

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Road Map Survey

EAST COUNTY LINE ROAD
& SOUTH SHORE BLVD.

Co. Rd. "E" So. Shore Blvd.
From East Co. Line To White Bear Ave.

Road Acc't. No. 34

Date Filed 4-7-26

File 10

Rd. # 34

East Co. Line From Co. Rd. "E" To So. Shore Blvd.

So. Shore Blvd From E. Co. Line To White Bear Ave

Sta.

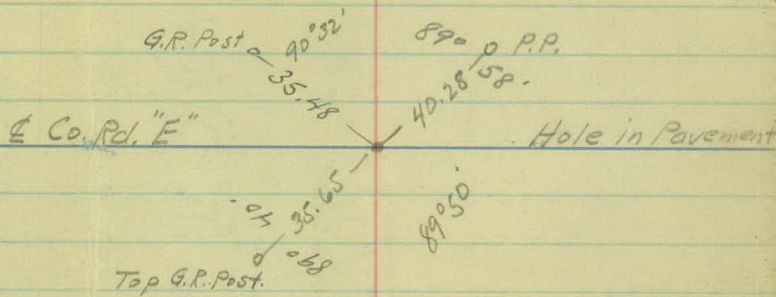
A-Lt. A-Rt.

517+43¹ P.O.T.

N 1° 39' E

503+34² P.I.

0° 12'



Station

Ang. Lt. Ang. Pt.

556+15⁹⁵ P.O.T. $\angle$ T.C. Elec. Ry.

N 1° 52' E

556+06¹⁰ Mont.
P.I.

0° 56'

544+88⁵ P.O.T.

N 0° 56' E

529+68⁸ Mont.
P.I.

0° 43'

N 1° 39' E

4-7-26
24" Triple Willow

M.C.
(Grade 10-28-32)

36.95
42.42

Cor. Ho.



11.48
15.38
16" W. Ash
Iron Rd. Sq.

28° 18'

352.6
370.92 R



10" Elm

62.0

P.P.

Conc. Mont.

(Grade 10-29-32)

N.E. cor 25

Iron Rd. Sq. 45.30

42.48
46.46

Iron F. Cor.

40.32
13.74

Gate. P.

31.6

12" Oak

110.84

15" Oak

22.77

35.44 F.P.

(Grade 10-28-32)

E 1/4. Cor. Sec. 25

30-22

Station

Ang. ht Ang. Pt

564+74.56 P.T.

N 29° 23' W

563+20.65 P.I.

38° 32'

561+53.45 P.C.

559+99.19 P.T.

N 67° 55' W

559+58.7 P.I. 69° 47'

559+04.45 P.C.

Sta - Def

561+53.45 - 0°00'

562+00 - 20°48'

+50 - 50°48'

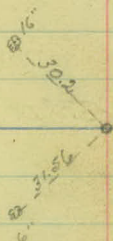
563+00 - 80°48'

+50 - 110°48'

564+00 - 140°48'

+50 - 170°48'

+74.36 - 190°16'



120° Curve. Rt.

$\Delta = 38°32'$

Rad = 476.34

Tang = 167.198

Length = 321.11

80° Curve. Lt.

$\Delta = 69°47'$

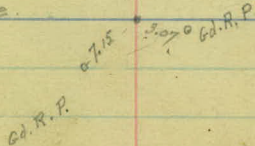
Rad = 77.786

Tang = 54.25

{ Arc Length = 94.74

559+51.82 Ctr. Curve.

Rad. 146.50



6d. R.P.

Station.

Ang. ht. Ang. Rt

572+48³⁸ P.T.

N 21° 23' W

570+48² P.I.

33° 00'

568+35⁸⁸ P.C.

567+13²⁹ P.T.

N 54° 23' W

566+18⁹ P.I.

25° 00'

565+20⁹⁸ P.C.

Sta - Def

566+35.88 - 0°00'

+50 - 0°34'

569+00 - 2°34'

+50 - 4°34'

570+00 - 6°34'

+50 - 8°34'

571+00 - 10°34'

+50 - 12°34'

572+00 - 14°34'

572+48.86 - 16°30'

8° Curve. RT.

 $\Delta = 33°00'$

Rad = 716.78'

Tang = 212.32'

Length = 412.50'



565+20.98 - 0°00'

+50 - 1°53'

566+00 - 5°08'

+50 - 8°23'

567+00 - 11°38'

+13.29 - 12°30'

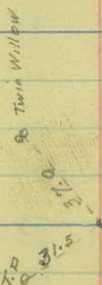
13° Curve. LT

 $\Delta = 25°00'$

Rad = 441.68'

Tang = 97.92'

Length = 192.31'



Station

Ang. ht. Ang. Rt

577+33.5 P.T.

N 81° 02' W

576+48.50 P.I. 17° 09'

575+62.0 P.C.

N 63° 53' W

575+55.0 P.T.

574+83.2 P.I. 42° 30'

574+03.33 P.C.

Sta - Def

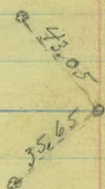
575+62.0 - 0°00'

576+00 - 1°54'

+50 - 4°24'

577+00 - 6°54'

+33.5 - 8°34½'



10° Curve ht.

$\Delta = 17°09'$

Rad = 573.69

Tang = 86.50

Length = 171.50

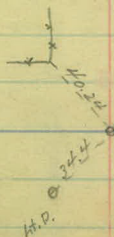
Sta. - Def

574+03.33 - 0°00'

+50 - 6°32'

575+00 - 13°32'

+55" - 21°15'



28° Curve ht.

$\Delta = 42°30'$

Rad = 206.68

Tang = 80.37

Length = 151.78

Station

Ang. ht. Ang. RI

+36.82

591+45.9 P.O.T

589+84.96 P.T.

582°49' W

588+79.5 P.I. 27°23'

25.01 e

587+65.6 P.C.

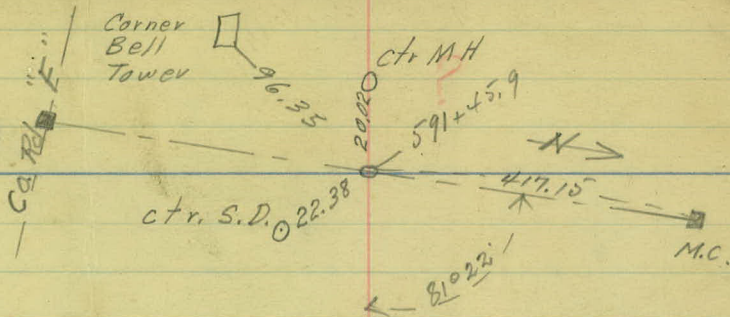
585+134.6 P.T.

N 59°48' W

583+82.4 P.I.

21°14'

582+46.04 P.C.



587+65.06-0000

588+00-2056' G.P.

+50-70/3'

589+00-11078'

+50-15043'

+84.96-180411'

40.06

14'

15
Believe 10' East

48.23

10.296

23.05

42.77

Cor $\Delta = 37^\circ 23'$

Rad = 338.27'

Tang = 114.44'

Length = 219.90'

Hyd

Found P.K. 5-1970

Cor. Fe. Post
In Conc

80 Curve ht.

$\Delta = 21^\circ 14'$

Rad = 716.78'

Tang = 134.36'

Length = 265.42'

62.74

42.74

T.P.

Station

Ang. ht. Ang. Rt

606+05¹⁴ P.T.

S 77° 24' W

606+63⁶ P.I. 5° 40'

605+21⁸¹ P.C.

S 83° 04' W

598+05⁰⁵ P.I.

00° 15'

Sta - Ref

605+21.81 - 0°00'

606+00 - 0°47'

607+00 - 1044' cor. Fo.

608+00 - 20°47'

608+00 - 20°50'

2368

84.25

95.06

Cor.
Brick

28.03 0 T.P.

2° Curve. ht.

A = 5040.

Rad = 2864.99

Tang = 141.79.

Length = 283.33.

25.17 0 T.P.

T.P. 0 - 41.48

27.300 ctr Bell
Telephone Mt
81.60
40

T.P.

Hyd

Station

Ang. Ht. Ang. Rt

614 + 90 ³⁴ P.T.

N 45° 02' W

613 + 82 ⁴⁴ P.I.

35° 52'

612 + 66 ¹⁷ P.C.

612 + 56 ⁶⁵ P.T.

N 80° 54' W

611 + 49 ⁵ P.I.

210 42'

610 + 39 ⁶⁵ P.C.

4-12-26

Sta - Def

612+66⁷ - 0°00'

613+00 - 2°42'

+50 - 6°42'

614+00 - 10°42'

+50 - 14°42'

+90³⁴ - 17°56'

16° Curve Rt

$\Delta = 35° 52'$

Rad. 359.27

Tang = 116.27

Length = 224.17

65.1 - 0 T.P.

53.3 - 40 T.P.

Sta - Def

610+396⁵ - 0°00'

+50 - 0°31'

611+00 - 3°01'

+50 - 5°31'

612+00 - 8°01'

+50 - 10°31'

+86⁶⁵ - 10°51'

10° Curve Rt

$\Delta = 21° 42'$

Rad = 573.87

Tang = 109.95

Length = 217.00

G.P.

0 - 0 T.P.

43.620 P.P.

Iron

Station

Ang. W. Ang. R.

N 36° 45' W

633 + 56.28 P.T.

632 + 83.65 P.I.

51014'

631 + 96.68 P.C.

623 + 94.2 P.O.T.

618 + 38.59 P.T.

617 + 46.45 P.I. 42° 57'

N 87° 59' W

36

616 + 43.66 P.C.

$$631+96.65 = 0^\circ 00'$$

$$632+00 - 0^\circ 32'$$

$$+50 - 8^\circ 32'$$

$$633+00 - 16^\circ 32'$$

$$+50 - 24^\circ 32'$$

$$+56.75 - 25^\circ 37'$$

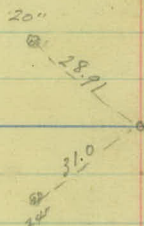
32° Curve H

$$\Delta = 51^\circ 14'$$

$$Rad = 181.39$$

$$Tang = 86.97$$

$$T.P. Length = 160.10$$



$$616+43.66 - 0^\circ 00'$$

$$617+00 - 6^\circ 14'$$

$$+50 - 11^\circ 44'$$

$$618+00 - 17^\circ 14'$$

$$+38.59 - 21^\circ 28'$$

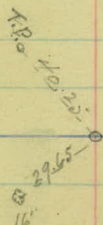
22° Curve H

$$\Delta = 42^\circ 57'$$

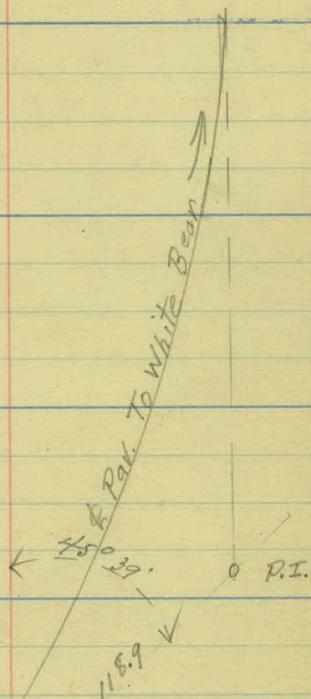
$$Rad = 262.04$$

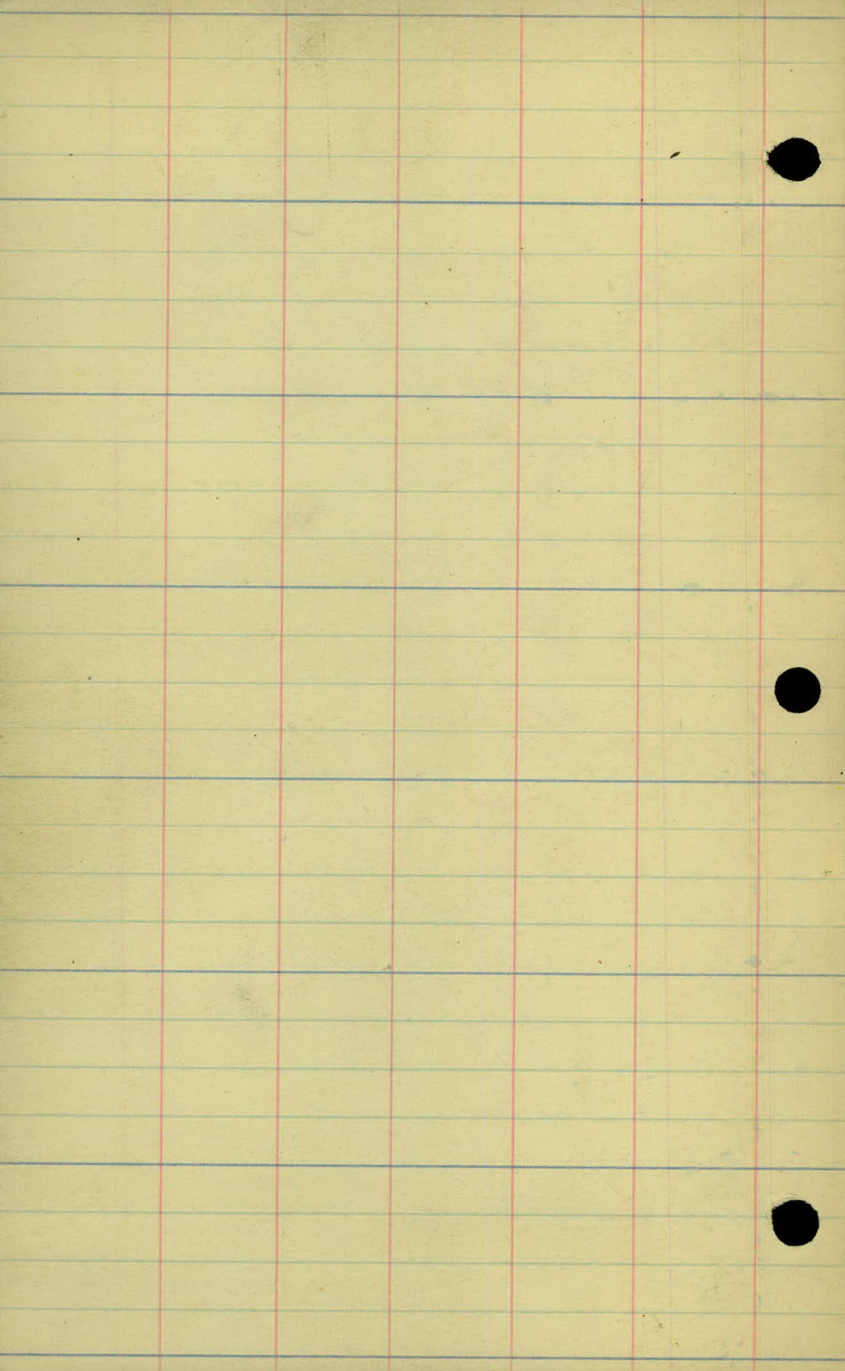
$$Tang = 103.09$$

$$Length = 195.23$$



636+09.1





3-6" Trees 48

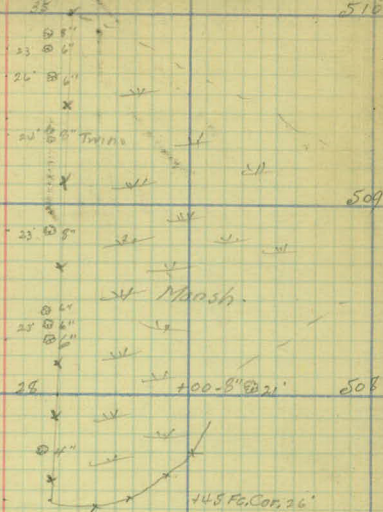
3-6" Trees 48 26

6" Trees 48 26

+51 - No Dumping Sign 15'

Cultivated

6" Trees 38 21



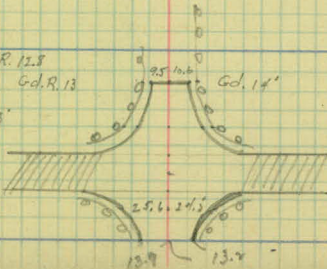
Cultivated band

Cultivated band

(5 Top)

+01 End. Gd. R. 14'
+93 Rd. Sign 15.5 Gd. R. 12.8
+64 Rd. Sign 22.5 Gd. R. 13
+62 Rd. Sign 23'
+60 Pav. 13.5 Gd. R. 23'

+20 Gd. Rail 42'
+13 Gd. Rail 28.5



+24 End. Gd. R. 14.8
+16 Gd. R. 13.8
Gd. R. 13.5
+84.5 End. Pav.
+60 Pav. 17.9 Gd. R. 22.1

+20 Gd. Rail 46'
+16 Gd. Rail 31

29

21

+89 - (2-3' @ 31')
 +76 (Clump 4-6" @ 31')

511

516

515

Cultivated land

Cultivated land

5' @ 25'

+60 F.E.

