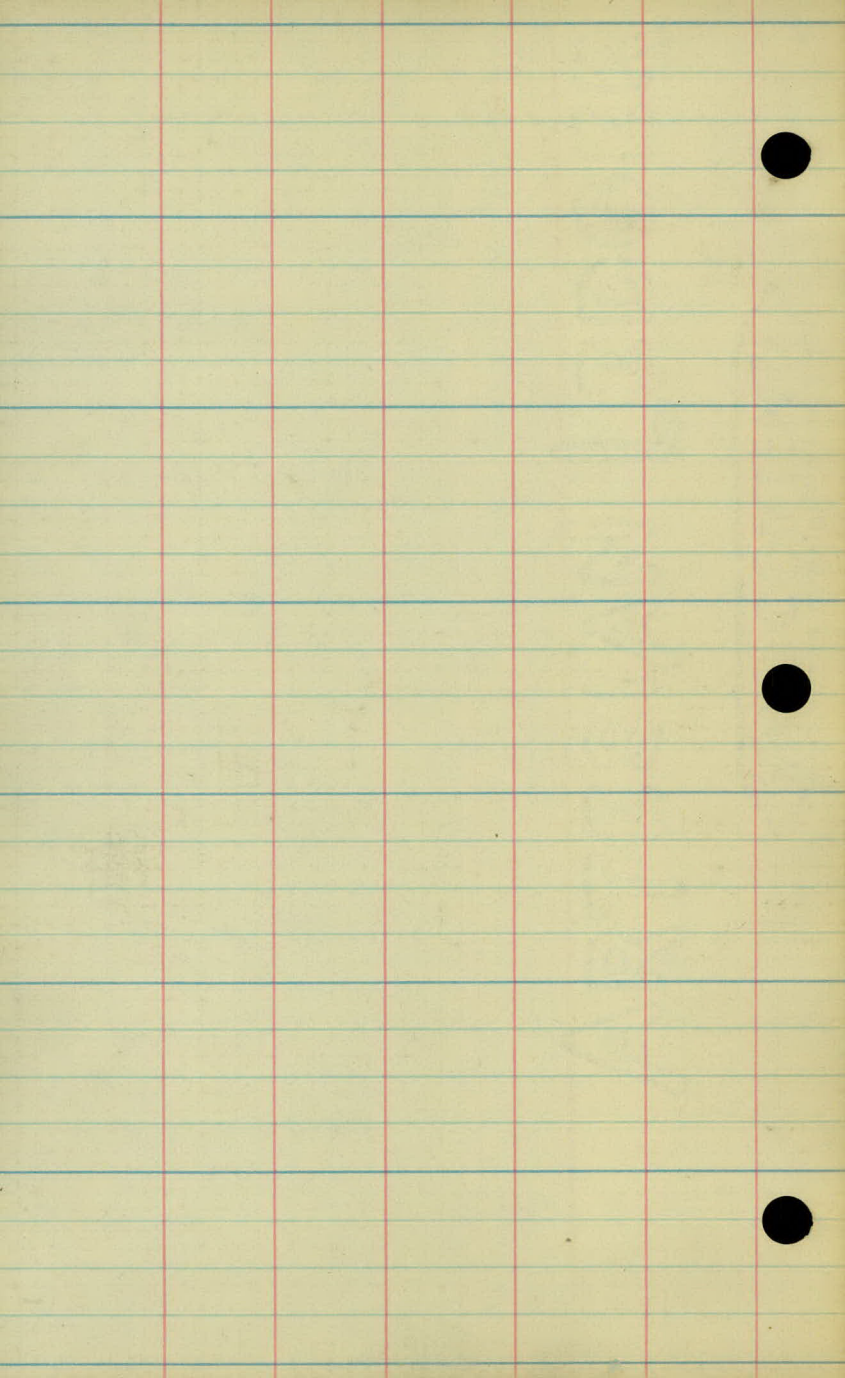
Orchard

+00-F.C. 5'

+25-F.C. 25'

+22-P.P. 16'

+16-12"X32' C.M. 20'



X-Sections

34-R10

Lake St.

B.M. 0.24 959.80 ✓

959.56 ✓

0+00

58.7

+08

57.2

+13 E Spring St.

+19

58.1

+25

58.9

+50

58.3

1

56.8

+50

55.2

2

54.3

+50

52.8

+73

51.8

3

49.1

+30

47.2

T.P.

3.74

950.22 ✓

13.32

946.48 ✓

4.

44.5

Spk. in 8" Elm NW Cor. Spring & Lake Sts.

$$\begin{array}{r} 0.8 \\ 40 \end{array} \quad \begin{array}{r} 0.8 \\ 27 \end{array} \quad 1.1 \quad \begin{array}{r} 0.0 \\ 28 \end{array} \quad \begin{array}{r} 0.0 \\ 40 \end{array}$$

$$\begin{array}{r} 0.8 \\ 40 \end{array} \quad \begin{array}{r} 0.8 \\ 18 \end{array} \quad 0.6 \quad \begin{array}{r} 0.3 \\ 24 \end{array} \quad \begin{array}{r} 0.0 \\ 40 \end{array}$$

$$\begin{array}{r} 0.8 \\ 40 \end{array} \quad \begin{array}{r} 0.7 \\ 21 \end{array} \quad 0.7 \quad \begin{array}{r} 0.7 \\ 20 \end{array} \quad \begin{array}{r} 0.0 \\ 40 \end{array}$$

