

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Road Map Survey

CO. RD. F

From Bellaire Ave To E. Co. Line

Road Acc't. No. 56

Date Filed 4-7-27

File

Plan Survey
Co Rd "F"
From Bellair to East Coline

HAW

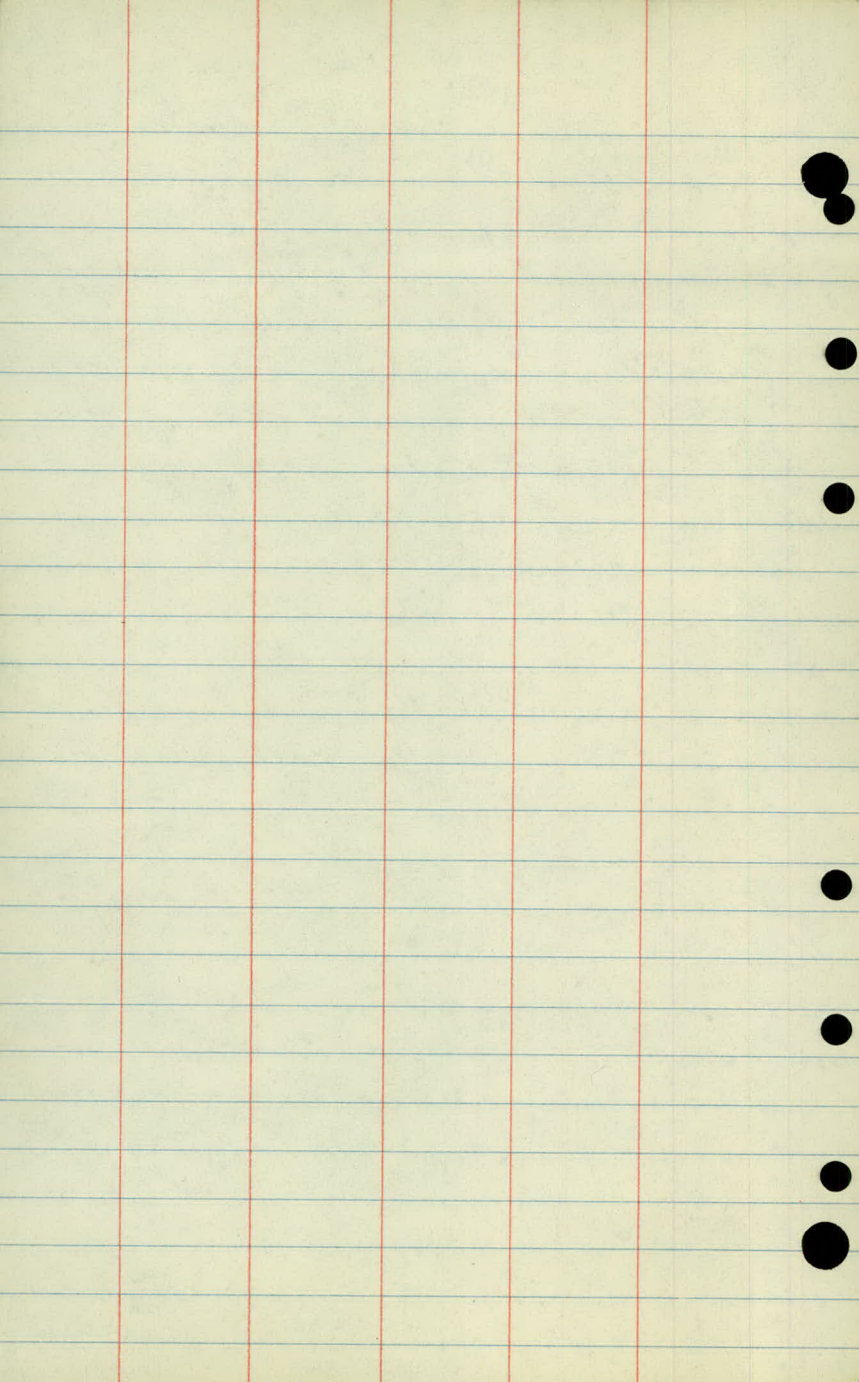
9-20-43

HAW

AM

L.C

Index	Pages
Align	2 to 4
Topography	4 to 9
X Sections	9 to 15



Align

Sta	Point	Alt	ARt
-----	-------	-----	-----

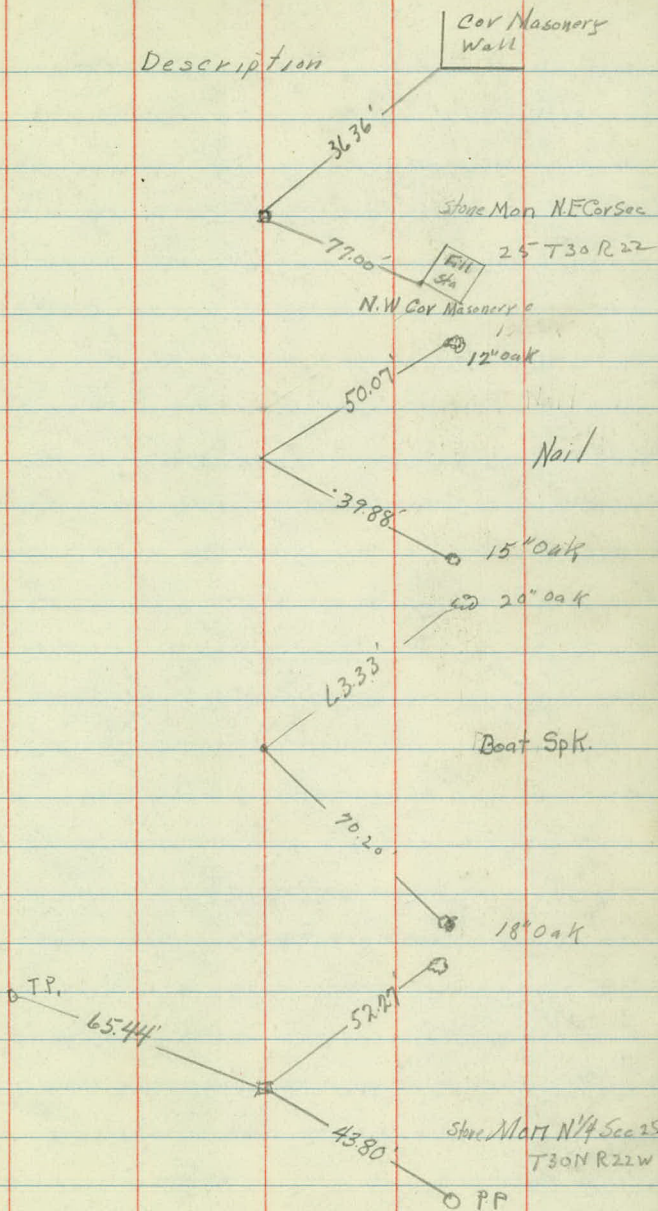
26+30.57	= E East Co Linn		
----------	-----------------------------	--	--