6' @ 20'
 6' @ 20'

514

+85 F.E.

+105 F.E. @ 33'

10' @ 10'
 10' @ 10'

22'

513

33'

512

+70 (Clump of Trees) 31'
 1/2" "

Cultivated land

Pasture

4" trees
 30'

35'

+04-12" @ 24'

511

BTwin 14"

10' @ 12"
 10' @ 10"

510

30'

20'

Cultivated hand

Cultivated hand

Cultivated hand

Cultivated hand

28' 20'

28' 20'

+95 Clamp 3-6" @ 29'

176-12" @ 28

PASTURE

ОРСНАРД

+ 71 T, P. 32'

188 F.E.

469 Fc. cor. 58'

465-12" @ 30.5

+82 Fc. Cor. 33

437 T.P. 32

$$+49 - (24^\circ \text{ to } 25^\circ)$$
 $+07(6^{\circ} 6' 20,5$

Cultivated land

+20 Drive

408-KR325

Pasture

4-38-10" @ 18"
+17-3(6" @ 19")

$280.12^{\circ} \pm 12'$ $+52 (12'' \pm 22')$
 $475 (6' \pm 11')$ $+65 T. P. 33'$
 $+60 F.C. Cor. 33'$

460 FC. Cor. 357

hard.

Form. 4 and

451. M. Box. 13' 6 ft.

+45¢ Private

Cultivated.

CaH. head

4th Trees →

524

29

20

535

29.5

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

X

-55-

29.5

29.5

33.5

33.5

31

32

0

0

0

0

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0

0

Cultivated

+59 T.P. 35

537

536

535

534

533

532

531

+37 M. Box. 14

+22 F. Line

+39 T.P. 34.5

+16 End. F.C. 36

FARM. YARD

+06 T.P. 35

+66 F. line

Cultivated land

ORCHARD

+66 T.P. 33

+81 F.C. line 33.5

+18-12" (3) 30'

+74 (clump 9-6" (3) 28'

POSS. CLUMP

ORCHARD

+16 T.P. 32.5

27 19

+92* Drive

X

X

Pasture

31.5

X

X

X

+04 F.C.H. 30.5

X X X

X

Cultivated land

X

X

30'

X

X

X

30.5

X

X

X

30'

X

X

X

29.5

X

X

X

32'

30'

Cult. land

Pasture

HERN YARD

Cultivated land

End. Fence

+25 T.P. 28.5

+03 F.C.H. 30'

+97 T.P. 29.5

+50 F. Drive

(4) 12" 10" 10" 10" +60-12" 32.2

+66 T.P. 31

+29 T.P. 32.5

+91 T.P. 33.5

542

543

544

541

546

539

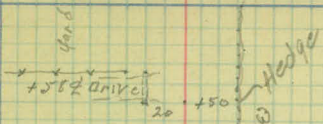
538

27' 18'

27' 19'

+99 (2-M. 13.5 N. 5)

+66 Fc. line 31
+48 M.B. 15.5



Hedge 31 552

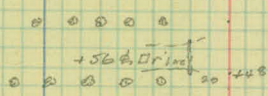
+75 P.P. 25'

Hedge 31 551

+63 P.P. 25'
12" x 16' C.M.P.

Hedge 31 550

+72 M.B. 13.5
12" x 16' C.M.P.



+34 P.P. 25'
12" x 16' C.M.P.
Hedge 31 549

+99 M.B. 13'
+81 T.P. 29.5

ORCHARD

+1052 Drive

+37 End Hedge 33'
+35 P.P. 39

+14 Beg. Hedge 34
10" x 40.5' C.M.P.

+87 End Hedge 39.5

+70 (2-M. Box 14.5)

+662 Drive

+35 Power line King
+36 P.P. 25'

+08 T.P. 25.5 548

+60 Beg. Hedge
+80 Fc. 33

12" x 16' C.M.P.

+11 T.P. 26.5 547

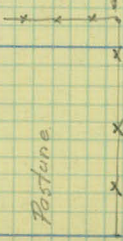
Hedge 34'

Farm land

Hedge

Farm land

+18 Beg. Hedge 33.3
+12 Fc. Cor. 33.5



+67 T.P. 29.5

546

545

29' 20'

28' 19'

Hedge

Gd. R. 12.5

559

+76 Rhine Xing

Hedge 33'

6" Trees

+50 Gd. R. 14.5

+28 End. Fc
+17 Fc. Cor. 23
+16-6" @ 21
+13 Beg. Gd. 18.5
+109 R.P. 38.5
12" X 31' C.M.P. 558

Hedge 33'

+78 R.R. Xing. Sign. 13.5

25

+82 T.P. 27

Hedge
Lawn

+29 P.P. 26

Hedge 32.5 557

+105 Hitch P. 20.5

+87 Hitch R. 21.3

+53 Hedge Cor. 33

+49 R.R. Xing P. 17

+45 P.P. 37

Power line Xing #41

+96 Drive

+40 Hedge Cor. 32
+57 R.P. 24
+40 P.P. 23
+38 Rd Sign 23
12" X 66.8 C.M.P.
+15.95 Track 556

+73 Hedge Cor. 33

+72 Rd. Sign. 30

12" X 40.3 C.M.P.

10.2 X 12.5 Waiting Sta.

+83 Xing Sign. 12.5

+79 Fc. Cor. 17

+58 P.P. 23

12" X 6 C.M.P.

+34.5 Steps / Wide

Hedge 34'

ORCHARD

552

Hedge 34'

+25 T.P. 23

+107 R.R. Sign. 13 554

12" X 14' C.M.P.

+226 Drive

Hedge 33.5

+60 R.P. 42.5

+77 Beg. Hedge 33

Yard

Yard

+39 Stop. Sign. 13

553

+95 P.P. 23
+91 Power line Xing
+60 R.R. Barrier P. 18.5
+58 Fc. Cor. 17
+50-8" @ 28.5

12" X 30.5' C.M.P.

+11 P.P. 24

+10 Hedge Cor. 33 552

12" X 16 C.M.P.

+12 Drive

28' 20'

39 28'

50 30

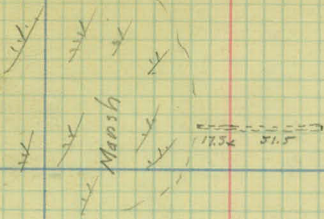
43 27'

35 24'

35 26

+50 39 25

30 19'



+65-8" @ 26.5
 +48-8" @ 31.5
 +45-8" @ 28'
 +40 Sharp Turn Sign 18'

+48 T.P. 34'

+24-24" x 69' C.M.S

563

+95 P.P. 31.5

+65-15" @ 30.5

+60 T.P. 35

+41-8" @ 28.5

+27-8" @ 27'

564

+85-3x3 Stone Post 26.3

+50 Hedge 29'

+30 3x3 Stone Post 27.3

+22 3x3 Stone Post 27'

Hedge 29'

+66-3x3 Stone P. 28.5
 +61 R. Drive
 +55-3x3 Stone P. 29.5
 +58 Fe. Cor. 30
 +53 M.B. 28.5
 +29 G.P. 27.5
 +34 Rd. Sign 20'
 +18 R.P. 26.5

+50 P.P. 35

+43 T.P. 44.5

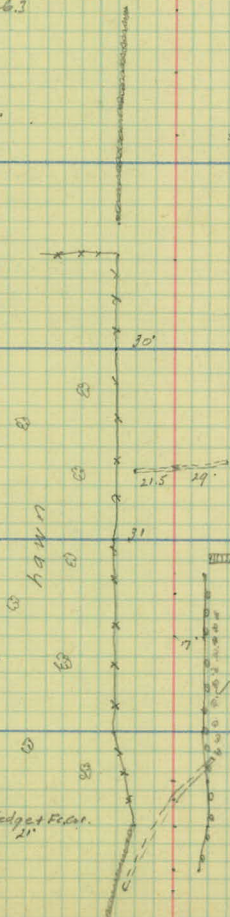
+16 Steps 29

+93 to the sign 24.5

563

+23 T.P. 31.5

562



+84 T.P. 28

+50 M.B. 15' Lt.

+32 R.R. Xing Sign 14'

Fence 31'

+6504 Xing P.
 12" x 86" C.M.P.
 +47 R.P. 19

+50 Hedge + Fence
 21'

+13 Culv. 25

+40-12" x 50.5' C.M.P.
 V.R.

+17 T.P. 32

561

+91-Steps 24'

+84 End Gd. R. 16

+64 End Willows

560

+96 T.P. 30.5

+87 Beg. Willows

+56 G.P. 23.5

+51-16" @ 29.5

Gd. R. 20'

+49 Rd. S. 22.5

+25 Gd. R. 15

+13 R.P. 27'

559

29' 20'

28' 22'

31' 22'

28' 20'

31' 22'

30' 20'

+99-10" E 38.5
12" X 42.5' C.M.P.
+67 Rd. 5.9 27
+62 M.B. 16

+68 20
+82 4 Drive

+30-12" @ 32'
+14 T.P. 30

+21 P.P. 24

+58 M.B. 14.5
12" X 16' C.M.P.

Walk
+77 17.5 20
+87

+92 4 Drive 12" X 16' C.M.P.

572

+32 Power Line Xing
+14 M.B. 12.5
12" X 16' C.M.P.

+14 T.P. 34'

+20 14.5 Ret. Wall 1' X 8.5' Concrete

+99 4 Drive 19.1 17

+89 M.B. 12.5

+61 P.P. 31.5

+67 14.5 Ret. Wall for Driveway 1' X 8.5' Concrete

571

+10 T.P. 26' 14
12" X 16' C.M.P.

+03 4 Drive 19.5 19

+16 M.B. 14.5
+70 Tah. Cable Xing

+25 End Hedge 31' E 33

+00 P.H. Xing 570

+19 Beg. Hedge 31'
10" X 16' C.M.P.
+66 Fe. Cor. 30'
+57-6' E 23.5
+32-12.6' @ 23'
+23 P.P. 23.5
+15 Fe. Cor. 28.5
10" X 16' C.M.P.

+06 Fe. Cor. 22.5 569

+82 M.B. 16'
12" X 22.5 C.M.P.

+66 4 Drive 19.5 20

+54 Fe. Cor. 27.5
+45 4 Drive 10" X 16' C.M.P.

+26 T.P. 28.5

568

+80-12" @ 31.5

+91 4 Drive 17.5 19.5
12" X 26.5 C.M.P.
+73 P.P. 34.5

+29 T.P. 38'

567

+62 M.B. 16'

+50 3 56
10" X 6' C.M.P.
+50 T.P. 39'
+42 P.P. 28.5
+26-12" @ 32'

566

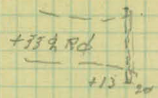
28'

22

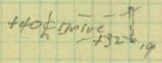
29'

22

+69-5 M. Box 14
 +55 T.P. 23.5
 12" X 40" C.M.P.
 +13 Rd. Sign 24'

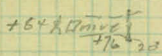


+78-12" X 37" V.P.
 +48 T.P. 24'
 12" X 16" C.M.P.
 +31 M.B. 15



+65-6" @ 27'
 +81-10" @ 30'
 +70-5" @ 29'
 +53 Fc. Cor. 36'
 +52 P.P. 22.5

12" X 16" C.M.P.
 +45-2 M.B. 15
 +38-10" X 8" C.M.P. 19.5
 +18 T.P. 25



+33-P.P. 15.5
 +14 1/2 Drive

+56 M. Box Rack 14.5
 +08-12" X 6"-16.5 ft
 +00 T.P. 21

+50 Fence 28'
 +31-8" @ 29'
 +16 P.P. 20'
 +14-24" @ 31'
 +99 G.P. 38'
 +75 1/2 Drive
 +70 Fc. Cor. 30

+69 1/2 Road
 +55 Rd Sign 24.5



+18-12" X 6" C.M.P. 19.

+15 P.P. 28
 +13 Fc. Cor. 31
 (12" X 14" C.M.P.)

+80-M. Box Rack 16.5
 +79 T.P. 26

+97 End. Hedge 31

+56-12" X 6"-22' H.

+51 Fc. Cor. 36
 +50-8" @ 31

+22-12" X 6"-10' H.

+31-10" @ 30

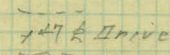
+03-T.P. 22

+04 Fc. Cor. 32
 +05-8" @ 27

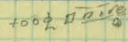
+83-10" @ 23

+84-P.P. 20

+68-10" @ 25
 +49-12" @ 22
 +45-10" @ 25



+16 M. Box Rack 14
 +12 T.P. 22
 +09 T.P. 22



Yards

Yard

Yard

29

22

587

+67 M.B. 18.5

+59 M.B. 17

10" X 14" C.M.P.
+16 T.P. 23.5

+73 $\frac{1}{2}$ Drive
+16 $\frac{1}{2}$

+93 P.P. 21.5

+172 Fc. Inc. 30.5

+43-6" $\odot$ 27.5
+41-12" $\odot$ 29.5

+19 $\frac{1}{2}$ Drive
+11 Fc. Cor. 32

+48 $\frac{1}{2}$ Drive
+90 P.P. 24.5

586

10" X 12" C.M.P.

