

OFFICE OF COUNTY ENGINEER
RAMSEY CO. MINN.

Road Map Survey

COUNTY ROAD D

From Labore Rd. To E. County Line

Road Acc't. No. 24

Date Filed 6-26-26 File _____

6-26-26

Co. Rd. D
Rd o/c N^o ~~53~~ 24

Office of Ramsey Co. Engineer	
ST. PAUL, MINN.	
Date Filed	6-26-26
File No.	

Sta Point Lt. Rt.

S 89° 33' E
750.685

33+11.9 P.I.

0° 26'

19+00 P.O.T.

S 89° 39' E
760.685

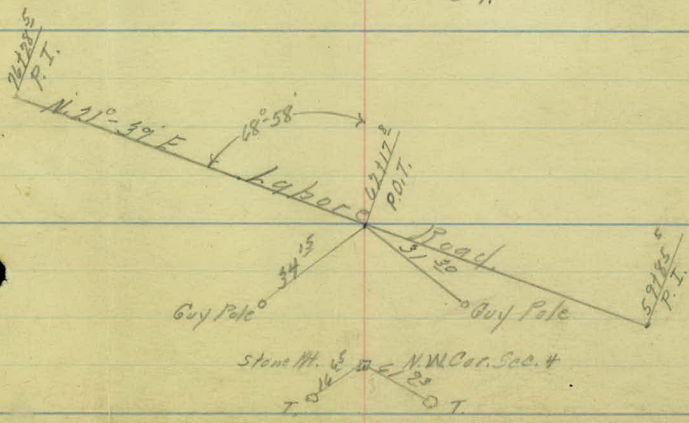
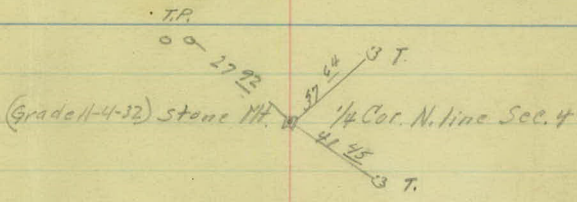
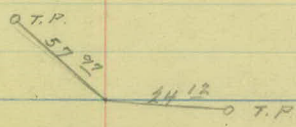
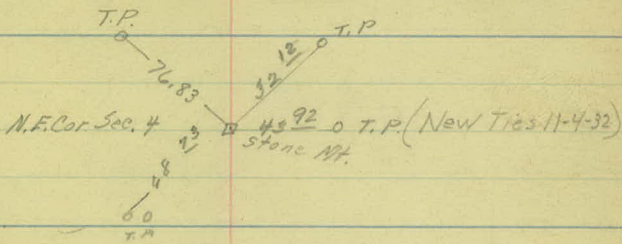
6+59.30 P.I.

0° 14'

S 89° 53' E
722.685

0+00 = 62+17.80 On Labore Road Survey Rd 0/c 41

1/18/26



Sta Point Lt. Rt.

N 84°-34'E
N 84°-54'E

57+75⁸⁰ P.I. 15°-02'

x

57+67⁸⁰ P.O.T.

57+53⁶⁵ P.O.T.

S 89°-24'E
S 78°-52'E

54+58⁷⁵ P.I.

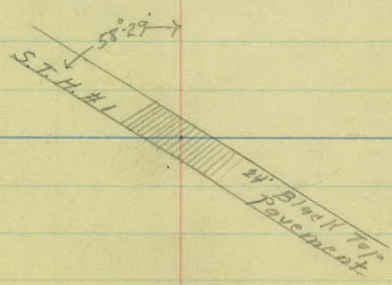
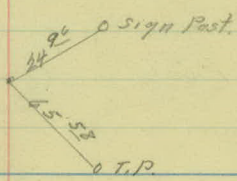
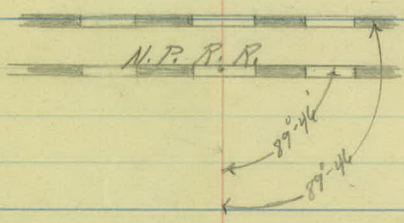
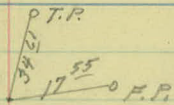
9°-09'

x

38+72⁷² P.O.T.

S 89°-33'E
S 89°-03'E

1/20/26



24' Black Top
Pavement

Sta Point Lt Rt.

106+57⁵ P.O.T. White Bear Rd.

S. 89°-55'E
589°-35'E

85+96²⁰ P.I. 0°-01'

x

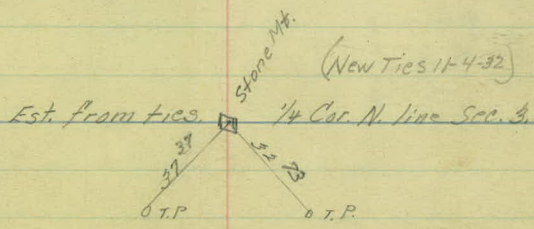
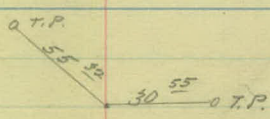
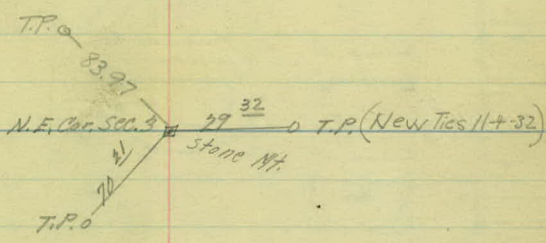
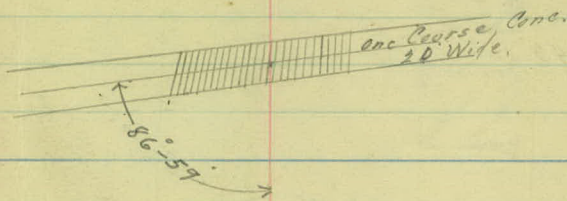
72+00 P.O.T.

S. 89°-54'E
589°-34'E

59+56⁶⁵ P.I. 5°-32'

N 84°-34'E x
N 84°-54'E

1/25/26



Sta. Point Lt. Rt.

191+48⁰ P.O.T. E. Co. line Rd.

589°-57'E

589°-37'E

165+10¹⁵ P.I.

0°-02'

138+73²⁰ P.O.T.

589°-58'E

589°-39'E

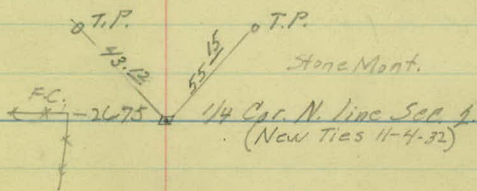
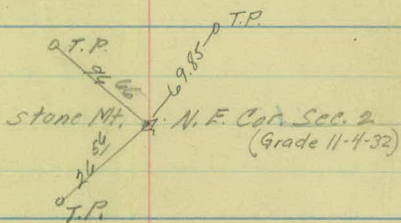
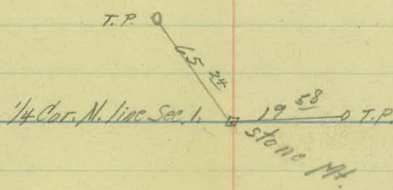
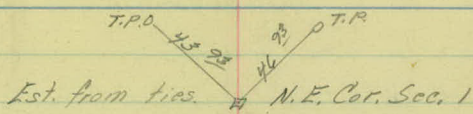
112+35⁷⁰ P.I. 0°-04'