$$\begin{array}{r} 1.2 \\ 40 \end{array} \quad \begin{array}{r} 0.9 \\ 21 \end{array} \quad 0.9 \quad \begin{array}{r} 1.3 \\ 11 \end{array} \quad \begin{array}{r} 2.8 \\ 24 \end{array} \quad \begin{array}{r} 2.3 \\ 40 \end{array}$$

$$\begin{array}{r} 1.1 \\ 40 \end{array} \quad \begin{array}{r} 1.8 \\ 21 \end{array} \quad \begin{array}{r} 2.4 \\ 13 \end{array} \quad \begin{array}{r} 1.9 \\ 9 \end{array} \quad 1.5 \quad \begin{array}{r} 1.6 \\ 10 \end{array} \quad \begin{array}{r} 3.1 \\ 16 \end{array} \quad \begin{array}{r} 4.1 \\ 24 \end{array} \quad \begin{array}{r} 3.8 \\ 40 \end{array}$$

$$\begin{array}{r} 2.8 \\ 40 \end{array} \quad \begin{array}{r} 3.3 \\ 14 \end{array} \quad \begin{array}{r} 3.8 \\ 12 \end{array} \quad \begin{array}{r} 3.1 \\ 6 \end{array} \quad 3.0 \quad \begin{array}{r} 2.9 \\ 15 \end{array} \quad \begin{array}{r} 4.4 \\ 21 \end{array} \quad \begin{array}{r} 4.2 \\ 40 \end{array} \quad \times$$

$$\begin{array}{r} 3.9 \\ 40 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad \begin{array}{r} 5.2 \\ 13 \end{array} \quad \begin{array}{r} 4.6 \\ 8 \end{array} \quad 4.6 \quad \begin{array}{r} 4.4 \\ 5 \end{array} \quad \begin{array}{r} 4.9 \\ 22 \end{array} \quad \begin{array}{r} 4.9 \\ 40 \end{array}$$

$$\begin{array}{r} 6.5 \\ 40 \end{array} \quad \begin{array}{r} 6.4 \\ 12 \end{array} \quad \begin{array}{r} 5.9 \\ 8 \end{array} \quad 5.5 \quad \begin{array}{r} 5.6 \\ 11 \end{array} \quad \begin{array}{r} 6.0 \\ 20 \end{array} \quad \begin{array}{r} 5.0 \\ 23 \end{array} \quad \begin{array}{r} 4.8 \\ 40 \end{array}$$

$$\begin{array}{r} 9.4 \\ 40 \end{array} \quad \begin{array}{r} 8.1 \\ 23 \end{array} \quad \begin{array}{r} 7.9 \\ 13 \end{array} \quad \begin{array}{r} 7.2 \\ 8 \end{array} \quad 7.0 \quad \begin{array}{r} 6.7 \\ 7 \end{array} \quad \begin{array}{r} 7.1 \\ 15 \end{array} \quad \begin{array}{r} 7.3 \\ 19 \end{array} \quad \begin{array}{r} 5.5 \\ 22 \end{array} \quad \begin{array}{r} 4.9 \\ 40 \end{array}$$

$$\begin{array}{r} 11.6 \\ 40 \end{array} \quad \begin{array}{r} 9.8 \\ 9 \end{array} \quad 8.0 \quad \begin{array}{r} 7.4 \\ 8 \end{array} \quad \begin{array}{r} 7.9 \\ 18 \end{array} \quad \begin{array}{r} 6.5 \\ 21 \end{array} \quad \begin{array}{r} 5.7 \\ 40 \end{array}$$

$$\begin{array}{r} 13.0 \\ 40 \end{array} \quad \begin{array}{r} 12.0 \\ 11 \end{array} \quad 10.7 \quad \begin{array}{r} 8.4 \\ 7 \end{array} \quad \begin{array}{r} 8.0 \\ 16 \end{array} \quad \begin{array}{r} 8.2 \\ 23 \end{array} \quad \begin{array}{r} 7.0 \\ 32 \end{array} \quad \begin{array}{r} 6.8 \\ 40 \end{array}$$

$$\begin{array}{r} 14.1 \\ 40 \end{array} \quad \begin{array}{r} 13.6 \\ 10 \end{array} \quad 12.6 \quad \begin{array}{r} 11.5 \\ 10 \end{array} \quad \begin{array}{r} 10.5 \\ 14 \end{array} \quad \begin{array}{r} 8.5 \\ 40 \end{array}$$

$$\begin{array}{r} 6.6 \\ 40 \end{array} \quad \begin{array}{r} 6.2 \\ 10 \end{array} \quad 5.7 \quad \begin{array}{r} 3.5 \\ 20 \end{array} \quad \begin{array}{r} 3.3 \\ 30 \end{array} \quad \begin{array}{r} 2.2 \\ 40 \end{array}$$

✓
950.22

4+50

43.2

5

42.6

+50

42.6

6

41.6

+39.88

2 Summer St.

42.5

B.M.