+71 $\frac{1}{2}$ Drive
+65 $\frac{1}{2}$

+40-14" $\odot$ 24

12" X 20" C.M.P.
+17 T.P. 24

+11 $\frac{1}{2}$ Drive
+101 $\frac{1}{2}$

+88-2 M.B. 14

+50 M.B. 14.5

+15 T.P. 29.5

+90 $\frac{1}{2}$ Drive
+85 Fc. Cor. 29
+97-18" $\odot$ 24

+48 P.P. 24
+46 Fc. Cor. 29

+35 $\frac{1}{2}$ Drive
+22 Fc. Cor. 26
+10 $\frac{1}{2}$ Drive

584

+83 M. Box Rack 15

+63 Rd. Sign 26

+45 $\frac{1}{2}$ Road

+50 Fc. Cor. 28

+16 T.P. 25

583

+98 P.P. 26

10" X 16" C.M.P.

+60 $\frac{1}{2}$ Drive
+72 $\frac{1}{2}$

+03 M.B. 14

+92 $\frac{1}{2}$ Cor. 12" X 6" C.M.P. 16 1/2
+96 T.P. 21

+60 M.B. 13

+51 $\frac{1}{2}$ Culv. 12" X 6" C.M.P. 16 1/2

+16 $\frac{1}{2}$ Drive
+10 $\frac{1}{2}$

Hedge 31
+80 P.P. 28.5

+54-6" $\odot$ 29
+51 Hedge Cor. 3
10" X 14" C.M.P.

+45 $\frac{1}{2}$ Drive
+38 $\frac{1}{2}$

Hedge 31

+03 $\frac{1}{2}$ Culv. 12" X 6" C.M.P.

581

12" X 16" C.M.P.

+71 $\frac{1}{2}$ Drive
+63 $\frac{1}{2}$

+84 $\frac{1}{2}$ Drive
+76 $\frac{1}{2}$

10" X 16" C.M.P.
+76 T.P. 23

+27 $\frac{1}{2}$ Drive
+19 $\frac{1}{2}$

+32 P.P. 28
10" X 16" C.M.P.

580

29' 21'

+62 P.P. 24.5

+93 T.P. 25

594

+42 P.P. 24

+55 T.P. 24

593

+79 M.B. Rack 14

+77-8" @ 25

+55 Catch Basin 25

Scattered Timber band

Dense Timber band

+68 T.P. 24

592

+24-12" X 65' V.P.

+21 P.P. 21.5

+11-12" @ 33

+14 M.B. 15

+09-12" @ 29

+99 T.P. 22

+87-4" @ 27

Catch Basin

+40 A. H.V.

+32 Tel. line Xing

+17 Rd. Sign 21

+Bellaine Ave

+95-15" @ 16

591

+35-6" @ 26

+17 T.P. 24

590

+67 M.B. 19

+63 P.P. 30

12" X 18" C.M.P.

+445

+36 T.P. 30

+54 X Drive

+445

+445 X Drive

+22 G.P. 24

589

+56 Power line Xing

+52 T.P. 27

+30 M.Box Rack 20

10" X 40.5' C.M.P. +03 1/2 St.

+48

+55 X Drive

+42-6" P. 31

+33-18" @ 32

+16-12" @ 29

+14 P.P. 22

+13-6" @ 30

+11-8" @ 26.5

+02-6" @ 27

588

+74 Rd. Sign 29 (3rd Ave

+52-10" @ 32.5

+44 T.P. 36

+53

+83-8" @ 26

+78-6" @ 26

+64-12" @ 27

+57-12" @ 27.5

+49-16" @ 24

+34 Tel. line 30

587

30

27' 20'

31' 20'

+3 P.P. 22

+27 T.P. 24

Timber land

+41 M.B. 155

+37 Drive (10" X 18" C.M.P.)
+28

+65 P.P. 21

+92 T.P. 25

+71 P.P. 24.5
+68 M.B. 16

+58 Drive
+79 T.P. 26

+86 Drive 10" X 18" C.M.P.
+77

+39 P.P. 24

+57 T.P. 25

Timber land

Timber land

+36-2 M.B. 17

+32 Drive 10" X 18" C.M.P.
+27

+18 P.P. 25

+26 T.P. 25.5

+14 Powerline Xing

32

22

+50 P.P. 20

+39 T.P. 22

+71 P.P. 26

Pasture

+17 Fe. Cor. 30

+19 P.P. 25

+07 P.P. 24

+03 M.B. 17

+00 Power line Xing

+93 M.B. 15.0

+69 P.P. 23

timber land

Tennis Court

+91 Court 40

+55 T.P. 22

+54 Tennis Court 15

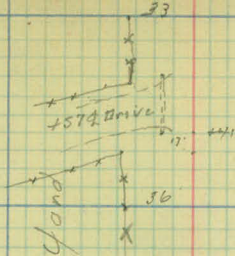
+30 Drive

36' 22'

33 24'

+77 M.B. 16.5
 +67 F.C. Cor. 32
 +64 5" 53 2.5
 15" X 31" C.M.P.

+30 G.P. 26.5
 +29 F.C. Cor. 38



+190 Bay Tree 29

+28 T.P. 22.7"

+57 P.P. 31.5
 +41-8" 53

+66 G.P. 16

+107 T.P. 20.5

+67 G.P. 24

+105 T.P. 24'

+76 P.P. 24'

+29 Lake Sign 20'

+83 G.P. 22

+93 Powerline Xing
 +86 T.P. 28'

+34 P.P. 26'

Pasture

Lake. Front

+68 T.P. 26'

+98 P.P. 27
 +95 Lake Sign 17

+48 T.P. 23'

30' 20'

34' 21

33. 20'

491-18" @ 22.0

+70 T.P.P. 32.5

468 T. P. 27

 $450 - 8'' \approx 23.5$

+29 M.B. 12.5

 $+69-8'' \approx 22.8$

150 Φ Drive

439. 4" E 22'

4 20. 2" @ 20'

499-5" @ 22.5"

455-2" E 20°

 $472.2^{\circ} \text{E} @ 20'$

+ 49 T. P. 27'

443 P.P. 27

+ 24 Curve Sign 14.5

+19 Power line xing

 $+13-24'' @ 25.5$

493 M.B.16

~~***~~ +55 Fe, Cor 39.2-

+45 4 Opine

 $435 \text{ km} \text{ d} / \text{hr} = 30$

184 P. P. 32

12" x 24, 8

+ 35 M. B. 16.5

+ 21 P. P. 53

421 T.P. 26

493 X Fence 34'

+0.4 g Gaive (12" x 20" C.M.P)

196 Fe. Cor 32

1981.05.01

+ 96 T.P. 24.

484 P.P. 3013

+67 $\frac{1}{2}$ Drive 12" x 20" C.M.P.

+14 Tel. Cable Xing

12" x 16" C.M.P.

403 G.P. 20.

184 T.P. 17'

432 P.D. 26.5

162 Powenhire Xing

+ 60 Fc. COB 30

+ 59 T.R. 17

✓ 03 P. B. 19

6.5

30 22

+99 M.B. 17

+66 T.P. 25.5

+66 Power line Xing

+21 P.P. 27

+66 T.P. 27

+65 M.B. 16

+93 P.P. 32

+49 T.P. 26.5

+46 M.B. 17

+69 T.P. 27

+67 P.P. 31.5

+59 & Drive

12" X 16" C.M.P.

+75-24" @ 21.5

+58 Fc. Cor. 33

+49-16" @ 25

+36 P.P. 31.5

+26 M.B. 19

+12-24" @ 23

+06 T.P. 26.5

+86-8" @ 21.5

+72-24" @ 24

+33-24" @ 23

+01-15" @ 24

+90 P.P. 32

+90 T.P. 16.5

+61-16" @ 23.5

+12-20" @ 22.5

+91-19

+91 & Drive 12" X 16" C.M.P.

+57 P.P. 23

+45 & St.

+15 End Hedge 34

+98-8" @ 28

+66-6" @ 25

+35-6" @ 28

+16-5" @ 25

10" X 18" C.M.P.

+98-10" @ 28

+77-4" @ 27.5

+58-6" @ 20

+56 Beg. Fc.

+56 End Fc. 34

12" X 16" C.M.P.

+93 P.P. 32

+79 Power line Xing

1' Con. Ret. wall

+46-2" @ 25

+21-2" @ 24

+93-2" @ 24

12" X 22.5 C.M.P.

+67-2" @ 24

+40-2" @ 24

+12-2" @ 24

+63-24" @ 23.5

+55-30" @ 23

+26-30" @ 23

End Fc. 34

+93-15" 23

+62-12" @ 22

+51-18" @ 23

+66 Fc. line

+05-15" @ 23.5

Hedge Form.

Shore

ORCHARD

416

32

22

55

24

29

19

+39 P.P. 25.8
+34 Rd. Sign 24.5

+02 G.P. 24

+53 F.C. Cor 27

+76 P.P. 27

+22 M.B. 12.5
+21 P.P. 25.5
+12 Cump. 3-12" (6)
12" X 24.5 C.M.P.

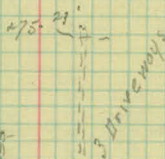
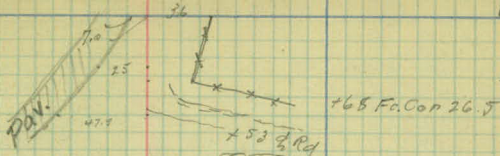
+03 Drive

+91 27.5

+93 M.B. 14.5
+77-10" X 8" C.M.P. +92 E. Walk

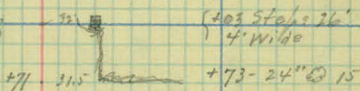
+53 M.B. 15.5

+10 P.P. 26



12" X 31.5 C.M.P.

+75 P.R. Hang on Sign
18' Rd



+38 E Rd
+23-12" X 40" V.P.