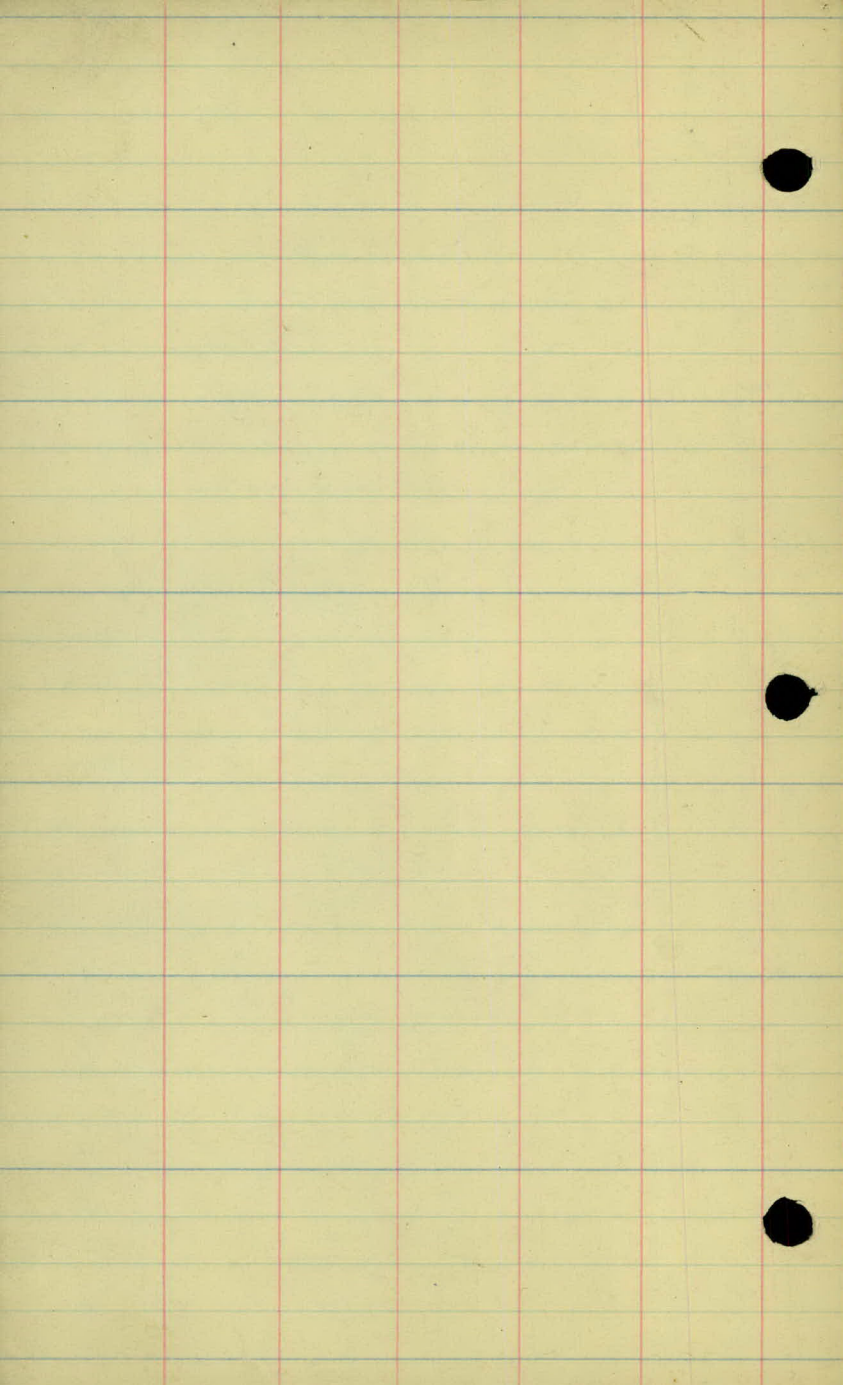
589°-55'E

589°-35'E

1/26/36

3
46





N

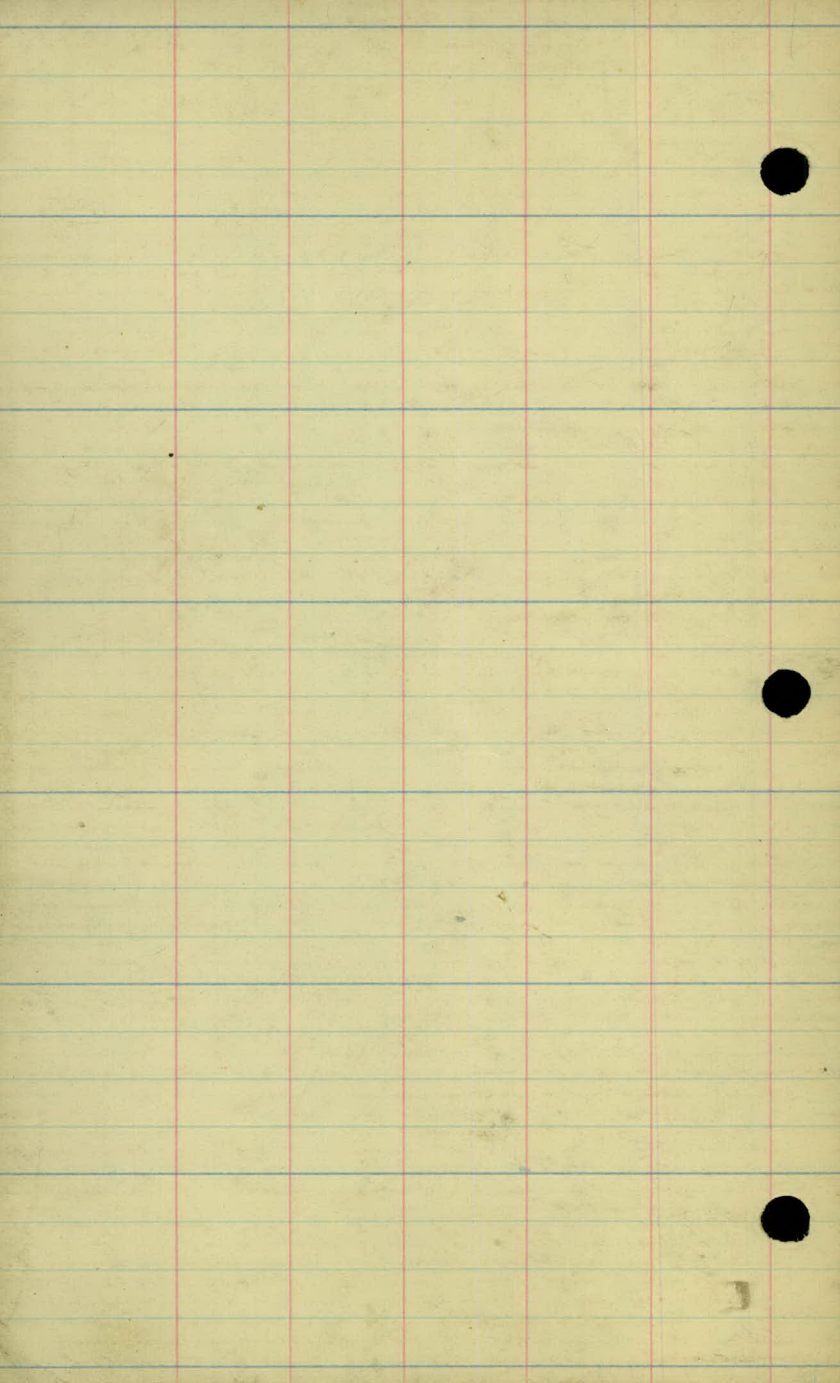
$$\begin{array}{r} 144 + 10.15 \\ 187 + 73.20 \\ \hline 24 + 83.35 \end{array}$$

Handwritten notes on a grid background, including:

- 36
- 2277.
- 2638.32
- 2638.33
- 2638.0
- 2636.35
- 262736.
- 2656
- 27067
- 4. EP. 4793
- 4693 TP.
- 6988 TP.
- 5/9
- TP.

70 LINE

See



53

7 6.93 5.91 1

59.845
40.4 FP.
LABORE

(374 62+62 Labour)

5EC 33

3E84

PI 76+28.5

3 T. H - 1

7P.04384

032
T.P.

34

$$\frac{3}{7} \times \frac{2}{3}$$

TP 3270

2644.0

✓

263342

7p

1

263635

7

...

