

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Road Map Survey

CO. RD. F

From Hodgson Rd. To McMenemy St.

Road Acc't. No. 274

Date Filed 4-7-27

File _____

Co. Rd. "F"
Alignment
0+00 - 61+02.25

3/28/27
C.W.S.
D.J.
A.B.
T.M.

ROAD MAP.

27

~~# 56~~

HODGSON ROAD
TO
MC. MENEMY ST.

Received 4-7-27
C. W. S. [Signature]

Office of Ramsey Co. Engineer	
ST. PAUL, MINN.	
Date Filed	4-7-27
File No.	16

Station Point Δ W. Δ R.

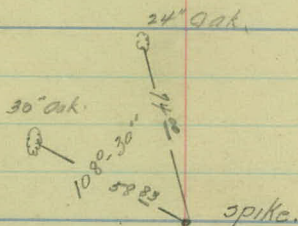
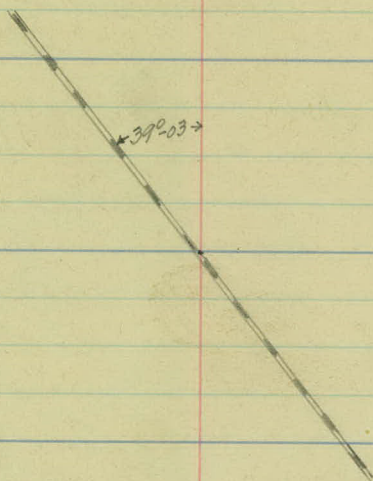
$30+44^{60}$ See line R.R.

$10+28^{90}$ PI

$00^{\circ}-08'$

$0+00,$

3/28/27



PI
2 Hodgson Rd.

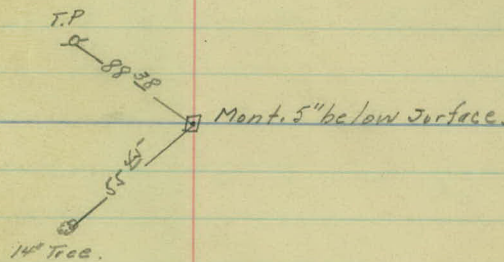
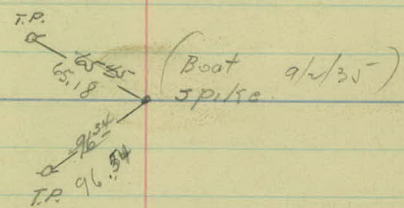
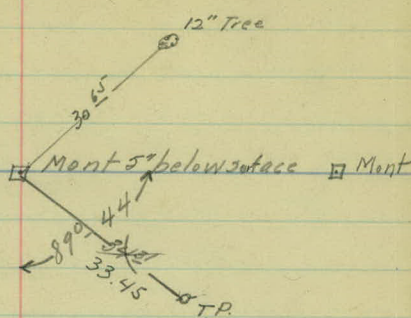
61+02⁷⁵

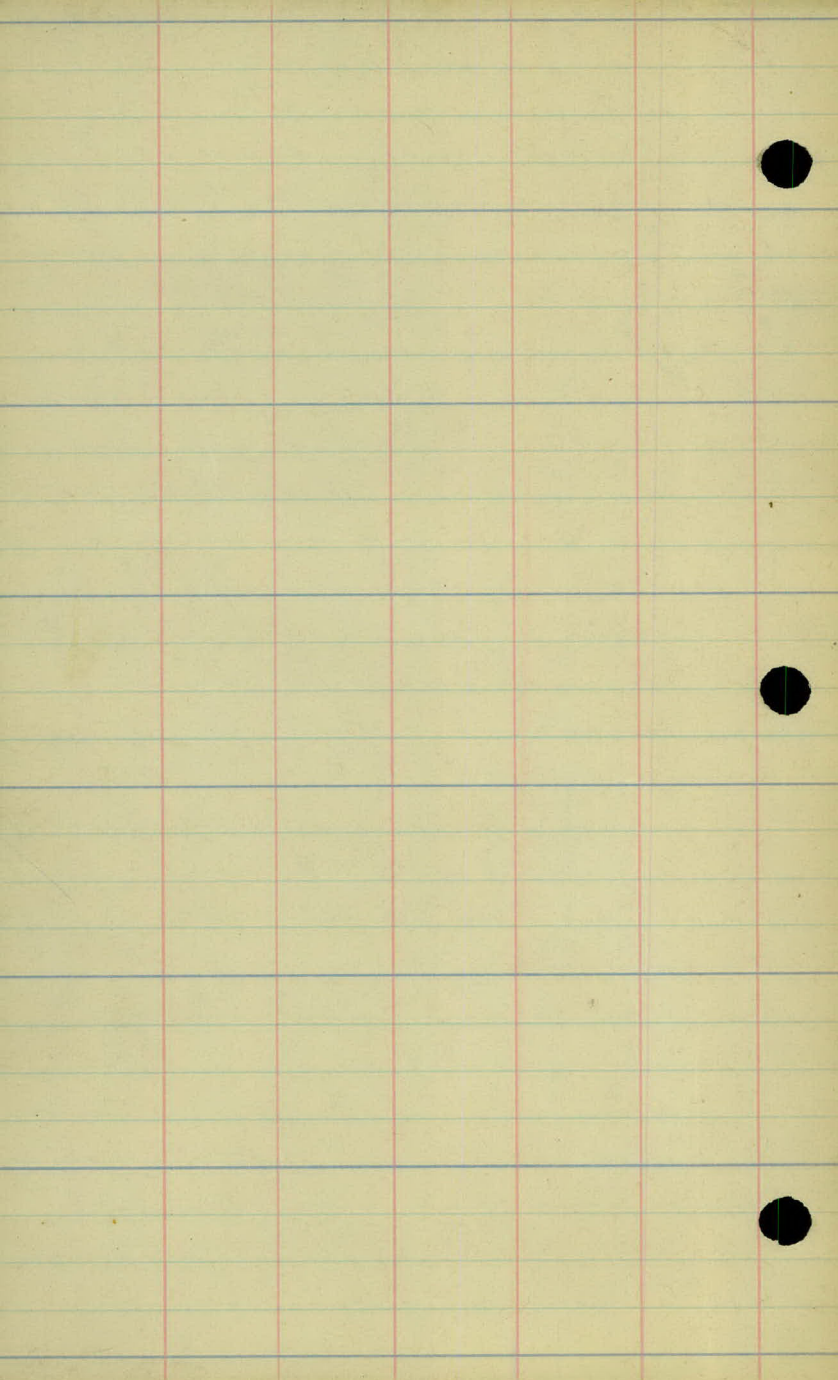
McMenemy Street

57+00 POT

34+67¹⁰ PI 00-01

3/28/27





3/28/27

C.W.S.

D.S.

A.B.

T.M.

Co. Rd. "F"

Topography
& Hodgson Rd.

To

Mc Menemy

Sta 0+00 - 61+02.25

4/27

Road Bed
ht. Pt.

2'

✓

5

+50 R Road ht.

2

1

12 11

+05 to FE Pt

0+00 to Hedgcock Road

3/28/27

+20-2 Tree 27

+99 TP 24

+84 E Tree 28

9 Trees.

Tree 28

+41 TP 23

15 Trees

Cultivated.

Cultivated.

13 T.

+56 Beg T 27

+69 End T 27

Tree 27

+89 TP 23

+78 T 31

17 T.

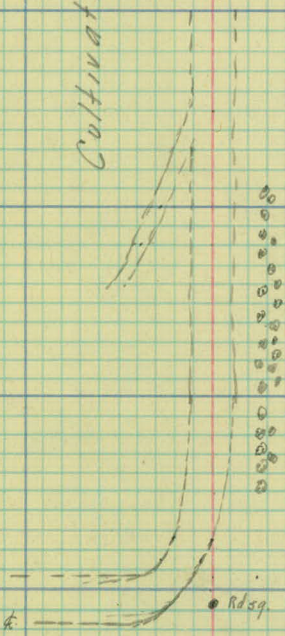
+66 TP 24

7 Trees.

+51 Beg Row T 29

-08 Rd 39 &

• Rd 39.



12

11

12 1

+55 X Drain 18" X 36' P2 194.17 R+

+289 $\frac{1}{2}$ Rice St.

10

9

12 12

8

7

6

12

12

3/28/27

+01 TP 25'

Cultivated

Cultivated

+77 TP 26'

+64 MB 13'
+59 MB 14'

Rice Street 24' Pav

+11 Rdog 32'

+62 TP 26'

12"

+05 TP 25'

Cultivated

Cultivated

+46 TP 24'

+50 X Rdog 13

19

18

17

16

10 8

15

14

13

5/28/27

+39 T 27
+29 T 28

Brush & Timber

Scattered Timber Brush

+94 T 21
+58 T 25
+16 T 23

+67 TP 18

+26 T 22

+31 TP 19

+69 T 23
+67 T 21
+55 T 29
+39 T 19
+59 EC 1/4 road
+25 T 29

+96 TP 21
+33 T 34
+20 T 33

Cultivated

Cultivated

+76 T 25
+07 T 25
+06 T 20

+64 TP 21
+26 X Rd 59 13

+32 TP 23

26

25

10 10

24

23

22

21

20

9 10

3/28/27

+77 T 22'
+57 RR 39 10'

+03 TP 15'

Cultivated

78 End cult.

+

7

+78 T 22'

+56 TP 16'

+27 End Timber

+12 TP 16'

+78 T 28'

Cultivated

Timber & Brush

+62 TP 16'

+33 T 25'

+18 TP 18'

+08 T 21'

33

32

31

+446 80 300 line Blank 32' 156+
17 R+

30

10' 7'

29

28

+23 8 Drive hti

27

3/28/27

+66 T30'

+52 39 10'

+98 RR 59 13'

+70 TP 12

+62 RR FCov 35'

+30 TP 14'

+29 TP 11

+00 BF 31'

+12 TP 12'

+96 TP 13'

+50 TP 15'

F 42'

F 42'

+65 FCov 43

+62 TP 30

+08 Beg F 32'

05 RR 59 13'

+98 EF 28'

+38 RR FCov 26

+96 T 19'

+75-3 T 15'

+17 29 11

+20 T 16

13 T 11'

Timber

Plank

RR ROW

Timber

Head Bed
L R.

+ 15' X Drain Conc 73'

36⁵ 36⁵ Rt

40

39

38

37

36

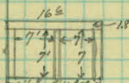
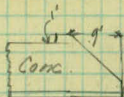
10' 10'

35

34

3/2 8127

+90 ET 25'
+55 T. 27'
+11 Beg Cult. 36'



Coenc. Cult.

GR 12

GR 12 F37

+92 TP 14'

+55 T 29'

ER 115

GR 12 F37

+76 Beg GR 13'

+59 GR 12'
+52 Beg GR 13'
+47 holo Sp 14'
+41 T 31'

+37 TP 14'

F38'

Cultivated

Timber

+60 T 31

F39

+99 TP 14'

F 41

Timber

+55 TP 13'

F 42'

31 RR 39 11'
+13 TP 13

Kaad Bed.
L R.

+ 88 \$ Drive Lt

47

14 15

46

4 16

45

4 17

44

5 16

43

7 15

42

+ 91 \$ Drive Lt.

15" X 30 CM

41

5/28/27

+22 T 13'
+22 E CUL

+86 F 37'
+83 X F 38

F 37'

+63 T 20
+36 T 20
+14 T 19'

POT. Hole.

+88 T 20'
+75 TP 13'

+31 T 32'
+23 T 35'

F 39

+28 TP 13'

+80 Beg F 39'

Cultivated.

+81 TP 13'

+55 End F 37'

+02 EGR 13
F 35'

+81 EGR 21
+77 GR 16'
+70 GR 11.5
+70 T 23'
+44 TP 14'
+38 SG 12'

+78 GR 12
+94 MB 12

GR 10'

GR 12' F 35'

Road Bed
L R

54

11' 8'

53

10' 10'

52

10' 12'

51

7' 12'

50

6' 13'

49

5' 13'

48

5' 14'

3/28/27

+79 TP 19'

F 135'

+26 TP 18'

Cultivated

Timber

F 132'

+79 Beg 501
+79 TP 16'

+50 T 23

+24 End F 16'

F 16'

F 135'

F 136'

+10 TP 14'

F 15'

F 137'

F 16'

Cultivated

Timber

F 136'

+68 TP 13
+50 T 21'
+29 T 20'

+07 T 19'

Beg F 13'

+01 MB 13

ROAD 500
L R.

+03⁷⁰ & Mc Menemy

61

+90 X Drain

23L. 31R.

60

12 8'

59

10' 8'

+71 & Drive Lt.

58

9 8'

57

10 7

56

11 7

55

10 7

5/28/27
C.W.B.
D.S.
A.B.
T.M.

McMenamy Street

+74 Rds 25'

+52 TP 21

+86 TP 30
+82 Co Rds 21

+38 M 15 10'

+16 TP 21
+16 END F 21'

F 21

F 20'

+62 Rds F 21
+62 TP 21

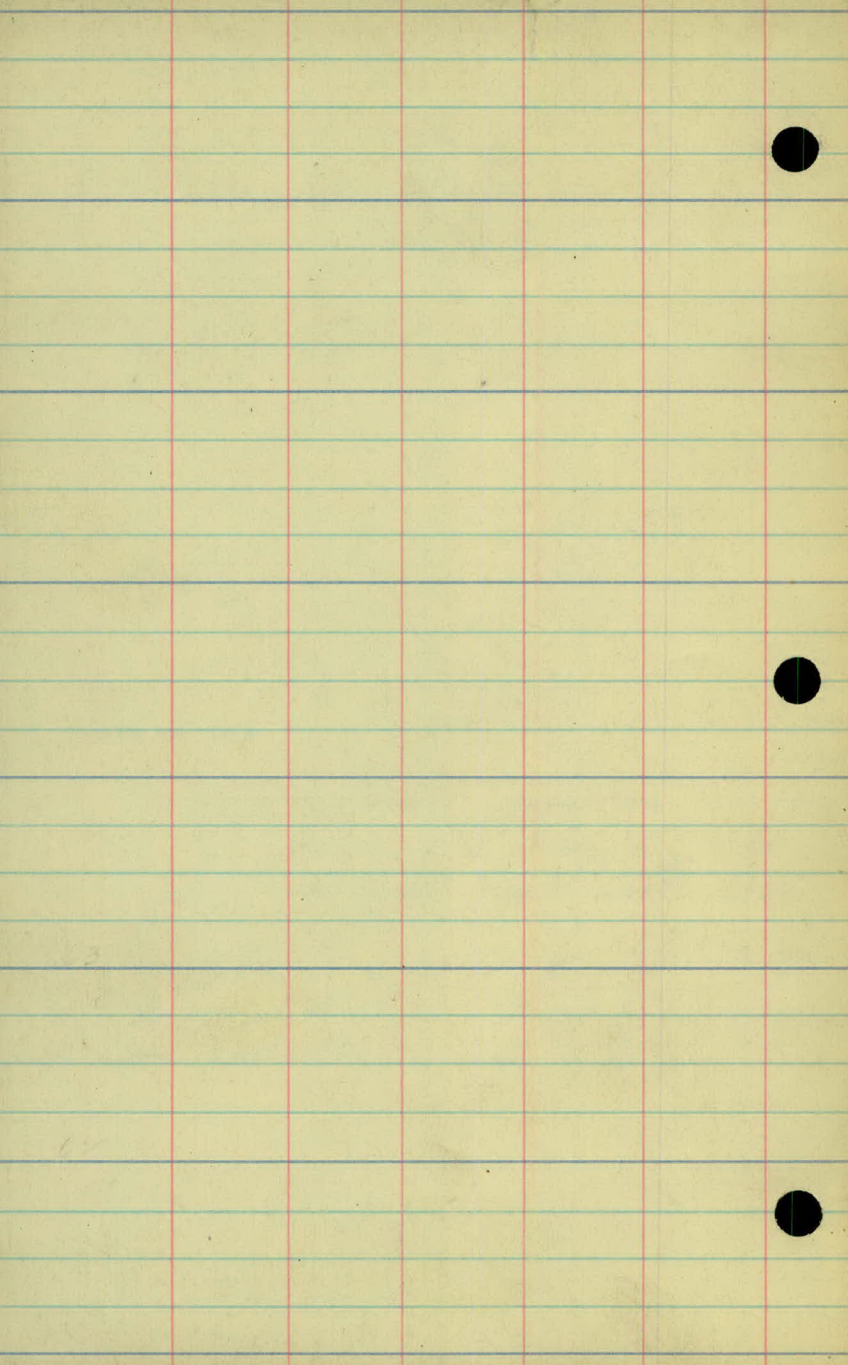
+66 TP 20'

Cultivated

Cultivated

+21 EFCor 39'

X X X



Gilfilan Road

Co. Road "F" to

X-Sections
for Borrow.

File with Co. Rd. "F"
Hodgson to McMeiterny

Bk 27 - Dr. 10

B.M.

12.00 943.50

931.50

39+83.38 = $\angle$ Co. Rd. F¹

Ditch Road

$$\begin{array}{r} 10.4 \\ 11.9 \\ \hline \end{array}$$

40+16

10.8

40+34

10.4

40+50

10.0

41+00 =

9.5

41+50 = R.O.T

12.7

42

$$\begin{array}{r} 12.9 \\ 13 \\ \hline \end{array}$$

+50

15.5

43+0

17.8

T.P.

243

11.90

42+75

43+0

L.

I

W. N. B.

Top mon.