4.31

945.91

945.90

$$\frac{7.0}{40} \quad \frac{7.2}{12} \quad 7.0 \quad \frac{6.8}{10} \quad \frac{5.4}{22} \quad \frac{5.1}{40}$$

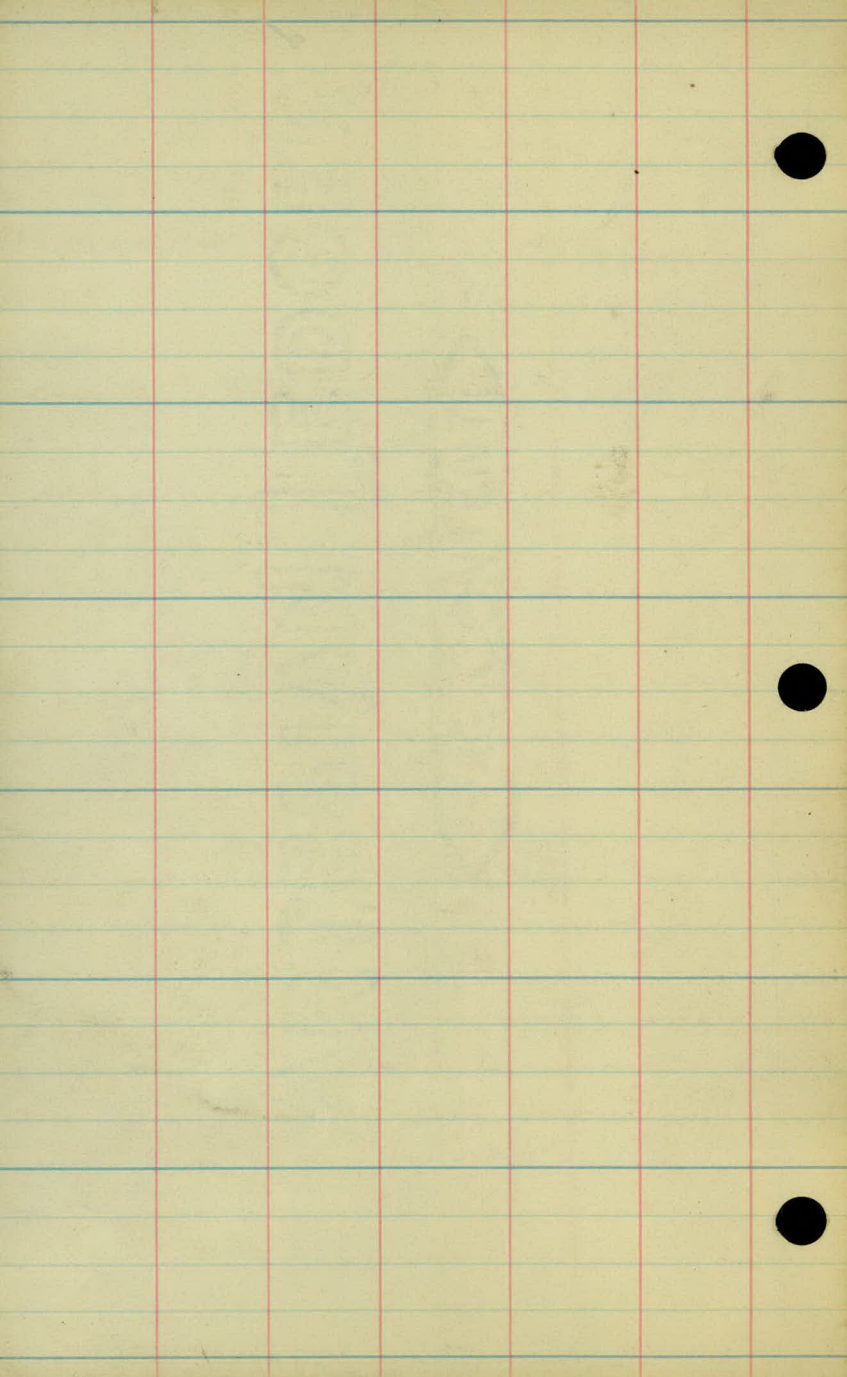
$$\frac{6.2}{40} \quad \frac{6.2}{38} \quad \frac{7.8}{28} \quad \frac{7.8}{12} \quad 7.6 \quad \frac{6.9}{20} \quad \frac{6.2}{23} \quad \frac{6.2}{40}$$

$$\frac{5.8}{40} \quad \frac{5.8}{37} \quad \frac{8.1}{27} \quad \frac{7.9}{15} \quad 7.6 \quad \frac{7.1}{16} \quad \frac{7.2}{40}$$

$$\frac{6.1}{40} \quad \frac{6.4}{35} \quad \frac{7.8}{12} \quad 8.6 \quad \frac{8.7}{20} \quad \frac{8.0}{40}$$

$$\frac{6.4}{40} \quad \frac{7.4}{20} \quad 7.7 \quad \frac{8.7}{40}$$

N. E. Cor. Conc. Railing of Steps Lt. 5+20



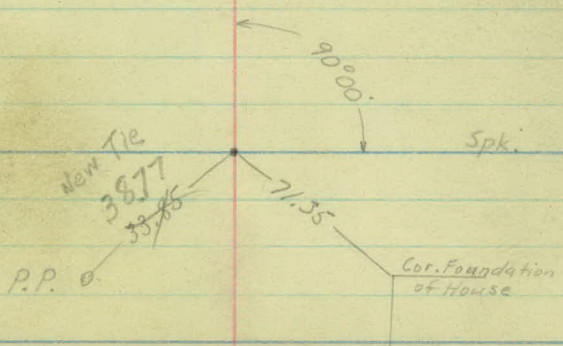
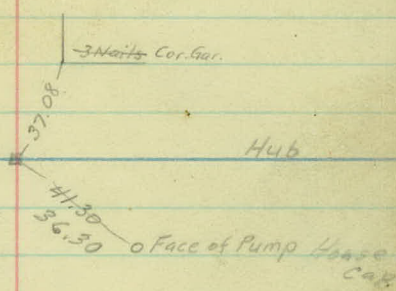
Alignment

Summer St.

