

Book #10, Dr. 11

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Plan Survey

GARDEN AVENUE

From Hamline Ave to Lexington Ave

&

DUNLAP STREET

From Larpenieur Ave to Garden Ave

Road Acc't. No. 33-R26

Date Filed 1933

File //

Dunlap St.

Alignment

5TH. POINT.

13+20.33 End

8+73.25 P.O.T.

0+00 @ Larpenieur Ave

1/4 1/4 Line 2

505'

Spk.

No Ties

91°11'

1/4 1/4 Line 2

Spk. in 15" B.F.

60.55

Spk.

69.85

Cor. Ho.

503'

41.68

Spk. 41.49

Iron

792.0

792.0

91°14'

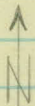
558.5

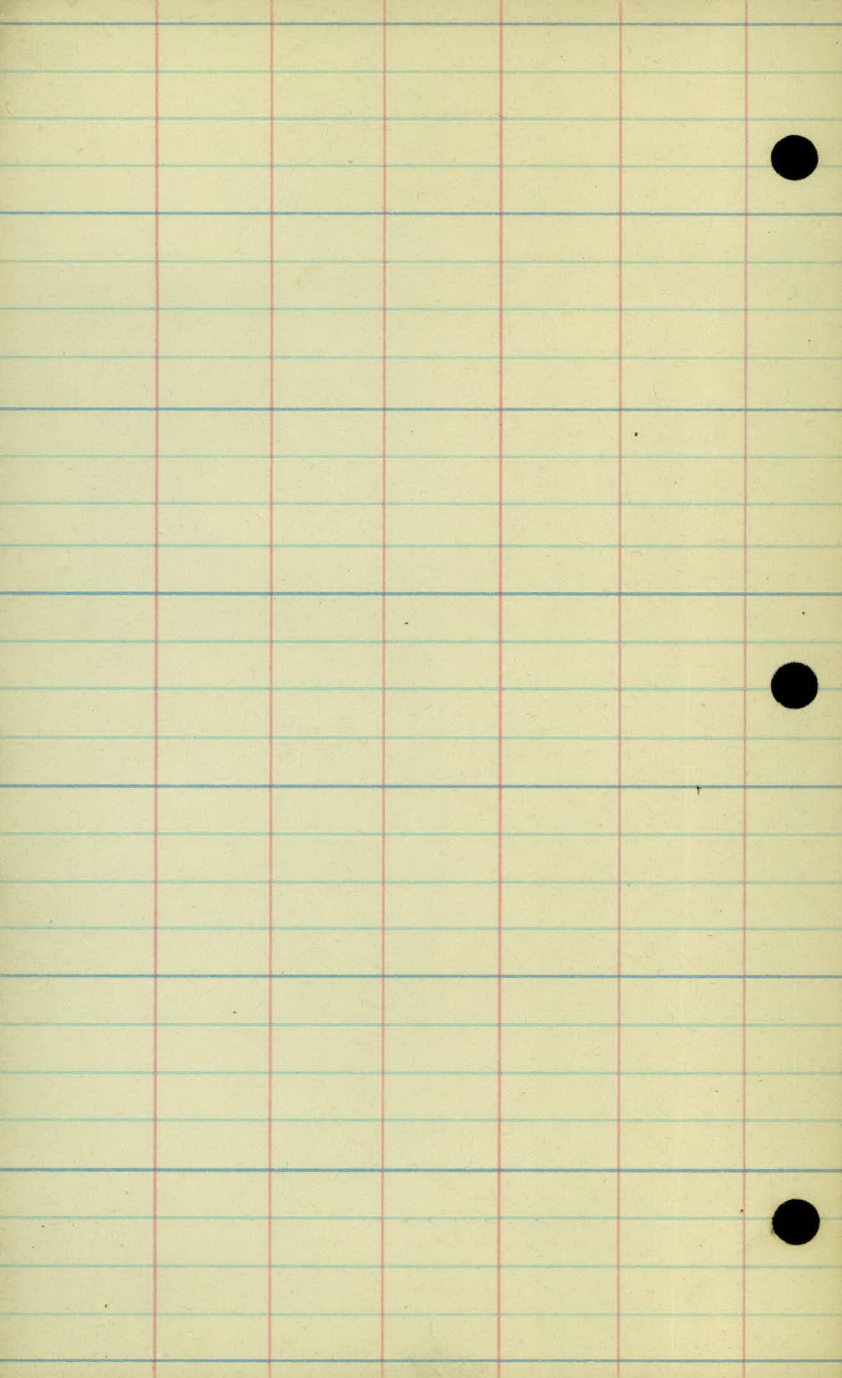
505'

Hole in Pavement

PP 6

45.30





Dunlap St.

X-Sections

STA	+	H.I.	-	ROD	ELEV
B.M.	11.57	921.50		909.93	
T.P.	2.33	923.11	0.72	920.78	
B.M.			3.08	920.03	

0+00	2 Larp. Ave		1.6	921.5
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+14			1.9	21.2
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+21			2.6	20.5
-----	--	--	-----	------

+26			2.8	20.3
-----	--	--	-----	------

+33			3.1	20.0
-----	--	--	-----	------

+38			3.4	19.7
-----	--	--	-----	------

+55			5.8	19.3
-----	--	--	-----	------

1			4.5	18.6
---	--	--	-----	------

+50			4.2	18.9
-----	--	--	-----	------

2			3.8	19.3
---	--	--	-----	------

+50			5.1	20.0
-----	--	--	-----	------

Gen. Mont. $1/4$ $1/4$ Cor. on Larp Ave

Spk. in T.P. N.E. Cor. Larp & Dunlap

$$\frac{2.8}{50} \quad \frac{2.3}{30} \quad 1.6 \quad \frac{0.8}{30} \quad \frac{0.15}{50}$$

$$\frac{2.9}{50} \quad \frac{2.5}{32} \quad \frac{2.3}{11} \quad 1.9 \quad \frac{1.9}{14} \quad \frac{1.0}{33} \quad \frac{0.5}{50}$$

$$\frac{5.8}{50} \quad \frac{5.8}{34} \quad \frac{5.8}{15} \quad \frac{2.8}{7} \quad 2.6 \quad \frac{2.6}{8} \quad \frac{5.2}{17} \quad \frac{6.2}{30} \quad \frac{5.8}{50}$$

$$\frac{8.2}{50} \quad \frac{9.2}{19} \quad \frac{7.6}{14} \quad \frac{5.3}{10} \quad \frac{2.8}{5} \quad 2.8 \quad \frac{2.8}{6} \quad \frac{7.8}{17} \quad \frac{5.8}{24} \quad \frac{5.8}{50}$$

$$\frac{7.8}{50} \quad \frac{8.1}{32} \quad \frac{7.7}{15} \quad \frac{6.1}{10} \quad \frac{3.1}{4} \quad 3.1 \quad \frac{3.0}{5} \quad \frac{8.1}{18} \quad \frac{8.0}{34} \quad \frac{7.6}{50}$$

$$\frac{8.0}{50} \quad \frac{8.0}{33} \quad \frac{8.4}{19} \quad \frac{8.2}{14} \quad \frac{5.6}{10} \quad \frac{5.5}{7} \quad \frac{3.4}{3} \quad 3.4 \quad \frac{3.3}{5} \quad \frac{8.2}{18} \quad \frac{7.7}{20} \quad \frac{7.1}{30} \quad \frac{7.1}{50}$$

$$\frac{7.4}{50} \quad \frac{7.4}{32} \quad \frac{8.0}{24} \quad \frac{8.4}{13} \quad \frac{6.2}{10} \quad \frac{5.6}{7} \quad \frac{3.8}{3} \quad 3.8 \quad \frac{3.7}{5} \quad \frac{8.2}{17} \quad \frac{7.5}{19} \quad \frac{6.7}{34} \quad \frac{6.6}{50}$$