630

630

634

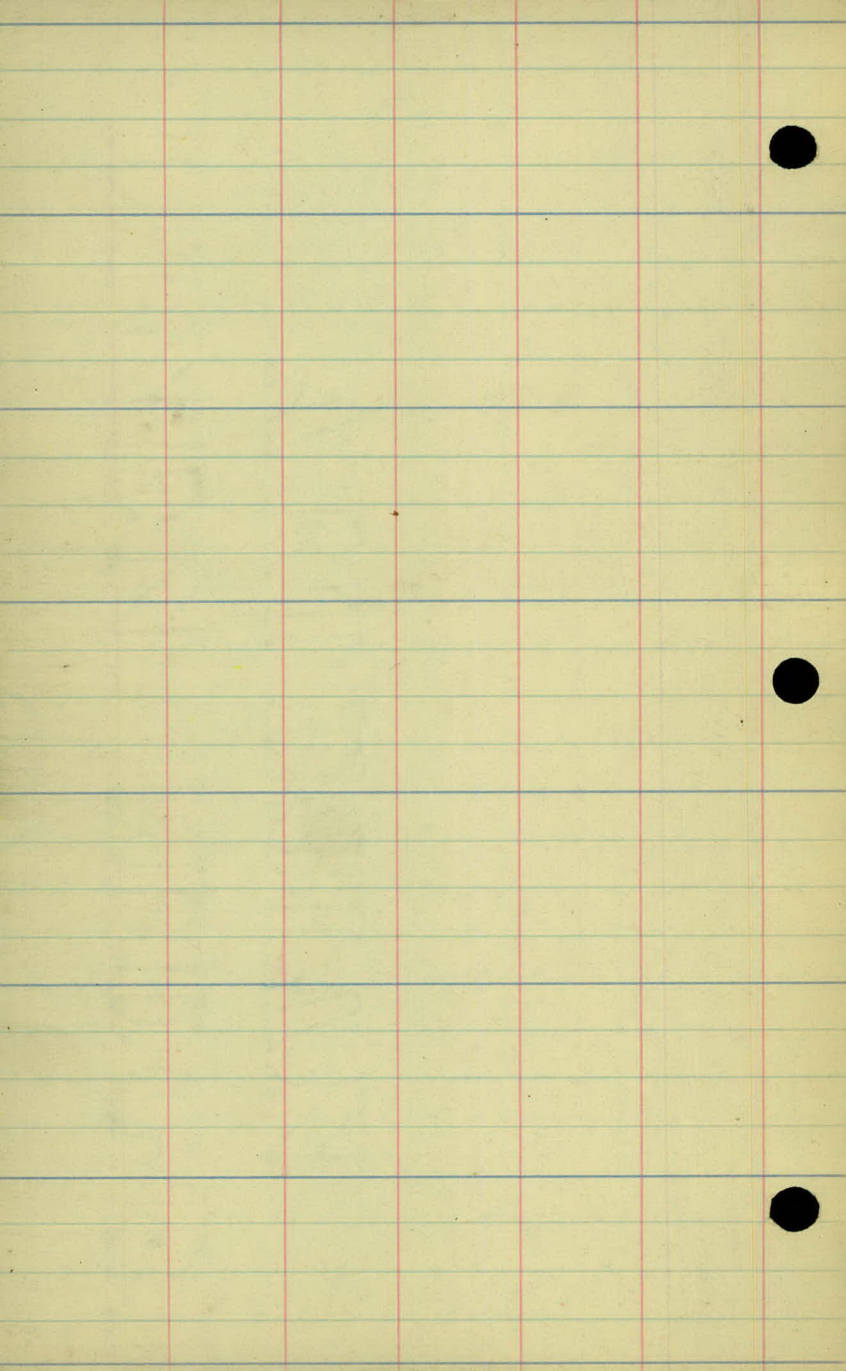
633

632

631

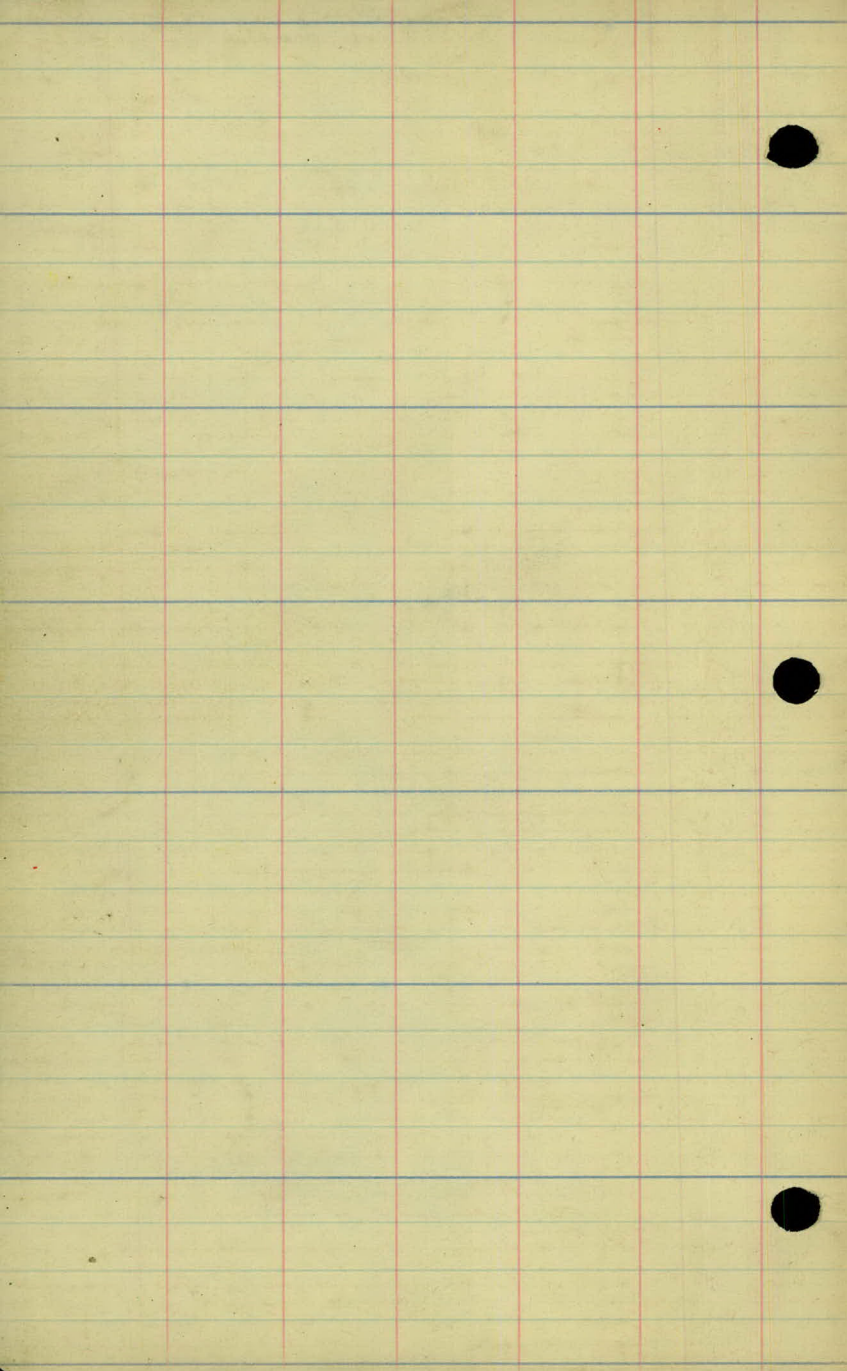
630

629



637

636



Final X-sec.

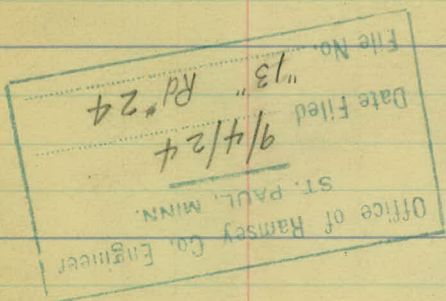
Maint. Project.

Acct #24

White Bear Blvd Road.

Sta. 0+00 to 78+08.85-78+14.5

15 pages.



Station	+	H.I	-	Elev.
B.M.	0.92	256.64 ✓		255.72
T.P.	0.31	245.07 ✓	11.88	244.76
T.P.	2.44	238.30 ✓	9.21	235.86

0+00

Note: No X-sec. Required.
Work covered by Paving Project.

1+50 5.0 233.3

2+00 5.4 232.9

2+50 3.5 232.8

3+00 5.8 232.5

3+50 5.6 232.7

4+00 5.0 233.3

4+50 4.2 234.1

5+00 3.0 235.3

5+50 1.8 236.5

T.P. 9.31 246.71 ✓ 0.90 237.40 ✓

6+00 9.3 237.4

Lt. 2 Rt.

R.R. spike 24" Maple 35' Lt. 13+15

W.H.G. }
Eck } Aug 12, 24
Gohm }
Franke }

$\frac{5.3}{33}$ $\frac{5.6}{24}$ $\frac{5.3}{16}$ $\frac{5.0}{33}$ $\frac{5.4}{11}$ $\frac{5.7}{25}$ $\frac{4.6}{33}$

(5.6)

$\frac{8.2}{33}$ $\frac{7.5}{22}$ $\frac{5.7}{17}$ $\frac{5.4}{33}$ $\frac{5.6}{14}$ $\frac{5.9}{16}$ $\frac{7.5}{21}$ $\frac{6.2}{33}$

(5.6)

$\frac{9.0}{33}$ $\frac{8.4}{20}$ $\frac{6.1}{16}$ $\frac{5.5}{33}$ $\frac{6.1}{17}$ $\frac{8.7}{21}$ $\frac{8.5}{16}$ $\frac{8.0}{27}$ $\frac{7.9}{33}$

(5.6)

$\frac{8.7}{33}$ $\frac{9.0}{22}$ $\frac{5.8}{17}$ $\frac{5.8}{33}$ $\frac{6.2}{12}$ $\frac{6.9}{17}$ $\frac{9.1}{21}$ $\frac{9.1}{29}$ $\frac{9.1}{33}$

(5.8)

$\frac{7.0}{33}$ $\frac{7.5}{23}$ $\frac{5.7}{20}$ $\frac{5.9}{15}$ $\frac{5.6}{33}$ $\frac{6.0}{10}$ $\frac{6.3}{15}$ $\frac{9.7}{21}$ $\frac{9.5}{16}$ $\frac{8.8}{27}$ $\frac{9.0}{33}$

(5.8)

$\frac{6.8}{33}$ $\frac{7.8}{21}$ $\frac{5.7}{17}$ $\frac{5.6}{8}$ $\frac{5.0}{33}$ $\frac{5.2}{14}$ $\frac{5.6}{20}$ $\frac{8.0}{25}$ $\frac{8.2}{33}$

(5.6)

$\frac{4.8}{33}$ $\frac{4.8}{19}$ $\frac{4.5}{7}$ $\frac{4.2}{33}$ $\frac{4.4}{12}$ $\frac{4.9}{18}$ $\frac{7.1}{24}$ $\frac{7.1}{33}$

(4.3)

$\frac{3.1}{33}$ $\frac{3.5}{22}$ $\frac{3.2}{15}$ $\frac{3.0}{33}$ $\frac{3.3}{11}$ $\frac{3.3}{14}$ $\frac{4.9}{18}$ $\frac{4.0}{25}$ $\frac{1.9}{29}$ $\frac{2.1}{33}$

(3.8)

(2.4)

$\frac{0.0}{33}$ $\frac{0.0}{30}$ $\frac{2.4}{26}$ $\frac{3.6}{22}$ $\frac{3.6}{18}$ $\frac{2.2}{14}$ $\frac{2.0}{13}$ $\frac{3.6}{17}$ $\frac{3.8}{26}$ $\frac{0.3}{31}$ $\frac{0.2}{33}$

(9.4)

$\frac{2.9}{33}$ $\frac{7.4}{31}$ $\frac{10.5}{26}$ $\frac{10.9}{19}$ $\frac{9.7}{15}$ $\frac{9.3}{33}$ $\frac{9.5}{13}$ $\frac{10.6}{17}$ $\frac{10.8}{24}$ $\frac{10.0}{28}$ $\frac{7.8}{31}$ $\frac{7.8}{33}$

Station	+	H.I	-	Elev.
		246.71		
6+50			8.2	238.5
7+00			7.2	239.5
7+50			5.5	241.2
8+00			3.9	242.8
8+80			2.5	244.2
T.P.	11.91	257.10	1.52	245.19
9+00			11.5	245.6
9+50			9.9	247.2
10+00			8.2	248.9
10+50			6.8	250.3
11+00			5.7	251.4
11+30			5.0	252.1
11+40			4.8	252.3
11+50			4.6	252.5

21

x

RT

3

(8.3)

10.1	7.9	8.7	8.2	8.8	10.6	10.3	9.3	9.3
33	25	14		14	21	28	31	33

(7.3)

10.0	9.5	9.2	7.8	7.7	7.2	7.6	9.3	10.1	10.1	9.4
33	27	18	15	12		14	19	21	32	33

(5.6)

6.7	6.3	7.0	7.2	6.0	5.5	6.2	8.3	8.5	7.4
33	22	20	17	15		16	21	32	33

(3.9)

3.8	4.0	5.2	5.2	4.2	3.9	4.4	6.5	6.3	5.2
33	22	21	17	14		16	21	30	33

(2.5)

3.5	3.1	3.5	3.5	2.8	2.5	2.9	4.8	5.0	3.6
33	23	20	18	15		14	30	31	33

10/1/10 T.P. RT. Sta. 7+30 (11.5)

13.1	12.3	13.3	13.2	11.8	11.5	11.8	13.5	13.9	12.4
33	24	21	18	15		14	19	30	33

(9.8)

orig	orig	11.3	11.7	11.4	10.6	9.9	10.6	11.7	11.8	9.3
33	22	20	17	15		16	20	27	33	

(8.2)

orig	9.6	10.1	10.0	9.0	8.2	8.9	9.9	10.1	7.0
33	22	21	18	16		16	19	27	33

(7.0)

6.6	6.6	7.1	7.1	6.8	6.8	7.5	8.5	8.2	4.5	4.2
33	25	23	18	15		17	20	24	31	33

(5.8)

1.6	2.4	6.1	7.0	6.9	6.0	5.7	6.3	7.3	7.3	1.6
33	30	26	21	18	15		16	19	24	33

0.8	0.9	3.2	6.2	6.0	5.2	5.0	5.6	6.7	6.7	1.2
33	30	24	20	18	15		16	20	24	33

(5.0)

1.2	1.3	5.1	5.8	5.9	5.1	4.8	5.0	4.8	4.0
33	30	24	20	18	15		16	28	33

(4.8)

4.0	4.3	5.6	5.6	5.0	4.6	5.1	5.8	5.5	4.7	4.1
33	23	21	18	16		16	19	21	25	33

Station	+	H.I	-	Elev.
		257.10		
12+00			3.9	253.2
12+50			3.0	254.1
13+00			2.7	254.4
B.M.	4.90	260.62 ✓	1.38	255.72
13+50			5.8	254.8
14+00			5.6	255.0
14+50			5.5	255.1
15+00			5.0	255.6
15+50			4.7	255.9
16+00			4.4	256.2
16+50			4.0	256.6
17+00			4.2	256.4
17+50			4.8	255.8
18+00			5.1	255.5
T.P.	2.85	257.75 ✓	5.72	254.90

Lt.

2

Rt.

4

(3.9)

4.1	4.0	5.0	5.1	4.4	3.9	3.6	3.6
<u>33</u>	<u>23</u>	<u>20</u>	<u>18</u>	<u>15</u>	<u>19</u>	<u>19</u>	<u>33</u>

(3.4)

3.2	3.2	4.0	4.2	3.5	3.0	3.6	3.2	3.5
<u>33</u>	<u>22</u>	<u>20</u>	<u>18</u>	<u>16</u>	<u>18</u>	<u>20</u>	<u>20</u>	<u>33</u>

(2.8)

3.2	3.2	3.7	3.6	3.2	2.7	2.9	3.6	3.8	4.0
<u>33</u>	<u>22</u>	<u>20</u>	<u>17</u>	<u>15</u>	<u>16</u>	<u>16</u>	<u>17</u>	<u>20</u>	<u>33</u>

(Same as Fall out 2.11.)

(R.R. Spike in 24" Maple 35' Lt. 13 + 15')

(6.0)

7.4	6.8	7.2	7.3	6.5	5.8	6.2	7.6	8.2
<u>33</u>	<u>22</u>	<u>20</u>	<u>18</u>	<u>15</u>	<u>13</u>	<u>16</u>	<u>33</u>	

(5.6)

7.8	6.8	7.5	7.3	6.1	5.6	5.7	7.2	7.7	7.2	7.6
<u>33</u>	<u>21</u>	<u>20</u>	<u>16</u>	<u>14</u>	<u>7</u>	<u>12</u>	<u>16</u>	<u>19</u>	<u>21</u>	<u>33</u>

(5.3)

9.6	8.9	5.8	5.5	5.9	8.8	8.5
<u>33</u>	<u>18</u>	<u>13</u>	<u>0</u>	<u>14</u>	<u>20</u>	<u>33</u>

(5.0)

7.3	6.7	5.3	5.0	5.4	8.6	8.4
<u>33</u>	<u>19</u>	<u>14</u>	<u>13</u>	<u>13</u>	<u>19</u>	<u>33</u>

(4.7)

4.9	5.4	4.9	4.7	6.5	6.2	5.4	5.6
<u>33</u>	<u>19</u>	<u>16</u>	<u>16</u>	<u>16</u>	<u>20</u>	<u>22</u>	<u>33</u>

(4.5)

6.9	5.9	4.7	4.4	4.4	6.2	6.0	5.6	4.8	5.1
<u>33</u>	<u>18</u>	<u>15</u>	<u>12</u>	<u>12</u>	<u>16</u>	<u>20</u>	<u>22</u>	<u>24</u>	<u>33</u>

(4.4)

4.8	4.7	4.6	4.0	4.1	5.4	5.0	3.7	3.6
<u>33</u>	<u>23</u>	<u>15</u>	<u>13</u>	<u>13</u>	<u>17</u>	<u>24</u>	<u>25</u>	<u>33</u>

(4.3)

2.8	3.3	4.8	5.0	4.1	4.2	4.9	4.9	4.4	4.1
<u>33</u>	<u>25</u>	<u>21</u>	<u>18</u>	<u>16</u>	<u>15</u>	<u>17</u>	<u>21</u>	<u>25</u>	<u>33</u>

(4.7)

4.0	4.5	5.9	6.0	5.1	4.8	4.8	5.8	5.3	2.5	only gr.
<u>33</u>	<u>25</u>	<u>21</u>	<u>19</u>	<u>17</u>	<u>15</u>	<u>15</u>	<u>17</u>	<u>21</u>	<u>26</u>	<u>33</u>

(5.1)

5.9	5.6	7.1	7.1	5.4	5.1	5.2	6.2	6.1	2.8	only gr.
<u>33</u>	<u>24</u>	<u>21</u>	<u>19</u>	<u>17</u>	<u>16</u>	<u>16</u>	<u>19</u>	<u>21</u>	<u>26</u>	<u>33</u>

station	+	H.I. ✓ 257.75	-	Elev.
18+50			2.9	254.9
19+00			3.8	254.0
19+50			5.2	252.6
20+00			6.6	251.2
20+50			7.5	250.3
21+00			9.0	248.8
21+50			10.2	247.6
22+00			11.5	246.3
T.P.	0.17	249.12 ✓	9.40	248.35
22+50			4.0	245.1
23+00			5.8	243.3
23+50			7.6	241.5
24+00			9.5	239.6
24+50			11.1	238.0

Lt.