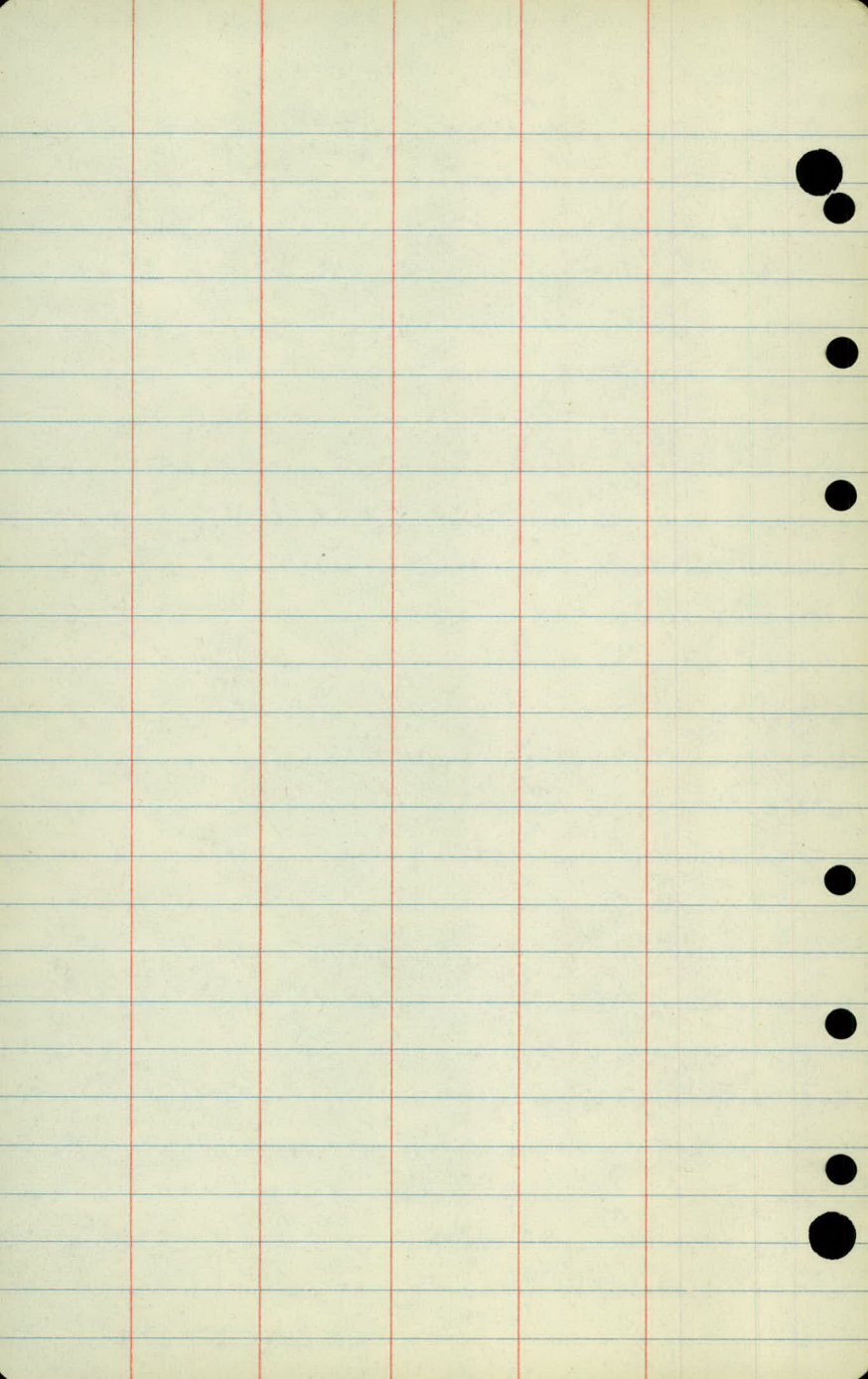
10+00	P.O.T.		
-------	--------	--	--

3+72.68	P.O.T.		
---------	--------	--	--

0+00	= E Bellair		
------	------------------------	--	--

Description





TOPOGRAPHY

Co Rd "F"

FROM Bellair To East Co Line

9-18-43

HAW

AM

LG1

6 Kd 12' Kb 13'

5 10' 12'

4 10' 12'

3 11 12'

+99.5 ft 82'

2 9' 12'

1 10' 12'

0 21' +32 x Drain 24" x 19

+105 Sta 33'
Brush 29'

+27 10" Oak 34'
Fe 33'

Brush 33'

Woods & Brush

+30 24" Oak 31'

Fe 31'

+90 Sta 22'

+51 Pop 30'

+10 10" Oak 34'

+00 10" Oak 34'
Fe 34

Brush 28'
+82 Sta 34'
+79 Sta 29'
+70 Sta 29'

Cultivated

+82 Sta 31

+68 36" Oak 31'

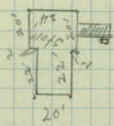
+46 Sta 31'

+28 Oak 31'

+51 Sta 35'
+50 Beg Wooded Brush 28'

+103 12" Oak 32'
Fe 32

+68 Can 9' Cone slab 23'
+64 Can Gas Pump 25'
+37 S.W. Coy Store 41'



+18 Sta 22'
+10 End Garden
+02 10" Oak 29'

+84 Sta 30'
+67 12" Oak 32'

+54 Sta 31'

+42 10" Oak 31'

+41 Sta 31'

+29 PP 33'

+25 Sta 32'
Fe 33

+92 24" Oak 29

Woods

Garden

+63 12" Oak 37'
+62 12" Oak Beg Fe 36

+49 End Rad 11'

+40 26" Oak 36

+47 End Rad 9

+33 Beg Garden

+08 Beg Rad 51

+25 TP 36
+10 Beg Rad 49

13 R_d R_d
12' 14'

12 12' 14'

11 11' 14'

10 11' 13'

9 11' 13'

8 9' 14'

7 10' 14'

6 12' 13'

Brush 28

Fe 39

6

Brush

+91 12" Tw oak 38'
 +77 12" Oak 34'
 +66 8" Oak 36'
 +56 18" Oak 35'

Fe 36'

+94 15" Oak 36'
 +93 12" Oak 34'
 +71 Tw 8" Oak 36'
 +54 Tw 10" Oak 35'
 +19 12" Oak 36'
 Fe 34'

+90 10" Oak 34'
 +85 6" Oak 33'

+56 10" Oak 34'
 +41 10" Oak 33'
 Fe 35'

+95 6" Oak 33'
 +94 6" Oak 34'
 +75 10" Oak 32'

+33 15" Oak 33'
 +22 10" Oak 35'
 +03 Bag Fe 12" Oak 32'

Brush 28

+75 End 12" CM 15'

+59 Bag 12" x 16" CM 15'

+48 Retic Ent

Brush 29'

Brush 29'

Woods & Brush

Brush 26'

Cultivated

+10 Bag Woods & Brush 25

+15 Field Ent

+67 End Fe 35'
 +35 10" Oak 26'
 +23 15" Elm 31'
 +05 24" Oak 29'

Fe 36'

+79 10" Oak 35'
 +75 8" Oak 35'
 +58 Tw oak 38'
 +51 Oak 31'

Uncult.

+41 Can 14' Rd.

+24 End Brush

Brush 24'

Fe 34'

20

Rd Kb
11 14

19

10' 13'

18

400 10" X 7 V. / A Drain 29
10 13

17

12' 14'

16

10' 13

15

13' 15'

14

15' 14'

13

12 14

Fe 28 SWP 31

Fe 34 Woods 7

+7 Twin Will 27'
SWP 18'-120'
Fe 24

Woods

+73 Fe Cor 33'
+40 10" Will 32'

+29 30" Pop 50'
+24 36" Pop 34'

Fe 36 End SWP 41'-80'

SWP 15'-95' Fe 25'

Fe 37 SWP 22'-80'

+25 Beg Path 1/2 c 18'-30'
+25 Beg Fe 25'
+00 End 15" CM 17'
+90 Ent
+85 Rgt 1/2 Ent
+80 Beg 15" x 20" CM 17'
+79 End Fe 25'

Uncultivated

Woods

Fe 37 SWP 23'-80'

Fe 25

Swamp
path hole

Fe 37 SWP 19'-130'

+75 Rgt 1/2 Fe
+36 Fe Cor 24'
+10 End Brush
Brush 28'

Fe 37 SWP 37'-200'

+18 Ent
Brush 30

Brush Woods

+50 SWP 55'-200'
+39 Rgt 1/2 Fe
+22 Δ Fe 40
+20 Beg SWP 90'-150'
+03 6" Oak 33
Fe 46
+71 Fe Cor 47' 17"
+85 6" Oak 35'
+67 Can Group 70' Oak 46
+49 18" Oak 29
+40 15" Oak 36'
+20 18" Oak 35'
+08 TW 8" Oak 35'
Fe 39'

Brush 28

27

Rd

Rd

106

+ 11 X Drain 15" Conc 206'

100'

26

+ 98 Q. Hedge 48'
 + 95 G.P. 39'

+ 99 Con 3' Conc Bass
 215 standard 3

+ 94 Con 3' Conc Island 47'
 + 84 Con 3' Conc Island 37'

25

5' 15'

24

9' 14'

23

12' 9'

22

12' 12'

21

11' 11'

+ 88 8" Oak 28'

20

11 14

+14 End Rad 50'
 +88 Beg Rad 21'
 +90 Δ Hedge 37'
 +54 End Fe 29'
 +30 Hedge 37'
 +56 Δ Hedge 35'
 +44 End 3 Rows Pop 33'
 Fe 20 Pop 23'-35'
 +00 Hedge 35'-70'

+61 Beg Hedge 26'
 +64 Beg 3 Rows 6" Pop 22'-34'
 +56 Beg Wood Fe 14
 +54 12" Oak 14