$$\frac{8.2}{40} \quad \frac{8.6}{15} \quad \frac{6.7}{9} \quad \frac{6.0}{5} \quad \frac{4.4}{2} \quad 4.5 \quad \frac{4.3}{6} \quad \frac{5.8}{11} \quad \frac{7.7}{17} \quad \frac{7.2}{19} \quad \frac{6.5}{40}$$

$$\frac{8.6}{40} \quad \frac{8.3}{11} \quad \frac{6.0}{6} \quad \frac{5.8}{4} \quad \frac{4.2}{2} \quad 4.2 \quad \frac{4.2}{6} \quad \frac{5.2}{12} \quad \frac{7.2}{17} \quad \frac{6.8}{19} \quad \frac{6.4}{40}$$

$$\frac{8.0}{40} \quad \frac{7.6}{23} \quad \frac{8.1}{16} \quad \frac{8.0}{11} \quad \frac{6.0}{5} \quad \frac{3.8}{1} \quad 3.8 \quad \frac{3.9}{7} \quad \frac{6.0}{13} \quad \frac{6.4}{16} \quad \frac{6.3}{40}$$

$$\frac{7.1}{40} \quad \frac{6.8}{20} \quad \frac{7.6}{15} \quad \frac{6.2}{7} \quad \frac{3.0}{2} \quad 3.1 \quad \frac{3.2}{6} \quad \frac{5.7}{11} \quad \frac{6.2}{16} \quad \frac{5.6}{30} \quad \frac{5.6}{40}$$

STA 7 H.I. - ROD ELEV

923.11

2+75

2.6

920.5

3

1.8

21.3

T.P.

9.67

930.91

1.87

921.24

+50

7.4

23.5

4

5.6

25.3

+50

4.2

26.7

5

2.4

28.5

T.P.

7.25

936.55

1.61

929.30

+50

6.6

30.0

6

4.5

32.1

+50

2.3

34.3

T.P.

10.34

945.84

1.05

935.50

7

8.2

37.6

+50

4.8

41.0

T.P.

2.87

952.66

1.05

944.79

8

1.7

44.1

51.0

+50

6.3

46.4

$$\frac{4.8}{40} \quad \frac{6.4}{26} \quad \frac{7.2}{15} \quad \frac{5.8}{10} \quad \frac{2.5}{2} \quad 2.6 \quad \frac{2.5}{6} \quad \frac{3.5}{9} \quad \frac{5.2}{13} \quad \frac{5.4}{18} \quad \frac{4.8}{28} \quad \frac{5.0}{40}$$

$$\frac{3.0}{40} \quad \frac{3.0}{20} \quad \frac{3.8}{12} \quad \frac{3.6}{8} \quad \frac{1.9}{3} \quad 1.8 \quad \frac{1.7}{7} \quad \frac{3.3}{12} \quad \frac{4.0}{18} \quad \frac{3.5}{28} \quad \frac{3.8}{40}$$

$$\frac{6.0}{40} \quad \frac{6.0}{25} \quad \frac{6.7}{18} \quad \frac{7.5}{16} \quad \frac{6.2}{12} \quad \frac{6.4}{9} \quad \frac{7.8}{7} \quad 7.4 \quad \frac{8.0}{8} \quad \frac{7.4}{13} \quad \frac{8.4}{16} \quad \frac{7.8}{26} \quad \frac{8.6}{40}$$

$$\frac{2.5}{40} \quad \frac{2.8}{23} \quad \frac{3.0}{19} \quad \frac{4.0}{15} \quad \frac{3.2}{12} \quad \frac{6.1}{7} \quad 5.6 \quad \frac{6.3}{8} \quad \frac{5.8}{11} \quad \frac{7.0}{15} \quad \frac{6.5}{21} \quad \frac{7.7}{40}$$

$$\frac{1.4}{40} \quad \frac{2.8}{16} \quad \frac{2.6}{12} \quad \frac{3.4}{10} \quad \frac{4.1}{6} \quad 4.2 \quad \frac{4.8}{7} \quad \frac{7.1}{10} \quad \frac{8.1}{14} \quad \frac{7.6}{22} \quad \frac{8.8}{40}$$

$$\frac{1.0}{40} \quad \frac{1.2}{24} \quad \frac{1.6}{12} \quad \frac{1.8}{9} \quad \frac{2.6}{7} \quad 2.4 \quad \frac{2.8}{4} \quad \frac{6.2}{9} \quad \frac{8.2}{14} \quad \frac{7.6}{24} \quad \frac{8.5}{40}$$

$$\frac{5.3}{40} \quad \frac{6.3}{17} \quad \frac{6.7}{8} \quad \frac{6.6}{5} \quad 6.6 \quad \frac{7.3}{5} \quad \frac{8.7}{9} \quad \frac{10.4}{13} \quad \frac{10.9}{17} \quad \frac{11.8}{40}$$

$$\frac{3.1}{40} \quad \frac{5.1}{14} \quad \frac{5.1}{7} \quad \frac{4.8}{4} \quad 4.5 \quad \frac{5.0}{5} \quad \frac{6.2}{10} \quad \frac{7.8}{13} \quad \frac{8.0}{17} \quad \frac{7.5}{25} \quad \frac{8.0}{40}$$

$$\frac{0.0}{40} \quad \frac{2.7}{12} \quad \frac{2.3}{6} \quad \frac{2.6}{4} \quad \frac{2.2}{3} \quad 2.3 \quad \frac{2.4}{9} \quad \frac{3.3}{13} \quad \frac{3.6}{18} \quad \frac{3.5}{26} \quad \frac{3.9}{40}$$

$$\frac{6.0}{40} \quad \frac{7.3}{21} \quad \frac{8.5}{12} \quad \frac{8.6}{4} \quad \frac{8.1}{3} \quad 8.2 \quad \frac{8.5}{12} \quad \frac{9.0}{18} \quad \frac{9.2}{29} \quad \frac{9.5}{40}$$

$$\frac{1.8}{40} \quad \frac{2.8}{26} \quad \frac{4.2}{11} \quad \frac{5.1}{4} \quad \frac{4.7}{2} \quad 4.8 \quad \frac{4.7}{12} \quad \frac{5.3}{17} \quad \frac{5.5}{40}$$

$$\frac{40.5}{40} \quad \frac{0.2}{20} \quad \frac{1.1}{7} \quad \frac{1.9}{5} \quad 1.7 \quad \frac{1.6}{11} \quad \frac{2.1}{16} \quad \frac{2.3}{40}$$

$$\text{Yard} \quad \frac{4.6}{40} \quad \frac{5.5}{10} \quad \frac{6.8}{6} \quad 6.3 \quad \frac{6.4}{11} \quad \frac{7.1}{15} \quad \frac{6.9}{20} \quad \frac{7.4}{40}$$

5717 + H.I. - ROD ELEV

952.66 ✓

B.M.

3.34

949.32 ✓

9

5.2

947.5

+50

5.3

47.4

10

5.3

47.4

+50

5.1

47.6

11

4.6

48.1

+50

4.2

48.5

12

3.4

49.3

+50

3.2

49.5

13

2.4

50.3

+20³³

2.2

50.5

+50

5.4

49.3

14

5.0

47.7

B.M.