L

Rt.

5

(3.0)

2.1	1.8	4.4	4.2	3.2	2.9	3.2	3.9	4.0	1.1	1.0
<u>33</u>	<u>26</u>	<u>22</u>	<u>18</u>	<u>16</u>	<u>17</u>	<u>20</u>	<u>24</u>	<u>29</u>	<u>33</u>	

(4.0)

1.9	1.5	5.0	5.0	4.1	3.8	3.9	5.0	4.8	2.0	2.1
<u>33</u>	<u>30</u>	<u>23</u>	<u>21</u>	<u>19</u>	<u>15</u>	<u>18</u>	<u>22</u>	<u>27</u>	<u>33</u>	

(5.4)

5.5	7.0	6.6	5.5	5.1	5.2	5.5	6.2	6.4	4.7	4.5
<u>36</u>	<u>33</u>	<u>27</u>	<u>23</u>	<u>9</u>	<u>15</u>	<u>18</u>	<u>21</u>	<u>26</u>	<u>33</u>	

(6.9)

(Assumed)

9.1	7.8	7.3	6.7	6.7	6.6	6.9	6.5	7.4	7.4	6.1	6.0
<u>33</u>	<u>31</u>	<u>22</u>	<u>19</u>	<u>14</u>	<u>7</u>	<u>17</u>	<u>23</u>	<u>24</u>	<u>27</u>	<u>33</u>	

16.2	13.1	8.2	7.9	7.5	7.7	8.5	8.4	4.2	4.0	
<u>33</u>	<u>27</u>	<u>18</u>	<u>14</u>	<u>18</u>	<u>17</u>	<u>19</u>	<u>22</u>	<u>30</u>	<u>33</u>	

20.2	17.1	9.5	9.2	9.0	9.0	9.6	9.5	8.6	3.5	
<u>33</u>	<u>21</u>	<u>16</u>	<u>10</u>	<u>9.1</u>	<u>16</u>	<u>18</u>	<u>21</u>	<u>32</u>	<u>33</u>	

(10.4)

21.0	17.3	11.0	10.6	10.2	10.2	10.7	10.5	3.3	3.3	
<u>33</u>	<u>24</u>	<u>15</u>	<u>11</u>	<u>17</u>	<u>20</u>	<u>23</u>	<u>32</u>	<u>33</u>		

(11.6)

21.8	19.3	12.3	12.0	11.5	11.1	11.8	11.5	4.3		
<u>33</u>	<u>25</u>	<u>15</u>	<u>12</u>	<u>18</u>	<u>21</u>	<u>24</u>	<u>33</u>			

Nail in T.P. Lt. 21+35 (4.1)

17.7	12.0	5.0	4.0	3.7	4.7	4.7				
<u>46</u>	<u>34</u>	<u>21</u>	<u>12</u>	<u>15</u>	<u>20</u>					

(5.9)

Aug. 18, 24

13.2	12.0	6.4	5.8	5.5	6.1	5.7				
<u>38</u>	<u>30</u>	<u>21</u>	<u>10</u>	<u>12</u>	<u>15</u>					

(7.8)

13.0	12.0	8.1	7.6	7.7	8.4	8.1				
<u>41</u>	<u>32</u>	<u>25</u>	<u>10</u>	<u>11</u>	<u>16</u>					

(9.5)

14.9	9.8	9.5	9.5	9.4	10.4	10.1	1.4			
<u>40</u>	<u>28</u>	<u>13</u>	<u>7</u>	<u>10</u>	<u>13</u>	<u>24</u>				

(11.3)

14.1	11.6	11.1	11.1	11.6	14.1	14.1	11.0	RT	5.9	
<u>37</u>	<u>30</u>	<u>12</u>	<u>6</u>	<u>12</u>	<u>18</u>	<u>22</u>	<u>25</u>	<u>33</u>		

[end of cut]

Notes
See next page
of 6

Station	+	H.I	-	Elev
		249.12		
T.P.			11.03	238.09
T.P.	10.86	259.21	0.77	248.35
22+50				
23+00				
23+50				
24+00				
T.P.	1.32	248.57	11.96	247.25
T.P. (as above)	2.21	246.36	10.48	238.09
25+00			3.7	236.7
D.M.			4.41	235.95
25+50			4.4	236.0
26+00			4.5	235.9
+50			4.6	235.8
27+00			4.6	235.8
+50			4.6	235.8
28+00			4.7	235.7
28+50			4.8	235.6

Lt.

2

Rt.

6

Top. Rock 44480

Na. / in T.P. 2485

(14.2)

120	3.8
30	28

(16.0)

2.7	0.1
31	40

(17.9)

9.0	3.1
27	33

10.2	5.8
28	41

10

top Rock 44450

(38)

76	42	3.6	3.7	40	5.8	7.0	7.6	7.6
43	30	12		8	10	16	28	33

(B.M. R.R. spike P. Pole Lt. 25+15)

89	5.1	46	4.4	4.4	5.0	7.7	8.0	7.9
44	30	25	12	(4.8)	10	15	25	33

(47)

92	5.2	45	4.7	5.3	7.9	7.8
36	22		8	16	22	33

(47)

9.1	7.8	5.4	4.6	5.0	7.3	7.1	8.0	8.1
33	24	18		15	21	26	29	33

(46)

9.9	9.2	5.4	5.0	4.6	4.8	5.4	7.7	7.4	8.0
33	29	18	8		14	19	25	32	33

(47)

7.6	7.6	5.2	4.8	4.6	5.0	5.5	7.8	7.8	7.0
33	22	16	10		17	21	27	31	33

(48)

9.9	8.8	5.4	5.0	4.7	4.7	5.4	6.8	7.8	7.3
33	22	16	7		9	20	24	31	33

(50)

10.0	9.8	8.5	5.7	5.0	4.8	4.9	5.6	7.6	7.7
33	25	21	13	6		10	20	25	33

Station	+	H.I.	-	Elev.
		240.36		
29+01.8			3.0	235.4
29+50			4.7	235.7
30+00			4.6	235.8
+50			4.1	236.3
31+00			3.4	237.0
T.P.	10.25	247.21	3.40	236.96
+50			9.0	238.2
32+00			7.6	239.6
+50			5.7	241.5
33+00			4.0	243.2
T.P.	7.19	253.56	2.84	244.37
+50			8.8	244.8
34+00			7.2	246.4
B.M.	7.76	260.22	1.10	252.46
34+50			12.6	247.6
35+00			11.0	249.2

Lt.

L

Rt.

7

(5.2)

13.2	9.5	8.0	5.4	5.2	5.0	4.9	5.3	8.0	8.9
33	27	19	12	8	9	19	26	33	

(4.9)

9.4	3.6	5.4	4.7	4.7	5.1	8.8	9.5
33	20	13	10	18	25	33	

(4.8)

8.8	7.7	5.0	4.8	4.8	5.2	9.6	10.7
33	21	15	8	9	18	25	33

(4.1)

7.8	7.1	5.8	4.5	4.0	4.4	4.8	10.5	11.4
33	24	19	16	10	9	17	26	33

(3.5)

6.5	6.0	6.8	6.8	3.6	3.4	3.6	4.0	9.0	9.3
33	26	24	23	18	9	10	17	24	33

No. 1 L.Rt. 31400

(8.9)

9.4	9.5	10.5	10.5	9.3	8.9	9.2	7.7	12.3	12.0	10.4
33	27	24	21	18	8	11	20	26	29	33

(7.5)

7.0	8.0	8.7	8.8	7.7	7.5	7.7	8.1	10.6	10.7	10.9
33	25	23	20	17	9	10	18	23	27	33

(5.8)

4.1	4.3	6.7	6.7	5.7	5.7	5.8	6.4	8.0	8.0	7.1	7.1
33	28	22	18	16	11	17	21	26	29	23	

(4.1)

1.4	1.4	5.2	5.2	4.3	4.0	4.2	4.4	5.2	5.0	2.4	2.4
33	27	21	17	15	8	10	17	20	24	29	33

(8.9)

4.2	4.2	9.7	9.7	8.8	8.8	8.8	9.0	9.9	9.6	7.0	6.8
33	28	21	17	14	8	10	17	20	24	28	33

(7.3)

2.4	2.4	8.4	8.4	7.1	7.3	7.4	7.5	8.9	8.2	6.3	6.7
33	30	27	17	15	11	9	16	24	28	33	

Sp. 16 M T.P. 20' Rt. 36775

(2.5)

10.3	11.0	13.4	13.4	12.6	12.8	12.6	12.6	13.0	14.2	14.3	12.0	12.2
33	27	23	20	18	12	7	15	18	22	25	33	

(11.0)

11.4	11.1	12.2	12.2	11.3	11.0	11.2	11.5	13.1	13.1	12.6	13.2
33	24	21	19	16	9	9	14	17	23	25	33

Station	+	H.I	-	Elev.
		260.22		
35+50			9.6	250.6
36+00			8.2	252.0
36+50			6.9	253.3
37+00			5.5	254.7
37+50			3.9	256.3
38+00			2.4	257.8
T.R	5.27	264.38 ✓	1.11	259.11
38+50			5.3	259.1
39+00			4.8	259.6
39+50			4.7	259.7
40+00			4.8	259.6
40+50			5.4	259.0
41+00			4.3	258.1
41+50			7.5	256.9

21

2

Rt.

8

10.5	10.8	10.2	9.6	9.6	9.6	9.8	12.1	12.0	10.8	10.3
33	20	18	9	9.7	7	13	18	22	25	33

11.2	10.6	8.4	8.3	8.2	8.4	8.5	10.8	10.9	9.1	9.1
33	20	18	7	8.1	8	13	17	22	27	33

12.1	12.0	7.4	7.0	6.9	7.0	7.0	9.5	9.1
33	25	16	8	7.0	8	13	18	33

9.1	8.9	5.6	5.5	5.5	5.8	6.1	8.9	8.4
33	20	14	7	5.5	7	14	20	33

5.0	5.5	4.2	4.1	3.9	4.0	4.1	7.0	7.0
33	20	15	8	3.8	7	14	19	33

1.0	1.7	3.8	3.9	2.7	2.7	2.7	4.4	4.0	4.2
33	27	22	17	15	2.1	15	18	26	33

1.7	3.3	6.3	6.5	5.5	5.3	5.8	7.1	6.9	4.2	4.7
33	28	23	18	15	5.6	15	17	21	26	33

1.3	2.7	5.5	5.8	5.0	4.8	4.9	6.1	6.0	5.8	1.9
33	28	23	20	17	4.8	16	18	22	28	33

1.1	3.0	5.2	5.2	4.3	4.7	4.7	5.7	5.5	0.8	0.6
33	28	23	19	18	4.9	16	18	21	28	33

1.5	4.2	5.4	5.8	4.8	4.8	5.0	5.9	5.9	1.1	1.4
33	27	24	20	18	4.9	16	18	22	29	33

1.7	3.6	6.3	6.7	5.7	5.4	5.4	6.2	6.2	1.2	1.6
33	27	22	19	16	5.7	15	17	20	27	33

5.3	4.7	7.9	8.0	6.5	6.3	6.5	7.1	6.7	1.2	1.2
33	30	23	18	16	6.5	17	19	22	29	33

9.5	8.9	9.5	9.6	7.7	7.5	7.4	8.1	7.7	1.8	1.8
33	27	24	20	17	7.8	17	20	22	30	33

station	t	H.I.	-	Elev.
		264.38		
42+00			8.8	255.6
42+50			10.5	253.9
T.P.	1.44	255.09	10.73	253.65
43+00			2.8	252.5
43+50			4.1	251.0
44+00			5.4	249.7
44+50			6.8	248.3
45+00			8.4	246.7
+30			9.1	246.0
+40			9.1	246.0
+75			9.5	245.6
45+85			9.5	245.6
46+50			9.1	246.0
T.P.	1.45	253.15	9.39	245.70
47+00			6.6	246.6

14

2

21.

9

$\frac{7.3}{33}$ $\frac{10.9}{26}$ $\frac{11.4}{23}$ $\frac{9.4}{20}$ $\frac{9.3}{15}$ $\frac{8.8}{9.0}$ $\frac{9.1}{15}$ $\frac{9.9}{19}$ $\frac{9.9}{22}$ $\frac{6.7}{28}$ $\frac{6.5}{33}$

$\frac{13.2}{33}$ $\frac{14.0}{20}$ $\frac{11.1}{16}$ $\frac{10.5}{10.7}$ $\frac{10.5}{15}$ $\frac{13.0}{20}$ $\frac{12.8}{33}$

$\frac{6.0}{33}$ $\frac{5.7}{19}$ $\frac{3.4}{15}$ $\frac{2.8}{3.0}$ $\frac{2.8}{13}$ $\frac{6.2}{20}$ $\frac{6.3}{33}$

$\frac{7.9}{33}$ $\frac{7.1}{18}$ $\frac{4.5}{14}$ $\frac{4.1}{4.3}$ $\frac{4.1}{14}$ $\frac{7.5}{20}$ $\frac{7.2}{33}$

$\frac{7.4}{33}$ $\frac{6.9}{23}$ $\frac{7.4}{21}$ $\frac{7.2}{18}$ $\frac{5.7}{14}$ $\frac{5.4}{5.6}$ $\frac{5.6}{14}$ $\frac{7.2}{17}$ $\frac{7.1}{20}$ $\frac{5.6}{23}$ $\frac{5.4}{33}$

$\frac{7.5}{33}$ $\frac{6.8}{24}$ $\frac{8.1}{21}$ $\frac{8.3}{17}$ $\frac{7.0}{14}$ $\frac{6.8}{7.1}$ $\frac{6.9}{14}$ $\frac{7.9}{16}$ $\frac{7.1}{20}$ $\frac{5.8}{23}$ $\frac{5.7}{33}$

$\frac{7.0}{33}$ $\frac{9.4}{24}$ $\frac{9.8}{21}$ $\frac{9.8}{18}$ $\frac{8.6}{15}$ $\frac{8.4}{8.7}$ $\frac{8.5}{14}$ $\frac{9.2}{16}$ $\frac{9.1}{19}$ $\frac{6.9}{23}$ $\frac{6.9}{33}$