10.0

June 22, 1936

1.5 ditch.

$$\begin{array}{r} 12.0 \\ \hline 10.4 \end{array} \quad 11.9$$

$$\begin{array}{r} 9.7 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 11.0 \\ \hline 14 \end{array}$$

$$\begin{array}{r} 10.8 \\ \hline \end{array}$$

$$\begin{array}{r} 12.0 \\ \hline 10.5 \end{array}$$

$$\begin{array}{r} 0.8 \\ \hline 32 \end{array} \quad 11.2$$

$$\begin{array}{r} 10.4 \\ \hline 21 \end{array}$$

$$\begin{array}{r} 10.4 \\ \hline \end{array}$$

$$\begin{array}{r} 12.1 \\ \hline 10.6 \end{array}$$

$$\begin{array}{r} 10.8 \\ \hline 33 \end{array}$$

$$\begin{array}{r} 0.7 \\ \hline 31 \end{array}$$

$$\begin{array}{r} 9.7 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 10.0 \\ \hline \end{array}$$

$$\begin{array}{r} 12.2 \\ \hline 10.7 \end{array}$$

$$\begin{array}{r} 11.0 \\ \hline 33 \end{array} \quad 11.2$$

$$\begin{array}{r} 1.0 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 5.4 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 8.6 \\ \hline 12 \end{array}$$

$$\begin{array}{r} 9.7 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 9.5 \\ \hline \end{array}$$

$$\begin{array}{r} 12.4 \\ \hline 10.9 \end{array}$$

$$\begin{array}{r} 2.2 \\ \hline 33 \end{array} \quad 11.2$$

$$\begin{array}{r} 1.6 \\ \hline 22 \end{array}$$

$$\begin{array}{r} 2.1 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 11.0 \\ \hline 7 \end{array}$$

$$\begin{array}{r} 10.7 \\ \hline \end{array}$$

$$\begin{array}{r} 14.4 \\ \hline 12.9 \end{array}$$

$$\begin{array}{r} 4.4 \\ \hline 33 \end{array} \quad 11.0$$

$$\begin{array}{r} 3.8 \\ \hline 21 \end{array}$$

$$\begin{array}{r} 4.7 \\ \hline 18 \end{array}$$

$$\begin{array}{r} 13.2 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 12.9 \\ \hline \end{array}$$

$$\begin{array}{r} 17.0 \\ \hline 11.7 \end{array}$$

$$\begin{array}{r} 11.0 \\ \hline 10.5 \end{array}$$

$$\begin{array}{r} 11.7 \\ \hline 33 \end{array} \quad 11.0$$

$$\begin{array}{r} 9.4 \\ \hline 26 \end{array}$$

$$\begin{array}{r} 13.7 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 13.7 \\ \hline 7 \end{array}$$

$$\begin{array}{r} 15.5 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 15.5 \\ \hline \end{array}$$

$$\begin{array}{r} 8.7 \\ \hline 7.2 \end{array}$$

$$\begin{array}{r} 6.7 \\ \hline 33 \end{array} \quad 11.0$$

$$\begin{array}{r} 6.7 \\ \hline 29 \end{array}$$

$$\begin{array}{r} 5.8 \\ \hline 20 \end{array}$$

$$\begin{array}{r} 6.1 \\ \hline 6 \end{array}$$

$$\begin{array}{r} 7.3 \\ \hline 4 \end{array}$$

$$\begin{array}{r} 7.2 \\ \hline \end{array}$$

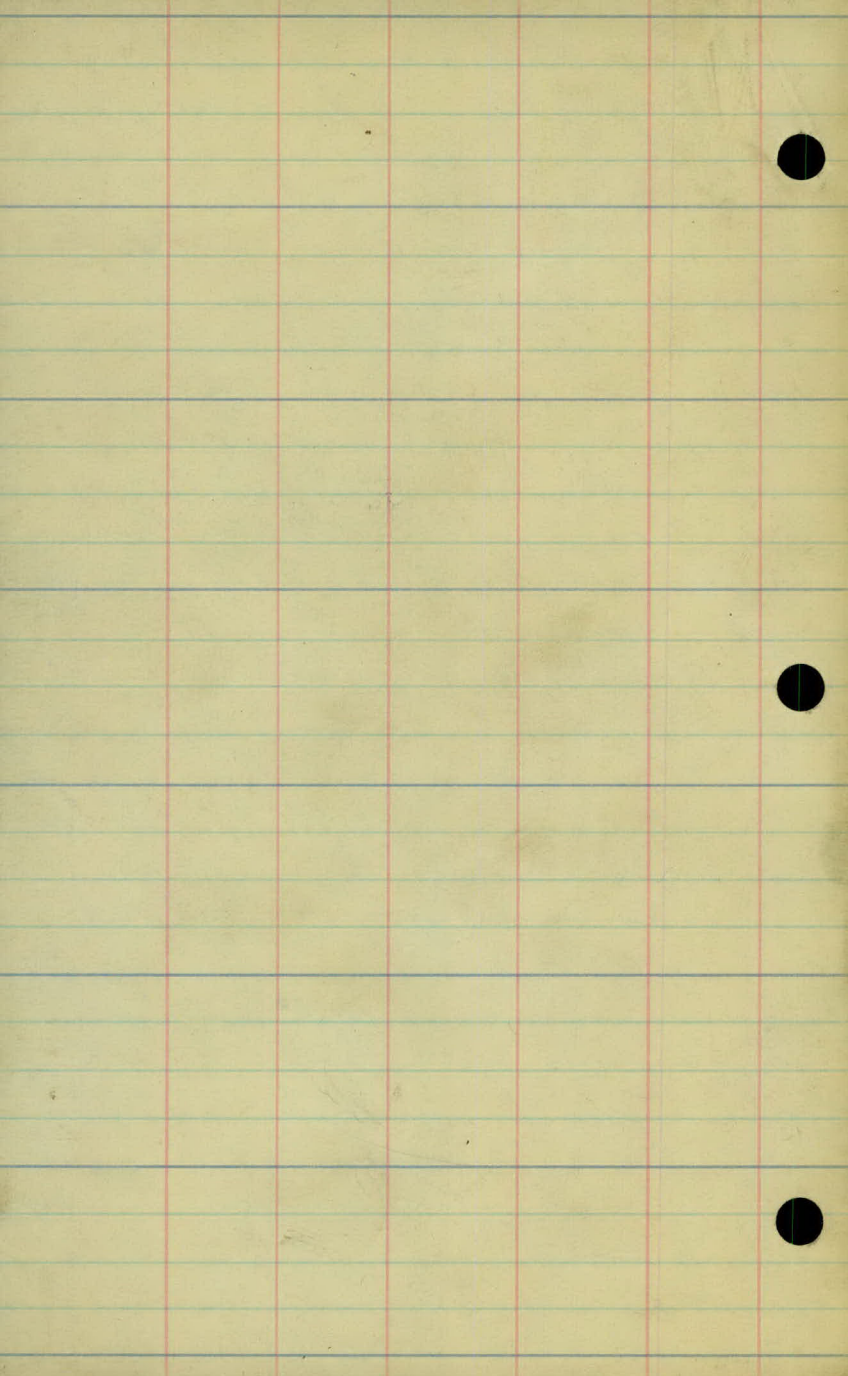
$$\begin{array}{r} 8.4 \\ \hline \end{array}$$

$$\begin{array}{r} 10.7 \\ \hline 33 \end{array} \quad 11.0$$

$$\begin{array}{r} 10.7 \\ \hline 13 \end{array}$$

$$\begin{array}{r} 8.6 \\ \hline 9 \end{array}$$

$$\begin{array}{r} 8.4 \\ \hline \end{array}$$



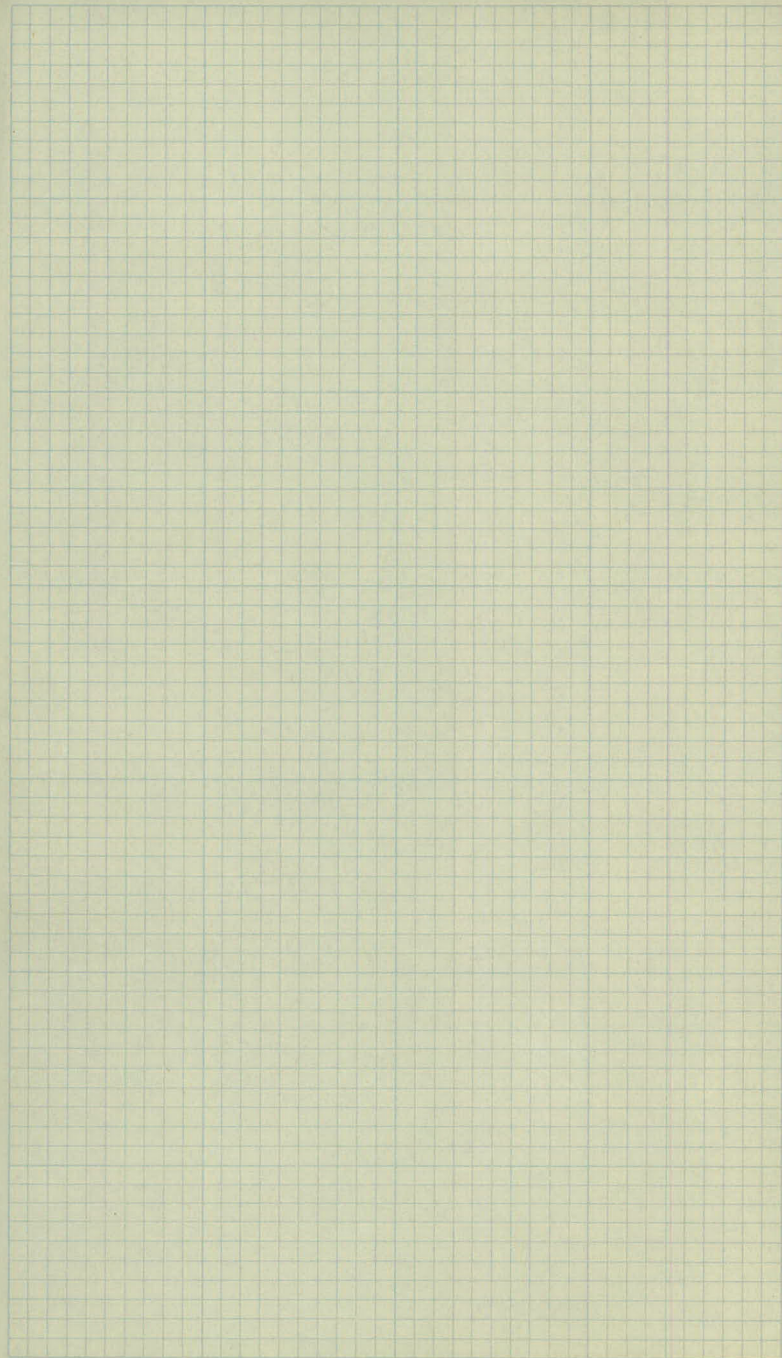
Plan Survey
CO. RD. "F"

Hodgson Rd. to McMenamy St.

INDEX

Align. 1-4
Topog. 5-15
X Sections 16-36

1945



1

Alignment

Sta	Point	ΔLt	ΔRt
-----	-------	-------------	-------------

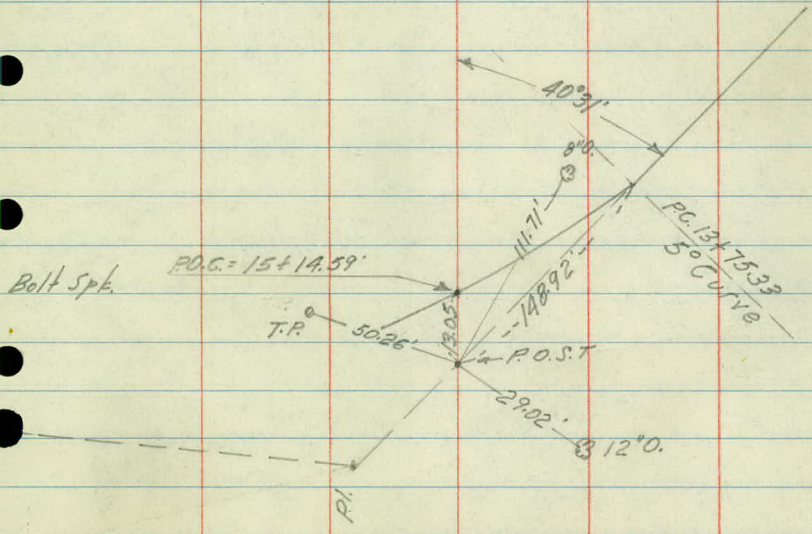
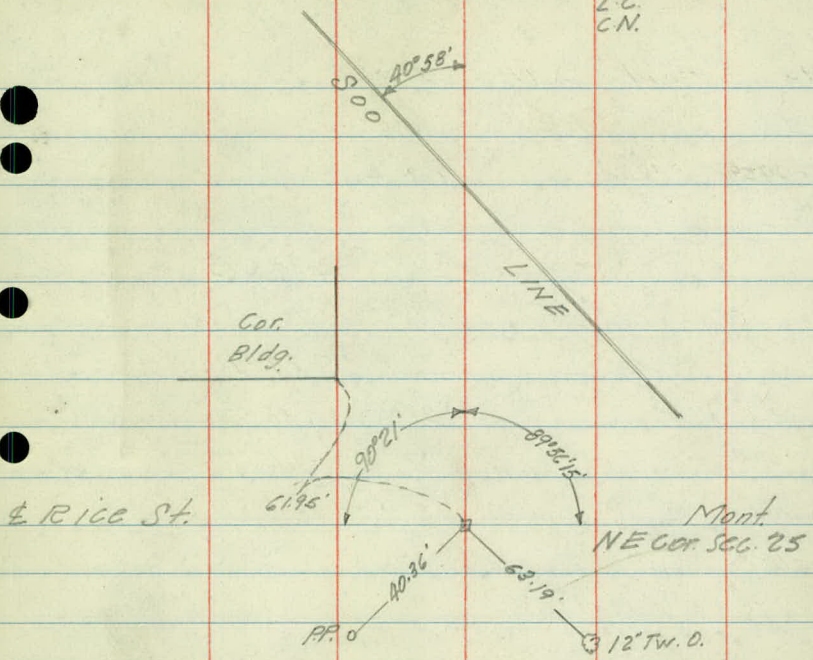
29+4.09	P.O.T.	=	E.R.R. Track.
---------	--------	---	---------------

9+24.84	P.I.		0° 07' 30"
---------	------	--	------------

0+00	=	E. Hodgson Rd.
------	---	----------------

4-21-94
K.A.
L.C.
C.N.

2



Sta	Point	ΔL	ΔR
60 + 00.18	= Mont. at McManamy St.		
+44.59	P.T.		6°45.25'
+25.1			5°58'
59		4°58'	$\Delta 13^{\circ}30\frac{1}{2}'$
+75		3°58'	D-8°-
58 + 60.63	P.I.		T-84.89'
+50		2°58'	L-168.85'
+25		1°58.2'	R-716.78'
58		0°58.2'	
57 + 75.74	P.C.	0°00'	

55 + 70.13 P.O.T.

33 + 63.25 P.I. 0°0'45"

McMenamy St.

Mont.

19 20

29 30

33.47'

139.55'

103°14'

57+78.24
1 68.83
59+47.07

T.P.

80.85'

2"x2" Hub

T.P.

73.36'

T.P.

92.22'

Mont.

T.P.

58.92'

Sta.	Point	ΔL	ΔR
------	-------	------------	------------

+40.77	P.T.	$6^{\circ} 62.75'$	
--------	------	--------------------	--

+25		$6^{\circ} 05.4'$	
-----	--	-------------------	--

			$\Delta - 13^{\circ} 45 \frac{1}{2}'$
--	--	--	---------------------------------------

61		$4^{\circ} 50'$	
----	--	-----------------	--

			$D - 10^{\circ} -$
--	--	--	--------------------

60 + 77.41	P.I.		
------------	------	--	--

			$T - 69.22'$
--	--	--	--------------

+75		$3^{\circ} 35'$	
-----	--	-----------------	--

			$L - 137.58'$
--	--	--	---------------

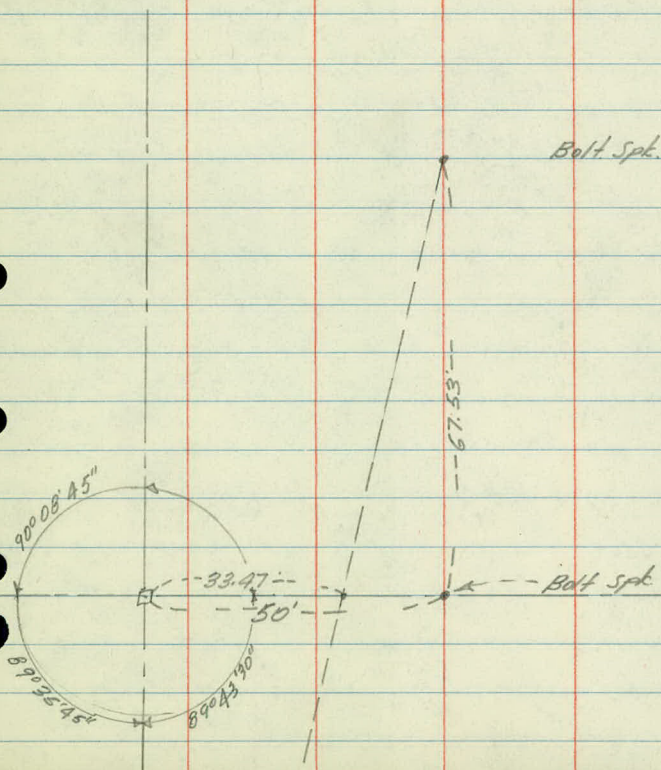
+50		$2^{\circ} 20'$	
-----	--	-----------------	--

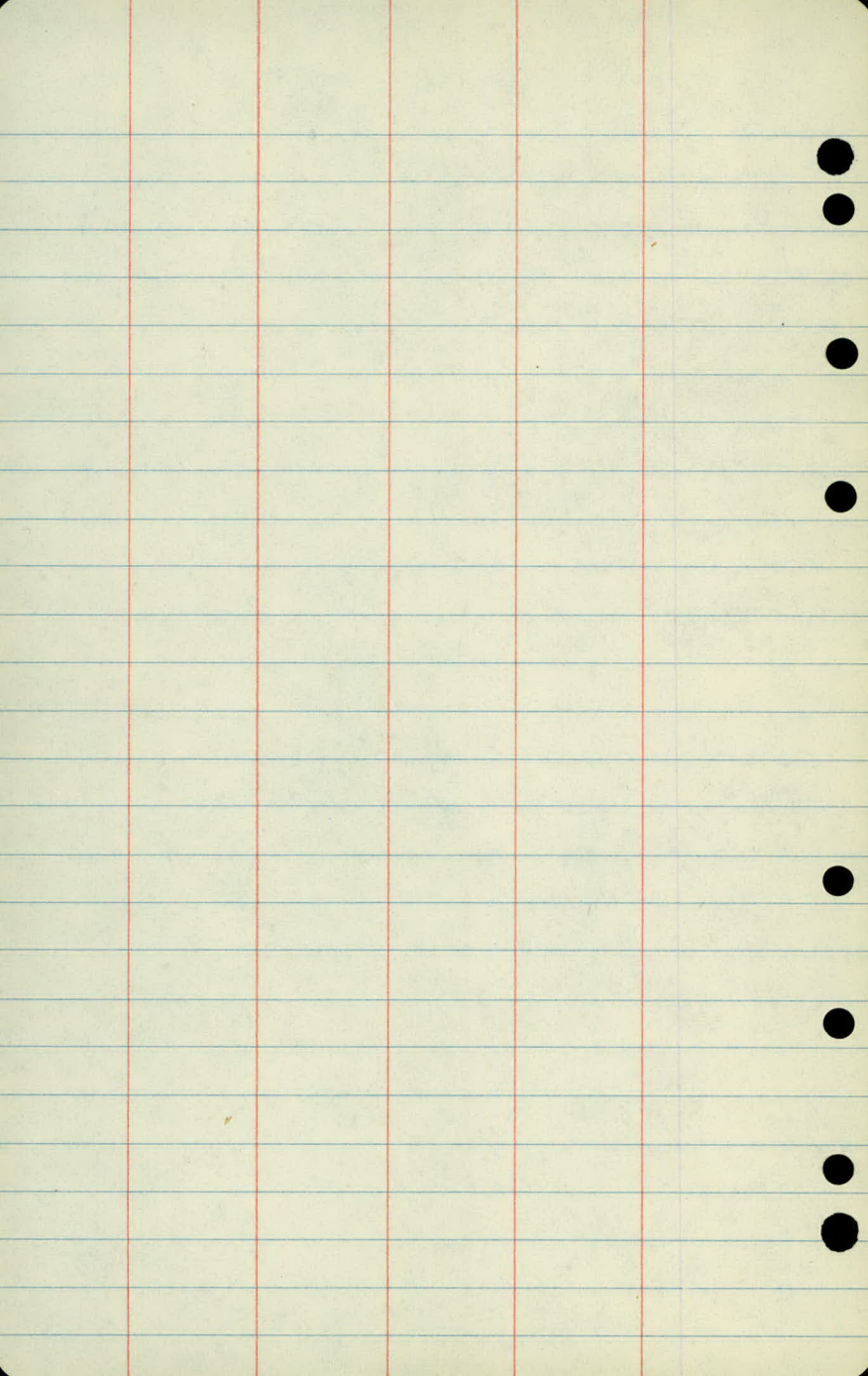
			$R - 573.69'$
--	--	--	---------------

+25		$1^{\circ} 05.4'$	
-----	--	-------------------	--

60 + 03.19	P.C.	$0^{\circ} 00'$	
------------	------	-----------------	--

60 + 03.02	P.O.T	$= \angle 17^{\circ}$ Menemay St.	
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Topography

+13-T.P

5

10' - 8'

4

+10-T.P

11' - 8' +12-12" O-30'

+76-12" O-27'
+58-12" O-27'
+45-12" Tw O-30'
+44-12" O-24'
+15-15" O-27'
+07-8" O-35'

3

11' - 9'

+92-8" Tw O-28'
+83-10" O-30'
+45-20" O-29'
+33-10" O-27'

+46-T.P-29'

+12-12" Tw O-30'
+01-10" O-31'

2

11' - 8'

+82-12" O-28' +95-8" Tw O-27'
+79-8" Tw O-27'
+77-6" O-30' +91-8" O-36'
+72-6" O-28'
+65-8" Tw O-29'
+57-10" Tw O-30'
+51-10" Tw O-27'

1

12' - 7'

+87-T.P-30'

+06-12" O-30'
+95-3-8" O-28'
+81-End 24" Conc Culv-37'

+50 15' 11' 60' of Culvert

+20-T.P-39'

+25- 17'

+43-End-28'
+37-End 24" Conc Culv-81'

0+00

35' - 19'

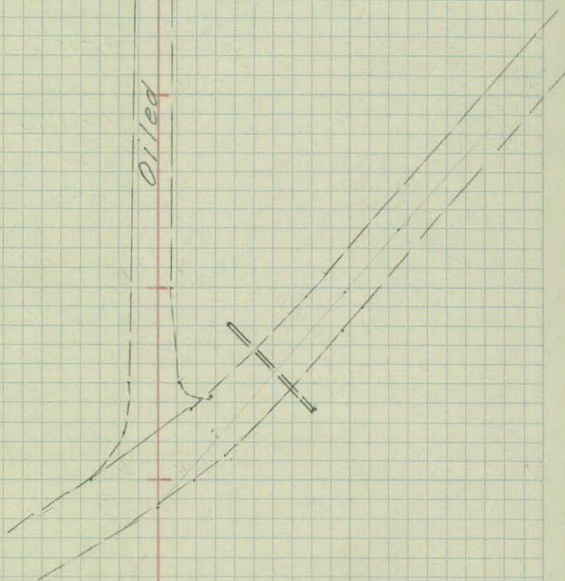
26" Wide Black Top on Hodgson's Rd.