3.34

949.32 ✓

Spk in 15" B.E. 45' Lt. Sta. 9+09

$$\frac{4.4}{40} \quad \frac{4.8}{6} \quad 5.2 \quad \frac{5.6}{10} \quad \frac{6.2}{14} \quad \frac{6.6}{40}$$

$$\frac{4.7}{40} \quad \frac{5.0}{22} \quad 5.3 \quad \frac{5.9}{18} \quad \frac{6.2}{40}$$

$$\frac{5.0}{40} \quad \frac{5.1}{21} \quad 5.3 \quad \frac{5.7}{18} \quad \frac{5.7}{40}$$

$$\frac{4.8}{40} \quad \frac{5.0}{14} \quad 5.1 \quad \frac{5.0}{13} \quad \frac{5.6}{40}$$

$$\frac{5.1}{40} \quad \frac{5.0}{20} \quad 4.6 \quad \frac{4.7}{17} \quad \frac{4.7}{40}$$

$$\frac{4.9}{40} \quad \frac{4.7}{20} \quad 4.2 \quad \frac{3.9}{13} \quad \frac{3.6}{40}$$

$$\frac{4.7}{40} \quad \frac{3.9}{18} \quad 3.4 \quad \frac{3.2}{19} \quad \frac{2.9}{40}$$

$$\frac{4.2}{40} \quad \frac{3.6}{20} \quad 3.2 \quad \frac{2.6}{12} \quad \frac{2.4}{17} \quad \frac{2.3}{40}$$

$$\frac{3.9}{40} \quad \frac{3.1}{17} \quad 2.4 \quad \frac{2.0}{11} \quad \frac{1.7}{28} \quad \frac{1.7}{40}$$

$$\frac{4.1}{40} \quad \frac{3.2}{20} \quad 2.2 \quad \frac{1.8}{8} \quad \frac{1.7}{21} \quad \frac{1.2}{40}$$

3.4

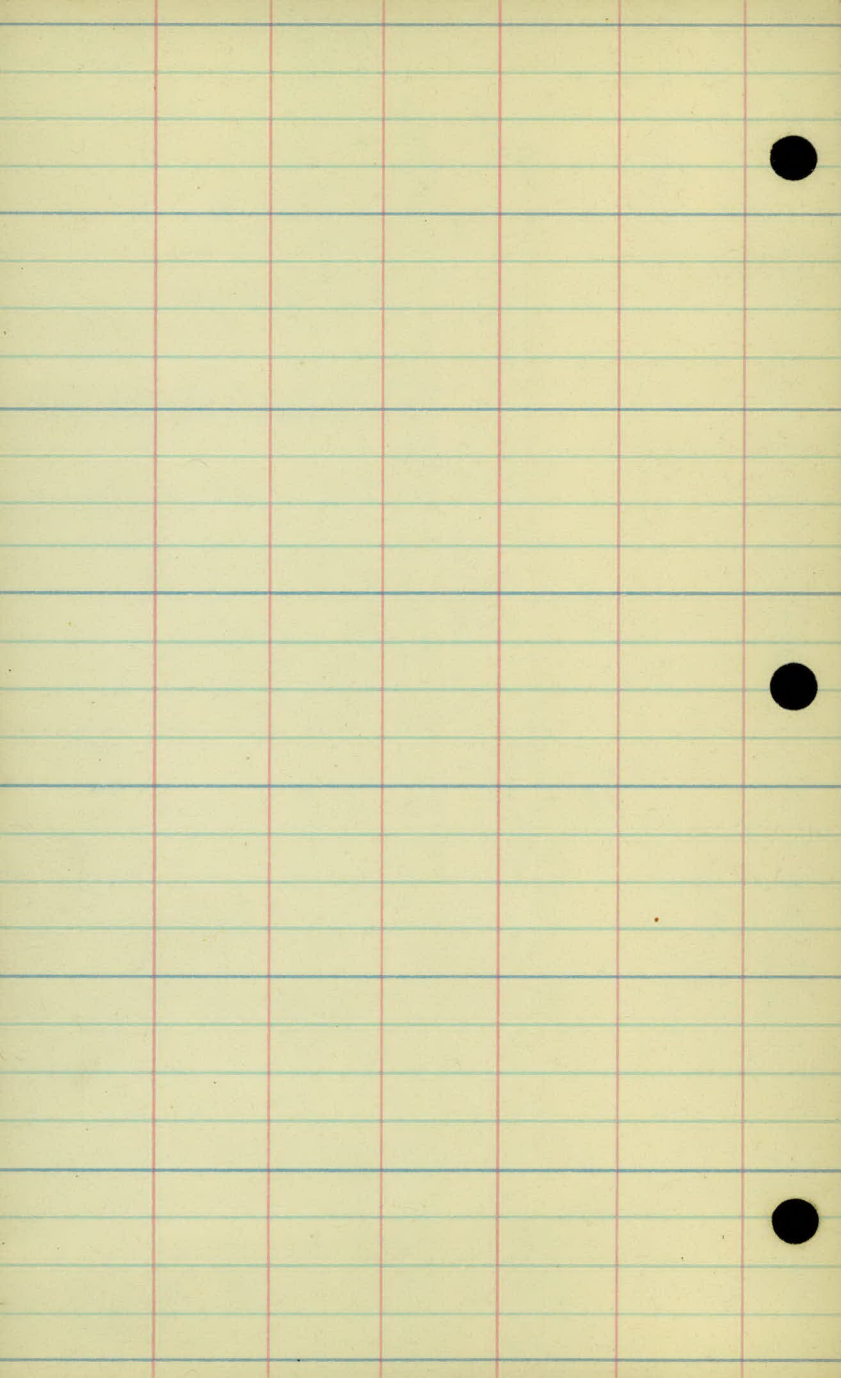
5.0

Check Levels

B.M.	1.08	950.40	✓	949.32	
T.P.	0.48	937.50	✓	13.58	936.82
"	1.39	930.71	✓	8.18	929.32
B.M.	2.57	922.61	✓	10.67	920.04
B.M.			✓	12.71	909.90
					909.93

Spk. in 15" B.E. 45' Lt. Sta. 9409

Spk. in T.P. N.E. Cor. Larp. & Dunlap
Cen. Mort. $\frac{1}{4}$ Cor. on Larp. Ave



Dunlap St.

Topog.

6

5

4

3

2

1

+28 15"X29"Vit.

0+00

+42-T.P. 6'

+88-T.P. 7'

+89-Tr. 8'

+51-T.P. 8'

+20-T.P. 9'

+91-T.P. 9'

+28-X-Drain

20' I.C.G.

Cultivated

Cultivated

14.6'

14.4'

Pavement

13

12

11

10

9

8

7

+20-Lot Iron 9.7'

Cultivated

Cultivated

+09-Tr. 24'

+88-Tr. 13'

+80-L Dr.

+69-Tr. 13'

+52-Tr. 13'

+44-House 64'

+17-L Dr. 10" X 18' C.M. 5'

+07-Tr. 13'

+95-Tr. 14' X 28'