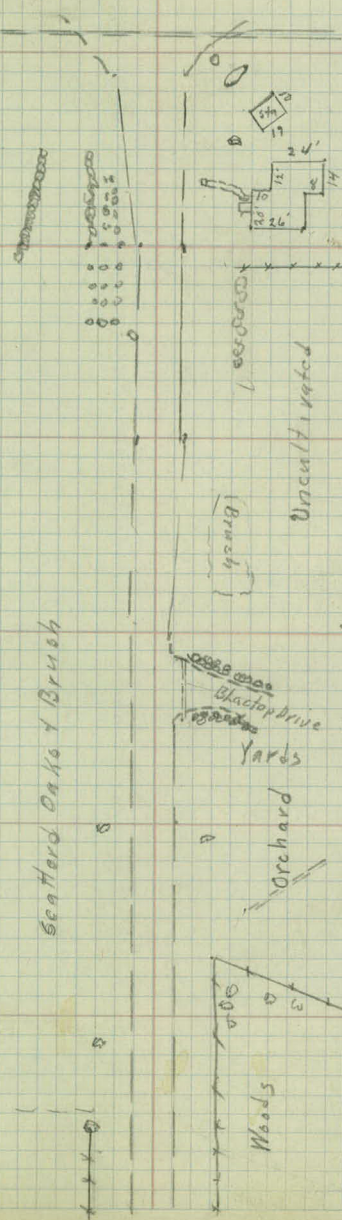
+98 15" Oak 15'
 +75 8" Oak 30'
 +71 6" Oak 24'

+17 10" Oak 25'

+93 8" Oak 33'

+99 8" Oak 29'

+50 Beg Woods
 +44 End Swp 124" CM 134'
 +41 12" Oak End Fe 34



+14 End Rad 50'
 +88 Beg Rad 15'
 +79 NE Cor Sta 20'
 +70 N.W. Cor Fill Sta 48
 +54 Tr. Oak 39'
 +33 End Rabbit Walk 25'
 +10 N.W. Cor Store
 +04 24" Pop 31'

+90 X Fe 38'
 +88 End Hedge 36
 +38 Beg Hedge 35'

+12 6" Birch 29'
 +05 18" Pop 30

+94 12" Bass 32'
 +75 End Branch 31'-50

+20 Beg 2" Pop Brush 31'-30
 +00 End Yard

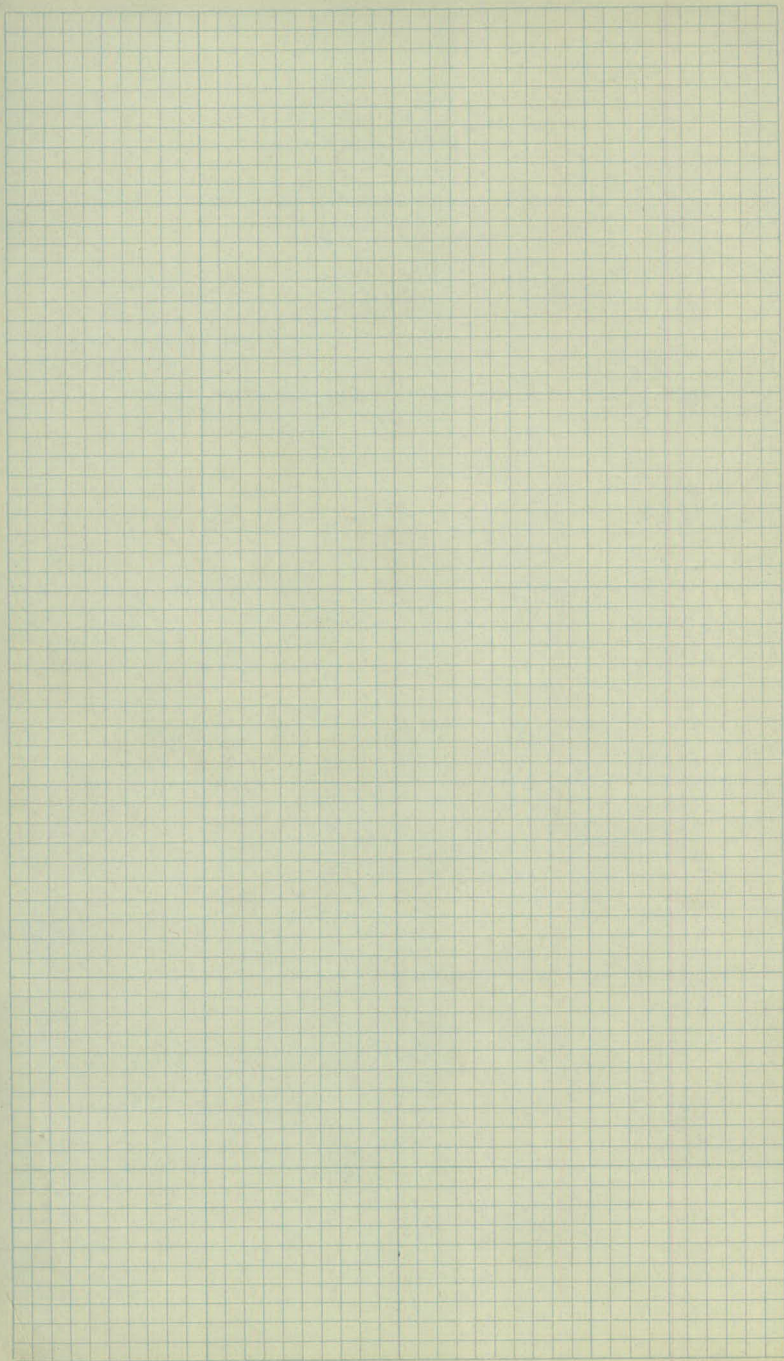
+87 End Wall 14
 +86 End 15" CM 13'
 +80 16' 6" Ent 14'
 +73 Ent 14'

+58 End Rubble Wall 14
 +56 Beg 15" x 30" CM 13'

+74 12" Birch 33'
 +44 6" Tr. 47'

+43 Root 12
 +30 Fe Cor 31
 +08 8" Birch 32'
 Fe 31

Fe 31



Sections

Sta	+	Σ	-	Elev
B.M	6.47	971.44		964.97
0+00				64.97
+17				65.3
+22				65.3
+33		24"X 40 X Drain		65.5
+50				65.7
1+00				67.1
+09				67.4
+22				67.8
T.P	8.45	978.32	1.57	969.87
+50				68.7
2+00				70.3
+15				70.6
+50				71.4

Lt

~~R~~

Rt

Top Mon 0100 & Bellair

$\frac{7.7}{100}$ $\frac{7.3}{50}$ L47

$\frac{5.8}{50}$ $\frac{4.8}{100}$

$\frac{7.5}{50}$ $\frac{7.5}{33}$ $\frac{6.4}{10}$ 61 $\frac{6.2}{11}$ $\frac{7.0}{34}$ $\frac{6.4}{50}$

$\frac{9.1}{50}$ $\frac{7.5}{28}$ $\frac{6.4}{10}$ 61 $\frac{6.2}{10}$ $\frac{7.0}{26}$ $\frac{7.5}{34}$ $\frac{7.1}{50}$

961.66 Inv

Inv 62.49

$\frac{10.5}{50}$ $\frac{10.1}{21}$ $\frac{9.78}{21}$ $\frac{7.2}{17}$ $\frac{6.1}{6}$ 59 $\frac{6.2}{9}$ $\frac{6.9}{18}$ $\frac{8.95}{19}$ $\frac{7.0}{19}$ $\frac{8.3}{21}$ $\frac{7.5}{35}$ $\frac{6.4}{50}$

$\frac{10.4}{50}$ $\frac{10.0}{28}$ $\frac{6.5}{12}$ 57 $\frac{6.5}{14}$ $\frac{7.0}{16}$ $\frac{7.2}{19}$ $\frac{6.5}{42}$ $\frac{5.4}{50}$

$\frac{9.1}{50}$ $\frac{8.0}{36}$ $\frac{6.5}{18}$ $\frac{5.1}{15}$ 43 $\frac{4.7}{15}$ $\frac{4.8}{20}$ $\frac{5.8}{23-26}$ $\frac{3.5}{21}$ $\frac{2.4}{50}$