Cult

Surface

Cult

Oiled



+28-T.P.-28

12

14' 12'

11

15' 11'

+97-T.P.-28'

+79-Ent-

+71-S.E. Cor Bldg.-42.5

+71-S.E. Cor Bldg.-42.5'

10

+127-Ent-
16' 11'

+75-T.P.-28'

+743-S.W. Cor Bldg.-39'

+75-Ent-17' 13'

+365-Pat-39' 30'

+365-Edge Pav

+127-Edge Pav

10' 10'

9

+96-T.P.-28

+90-12" TW. 0-53'

8

9' 9'

+36-T.P.-

7

10' 9'

6

10' 8'

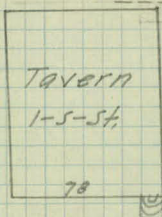
4-2A-44
K.P.
L.C.
C.N.

7

Surface

Cult

Dilled



24' Pav.

Rice

St.

Cult

Cult

Excl Trees + Brush - 40
+95-T.P.-28

+54-24" O.-36

+45-Fc-36'
+96-Reg Fc.-27'

19 Trees + Brush - 38'

12 12' Trees + Brush - 40

+92-24" O.-31

+42-T.P.-

18

12 12' Trees + Brush - 38'

+25-Brush-35'

17 Fc + Brush - 43

12' 12'

+86-T.P.-28'

+35-Reg Brush - 43'

16 Brush + Fc - 44

12' 13'

+60-8" O.-51'

~~+59-Ent-15"~~
+34-T.P.-

+59-Ent $\frac{15 \times 20' \text{ C.M.}}{23}$

+44-Range Tie.

15

12' 10'

+61-Range Tie
+56-Fc Cox - 37' R

+49-Ent $\frac{15 \times 20' \text{ C.M.}}{24}$

14

12' 12

+80-T.P.-

13

13' 12'

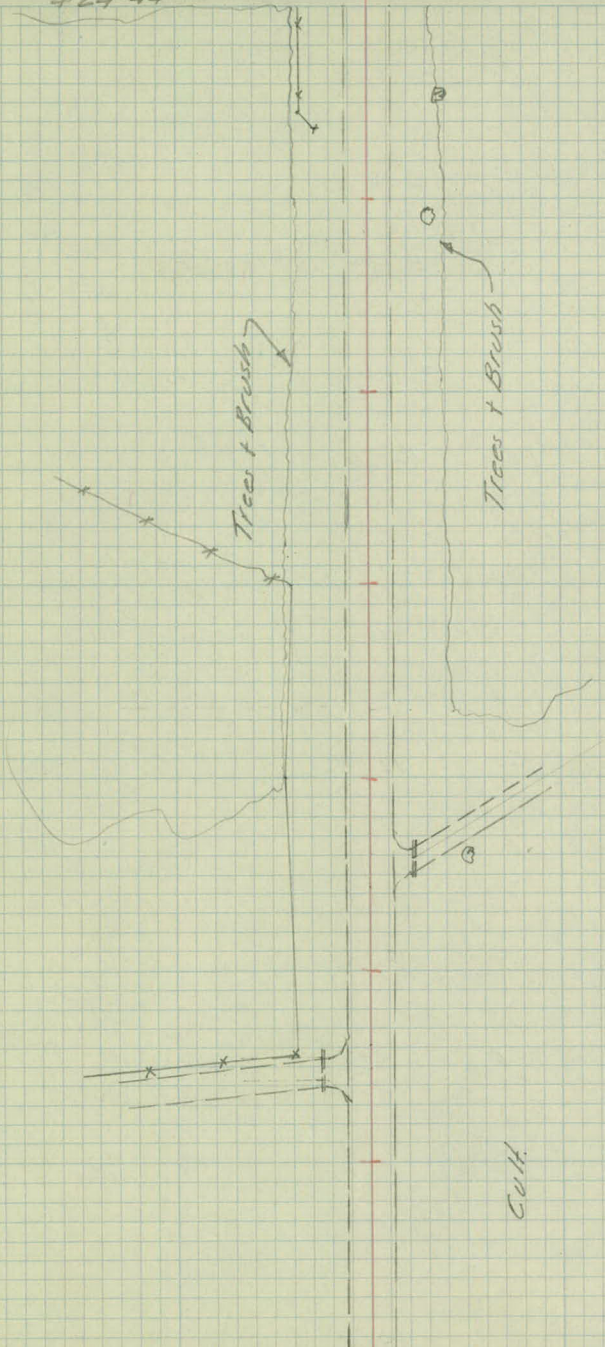
4-24-14

8

Trees + Brush

Trees + Brush

Cult.



26 +09-T.P.

13' 12'

25 Fe-34

13' 12'

Fe-33'

+52-T.P.

+46-Rod-13'

+29-Rod-33'

+06-Rod-33'

24

12'

+87-Rod-13'

23 Fe-35'
+99-T.P.-28'

13' 13'

Fe-33'

22

13' 12'

+47-T.P.

21 Fe-36'

13' 12'

Trees-46'

+40-Fe Cor-33'

20

13' 12'

4-25-14

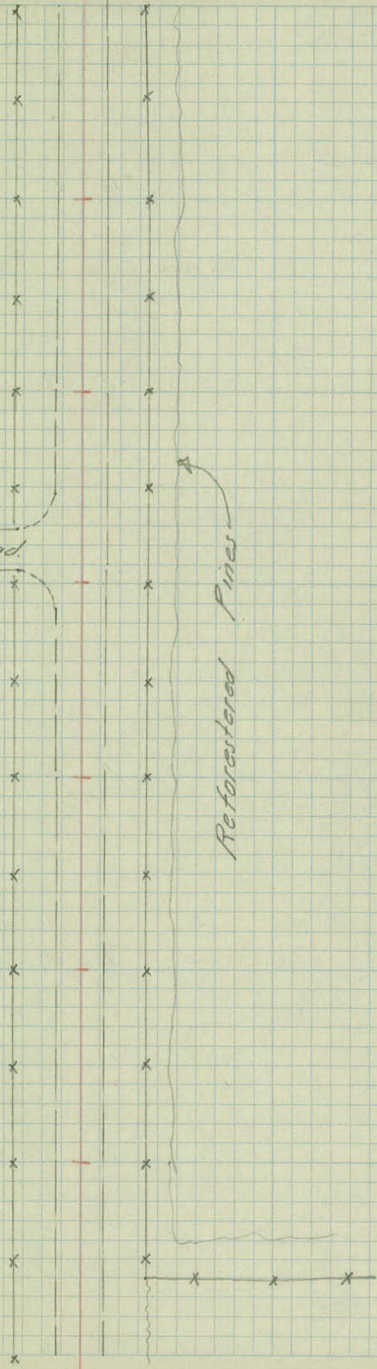
9

Pines

St. Paul Water Works Road.

Reforested

Reforested Pines



33 +11-TP-27

12' 12' FC-71'

+50-FC-81'
+50-Range Tie to Rd.

32

12' 13' FC-102'

+80-Rd-30'

+65-T.P.-

+70-Rd-70'
+37-Rd-46'
+20-Rd-13'

31

+87-FC-Cor-42'

+67-Range Tie FC.

+44-T.P.-28'

+24-T.P.-24'

30

11' 11'

+85-809-FC-43'

+61-T.P.-31'

+27-TP-27

29 End FC-33'

9' 10'

+20-FC-Cor-33'
+07-18°-94'

28

11' 12'

+77-Cor Pkgs 48

+68-TP-27

27

FC-33'

12' 12'

FC-33'

Gulf

Lowland

Lowland

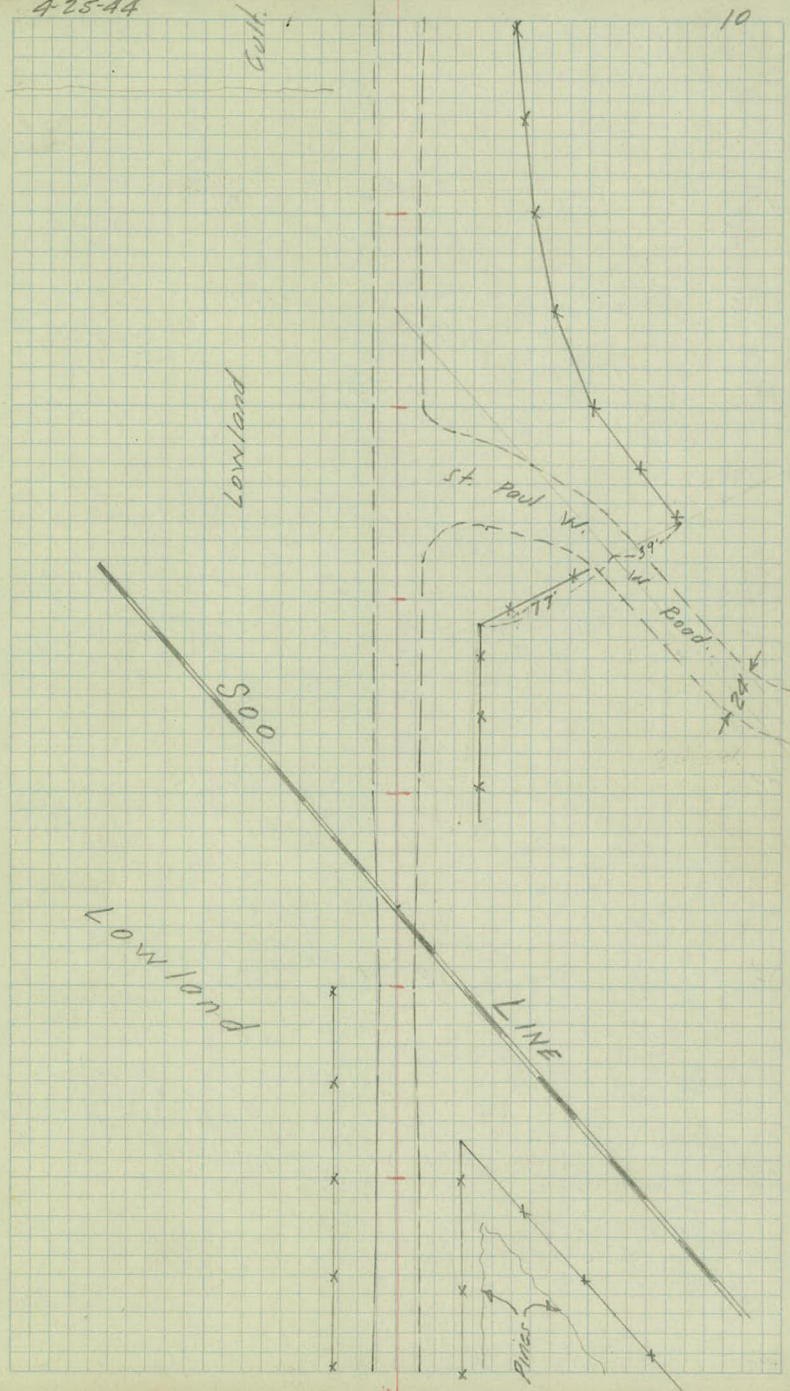
300

LINE

St. Paul W.

W. Road.

Pillar



12' 11' 104-End G.R.-133'

+92-Ent 15' R306M
28'

+78-End G.R.-22'

+67-Div G.R.-12' 18" Elm.-24'

+92-T.P.-28

40 G.R.-12'

+67-12" Ark-37'
11' 10' G.R.-23' Fc.-33'

+87-Cor. Willows-27

(See next page for
Canal Location and
Culvert Details)

+68-Cor. Willows-29

+81-10" Willow-29'

+41-Row 4" Pines-37'

+15-Ctr Double T'X7' Mono. Culv.
36.8'-End of Barrel-37.3'

39 +67-Beg. G.R.-12'

11' 10'

+88-Cor. Pines-38'

+13-T.P.-29'

+85-Cor. Trees-38'

+53-Beg. G.R.-13.3'

38

12' 12' Fc.-32'

+95-Cor. Pines-44'

+85-Cor. Pines-39'-73'

+85-Ent-

+35-T.P.-

37

12' 12' Fc.-32'

36

11' 11' Fc.-36'

+96-T.P.-29'

+76-Stop.-29'

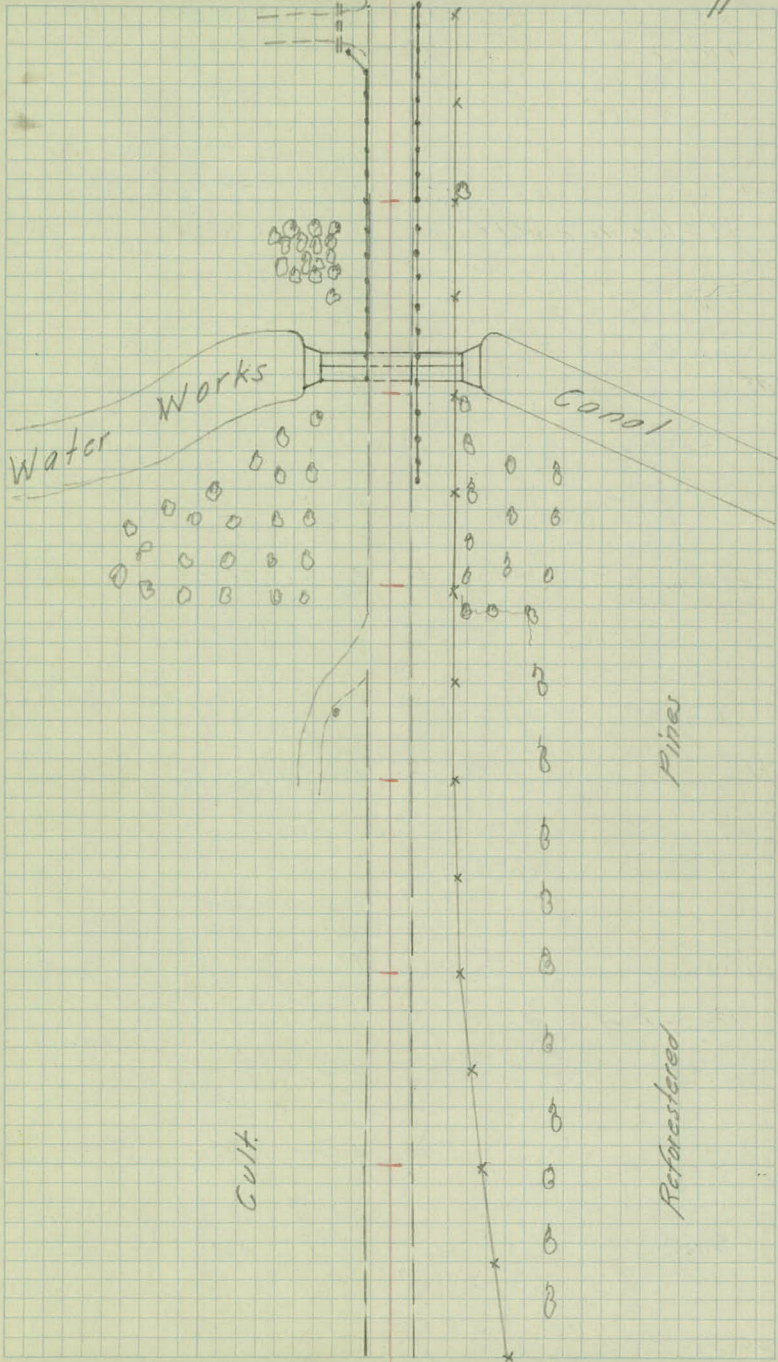
35

13' 12' Fc.-48'

+52-T.P.-

34

13' 13' Fc.-61'



+70-T.P.-

44 11' 15' Fe-32'

+83-± 18' Wide Gravel Road. ———→

+27-T.P.-

43 10' 15'

42 11' 15' Fe-32'

+77-T.P.-28'

41 11' 12'

At sta. 39+50
East = 0°00'

Top of Rubble Slope.

Dist.	Alt.
158'	259°
135'	240°
108'	238°
86'	232°
70'	221°
48'	250°
90'	257°
122'	256°
158'	252°
205'	247°
250'	245°

Top of Rubble Slope.

Dist.	Alt.
214'	108°
85'	96°45'
63'	96°
47'	102°
42'	120°
63'	142°
183'	124°-30'

W. W. Service Rd.



51

13' 15'

Fc.-35'

+73-PP.

+45-15"O.-23'

+35-24"O.-42'

+22-Range Tie 2

+29-16"O.-44'

+16-Row 5" B.E.-31'

50

12' 15'

Fc.-37'

+75-Pond-62'

+58-Pond-38'

+57-12" B.E.-38'

+20-Pond-28'

+07-TP-28' Pond-30

49

11' 15'

+08-10" Willow-37'

12" Pop-37' Water-37'

+95-6" Tw Willow-37' Fc.