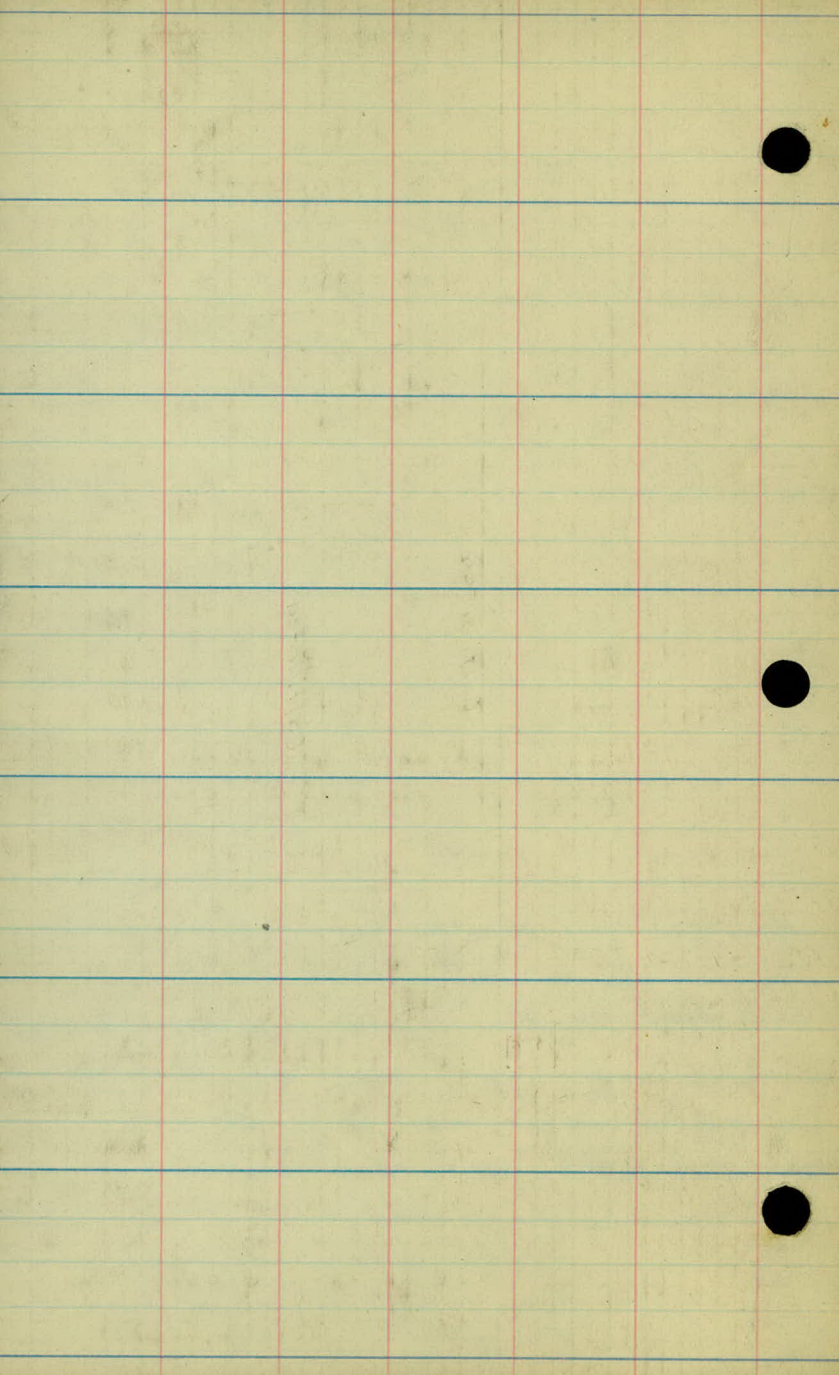
+92-Lot Iron 6'

+82-T.P. 6'

155-F
26'

Yard

Cult.



Alignment
Garden Ave

33-R26 Div B

26+24.10 & Lexington Ave

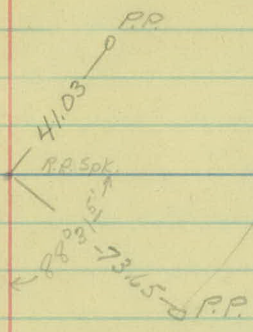
18+17.05 P.O.T. & Dunlap St.

13 12 05

30500

13+12.05 & Ferris Rd

0+00 & Hamline Ave



SE Cor Fdn.

64.60'

Spk

95.78'

S.E. Cor No 1

Ehm

32.50

Boat Spk

R.P. 11

42.17

47.17'

Iron Rd. Sq.

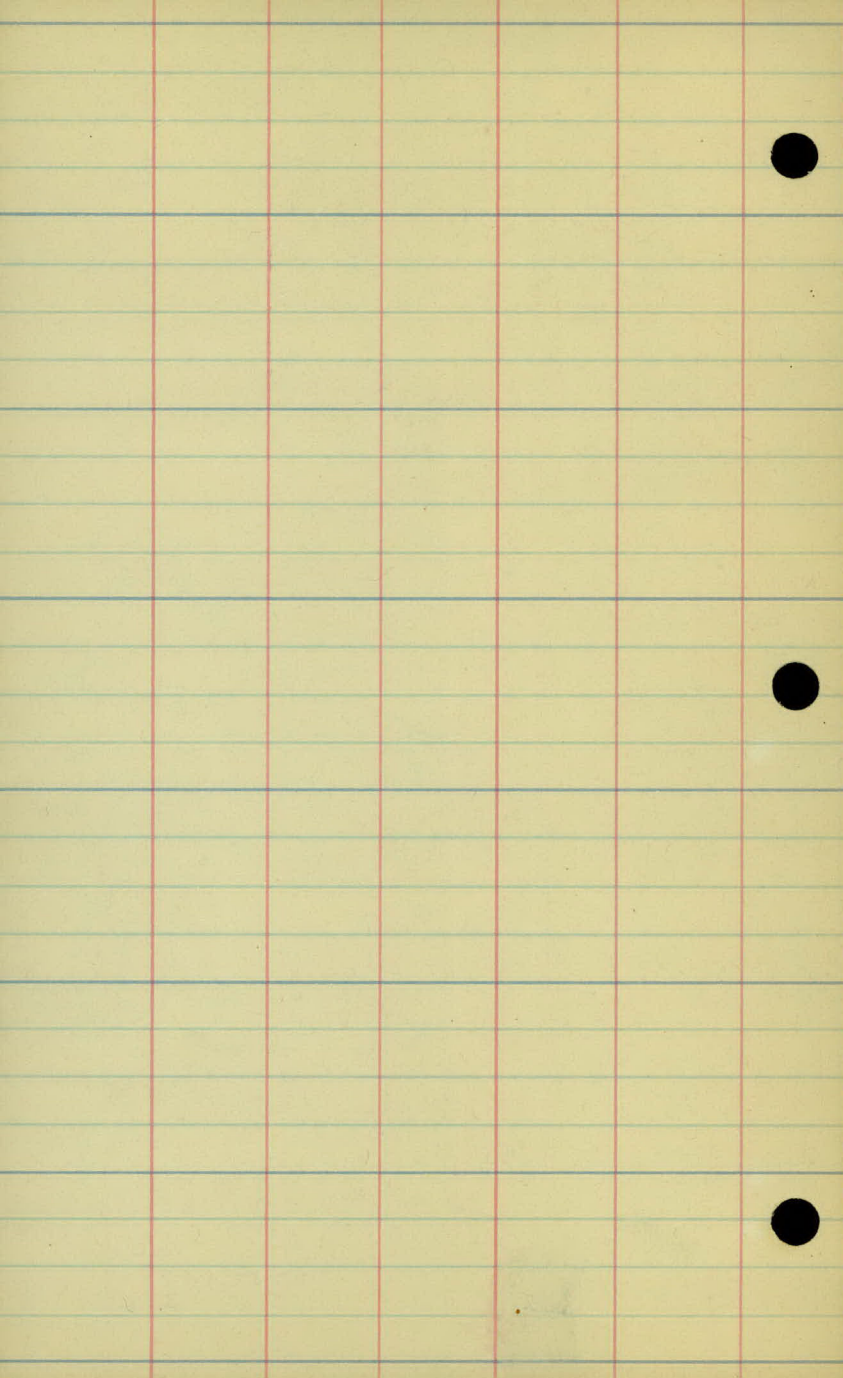
Iron

43.30

90.87' Spk

26.73

36" Maple



Topog
Garden Ave

2

1

0400

+46-£ Dr. 29'
10" X 14' C.M.

+97-F. Cor. 33'

+60-£ Ho. Ent.

+46-£ Dr.

+32-F. Cor. 33'
+25-£ Dr.

£ Garden Ave

Cultivated

+44-Tr. 38'

+19-Iron Rd. 38'
+13-12" X 40' C.M.