34-R10

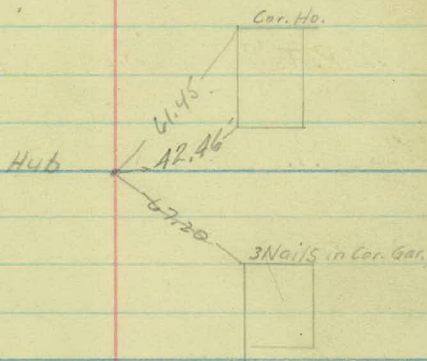
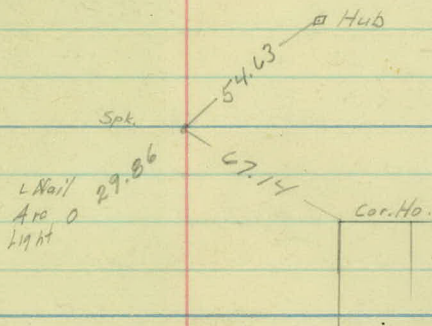
1+56.79	P.T.	14°08 ⁵	
+50		13°21 ⁵	A-28°17'
1		7°36 ⁵	D-23°L
0+97.0	P.I.		T-63.18
+50		1°51 ⁵	L-122.97
0+33.82	P.C.	0°00'	R-250.79

0+00 £ Pleasant St.



			$\Delta-24^{\circ}14'$	
3+47.76	P.R.C.	$12^{\circ}07'$	D-43°L	
3+19.35	P.I.		T-29.29	Ext 3.1
3		$2^{\circ}08'$	L-57.70	
2+90.06	P.C.	$0^{\circ}00'$	R-136.43	

2+88.51	P.T.	$10^{\circ}24'$	$\Delta-20^{\circ}48'$
+50 ^{.12}		$6^{\circ}56'$	D-18°R
2+31.61	P.I.		T-58.66
2 ^{.15}		$2^{\circ}26'$	L-115.56
1+72.95	P.C.	$0^{\circ}00'$	R-319.62



6+69.68 E Fulham St.

4+03.26 P.T.

15°54' Δ-31°48'

4

15°40' D-60°R.

3+76.25 P.I.

T-28.49

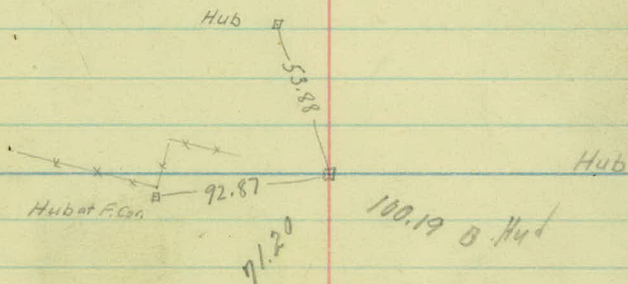
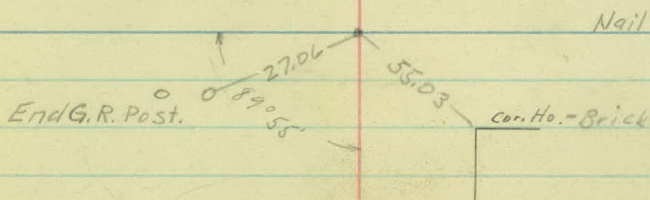
Ext. 3.9