2

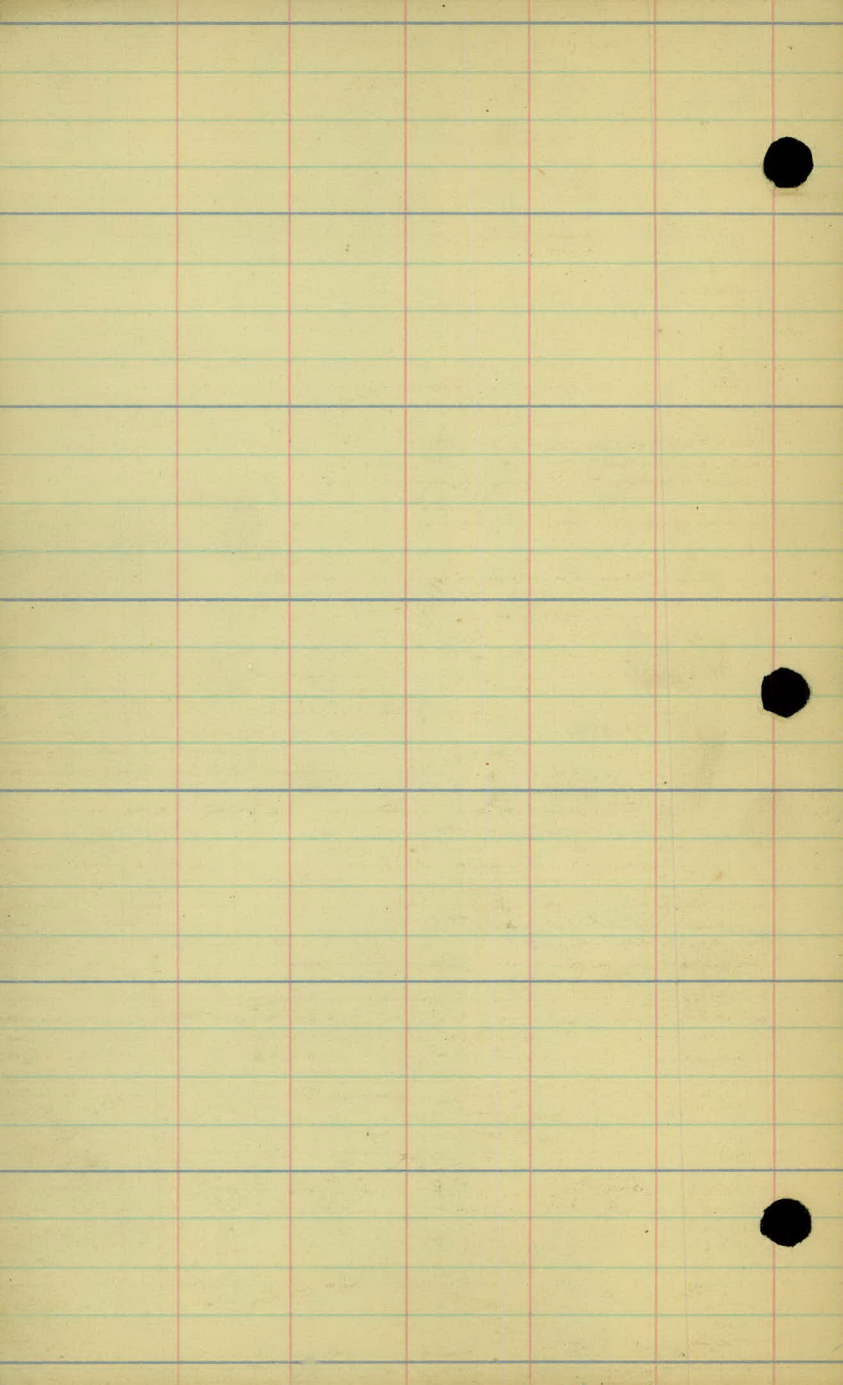
W. B.

L.P. RD.

35 35

352

T.P. 6.975



Co. Rd. D.

Road 9/10 # ~~55~~ 24

Art. Topog. from the
Labore Rd. to the E. Co. line Rd.

Sta.

5

4

3

2

1

0+00

11

10

9

8

7

6

5

1/20/24

11.24

481 T.P. 22'

406 F. Coe. 41

F. 25

Pl. 9

5. 1. 12

f45 T.P. 21'

F. 25

f14 T.P. 21

F. 26

482 7.10.24

482 T. 1st 17

F. 24

450 T. R. 20

F. 19

460-40"-T.-30

f14 T.P. 17

C. L. 10

5, 2, 13

735 F. Cor. 20

+11 F. Ent.

496 F. Cor. 20

492 T. P. 18

414 F. Co. 21

+ 70 T.P. 18

+20 F. Ent.

408 F. Cor. 21

#03 Mail Box 14

793 T.P. 19

F21

#18 T.P. 19

17

16

15

14

13

12

11

1/20/26

+89 T.P. 24'

+58 F. 29
+58 F.C. 26

+73 T.P. 24

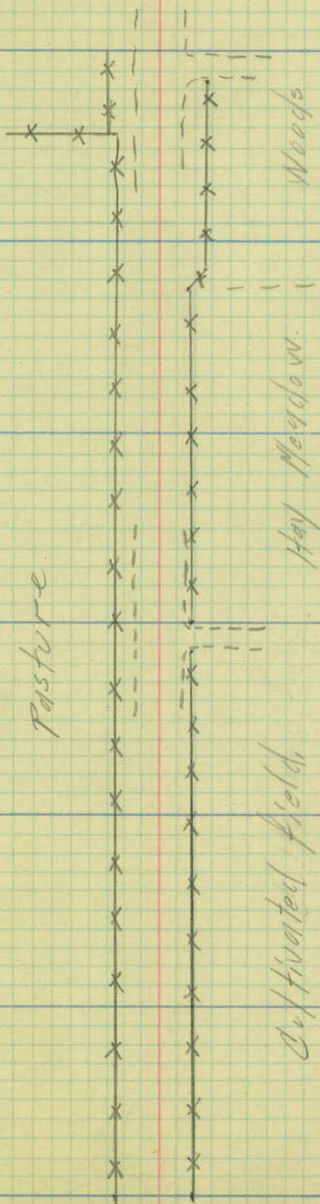
21-10
51-12

+50 T.P. 24'

F. 26'

+17 T.P. 26'

+14 T.P. 26
+14 T.P. 19
F. 25



+90 Farm E. 26'

+84 F.C. 27'

+48 G. 13/c 18
+48 T.P. 13

+85 F. 26
+76 F. 16

+26 T.P. 13

21-9
31-12

+100 T.P. 14
+93 F. E. 26'

+73 T.P. 16

F. 18

+47 T.P. 14

23

22

21

20

19

18

17

1/20/28

F. 27

+13 T.P. 26
F. 28

+87 T.P. 25
+87 F. Cor. 27
+77 Field Ent.
+67 F. Cor. 33

+53 T.P. 30
+53 T.P. 23

+28 T.P. 24
F. 32

Woods

Pasture

Pasture

+74 F. Cor. 27

+65 T.P. 14

F. 27

+32 T.P. 15

F. 27

+47 F. 35

+11 T.P. 23

Pasture

Wood

+94 T.P. 23

+77 T.P. 22

29

28

27

26

25

24

23

1/20/26

C.L. 10
S.L. 12

C.L. 9
S.L. 12

+62 T.P. 24

+55 Farm Ent.
+55 Side Drain 19
12" x 16 C.M.
Fair Cond.

+60 Cross Drain
12" x 55 C.M. Fair Cond.
Extends 27 L. & 28 R.
Drains 17.
+50 T.P. 26

+33 Field Ent.

C.L. 7
S.L. 12
+97 Shed 32.5
+87 Shed 31

+50 F. Cor. 29

+20 T.P. 31
+20 T.P. 24

+78 T.P. 24

+45 T.P. 24

+44 T.P. 18

Pot
Hole.

+29 T.P. 18

C.L. - 9
S.L. - 12

+29 F. Cor. 28
+22 T.P. 17

+99 T.P. 17

+88 Cross Drain
12" x 56 Fair Cond.
Extends 29 L. & 28 R.
Drains 17.
+82 T.P. 17

Woods.

pasture.



36

35

34

33

32

31

30

29

1729/2

498 T. P. 15

104 T.P. 26

468 T.P. 18
469 P.P. 28

467 P.P. 28

784 T. P. 26

440 T.P. 19'

f30 p.p. 29

707 T.P. 44

750 T.P. 31
750 T.P. 24

+50 T.P. 29

f10 T.P. 18

+33 Farm Ent.

+80 P.P. 27

764 Farm Ent

+43 Mail Box 12

f19 T.P. 26'

490 T.P. 19

+ 90 T.R. 24.