£ Hamline Ave

+43-Beg. Brush
a Small Trees 1'
+30-F. Cor. 1'

+27-Tr. 24'

+11-T.P. 14'

12" X 52' C.M. 19'



5



4

3



+94 - E Dr. 30'
12" X 24' C.M.

+32 - E Dr. 30'
12" X 16' C.M.

+97 - E Dr. 30'
12" X 18' C.M.

+62 - 12" X 28' C.M. 1'

+94 - E Dr. 30'
10" X 14' C.M.
+85 - F. Cor. 33'

+29 - F. Int. 33'

+74 - E Dr. 29'
10" X 14' C.M.

+64 - F. Cor. 33'

+53 - Reg. Trees 1'

Uncultivated

+90 - End. Brush +
Small Trees 1'

Cultivated

9



8



7



6

+39-4 Ho. Ent.

+25-4 Dr. 30'
10" X 14' C.M.

+55-6 Ho. Ent.

+60-4 Dr. 30'
14' Metal Pipe

+97-4 Dr. 31'
12" X 20' C.M.

+30-4 Dr. 31'
12" X 12' C.M.

+12-4 Dr. 31'
12" X 16' C.M.

+83-End Treas 1'

Uncultivated

12

11

10

Trail

+80 - End of Yards

+75 - Dr.

+84 - E Ho. Ent.

+56 - E Dr. 31'
Metal Pipe

+49 - End Wall 33'

+40 - E Dr. 30'

10" K14" C.M.

+07 - E Ho. Ent. 29'

5' Metal Pipe

+85 - Stone Wall 33'

Garden Ave

Uncultivated

19

18

17

16

15

14

13

Cultivated

x x x x 108-F. Cor. 1'

26

25

24

23

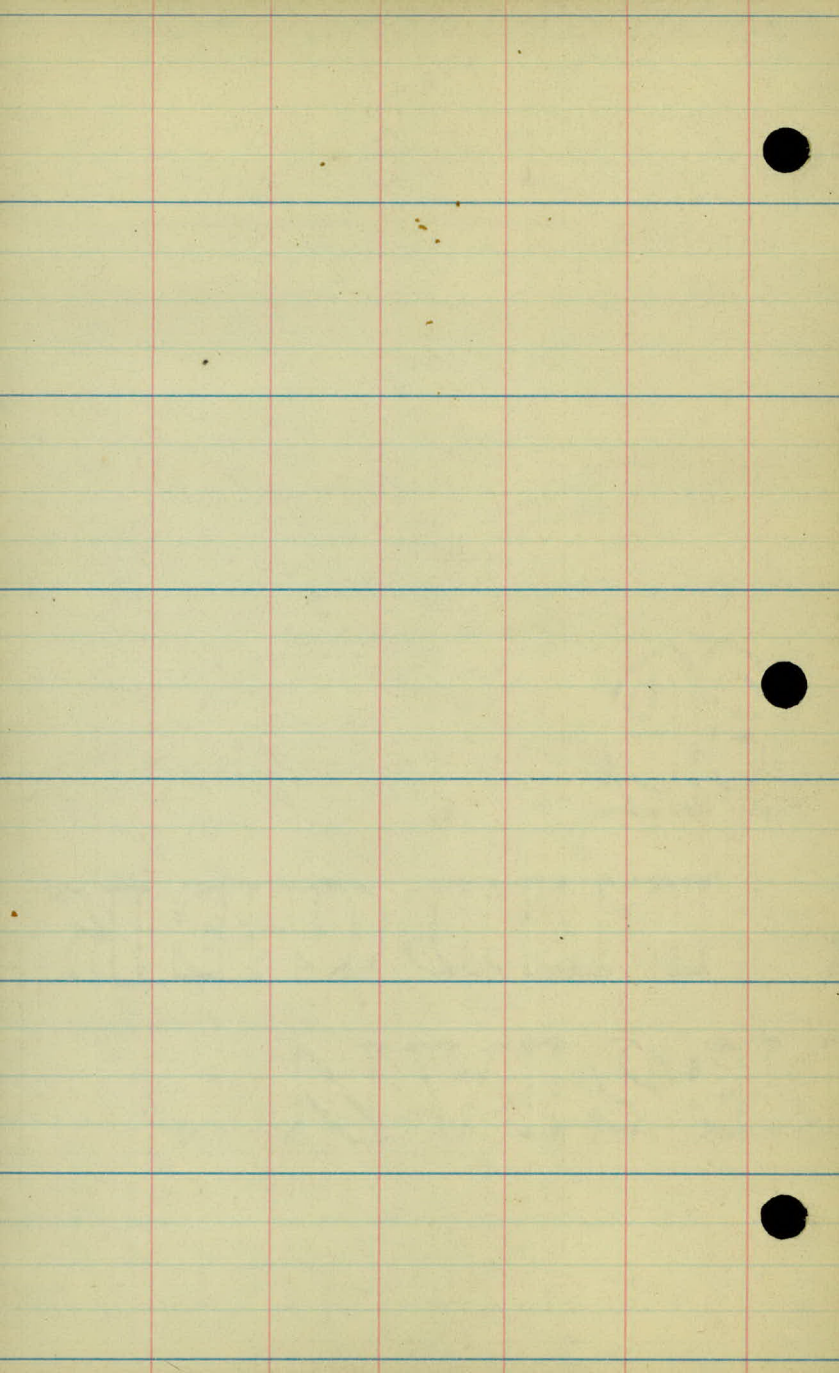
22

21

20

+24.10 - / 27 / Flamingo / 114 Lexington Ave

cultivated



X-Sections

Garden Ave

B.M.	4.53	948.11 ✓	943.58
0+00	& Hamline Ave		42.8
+13			41.9
+17			42.2
+24			42.2
+35			42.9
+75			44.8
1			45.1
+50			44.2
2			44.0
+50			41.7
3			38.8
T.P.	1.03	937.05 ✓	12.09 936.02 ✓
+50			34.3
4			30.6

Spk. in 36" Maple 0-27

5.2	5.4
50	50

6.0	5.7	5.5	5.2	5.3	5.9	6.1	6.3	6.3
50	32	25	16	8	42	8	14	37

Flow Line					Flow Line X-Drain				
6.8	6.9	5.8	5.6	5.1	5.4	7.6	7.5	6.8	7.3
50	34	31	26	16	8	6	14	23	38

5.1	5.6	5.6	5.0	5.4	6.7	7.1	7.4	8.7
50	33	26	16	8	5.9	5	14	23

4.7	5.1	5.4	5.1	4.9	5.3	5.5	5.9	5.5	5.5	6.0	7.1
50	38	29	25	16	8	5	2	5.2	6	17	29

4.3	4.2	4.7	4.6	4.5	4.3	4.9	5.1	5.4	3.3	3.3	3.2	4.2
40	34	32	29	24	16	7	5	3	1	3.3	9	20

4.0	4.0	5.2	4.8	4.7	4.4	4.9	5.0	4.7	3.0	3.2	3.3	3.5	4.1
40	33	31	28	23	17	8	5	3	1	3.0	5	8	33

3.3	3.5	4.5	5.1	5.2	4.9	5.2	5.1	4.9	3.7	4.5	5.3
40	33	32	28	24	17	9	5	3	3.9	4	19

3.4	3.4	5.0	6.8	6.9	6.1	5.9	6.3	6.5	6.7	4.5	5.2	5.9	7.1
40	33	33	30	29	27	16	9	5	3	4.1	4	11	23

4.3	4.1	7.0	8.2	8.2	8.5	8.9	8.4	6.2	7.0	7.8	8.8
40	33	33	30	17	8	5	2	6.4	2	5	17

7.6	7.6	10.4	10.6	10.3	10.2	10.8	10.8	9.2	10.8	12.1	13.3
40	33	31	29	25	17	8	4	9.3	2	7	22

0.7	1.2	2.0	2.0	1.7	2.5	4.6	5.7	7.2
40	33	31	28	19	9	2.8	6	17

4.2	4.3	3.8	3.6	4.3	5.9	8.0	9.1	10.1
40	32	28	19	8	4	6.5	4	16

937.05 ✓

4+50

29.6

H62

X-Drain

5

30.1

+50

30.5

6

30.5

+50

30.7

7

30.6

+50

31.3

8

32.6

+50

33.8

9

34.0 ✓

B.M.