$\frac{7.9}{33}$ $\frac{7.1}{30}$ $\frac{7.8}{27}$ $\frac{11.0}{25}$ $\frac{11.0}{24}$ $\frac{10.0}{21}$ $\frac{9.5}{12}$ $\frac{9.1}{9.1}$ $\frac{9.4}{13}$ $\frac{10.0}{15}$ $\frac{9.8}{18}$ $\frac{7.0}{22}$ $\frac{7.9}{33}$

$\frac{11.3}{38}$ $\frac{11.7}{33}$ $\frac{11.1}{31}$ $\frac{10.8}{29}$ $\frac{10.4}{19}$ $\frac{9.7}{11}$ $\frac{7.1}{9.2}$ $\frac{9.6}{11}$ $\frac{10.0}{16}$ $\frac{10.2}{18}$ $\frac{7.3}{23}$ $\frac{8.1}{33}$

$\frac{12.2}{33}$ $\frac{11.2}{20}$ $\frac{10.0}{10}$ $\frac{9.5}{9.6}$ $\frac{9.6}{12}$ $\frac{9.7}{25}$ $\frac{9.9}{33}$

$\frac{11.5}{33}$ $\frac{11.1}{25}$ $\frac{10.5}{14}$ $\frac{9.7}{8}$ $\frac{9.5}{9.7}$ $\frac{9.8}{14}$ $\frac{10.6}{15}$ $\frac{10.6}{17}$ $\frac{8.8}{21}$ $\frac{8.1}{33}$

$\frac{12.1}{33}$ $\frac{11.5}{18}$ $\frac{9.1}{15}$ $\frac{9.1}{9.4}$ $\frac{9.4}{15}$ $\frac{10.2}{18}$ $\frac{10.2}{21}$ $\frac{9.8}{23}$ $\frac{9.2}{33}$

$\frac{9.7}{33}$ $\frac{7.9}{17}$ $\frac{6.8}{14}$ $\frac{6.6}{6.9}$ $\frac{6.8}{12}$ $\frac{7.0}{16}$ $\frac{7.4}{19}$ $\frac{7.3}{21}$ $\frac{4.0}{25}$ $\frac{3.6}{30}$ $\frac{3.0}{33}$

Station	+	H.I	-	Elev.
		253.15		
47+50			6.1	247.1
48+00			5.6	247.6
48+50			5.0	248.2
B.M.	9.15	255.96	6.34	246.81
49+00			7.4	248.6
49+50			6.2	249.8
50+00			5.5	250.5
50+50			4.7	251.3
51+00			4.0	252.0
51+30			3.5	252.5
52+00			2.8	253.2
T.P.	3.83	257.96	1.83	254.13
52+50			4.4	253.6
53+00			4.5	253.5
53+50			4.4	253.6

L

L

At.

10

9.2	7.6	6.5	6.1	6.0	6.9	6.7	5.4	2.7
33	23	11	(6.4)	19	21	24	29	33

5.9	6.4	6.8	5.9	5.6	5.8	6.5	6.5	2.1
33	28	22	16	(6.0)	20	22	26	34

7.2	6.2	5.4	5.0	5.2	6.0	6.0	0.9	0.5
33	28	18	(5.5)	19	21	23	29	33

Nail in T.P. 30' Lt. 48+52

10.6	10.4	8.3	7.5	7.4	7.1	7.1
33	28	18	12	(7.5)	18	33

7.0	7.1	6.4	6.2	6.4	7.2	7.0	5.3	4.2	3.0
33	20	13	(6.5)	17	19	23	25	31	31

4.4	5.0	6.4	6.0	5.7	5.5	5.8	6.5	6.3	4.6	4.0	0.6
33	23	20	17	13	(5.5)	18	19	20	24	29	33

4.2	4.6	5.5	5.2	4.7	5.1	5.6	5.4	3.5	3.2
33	24	22	19	(4.8)	15	16	20	23	33

3.3	4.0	4.4	4.4	4.0	4.2	5.0	4.9	2.9	2.4
33	24	19	15	(4.1)	18	17	20	23	33

0.9	1.3	4.4	4.0	3.5	4.8	4.8	3.3	2.4
33	24	18	14	(3.7)	17	18	23	33

3.7	3.1	4.0	4.0	3.6	2.4	3.2	4.2	4.0	2.5	2.3
33	21	19	18	16	(2.9)	14	16	20	23	33

Nail in R.P. Lt. 52+50

Aug. 19. 1924

4.3	4.5	4.8	4.8	4.4	4.5	5.0	5.6	5.6	4.7	4.4
33	19	16	11	(4.6)	10	15	17	20	22	33

5.1	5.3	5.3	5.0	4.5	4.7	5.6	5.6	5.1	4.0
33	18	16	14	(4.6)	15	17	20	21	33

4.3	4.7	6.1	5.8	4.9	4.4	4.4	4.2	3.5
33	21	18	16	13	(4.6)	13	20	33

station	+	H.I	-	Elev.
		257.96		
54400			4.6	253.4
54450			4.9	253.1
55100			5.7	252.3
55450			6.5	251.5
56100			7.4	250.6
56450			8.4	249.6
57100			9.0	249.0
57450			9.9	248.1
T.P.	408	251.68	10.36	247.60
58100			4.1	247.6
58450			4.4	247.3
59100			4.6	247.1
59450			4.9	246.8
60100			5.1	246.6

Lt.

Z

Rt.

(11)

5.5	5.4	6.5	6.5	5.3	4.6	4.8	5.5	5.4	4.4	3.7	17
33	24	21	18	15	4.7	15	17	20	22	39	34

4.7	4.2	6.2	6.4	5.9	5.4	4.9	5.2	6.0	5.9	4.7	4.0	18
33	23	20	17	15	13	4.9	14	16	18	21	28	33

7.3	6.6	7.2	7.3	6.3	5.7	6.1	6.8	6.7	5.5	4.8	2.4
33	21	18	16	13	5.8	13	15	18	20	29	34

8.2	7.3	7.9	7.9	7.0	6.5	6.9	7.7	7.5	5.7	5.1	3.1
33	19	18	16	13	6.8	14	16	18	21	30	36

8.4	7.8	8.9	8.8	7.9	7.4	7.8	8.7	7.8	6.8	5.7	4.2
33	22	19	16	14	7.7	14	16	18	21	31	37

9.5	9.2	9.9	9.8	8.9	8.4	8.8	9.6	9.7	8.6	8.3
33	22	20	17	15	8.5	15	17	18	21	33

10.3	10.3	10.9	10.8	9.7	9.0	9.5	10.3	10.6	9.7	9.9
33	22	19	17	16	9.2	13	16	18	21	33

13.6	12.5	11.0	10.3	9.9	9.9	11.4	11.5	10.6	10.4
33	24	18	13	9.8	15	18	21	22	33

8.2	6.6	4.7	4.1	4.2	6.0	6.0	4.0	3.4
33	24	19	4.1	14	16	20	24	33

8.0	7.1	5.1	4.4	4.9	6.3	6.1	4.7	4.3
33	22	16	4.3	16	18	21	25	33

6.4	6.4	6.1	5.2	4.6	4.6	6.0	6.0	4.7	4.0
33	27	20	17	4.6	16	18	20	22	33

6.9	6.7	6.5	5.3	4.4	5.0	6.0	6.0	4.8	4.0
33	26	20	13	4.8	15	17	20	23	33

8.0	7.6	7.4	6.1	5.1	5.1	6.2	6.1	4.9	4.3	2.5
33	25	19	16	5.0	15	18	21	24	27	33

station	+	H.I	-	Elev
		251.68		
60+50			4.9	246.8
B.M.	5.40	251.68 ✓	3.40	246.28
61+00			5.2	246.5
61+18			5.3	246.4
+25			5.2	246.5
+45			5.4	246.3
61+50			5.4	246.3
62+00			5.6	246.1
62+50			6.1	245.6
T.P.	4.99	245.70 ✓	6.97	244.71
63+00			4.7	245.0
63+50			5.0	244.7
64+00			4.9	244.8
64+50			5.0	244.7
65+00			4.8	244.9

Lt.

R

Rt.

12

8.0	7.6	7.0	5.4	4.9	4.9	5.1	6.2	6.2	2.8	0.0
33	24	16	13	(4.9)	9	17	20	23	30	34

Spike in P.P. 12' Lt. 60+75

7.3	6.4	6.0	5.3	5.2	5.1	4.8	5.5	5.2	1.3
33	18	7	4	(5.6)	13	24	26	30	36

7.3	7.1	6.2	5.6	5.3	5.0	4.6	5.2	5.1	0.4
33	27	15	5	(5.7)	13	28	29	34	41

7.2	6.2	5.6	5.2	5.1	4.5	3.7
33	17	6	(5.7)	19	28	33

6.4	5.6	6.1	5.7	5.4	5.4	5.0	5.1
33	17	12	7	(5.8)	12	27	33

6.0	5.6	6.4	5.7	5.4	5.5	5.2	5.5	2.1
33	16	12	10	(5.8)	12	23	30	34

7.0	6.5	7.9	7.9	6.1	5.6	6.0	6.0	6.9	6.7	3.6	1.6
33	18	16	14	10	(6.0)	12	20	22	26	30	33

9.6	7.2	7.2	6.5	6.1	6.5	6.6	7.4	7.5	6.6	4.6
33	23	18	14	(6.2)	9	18	20	23	25	33

Top Side Drain 62+70

10.4	9.2	4.8	4.7	5.0	6.1	6.2	5.8	5.5	3.9
33	25	19	(4.6)	14	16	19	20	25	33

8.7	8.4	5.3	5.0	5.6	5.7	6.9	6.6	6.0
33	25	17	(4.8)	13	15	19	20	33

8.5	8.0	5.4	4.9	5.3	5.5	6.5	6.7	5.8	6.1
33	18	24	(5.0)	11	20	21	23	25	33

6.0	5.7	6.9	6.9	5.4	5.0	5.2	6.5	6.6	5.0	4.5	
33	20	18	13	11	(5.1)	9	20	23	26	30	33

5.5	4.8	6.3	6.2	5.2	4.8	4.7	4.8	6.6	6.8	4.6	2.6
33	22	18	13	9	(5.2)	9	20	23	26	30	33

Station	+	H.I	-	Elev.
		249.70		
65+50			4.9	244.8
66+00			5.0	244.7
66+50			5.1	244.6
67+00			5.0	244.7
67+50			5.3	244.4
T.P.	8.87	253.20	5.37	244.33
68+00			8.9	244.3
68+23			9.0	244.2
68+31			9.0	244.2
68+40			9.0	244.2
68+48			9.0	244.2
69			9.2	244.0
70+50			10.9	243.3
T.P.	1.22	243.33	11.09	242.11
70+00			3.0	240.3

$\frac{4.3}{33}$	$\frac{4.2}{29}$	$\frac{5.3}{27}$	$\frac{5.3}{23}$	$\frac{6.7}{20}$	$\frac{6.6}{13}$	$\frac{5.4}{10}$	$\frac{4.9}{9}$	$\frac{4.8}{9}$	$\frac{4.9}{19}$	$\frac{6.8}{23}$	$\frac{6.8}{25}$	$\frac{3.8}{30}$	$\frac{3.6}{33}$
							(5.0)						

$\frac{5.2}{33}$	$\frac{5.7}{21}$	$\frac{6.7}{18}$	$\frac{6.7}{12}$	$\frac{5.4}{10}$	$\frac{5.0}{9}$	$\frac{4.9}{19}$	$\frac{7.1}{22}$	$\frac{7.0}{24}$	$\frac{4.4}{27}$	$\frac{4.9}{33}$
					(4.9)					

$\frac{6.4}{33}$	$\frac{6.4}{22}$	$\frac{7.2}{20}$	$\frac{6.9}{12}$	$\frac{5.2}{9}$	$\frac{5.1}{9}$	$\frac{5.0}{19}$	$\frac{5.0}{19}$	$\frac{7.0}{22}$	$\frac{7.0}{24}$	$\frac{4.3}{29}$	$\frac{3.7}{33}$
					(5.1)						

$\frac{6.8}{33}$	$\frac{6.7}{19}$	$\frac{7.1}{16}$	$\frac{7.4}{12}$	$\frac{5.4}{9}$	$\frac{5.0}{9}$	$\frac{4.7}{9}$	$\frac{4.7}{20}$	$\frac{7.4}{23}$	$\frac{7.4}{27}$	$\frac{4.2}{29}$	$\frac{4.0}{33}$
					(5.0)						

$\frac{6.6}{33}$	$\frac{6.3}{17}$	$\frac{7.4}{14}$	$\frac{7.4}{12}$	$\frac{5.7}{9}$	$\frac{5.3}{9}$	$\frac{4.8}{10}$	$\frac{4.9}{21}$	$\frac{7.2}{24}$	$\frac{7.1}{29}$	$\frac{0.6}{27}$
					(5.3)					

$\frac{10.2}{33}$	$\frac{9.1}{18}$	$\frac{11.0}{15}$	$\frac{1.4}{12}$	$\frac{7.1}{10}$	$\frac{8.7}{9}$	$\frac{8.8}{9}$	$\frac{8.8}{22}$	$\frac{10.6}{25}$	$\frac{10.6}{28}$	$\frac{4.2}{32}$
					(8.7)					

$\frac{7.8}{33}$	$\frac{8.8}{20}$	$\frac{10.9}{15}$	$\frac{10.8}{12}$	$\frac{7.1}{9}$	$\frac{9.0}{9}$	$\frac{8.7}{8}$	$\frac{8.3}{23}$	$\frac{10.2}{26}$	$\frac{10.1}{30}$	$\frac{3.8}{29}$
					(9.0)					

$\frac{7.6}{33}$	$\frac{8.6}{22}$	$\frac{10.8}{16}$	$\frac{10.7}{12}$	$\frac{9.5}{10}$	$\frac{9.0}{9}$	$\frac{8.7}{11}$	$\frac{8.2}{23}$	$\frac{8.0}{26}$	$\frac{7.8}{30}$	$\frac{7.0}{40}$
					(9.0)					

$\frac{7.6}{33}$	$\frac{8.4}{21}$	$\frac{11.1}{18}$	$\frac{11.1}{11}$	$\frac{9.3}{10}$	$\frac{7.0}{9}$	$\frac{8.7}{11}$	$\frac{8.2}{22}$	$\frac{8.1}{25}$	$\frac{7.9}{28}$	$\frac{7.2}{37}$
					(9.1)					

$\frac{7.4}{33}$	$\frac{9.6}{23}$	$\frac{10.0}{16}$	$\frac{11.0}{14}$	$\frac{7.4}{11}$	$\frac{9.0}{9}$	$\frac{8.9}{9}$	$\frac{8.7}{20}$	$\frac{10.1}{23}$	$\frac{10.1}{26}$	$\frac{3.5}{38}$
					(9.1)					

$\frac{5.8}{33}$	$\frac{7.9}{22}$	$\frac{11.2}{17}$	$\frac{11.2}{14}$	$\frac{8.9}{13}$	$\frac{9.2}{9}$	$\frac{9.4}{8}$	$\frac{7.6}{17}$	$\frac{11.4}{20}$	$\frac{11.4}{21}$	$\frac{0.5}{36}$
					(9.2)					

$\frac{8.1}{33}$	$\frac{7.1}{22}$	$\frac{12.5}{17}$	$\frac{12.5}{15}$	$\frac{11.4}{13}$	$\frac{10.9}{9}$	$\frac{11.0}{8}$	$\frac{10.9}{16}$	$\frac{12.9}{20}$	$\frac{12.9}{22}$	$\frac{5.0}{35}$
					(11.0)					

$\frac{0.2}{36}$	$\frac{0.7}{24}$	$\frac{3.8}{20}$	$\frac{3.8}{17}$	$\frac{3.1}{15}$	$\frac{3.0}{9}$	$\frac{3.0}{8}$	$\frac{3.3}{17}$	$\frac{4.6}{20}$	$\frac{4.9}{24}$	$\frac{1.2}{33}$
					(3.0)					

Station	+	H.I	-	Elev.
		243.33		
70+50			4.5	238.8
B.M.	1.25	240.16	4.42	238.91
71+00			2.8	237.4
71+50			4.6	235.6
72+00			4.8	235.4
72+50			4.7	235.5
73+00			5.0	235.2
73+50			5.2	235.0
T.P.	9.93	244.33	5.76	234.40
74+00			9.5	234.8
74+50			9.4	234.9
75+00			9.1	235.2
75+50			8.9	235.4
76+00			8.4	235.9
76+50			7.3	237.0

Lt. R. Rf.