$\frac{8.2}{50}$ $\frac{7.2}{36}$ $\frac{5.7}{22}$ $\frac{4.7}{16}$ 40 $\frac{4.4}{14}$ $\frac{4.1}{21}$ $\frac{5.0}{23-26}$ $\frac{1.5}{33}$ $\frac{1.8}{50}$

$\frac{4.0}{50}$ $\frac{4.2}{28}$ $\frac{4.1}{17}$ $\frac{4.1}{11}$ 36 $\frac{4.0}{17}$ $\frac{3.2}{20}$ $\frac{4.2}{24-27}$ $\frac{1.4}{33}$ $\frac{1.0}{50}$

Gr. at store

$\frac{9.3}{38}$ $\frac{9.4}{27}$ $\frac{10.2}{12}$ $\frac{9.9}{9}$ 9.6 $\frac{10.1}{16}$ $\frac{8.6}{20}$ $\frac{9.3}{24-27}$ $\frac{6.7}{31}$ $\frac{6.4}{37}$ $\frac{6.2}{50}$

$\frac{8.3}{50}$ $\frac{8.4}{22}$ $\frac{8.7}{14}$ $\frac{8.2}{8}$ 8.0 $\frac{8.7}{16}$ $\frac{6.4}{21}$ $\frac{7.0}{27}$ $\frac{4.9}{32}$ $\frac{5.0}{50}$

$\frac{7.6}{50}$ $\frac{7.8}{32}$ $\frac{8.3}{19}$ $\frac{8.0}{11}$ 7.7 $\frac{8.4}{16}$ $\frac{5.9}{20}$ $\frac{6.3}{27}$ $\frac{4.4}{33}$ $\frac{5.2}{35}$ $\frac{5.2}{50}$

$\frac{4.5}{50}$ $\frac{4.2}{36}$ $\frac{6.8}{32}$ $\frac{7.2}{19}$ $\frac{7.6}{16}$ $\frac{7.1}{10}$ 6.9 $\frac{7.1}{15}$ $\frac{5.1}{21}$ $\frac{5.6}{25-28}$ $\frac{4.5}{33}$ $\frac{4.7}{50}$

Sta	+	Δ	-	Elev
		978.32		
3	+00			72.6
	+50			73.2
4				73.4
	+50			73.0
5				72.3
	+50			71.3
6				70.1
	+23			69.7
T.P.	461	974.80	8.13	970.19
	+29			69.6
	+50			69.2
	+60			68.9
	+82			68.5

L+

R

R+

11

$$\frac{4.0}{50} \quad \frac{3.9}{21} \quad \frac{5.8}{18} \quad \frac{6.3}{16} \quad 5.7 \quad \frac{6.0}{14} \quad \frac{3.5}{18} \quad \frac{4.7}{25-28} \quad \frac{3.5}{35} \quad \frac{4.3}{50}$$

$$\frac{4.6}{58} \quad \frac{3.6}{19} \quad \frac{5.7}{15} \quad 5.1 \quad \frac{5.5}{15} \quad \frac{3.3}{17} \quad \frac{3.6}{29} \quad \frac{2.8}{33} \quad \frac{3.6}{50}$$

$$\frac{6.0}{50} \quad \frac{5.0}{34} \quad \frac{4.1}{17} \quad \frac{5.5}{16} \quad \frac{5.2}{9} \quad 4.9 \quad \frac{5.2}{14} \quad \frac{3.2}{17} \quad \frac{3.9}{28} \quad \frac{3.1}{33} \quad \frac{3.4}{50}$$

$$\frac{8.5}{50} \quad \frac{7.5}{37} \quad \frac{5.4}{17} \quad \frac{6.0}{15} \quad \frac{5.5}{9} \quad 5.3 \quad \frac{5.5}{15} \quad \frac{4.1}{17} \quad \frac{4.3}{27} \quad \frac{2.5}{33} \quad \frac{2.9}{50}$$

$$\frac{10.7}{50} \quad \frac{10.2}{38} \quad \frac{7.8}{16} \quad \frac{6.5}{10} \quad 6.0 \quad \frac{6.5}{14} \quad \frac{5.3}{16} \quad \frac{5.3}{30} \quad \frac{4.0}{33} \quad \frac{4.8}{39} \quad \frac{4.2}{50}$$

$$\frac{7.5}{50} \quad \frac{9.3}{28} \quad \frac{8.7}{18} \quad \frac{7.6}{14} \quad 7.0 \quad \frac{7.4}{14} \quad \frac{6.4}{16} \quad \frac{7.4}{27} \quad \frac{7.2}{50}$$

$$\frac{8.0}{50} \quad \frac{5.6}{20} \quad \frac{8.5}{13} \quad 8.2 \quad \frac{8.4}{15} \quad \frac{7.0}{17} \quad \frac{7.6}{27} \quad \frac{6.1}{30} \quad \frac{6.0}{34} \quad \frac{7.1}{50}$$

$$\frac{8.8}{50} \quad \frac{7.0}{31} \quad \frac{6.4}{19} \quad \frac{9.3}{14} \quad 8.6 \quad \frac{9.0}{15} \quad \frac{7.7}{17} \quad \frac{8.4}{27} \quad \frac{5.7}{33} \quad \frac{6.7}{40} \quad \frac{6.7}{50}$$

$$\frac{8.2}{50} \quad \frac{6.7}{22} \quad \frac{5.5}{11} \quad 5.2 \quad \frac{5.7}{15} \quad \frac{4.6}{14} \quad \frac{5.2}{24-27} \quad \frac{2.6}{32} \quad \frac{3.9}{50}$$

$$\frac{8.5}{50} \quad \frac{6.2}{22} \quad 5.6 \quad \frac{6.2}{15} \quad \frac{5.4}{14} \quad \frac{5.9}{27} \quad \frac{4.0}{32} \quad \frac{4.8}{50}$$

$$\frac{9.0}{58} \quad \frac{7.3}{36} \quad \frac{5.7}{19} \quad \frac{6.1}{17} \quad \frac{6.1}{13} \quad 5.9 \quad \frac{6.4}{15} \quad \frac{5.6}{17} \quad \frac{6.5}{28} \quad \frac{4.6}{36} \quad \frac{5.7}{50}$$

$$\frac{9.7}{50} \quad \frac{8.2}{32} \quad \frac{6.5}{12} \quad 6.3 \quad \frac{6.9}{15} \quad \frac{6.5}{14} \quad \frac{8.0}{28} \quad \frac{6.9}{34} \quad \frac{8.1}{50}$$

Sta	+	Σ	-	Elev
		97480		
7+00				68.2
+50				67.0
8+00				66.1
+50				65.2
9				63.8
T.P.	5.55	968.86	11.49	963.31
+50				62.3
10				60.5
+50				58.9
11				56.8
T.P.	6.95	963.17	12.64	956.22
B.M.	3.46	963.19	3.42	959.75 959.73
+50				54.6
T.P.	3.90	956.18	10.91	952.28
12				52.3
+50				49.6

Lt

K

Rt

12

$$\begin{array}{r} 10.7 \\ 50 \end{array} \quad \begin{array}{r} 8.8 \\ 19 \end{array} \quad \begin{array}{r} 7.4 \\ 15 \end{array} \quad \begin{array}{r} 7.0 \\ 10 \end{array} \quad 6.6 \quad \begin{array}{r} 7.2 \\ 15 \end{array} \quad \begin{array}{r} 7.6 \\ 21 \end{array} \quad \begin{array}{r} 9.3 \\ 31 \end{array} \quad \begin{array}{r} 8.5 \\ 36 \end{array} \quad \begin{array}{r} 9.5 \\ 50 \end{array}$$

$$\begin{array}{r} 12.4 \\ 50 \end{array} \quad \begin{array}{r} 11.0 \\ 18 \end{array} \quad \begin{array}{r} 8.4 \\ 12 \end{array} \quad 7.8 \quad \begin{array}{r} 8.4 \\ 14 \end{array} \quad \begin{array}{r} 9.7 \\ 18 \end{array} \quad \begin{array}{r} 11.4 \\ 33 \end{array} \quad \begin{array}{r} 10.4 \\ 35 \end{array} \quad \begin{array}{r} 11.0 \\ 50 \end{array}$$

$$\begin{array}{r} 11.0 \\ 50 \end{array} \quad \begin{array}{r} 11.4 \\ 17 \end{array} \quad \begin{array}{r} 9.3 \\ 13 \end{array} \quad 8.7 \quad \begin{array}{r} 9.5 \\ 15 \end{array} \quad \begin{array}{r} 10.6 \\ 24 \end{array} \quad \begin{array}{r} 11.0 \\ 29 \end{array} \quad \begin{array}{r} 9.0 \\ 33 \end{array} \quad \begin{array}{r} 10.4 \\ 50 \end{array}$$