8.58

✓
944.97

0.64

936.41

936.39

+50

34.6

10

35.8

6.3	6.3	4.9	4.8	5.4	7.1		9.1	9.8	10.7
40	31	27	18	8	3	7.5	4	15	40

7.5	8.4
29	1

4.9	5.9	5.9	5.2	5.4	6.1	7.7	7.7		7.5	8.3	8.9	9.9
40	32	29	27	18	8	5	2	7.0	3	5	17	40

4.9	5.6	6.1	5.8	5.6	6.5	7.3	7.5	6.6		7.1	7.6	8.3	9.4
40	33	31	29	18	7	5	4	2	6.6	4	6	20	40

4.9	5.6	5.6	6.5	7.5	7.6		7.5	8.3	8.5	8.1
40	27	17	8	4	2	6.6	12	24	31	40

5.6	6.4	6.2	5.8	5.8	6.6	7.3	7.4		6.6	7.3	7.5	7.2
40	30	28	26	17	6	4	2	6.4	3	6	23	40

5.7	6.0	6.5	6.1	5.9	5.6	6.4	7.3	7.3	6.6		6.5	7.1	7.0	7.0
40	33	31	29	27	17	7	4	2	1	6.5	3	9	23	40

5.3	5.4	6.0	5.7	5.0	6.1	6.7	6.9	5.8		6.0	6.5	6.5	6.5
40	33	31	27	17	6	4	2	1	5.8	4	10	30	40

4.2	4.8	4.3	4.4	5.5	6.0	4.5		4.5	5.2	5.6	5.8
40	27	17	7	5	3	1	4.5	4	11	26	40

3.2	3.4	4.1	3.8	3.4	4.1	4.9	4.9	3.3		3.3	4.3	4.5
40	32	29	26	17	5	4	2	1	3.3	3	16	40

3.0	3.1	3.7	3.3	3.1	3.5	3.6	3.1		2.9	3.7	3.7
40	32	30	28	17	7	4	2	3.1	3	16	40

S.W. Cor. Stone Wall 33' Lt. 9+85

10.2	10.4	10.3	10.9	10.7	10.9	11.1	10.6		10.5	10.9	10.9	10.8
40	34	30	26	17	6	4	2	10.4	5	11	23	40

8.4	8.4	9.5	10.1	9.6	9.5	9.9	9.2		9.0	9.3	9.3
40	33	33	29	27	16	3	2	9.2	6	20	40

✓
944.97

10+50

38.0

11

39.3

+50

40.4

12

41.7

+50

41.8

13

41.3

+50

41.5

14

42.2

T.P.

2.70

✓
950.97

1.70

943.27 ✓

+50

43.0

15

43.2

+50

42.9

16

42.7

+35

42.8

$$\begin{array}{r} 8.4 \quad 7.8 \quad 8.6 \quad 9.0 \quad 8.6 \quad 7.8 \quad 8.4 \quad 8.0 \quad 7.2 \\ 40 \quad 33 \quad 33 \quad 30 \quad 26 \quad 16 \quad 5 \quad 3 \quad 2 \end{array} \quad \begin{array}{r} 6.8 \quad 7.2 \quad 7.5 \quad 6.9 \\ 4 \quad 14 \quad 26 \quad 40 \end{array}$$

$$\begin{array}{r} 7.1 \quad 7.1 \quad 7.8 \quad 7.8 \quad 7.1 \quad 7.2 \quad 6.9 \\ 40 \quad 37 \quad 31 \quad 25 \quad 16 \quad 6 \quad 2 \end{array} \quad \begin{array}{r} 5.2 \quad 5.8 \quad 4.8 \\ 2 \quad 13 \quad 40 \end{array}$$

$$\begin{array}{r} 6.7 \quad 7.2 \quad 6.9 \quad 6.3 \quad 6.2 \quad 5.6 \\ 40 \quad 31 \quad 25 \quad 16 \quad 6 \quad 3 \end{array} \quad \begin{array}{r} 4.1 \quad 4.3 \quad 4.3 \quad 3.4 \\ 5 \quad 11 \quad 21 \quad 40 \end{array}$$

$$\begin{array}{r} 6.8 \quad 6.7 \quad 6.3 \quad 5.9 \quad 5.0 \quad 5.0 \quad 4.4 \quad 3.3 \\ 40 \quad 31 \quad 28 \quad 26 \quad 16 \quad 6 \quad 3 \quad 1 \end{array} \quad \begin{array}{r} 2.6 \quad 2.8 \quad 2.5 \quad 1.8 \\ 2 \quad 13 \quad 26 \quad 40 \end{array}$$

$$\begin{array}{r} 6.7 \quad 5.5 \quad 4.5 \quad 4.3 \quad 4.3 \quad 3.3 \\ 40 \quad 26 \quad 16 \quad 7 \quad 4 \quad 2 \end{array} \quad \begin{array}{r} 2.8 \quad 2.4 \quad 1.9 \\ 6 \quad 24 \quad 40 \end{array}$$

$$\begin{array}{r} 6.7 \quad 6.0 \quad 4.8 \\ 40 \quad 26 \quad 11 \end{array} \quad \begin{array}{r} 3.7 \quad 3.3 \quad 2.7 \quad 1.6 \\ 2 \quad 19 \quad 40 \end{array}$$

$$\begin{array}{r} 6.0 \quad 4.8 \quad 4.7 \\ 40 \quad 27 \quad 20 \end{array} \quad \begin{array}{r} 2.2 \quad 1.1 \\ 21 \quad 40 \end{array}$$

$$\begin{array}{r} 4.9 \quad 3.3 \quad 2.6 \\ 40 \quad 25 \quad 9 \end{array} \quad \begin{array}{r} 1.2 \quad 0.1 \\ 22 \quad 40 \end{array}$$

$$\begin{array}{r} 9.8 \quad 8.4 \quad 7.7 \\ 40 \quad 26 \quad 9 \end{array} \quad \begin{array}{r} 6.7 \quad 5.7 \\ 20 \quad 40 \end{array}$$

$$\begin{array}{r} 9.9 \quad 8.4 \quad 7.6 \\ 40 \quad 20 \quad 7 \end{array} \quad \begin{array}{r} 6.3 \quad 5.3 \\ 20 \quad 40 \end{array}$$

$$\begin{array}{r} 10.1 \quad 8.9 \quad 8.1 \\ 40 \quad 20 \quad 9 \end{array} \quad \begin{array}{r} 6.4 \quad 5.4 \\ 20 \quad 40 \end{array}$$

$$\begin{array}{r} 10.7 \quad 9.4 \quad 8.6 \\ 40 \quad 25 \quad 10 \end{array} \quad \begin{array}{r} 6.7 \quad 5.8 \\ 20 \quad 40 \end{array}$$

$$\begin{array}{r} 10.6 \quad 10.0 \\ 40 \quad 20 \end{array} \quad \begin{array}{r} 7.7 \quad 7.3 \\ 20 \quad 40 \end{array}$$

950.97 ✓

16 + 50

43.5

17

45.4

+ 50

47.7

18

49.5 ✓

T.P.

6.63

957.19 ✓

0.41

950.56

+ 50

51.1 ✓

B.M.

7.88

949.31

949.32

19

51.7

+ 50

51.9

20

51.0

+ 50

51.7

21

51.1

+ 50

50.3

22

48.8

+ 50

45.2 ✓

T.P.