+50-Pond-27'

48

11' 15'

Fc.-36'

+76-TP-28'

+67-Cor Pond-28'

+46-18" B.E.-22'

+25-18" B.E.-21'

+03-15" B.E.-20'

47

12' 14'

+87-Ent

+89-Fc-33'

+88-Range Tie

+82-Fc Cor-31' 2

+80-Fc Cor-38'

+64-Cor Trees-47

+16-TP-28

46

12' 15'

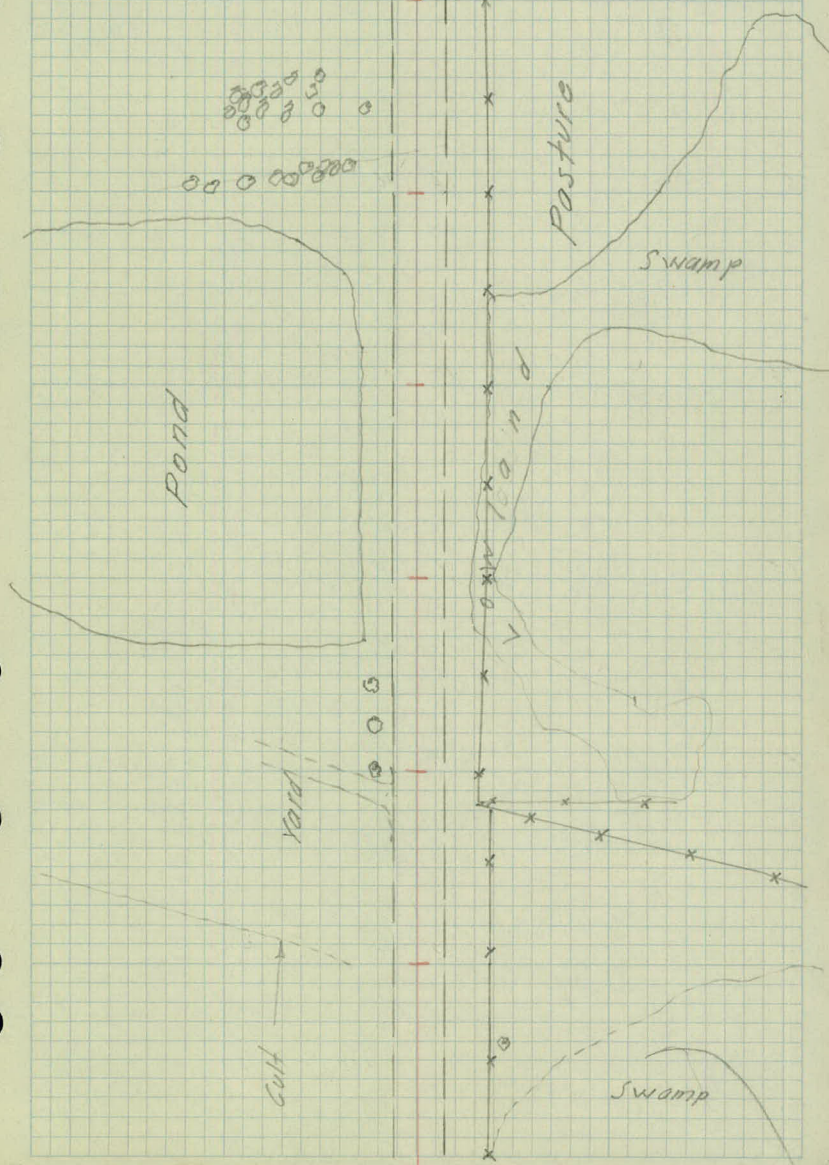
Fc.-37'

+59-Box Trees-45-18"O

+58-Six 34-38'

+55-Sfp-35'

45



122

18'-150'

58

12' 14'

+98-T.P.-29

12

57

12' 14'

+45-T.P.-28'

56

13' 10'

55 +104-T.P.-

13 10

+24-Fc Cor.-39'

54

14' 11'

Fc-39'

+13-T.P.

53

14' 10'

Fc-35'

+83-18°0'-48'

+40-15°0'-42'

+22-T.P.-26'

52

14 12'

Fc-33'

K.A.
L.G.
C.N.

14

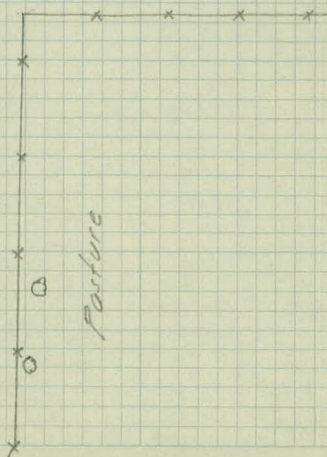
Hayfield

Surface

Cult.

Oiled

Pasture



Co Rd. "F" Twp Rd. Conn.

+40-16 14

61

16' 16'

+31-PP 35

+50-15' 22' +44'

+10 - 33'

52-+25

45

+35-Str. 3' Spill/Ways-35'

15' long

60

+93-PP-52'

19-+71

18-+50'

59

+11-Edge Rd. + Reg. Rd. Rd.

60

+85-50'

+77-28'

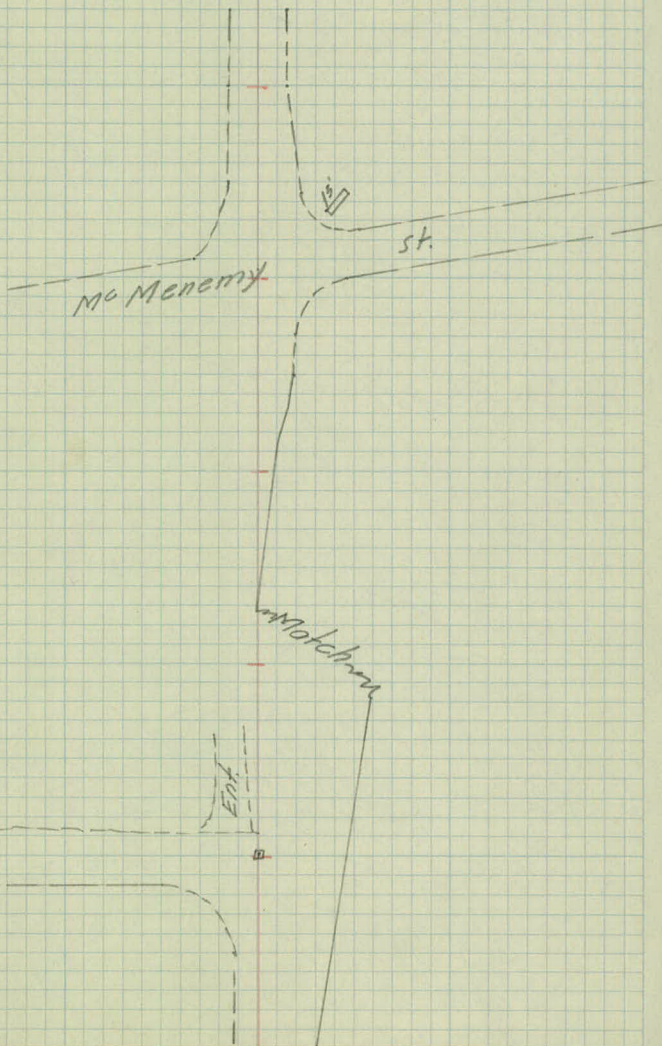
+40-TP-29'

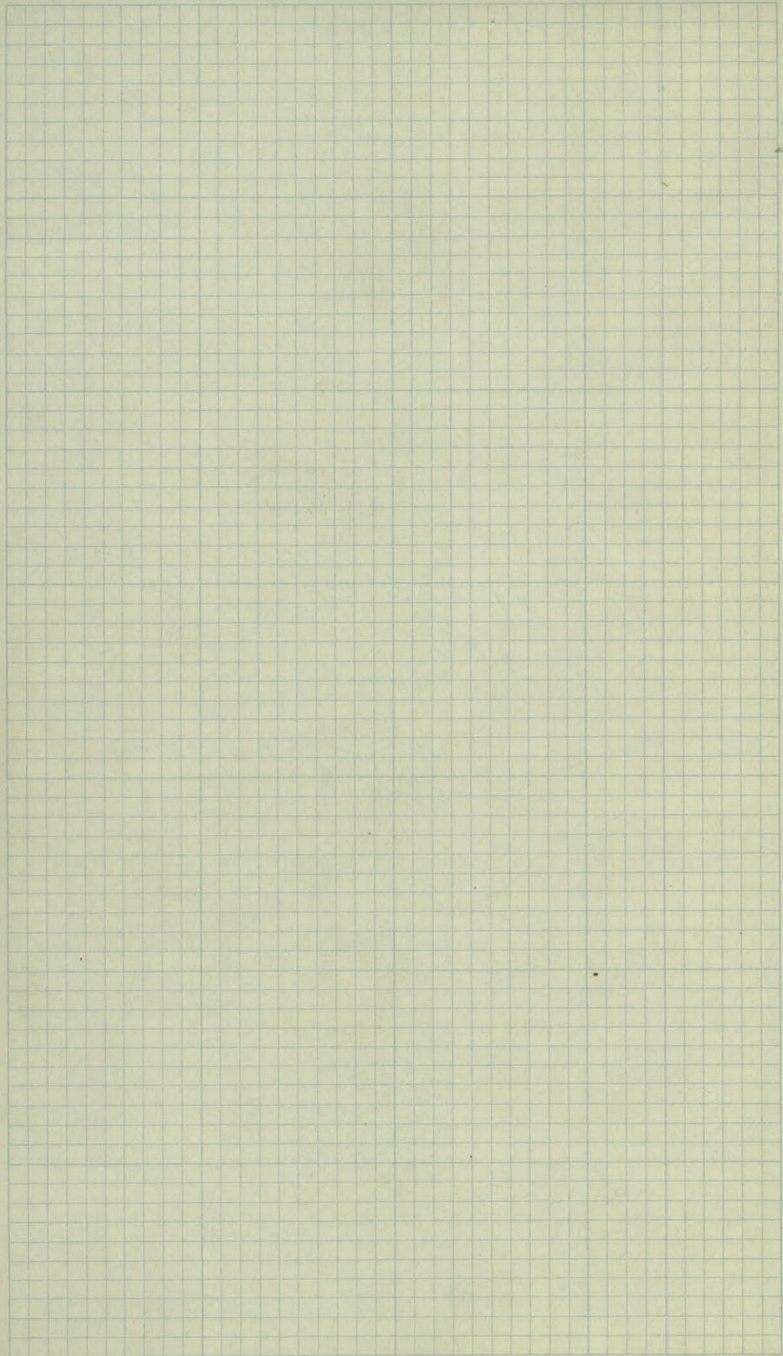
+50-13'

59

13' 30

4-25-44
K.A.
L.C.
C.N.





4/28/44

H.M.

C.F.

L.L.

X SECTIONS

Co. RD "F"

HODGSON RD To McMENNEMY

STA	+	Δ	—	ELEV
B.M	0.21	917.90 ✓		917.69
0-25				917.6
0-13				917.3
0+00	2	RTANGLES RD ^{HODGSON}		916.8
0+00	2	PROFILE HODGSON		916.8
+17				916.2
+35				915.2
+50				914.3
+62				913.7
1+00				912.9
+50				912.6
2+00				912.6
2+50				912.6

LT

E

RT

SPIKE IN 12" TWIN OAK STA. 0-30

26' RT

$$\frac{2.6}{50} \frac{2.3}{48} \frac{1.3}{29} \frac{0.5}{12} \frac{0.3}{17} \frac{3.7}{11} \frac{4.1}{14} \frac{3.7}{18} \frac{0.7}{25} \frac{0.0}{40} \frac{0.1}{50}$$

$$\frac{3.3}{50} \frac{2.3}{40} \frac{1.2}{15} \quad 0.6 \quad \frac{0.4}{13} \frac{3.5}{22} \frac{4.2}{26} \frac{3.7}{30} \frac{0.5}{50}$$

$$\frac{4.7}{50} \frac{4.5}{47} \frac{4.4}{43} \frac{3.3}{26} \frac{3.2}{21} \frac{1.8}{18} \frac{1.1}{17} \quad \frac{0.4}{17} \frac{0.6}{28} \frac{3.9}{43} \frac{4.2}{50}$$

$$\frac{1.5}{100} \quad \frac{1.3}{50}$$

1.1

$$\frac{1.0}{50} \quad \frac{0.8}{100}$$

HODGSON

$$\frac{3.2}{50} \frac{2.9}{39} \frac{4.8}{33} \frac{4.5}{27} \frac{3.8}{25} \frac{2.7}{15} \frac{1.7}{18} \quad \frac{1.0}{18} \frac{0.6}{35} \frac{0.5}{50}$$

HODGSON

$$\frac{4.0}{50} \frac{3.8}{33} \frac{4.8}{26-23} \frac{3.9}{19} \frac{3.2}{10} \frac{2.7}{18} \frac{1.6}{25} \frac{1.0}{50} \frac{3.6}{50}$$

HODGSON

$$\frac{4.7}{50} \frac{4.2}{28} \frac{5.3}{23-20} \frac{4.6}{18} \frac{4.3}{14} \frac{3.6}{14}$$

$$\frac{3.6}{12} \frac{2.3}{24} \frac{1.7}{32} \frac{0.9}{50}$$

$$\frac{4.8}{50} \frac{4.2}{28} \frac{5.4}{22-19} \frac{4.8}{16} \frac{4.5}{13} \frac{4.2}{7} \frac{4.2}{15} \frac{4.7}{19} \frac{4.9}{25} \frac{2.2}{36} \frac{1.5}{46} \frac{1.3}{50}$$

$$\frac{6.6}{50} \frac{6.2}{22} \frac{6.3}{21-19} \frac{5.9}{17} \frac{5.4}{11} \frac{5.0}{50} \frac{5.0}{9} \frac{5.3}{16} \frac{6.3}{22-24} \frac{5.8}{25} \frac{5.0}{39} \frac{5.5}{50}$$

$$\frac{8.2}{50} \frac{8.0}{28} \frac{6.1}{20} \frac{5.5}{11} \frac{5.3}{53} \frac{5.3}{7} \frac{5.5}{15} \frac{5.8}{21} \frac{7.5}{26} \frac{7.2}{50}$$

$$\frac{8.7}{50} \frac{8.6}{25} \frac{6.1}{18} \frac{5.6}{10} \frac{5.3}{53} \frac{5.4}{8} \frac{5.8}{16} \frac{8.3}{25} \frac{7.4}{50}$$

$$\frac{8.5}{50} \frac{8.7}{32} \frac{8.6}{23} \frac{5.9}{16} \frac{5.6}{11} \frac{5.3}{53} \frac{5.4}{7} \frac{5.8}{15} \frac{7.9}{21} \frac{8.0}{29} \frac{1.5}{34} \frac{7.3}{50}$$

STA	+	Δ	-	ELEV
		917.90 [✓]		

3+00				912.7
------	--	--	--	-------

+50				912.8
-----	--	--	--	-------

4				913.2
---	--	--	--	-------

+50				914.0
-----	--	--	--	-------

5				915.0
---	--	--	--	-------

+50				916.4
-----	--	--	--	-------

T.P	10.20	927.50	0.60	917.30 [✓]
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6				917.7
---	--	--	--	-------

+50				919.2
-----	--	--	--	-------

7				920.4
---	--	--	--	-------

+50				921.7
-----	--	--	--	-------

8				923.0
---	--	--	--	-------

+50				924.5
-----	--	--	--	-------

LT

Z

RT

$$\frac{8.7}{50} \quad \frac{8.0}{24} \quad \frac{5.7}{17} \quad \frac{5.4}{11} \quad \frac{5.2}{51} \quad \frac{5.3}{9} \quad \frac{5.7}{17} \quad \frac{7.2}{21} \quad \frac{7.3}{31} \quad \frac{7.5}{40} \quad \frac{6.7}{50}$$

$$\frac{7.2}{50} \quad \frac{7.5}{25} \quad \frac{6.7}{20} \quad \frac{5.5}{16} \quad \frac{5.3}{11} \quad \frac{5.1}{6} \quad \frac{5.8}{17} \quad \frac{6.7}{23} \quad \frac{7.0}{31} \quad \frac{6.4}{41} \quad \frac{6.4}{50}$$

$$\frac{6.2}{50} \quad \frac{5.8}{34} \quad \frac{6.4}{29-22} \quad \frac{5.4}{17} \quad \frac{5.0}{12} \quad \frac{4.7}{7} \quad \frac{4.9}{13} \quad \frac{7.6}{29} \quad \frac{7.6}{35} \quad \frac{7.2}{38} \quad \frac{7.8}{50}$$

$$\frac{4.9}{50} \quad \frac{4.9}{35} \quad \frac{6.0}{30} \quad \frac{5.8}{24} \quad \frac{4.5}{15} \quad \frac{4.3}{10} \quad \frac{3.9}{39} \quad \frac{4.2}{7} \quad \frac{6.9}{15} \quad \frac{8.4}{25} \quad \frac{8.4}{50}$$

$$\frac{3.1}{50} \quad \frac{3.4}{36} \quad \frac{4.9}{30} \quad \frac{4.5}{21} \quad \frac{3.6}{18} \quad \frac{3.1}{10} \quad \frac{2.9}{29} \quad \frac{3.1}{9} \quad \frac{3.5}{15} \quad \frac{4.9}{18} \quad \frac{6.9}{27} \quad \frac{8.6}{50} \quad \checkmark$$

$$\frac{6.3}{50} \quad \frac{1.4}{36} \quad \frac{3.7}{29} \quad \frac{3.5}{21} \quad \frac{2.1}{18} \quad \frac{1.8}{10} \quad \frac{1.5}{15} \quad \frac{1.6}{9} \quad \frac{2.0}{14} \quad \frac{4.0}{20} \quad \frac{5.7}{31} \quad \frac{7.5}{50} \quad \checkmark$$

$$\frac{8.8}{50} \quad \frac{8.9}{35} \quad \frac{10.7}{31} \quad \frac{11.9}{(35)} \quad \frac{11.5}{22} \quad \frac{10.3}{19} \quad \frac{10.0}{11} \quad \frac{9.8}{28} \quad \frac{9.9}{9} \quad \frac{10.3}{13} \quad \frac{12.4}{21} \quad \frac{13.0}{50} \quad \checkmark$$

$$\frac{7.6}{50} \quad \frac{7.7}{34} \quad \frac{10.3}{28} \quad \frac{10.2}{22} \quad \frac{9.2}{18} \quad \frac{8.8}{16} \quad \frac{8.5}{10} \quad \frac{8.6}{9} \quad \frac{9.6}{18} \quad \frac{10.6}{20-22} \quad \frac{9.9}{25} \quad \frac{10.3}{33} \quad \frac{12.8}{50} \quad \checkmark$$

$$\frac{6.2}{50} \quad \frac{5.9}{35} \quad \frac{8.2}{28} \quad \frac{9.0}{25} \quad \frac{7.6}{17} \quad \frac{7.3}{10} \quad \frac{7.1}{71} \quad \frac{7.4}{8} \quad \frac{7.9}{15} \quad \frac{9.1}{20} \quad \frac{7.2}{25} \quad \frac{7.8}{30-33} \quad \frac{9.1}{39} \quad \frac{9.9}{50} \quad \checkmark$$

$$\frac{4.6}{50} \quad \frac{4.6}{34} \quad \frac{6.5}{30} \quad \frac{7.5}{27} \quad \frac{7.8}{24} \quad \frac{7.1}{20} \quad \frac{6.2}{10} \quad \frac{5.8}{58} \quad \frac{6.1}{9} \quad \frac{6.4}{14} \quad \frac{7.2}{17} \quad \frac{7.9}{22-25} \quad \frac{5.6}{31-33} \quad \frac{6.5}{38} \quad \frac{7.3}{50} \quad \checkmark$$

$$\frac{3.1}{50} \quad \frac{3.3}{33} \quad \frac{5.9}{26} \quad \frac{3.9}{22} \quad \frac{5.3}{16} \quad \frac{4.8}{9} \quad \frac{4.5}{45} \quad \frac{4.8}{10} \quad \frac{5.2}{15} \quad \frac{6.3}{31} \quad \frac{6.0}{26} \quad \frac{3.7}{31} \quad \frac{4.0}{35} \quad \frac{4.9}{40} \quad \frac{5.3}{50} \quad \checkmark$$

$$\frac{2.0}{50} \quad \frac{1.7}{34} \quad \frac{3.6}{30} \quad \frac{4.6}{25} \quad \frac{4.6}{21} \quad \frac{3.9}{18} \quad \frac{3.3}{9} \quad \frac{3.0}{30} \quad \frac{3.4}{10} \quad \frac{3.6}{13} \quad \frac{4.5}{17} \quad \frac{5.0}{25} \quad \frac{2.0}{31-34} \quad \frac{3.3}{50} \quad \checkmark$$

STA	+	PK	-	ELEV
		927.50 [✓]		
8+95				926.0
9				926.2
+04				926.3
+09				926.3
+13	WEST-EDGE PAVEMENT			926.28
+24 ⁸⁴	¢ RICE ST PAVEMENT			926.40
+37	EAST EDGE PAVEMENT			926.39
+45				926.6
+50				926.6
B.M	3.75	930.14 [✓]	1.10	926.40 [✓] 926.39
+54				926.6
+59				926.5
10				926.3