$$\begin{array}{r} 11.2 \\ 50 \end{array} \quad \begin{array}{r} 11.1 \\ 27 \end{array} \quad \begin{array}{r} 10.9 \\ 15 \end{array} \quad \begin{array}{r} 10.1 \\ 12 \end{array} \quad 9.6 \quad \begin{array}{r} 10.2 \\ 15 \end{array} \quad \begin{array}{r} 10.2 \\ 20 \end{array} \quad \begin{array}{r} 11.4 \\ 29 \end{array} \quad \begin{array}{r} 9.1 \\ 35 \end{array} \quad \begin{array}{r} 9.3 \\ 50 \end{array}$$

$$\begin{array}{r} 9.8 \\ 50 \end{array} \quad \begin{array}{r} 9.6 \\ 20 \end{array} \quad \begin{array}{r} 12.1 \\ 15 \end{array} \quad \begin{array}{r} 11.4 \\ 13 \end{array} \quad 11.0 \quad \begin{array}{r} 11.4 \\ 17 \end{array} \quad \begin{array}{r} 10.4 \\ 20 \end{array} \quad \begin{array}{r} 11.1 \\ 31 \end{array} \quad \begin{array}{r} 9.3 \\ 35 \end{array} \quad \begin{array}{r} 8.4 \\ 50 \end{array}$$

$$\begin{array}{r} 2.6 \\ 33 \end{array} \quad \begin{array}{r} 3.4 \\ 21 \end{array} \quad \begin{array}{r} 7.2 \\ 14 \end{array} \quad 6.6 \quad \begin{array}{r} 7.1 \\ 15 \end{array} \quad \begin{array}{r} 4.8 \\ 20 \end{array} \quad \begin{array}{r} 5.0 \\ 29 \end{array} \quad \begin{array}{r} 2.5 \\ 34 \end{array} \quad \begin{array}{r} 1.8 \\ 41 \end{array} \quad \begin{array}{r} 1.4 \\ 50 \end{array}$$

$$\begin{array}{r} 2.6 \\ 50 \end{array} \quad \begin{array}{r} 4.2 \\ 27 \end{array} \quad \begin{array}{r} 4.5 \\ 21 \end{array} \quad \begin{array}{r} 8.9 \\ 14 \end{array} \quad 8.4 \quad \begin{array}{r} 8.9 \\ 16 \end{array} \quad \begin{array}{r} 5.6 \\ 18 \end{array} \quad \begin{array}{r} 5.6 \\ 28 \end{array} \quad \begin{array}{r} 2.0 \\ 36 \end{array} \quad \begin{array}{r} 1.9 \\ 50 \end{array}$$

$$\begin{array}{r} 4.1 \\ 50 \end{array} \quad \begin{array}{r} 5.7 \\ 33 \end{array} \quad \begin{array}{r} 6.3 \\ 20 \end{array} \quad \begin{array}{r} 9.8 \\ 14 \end{array} \quad \begin{array}{r} 10.6 \\ 13 \end{array} \quad 11.0 \quad \begin{array}{r} 10.4 \\ 16 \end{array} \quad \begin{array}{r} 7.2 \\ 19 \end{array} \quad \begin{array}{r} 7.4 \\ 26 \end{array} \quad \begin{array}{r} 4.2 \\ 35 \end{array} \quad \begin{array}{r} 4.4 \\ 50 \end{array}$$

$$\begin{array}{r} 7.5 \\ 50 \end{array} \quad \begin{array}{r} 8.8 \\ 35 \end{array} \quad \begin{array}{r} 10.0 \\ 27 \end{array} \quad \begin{array}{r} 9.3 \\ 19 \end{array} \quad \begin{array}{r} 12.5 \\ 15 \end{array} \quad 12.1 \quad \begin{array}{r} 13.0 \\ 17 \end{array} \quad \begin{array}{r} 10.0 \\ 19 \end{array} \quad \begin{array}{r} 10.0 \\ 28 \end{array} \quad \begin{array}{r} 6.6 \\ 35 \end{array} \quad \begin{array}{r} 7.1 \\ 50 \end{array}$$

SpK in 15" Oak 45' Lt 54 117 20

$$\begin{array}{r} 6.0 \\ 50 \end{array} \quad \begin{array}{r} 6.3 \\ 36 \end{array} \quad \begin{array}{r} 6.2 \\ 21 \end{array} \quad \begin{array}{r} 8.7 \\ 15 \end{array} \quad 8.6 \quad \begin{array}{r} 9.4 \\ 17 \end{array} \quad \begin{array}{r} 6.5 \\ 20 \end{array} \quad \begin{array}{r} 6.8 \\ 26 \end{array} \quad \begin{array}{r} 4.0 \\ 37 \end{array} \quad \begin{array}{r} 5.6 \\ 50 \end{array}$$

$$\begin{array}{r} 1.8 \\ 50 \end{array} \quad \begin{array}{r} 2.8 \\ 32 \end{array} \quad \begin{array}{r} 1.7 \\ 20 \end{array} \quad \begin{array}{r} 4.4 \\ 15 \end{array} \quad 3.9 \quad \begin{array}{r} 4.8 \\ 16 \end{array} \quad \begin{array}{r} 3.0 \\ 18 \end{array} \quad \begin{array}{r} 3.8 \\ 28 \end{array} \quad \begin{array}{r} 4.3 \\ 44 \end{array} \quad \begin{array}{r} 5.1 \\ 50 \end{array}$$

$$\begin{array}{r} 6.8 \\ 50 \end{array} \quad \begin{array}{r} 7.3 \\ 33 \end{array} \quad \begin{array}{r} 7.2 \\ 16 \end{array} \quad \begin{array}{r} 7.4 \\ 14 \end{array} \quad 6.6 \quad \begin{array}{r} 7.2 \\ 16 \end{array} \quad \begin{array}{r} 7.0 \\ 17 \end{array} \quad \begin{array}{r} 7.0 \\ 22 \end{array} \quad \begin{array}{r} 8.0 \\ 34 \end{array} \quad \begin{array}{r} 7.0 \\ 37 \end{array} \quad \begin{array}{r} 7.7 \\ 50 \end{array}$$

Sta	+	T.	-	Elev
		956.18		
13		.		46.7
T.P	5.71	950.31	11.58	944.60
+50				44.5
14				42.5
+30				41.4
+50				40.7
T.P	5.01	944.14	11.18	937.13
+69				40.0
+83				39.6
15				39.0
+50				37.8
16				37.2
+50				37.0
17		.		37.1
T.P	4.80	946.94	7.00	937.14

LT

X

RT

$\frac{11.9}{50}$ $\frac{12.3}{31}$ $\frac{12.0}{17}$ $\frac{10.2}{13}$ 95 $\frac{10.4}{15}$ $\frac{11.5}{18}$ $\frac{12.4}{27}$ $\frac{12.3}{38}$ $\frac{10.2}{50}$

$\frac{8.4}{50}$ $\frac{9.2}{44}$ $\frac{9.2}{30}$ $\frac{8.9}{20}$ $\frac{6.6}{15}$ 5.8 $\frac{6.6}{16}$ $\frac{7.6}{18}$ $\frac{7.6}{34}$ $\frac{4.8}{50}$

$\frac{5.5}{50}$ $\frac{7.1}{36}$ $\frac{9.1}{31}$ $\frac{9.0}{20}$ $\frac{7.6}{14}$ $\frac{7.9}{13}$ 7.8 $\frac{8.3}{17}$ $\frac{8.9}{29}$ $\frac{5.2}{34}$ $\frac{4.6}{45}$ $\frac{5.0}{50}$

$\frac{4.3}{50}$ $\frac{4.5}{38}$ $\frac{7.7}{33}$ $\frac{7.8}{25}$ $\frac{8.3}{13}$ $\frac{8.7}{12}$ 8.9 $\frac{9.6}{17}$ $\frac{9.3}{21}$ $\frac{10.3}{24}$ $\frac{9.4}{30}$ $\frac{15.7}{50}$