4.5	4.7	5.7	5.8	4.6	4.5	4.7	4.7	5.8	5.8	5.5	5.8
33	25	23	21	19	45	9	14	18	23	27	33

Nail in P.O.P. Lt. Sta. 70+60

5.7	4.7	3.1	2.8	2.8	3.2	8.2
33	22	18	9	28	14	33

6.8	6.4	4.6	4.6	4.6	4.7	8.1	10.5
33	24	18	8	4.7	12	19	33

6.6	6.2	5.2	5.0	4.8	5.1	7.4	7.6
33	20	16	8	4.9	12	18	33

8.1	8.1	7.2	6.3	5.3	5.0	4.7	5.0	5.5	6.5	6.3
33	28	23	19	18	8	4.9	8	16	21	33

8.8	6.1	5.3	5.0	5.5	6.4	7.2	6.5
33	27	13	5.0	10	15	20	33

9.3	6.4	5.4	5.2	5.5	6.2	7.1	6.4
43	38	16	5.2	7	14	20	33

Nail in Guj Pole Lt. 74+75 (Aug 20, 24)

14.0	10.1	9.7	9.5	9.8	10.6	11.3	11.3
48	39	15	9.4	7	13	17	33

14.3	10.3	9.5	9.4	9.6	10.7	11.0
48	40	19	9.3	8	16	33

14.1	10.2	9.6	9.1	9.4	10.0	11.4	10.9	11.0
43	36	15	9.1	5	10	13	20	33

14.3	9.7	9.0	8.9	9.0	9.3	11.4	11.0	11.0
37	30	12	8.7	6	11	16	22	33

14.1	9.8	8.7	8.3	8.4	8.5	9.0	11.0	11.0
33	24	19	11	8.3	7	11	18	33

14.0	8.0	7.2	7.3	7.6	10.8	11.0	11.0
33	24	11	6.8	10	20	24	33

Station	+	H.I	-	Elev.
		244.33		
77+00			5.2	239.1
77+50			3.8	240.5
78+00			1.1	242.2
78+08.85 = 78+14.5 End of Proj			0.5	243.8
<u>B.M.</u>			3.43	240.90

Lt.

E

Rt.

15

$\frac{13.2}{34}$	$\frac{6.0}{22}$	$\frac{4.8}{14}$	$\frac{5.2}{5.2}$	$\frac{5.6}{8}$	$\frac{6.3}{14}$	$\frac{10.2}{22}$	$\frac{10.2}{33}$
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$\frac{10.2}{42}$	$\frac{3.3}{31}$	$\frac{3.3}{14}$	$\frac{3.8}{3.7}$	$\frac{4.0}{11}$	$\frac{7.2}{16}$	$\frac{8.2}{33}$
-------------------	------------------	------------------	-------------------	------------------	------------------	------------------

$\frac{6.0}{33}$	$\frac{5.6}{25}$	$\frac{1.0}{16}$	$\frac{1.1}{1.4}$	$\frac{1.7}{15}$	$\frac{6.0}{21}$	$\frac{7.0}{33}$
------------------	------------------	------------------	-------------------	------------------	------------------	------------------

$\frac{4.7}{33}$	$\frac{5.0}{24}$	$\frac{0.3}{16}$	$\frac{0.5}{0.5}$	$\frac{1.0}{14}$	$\frac{6.4}{22}$
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R.R. spike in P.O. 13' Rt. Sta 77+55

Finished

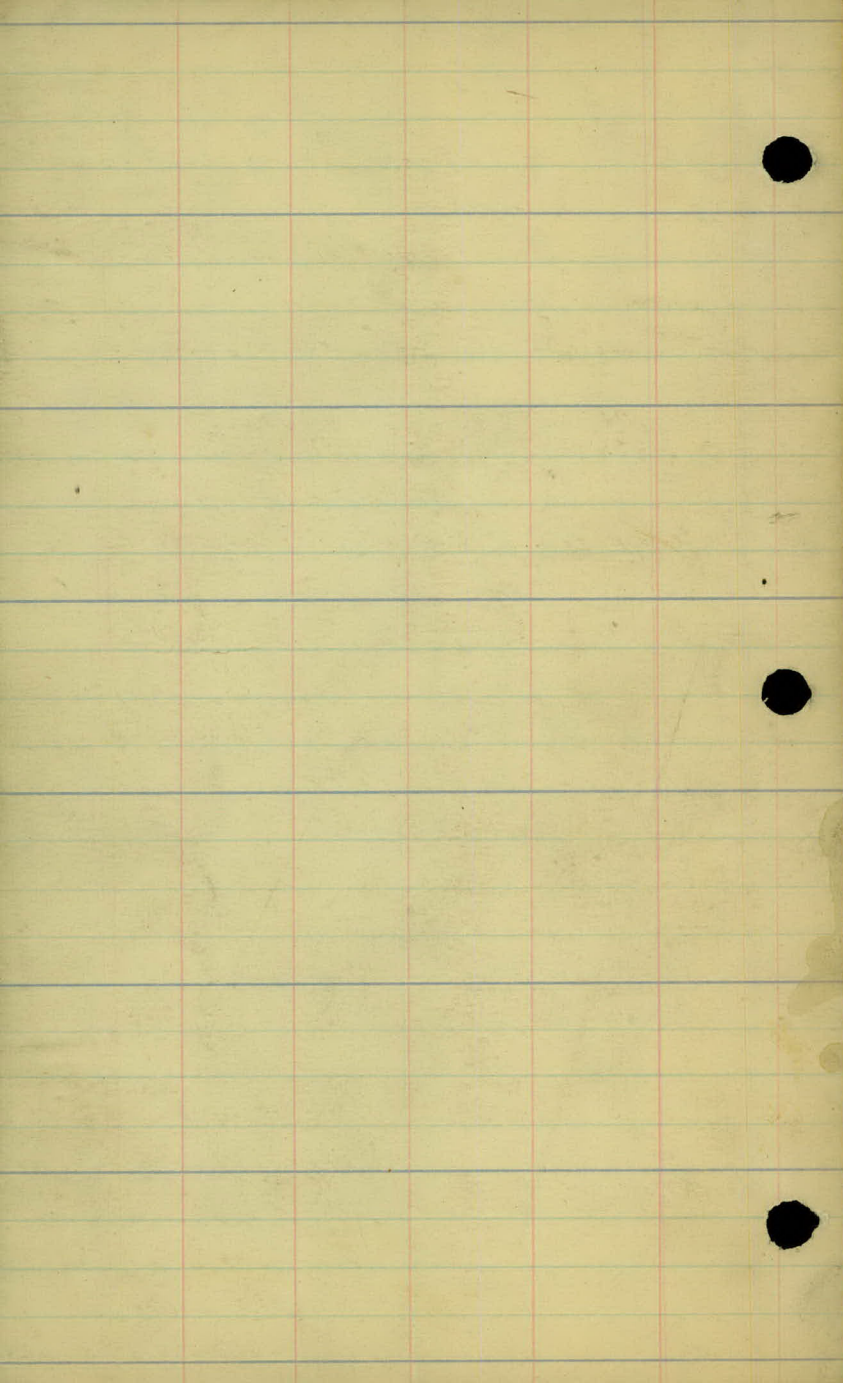
W.H.C.

Eck.

Calvin

Franko

Aug 20, 1974



Reduced & plotted by C.M.N 9/16/59

South Shore Blvd.

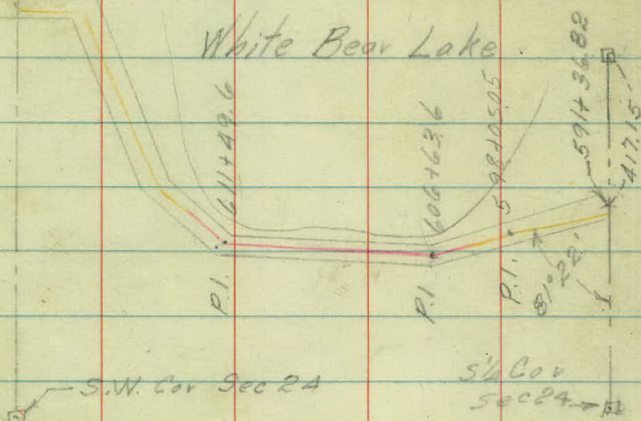
Schneider Bay Area

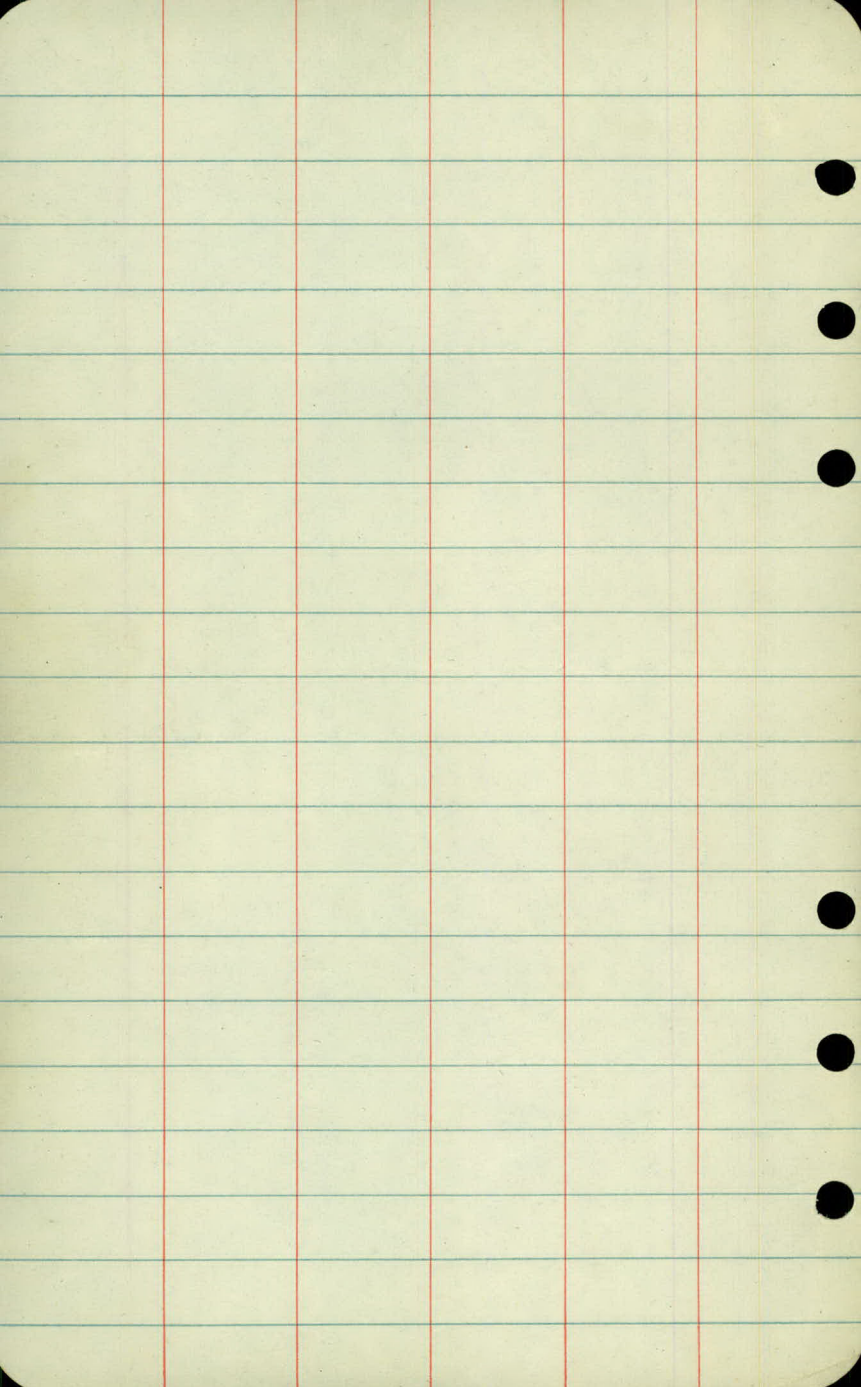
Lake front



10 Pages

D.R. Auklan
3101 W. Owasco Blv.

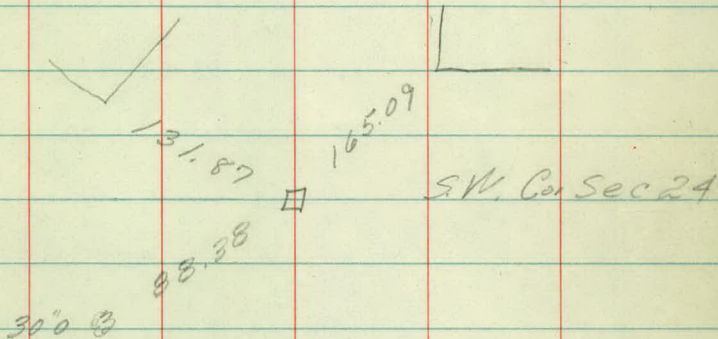




Sept. 10, 1959

2

Alignment



Sta Point Δ RT

612+56.65 PT

$$\Delta = 21^{\circ}42'$$

$$D = 10^{\circ}$$

611+49.6 P1

$$21^{\circ}42' T = 109.95$$

$$L = 217.00$$

$$R = 573.87$$

610+39.65 PC

608+05.14

446.25

606+63.60 PT

$$\Delta = 5^{\circ}40'$$

$$D = 2^{\circ}$$

606+63.6 P.I. $5^{\circ}40'$

$$T = 141.79$$

$$L = 283.33$$

$$R = 2864.93$$

605+21.81 PC

598+05.05 P.I.

$$00^{\circ}15'$$

Sept. 10, 1959

3

ctr. M.H. °

ctr. M.H. °

22.26

22.65

⊕

23.38

ctr. w.s.o. °

Hyd. ♂

17.17

ctr. M.H. ° 43.92

Boat Spike

33.37

Disk
° P.P.