+50

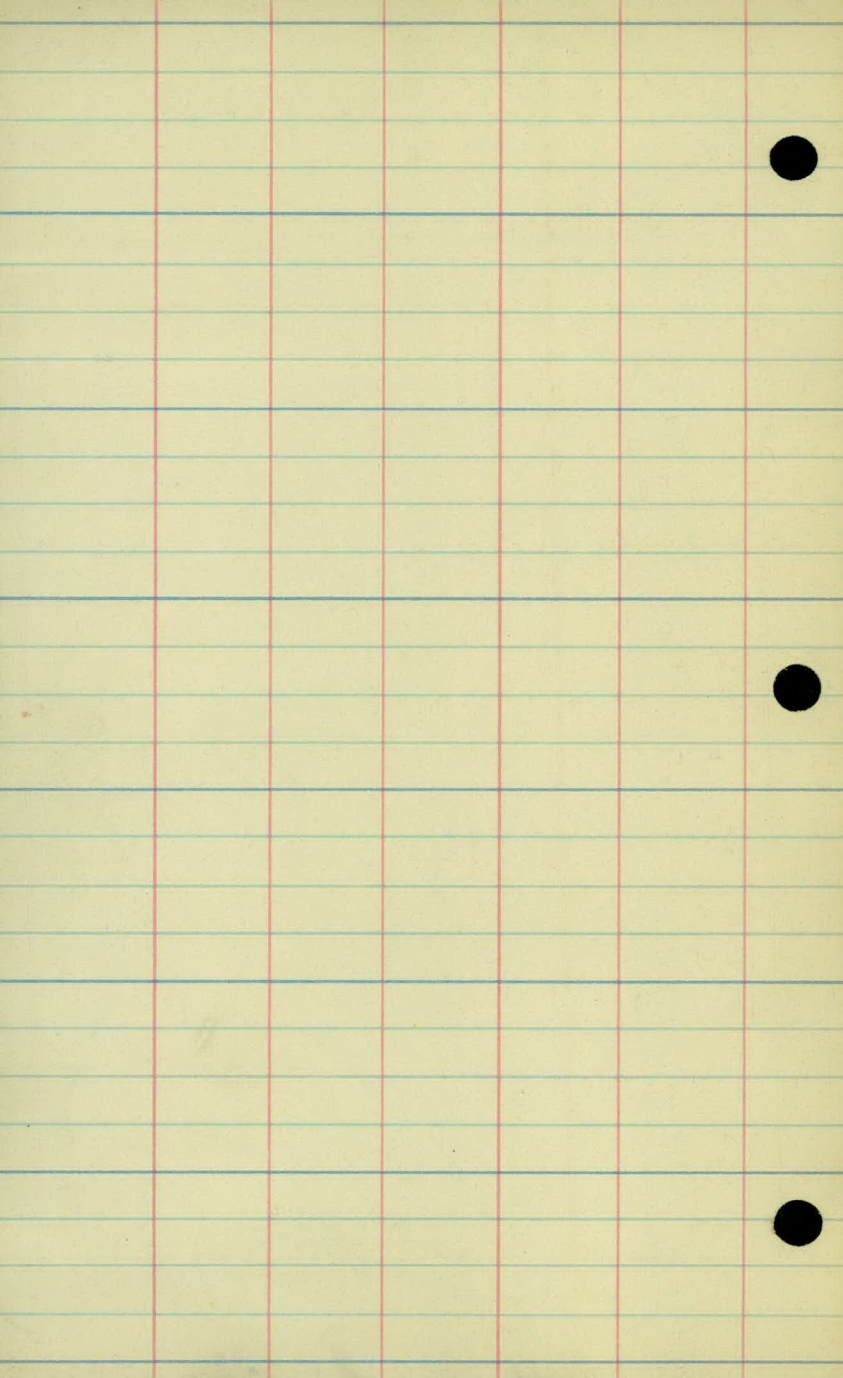
0°40' L-55.50

3+47.76 P.R.C.

0°00' R-100.0



PPD
 One Nail (side)



Topog.

34-R10

Summer St.

7

6

5

4

3

2

1

0+00

+58-G.P. 24'

+42-F.C. 13'

F. 10'

F. 5'

+71-F.C. 4'

+63-P.P. 24'

+68-E.Dr. 12" x 18" C.M.

+69-P.P. 30'

Fulham St.

Posture

Cut

+50-15" x 24" C.M. 10'

+37-Steps 27'

+91-Ho. 35'

+71-2T. 20'

+63-End Bushes 30'

+46-Beg. Bushes 24'

+21-T. 18'

+91-T. 16'

+75-T. 13'

+55-T. 8'

+51-St. 4.9'

+48-T. 2'

+39-St. 1.8'

+89-T. 25'

+83-T. 25'

+60-T. 28'

+28-Ho. 37'

+75-E.Dr.

+56-Gar. 18'

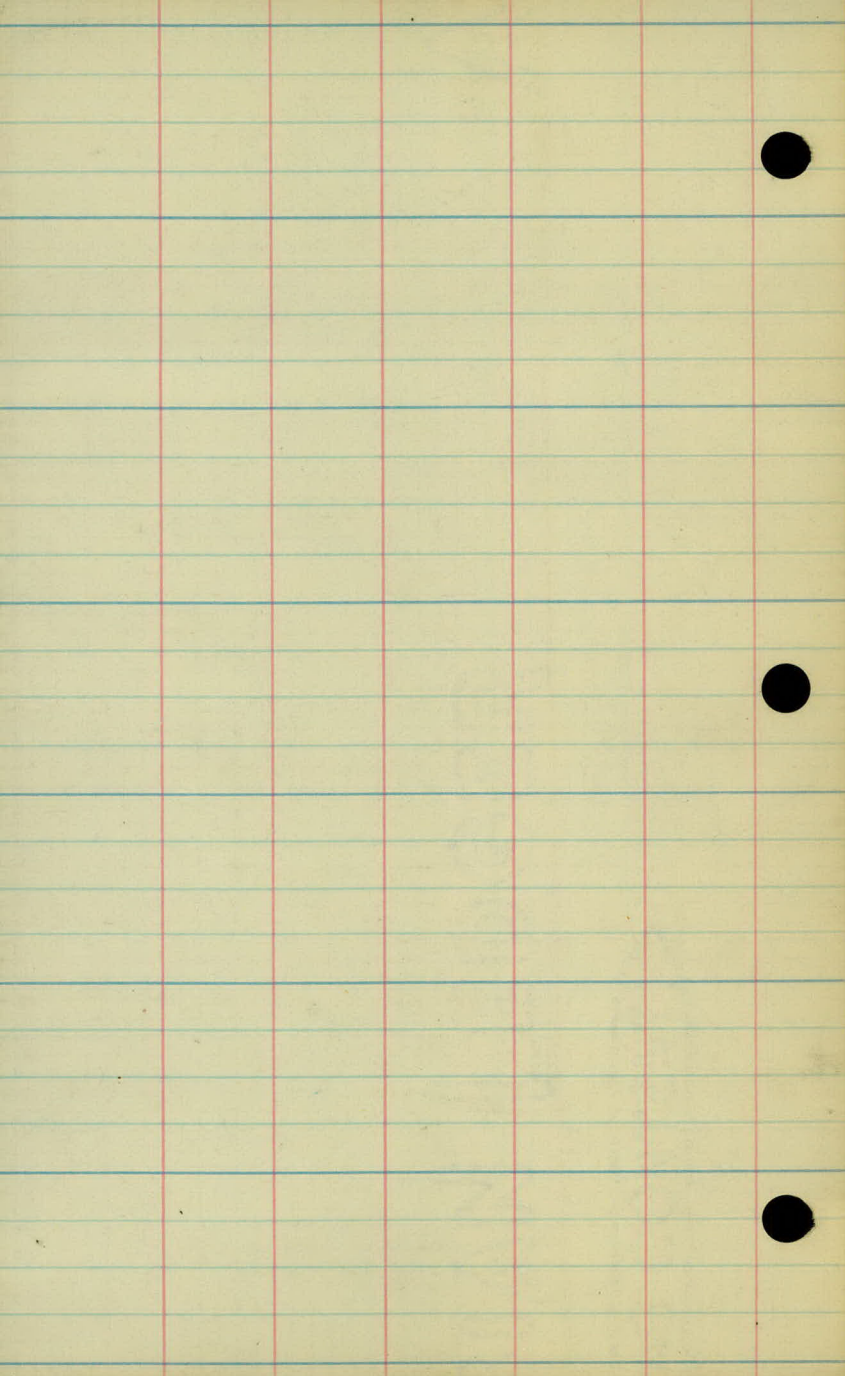
+40-E.Dr.