$\frac{2.5}{50}$ $\frac{7.5}{41}$ $\frac{8.6}{27}$ $\frac{9.0}{15}$ $\frac{9.7}{14}$ 9.6 $\frac{9.9}{10}$ $\frac{10.6}{20}$ $\frac{14.0}{29}$ $\frac{14.6}{37}$ $\frac{16.6}{50}$

Sta 15+00

$\frac{10.4}{50}$ $\frac{2.0}{36}$ $\frac{2.7}{28}$ $\frac{3.7}{15}$ $\frac{4.3}{14}$ 4.1 $\frac{4.8}{19}$ $\frac{7.9}{27}$ $\frac{9.3}{37}$ $\frac{10.1}{50}$

$\frac{14.6}{50}$ $\frac{14.6}{41}$ $\frac{0.0}{34}$ $\frac{3.4}{28}$ $\frac{4.1}{15}$ $\frac{4.7}{14}$ 4.5 $\frac{5.3}{19}$ $\frac{7.7}{26}$ $\frac{9.3}{37}$ $\frac{10.8}{50}$

$\frac{12.5}{50}$ $\frac{12.0}{40}$ $\frac{2.8}{34}$ $\frac{5.6}{29}$ $\frac{6.4}{20}$ $\frac{5.4}{15}$ 5.1 $\frac{5.9}{16}$ $\frac{7.5}{20}$ $\frac{8.9}{27}$ $\frac{9.8}{36}$ $\frac{10.7}{37}$ $\frac{11.5}{50}$

$\frac{6.3}{50}$ $\frac{7.5}{46}$ $\frac{9.0}{34}$ $\frac{8.6}{17}$ $\frac{6.9}{14}$ 6.3 $\frac{7.0}{15}$ $\frac{8.6}{17}$ $\frac{10.3}{25}$ $\frac{11.9}{31}$ $\frac{12.8}{40}$

$\frac{8.6}{50}$ $\frac{9.2}{36}$ $\frac{9.7}{17}$ $\frac{7.4}{14}$ 6.9 $\frac{7.8}{15}$ $\frac{9.6}{18}$ $\frac{11.0}{25}$ $\frac{12.8}{34}$

$\frac{7.8}{50}$ $\frac{9.1}{31}$ $\frac{9.1}{19}$ $\frac{7.5}{14}$ 7.1 $\frac{8.1}{16}$ $\frac{9.8}{19}$ $\frac{11.4}{27}$ $\frac{12.8}{37}$

$\frac{4.6}{50}$ $\frac{4.9}{25}$ $\frac{8.9}{17}$ $\frac{7.4}{14}$ 7.0 $\frac{7.2}{9}$ $\frac{8.1}{16}$ $\frac{8.9}{18}$ $\frac{10.8}{25}$ $\frac{12.8}{40}$ W.S. 10.21

9-23-43

Sta	+	π	-	Elev
		941.94		

17450			7.00	34.94
-------	--	--	------	-------

18		10" X P.V. X Drain		37.5
----	--	--------------------	--	------

+50				38.5
-----	--	--	--	------

19				40.5
----	--	--	--	------

+50				43.3
-----	--	--	--	------

T.P	9.46	951.22	0.18	941.76
19+50				43.3

20				47.0
----	--	--	--	------

+30				49.5
-----	--	--	--	------

+40				50.4
-----	--	--	--	------

T.P	6.28	954.79	2.71	948.51
-----	------	--------	------	--------

B.M	13.20	963.41	4.58	950.21 952.83
-----	-------	--------	------	---------------

20+30				49.5
-------	--	--	--	------

+40				50.4
-----	--	--	--	------

LT X RT

Flow line Str. R.R. Culv. in old R.O.W.

Northside
WS 9.21
934.737

$\frac{29}{50}$	$\frac{8.5}{36}$	$\frac{79}{17}$	$\frac{5.2}{12}$	47	$\frac{5.5}{15}$	$\frac{69}{17}$	$\frac{97}{25}$	$\frac{110}{33}$	$\frac{110}{50}$
									931.54 Inv
$\frac{92}{50}$	$\frac{9.6}{35}$	$\frac{9.8}{23}$	$\frac{74.50}{16}$	$\frac{12}{12}$	4.4	$\frac{51}{14}$	$\frac{67}{17}$	$\frac{84}{27}$	$\frac{10.4}{36}$
									$\frac{10.40}{29}$

$\frac{10.6}{50}$	$\frac{11.1}{33}$	$\frac{10.2}{24}$	$\frac{8.6}{17}$	$\frac{42}{12}$	3.4	$\frac{41}{14}$	$\frac{68}{19}$	$\frac{89}{25}$	$\frac{103}{42}$
-------------------	-------------------	-------------------	------------------	-----------------	-----	-----------------	-----------------	-----------------	------------------

$\frac{12.4}{50}$	$\frac{10.7}{46}$	$\frac{9.9}{32}$	$\frac{72}{19}$	$\frac{21}{11}$	1.4	$\frac{2.0}{14}$	$\frac{44}{19}$	$\frac{66}{30}$	$\frac{73}{42}$	$\frac{79}{50}$
-------------------	-------------------	------------------	-----------------	-----------------	-----	------------------	-----------------	-----------------	-----------------	-----------------

$\frac{84}{50}$	$\frac{7.8}{38}$	$\frac{6.4}{32}$	$\frac{55}{19}$	-1.4	$\frac{02}{18}$	$\frac{22}{29}$	$\frac{30}{37}$	$\frac{40}{50}$
-----------------	------------------	------------------	-----------------	------	-----------------	-----------------	-----------------	-----------------

$\frac{84}{15}$ 7.9 $\frac{84}{15}$

$\frac{15.6}{50}$	$\frac{143}{36}$	$\frac{132}{32}$	$\frac{121}{24}$	$\frac{5.0}{13}$	42	$\frac{48}{18}$	$\frac{76}{31}$	$\frac{86}{35}$	$\frac{62}{42}$	$\frac{5.7}{50}$
-------------------	------------------	------------------	------------------	------------------	----	-----------------	-----------------	-----------------	-----------------	------------------

$\frac{12.9}{50}$	$\frac{9.4}{23}$	$\frac{2.7}{15}$	1.7	$\frac{22}{16}$	$\frac{2.0}{17}$	$\frac{08}{18}$
-------------------	------------------	------------------	-----	-----------------	------------------	-----------------

$\frac{5.4}{50}$	$\frac{3.7}{39}$	$\frac{2.4}{22}$	$\frac{5.1}{20}$	$\frac{46}{16}$	$\frac{16}{11}$	0.8	$\frac{1.4}{15}$	$\frac{08}{16}$
------------------	------------------	------------------	------------------	-----------------	-----------------	-----	------------------	-----------------

Top Rock

13.9

948.7

$\frac{147}{30}$	$\frac{147}{33}$	$\frac{140}{37}$	$\frac{7.5}{50}$
------------------	------------------	------------------	------------------

13.0

$\frac{120}{22}$	$\frac{126}{27}$	$\frac{126}{30}$	$\frac{111}{31}$	$\frac{105}{38}$	$\frac{64}{50}$
------------------	------------------	------------------	------------------	------------------	-----------------

Sta + Δ - Elev

963.41

20+57 51.7

+87 53.9

21 54.7

+50 57.5

22 60.2

+50 63.1

T.P. 8.18 971.05 0.54 962.87.