471 T.P. 18

2

42

41

40

39

38

37

36

1/29/26

+176 T.P. 29

+36 Cross Drain
96" X 51 C.M. Fair Con.
Extends 26' & 25' ft.
Origins Pt.
6' X 1/2" Head Wall 25
+33 F.C.O. 29

Cultivated Field

X
X
X
X

Cultivated Field

+14 T.P. 31

+33 T.P. 27

+09 T.P. 21

+44 Arterial
Stop Sign 17

+27 T.P. 28

+22 Rd. Sign 31

+29 T.P. 21

+57 Rd. Sign 25

+53 Co. Rd. Sign 21

Nor. 10' & 10' 10' 10'

+52 F.C.O. 52

+47 T.P. 27

+78⁷² T.H. #1
24 Black Top Pav.

+12 T.P. 20
+10 T.P. 26

+51 T.P. 27

+24 F.C.O. 33

G.L. 10
S.L. 12

+98 Arterial Sign 12

+54 Cross Drain

12' X 47 C.M.

Extends 25' & 22' ft.

Origins Pt.
+27 T.P. 19

G.L. 9
S.L. 11

+36 T.P. 27

+88 P.P. 24

48

47

46

45

44

43

42

1/29/26

+90 F. Cor. 36'

+15 Cross F. 36

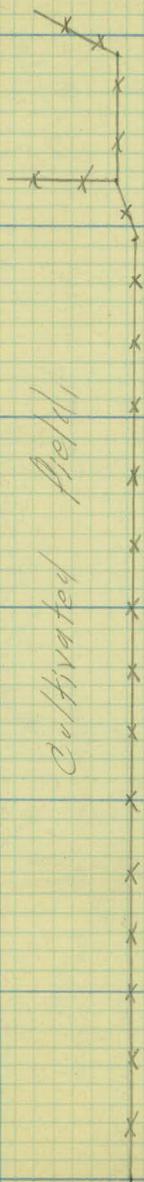
+91 T.P. 27
+92 F. 27

+59 T.P. 27

+32 T.P. 27

+10 T.P. 27

F 29



+54 T.P. 23

+30 T.P. 21

+96 T.P. 21

+76 T.P. 22

+42 T.P. 21

54

53

52

51

50

49

48

1/29/26

F. 24
+99 T.P. 24

+42 T.P. 25

G.L. 12
S.L. 14

G.L. - 8
S.L. - 10
F. 24
+76 T.P. 24

+17 T.P. 25

Cultivated field.

Cultivated field.

+76 T.P. 25

+46 T.P. 26

+20 T.P. 23

+47 T.P. 25

G.L. - 13
S.L. - 14

G.L. 8
S.L. 10
+90 T.P. 23

+17 T.P. 26

+11 Cor. 35 Paving
18' x 18' C.P. Pavement
Extending 24' x 24' to
Pranks St.

5' x 5' x 12" Conc.
Heat Wall At. & R.

+21 Floor 23

40

59

58

57

56

55

54

1/27/20

C.L. 11
S.L. 13

+98 Cross Drain
12" x 40' C.N. Pipe Road
to N.P. 10' L.B. 20' R.

+36 T.P. 32

+59 T.P. 40
+55 F. 41

+46 F.Cor. 20

+90 F.Cor. 17
+91 25 Wing Wall 19'

+75² Abut. 10'

+45² Abut. 10'
+35 Wing Wall 22'

+36 F.Cor. 21

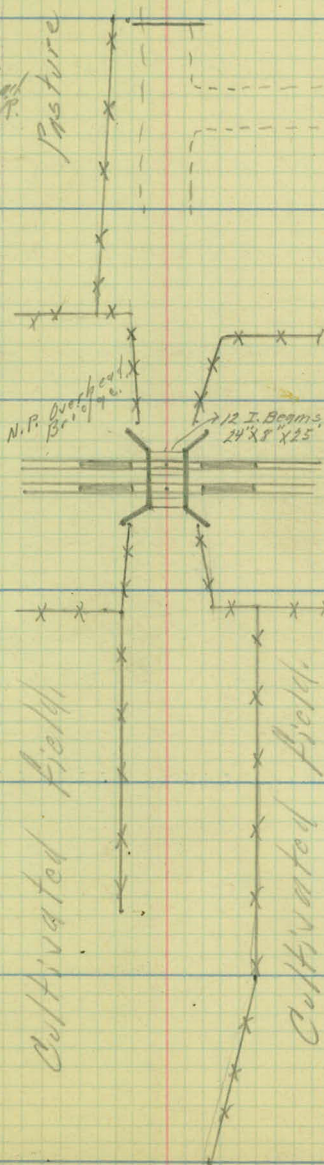
+90 F.Cor. 27

+24 T.P. 32

+95 T.P. 27
+95 F. 27

+34 F.Cor. 27

+67 T.P. 25



C.L. 9
S.L. 12

+59² Side Rd.

+33 T.P. 24

+33 F.Cor. 31

+09 T.P. 12

+80 F.Cor. 18
+80² Wing Wall 24'

+75² Abut. 10'

+45² Abut. 10'
+35 Wing Wall 22'

+36 F.Cor. 18

+92 F.Cor. 25

+90 T.P. 22

+77 Sign 17

+98 T.P. 26

+05 T.P. 24

F. 50

Pasture

Cultivated Field

Cultivated Field

66

65

64

63

62

61

60

1/29/20

Q.L. - 10.
S.L. - 12.
+90 T.P. 30

R.L. - 10
S.L. - 12

+18 12" T-24'

+62 F.C. 31

+59 T.P. 28

F. 30

+41 T.P. 30

+27 T.P. 28

+74 Cross Drain
12" X 51' C.M.
Extends 24' L. & 27' R.

+28 T.P. 30

+06 T.P. 27

F. 31

+96 T.P. 30

Pasture

Cultivated
1/18/20

F. 30

+62 T.P. 30

+75 T.P. 26

Hay Meadow

+51 T.P. 29

72

71

70

69

68

67

66

1/29/26

+95 T.P. 30'
+82 Mail Box 13

+50 F. Ent.

+10 T.P. 30

+69 T.P. 29

+85 T.P. 17
+85 T.P. 32

cultivated field.

cultivated field.

+46 T.P. 29

+52 T.P. 32

+08 T.P. 28

+25 T.P. 21

+89 Mail Box 14
+71 F. Ent.

+86 T.P. 29

78

77

76

75

74

73

72

1/29/34

+50 T.P.31

+10 T.P.31

+33 T.P.31

Cultivated field

Cultivated field

+76 T.P.31

+43 T.P.30
G.L. - 10
S.L. - 12

G.L. 9
S.L. 12

+57 T.P.31

+15 Mail Box 22

+20 Farm Rd.

+68 T.P.31

+21 T.P.34
+21 T.P.28

+47 T.P.31 — — —

84

83

82

81

80

79

78

1/27/36

+71 T.P. 27
+71 T.P. 32

F. 32

+52 T.P. 32

+69 F.C. 30
+69 T.P. 30

+31 F.C. 32
+31 T.P. 32

G.L. 10
S.L. 12

G.L. 10
S.L. 12

+36 T.P. 29

F. 29

Woods

Cultivated field

+96 T.P. 31

+06 T.P. 31

+70 T.P. 31

+40 F.C. 33

+81 T.P. 31

+55 T.P. 31

90

89

88

87

86

85

84

1/29/26

F. 28

+37 T.P. 28

+07 T.P. 30

+75 T. P. 30

+99 F. Cor. 33

+33 T.P. 30

+69 F. Ent

Cultivated field

Swamp

Cultivated field

+62 C.F.

+58 Cross prairie
30" x 51 1/2" Land Exp.
Extends 27 L. & 24 R.
prairie N.

+66 T.P. 32

+36 T.P. 32

+01 C.F. 32

+99 T.P. 35
+99 T.P. 29

+71 T.P. 32

Cultivated field

96

95

94

93

92

91

90

1/30/22

+44 F. 26
+46 T.P. 25

+41 T.P. 24

F. 27

+16 T.P. 27

F. 28
S.L. 10
S.L. 12
+86 T.P. 28

S.L. 11
S.L. 13
F. 28
+63 T.P. 28

Cultivated field.