12" x 24" C.M.

+20-Gar. 32'

+77-Water Pump 44'

+16-Rd. Sq. 20'



Summer St.
Division A.

1+40 Rt. 12" x 24" C.M. Rem & Rep.

1+68 Lt. R Rep 12" x 18' C.M.

1+75 Rt. Place 12" x 20' C.M.

✓ 3+75± Pl. 18" x 36' P.3.

4+50 to 6+00 Clear 4

Sub 7

5+50 Rt. Pl. 12" x 20' C.M.

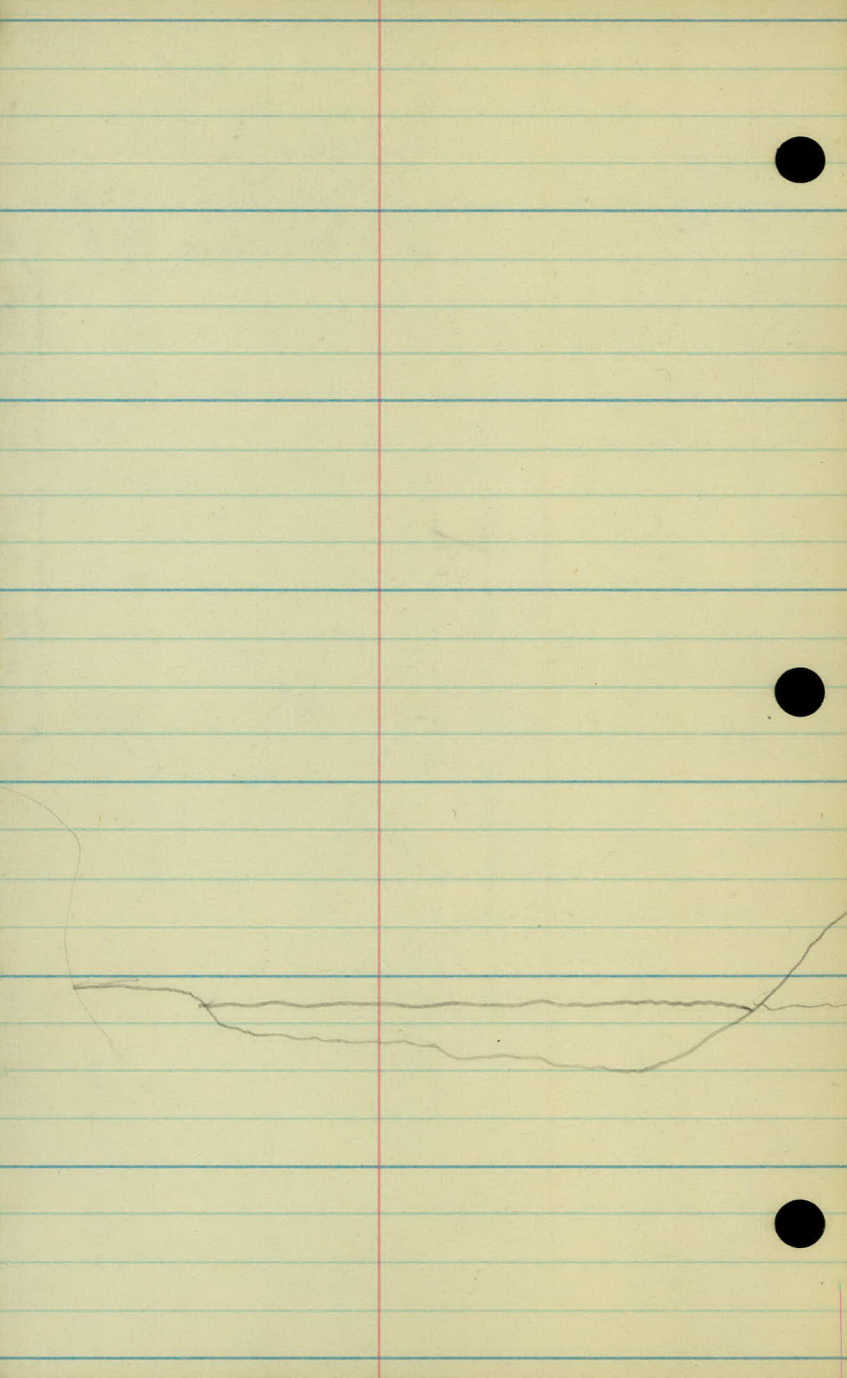
~~Rem 15" C.M. + Rep 18" C.M.~~

~~Extend 15" C.M.~~

15" x 24" C.M.

6+50 Rt. Rem & Replace.

Extend 30'



Plants in hand. Lake St.
3/27/34 Spring St.
Carley Proj. 34-R10
Grubbarz. Rose Twp.