LT

Q

RT

$$\frac{1.1}{30} \frac{1.0}{34} \frac{3.0}{29} \frac{3.0}{23} \frac{2.3}{20} \frac{2.0}{10} \frac{1.5}{15} \quad \frac{1.5}{11} \frac{1.8}{19} \frac{2.8}{22} \frac{3.3}{27} \frac{1.5}{32} \frac{1.8}{50} \checkmark$$

$$\frac{2.5}{50} \frac{2.6}{38} \frac{2.5}{29} \frac{1.9}{24} \frac{1.8}{19} \frac{1.8}{12} \frac{1.3}{21} \frac{3.0}{29} \frac{3.6}{43} \frac{3.7}{50} \checkmark$$

$$\frac{2.2}{50} \frac{1.9}{36} \frac{1.6}{22} \frac{1.5}{11} \frac{1.2}{12} \quad \frac{1.3}{13} \frac{1.8}{27} \frac{3.3}{42} \frac{3.6}{50} \checkmark$$

$$\frac{0.7}{50} \frac{1.1}{35} \frac{1.4}{21} \frac{1.2}{10} \frac{1.2}{12} \frac{1.6}{28} \frac{2.0}{50} \checkmark$$

$$\frac{0.73}{50} \frac{0.83}{42} \frac{0.96}{28} \frac{1.12}{13} \frac{1.22}{12} \quad \frac{1.33}{12} \frac{1.51}{31} \quad \frac{1.86}{50} \checkmark$$

$$\frac{0.14}{100} \quad \frac{0.59}{50} \frac{0.84}{25} \quad \frac{1.38}{25} \quad \frac{1.75}{50} \frac{2.51}{100} \checkmark$$

$$\frac{0.63}{50} \frac{0.89}{25} \frac{1.11}{11} \quad \frac{1.41}{25} \quad \frac{1.80}{50} \checkmark$$

$$\frac{0.5}{50} \quad \frac{0.9}{36} \frac{0.8}{21} \quad \frac{0.9}{15} \frac{1.4}{22} \frac{2.2}{38} \frac{2.0}{43} \frac{1.9}{50} \checkmark$$

$$\frac{0.4}{50} \frac{0.4}{42} \frac{1.0}{31} \frac{0.9}{23} \frac{0.8}{12} \frac{0.9}{09} \quad \frac{1.0}{11} \frac{1.6}{23} \frac{2.6}{31} \frac{3.4}{43} \frac{3.5}{50} \checkmark$$

HIGH POINT MONT RICE + CO. RD "F"

$$\frac{3.0}{50} \frac{3.2}{38} \frac{3.7}{16} \frac{3.5}{12} \frac{3.5}{11} \frac{4.3}{20} \frac{5.0}{26} \frac{5.9}{31} \frac{5.8}{36} \frac{5.9}{50} \checkmark$$

$$\frac{3.4}{50} \frac{3.7}{26} \frac{3.6}{16} \quad \frac{3.6}{8} \frac{3.8}{19} \frac{4.5}{25} \frac{5.8}{29} \frac{5.0}{34} \frac{4.4}{50} \checkmark$$
FLOOR
TAVERN
$$\frac{0.4}{40} \frac{3.3}{40} \frac{3.1}{32} \frac{4.1}{22} \frac{4.0}{15} \frac{3.8}{9} \frac{4.2}{16} \frac{4.8}{21} \frac{5.6}{36} \frac{5.8}{39} \frac{5.4}{42} \frac{4.0}{50} \frac{3.9}{50} \checkmark$$

STA	+	π	ELEV
		930.14	
10+50			926.2
11			926.2
+50			926.4
12			926.3
+50			926.1
13			925.6
+50			924.8
14			923.7
+50			922.4
15			921.1
+50			919.5
16			917.6

LT

A

RT

FAVOR
TRIVERN

<u>0.4</u>	<u>3.4</u>	<u>4.3</u>	<u>4.3</u>	<u>4.1</u>		<u>4.3</u>	<u>4.8</u>	<u>5.5</u>	<u>5.7</u>	<u>5.6</u>	<u>4.1</u>	<u>4.1</u>	✓
42	42	25	18	14	3.9	10	16	19	24	28	32	50	

<u>2.8</u>	<u>3.2</u>	<u>4.5</u>	<u>4.5</u>	<u>4.3</u>	<u>4.2</u>		<u>4.4</u>	<u>4.7</u>	<u>5.6</u>	<u>5.9</u>	<u>5.7</u>	<u>4.0</u>	<u>4.2</u>	<u>4.5</u>	✓
50	33	28	23	18	13	3.9	11	16	20	24	28	32	41	50	

<u>2.7</u>	<u>3.1</u>	<u>4.8</u>	<u>5.0</u>	<u>4.9</u>	<u>4.3</u>	<u>4.1</u>		<u>4.0</u>	<u>4.3</u>	<u>5.5</u>	<u>5.8</u>	<u>5.6</u>	<u>3.3</u>	<u>3.8</u>	✓
50	33	29	25	21	17	13	3.7	11	16	20	24	27	32	50	

<u>2.5</u>	<u>2.8</u>	<u>5.3</u>	<u>5.5</u>	<u>5.0</u>	<u>4.4</u>	<u>4.0</u>		<u>4.0</u>	<u>4.3</u>	<u>5.9</u>	<u>5.9</u>	<u>5.5</u>	<u>2.7</u>	<u>2.8</u>	✓
50	33	27	24	19	16	13	3.8	11	16	21	24	27	32	50	

<u>2.2</u>	<u>2.2</u>	<u>4.8</u>	<u>5.7</u>	<u>5.4</u>	<u>4.7</u>	<u>4.2</u>		<u>4.2</u>	<u>4.5</u>	<u>5.5</u>	<u>5.7</u>	<u>5.2</u>	<u>2.2</u>	<u>2.6</u>	✓
50	33	28	24	20	16	12	4.0	11	16	19	23	26	32	50	

<u>2.3</u>	<u>2.4</u>	<u>4.8</u>	<u>6.2</u>	<u>6.0</u>	<u>5.1</u>	<u>4.7</u>		<u>4.7</u>	<u>5.2</u>	<u>5.8</u>	<u>6.1</u>	<u>5.4</u>	<u>2.4</u>	<u>2.7</u>	✓
50	34	30	24	19	16	13	4.5	11	15	19	24	26	31	50	

<u>3.3</u>	<u>3.5</u>	<u>5.7</u>	<u>6.5</u>	<u>7.1</u>	<u>6.9</u>	<u>5.9</u>	<u>5.5</u>		<u>5.6</u>	<u>5.9</u>	<u>6.8</u>	<u>7.1</u>	<u>7.1</u>	<u>3.8</u>	<u>3.8</u>	✓
50	33	29	26	22	19	15	12	5.3	11	15	20	23	26	32	50	

<u>5.1</u>	<u>5.1</u>	<u>7.5</u>	<u>7.9</u>	<u>7.6</u>	<u>7.0</u>	<u>6.6</u>		<u>6.6</u>	<u>6.9</u>	<u>7.8</u>	<u>8.1</u>	<u>7.8</u>	<u>5.3</u>	<u>5.2</u>	✓
50	33	27	23	20	16	12	6.4	11	16	20	25	28	32	50	

<u>5.9</u>	<u>5.8</u>	<u>8.4</u>	<u>10.7</u>	<u>10.5</u>	<u>8.7</u>	<u>7.9</u>		<u>7.9</u>	<u>8.1</u>	<u>9.3</u>	<u>9.5</u>	<u>9.4</u>	<u>6.8</u>	<u>6.7</u>	✓
50	34	31	27	21	17	10	7.7	12	17	20	24	27	32	50	

<u>5.7</u>	<u>5.8</u>	<u>8.0</u>	<u>11.7</u>	<u>11.9</u>	<u>9.6</u>	<u>9.2</u>		<u>9.3</u>	<u>9.6</u>	<u>10.4</u>	<u>10.5</u>	<u>10.1</u>	<u>7.8</u>	<u>7.5</u>	✓
50	36	34	27	22	15	11	9.0	12	16	19	25	28	32	50	

<u>7.4</u>	<u>7.5</u>	<u>9.8</u>	<u>12.5</u>	<u>13.8</u>	<u>11.4</u>	<u>11.0</u>		<u>10.8</u>	<u>11.0</u>	<u>11.4</u>	<u>11.6</u>	<u>11.2</u>	<u>8.2</u>	<u>7.3</u>	✓
50	33	32	28	24	21	16	11	10.6	11	16	18	23	27	33	50

<u>9.0</u>	<u>9.3</u>	<u>10.8</u>	<u>14.0</u>	<u>15.5</u>	<u>14.2</u>	<u>13.2</u>	<u>12.8</u>		<u>12.7</u>	<u>12.8</u>	<u>13.9</u>	<u>14.7</u>	<u>13.0</u>	<u>10.1</u>	<u>9.2</u>	✓
50	33	32	26	23	21	19	16	11	12.5	12	16	18	23	27	31	50

STA	+	π	-	ELEV
		930.14 [✓]		

16+50				915.6
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T.P.	0.31	917.95 [✓]	12.50	917.64 [✓]
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17				913.9
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+50				912.3
-----	--	--	--	-------

18				910.9
----	--	--	--	-------

T.P.	4.45	911.95 [✓]	10.45	907.50 [✓]
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+25				910.2
-----	--	--	--	-------

+50				909.6 [✓]
-----	--	--	--	--------------------

19				908.6 [✓]
----	--	--	--	--------------------

+50				907.5
-----	--	--	--	-------

20				906.5
----	--	--	--	-------

+50				905.6
-----	--	--	--	-------

21				904.5
----	--	--	--	-------

+50				903.3
-----	--	--	--	-------

LT

Q

RT

$$\frac{10.8}{50} \frac{10.9}{34} \frac{12.4}{33} \frac{14.9}{27} \frac{16.5}{24-21} \frac{15.1}{15} \frac{14.7}{12} 14.5 \frac{14.8}{16} \frac{15.0}{16} \frac{16.5}{21} \frac{15.4}{24} \frac{12.1}{28} \frac{11.4}{32} \frac{11.4}{50} \quad \checkmark$$

$$\frac{2.2}{50} \frac{1.8}{32} \frac{3.9}{30} \frac{5.2}{24-19} \frac{4.6}{16} \frac{4.3}{12} \quad 4.1 \frac{4.3}{12} \frac{4.4}{16} \frac{5.3}{19} \frac{6.0}{23-26} \frac{5.5}{29} \frac{3.5}{32} \frac{2.6}{50} \quad \checkmark$$

$$\frac{6.8}{50} \frac{6.3}{32} \frac{6.7}{30} \frac{6.4}{21-18} \frac{6.0}{16} \frac{5.9}{11} 5.7 \quad 5.9 \frac{6.2}{12} \frac{7.4}{16} \frac{7.7}{20} \frac{6.4}{24-29} \frac{6.4}{33} \frac{6.4}{50} \quad \checkmark$$

$$\frac{11.1}{50} \frac{8.6}{28} \frac{8.7}{23} \frac{8.7}{19} \frac{7.7}{16} \frac{7.6}{12} \quad 7.1 \frac{7.3}{12} \frac{7.6}{15} \frac{7.9}{18} \frac{9.4}{23} \frac{9.6}{41} \frac{9.7}{50} \quad \checkmark$$

$$\frac{7.7}{50} \frac{7.5}{45} \frac{6.0}{26} \frac{2.7}{17} \frac{2.1}{13} \quad 1.8 \frac{1.8}{9} \frac{2.2}{15} \frac{4.7}{23} \frac{4.7}{33} \frac{4.6}{50} \quad \checkmark$$

$$\frac{9.5}{50} \frac{9.0}{35} \frac{8.1}{26} \frac{3.2}{15} \frac{2.7}{13} \quad 2.4 \frac{2.4}{11} \frac{2.8}{15} \frac{6.7}{24} \frac{7.0}{50} \quad \checkmark$$

$$\frac{12.8}{50} \frac{12.7}{43} \frac{11.0}{32} \frac{6.7}{22} \frac{4.1}{16} \frac{3.7}{12} \quad 3.4 \frac{3.6}{9} \frac{3.9}{13} \frac{4.4}{17} \frac{8.3}{27} \frac{8.1}{50} \quad \checkmark$$

$$\frac{7.7}{50} \frac{7.4}{37} \frac{7.4}{30} \frac{6.8}{24} \frac{6.4}{20} \frac{5.0}{17} \frac{4.6}{12} \quad 4.5 \frac{4.7}{10} \frac{5.0}{16} \frac{6.3}{19} \frac{6.6}{23} \frac{6.8}{26} \frac{6.2}{29} \frac{6.5}{50} \quad \checkmark$$

$$\frac{4.0}{50} \frac{4.0}{32} \frac{6.8}{26} \frac{7.4}{22} \frac{7.2}{19} \frac{6.1}{16} \frac{5.8}{11} \quad 5.5 \frac{5.7}{12} \frac{6.0}{15} \frac{6.9}{18} \frac{7.4}{23} \frac{6.4}{27} \frac{3.1}{32} \frac{3.3}{50} \quad \checkmark$$

$$\frac{3.9}{50} \frac{4.1}{33} \frac{7.4}{28} \frac{8.4}{23} \frac{8.3}{19} \frac{7.2}{16} \frac{6.7}{12} \quad 6.4 \frac{6.6}{10} \frac{7.0}{15} \frac{7.8}{19} \frac{8.2}{23} \frac{7.2}{26} \frac{2.8}{33} \frac{2.8}{50} \quad \checkmark$$

$$\frac{4.8}{50} \frac{5.3}{35} \frac{5.8}{31} \frac{7.5}{29} \frac{8.9}{26} \frac{9.6}{21} \frac{9.1}{17} \frac{8.1}{15} \frac{7.7}{12} \quad 7.5 \frac{7.7}{10} \frac{8.2}{15} \frac{8.9}{19} \frac{9.1}{23} \frac{8.0}{27} \frac{3.5}{33} \frac{2.5}{50} \quad \checkmark$$

$$\frac{7.6}{50} \frac{6.3}{40} \frac{6.5}{35} \frac{8.2}{31} \frac{10.1}{26} \frac{10.8}{22} \frac{10.6}{18} \frac{9.2}{16} \frac{8.9}{11} \quad 8.7 \frac{8.9}{11} \frac{9.3}{15} \frac{10.2}{19-23} \frac{8.5}{26} \frac{3.5}{32} \frac{3.0}{50} \quad \checkmark$$

STA	+	π	-	ELEV
		911.95 [✓]		

22+00				902.1
-------	--	--	--	-------

+50				900.9
-----	--	--	--	-------

23				899.8
----	--	--	--	-------

T.P.	0.59	902.69 [✓]	9.85	902.10 [✓]
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+20				899.5
-----	--	--	--	-------

+30				899.3
-----	--	--	--	-------

+50				898.9
-----	--	--	--	-------

24				897.8
----	--	--	--	-------

+15	$\frac{1}{2}$ WATER WORKS SERVICE DRIVE LT			897.6
-----	--	--	--	-------

+36				897.2
-----	--	--	--	-------

+50				896.9
-----	--	--	--	-------

25				896.1
----	--	--	--	-------

+50				895.7
-----	--	--	--	-------

LT

4

RT

$\frac{10.5}{50}$ $\frac{9.5}{39}$ $\frac{9.2}{33}$ $\frac{11.2}{27}$ $\frac{11.8}{23}$ $\frac{11.6}{18}$ $\frac{10.5}{15}$ $\frac{10.1}{12}$ $\frac{10.2}{12}$ $\frac{10.7}{17}$ $\frac{11.3}{20}$ $\frac{9.4}{27}$ $\frac{4.7}{33}$ $\frac{2.9}{50}$ ✓

$\frac{15.5}{50}$ $\frac{14.7}{35}$ $\frac{13.8}{24}$ $\frac{13.0}{20}$ $\frac{11.8}{17}$ $\frac{11.4}{11}$ $\frac{11.1}{11}$ $\frac{11.5}{13}$ $\frac{11.6}{17}$ $\frac{12.1}{20}$ $\frac{12.3}{25}$ $\frac{11.6}{28}$ $\frac{9.5}{32}$ $\frac{8.1}{50}$ ✓

$\frac{18.2}{50}$ $\frac{18.1}{36}$ $\frac{17.6}{26}$ $\frac{13.2}{18}$ $\frac{12.5}{12}$ $\frac{12.2}{12}$ $\frac{12.5}{13}$ $\frac{12.9}{18}$ $\frac{15.4}{24}$ $\frac{14.2}{30}$ $\frac{12.6}{33}$ $\frac{12.6}{50}$ ✓

$\frac{9.6}{50}$ $\frac{9.2}{39}$ $\frac{8.3}{31}$ $\frac{3.9}{19}$ $\frac{3.8}{12}$ $\frac{3.2}{12}$ $\frac{3.6}{11}$ $\frac{3.8}{17}$ $\frac{7.0}{24}$ $\frac{6.8}{29}$ $\frac{5.7}{32}$ $\frac{5.2}{50}$ ✓

$\frac{5.2}{50}$ $\frac{5.0}{28}$ $\frac{4.1}{18}$ $\frac{3.9}{12}$ $\frac{3.4}{12}$ $\frac{3.8}{12}$ $\frac{4.0}{16}$ $\frac{7.0}{24}$ $\frac{7.4}{30}$ $\frac{6.5}{34}$ $\frac{6.2}{50}$ ✓

$\frac{4.8}{50}$ $\frac{4.9}{37}$ $\frac{4.9}{28}$ $\frac{4.2}{12}$ $\frac{3.8}{12}$ $\frac{4.2}{12}$ $\frac{4.3}{16}$ $\frac{7.5}{24}$ $\frac{7.6}{31}$ $\frac{6.9}{34}$ $\frac{6.7}{50}$ ✓

$\frac{4.8}{50}$ $\frac{4.6}{35}$ $\frac{5.3}{17}$ $\frac{5.1}{12}$ $\frac{4.9}{12}$ $\frac{5.2}{12}$ $\frac{5.4}{15}$ $\frac{8.1}{21}$ $\frac{8.1}{29}$ $\frac{6.1}{34}$ $\frac{5.7}{50}$ ✓

$\frac{4.1}{75}$ $\frac{4.2}{50}$ $\frac{4.5}{33}$ $\frac{5.3}{13}$ $\frac{5.1}{12}$ $\frac{5.5}{12}$ $\frac{5.7}{15}$ $\frac{8.1}{20}$ $\frac{8.3}{29}$ $\frac{5.9}{34}$ $\frac{5.8}{50}$ ✓

$\frac{6.5}{50}$ $\frac{6.3}{35}$ $\frac{7.1}{29}$ $\frac{7.1}{19}$ $\frac{7.1}{12}$ $\frac{5.5}{12}$ $\frac{5.8}{12}$ $\frac{6.1}{15}$ $\frac{8.2}{20}$ $\frac{8.5}{27}$ $\frac{5.9}{34}$ $\frac{5.8}{50}$ ✓

$\frac{6.7}{50}$ $\frac{7.2}{34}$ $\frac{7.6}{28}$ $\frac{7.3}{20}$ $\frac{6.3}{17}$ $\frac{6.2}{13}$ $\frac{5.8}{12}$ $\frac{6.0}{11}$ $\frac{6.2}{15}$ $\frac{8.4}{21}$ $\frac{8.5}{28}$ $\frac{5.5}{34}$ $\frac{5.6}{50}$ ✓

$\frac{8.0}{50}$ $\frac{7.7}{34}$ $\frac{7.8}{28}$ $\frac{8.1}{25}$ $\frac{7.9}{20}$ $\frac{7.3}{15}$ $\frac{7.3}{13}$ $\frac{6.6}{12}$ $\frac{6.8}{11}$ $\frac{7.0}{15}$ $\frac{8.4}{20}$ $\frac{8.7}{26}$ $\frac{4.9}{34}$ $\frac{5.3}{50}$ ✓