20+87 53.9

21 54.7

+50 57.5

22 60.2

+50 63.1

+65 64.1

Lt R

Rt

4.2
50

$\frac{160}{50}$ $\frac{132}{29}$ $\frac{120}{19}$ $\frac{125}{14}$ 11.7 $\frac{12.3}{15}$ $\frac{11.7}{16}$ $\frac{11.8}{19}$ $\frac{10.3}{21-23}$ $\frac{10.7}{27}$ $\frac{6.8}{34}$ $\frac{6.9}{40}$

$\frac{6.9}{50}$ $\frac{1.4}{26}$ $\frac{2.0}{15}$ $\frac{10.4}{13}$ $\frac{9.8}{8}$ 9.5 $\frac{10.0}{15}$ $\frac{9.2}{16-18}$ $\frac{6.7}{21-25}$

$\frac{8.1}{16}$ $\frac{2.4}{15}$ $\frac{9.0}{7}$ 8.7 $\frac{9.2}{15}$ $\frac{5.1}{21-25}$

$\frac{5.4}{16}$ $\frac{6.5}{15}$ 5.9 $\frac{6.1}{14}$ $\frac{0.8}{21}$ $\frac{0.3}{26}$

$\frac{1.5}{16}$ $\frac{3.7}{12}$ 3.2 $\frac{3.3}{14}$

$\frac{1.1}{16}$ 0.3 $\frac{0.2}{11}$

Top start

+10.7

(17.2) $\frac{6.5}{34}$ $\frac{3.5}{40}$ $\frac{5.5}{50}$

$\frac{13.2}{50}$ $\frac{7.8}{26}$ (16.4) $\frac{6.8}{34}$ $\frac{5.9}{39}$ $\frac{3.4}{41}$ $\frac{6.0}{50}$

$\frac{8.2}{50}$ $\frac{6.2}{40}$ $\frac{4.7}{26}$ (13.6) $\frac{3.9}{34}$ $\frac{0.4}{50}$

$\frac{5.7}{50}$ $\frac{2.2}{31}$ $\frac{1.8}{25}$ $\frac{6.2}{20}$ (10.9) $\frac{5.1}{21}$ $\frac{1.4}{31}$ $\frac{+1.5}{36}$ $\frac{+0.5}{50}$

$\frac{3.9}{50}$ $\frac{0.3}{24}$ $\frac{5.4}{18}$ (8.0) $\frac{6.4}{12}$ $\frac{4.0}{21}$ $\frac{1.5}{23}$ $\frac{+3.0}{38}$ $\frac{+3.0}{50}$

$\frac{2.5}{50}$ $\frac{2.0}{36}$ $\frac{0.6}{23}$ $\frac{2.9}{22}$ $\frac{5.0}{17}$ $\frac{7.9}{16}$ $\frac{7.4}{10}$ 7.0 $\frac{6.9}{9}$ $\frac{3.8}{28}$ $\frac{1.5}{50}$

Sta	+	Δ	-	Elev
		971.05		
22+75				64.6
T.P	8.76	973.82	5.99	965.06
23				65.5
+20				66.2
+24				66.4
+50				67.2
24				68.2
+50				68.6
25				69.2
T.P	6.15	975.96	4.01	969.81
+50				69.8
26				70.4
+11	x Drain 15" x Conc			70.8
+30.57		$\pm$ E		70.8
B.M			5.23	970.73 970.74

L+

✕

R+

$$\frac{42}{50} \quad \frac{25}{36} \quad \frac{11}{22} \quad \frac{51}{17} \quad \frac{72}{16} \quad 65 \quad \frac{62}{11} \quad \frac{37}{28} \quad \frac{25}{30} \quad \frac{+11}{40} \quad \frac{+23}{46} \quad \frac{+30}{50}$$

$$\frac{78}{50} \quad \frac{29}{22} \quad \frac{70}{16} \quad \frac{89}{15} \quad 83 \quad \frac{85}{11} \quad \frac{45}{22} \quad \frac{04}{34} \quad \frac{+04}{43} \quad \frac{+04}{50}$$

$$\frac{97}{50} \quad \frac{81}{33} \quad \frac{46}{31} \quad \frac{32}{22} \quad \frac{64}{16} \quad \frac{80}{15} \quad 76 \quad \frac{78}{12} \quad \frac{51}{19} \quad \frac{20}{24} \quad \frac{+26}{42} \quad \frac{+10}{50}$$

$$\frac{98}{50} \quad \frac{74}{23} \quad \frac{73}{15} \quad \frac{80}{15} \quad 74 \quad \frac{78}{12} \quad \frac{51}{19} \quad \frac{20}{24} \quad \frac{+26}{42} \quad \frac{+10}{50}$$

$$\frac{103}{50} \quad \frac{81}{27} \quad \frac{73}{14} \quad 66 \quad \frac{70}{14} \quad \frac{65}{17} \quad \frac{13}{23} \quad \frac{00}{50}$$

$$\frac{103}{50} \quad \frac{99}{28} \quad \frac{66}{14} \quad 56 \quad \frac{54}{17} \quad \frac{17}{23} \quad \frac{12}{33} \quad \frac{02}{35} \quad \frac{+20}{50}$$

$$\frac{84}{50} \quad \frac{71}{30} \quad \frac{59}{9} \quad 52 \quad \frac{50}{18} \quad \frac{40}{25} \quad \frac{33}{32} \quad \frac{08}{40} \quad \frac{+03}{50}$$

$$\frac{68}{50} \quad \frac{51}{20} \quad \frac{52}{11} \quad 46 \quad \frac{41}{19} \quad \frac{24}{36} \quad \frac{00}{50}$$

$$\frac{87}{50} \quad \frac{76}{30} \quad \frac{69}{18} \quad 62 \quad \frac{56}{25} \quad \frac{45}{30} \quad \frac{13}{50}$$

$$\frac{85}{50} \quad \frac{75}{39} \quad \frac{71}{25} \quad \frac{62}{10} \quad 52 \quad \frac{48}{25} \quad \frac{34}{50}$$

960.26

InV
15.7

$$\frac{92}{50} \quad 52$$

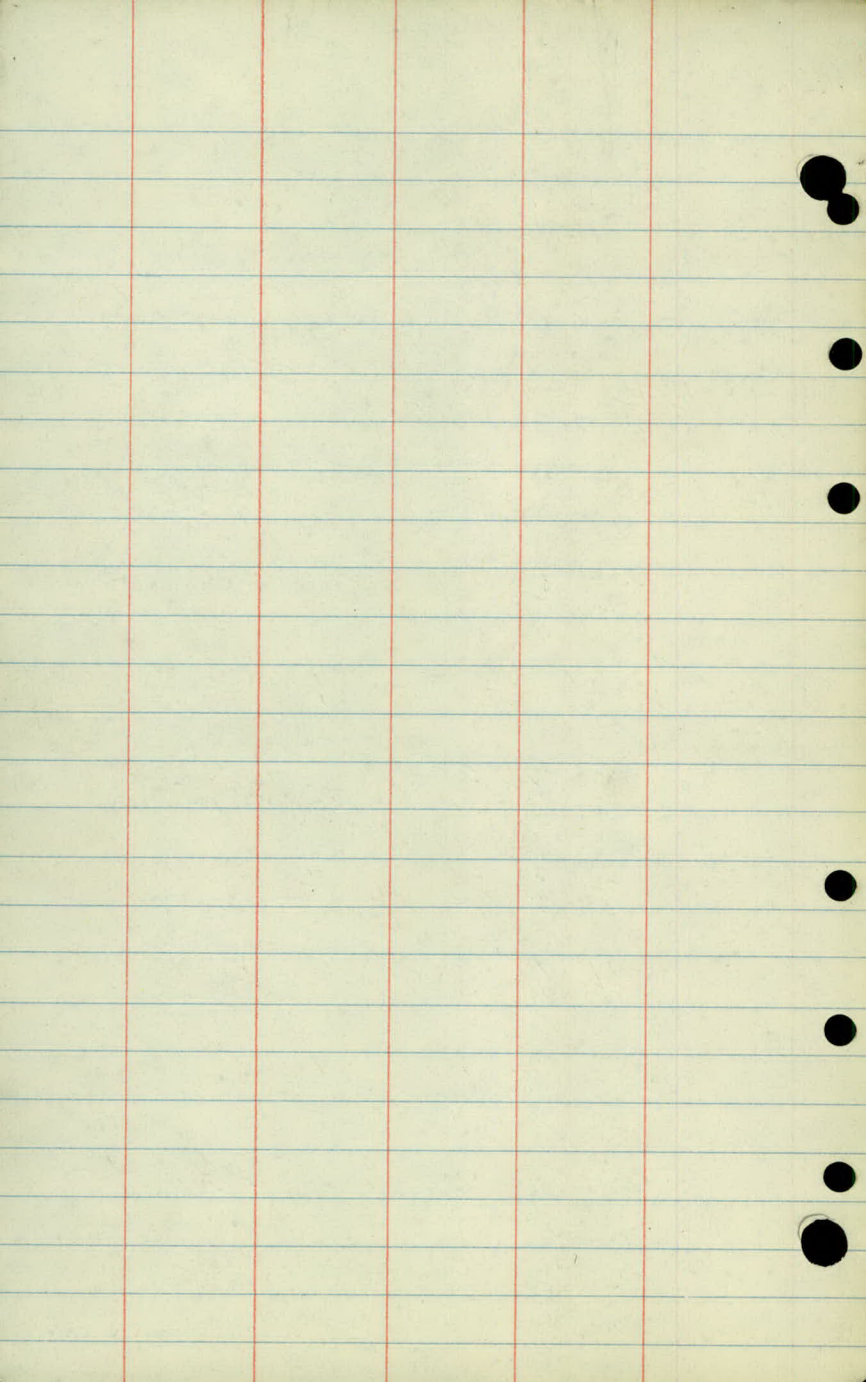
$$\frac{37}{50}$$

InV 971.96

400

$$\frac{94}{50} \quad \frac{64}{22} \quad 52 \quad \frac{41}{27} \quad \frac{33}{50}$$

Top Mon Co Rd "F" v East Co Line



Alignment
Co. R.O. "F" 9/c No 56.