Division "B"

Sta 0+16 Rt. Remove + Place
15' ~~18'~~ c.m. x 40'

2+00 Lt Rep. 12" c.m. x 24' c.m.
from 0+16

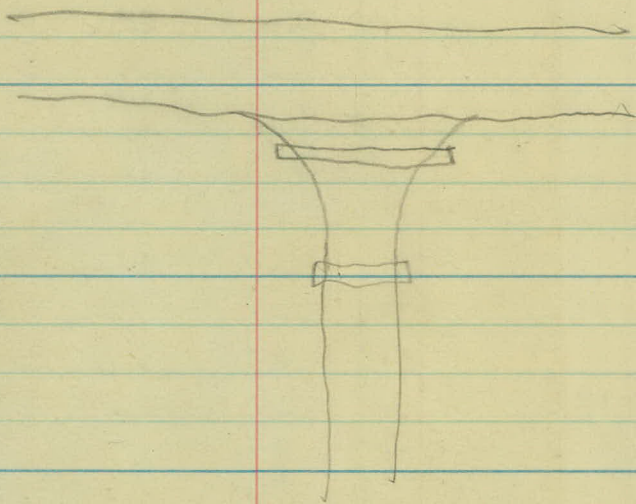
3+05 Rt. Rem. + replace
Extend with 12" x 8' c.m.
from 0+16

3+50 to 4+00 Clear 3 trees
Grub 3 "

5+00 to 5+50 Clear + Grub 1 tree

4+90 Lt Pl. 12" x 20" c.m.

6+00 ± Pl. 18" x 32' P. 3



11 Sept 1952
FK
AM
MB
FB

1

Summer St

Profile & X-Sections

Note:

End of traveled Roadway is 15' Rt of
Located &

5 pages

Drawn up

Sta	+	π	-	Elev
BM	5.46	952.62		947.16
	10.55	961.87	1.30	951.32
BM			0.96	960.91

0+00 ~~Eustis St~~ 58.4

+18 58.1

+50 57.9

TP 6.28 964.12 4.03 957.84

1 57.5

+50 57.2

2 57.0

+50 56.9

Lt

L

Rt

2

Top Deer Sill Front of Ho NE. Cor. Carl & Roselawn

Top Hyd S.W. Cor Summer & Eustis

57.5

4.4

3.5

3.5

15

58.6

3.3

50

3.8

15

4.0

15

6.6

15

6.9

15

7.1

75

72

Sta	+	π	-	Elev
		964.12		
2+60				56.6
3				56.9
+50				57.3
+73				57.5
+78				57.7
4				58.4
+36				56.6
+50				56.0

H

I

R

✓

55.7	55.6	55.2	56.0	57.4	56.4	56.6	56.8	56.7	57.5	57.6
8.4	8.5	8.9	8.1	6.7	7.5	7.7	7.3	7.4	6.6	6.5
35	40	17	10	6	7	15	25	32	36	50
57.8	57.3	57.2	57.2	57.2	56.6	57.2	57.2	57.2	57.4	✓
6.3	6.8	6.8	6.9	7.5	6.9	6.9	6.9	6.9	6.7	✓
35	16	3	5	15	28	30	65	✓	✓	✓
58.0	57.7	57.7	57.5	56.5	57.0	56.7	57.1	57.5	57.5	✓
6.1	6.4	6.4	6.6	6.6	7.6	7.1	7.4	7.0	6.6	✓
35	18	7	1	4	15	28	31	42	50	✓
58.1	57.8	57.9	57.4	56.5	56.8	56.6	58.4	59.2	✓	✓
6.0	6.3	6.2	6.4	6.7	7.6	7.3	7.5	5.7	4.9	✓
35	19	9	2	4	15	29	32	50	✓	✓
59.0	58.7	58.9	56.2	56.7	56.3	59.4	59.9	60.0	✓	✓
5.1	5.4	5.2	5.7	7.9	7.4	7.8	4.7	4.2	4.1	✓
35	13	2	2	15	30	38	40	50	✓	✓
61.1	60.4	60.5	60.4	56.0	56.5	56.6	59.6	60.1	60.1	✓
3.0	3.7	3.6	3.7	8.1	7.6	7.5	4.5	4.0	4.0	✓
35	25	7	2	9	15	28	32	37	✓	✓
61.1	61.1	57.1	55.9	56.5	56.4	58.8	60.1	60.1	✓	✓
3.0	3.0	7.0	8.1	7.6	7.7	5.9	4.0	4.0	✓	✓
35	30	18	2	15	29	31	35	50	✓	✓

Sta	+	Δ	-	Elev
		964.12		.
+53				56.0
+62				55.9
+66				55.7
+75				60.0
5				58.6
+18				57.7
TP	4.49	938.94	9.67	954.45
+27				56.0
+50				54.6

4

2

21

2

59.1
5.0
35

56.5
7.6
10

8.1

55.8
8.3
5

56.4
7.7
15

56.4
7.7
28

59.7
7.4
33

60.1
4.0
50

59.1
5.0
35

57.2
6.9
18

8.2

55.5
8.6
4

56.4
7.7
15

56.3
7.8
29

59.4
7.7
32

59.6
4.5
15

60.8
2.9
33
61.2
2.9
10

61.6
2.8
5
56.0
2.1
3

55.5
8.6
4

56.3
7.8
15

56.3
7.8
29

59.4
7.7
32

59.6
4.5
45

62.0
2.3
21
61.6
2.3
15

61.5
2.6
3

55.4
8.7
4

56.1
8.0
15

56.1
8.0
28

58.9
5.2
32

59.4
4.7
50

62.5
1.6
Ho.
60'

61.5
2.6
35
61.0
3.1
18

60.5
3.6
4

55.1
9.0
4

55.7
8.4
15

55.9
8.2
25

57.7
6.4
40

58.2
5.9
50

59.0
3.1
35
58.4
3.7
12

54.7
9.4
5

55.3
8.8
15

55.3
8.8
26

56.8
7.3
32

57.2
6.9
50

57.9
1.0
35
57.5
1.4
13

57.0
1.9
3

54.5
4.4
4

55.1
3.8
15

54.9
4.0
27

55.9
3.0
29

55.4
3.5
35

55.9
3.0
35
55.5
3.4
18

55.0
3.9
4

54.0
4.9
7

54.4
4.5
15

53.9
5.0
29

52.6
6.3
37

52.6
6.3
50

Sta	+	π	-	Elev
		958.94		.