$\frac{8.8}{50}$ $\frac{8.8}{33}$ $\frac{9.0}{27}$ $\frac{8.6}{18}$ $\frac{7.7}{15}$ $\frac{7.4}{12}$ $\frac{7.0}{12}$ $\frac{7.2}{11}$ $\frac{7.5}{15}$ $\frac{8.7}{24}$ $\frac{8.7}{27}$ $\frac{5.7}{35}$ $\frac{6.5}{50}$ ✓

STA	+	π	-	ELEV
		902.69		

26				895.8
----	--	--	--	-------

+30				896.2
-----	--	--	--	-------

+50				896.6
-----	--	--	--	-------

27				897.7
----	--	--	--	-------

+50				899.3
-----	--	--	--	-------

28				900.8
----	--	--	--	-------

B.M	12.27	907.58	7.38	895.31	895.31
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+50				901.8
-----	--	--	--	-------

29				902.8
----	--	--	--	-------

+25				903.4
-----	--	--	--	-------

+41	⊥ R.R. TRACK RIGHT ANGLE			903.5
-----	--------------------------	--	--	-------

+41	⊥ PROFILE R.R. TRACKS			903.46
-----	-----------------------	--	--	--------

+50				903.5
-----	--	--	--	-------

LT

Q

RT

8.9	8.8	9.3	8.7	7.6	7.3		7.1	7.5	9.4	9.9	7.6	7.7	✓
50	33	29	18	76	12	6.9	12	16	22	25-29	33	50	

11.3	10.6	10.0	7.2	6.8		6.7	7.0	7.7	10.6	11.3	11.9	✓
50	27	22	16	12	6.5	12	14	17	24	33	50	

12.4	11.6	11.0	7.3	6.7	6.4	6.4	6.6	7.1	11.2	11.2	10.5	10.9	✓
50	33	27	18	14	12	11	14	17	25	29	33	50	

14.6	14.4	14.4	13.4	6.4	5.7	5.4	5.2	5.4	5.8	10.1	8.8	8.0	✓
75	50	42	33	17	15	12	11	14	17	26-29	32	50	

14.0	14.4	13.1	12.5	4.2	3.9	3.7	3.9	4.3	9.2	9.2	8.3	✓
75	50	33	30	16	12	12	15	17	28	36	50	

14.0	14.0	11.7	7.6	2.4	1.9	2.3	2.2	10.7	11.1	9.3	9.5	13.5	✓
75	50	32	14	11	19	12	16	32	38	50	58	77	

34' RT STA 28+18

SPIKE IN TOP COR F.P. S.W. COR OF FENCE + R.R. TRACKS

20.5	19.1	19.2	19.7	18.1	6.8	6.4	6.1	6.0	6.4	7.2	14.2	15.2	14.3	4.8	3.5	✓
75	70	60	57	35	16	14	11	5.8	11	14	18	31	42	46	65	72

19.7	18.6	15.4	5.2	5.1	4.8	4.8	5.0	5.3	3.9	4.7	5.3	7.4	✓
80	50	32	15	10	9	15	23	32	39	44	50	50	

TOP
W. RAIL

19.2	18.6	18.7	16.8	6.0	5.2	4.6	4.1	4.0	4.0	5.3	12.0	15.3	✓
75	56	50	37	17	15	8	4.2	9	11	20	24	39	50

TOP
W. RAIL

18.8	19.1	19.8	18.8	16.8	14.3	4.6	4.2	4.4	4.9	13.3	18.6	19.1	15.3	✓
75	67	64	50	42	34	16	8	10	14	33	50	62	75	

4.78	4.82	4.60	4.52	4.43	4.2	4.02	3.92	3.78	3.62	3.22	2.85	✓
700	150	100	75	50	25	25	50	75	100	150	200	

19.0	20.0	18.7	5.5	4.9	4.2	4.4	4.8	5.6	15.7	17.2	18.0	5.6	4.7	✓
75	67	53	23	19	7	10	13	16	37	43	53	64	75	

STA	+	Δ	-	ELEV
		907.58 ✓		
29+78				903.0
30				902.7
+15				902.7
+50				902.7
31				902.8
+50	⊥ WATER WORKS SERVICE +			903.2 ! DRIVE RT
32				904.0
T. P	10.20	912.28 ✓	5.50	902.08 ✓
+50				904.9
33				905.7
+40				906.3
+50				906.5
+64				906.6

LT

E

RT

TOP
W. RAIL

20.3	19.0	17.2	6.8	5.3	4.4	5.0	4.6	4.8	5.2	6.2	10.0	15.4	15.5	14.0	✓
83	68	62	42	36	30	18	9	46	8	13	17	24	34	50	69

TOP
W. RAIL

8.0	6.2	4.5	6.1	10.7	5.6	5.0	5.1	5.8	10.0	14.4	14.0	12.9	✓
75	70	50	37	28-26	14	10	49	12	16	24	32	50	70

TOP
W. RAIL

6.2	4.6	5.8	14.4	8.7	5.8	5.3	5.3	6.2	9.5	12.8	13.6	13.1	✓
75	66	52	34	30	15	11	49	11	19	23	30	50	65

15.3	18.0	17.5	5.8	5.3	5.3	5.6	9.7	12.5	12.5	11.6	✓
58	52	40	16	10	49	12	18	25	34	44	65

12.2	17.1	14.8	5.8	5.2	4.9	5.6	7.9	9.7	10.6	10.1	10.0	✓
75	50	34	15	11	4.9	7	17	23	27	44	46	50

17.0	13.6	13.8	2.0	5.5	4.8	4.4	4.4	4.4	4.3	4.2	4.0	✓
75	50	32	23	16	11	4.4	12	19	38	50	75	

14.2	13.2	12.3	14.4	9.0	4.5	3.9	3.7	4.2	6.3	6.2	6.0	✓
75	71	50	33	26	17	11	3.6	11	17	24	50	80

14.2	14.8	13.8	13.0	8.3	7.7	7.7	8.1	10.8	11.5	9.6	✓
75	50	37	29	17	11	7.4	11	16	24	50	61

14.2	13.5	11.6	7.5	7.0	7.0	7.8	10.9	11.4	10.1	5.6	✓
75-50	33	25	16	11	6.6	12	15	26	39	44	50

12.4	12.5	11.9	6.5	6.3	6.3	6.7	10.5	11.5	9.4	3.6	✓
75	38	26	15	12	6.0	11	16	26	34	41	50

10.1	10.0	10.8	6.2	6.1	6.2	6.6	10.0	11.0	11.4	10.2	6.1	✓
75-50	29	25	15	12	5.8	12	16	24	30	35	39	46

2.2	2.1	1.4	7.6	6.0	5.8	6.1	6.4	8.9	10.6	11.2	10.4	7.4	6.0	✓
75	50	33	21	18	11	5.7	12	16	22	28	34	38	42	46

STA	+	π	-	ELEV
		912.28		

34+00				907.0
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+50				907.1
-----	--	--	--	-------

35				907.1
----	--	--	--	-------

+50				906.6
-----	--	--	--	-------

36				905.8
----	--	--	--	-------

+50				904.9
-----	--	--	--	-------

37				903.8
----	--	--	--	-------

+40				902.8
-----	--	--	--	-------

+50				902.5
-----	--	--	--	-------

T.P	9.10	92034	1.04	911.24
-----	------	-------	------	--------

33+40				(906.3)
-------	--	--	--	---------

+50				(906.5)
-----	--	--	--	---------

+64				(906.6)
-----	--	--	--	---------

LT

4

RT

$$\frac{5.4}{23} \quad \frac{5.9}{21} \quad \frac{5.6}{72}$$

$$\frac{5.7}{73} \quad \frac{6.0}{76} \quad \frac{9.2}{24} \quad \frac{10.4}{28} \quad \frac{10.7}{34} \quad \frac{9.9}{38} \quad \frac{5.4}{46}$$

$$\frac{5.4}{22} \quad \frac{5.4}{13} \quad \frac{5.2}{52} \quad \frac{5.3}{11} \quad \frac{5.7}{16} \quad \frac{10.4}{27} \quad \frac{10.5}{31} \quad \frac{10.0}{37} \quad \frac{7.2}{41} \quad \frac{4.00}{48}$$

$$\frac{5.5}{31} \quad \frac{5.6}{16} \quad \frac{5.5}{11} \quad \frac{5.2}{52} \quad \frac{5.0}{11} \quad \frac{5.7}{76} \quad \frac{10.5}{28} \quad \frac{11.0}{35} \quad \frac{9.5}{41} \quad \frac{7.0}{46} \quad \checkmark$$

$$\frac{5.7}{23} \quad \frac{6.0}{21} \quad \frac{6.0}{10} \quad \frac{5.7}{57} \quad \frac{5.9}{11} \quad \frac{6.2}{15} \quad \frac{10.8}{28} \quad \frac{10.4}{45} \quad \checkmark$$

$$\frac{6.4}{23} \quad \frac{7.0}{18} \quad \frac{6.8}{12} \quad \frac{6.6}{65} \quad \frac{7.0}{11} \quad \frac{11.4}{15} \quad \frac{12.0}{29} \quad \frac{11.2}{36} \quad \frac{10.2}{48} \quad \frac{7.3}{58} \quad \checkmark$$

$$\frac{7.7}{23} \quad \frac{7.9}{18} \quad \frac{2.9}{13} \quad \frac{7.4}{7.4} \quad \frac{7.5}{11} \quad \frac{7.9}{15} \quad \frac{11.7}{26} \quad \frac{12.4}{32} \quad \frac{11.9}{50} \quad \frac{11.3}{58} \quad \checkmark$$

$$\frac{7.3}{75} \quad \frac{6.2}{50} \quad \frac{6.0}{39} \quad \frac{5.3}{34} \quad \frac{9.3}{25} \quad \frac{9.2}{18} \quad \frac{8.8}{12} \quad \frac{8.5}{8.5} \quad \frac{8.7}{10} \quad \frac{9.1}{15} \quad \frac{12.1}{24} \quad \frac{12.5}{32} \quad \frac{12.7}{50} \quad \frac{13.5}{66} \quad \frac{8.0}{73} \quad \frac{4.74}{78-100}$$

$$\frac{11.2}{55} \quad \frac{10.0}{50} \quad \frac{10.9}{38} \quad \frac{10.3}{25} \quad \frac{10.1}{18} \quad \frac{10.1}{13} \quad \frac{9.5}{9.5} \quad \frac{9.8}{11} \quad \frac{10.2}{15} \quad \frac{12.6}{23} \quad \frac{12.7}{31} \quad \frac{12.1}{50} \quad \frac{13.6}{67} \quad \frac{12.4}{71}$$

$$\frac{13.4}{55} \quad \frac{12.7}{50} \quad \frac{11.4}{31} \quad \frac{11.5}{26} \quad \frac{10.8}{18} \quad \frac{10.5}{13} \quad \frac{9.8}{9.8} \quad \frac{10.2}{11} \quad \frac{10.6}{15} \quad \frac{11.9}{21} \quad \frac{12.7}{32} \quad \frac{13.2}{50} \quad \frac{14.0}{65} \quad \checkmark$$

$$\frac{14.0}{67} \quad \frac{1.0}{67} \quad \frac{0.8}{80} \quad \frac{0.3}{100} \quad \checkmark$$

$$\frac{13.8}{66} \quad \frac{1.1}{66} \quad \frac{0.3}{91} \quad \frac{+0.5}{100} \quad \checkmark$$

$$\frac{13.7}{67} \quad \frac{0.5}{67} \quad \frac{+0.5}{100} \quad \checkmark$$

STA	+	π	-	ELEV
		920.34		
34+00				(907.0)
+50				(907.1)
35				(907.1)
+50				(906.6)
36				(905.8)
+50				(904.9)
T.P	0.85	912.09	9.10	911.24
T.P	3.17	903.46	1180	900.29
37+65				902.0
+83				901.4
38				900.9
+50				899.3
+72				898.8
+89				898.5

LT

E

RT

$$\frac{9.9}{75} \quad \frac{8.4}{50} \quad \frac{2.9}{32} \quad (13.3) \quad \frac{0.0}{66} \quad \frac{+0.7}{100} \quad \checkmark$$

$$\frac{8.0}{75} \quad \frac{6.7}{50} \quad \frac{6.0}{33} \quad (13.2) \quad \frac{0.0}{65} \quad \frac{+0.5}{67} \quad \frac{+0.5}{100} \quad \checkmark$$

$$\frac{7.3}{75} \quad \frac{6.0}{50} \quad \frac{5.1}{34} \quad (13.2) \quad \frac{9.3}{55} \quad \frac{0.0}{69} \quad \frac{+0.5}{70} \quad \frac{+0.1}{100} \quad \checkmark$$

$$\frac{8.4}{75} \quad \frac{6.8}{50} \quad \frac{6.1}{34} \quad (13.7) \quad \frac{10.3}{61} \quad \frac{5.6}{65} \quad \frac{1.1}{73} \quad \frac{0.4}{100} \quad \checkmark$$

$$\frac{9.5}{75} \quad \frac{8.2}{50} \quad \frac{7.6}{34} \quad (14.5) \quad \frac{9.9}{66} \quad \frac{2.3}{76} \quad \frac{1.9}{100} \quad \checkmark$$

$$\frac{12.0}{75} \quad \frac{9.8}{50} \quad \frac{8.8}{33} \quad (15.4) \quad \frac{12.7}{70} \quad \frac{5.3}{80} \quad \frac{5.5}{100} \quad \checkmark$$

$$\frac{8.7}{70} \quad \frac{6.8}{50} \quad \frac{5.2}{33} \quad \frac{4.1}{25} \quad \frac{2.1}{16} \quad \frac{1.8}{10} \quad 1.5 \quad \frac{1.7}{9} \quad \frac{2.1}{15} \quad \frac{3.5}{31} \quad \frac{4.2}{32} \quad \frac{4.8}{50} \quad \frac{6.4}{68} \quad \checkmark$$

$$\frac{10.1}{65} \quad \frac{8.2}{50} \quad \frac{6.6}{34} \quad \frac{5.1}{21} \quad \frac{2.7}{14} \quad \frac{2.2}{9} \quad 2.1 \quad \frac{2.3}{9} \quad \frac{2.8}{15} \quad \frac{5.7}{22} \quad \frac{6.9}{32} \quad \frac{9.1}{50} \quad \checkmark$$

$$\frac{9.3}{30} \quad \frac{6.7}{22} \quad \frac{3.2}{13} \quad \frac{2.8}{9} \quad 2.6 \quad \frac{2.8}{9} \quad \frac{3.4}{15} \quad \frac{7.3}{24} \quad \frac{8.2}{28} \quad \frac{8.5}{33} \quad \frac{10.2}{50} \quad \checkmark$$

$$\frac{11.5}{50} \quad \frac{10.1}{35} \quad \frac{9.2}{20} \quad \frac{4.6}{14} \quad \frac{4.2}{8} \quad 4.2 \quad \frac{4.5}{9} \quad \frac{5.0}{17} \quad \frac{11.4}{78} \quad \frac{13.0}{33} \quad \frac{15.4}{50} \quad \checkmark$$

$$\frac{12.1}{50} \quad \frac{10.1}{27} \quad \frac{5.2}{16} \quad \frac{4.7}{7} \quad 4.7 \quad \frac{5.0}{9} \quad \frac{5.3}{15} \quad \frac{16.1}{35} \quad \frac{17.6}{50} \quad \checkmark$$

$$\frac{12.2}{50} \quad \frac{10.6}{37} \quad \frac{11.3}{29} \quad \frac{9.4}{23} \quad \frac{5.3}{14} \quad \frac{5.0}{9} \quad 5.0 \quad \frac{5.2}{9} \quad \frac{6.0}{14} \quad \frac{14.0}{27} \quad \frac{16.8}{38} \quad \frac{18.0}{50} \quad \checkmark$$

STA	+	π	—	ELEV	
		903.46			
39+00				898.3	
+15	Φ MONOLITHIC CULVERT			898.1	SUCKERTS VERNALIS CHANNEL
+38				897.9	
+50				897.8	
40				898.0	
T.P.	10.40	913.56	0.30	903.16	
+50				898.7	
+72				899.1	
+85				899.5	
41				899.9	
+20				900.5	
+50				901.5	
42				903.2	

LT

Z

RT

$\frac{18.4}{50}$ $\frac{17.2}{35}$ $\frac{10.8}{26}$ $\frac{9.7}{22}$ $\frac{5.3}{14}$ $\frac{5.3}{8}$ $\frac{5.4}{9}$ $\frac{5.5}{14}$ $\frac{16.6}{30}$ $\frac{17.3}{38}$ $\frac{18.2}{38}$ ✓

F.L. TOP H. WALL

TOP H. WALL FL

$\frac{26.6}{38}$ $\frac{26.70}{37}$ $\frac{17.73}{37}$ $\frac{17.3}{32}$ $\frac{13.8}{26}$ $\frac{9.0}{19}$ $\frac{6.0}{13}$ $\frac{5.4}{9}$ $\frac{5.4}{9}$ $\frac{5.5}{9}$ $\frac{5.8}{14}$ $\frac{16.9}{31}$ $\frac{17.92}{37}$ $\frac{26.80}{37}$ $\frac{25.9}{38}$ ✓

$\frac{18.6}{50}$ $\frac{17.9}{30}$ $\frac{5.9}{13}$ $\frac{5.7}{9}$ $\frac{5.6}{10}$ $\frac{5.8}{10}$ $\frac{6.0}{14}$ $\frac{13.8}{25}$ $\frac{16.3}{33}$ $\frac{18.0}{40}$ $\frac{22.14}{50}$ ✓

$\frac{18.2}{50}$ $\frac{18.0}{31}$ $\frac{5.9}{12}$ $\frac{5.8}{9}$ $\frac{5.7}{10}$ $\frac{5.9}{10}$ $\frac{6.0}{13}$ $\frac{16.5}{30}$ $\frac{18.0}{50}$ ✓

$\frac{17.4}{50}$ $\frac{17.0}{30}$ $\frac{5.8}{13}$ $\frac{5.7}{9}$ $\frac{5.5}{10}$ $\frac{5.6}{10}$ $\frac{5.6}{14}$ $\frac{16.5}{32}$ $\frac{16.3}{50}$ ✓

$\frac{24.0}{50}$ $\frac{23.5}{24}$ $\frac{16.3}{15}$ $\frac{15.2}{14}$ $\frac{15.1}{10}$ $\frac{14.9}{10}$ $\frac{15.0}{10}$ $\frac{15.4}{14}$ $\frac{23.8}{28}$ $\frac{23.6}{38}$ $\frac{23.4}{50}$ ✓

$\frac{22.9}{50}$ $\frac{22.5}{27}$ $\frac{20.2}{24}$ $\frac{15.1}{14}$ $\frac{14.7}{10}$ $\frac{14.5}{10}$ $\frac{14.7}{11}$ $\frac{15.0}{14}$ $\frac{21.2}{25}$ $\frac{22.4}{32}$ $\frac{22.2}{50}$ ✓

$\frac{17.1}{50}$ $\frac{16.2}{31}$ $\frac{15.2}{17}$ $\frac{14.3}{10}$ $\frac{14.1}{10}$ $\frac{14.3}{10}$ $\frac{14.7}{15}$ $\frac{20.0}{25}$ $\frac{21.3}{33}$ $\frac{21.2}{50}$ $\frac{20.0}{65}$ ✓

$\frac{17.0}{50}$ $\frac{17.3}{30}$ $\frac{17.6}{27}$ $\frac{14.1}{24}$ $\frac{13.8}{16}$ $\frac{13.7}{10}$ $\frac{14.0}{12}$ $\frac{14.2}{15}$ $\frac{19.1}{24}$ $\frac{20.0}{31}$ $\frac{20.2}{50}$ $\frac{19.4}{65}$ ✓