115.00

ctr. M.H. °

Boat Spike

Sta Point ΔL ΔR

618+93.07 W. Line Sec 24

618+38.59 P.T.

54.48

$\Delta = 42^{\circ} 57'$

$D = 22^{\circ}$

617+46.45 P.I. $42^{\circ} 57'$

$T = 103.09$

$L = 195.23$

$R = 262.04$

616+43.36 P.C.

614+90.24 P.T.

$\Delta = 35^{\circ} 52'$

$D = 16^{\circ}$

613+82.44 P.I.

$35^{\circ} 52' T = 116.27$

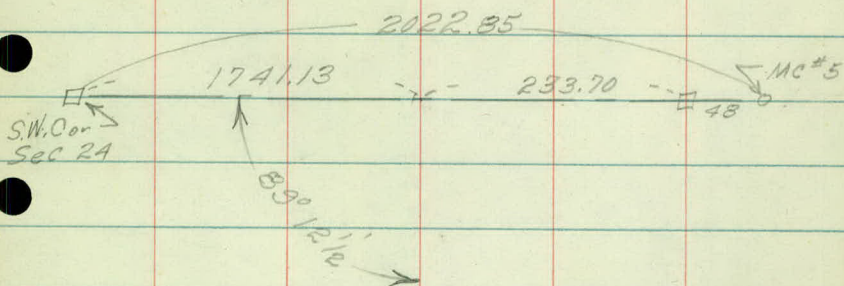
$L = 224.17$

$R = 359.27$

612+66.17 P.C.

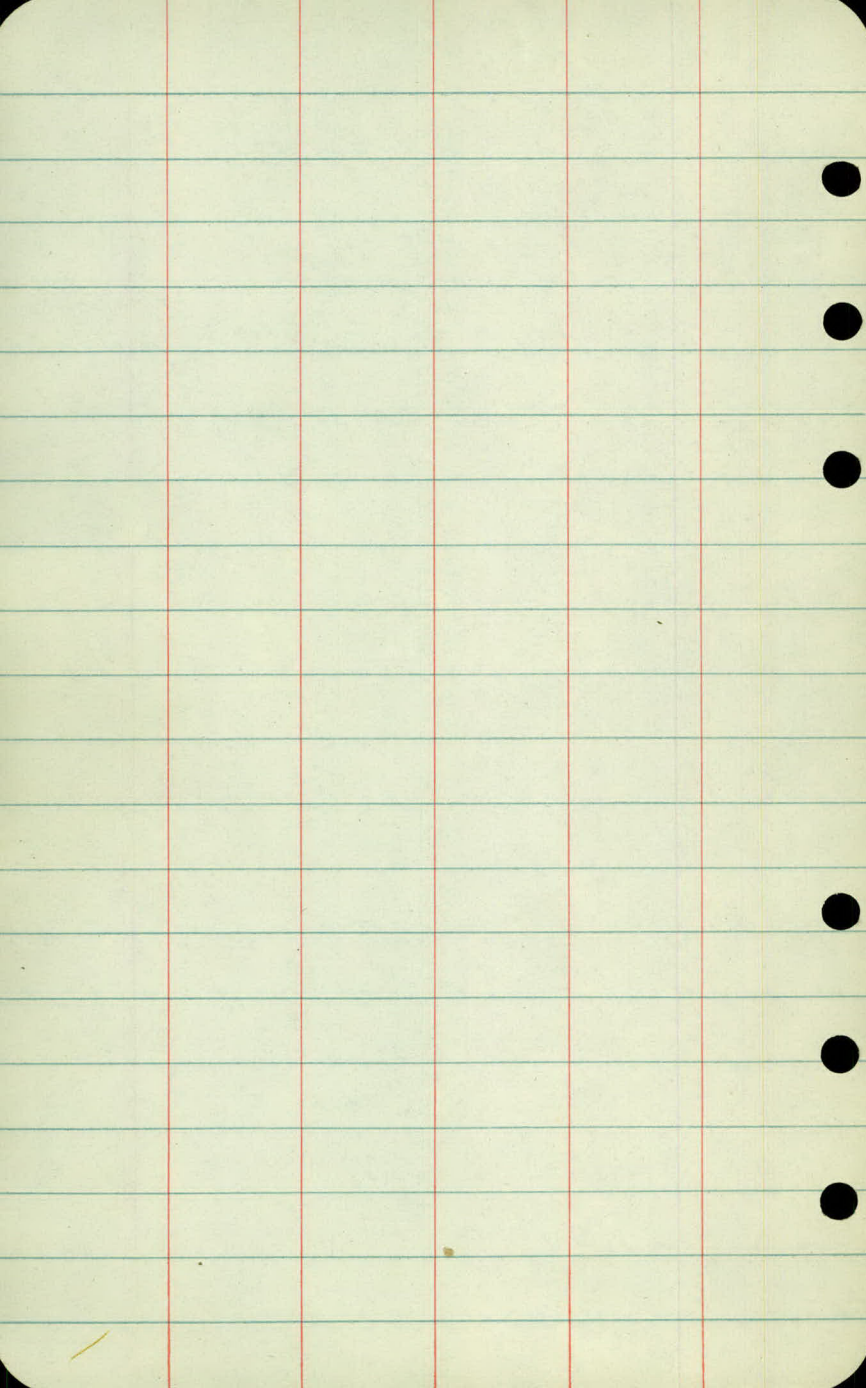
Sept. 23, 1959

3a



Boat Spike

Boat Spike



Sept 10, 1959

4

X-Section

Sta + X - Elev.

BM 1.15 929.89 • 928.74

W.S 11.38 934.45 • 6.82 923.07 •

606+50

BM 2.19 934.46 • 2.18 932.27 • 932.27

607

+50

FK
RL
RR
RG
JH

Sept. 10, 1959 5
Clear, Cold 47° RT

Top E. Cor Pump #1 outlet Headwall
White Bear Lake

30.42
930.43 30.6 29.9 27.7 27.2 25.7 25.7 24.8
403 3.9 4.6 6.8 7.3 8.8 8.8 9.7
12 21 26 31 57 72 89
Fe

33.0 23.4 24.6
11.5 11.1 9.9
126 115 99
Top Hyd Lt Sta 608+15

30.0 29.9 29.4 28.0 27.3 26.1 25.1 24.2
4.5 4.6 5.1 6.5 7.2 8.4 9.4 10.3
11 21 26 32 45 56 72
Fe

33.1 23.1
11.4 11.4
97 86

30.0 29.8 29.6 29.4 25.5 24.7 23.7
4.5 4.7 4.9 5.1 9.0 9.8 10.8
10 19 22 31 45 54
Fe

23.1
11.4
64

-Red 9-16-59

Sta + π - Elev

934.46 ✓

608

✓

+50

✓

609

+50

£

Sept 10, 1959

6

BT

29.9	29.7	29.4	28.4	27.3	25.0	24.1
4.6	4.8	5.1	6.1	7.2	9.5	10.4
	9	17	18	23	32	45
					Fe	

23.1
11.4
58

29.9	29.8	29.4	29.0	27.0	24.9	24.1
4.6	4.7	5.1	5.5	7.5	9.6	10.4
	10	16	20	22	32	43
					Fe	

23.1
11.4
55

30.0	29.8	29.3	27.3	25.0	24.1	23.1
4.5	4.7	5.2	7.2	9.5	10.4	11.4
	10	21	24	32	43	51
				Fe		

30.1	30.1	29.6	28.5	27.2	26.5	24.4	23.5
4.4	4.4	4.9	6.0	7.3	9.0	10.1	11.0
	10	20	24	26	32	44	47
					Fe		

23.1
11.4
51

-000

Sta + π - Elev

934.46 ✓

610

✓

+50

✓

611

+15 Fe Cor 34' Rt

✓ +18 R. Tie Fe Rt

2

Sept. 10, 1959

7

RT

30.2	30.0	29.8	29.3	27.4	25.7	24.6
4.3	4.5	4.7	5.2	7.1	8.8	9.9
	10	18	23	26	33	45
					Fe	

23.1	23.8
11.4	10.7
55	49

30.2	29.9	29.2	27.5	26.9	26.2	25.0
4.3	4.6	5.3	7.0	7.6	8.3	9.5
	12	24	28	34	41	48
				Fe		

23.1	23.7
11.4	10.8
58	52

	30.0					
30.2	30.5	29.6	28.3	27.6	25.3	24.2
4.3	4.5	4.9	6.2	6.9	9.2	10.3
	13	24	28	34	47	55
				Fe		

23.1
11.4
65

1020

Sta + π - Elev

934.46 ✓

611+50

+77.5 Begin Platted Area

612

✓

BM

11.40 923.06 (923.07)

L

Sept. 10, 1959

8

RT

23.1

30.4	30.2	29.7	27.5	25.9	24.5	24.1
4.1	4.3	4.8	7.0	8.6	10.0	11.4
12	23	30	40	52	64	

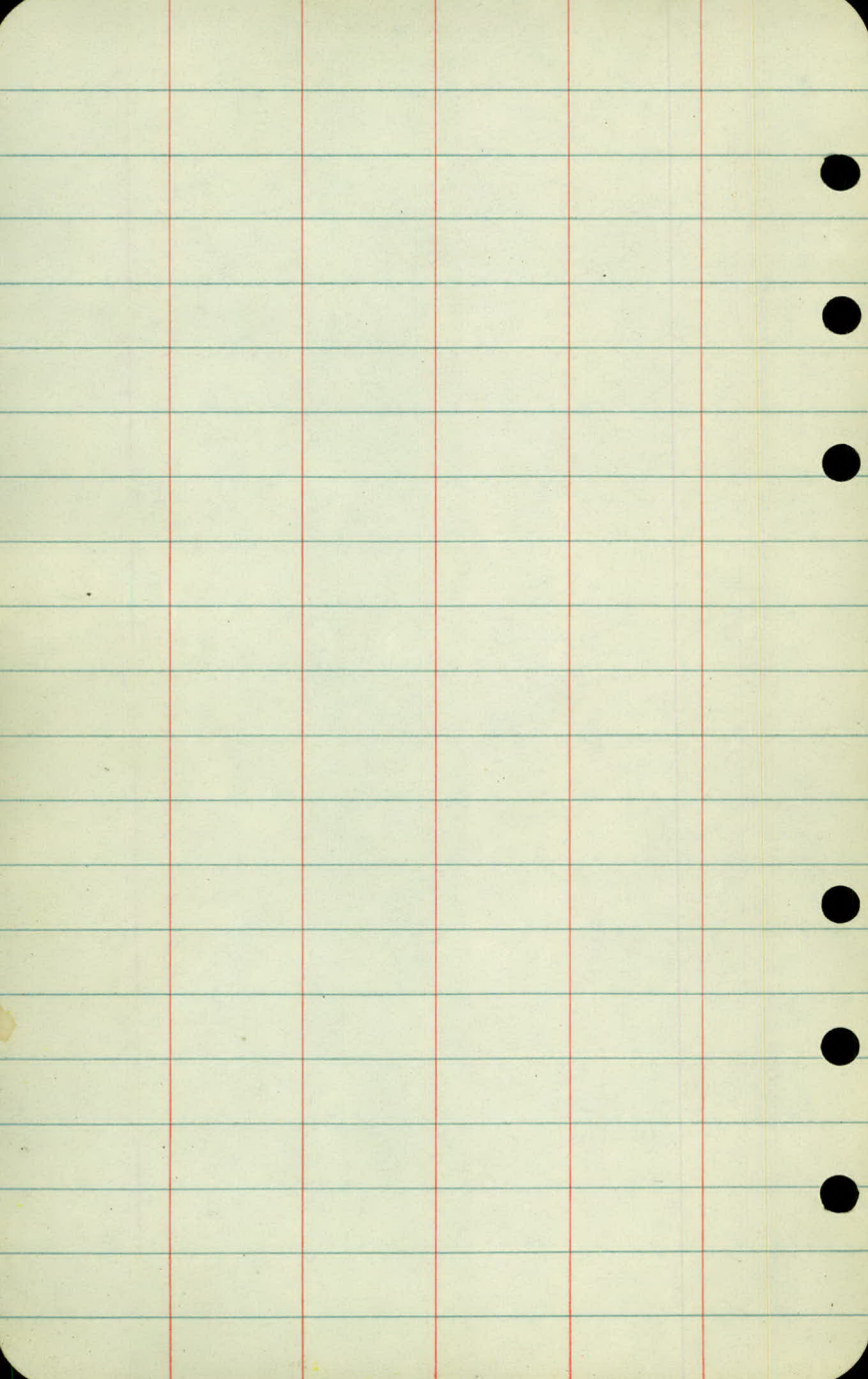
31.1	30.9	30.7	28.5	26.3	26.0	27.3
3.4	3.6	3.8	6.0	8.2	8.5	7.2
12	23	27	37	44	47	

23.0	24.7
11.5	9.8

67 53

W. S. White Bear Lake Sept 10, 1959

✓ 1048



Sept. 15, 1959

9

Soundings
Borings

Sta 607 33' Rt B-1 27.3

Feet Material

0-1.5 New fill 25.8

1.5-4.8 Sand

4.8 ^{what?} Possible original Ground Indication 22.5

1.5-5.3 sand

Sta 607+50 33' Rt B-2

0-0.8 clay

0.8-2.7 sand

2.7 ^{why} old Lake Shore

Sta 608 33' Rt B-3 25.0

Feet Material

0-2.6 Sand 22.4

Sta 608+50 33' Rt B-4

Feet Material

0-0.6 New Fill

0.6-20 Sand Lake Bed

Sept. 11, 1959 10

Sta 609

33' Rt

B-5

Feet

Material

0-0.6

New Fill

0.6-1.1

old Fill

1.1-2.3

Sand

Sta 609+50

33' Rt

B-6

Feet

Material

0-0.8

New Fill

0.8-2.8

Sand

3.0

old Lake Bed

Sta 610

33' Rt

B-7

Feet

0-3

Sand

Sta 610+50

33' Rt

B-8

Feet

0-1.2

New Fill

1.2-4.8

Sand

4.8

old Lake Bottom

Sta 611 33' Rt B. 9

Feet	Material
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0-1.8	New Fill
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1.8-5.8	Sand
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5.8	old Lake Bed
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