Cultivated field

+69 C.F. 34

+14 T.P. 32

+88 T.P. 32

+64 T.P. 32

S.L. 10
S.L. 12
F. 32

+52 T.P. 32

S.L. 10
S.L. 12
F. 32

+02 T.P. 32

Swamp

102

101

100

99

98

97

96

1/30/26

F. 25

+85 T.P. 33

+84 T.P. 25

Swamp

+76 T.P. 33

F. 22
G.L. - 10
S.L. - 13

F. 33
G.L. - 10
S.L. - 12

+66 T.P. 33

+48 T.P. 24

F. 24

F. 32

Cultivated Field

Cultivated Field

+17 T.P. 25

+53 F. 32
+55 T.P. 32

F. 50

+54 T.P. 33

F. 48

+86 T.P. 17
+86 T.P. 21

+54 T.P. 35
+54 T.P. 30

108

107

106

105

104

103

102

1/30/24

F. 26

+69 P.P. 26

+91 P.P. 26
+84 P.C. 23
+83 T.P. 23

+27 P.P. 24
+24 P.C. 25

+81 Co. 136 27

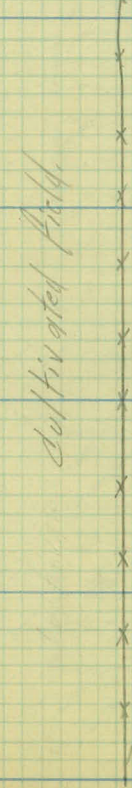
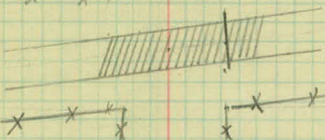
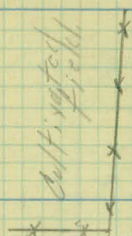
+45 T.P. 24

+67 T.P. 25

C.L. 9
S.L. 11

+34 T.P. 25

+11 T.P. 25



+92 T.P. 31

+90 Mail Box 18
+94 T.P. 31
+86 T.P. 42
+36 Co. 136 24
Direction Sign
+27 P.C. 31

+27 T.P. 31
+12 Arterial Stop
Sign 14 ft.

105+57 Side Drain 32 ft.
24" X 40" Conc. C.C. 14

+18 T.P. 32

+07 T.P. 33

C.L. 11
S.L. 13

+95 T.P. 33

+04 Cross Drain
18" X 40" C.M.
Extends 30' & 20'

114

113

112

111

110

109

108

1/30/26

768 P.P. 25

Cultivated field

767 P.P. 26

766 F. Cor. 27

Q.L. 9
S.L. 12

769 P.P. 26

789 Mail 130 x 12
771 P.P. 26

772 P.P. 26

Pasture

790 C.F. 27

771 P.P. 26

Cultivated field

783 T.P. 30

Q.L. 10
S.L. 12

755 T.P. 24
756 Guy P.O. 31

752 T.P. 30

760 F. Kent.

705 T.P. 32

Farmer's yard

120

119

118

117

116

115

114

1/30/29

f70 P.P. 26

468 P. P. 26

C.L. 10
S.L. 12

468 P. P. 26

468 P.P. 24

PL9 P.P. 26

767 P.R. 26

Cultivated Field

Cultivated field

Per 5/11/2.

Cultivated 4/10/4

f. 27 p. 28
F. 29

2.6.10
 5.6.12
 +73 C.F. 29
 +73 T.P. 29

+39 T.P. 30

454 F. Cor. 31

422 T. P. 30

118 T. P. 31

126

125

124

123

122

121

120

1/30/20

+65 P.P. 24

X
X
X X X
X

+57 C.F. 27

+35 T.P. 27

+69 P.P. 24

X
X
X

+69 P.P. 24

Cultivated field

X
X
X
X

+08 T.P. 27
F. 28

+69 P.P. 24

X
X

+85 T.P. 27

~~4.1.12~~
~~5.1.15~~

+71 P.P. 24

X
X

C.L. 16
S.L. 12

+54 T.P. 27

+67 P.P. 24

X
X
X
X

+30 T.P. 17
+30 T.P. 27

132

131

130

129

128

127

124

1/30/26

+66 P.P. 24

+65 P.P. 24

+62 P.P. 24

+64 Nail Box 12

+67 T.P. 24

+69 P.P. 24

+69 P.P. 24

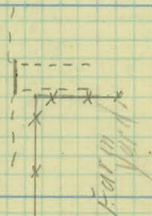


+64 C.F. 22
+64 T.P. 22

+68 T.P. 24

+35 F. Cor. 24
+30 Mill Stairs 12
+08 T.P. 24

Cultivated field



+61 Farm Ent.
+61 Side Drain 15
+12 Kiln 19. Fair Cor.
+50 F. Cor. 45

+78 T.P. 33
+78 T.P. 25
+66 C.F. 25

Cultivated field

+56 T.P. 25

138

137

136

135

134

133

132

1/30/26

F 22

+66 P.P. 26

+65 P.P. 26

B.L. 10
S.L. 13

+64 P.P. 26

+65 P.P. 26

+64 P.P. 26

+81 P.P. 26

+65 P.P. 26

+89 Mail Box 12

+10 Farm Rd

Cultivated field

Poplar

orchard

+82 T.P. 21

+12 Cross Drain
18" x 41' C.M.
Extends 23 L. & 18 R.
Good Cond

C.L. 10
S.L. 12

+53 T.P. 25

+58 T.P. 17

+18 T.P. 22

F 23

+92 T.P. 23

+72 Field. Ent

Cultivated field

144

143

142

141

140

139

138

1/30/26

F. 27

+68 P.P. 26

+66 P.P. 26

+67 P.P. 26

F. 27

+65 P.P. 26

+66 P.P. 26

C.L. 18
S.L. 14

+64 P.P. 26

+57 F.O.R. 27

Cultivated Field

Cultivated Field

+22 T.P. 20

+97 T.P. 20

+72 T.P. 20

+41 T.P. 20

C.L. 8
S.L. 11

+57 F. Cor. 20

+12 T.P. 20

150

149

148

147

146

145

144

1/30/24

+66 P.P. 26

+66 T.P. 20

+68 P.P. 26

+35 T.P. 20

G.L. - 12
S.L. - 13

G.L. 8
S.L. 11

+67 P.P. 26

+13 T.P. 21

+62 P.P. 24

+95 Farm Ent.

+79 T.P. 21

+63 F.C. 24
+63 P.P. 24

+64 Mail Box 14

+65 P.P. 24

+50 T.P. 18
+50 T.P. 13

Cultivated field

Cultivated field

x
x
x
x
x
x

154

155

154

153

152

151

150

1/30/26

G.L. 11
S.L. 14

G.L. 8
S.L. 11
F. 21

+68 P.P. 24

+22 T.P. 10

+68 P.P. 24

+32 T.P. 10

+67 P.P. 24

+44 T.P. 22
+44 T.P. 17

+66 P.P. 24

+26 T.P. 10

+67 P.P. 24

+91 F. Cor. 21

+52 Farm Ref.

G.L. - 10
S.L. - 13

G.L. 8
S.L. 11
+95 T.P. 20

+68 P.P. 24

Cultivated field

Cultivated field

162

161

160

159

158

157

154

1/30/22

+66 P.P. 24

+54 T.P. 20

+68 P.P. 24

+66 T.P. 19
+66 T.P. 23

+70 P.P. 24

+74 T.P. 20

+68 P.P. 24

+83 T.P. 20
+83 F. Cor. 21

+68 P.P. 24

+93 T.P. 20

+70 P.P. 24

+02 T.P. 20

+11 T.P. 20

Cultivated field

Cultivated field

x
x
x
x
x
x
x
x
x
x
x

168

167

166

165

164

163

162

1/30/20

G.L. 10
S.L. 12
+66 P.P. 23

F 22'
G.L. 10
S.L. 12
+78 T.P. 24
+78 T.P. 18

+71 P.P. 24

+90 T.P. 20

+70 P.P. 24

+93 T.P. 20

+67 P.P. 24

+05 F. Cor. 20
+05 T.P. 20

+69 P.P. 24

+10 T.P. 20

+69 P.P. 24

+03 F. Cor. 20
+26 T.P. 20

+41 T.P. 20

Cultivated field

Cultivated field

Cultivated field

174

173

172

171

170

169

148

2/1/26

F. 24

F. 17

+87 P.P. 26

+14 T.P. 22

+86 P.P. 26

Payser e.