1.52

951.17 ✓

7.54

949.65

$$\frac{10.8}{40} \quad \frac{10.0}{25} \quad \frac{8.7}{11} \quad 7.5 \quad \frac{7.0}{20} \quad \frac{6.5}{40}$$

$$\frac{9.2}{40} \quad \frac{7.2}{20} \quad \frac{5.5}{4} \quad 5.6 \quad \frac{5.8}{3} \quad \frac{5.1}{15} \quad \frac{4.8}{40}$$

$$\frac{6.2}{40} \quad \frac{5.1}{20} \quad \frac{3.5}{4} \quad 3.3 \quad \frac{3.7}{2} \quad \frac{3.1}{20} \quad \frac{3.1}{40}$$

$$\frac{2.9}{40} \quad \frac{2.3}{20} \quad \frac{1.2}{4} \quad 1.5 \quad \frac{1.8}{3} \quad \frac{1.4}{20} \quad \frac{1.4}{40}$$

Top Stake 18+00

$$\frac{6.6}{40} \quad \frac{6.0}{20} \quad 6.1 \quad \frac{6.2}{20} \quad \frac{6.5}{40}$$

Spk. in 12" B.F. 400' R.L. 17+70

$$\frac{5.7}{40} \quad \frac{5.3}{20} \quad 5.5 \quad \frac{5.6}{20} \quad \frac{5.7}{40}$$

$$\frac{5.6}{40} \quad \frac{5.2}{20} \quad 5.3 \quad \frac{5.3}{20} \quad \frac{5.6}{40}$$

$$\frac{5.1}{40} \quad \frac{4.7}{20} \quad 6.2 \quad \frac{5.4}{20} \quad \frac{5.9}{40}$$

$$\frac{4.9}{40} \quad \frac{4.8}{20} \quad 5.5 \quad \frac{5.8}{20} \quad \frac{6.2}{40}$$

$$\frac{5.2}{40} \quad \frac{5.4}{20} \quad 6.1 \quad \frac{6.6}{20} \quad \frac{7.0}{40}$$

$$\frac{5.8}{40} \quad \frac{6.1}{20} \quad 6.9 \quad \frac{7.6}{20} \quad \frac{8.4}{40}$$

$$\frac{7.3}{40} \quad \frac{7.6}{20} \quad 8.4 \quad \frac{9.4}{20} \quad \frac{10.4}{40}$$

$$\frac{9.4}{40} \quad \frac{10.1}{20} \quad 12.8 \quad \frac{12.6}{20} \quad \frac{13.9}{40}$$

951.17

23 42.7

+50 41.1

+70 40.9

24 42.0

+50 44.0

25 45.2

+50 45.6

+92 44.8

26 42.8

+03 42.8

+07 44.3

+24.1 2 Lexington Ave 44.7

B.M. 11.37 939.80 939.82

$$\frac{6.0}{40} \quad \frac{6.8}{20} \quad \frac{7.8}{2} \quad 8.5 \quad \frac{9.6}{20} \quad \frac{10.5}{40}$$

$$\frac{7.7}{40} \quad \frac{8.3}{26} \quad \frac{9.5}{2} \quad 10.1 \quad \frac{11.3}{20} \quad \frac{12.1}{40}$$

$$\frac{7.8}{40} \quad \frac{8.1}{23} \quad \frac{9.5}{5} \quad 10.3 \quad \frac{11.1}{20} \quad \frac{12.1}{40}$$

$$\frac{6.8}{40} \quad \frac{7.1}{24} \quad \frac{7.6}{13} \quad 9.2 \quad \frac{10.1}{20} \quad \frac{11.2}{40}$$

$$\frac{5.1}{40} \quad \frac{5.3}{28} \quad \frac{5.4}{15} \quad \frac{6.0}{8} \quad 7.2 \quad \frac{8.2}{20} \quad \frac{9.8}{40}$$

$$\frac{3.7}{40} \quad \frac{4.3}{12} \quad \frac{5.0}{6} \quad 6.0 \quad \frac{7.1}{20} \quad \frac{8.3}{40}$$

$$\frac{3.3}{40} \quad \frac{4.0}{12} \quad \frac{4.7}{6} \quad 5.6 \quad \frac{6.4}{20} \quad \frac{7.8}{40}$$

$$\frac{3.5}{40} \quad \frac{4.3}{12} \quad \frac{4.9}{5} \quad 6.4 \quad \frac{7.2}{20} \quad \frac{8.1}{40}$$

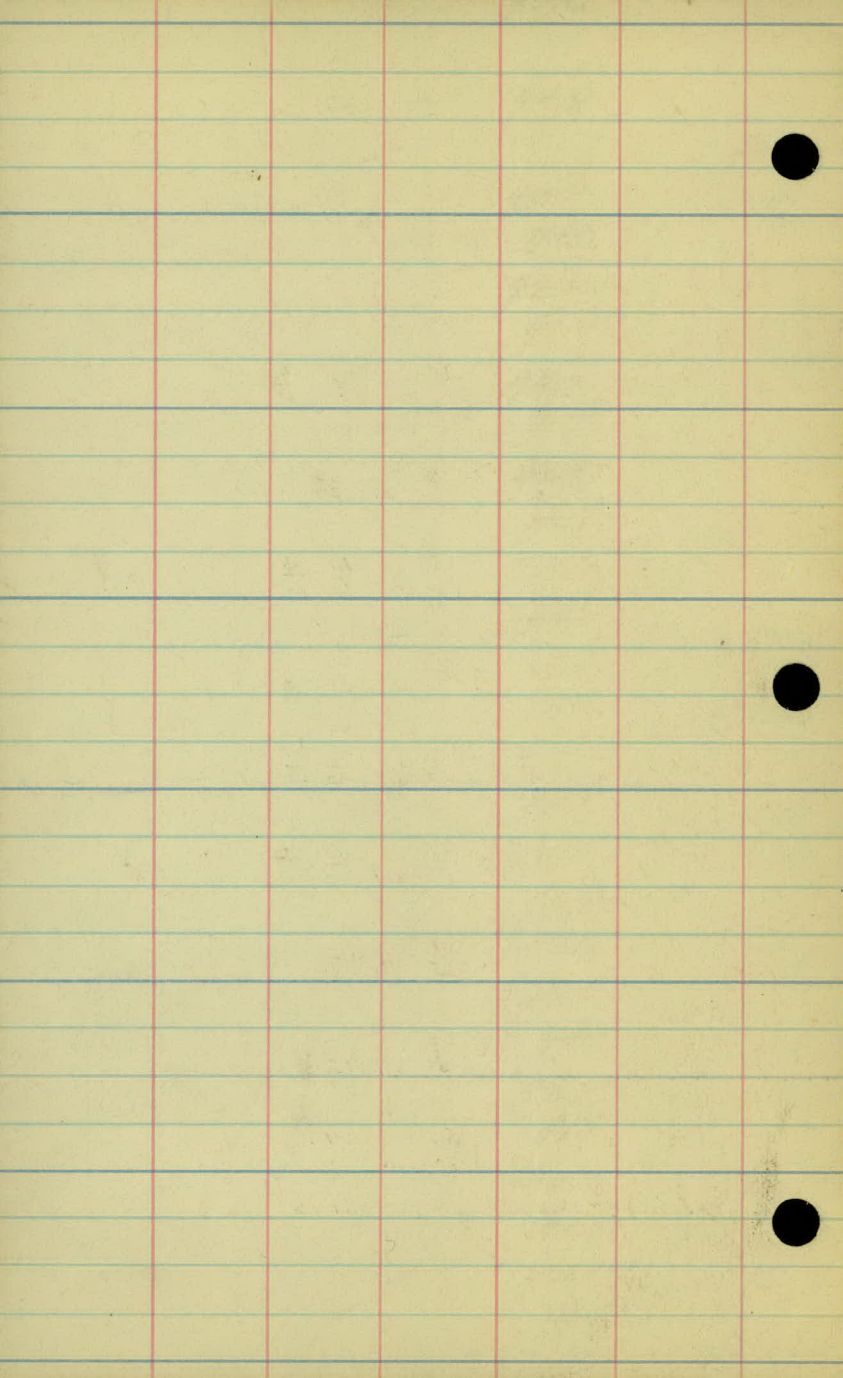
$$\frac{8.0}{50} \quad \frac{8.4}{25} \quad 8.4 \quad \frac{9.3}{25} \quad \frac{10.2}{50}$$