$\frac{14.9}{50}$ $\frac{15.3}{31}$ $\frac{15.7}{27}$ $\frac{13.2}{19}$ $\frac{13.2}{16}$ $\frac{13.3}{10}$ $\frac{13.4}{11}$ $\frac{13.7}{16}$ $\frac{18.6}{25}$ $\frac{18.4}{31}$ $\frac{18.8}{50}$ $\frac{17.1}{70}$ ✓

$\frac{10.5}{50}$ $\frac{11.0}{32}$ $\frac{13.2}{26}$ $\frac{12.5}{16}$ $\frac{12.3}{11}$ $\frac{12.1}{12}$ $\frac{12.5}{11}$ $\frac{12.7}{16}$ $\frac{17.2}{26}$ $\frac{17.6}{32}$ $\frac{17.2}{50}$ $\frac{14.6}{75}$ ✓

$\frac{2.2}{35}$ $\frac{10.6}{24}$ $\frac{11.3}{21}$ $\frac{11.0}{19}$ $\frac{10.7}{16}$ $\frac{10.4}{10}$ $\frac{10.8}{13}$ $\frac{7.2}{17}$ $\frac{14.5}{26}$ $\frac{15.1}{31}$ $\frac{15.6}{50}$ $\frac{15.0}{65}$ $\frac{12.2}{85}$ ✓

STA	+	Δ	-	ELEV
		913.56		
42	+50			904.8
	+80			905.7
43				906.3
	+50			907.8
	+60			908.1
	+70			908.4
+83	Φ	WATER WORK SERVICE		908.7 DRIVE, RT.
44				909.1
	+06			909.2
	+16			909.5
	+50			910.1
	+75			910.6

LT

E

RT

$$\frac{8.4}{21} \frac{9.5}{13-12} \frac{9.3}{11} \frac{9.1}{8} \underline{8.8}$$

$$\frac{9.2}{13} \frac{9.6}{17} \frac{14.1}{32} \frac{14.7}{50} \frac{12.6}{89} \checkmark$$

$$\frac{7.0}{20} \frac{7.9}{15} \frac{8.6}{14-12} \frac{8.1}{9} \underline{7.9}$$

$$\frac{8.3}{13} \frac{8.6}{17} \frac{12.8}{28} \frac{13.9}{50} \frac{13.5}{78} \frac{11.3}{90} \checkmark$$

$$\frac{6.5}{20} \frac{2.9}{14} \frac{7.6}{11} \frac{7.4}{7} \underline{7.3}$$

$$\frac{7.6}{12} \frac{8.1}{17} \frac{12.4}{28} \frac{13.0}{32} \frac{13.4}{50} \frac{13.4}{80} \frac{12.1}{90} \checkmark$$

$$\frac{4.6}{22} \frac{6.0}{16} \frac{6.3}{13} \frac{6.0}{9} \underline{5.8}$$

$$\frac{6.1}{10} \frac{6.5}{15} \frac{6.3}{20} \frac{9.9}{28} \frac{10.0}{32} \frac{11.3}{50} \frac{11.0}{76} \frac{9.4}{85} \checkmark$$

$$\frac{5.3}{22} \frac{5.9}{16} \frac{5.7}{9} \underline{5.5}$$

$$\frac{5.9}{11} \frac{6.1}{15} \frac{6.1}{19} \frac{9.7}{26} \frac{9.4}{32} \frac{10.0}{50} \frac{9.6}{78} \frac{7.2}{87} \checkmark$$

$$\frac{4.5}{22} \frac{5.8}{17-15} \frac{5.5}{12} \frac{5.4}{9} \underline{5.2}$$

$$\frac{5.5}{11} \frac{5.8}{16} \frac{6.3}{30} \frac{6.0}{50} \checkmark$$

$$\frac{4.3}{24} \frac{5.6}{16} \frac{5.2}{9} \underline{4.9}$$

$$\frac{5.2}{11} \frac{5.2}{17} \frac{4.8}{32} \frac{4.6}{50} \frac{4.3}{100} \checkmark$$

$$\frac{3.8}{26} \frac{6.1}{20} \frac{5.8}{17} \frac{5.1}{15} \frac{4.9}{10} \underline{4.5}$$

$$\frac{4.8}{12} \frac{5.1}{17} \frac{5.5}{24} \frac{5.0}{30} \frac{4.8}{50} \checkmark$$

$$\frac{4.5}{25} \frac{6.1}{20-18} \frac{4.9}{15} \frac{4.7}{9} \underline{4.4}$$

$$\frac{4.7}{13} \frac{5.1}{18} \frac{5.5}{26} \frac{4.9}{33} \frac{4.8}{50} \checkmark$$

$$\frac{4.7}{25} \frac{5.9}{21-19} \frac{5.0}{16} \frac{4.5}{11} \underline{4.1}$$

$$\frac{4.6}{13} \frac{5.1}{21} \frac{5.3}{27} \frac{4.3}{30} \frac{4.5}{36} \frac{5.7}{43} \frac{6.0}{50} \checkmark$$

$$\frac{0.6}{50} \frac{1.5}{32} \frac{4.6}{26} \frac{5.5}{24-20} \frac{4.1}{15} \frac{3.8}{9} \underline{3.5}$$

$$\frac{3.6}{8} \frac{3.9}{15} \frac{4.7}{20} \frac{5.0}{27} \frac{5.8}{36} \frac{5.8}{45} \frac{6.2}{50} \checkmark$$

$$\frac{1.7}{50} \frac{2.8}{32} \frac{4.9}{26} \frac{5.0}{23} \frac{5.1}{19} \frac{3.7}{16} \frac{3.5}{10} \underline{3.0}$$

$$\frac{3.3}{10} \frac{3.7}{16} \frac{4.5}{20} \frac{5.5}{37} \frac{5.7}{50} \checkmark$$

STA	+	IK ✓	-	ELEV
		913.56		
44+85				910.7'
45				910.9'
+50				911.7'
+60				911.8' ✓
B.M	11.35	920.50 ✓	4.37	909.19 (909.15)
42				(903.2)
+50				(904.8)
+80				(905.7)
43				(906.3)
+50				(907.8)
+60				(908.1)
+70				(908.4)
+83				(908.7)

LT

4

RT

$$\frac{2.1}{50} \quad \frac{2.8}{31} \quad \frac{4.7}{27} \quad \frac{4.9}{23} \quad \frac{4.9}{19} \quad \frac{3.7}{13} \quad \frac{3.2}{9} \quad \frac{2.9}{2.9} \quad \frac{3.2}{13} \quad \frac{3.6}{17} \quad \frac{4.4}{20} \quad \frac{5.2}{37} \quad \frac{7.2}{38} \quad \frac{8.3}{50}$$

2

$$\frac{2.2}{50} \quad \frac{3.3}{31} \quad \frac{4.9}{29} \quad \frac{5.9}{24} \quad \frac{5.0}{20} \quad \frac{3.5}{16} \quad \frac{3.0}{10} \quad \frac{2.7}{2.7} \quad \frac{2.8}{13} \quad \frac{3.3}{17} \quad \frac{4.2}{19} \quad \frac{4.9}{31} \quad \frac{7.1}{38} \quad \frac{8.3}{50}$$

$$\frac{2.5}{50} \quad \frac{3.2}{32} \quad \frac{4.3}{29} \quad \frac{4.4}{24} \quad \frac{4.3}{20} \quad \frac{2.6}{16} \quad \frac{2.0}{10} \quad \frac{1.9}{1.9} \quad \frac{2.1}{11} \quad \frac{2.5}{16} \quad \frac{3.7}{21} \quad \frac{4.4}{31} \quad \frac{5.6}{34} \quad \frac{6.8}{39} \quad \frac{7.3}{50}$$

$$\frac{2.7}{50} \quad \frac{3.1}{32} \quad \frac{4.0}{30} \quad \frac{4.2}{25} \quad \frac{2.5}{20} \quad \frac{2.0}{16} \quad \frac{1.8}{1.8} \quad \frac{2.0}{12} \quad \frac{2.8}{15} \quad \frac{3.4}{19} \quad \frac{4.1}{32} \quad \frac{4.8}{37} \quad \frac{5.4}{44} \quad \frac{6.2}{50}$$

SPIKE IN 24" OAK 44' LT STA 45+58

$$\frac{12.4}{100} \quad \frac{11.8}{75} \quad \frac{10.8}{50} \quad \frac{9.0}{34} \quad (17.3)$$

$$\frac{4.4}{100} \quad \frac{3.8}{75} \quad \frac{3.5}{50} \quad \frac{3.3}{35} \quad (15.7)$$

$$\frac{2.7}{100} \quad \frac{1.4}{75} \quad \frac{0.5}{50} \quad \frac{0.8}{34} \quad (14.8)$$

$$\frac{1.6}{100} \quad \frac{0.6}{75} \quad \frac{0.3}{50} \quad \frac{1.0}{34} \quad (14.2)$$

$$\frac{+0.8}{100} \quad \frac{+0.4}{75} \quad \frac{0.0}{50} \quad \frac{1.3}{34} \quad (12.7)$$

$$\frac{+1.1}{100} \quad \frac{+0.4}{75} \quad \frac{1.2}{50} \quad \frac{1.5}{34} \quad (12.4)$$

$$\frac{+1.2}{100} \quad \frac{+0.5}{75} \quad \frac{1.1}{50} \quad \frac{2.1}{34} \quad (12.1)$$

$$\frac{0.0}{100} \quad \frac{0.1}{75} \quad \frac{1.8}{50} \quad \frac{3.0}{34} \quad (11.8)$$

STA	+	π	—	ELEV
		920.50		
44+00				909.1
+06				909.2
+16				909.5
+50				910.1
+75				910.6
46				912.2
+50				913.1
+80				913.5
47				913.8
+50				914.5
T.P.	10.37	919.52	11.35	909.15
+75				915.0
48				915.6

LT

E

RT

$$\begin{array}{r} 3.3 \\ 0.0 \quad 1.0 \quad 8.3 \quad 4.6 \\ 100 \quad 75 \quad 30 \quad 34 \end{array}$$

(11.4.)

✓

$$\begin{array}{r} 0.4 \quad 1.7 \quad 3.2 \quad 5.1 \\ 100 \quad 75 \quad 50 \quad 33 \end{array}$$

(11.3.)

✓

$$\begin{array}{r} 1.2 \quad 2.7 \quad 5.0 \quad 5.7 \\ 100 \quad 75 \quad 50 \quad 33 \end{array}$$

(11.0.)

✓

$$\begin{array}{r} 3.3 \quad 5.6 \\ 100 \quad 75 \end{array}$$

(10.4.)

✓

$$\begin{array}{r} 4.3 \quad 7.0 \\ 100 \quad 75 \end{array}$$

(9.9.)

✓

$$\begin{array}{r} 8.6 \quad 9.1 \quad 10.6 \quad 10.7 \quad 10.5 \quad 8.7 \quad 8.4 \quad 8.3 \quad 8.6 \quad 9.0 \quad 10.0 \quad 6.5 \quad 6.8 \quad 8.1 \\ 50 \quad 32 \quad 28 \quad 24 \quad 20 \quad 16 \quad 8 \quad 13 \quad 17 \quad 20 \quad 27 \quad 34 \quad 40 \quad 50 \end{array}$$

✓

$$\begin{array}{r} 7.6 \quad 8.0 \quad 9.4 \quad 9.7 \quad 9.5 \quad 8.0 \quad 7.6 \quad 7.4 \quad 7.8 \quad 8.1 \quad 9.4 \quad 9.8 \quad 9.7 \quad 6.7 \quad 6.5 \quad 7.8 \\ 50 \quad 31 \quad 28 \quad 23 \quad 19 \quad 15 \quad 9 \quad 12 \quad 12 \quad 16 \quad 19 \quad 23 \quad 27 \quad 33 \quad 42 \quad 50 \end{array}$$

$$\begin{array}{r} 7.7 \quad 8.0 \quad 8.3 \quad 7.4 \quad 7.1 \quad 7.0 \quad 7.3 \quad 7.6 \quad 8.5 \quad 9.8 \quad 9.8 \quad 7.7 \quad 7.7 \quad 8.5 \\ 50 \quad 31 \quad 24 \quad 15 \quad 10 \quad 12 \quad 16 \quad 19 \quad 23 \quad 28 \quad 33 \quad 39 \quad 50 \end{array}$$

$$\begin{array}{r} 8.8 \quad 9.0 \quad 8.1 \quad 8.0 \quad 7.2 \quad 7.0 \quad 7.0 \quad 7.3 \quad 8.7 \quad 9.5 \quad 10.1 \\ 50 \quad 36 \quad 24 \quad 19 \quad 14 \quad 10 \quad 6.7 \quad 11 \quad 15 \quad 21 \quad 33 \quad 50 \end{array}$$

✓

$$\begin{array}{r} 12.0 \quad 11.3 \quad 11.0 \quad 10.5 \quad 6.6 \quad 6.3 \quad 6.0 \quad 6.2 \quad 6.6 \quad 10.2 \quad 11.2 \quad 11.5 \\ 50 \quad 36 \quad 29 \quad 24 \quad 15 \quad 12 \quad 11 \quad 15 \quad 22 \quad 34 \quad 50 \end{array}$$

✓

$$\begin{array}{r} 12.7 \quad 12.1 \quad 11.3 \quad 6.0 \quad 5.1 \quad 4.8 \quad 4.5 \quad 4.8 \quad 5.2 \quad 10.9 \quad 11.5 \quad 11.8 \quad 11.2 \\ 50 \quad 28 \quad 25 \quad 15 \quad 13 \quad 10 \quad 12 \quad 16 \quad 26 \quad 30 \quad 39 \quad 50 \end{array}$$

✓

$$\begin{array}{r} 15.2 \quad 15.1 \quad 12.6 \quad 12.5 \quad 10.7 \quad 4.4 \quad 4.2 \quad 4.2 \quad 4.7 \quad 11.4 \quad 12.2 \quad 11.8 \quad 11.2 \\ \text{WINTER} \quad 75 \quad 50 \quad 28 \quad 27 \quad 22 \quad 12 \quad 9 \quad 39 \quad 11 \quad 16 \quad 27 \quad 31 \quad 34 \quad 35 \quad 50 \end{array}$$

✓

STA	+	Δ	-	ELEV
		919.52 [✓]		

48+50				917.2
-------	--	--	--	-------

49				919.2
----	--	--	--	-------

+50				21.4
-----	--	--	--	------

+75				22.6
-----	--	--	--	------

50				23.8
----	--	--	--	------

+10				24.4
-----	--	--	--	------

+20				24.9
-----	--	--	--	------

+41				25.9
-----	--	--	--	------

T.P	11.82	931.15 [✓]	0.19	919.33
-----	-------	---------------------	------	--------

49+50				21.4
-------	--	--	--	------

+75				22.6
-----	--	--	--	------

50				23.8
----	--	--	--	------

+10				24.4
-----	--	--	--	------

LT

L

RT

$$\begin{array}{r} 12.1 \quad 15.9 \quad 18.3 \quad 12.5 \quad 11.1 \quad 10.6 \quad 3.6 \quad 2.9 \quad 2.6 \\ \text{WATER } 75 \quad 50 \quad 28 \quad 24 \quad 22 \quad 16 \quad 14 \quad 9 \quad 23 \end{array} \quad \begin{array}{r} 2.6 \quad 2.9 \quad 3.2 \quad 11.6 \quad 12.5 \quad 12.2 \\ 12 \quad 15 \quad 17 \quad 30 \quad 37 \quad 50 \end{array} \quad \checkmark$$

$$\begin{array}{r} 12.1 \quad 14.9 \quad 14.6 \quad 12.8 \quad 10.2 \quad 9.5 \quad 1.8 \quad 10.06 \\ \text{WATER } 75 \quad 50 \quad 33 \quad 27 \quad 25 \quad 16 \quad 14 \quad 9 \quad 0.3 \end{array} \quad \begin{array}{r} 0.7 \quad 1.2 \quad 1.6 \quad 11.1 \quad 12.6 \quad 13.2 \quad 13.0 \\ 12 \quad 15 \quad 17 \quad 32 \quad 38 \quad 50 \quad 75 \end{array} \quad \checkmark$$

$$\begin{array}{r} 14.1 \quad 13.7 \quad 12.2 \quad 10.5 \\ 75 \quad 50 \quad 38 \quad 32 \end{array} \quad (+1.9) \quad \begin{array}{r} 10.2 \quad 11.8 \quad 12.0 \\ 33 \quad 50 \quad 75 \end{array} \quad \checkmark$$

$$\begin{array}{r} 11.9 \quad 11.8 \quad 10.7 \quad 10.5 \quad 9.5 \\ 75 \quad 62 \quad 50 \quad 46 \quad 33 \end{array} \quad (+3.1) \quad \begin{array}{r} 9.3 \quad 10.3 \quad 10.8 \quad 11.0 \\ 34 \quad 39 \quad 50 \quad 75 \end{array} \quad \checkmark$$

$$\begin{array}{r} 9.0 \quad 7.4 \quad 6.8 \\ 75 \quad 50 \quad 31 \end{array} \quad (+4.3) \quad \begin{array}{r} 8.8 \quad 9.4 \quad 9.9 \\ 34 \quad 50 \quad 75 \end{array} \quad \checkmark$$

$$\begin{array}{r} 8.5 \quad 6.3 \quad 5.5 \quad 4.3 \\ 75 \quad 50 \quad 35 \quad 28 \end{array} \quad (+4.9) \quad \begin{array}{r} 6.3 \quad 7.6 \quad 7.6 \quad 7.5 \quad 8.1 \quad 8.4 \\ 31 \quad 34 \quad 39 \quad 44 \quad 50 \quad 75 \end{array}$$

$$\begin{array}{r} 3.8 \quad 3.4 \quad 2.4 \quad 0.8 \\ 75 \quad 50 \quad 37 \quad 31 \end{array} \quad (+5.4) \quad \begin{array}{r} 6.0 \quad 6.7 \quad 6.7 \quad 7.1 \\ 33 \quad 38 \quad 41 \quad 50 \end{array} \quad \checkmark$$

$$\begin{array}{r} 3.2 \quad 3.0 \quad 1.6 \\ 75 \quad 50 \quad 41 \end{array} \quad (+6.4) \quad \begin{array}{r} 2.8 \quad 3.3 \quad 5.0 \quad 6.3 \\ 30 \quad 33 \quad 41 \quad 50 \end{array} \quad \checkmark$$

$$\begin{array}{r} 10.4 \quad 10.1 \quad 9.8 \quad 10.0 \quad 10.5 \quad 10.7 \\ 75 \quad 11 \quad 9 \quad 9 \quad 14 \quad 16 \end{array} \quad \checkmark$$

$$\begin{array}{r} 9.4 \quad 8.9 \quad 8.6 \quad 8.9 \quad 9.5 \\ 15 \quad 11 \quad 9 \quad 9 \quad 15 \end{array} \quad \checkmark$$

$$\begin{array}{r} 8.0 \quad 7.6 \quad 7.4 \quad 7.6 \quad 8.3 \\ 14 \quad 10 \quad 9 \quad 9 \quad 15 \end{array} \quad \checkmark$$

$$\begin{array}{r} 7.4 \quad 7.0 \quad 6.8 \quad 7.1 \quad 7.8 \\ 15 \quad 9 \quad 9 \quad 9 \quad 15 \end{array} \quad \checkmark$$

STA	+	π	-	ELEV
		931.15 ✓		
50+20				24.9
+41				25.9
+50				26.4
+65				27.1
+85				28.1
51				28.8
+50				31.0
T.P	12.59	943.65 ✓	0.09	931.06 ✓
51+50				(31.0)
52				33.3
+50				35.7
53				37.8
+50				40.0