+25 T.P. 22

A.L. 10
S.L. 12

A.L. 10
S.L. 11

+68 P.P. 25

Swamp

+36 C.F. 24
+36 T.P. 21

+64 P.P. 25

Swamp

+46 T.P. 22

+77 P.Cor. 25

+70 P.P. 25

Cultivated field

+58 T.P. 21

+69 P.P. 24

Cultivated field

+70 T.P. 21

180

179

178

177

176

175

174

2/1/26

F. 25

+86 P.P. 25

+82 F.C. 25
+83 F.C. 25
+83 C.F. 25
+83 P.P. 25
+83 F.C. 25
+83 F.C. 25
+83 F.C. 25

+84 P.P. 25

+86 P.P. 26

+85 P.P. 26

+85 P.P. 26
+85 C.F. 26

Cultivated
field

Swamp

Pasture

Cultivated field

Orchard

Farm
yard

Farm
yard

Swamp

F. 36

+17 T.P. 23
F. 35

+82 C.F. 30

+82 T.P. 23

+84 F.C. 26
+80 T.P. 22

+15 Farm Est
+87 F.C. 27

+84 T.P. 22

+88 C.F. 27
F. 24

+84 T.P. 19
+87 T.P. 25

+82 T.P. 22

184

185

144

183

182

181

180

2/1/26

F. 27

F. 26

+84 P.P. 26

+48 T.P. 23

+85 P.P. 26
+63 P.P. 26

+55 Field/Ent

+24 T.P. 25

+80 P.P. 26

+09 O.F. 27

+02 T.P. 26
+00 T.P. 20

+83 P.P. 24

G.L. 10
S.L. 11

+72 T.P. 23

G.L. 9
S.L. 11

+81 P.P. 24

+71 Goes Drain
18 X 7 1/2 ft. Fair Cond.
Extends 38 ft. S 27 E
prains Lt.

+86 P.P. 24

+38 T.P. 22

Cultivated field

Cultivated field

Small trees

192

191

190

189

188

187

184

4/1/26

E. Co. Line Road

+23 Co. Rd. Sign 26
Marker & Direction
+22 Iron M. Sign 24
+21 F. Co. Rd.

+85 F. 41
+55 F. 26
+55 P.P. 26

+48 T.P. 22

+88 T.P. 24

+35 T.P. 26

+86 P.P. 24

+08 T.P. 23

+86 P.P. 24

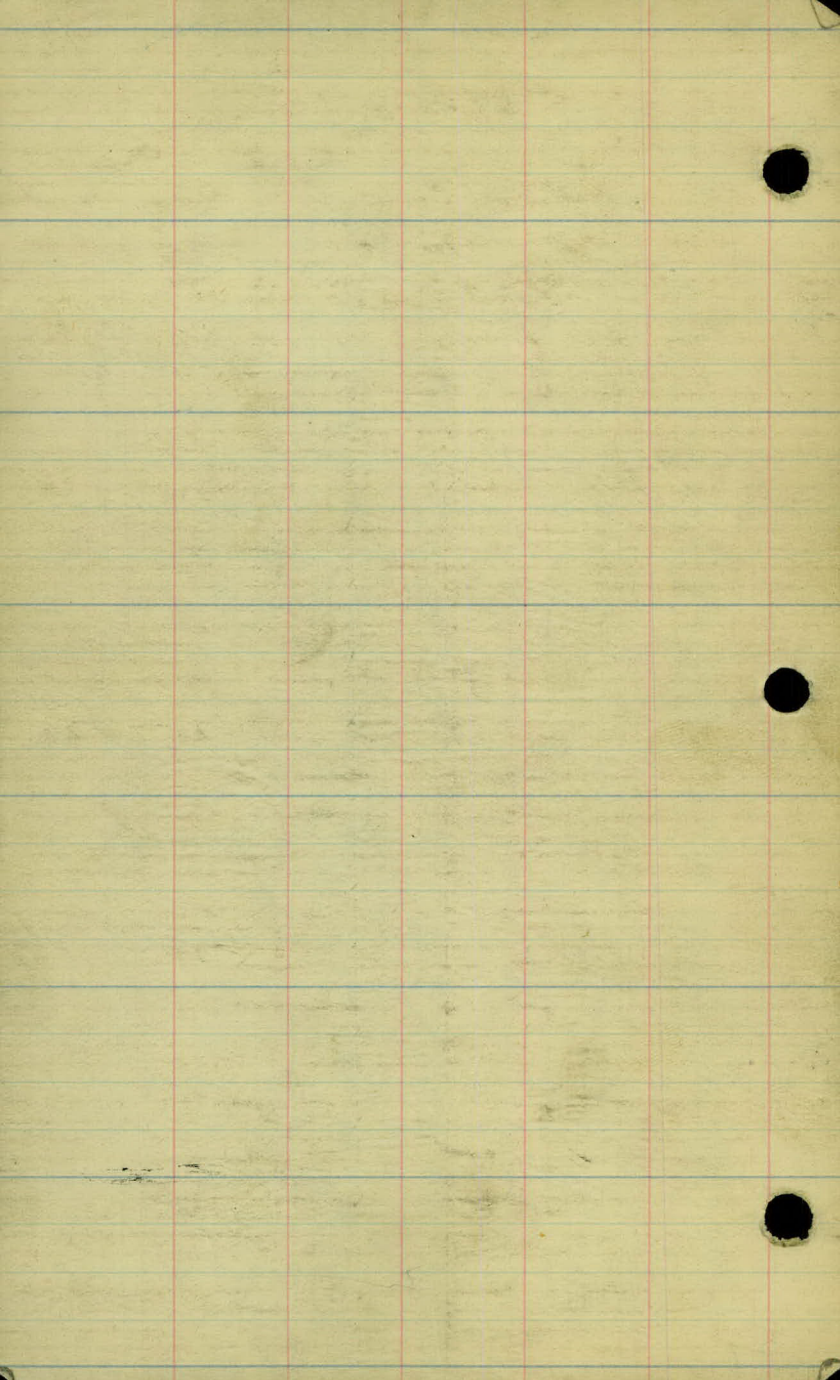
+82 P.P. 14

+83 T.P. 23

Cultivated Field

Cultivated Field

Small Trees



X sections

Co. Rd. "D"

Rd 9/6 No 53

Sta.	+	H. I.	-	Red.	Elev.
B.M.	3.98	930.08		926.10	
0+10				5.3	24.78

0+00				4.9	25.18
------	--	--	--	-----	-------

0+00	-	Q. La. Bore Rd.		4.9	25.18
------	---	-----------------	--	-----	-------

+30					25.28
-----	--	--	--	--	-------

1+00					24.38
------	--	--	--	--	-------

2+00					23.18
------	--	--	--	--	-------

+55					22.28
-----	--	--	--	--	-------

3+00					21.58
------	--	--	--	--	-------

	5.88	927.34	8.62	921.46	
--	------	--------	------	--------	--

+30					21.34
-----	--	--	--	--	-------

+	Cross prain				
---	-------------	--	--	--	--

4+00					20.94
------	--	--	--	--	-------

5+00					23.14
------	--	--	--	--	-------

+44					24.54
	6.82	931.34	2.82	924.52	

6/2/26

Spk. in Coy Pale 17' Mt. Stg. 0-25.

$\frac{5.8}{33}$	$\frac{5.6}{22}$	5.3	$\frac{4.8}{24}$	$\frac{5.2}{46}$
------------------	------------------	-----	------------------	------------------

$\frac{5.4}{33}$	$\frac{5.4}{20}$	4.9	$\frac{5.0}{23}$	$\frac{5.6}{33}$
------------------	------------------	-----	------------------	------------------

$\frac{4.6}{100}$	$\frac{4.8}{50}$	4.9	$\frac{4.7}{50}$	$\frac{4.5}{100}$
-------------------	------------------	-----	------------------	-------------------

$\frac{5.7}{33}$	$\frac{5.7}{22}$	4.8	$\frac{5.5}{15}$	$\frac{5.3}{22}$	$\frac{4.2}{30}$	$\frac{4.7}{33}$
------------------	------------------	-----	------------------	------------------	------------------	------------------

$\frac{5.2}{33}$	$\frac{5.9}{15}$	$\frac{6.3}{12}$	5.7	$\frac{6.3}{12}$	$\frac{6.8}{33}$
------------------	------------------	------------------	-----	------------------	------------------