$$\frac{8.0}{50} \quad \frac{8.4}{25} \quad 8.4 \quad \frac{9.3}{25} \quad \frac{10.2}{50}$$

$$\frac{5.5}{50} \quad \frac{6.2}{25} \quad 6.9 \quad \frac{7.8}{25} \quad \frac{8.5}{50}$$

$$\frac{5.3}{50} \quad 6.5 \quad \frac{7.9}{50}$$

Spt. in 12" Maple 100' RT 25+70



Check Levels
Garden Ave

B.M.	2.25	951.57		949.32	
T.P.	1.58	944.85	8.30	943.27	
B.M.	1.00	937.38	8.47	936.38	
T.P.	13.01	945.51	4.88	932.50	
B.M.			1.93	943.58	
T.P.	4.91	937.41	13.01	932.50	
B.M.	8.46	944.85	1.02	936.39	936.38
T.P.	6.44	949.72	1.57	943.28	
"	8.25	956.71	1.26	948.46	
"	1.97	948.11	10.57	946.14	
B.M.			8.29	939.82	
T.P.	7.44	953.38	2.17	945.94	
B.M.			4.04	949.34	949.32

Spk. in B.E. on Dunlap St.

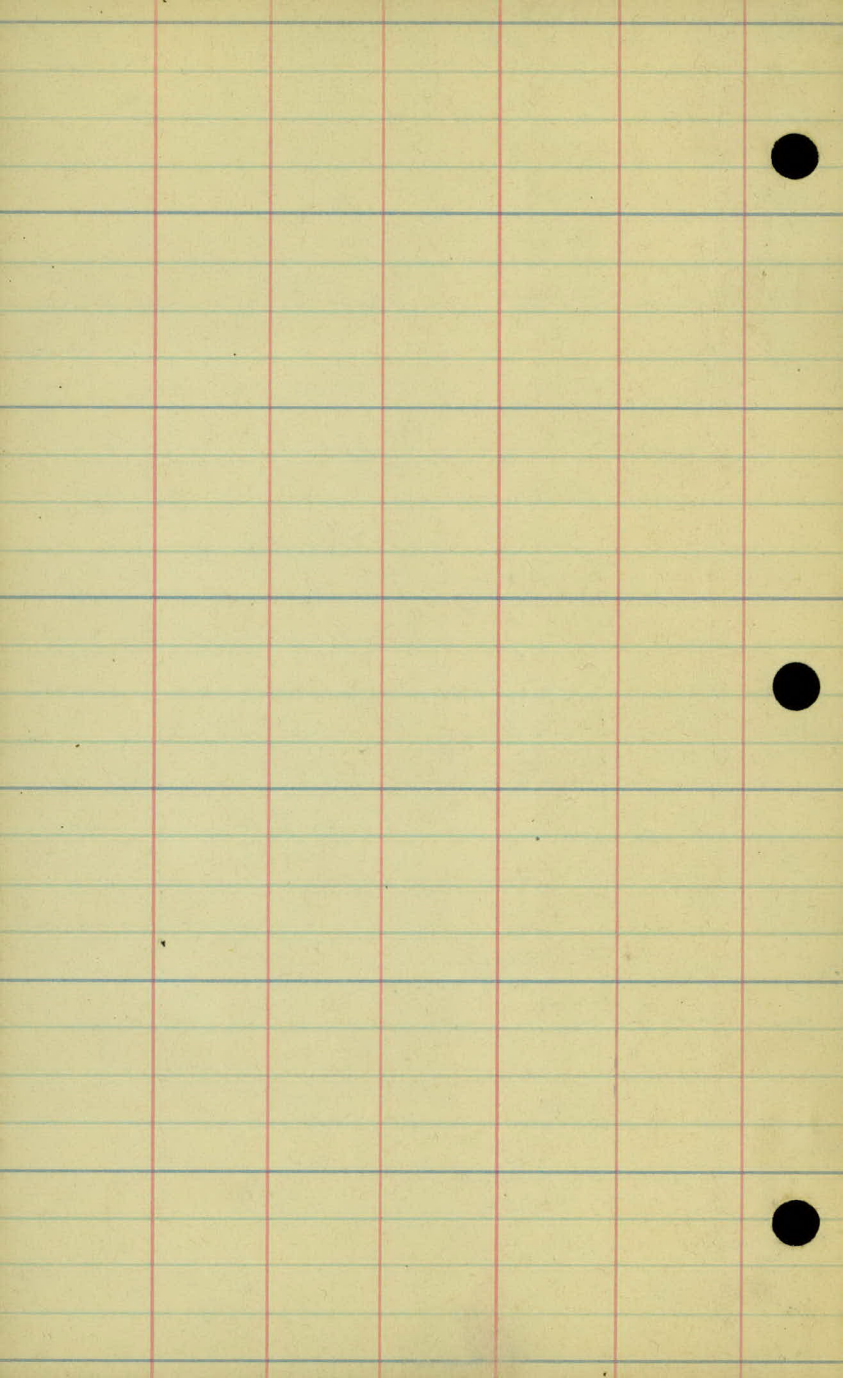
S.W. Cor. Stone Wall 33' Lt 9+85

Spk. in 36" Maple 0-27

S.W. Cor. Stone Wall 33' Lt 9+85

Spk. in 12" Maple 100' Rt 25+70

Spk. in B.E. on Dunlap St.



Proj: 33-R26B

- 0+17 Reint. Pl. 15" X 44 C.M.
- X 1+25 Lt. No colv. reg
- X 1+46 Lt - Rep. 12" X 20' C.M.
- X 1+60 Lt " 12" X 20' C.M.
- X 2+46 Lt Reint - Pl. 12" X 20' C.M.
- X 2+74 Lt " "
- X 3+94 Lt " Rep. "
- X 4+62 - Reint - Pl. 18" X 36 P3
- X 0+00 - 4+00 Cl. 35 Gr. 45
- X 4+97 Lt - Reint + Reint
- X 5+32 Lt - " "
- X 5+94 Lt " "
- X 7+12 Lt " " with 15" (7+12)
- X 7+30 Lt Reint & Rep. Ext 8' 16"
- X 7+97 Lt " "
- X 8+60 Lt " Pl. 12" X 20
- X 9+25 Lt " Pl. 12" X 20' C.M.
- X 9+85 Lt " Pl. 12" X 20' C.M.
- X 10+07 Lt " Pl. 12" X 20
- X 10+40 Lt " Pl. 12" X 20
- X 10+56 Lt " "
- X 9+38 Lt Pl. 12" X 20' C.M.
- X 10+84 Lt No colv. reg
- X 11+75 Lt " " "
- X 1+00 Rt No colv. reg
- 10+00 Rt Pl. 12" X 20 C.M.

X 5+00 - 9+00 Cl. 38 Gr. 29
X 13+00 Lt. No. 10/11, 15/9
X 19+50 Lt. " " "
X 15+00 Rt Pl. 12" X 20' C.M.
X 22+00 Rt Pl. 12" X 20' C.M.
X 23+70 Pl. 24" X P3
26+03 Pl. 18" X P3 48'