5+95				53.0
------	--	--	--	------

+95

BM		3.06	955.88	
----	--	------	--------	--

Lt

Φ

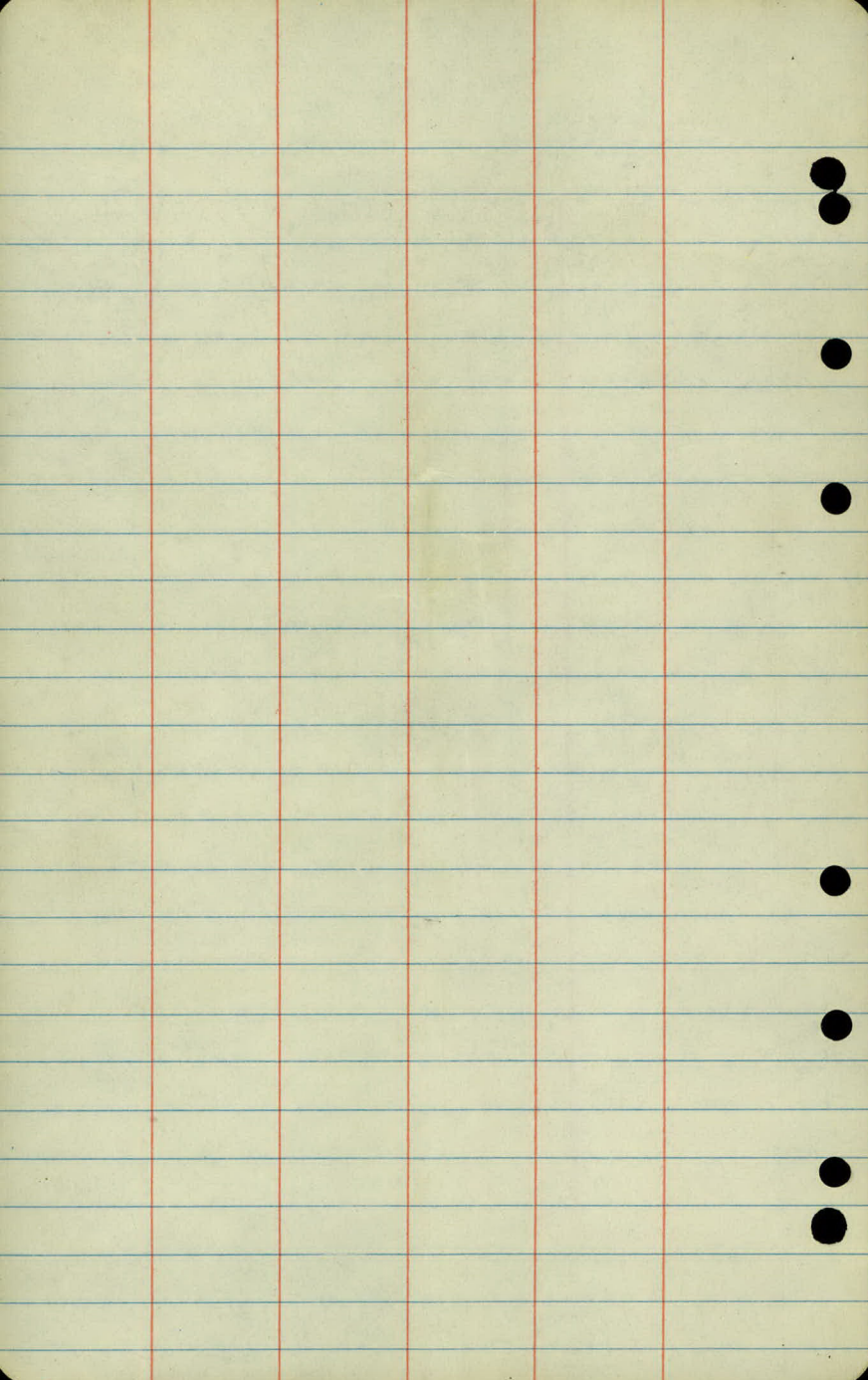
Rt.

52.6	51.9	52.1	52.0	52.3		53.6	53.8	52.8	✓
6.3	7.0	6.8	6.9	6.6	5.9	5.3	5.1	6.1	0
140	100	50	34	10		15	32	50	

54.1
4.8
170

could Drain if Ditched

Top Hyd S.W. Cor. Summer & Pleasant



2.54

6.49
C/O

6.44

4.83

Sta	+	x	-	Elev
BM	0.25	956.13		955.88
	10.37	954.44	12.06	944.07
BM			0.59	953.85
TP	4.23	945.15	13.52	940.92
			1.30	943.85 943.87

Top Hyd S.W. Cor Summer & Pleasant

Top Hyd S.W. Cor. Summer & Fulham

Spike in P.P. N.W. Cor Lake & Roselawn
BM Has been Disturbed