$\frac{5.9}{33}$	$\frac{7.5}{24}$	$\frac{9.4}{17}$	$\frac{7.7}{13}$	$\frac{7.3}{7}$	4.9	$\frac{7.4}{14}$	$\frac{8.8}{17}$	$\frac{10.0}{33}$
------------------	------------------	------------------	------------------	-----------------	-----	------------------	------------------	-------------------

$\frac{6.3}{33}$	$\frac{6.7}{24}$	$\frac{9.2}{19}$	$\frac{9.7}{14}$	$\frac{8.4}{12}$	7.8	$\frac{8.6}{13}$	$\frac{9.9}{20}$	$\frac{10.1}{33}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	-------------------

$\frac{10.2}{33}$	$\frac{10.8}{23}$	$\frac{11.9}{17}$	$\frac{11.9}{15}$	$\frac{9.2}{10}$	8.5	$\frac{9.1}{13}$	$\frac{11.7}{17}$	$\frac{12.7}{33}$
-------------------	-------------------	-------------------	-------------------	------------------	-----	------------------	-------------------	-------------------

$\frac{10.6}{33}$	$\frac{11.1}{17}$	$\frac{6.7}{10}$	6.0	$\frac{6.6}{12}$	$\frac{12.0}{21}$	$\frac{12.8}{33}$
-------------------	-------------------	------------------	-----	------------------	-------------------	-------------------

12.4 = Invert.14.4 = Out let.

$\frac{11.5}{33}$	$\frac{11.5}{18}$	$\frac{7.2}{11}$	6.4	$\frac{7.5}{14}$	$\frac{13.4}{23}$	$\frac{13.8}{33}$
-------------------	-------------------	------------------	-----	------------------	-------------------	-------------------

$\frac{8.1}{33}$	$\frac{8.3}{26}$	$\frac{9.2}{17}$	$\frac{5.1}{11}$	4.2	$\frac{5.1}{12}$	$\frac{14.1}{24}$	$\frac{15.2}{33}$
------------------	------------------	------------------	------------------	-----	------------------	-------------------	-------------------

$\frac{3.5}{33}$	$\frac{3.1}{24}$	$\frac{5.1}{18}$	$\frac{5.1}{15}$	$\frac{3.8}{12}$	2.8	$\frac{3.7}{12}$	$\frac{6.6}{18}$	$\frac{8.1}{33}$
------------------	------------------	------------------	------------------	------------------	-----	------------------	------------------	------------------

Sta.	+	H. I.	-	Red.	Elev.
6+00		731.34			25.24
+75					26.54
7+00					26.84
+18					26.84
8+00					26.64
+40					26.54
9+00					26.14 ✓
10+00					25.64
+72					26.24
11+00					26.64
+50					27.64
11.15		✓ 739.78	2.71	✓ 728.63	
12+00					29.08
+45					34.68

6/2/26

$\begin{array}{r} 27. \\ 3.6 \quad 3.6 \quad 4.0 \quad 7.3 \quad 7.3 \\ 33 \quad 27 \quad 19 \quad 14 \quad 13 \end{array}$
 $\begin{array}{r} RT. \\ 6.7 \quad 7.0 \quad 6.4 \quad 7.6 \\ 7 \quad 13 \quad 17 \quad 33 \end{array}$

Above H.I.

$\begin{array}{r} 72.8 \quad 72.2 \quad 5.1 \quad 6.0 \\ 33 \quad 29 \quad 21 \quad 14 \end{array}$
 $\begin{array}{r} 5.9 \quad 1.8 \quad 3.1 \\ 15 \quad 21 \quad 33 \end{array}$

$\begin{array}{r} 71.7 \quad 71.0 \quad 5.5 \quad 5.3 \\ 33 \quad 28 \quad 19 \quad 13 \end{array}$
 $\begin{array}{r} 5.3 \quad 5.0 \quad 2.7 \quad 3.3 \\ 13 \quad 17 \quad 21 \quad 33 \end{array}$

$\begin{array}{r} 70.5 \quad 0.2 \quad 5.4 \quad 5.5 \\ 33 \quad 24 \quad 19 \quad 14 \end{array}$
 $\begin{array}{r} 5.2 \quad 5.0 \\ 13 \quad 33 \end{array}$

$\begin{array}{r} 71.4 \quad 71.5 \quad 5.8 \quad 5.4 \\ 33 \quad 20 \quad 15 \quad 12 \end{array}$
 $\begin{array}{r} 5.3 \quad 6.0 \quad 4.1 \quad 4.9 \\ 10 \quad 15 \quad 18 \quad 33 \end{array}$

$\begin{array}{r} 72.5 \quad 3.1 \quad 5.5 \quad 5.4 \\ 33 \quad 18 \quad 13 \quad 8 \end{array}$
 $\begin{array}{r} 5.4 \quad 6.1 \quad 7.1 \\ 12 \quad 20 \quad 33 \end{array}$

$\begin{array}{r} 72.5 \quad 7.8 \quad 5.9 \\ 33 \quad 17 \quad 12 \end{array}$
 $\begin{array}{r} 5.9 \quad 8.7 \quad 9.7 \\ 12 \quad 20 \quad 33 \end{array}$

$\begin{array}{r} 70.7 \quad 70.3 \quad 6.6 \\ 33 \quad 20 \quad 13 \end{array}$
 $\begin{array}{r} 6.4 \quad 12.6 \quad 13.1 \\ 12 \quad 22 \quad 33 \end{array}$

$\begin{array}{r} 70.4 \quad 71.0 \quad 9.6 \quad 5.9 \\ 33 \quad 27 \quad 18 \quad 12 \end{array}$
 $\begin{array}{r} 5.8 \quad 10.4 \quad 9.9 \\ 12 \quad 19 \quad 33 \end{array}$

$\begin{array}{r} 5.8 \quad 6.7 \quad 6.6 \quad 5.4 \\ 33 \quad 28 \quad 16 \quad 11 \end{array}$
 $\begin{array}{r} 5.3 \quad 6.8 \quad 6.8 \\ 12 \quad 15 \quad 33 \end{array}$

Above H.I.

Above H.I.

$\begin{array}{r} 72.1 \quad 2.9 \quad 3.6 \quad 4.7 \\ 33 \quad 24 \quad 17 \quad 14 \end{array}$
 $\begin{array}{r} 4.4 \quad 5.5 \quad 4.5 \quad 7.0 \quad 7.9 \\ 10 \quad 17 \quad 21 \quad 28 \quad 33 \end{array}$

$\begin{array}{r} 3.2 \quad 3.2 \quad 9.5 \quad 10.7 \quad 11.6 \\ 35 \quad 33 \quad 25 \quad 19 \quad 13 \end{array}$
 $\begin{array}{r} 11.5 \quad 12.3 \quad 11.1 \quad 2.4 \quad 3.5 \\ 13 \quad 15 \quad 21 \quad 30 \quad 33 \end{array}$

$\begin{array}{r} 7.3 \quad 7.3 \quad 7.1 \quad 10.0 \\ 33 \quad 30 \quad 20 \quad 14 \end{array}$
 $\begin{array}{r} 9.6 \quad 10.2 \quad 10.0 \quad 3.6 \quad 4.4 \\ 11 \quad 14 \quad 17 \quad 25 \quad 33 \end{array}$

Sta.	+	H.I.	-	Red.	Elev.
		939.78			
13+00				8.5	31.28
+50				7.2	32.58
14+00				6.3	33.48
B.M.	3.82	939.76	3.82	935.96	935.94
+40				5.5	34.26
+80				4.5	35.26
15+00				4.0	35.76
T. P.	7.52	947.73	1.55	938.21	
+50				10.4	37.13
16+00				9.3	38.43
+55					40.43
17+00					41.43
+40					42.13
18+00					43.33
+50					43.63

6/2/26

RT.

$\frac{12.0}{33}$ $\frac{12.0}{29}$ $\frac{9.4}{15}$ 8.5 $\frac{9.0}{13}$ $\frac{9.2}{14}$ $\frac{5.8}{21}$ $\frac{6.3}{33}$

$\frac{14.7}{33}$ $\frac{14.7}{28}$ $\frac{12.4}{19}$ $\frac{8.2}{12}$ 7.2 $\frac{7.7}{10}$ $\frac{8.3}{19}$ $\frac{8.2}{33}$

$\frac{11.0}{33}$ $\frac{11.4}{29}$ $\frac{9.2}{14}$ $\frac{7.0}{10}$ 6.3 $\frac{7.1}{13}$ $\frac{8.5}{19}$ $\frac{9.3}{33}$

Sp. N. in T. 12 28 21. 54 14 150.