8/11/27
C.W.S.
D.S.
A.B.
A.M.

From Bellaire Ave
To East Co Line
9/c 56.

Office of Ramsey Co. Engineer
ST. PAUL, MINN.
Date Filed 4-7-27
File No. 16

Received 3-21-27
C. H. Keweler

26 + 29²⁰ Mont. & East Coline

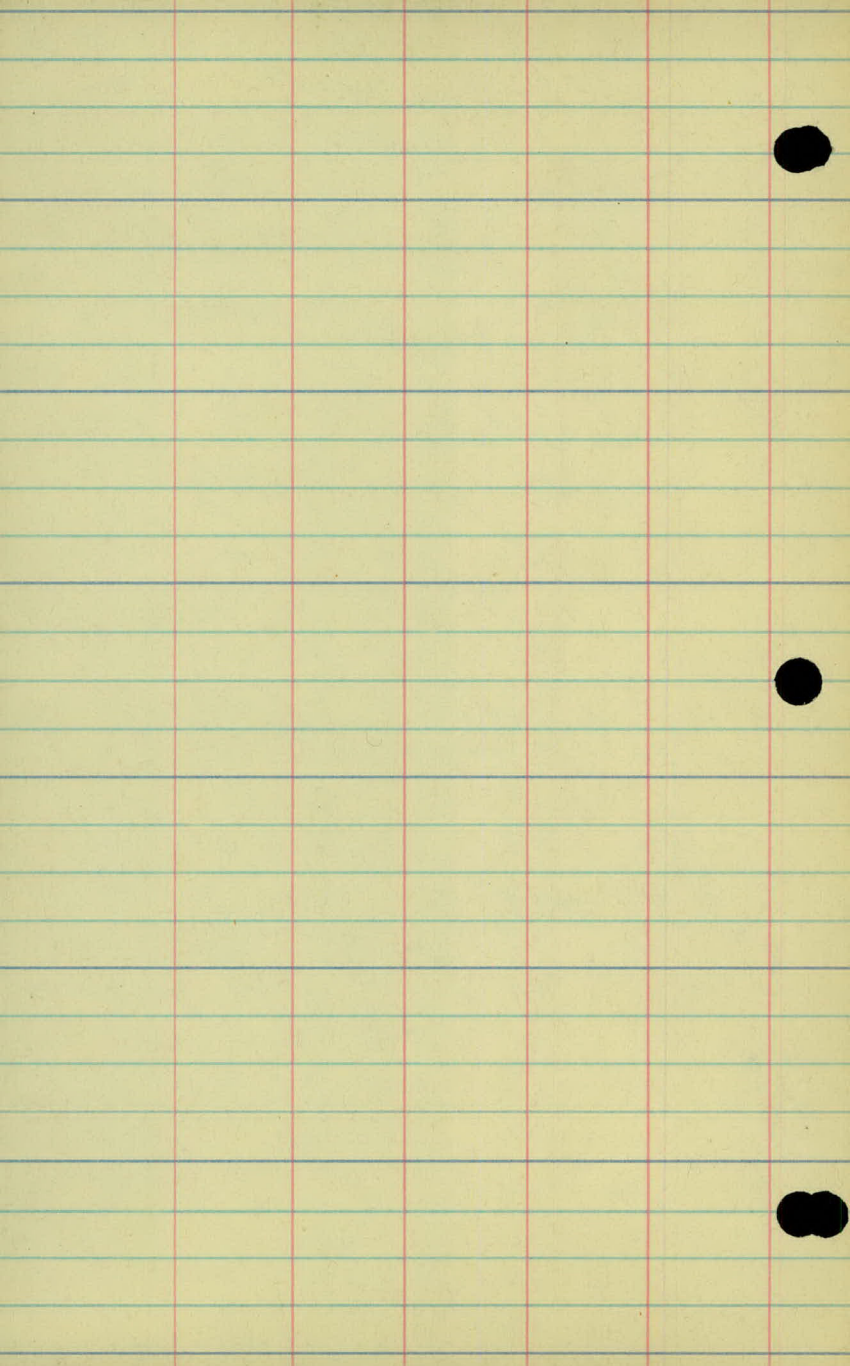
4 + 32' P.O.T.

0 + 00 Mont & Bellair Av.

TP
O - 6119 -
O - 5437 -
T.P.
90°-25' →
5" below surface

10" Oak.
O - 2223 - spike.
4224 -
O Twin Oak.

M.C. ?
89°-53' 15" Oak.
P463
5261 20" Oak
Mont 3" below surface



3/17/27
CHAS.
D.
A.S.
A.M.

Topography.

Co. Rd. F.

From Bellaire Ave

East Countyline

T/C No 56

Need Road
L+ R+

5+00

11 11

4+00

3+00

2+00

1+00

11' 11'

0+00

& Bellairs Ave.

3/1728

+ 83 T 24'
+ 78 T 29'

+ 27 2 T 34'

F 34

+ 29 T 31'

F 32

+ 88 T 23'

+ 82 T 28'

+ 10 T 34'

F 34'

+ 91 T 33'

+ 69 T 32'

+ 45 T 30'

+ 28 T 31'

+ 10 T 31'

F 31

+ 84 T 29'

+ 44 T 34'

+ 53 T 34'

+ 40 T 34'

+ 24 T 34'

F 34'

+ 70 T 37'

+ 62 T 36'

+ 40 T 36'

+ 28 F Cor 37'

+ 38 T 28'

X Rd.
+ 95 Rd 5g 10

+ 90 T 24'

+ 78 T 23'

+ 68 T 30'

+ 71 T 24'

+ 14 T 23'

+ 90 T 29'

+ 33 F 35

- 12 3 R

Timber & Brush

Timber & Brush

Bellair Ave.

Cultivated

Cultivate

12+00

+67 8 Drivcht

12" x 16 CM.

11+00

10+00

10'

10'

9+00

8+00

7+00

6+00

Br 17.

F 34

T 33'

Cleared land.
Not under cult.

Pasture

19+00

18+00

17+00

16+00

15+00

11' 11'

+17 E Drive Lt

Side D 12" 120 CM.

14+00

13+00

3/28/27

+120 E Br 17'

+53 Beg Br 14'

+90 End Br 16'

B. 15'

Wetland

Cultivated

Brush.

Timber

Pond

+12 F Cr 33'

+40 T 33'

+26 T 35'

F 31'

+68 T 33

+85 E Br 11

F 37' Br 11'

F 26' Br 17'

+32 T. 26'

F 36'

F 35 Br 17'

+60 Beg Timber

+60 E Pasture

+41 T. 31'

+14 F 34'

+08 T 28

+90 F 47

+76 T 25'

+68 T 36

+49 T 28'

+41 T 36

+19 T 35'

+101 T 39

F 40'

+292 * East Coline

26+00

+97 * X Drain 12" x 40 CM

25+00

1 25

24+00

7' 15'

23+00

10' 10'

165 * Drive Rt.

10' x 12'

22+00

21+00

+50

* Drive Lt.

20+00

10 11

+3990-T 92.

East Co. wine

T 16 1/2

+52 P P 5'

+47 F Cor 4'

R R F 8' 5 T. 37

+54 End 4'

P Tree

R R T 60. R W F 30.

18 Trees

+15 T 22

+10 T 20

3 T Cor RR

R.R. 4'

+15 R 41'

H 2 35'

R 26'

Store.

33'

+00 Rd 5 34'

+99 Gas Sq 33

+8 F Hedge 33

+25 Hedge 34'

+473 R stops 29'

+72 F House 46'

+63 Cor House 46'

+62 Gas Pump 32

+04 T 30

Hedge 33

+20 B Hedge 33

+04 T 29'

+68 X Rd 29. 13

+28 R R Sq. 13

+30 E F Cor 35'

F 32'

F 35'

Orchard

Timber

Timber

27+00