LT

E

PT

$$\frac{12.0}{22} \frac{6.8}{13} \frac{6.5}{8} \underline{6.3}$$

$$\frac{6.8}{10} \frac{7.1}{16}$$

$$\frac{9.2}{23} \frac{7.3}{16} \frac{5.8}{11} \frac{5.5}{8} \underline{5.3}$$

$$\frac{5.5}{9} \frac{6.0}{16}$$

$$\frac{6.9}{50} \frac{8.7}{34} \frac{10.3}{31} \frac{6.5}{28} \frac{5.3}{21} \frac{5.0}{12} \frac{5.0}{9} \underline{4.8} \frac{5.0}{9} \frac{5.6}{16} \frac{9.5}{25} \frac{11.8}{31} \frac{13.4}{37} \frac{15.8}{58}$$

$$\frac{1.5}{50} \frac{2.3}{32} \frac{5.4}{26} \frac{6.2}{24} \frac{6.1}{21} \frac{5.0}{18} \frac{4.4}{11} \underline{4.1} \frac{4.3}{10} \frac{4.7}{12} \frac{7.5}{26} \frac{9.7}{36} \frac{11.7}{47} \frac{11.8}{50}$$

$$\frac{+0.4}{50} \frac{0.4}{32} \frac{4.3}{25} \frac{4.4}{22} \frac{4.3}{19} \frac{3.6}{17} \frac{3.7}{14} \frac{3.2}{8} \underline{3.1} \frac{3.2}{9} \frac{3.6}{16} \frac{4.5}{21} \frac{5.2}{29} \frac{5.9}{35} \frac{8.2}{50}$$

$$\frac{+5.1}{75} \frac{+2.0}{50} \frac{+1.6}{33} \frac{4.0}{24-21} \frac{3.0}{17} \frac{2.2}{10} \underline{2.4} \frac{2.7}{10} \frac{3.2}{16} \frac{4.1}{20} \frac{4.1}{27} \frac{7.7}{32} \frac{7.7}{35} \frac{5.5}{45} \frac{7.2}{50}$$

$$\frac{1.0}{22} \frac{0.8}{16} \frac{0.4}{10} \underline{0.2} \frac{0.7}{12} \frac{1.1}{19} \frac{1.5}{24}$$

$$(12.7) \frac{9.7}{33} \frac{10.3}{37} \frac{12.6}{44} \frac{14.1}{50}$$

$$\frac{11.6}{21-19} \frac{11.7}{17} \frac{10.8}{12} \underline{10.4} \frac{10.9}{14} \frac{11.4}{18} \frac{12.0}{20-23} \frac{6.3}{33} \frac{11.0}{50} \frac{12.6}{60} \frac{15.7}{75}$$

$$\frac{9.4}{21-19} \frac{8.8}{17} \frac{8.4}{13} \underline{8.0} \frac{8.5}{12} \frac{8.9}{18} \frac{9.2}{20-23} \frac{3.1}{33} \frac{3.8}{39} \frac{5.1}{50} \frac{6.7}{65} \frac{6.2}{75}$$

$$\frac{7.0}{21-19} \frac{6.6}{18} \frac{6.3}{15} \underline{5.9} \frac{6.3}{12} \frac{6.6}{17} \frac{6.9}{19-21} \frac{6.6}{22}$$

$$\frac{4.7}{21-19} \frac{4.3}{18} \frac{4.0}{14} \underline{3.7} \frac{4.1}{12} \frac{4.3}{18} \frac{4.1}{22}$$

STA	+	π	-	ELEV
-----	---	-------	---	------

943.65

54				41.8
----	--	--	--	------

+50				43.4
-----	--	--	--	------

T.P.	13.14	956.47	0.32	943.33
------	-------	--------	------	--------

51+50				31.0
-------	--	--	--	------

52				33.3
----	--	--	--	------

+50				35.7
-----	--	--	--	------

53				37.8
----	--	--	--	------

+50				40.0
-----	--	--	--	------

54				41.8
----	--	--	--	------

+50				43.4
-----	--	--	--	------

55				44.5
----	--	--	--	------

+50				44.9
-----	--	--	--	------

+80				44.8
-----	--	--	--	------

LT

Q

RT

$$\frac{2.2}{22} \quad \frac{2.6}{20} \quad \frac{2.8}{18} \quad \frac{2.1}{14} \quad \underline{1.9} \quad \frac{2.1}{11} \quad \frac{2.5}{15} \quad \frac{1.2}{23} \quad \checkmark$$

$$\frac{0.7}{23} \quad \frac{1.2}{20} \quad \frac{0.7}{15} \quad \underline{0.3} \quad \frac{0.5}{10} \quad \frac{0.7}{15} \quad \checkmark$$

$$\frac{12.3}{100} \quad \frac{12.4}{75} \quad \frac{14.6}{50} \quad \frac{15.8}{34} \quad \underline{26.5} \quad \checkmark$$

$$\frac{11.7}{100} \quad \frac{10.2}{75} \quad \frac{10.1}{50} \quad \frac{10.4}{36} \quad \underline{23.2} \quad \checkmark$$

$$\frac{12.3}{100} \quad \frac{11.5}{75} \quad \frac{10.6}{50} \quad \frac{10.1}{35} \quad \underline{20.8} \quad \checkmark$$

$$\frac{12.8}{100} \quad \frac{11.5}{75} \quad \frac{11.0}{50} \quad \frac{10.5}{33} \quad \underline{18.7} \quad \frac{8.1}{34} \quad \frac{10.0}{50} \quad \frac{13.6}{75} \quad \frac{16.4}{100} \quad \checkmark$$

$$\frac{12.1}{100} \quad \frac{9.2}{75} \quad \frac{8.5}{50} \quad \frac{7.6}{34} \quad \underline{16.5} \quad \frac{3.8}{36} \quad \frac{4.6}{50} \quad \frac{7.2}{75} \quad \frac{11}{100} \quad \checkmark$$

$$\frac{10.2}{100} \quad \frac{6.5}{75} \quad \frac{4.9}{50} \quad \frac{4.3}{36} \quad \underline{14.7} \quad \frac{1.9}{36} \quad \frac{2.6}{50} \quad \frac{4.1}{75} \quad \frac{8.2}{100} \quad \checkmark$$

$$\frac{9.2}{100} \quad \frac{5.7}{75} \quad \frac{4.2}{50} \quad \frac{3.3}{34} \quad \underline{13.1} \quad \frac{11.2}{23} \quad \frac{7.0}{32} \quad \frac{1.2}{36} \quad \frac{2.1}{50} \quad \frac{4.5}{75} \quad \frac{8.8}{100} \quad \checkmark$$

$$\frac{9.4}{100} \quad \frac{6.6}{75} \quad \frac{5.4}{50} \quad \frac{4.1}{33} \quad \underline{12.0} \quad \frac{2.2}{32} \quad \frac{3.5}{50} \quad \frac{6.4}{75} \quad \frac{9.7}{100} \quad \checkmark$$

$$\frac{9.8}{100} \quad \frac{7.8}{75} \quad \frac{7.2}{50} \quad \frac{6.7}{32} \quad \underline{11.6} \quad \frac{2.6}{32} \quad \frac{4.2}{50} \quad \frac{7.4}{75} \quad \frac{10.6}{100} \quad \checkmark$$

$$\frac{7.4}{75} \quad \frac{7.5}{50} \quad \frac{7.0}{31} \quad \underline{11.7} \quad \frac{3.5}{32} \quad \frac{4.5}{50} \quad \frac{7.4}{75} \quad \frac{11.4}{100} \quad \checkmark$$

STA	+	∇	-	ELEV
		956.47		
56+00				44.5
T.P.	3.87	948.66	11.68	944.79
55				44.5
+50				44.9
+80				44.8
56				44.5
+50				43.5
+85				42.6
57				42.1
+30				41.2
+50				40.7
+76				40.0
58				39.3

LT

♀

RT

 $\frac{2.0}{75} \frac{1.8}{50} \frac{1.2}{32} \quad (12.0) \quad \frac{5.2}{32} \frac{6.1}{50} \frac{8.7}{75} \frac{12.3}{100}$

✓

 $\frac{4.9}{23} \frac{5.3}{21} \frac{5.0}{19} \frac{4.6}{14} \quad 4.2 \quad \frac{4.3}{9} \frac{4.5}{16} \frac{3.2}{23}$

✓

 $\frac{5.0}{23} \frac{5.2}{21} \frac{4.7}{19} \frac{4.2}{14} \quad 3.8 \quad \frac{4.0}{10} \frac{4.3}{16} \frac{3.3}{23}$

✓

 $\frac{5.3}{23} \frac{5.4}{20} \frac{4.8}{17} \frac{4.2}{11} \quad 3.9 \quad \frac{4.2}{10} \frac{4.5}{17} \frac{3.4}{23}$

✓

 $\frac{5.5}{23} \frac{5.2}{20} \frac{4.6}{19} \frac{4.6}{13} \quad 4.2 \quad \frac{4.4}{9} \frac{4.8}{17} \frac{5.0}{19} \frac{3.6}{24}$

✓

 $\frac{4.4}{100} \frac{2.8}{75} \frac{1.7}{50} \frac{1.6}{33} \frac{5.8}{24} \frac{6.3}{22} \frac{6.1}{19} \frac{5.7}{14} \quad 5.2 \quad \frac{5.5}{11} \frac{5.8}{16} \frac{6.3}{19} \frac{6.2}{24} \frac{2.2}{31} \frac{2.1}{50} \frac{2.8}{75} \frac{5.8}{100}$
 $\frac{5.0}{100} \frac{3.6}{75} \frac{3.1}{50} \frac{2.7}{33} \frac{1.5}{25} \frac{8.1}{23} \frac{7.2}{21} \frac{6.6}{19} \frac{6.6}{15} \quad 6.1 \quad \frac{6.5}{11} \frac{7.0}{17} \frac{7.9}{21} \frac{7.2}{23} \frac{4.1}{25} \frac{4.0}{31} \frac{4.3}{50} \frac{8.1}{70} \frac{8.1}{100}$
 $\frac{5.2}{100} \frac{4.0}{75} \frac{3.7}{50} \frac{3.2}{33} \frac{2.8}{25} \frac{8.6}{23} \frac{7.5}{21} \frac{6.9}{19} \frac{6.6}{14} \quad 6.6 \quad \frac{7.0}{11} \frac{7.6}{19} \frac{8.0}{20} \frac{8.4}{23} \frac{5.5}{30} \frac{5.7}{50} \frac{6.5}{72} \frac{10.6}{100}$
 $\frac{5.9}{100} \frac{4.7}{75} \frac{4.5}{50} \frac{4.5}{32} \frac{8.6}{24} \frac{9.6}{23} \frac{8.4}{21} \frac{8.0}{18} \frac{8.0}{15} \quad 7.5 \quad \frac{7.8}{11} \frac{8.4}{19} \frac{8.9}{21} \frac{8.5}{23} \frac{8.4}{25} \frac{9.6}{30} \frac{9.6}{50} \frac{11.6}{75} \frac{14.4}{100}$
 $\frac{6.6}{100} \frac{5.6}{75} \frac{5.3}{50} \frac{5.2}{32} \frac{10.2}{23} \frac{9.0}{21} \frac{8.4}{17} \frac{8.4}{12} \quad 8.0 \quad \frac{8.5}{12} \frac{9.0}{78} \frac{9.5}{20} \frac{9.2}{22} \frac{9.3}{28} \frac{11.3}{50} \frac{13.3}{75} \frac{15.4}{100}$
 $\frac{7.3}{100} \frac{6.0}{75} \frac{5.5}{50} \frac{5.8}{33} \frac{10.0}{25} \frac{11.1}{24} \frac{9.6}{21} \frac{9.0}{18} \frac{9.0}{10} \quad 8.7 \quad \frac{9.3}{14} \frac{9.7}{19} \frac{10.2}{20} \frac{10.0}{22} \frac{12.0}{24} \frac{14.8}{50} \frac{18.1}{75} \frac{18.1}{100}$
 $\frac{7.8}{100} \frac{6.2}{75} \frac{5.8}{50} \frac{6.1}{33} \frac{10.5}{25} \frac{11.5}{22} \frac{10.4}{20} \frac{9.9}{18} \frac{9.9}{11} \quad 9.4 \quad \frac{10.0}{12} \frac{10.5}{18} \frac{10.8}{20} \frac{10.7}{23} \frac{10.4}{32} \frac{11.8}{50} \frac{14.3}{75} \frac{17.7}{100}$

STA	+	π ✓	-	ELEV
		948.66		

58+25				38.5
-------	--	--	--	------

+50				37.7
-----	--	--	--	------

+75				(36.8)
-----	--	--	--	--------

59				(35.8)
----	--	--	--	--------

+25				(34.8)
-----	--	--	--	--------

+50				(33.7)
-----	--	--	--	--------

+59				(33.0)
-----	--	--	--	--------

T.P.	0.82	938.22 ✓	11.26	937.40 ✓
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58+75				36.8
-------	--	--	--	------

59+00				35.8
-------	--	--	--	------

+25				34.8
-----	--	--	--	------

+50				33.7
-----	--	--	--	------

+59				33.0
-----	--	--	--	------

LT

♀

RT

$\frac{7.8}{100}$ $\frac{7.0}{75}$ $\frac{6.1}{56}$ $\frac{6.0}{50}$ $\frac{6.0}{34}$ $\frac{10.6}{27}$ $\frac{12.6}{24}$ $\frac{11.2}{22}$ $\frac{10.6}{19}$ $\frac{10.6}{11}$ $\frac{10.8}{10.2}$ $\frac{11.1}{13}$ $\frac{11.6}{17}$ $\frac{11.3}{18}$ $\frac{10.8}{20}$ $\frac{11.4}{22}$ $\frac{12.0}{32}$ $\frac{15.1}{42}$ $\frac{17.0}{50}$ $\frac{18.1}{73}$ $\frac{18.1}{86}$ $\frac{18.1}{100}$

$\frac{7.6}{100}$ $\frac{6.6}{75}$ $\frac{5.5}{50}$ $\frac{5.4}{36}$ $\frac{11.1}{29}$ $\frac{13.4}{25}$ $\frac{12.0}{23}$ $\frac{11.3}{18}$ $\frac{11.3}{12}$ $\frac{11.0}{11.0}$ $\frac{11.7}{14}$ $\frac{12.1}{17}$ $\frac{12.5}{17}$ $\frac{11.7}{21}$ $\frac{12.0}{30}$ $\frac{13.0}{41}$ $\frac{16.0}{53}$ $\frac{19.8}{75}$ $\frac{19.8}{100}$

$\frac{7.1}{100}$ $\frac{6.2}{75}$ $\frac{5.5}{50}$ $\frac{5.1}{40}$

(11.9.)

$\frac{6.1}{125}$ $\frac{6.1}{100}$ $\frac{6.1}{75}$ $\frac{6.3}{50}$

(12.9.)

$\frac{6.8}{150}$ $\frac{4.8}{100}$ $\frac{5.7}{75}$ $\frac{6.0}{55}$

(13.9.)

$\frac{5.5}{118}$ $\frac{3.7}{111}$ $\frac{4.6}{100}$ $\frac{5.6}{75}$ $\frac{6.1}{65}$

(15.0.)

$\frac{8.9}{100}$ $\frac{6.8}{96}$ $\frac{5.0}{88}$ $\frac{6.0}{71}$

(15.7.)

$\frac{1.0}{34}$ $\frac{2.8}{30}$ $\frac{3.9}{29}$ $\frac{2.4}{26}$ $\frac{1.7}{23}$ $\frac{1.7}{11}$ $\frac{1.4}{1.4}$ $\frac{1.8}{10}$ $\frac{2.4}{16}$ $\frac{3.9}{21}$ $\frac{2.6}{23}$ $\frac{2.8}{24}$ $\frac{4.2}{39}$ $\frac{5.7}{53}$ $\frac{6.3}{68}$ $\frac{11.6}{70}$ $\frac{13.4}{100}$ $\frac{13.4}{125}$

$\frac{2.2}{40}$ $\frac{3.8}{35}$ $\frac{4.3}{34}$ $\frac{3.2}{31}$ $\frac{2.4}{27}$ $\frac{2.4}{13}$ $\frac{2.4}{2.4}$ $\frac{3.1}{11}$ $\frac{3.3}{20}$ $\frac{4.1}{23}$ $\frac{4.7}{43}$ $\frac{6.7}{61}$ $\frac{9.4}{75}$ $\frac{13.3}{100}$ $\frac{15.4}{125}$

$\frac{1.8}{47}$ $\frac{4.2}{42}$ $\frac{4.8}{38}$ $\frac{3.8}{36}$ $\frac{3.4}{31}$ $\frac{3.2}{24}$ $\frac{3.1}{18}$ $\frac{3.1}{12}$ $\frac{3.4}{3.4}$ $\frac{4.0}{16}$ $\frac{4.4}{21}$ $\frac{5.9}{27}$ $\frac{6.9}{34}$ $\frac{9.1}{53}$ $\frac{10.1}{59}$ $\frac{12.9}{75}$ $\frac{16.4}{100}$ $\frac{18.4}{125}$

$\frac{2.0}{56}$ $\frac{4.0}{51}$ $\frac{4.7}{49}$ $\frac{4.9}{45}$ $\frac{4.6}{40}$ $\frac{4.0}{29}$ $\frac{4.0}{14}$ $\frac{4.0}{4.5}$ $\frac{5.7}{14}$ $\frac{6.5}{18}$ $\frac{6.0}{20}$ $\frac{8.8}{24}$ $\frac{7.8}{31}$ $\frac{11.3}{36}$ $\frac{14.8}{50}$ $\frac{12.9}{75}$ $\frac{20.0}{100}$ $\frac{20.0}{125}$

$\frac{1.8}{60}$ $\frac{4.6}{54}$ $\frac{5.0}{51}$ $\frac{4.7}{44}$ $\frac{4.4}{32}$ $\frac{4.4}{21}$ $\frac{4.4}{21}$ $\frac{5.2}{5.2}$ $\frac{6.1}{12}$ $\frac{7.1}{17}$ $\frac{6.8}{21}$ $\frac{7.3}{26}$ $\frac{10.2}{33}$ $\frac{12.0}{36}$ $\frac{14.8}{54}$ $\frac{16.1}{75}$ $\frac{19.2}{100}$ $\frac{21.2}{125}$

STA	+	Δ	-	ELE
		938.22 ✓		
59+66				32.6
+80				31.8
+96				30.8
60				30.5
+03	Δ	McMENEMY		30.4
+18				29.4
+31				28.6
+50				27.6
+75				26.5
61				25.7
+25				25.0
+40 ²¹				24.7
62				23.6 ✓
B.M			11.04	927.18 927.18

LT
♀
McMENEMY

5.7 5.5 5.1 4.9 4.7 5.1 6.6 7.5 7.2 9.3 11.6 12.7 13.1 13.8 16.8 19.6 21.7
175 100 75 50 27 14 5.6 12 19 26 29 35 37 45 59 75 100 125

♀
McMENEMY

5.1 5.1 5.3 5.6 5.9 6.4 6.9 8.7 8.2 11.8 14.9 16.6 18.5 20.0 21.0
100 94 50 33 14 10 23 25 27 36 46 68 81 100 125

♀
McMENEMY

5.7 6.3 6.9 7.4 7.8 8.7 10.1 10.0 15.5 18.1 20.8 22.1
100 34 17 12 28 34 36 42 61 78 100 125

♀
McMENEMY

5.7 6.2 6.6 7.2 7.7 8.7 9.4 10.7 12.4 20.9 23.4 ✓
97 58 33 14 13 32 44 64 130 162

7.8

♀
McMENEMY

0.0 1.2 3.2 3.5 8.6 8.8 8.6 8.8 9.8 11.6 13.8 ✓
85 70 34 37 29 25 17 13 28 68 100

0.4 2.2 4.2 9.9 9.9 9.8 10.0 10.6 11.3 11.4 12.5 13.6 ✓
87 66 39 30 19 9 12 24 33 45 70 100

10.6

11.7

12.5

13.2

13.5

14.6

SPIKE IN P. POLE S.W. COR McMENEMY + CORD "F"