$\frac{6.2}{33}$ $\frac{6.2}{28}$ $\frac{6.6}{20}$ $\frac{6.0}{11}$ 5.5 $\frac{6.3}{12}$ $\frac{9.2}{18}$ $\frac{11.0}{33}$

$\frac{1.9}{33}$ $\frac{3.3}{29}$ $\frac{4.3}{18}$ $\frac{5.5}{15}$ $\frac{5.0}{10}$ 4.5 $\frac{5.1}{12}$ $\frac{8.0}{19}$ $\frac{9.3}{33}$

$\frac{4.1}{33}$ $\frac{4.7}{28}$ $\frac{5.0}{14}$ $\frac{4.4}{11}$ 4.0 $\frac{4.6}{10}$ $\frac{8.9}{19}$ $\frac{9.8}{33}$

$\frac{14.6}{33}$ $\frac{14.5}{17}$ $\frac{11.5}{12}$ 10.6 $\frac{11.4}{10}$ $\frac{17.0}{22}$ $\frac{18.5}{33}$

$\frac{10.1}{33}$ $\frac{10.2}{19}$ $\frac{10.9}{13}$ $\frac{9.9}{11}$ 9.3 $\frac{10.0}{10}$ $\frac{10.8}{15}$ $\frac{11.4}{33}$

$\frac{6.5}{33}$ $\frac{6.1}{17}$ $\frac{8.0}{15}$ 7.3 $\frac{7.7}{9}$ $\frac{8.1}{15}$ $\frac{4.4}{18}$ $\frac{4.3}{33}$

$\frac{11.8}{33}$ $\frac{7.9}{20}$ $\frac{7.7}{14}$ $\frac{6.9}{11}$ 6.3 $\frac{6.7}{17}$ $\frac{5.9}{19}$ $\frac{4.9}{33}$

$\frac{9.0}{33}$ $\frac{6.8}{27}$ $\frac{4.0}{19}$ $\frac{7.0}{15}$ $\frac{6.3}{11}$ 5.4 $\frac{6.1}{11}$ $\frac{6.3}{18}$ $\frac{4.8}{20}$ $\frac{5.9}{26}$ $\frac{1.8}{18}$ $\frac{1.7}{33}$
Above H.I. Above H.I.

$\frac{+0.6}{33}$ $\frac{+1.6}{30}$ $\frac{+2.5}{23}$ $\frac{5.2}{15}$ $\frac{5.1}{10}$ 4.4 $\frac{5.3}{13}$ $\frac{4.3}{23}$ $\frac{+2.5}{36}$ $\frac{+8.7}{38}$ $\frac{+10.2}{42}$
Above H.I. Above H.I.

$\frac{0.6}{33}$ $\frac{0.2}{32}$ $\frac{+1.0}{22}$ $\frac{4.3}{17}$ $\frac{4.9}{13}$ 4.1 $\frac{4.8}{13}$ $\frac{6.4}{17}$ $\frac{4.9}{28}$ $\frac{0.2}{36}$ $\frac{+0.9}{47}$ $\frac{+14.6}{51}$ $\frac{+15.4}{57}$

Sta.	+	H.I.	-	Red.	Elev
		747.73			
19+00				5.3	42.43
+50				7.1	40.63
20+00				7.4	38.13
+67				12.7	35.03
	0.65	936.22	12.14	935.57	
21					33.32
+60					30.42
22					28.62
23					24.02
	0.55	924.70	12.07	924.15	
+	Cross Drain.				
24					19.80
+60					17.20
25					15.30
+45					13.30

6/3/26

Above H.I.

$\frac{5.8}{33} \quad \frac{1.6}{22} \quad \frac{6.5}{15} \quad \frac{5.9}{12} \quad \frac{6.6}{15} \quad \frac{5.0}{26} \quad \frac{0.0}{35} \quad \frac{+13.5}{50} \quad \frac{+12.5}{52} \quad \frac{+12.0}{59}$
 Above H.I.

Above H.I.

$\frac{1.4}{33} \quad \frac{+0.3}{25} \quad \frac{5.7}{19} \quad \frac{7.8}{13} \quad \frac{8.0}{71} \quad \frac{7.1}{14} \quad \frac{1.0}{23} \quad \frac{+7.5}{32} \quad \frac{+19.0}{45} \quad \frac{+20.5}{51} \quad \frac{+20.5}{60}$
 Above H.I.

$\frac{0.8}{33} \quad \frac{0.2}{27} \quad \frac{9.8}{18} \quad \frac{10.3}{12} \quad \frac{9.4}{7.4} \quad \frac{10.5}{13} \quad \frac{8.3}{24} \quad \frac{+11.4}{48} \quad \frac{+12.5}{55}$

$\frac{10.4}{33} \quad \frac{7.8}{23} \quad \frac{13.1}{18} \quad \frac{13.2}{10} \quad \frac{12.7}{12.7} \quad \frac{13.3}{11} \quad \frac{13.4}{18} \quad \frac{7.4}{29} \quad \frac{6.7}{33}$
 Above H.I.

$\frac{0.0}{33} \quad \frac{+0.8}{21} \quad \frac{3.3}{16} \quad \frac{3.7}{13} \quad \frac{2.9}{2.9} \quad \frac{3.8}{10} \quad \frac{3.3}{15} \quad \frac{+2.3}{22} \quad \frac{+2.8}{33}$

$\frac{6.7}{33} \quad \frac{6.0}{18} \quad \frac{6.3}{10} \quad \frac{5.8}{5.8} \quad \frac{6.3}{7} \quad \frac{6.1}{15} \quad \frac{6.1}{26} \quad \frac{5.5}{30} \quad \frac{5.1}{33}$

$\frac{12.7}{33} \quad \frac{11.2}{17} \quad \frac{8.3}{12} \quad \frac{9.4}{9.4} \quad \frac{8.2}{8} \quad \frac{8.0}{14} \quad \frac{11.2}{21} \quad \frac{16.6}{34}$

$\frac{18.4}{33} \quad \frac{18.5}{25} \quad \frac{15.2}{19} \quad \frac{12.7}{12} \quad \frac{12.2}{12.2} \quad \frac{12.6}{12} \quad \frac{19.6}{26} \quad \frac{10.8}{33}$

Outlet = 13.7

11.5 = Invert.

$\frac{16.5}{33} \quad \frac{15.1}{29} \quad \frac{13.0}{22} \quad \frac{6.0}{13} \quad \frac{4.7}{4.7} \quad \frac{5.4}{8} \quad \frac{5.0}{13} \quad \frac{8.9}{29} \quad \frac{8.2}{33}$

$\frac{17.0}{33} \quad \frac{16.6}{27} \quad \frac{15.0}{22} \quad \frac{13.0}{18} \quad \frac{8.2}{12} \quad \frac{7.5}{7.5} \quad \frac{8.0}{8} \quad \frac{8.1}{13} \quad \frac{8.8}{15} \quad \frac{5.6}{33}$

$\frac{14.7}{33} \quad \frac{14.2}{20} \quad \frac{7.8}{12} \quad \frac{7.4}{7.4} \quad \frac{10.0}{7} \quad \frac{7.3}{13} \quad \frac{8.2}{14} \quad \frac{6.1}{27} \quad \frac{5.8}{33}$

$\frac{11.4}{33} \quad \frac{12.1}{30} \quad \frac{13.1}{24} \quad \frac{12.8}{17} \quad \frac{12.1}{14} \quad \frac{11.4}{11.4} \quad \frac{11.9}{7} \quad \frac{11.7}{12} \quad \frac{12.6}{15} \quad \frac{10.0}{33}$

Sta.	+	H.I.	-	Red.	Elev.
		924.70			
24					10.70
	0.49	✓ 912.93	12.24	✓ 912.44	
27					06.63
B.M.			4.94	✓ 907.99	907.98
+50					04.43
+60	cross drain.				
28					03.63
29					04.53
+50					05.43
30					06.23
	5.71	✓ 911.72	6.92	✓ 906.01	
+50					06.62
31					07.22
+20					07.32
+25					07.32
32					07.42

6/3/26

$\frac{13.7}{33}$ $\frac{14.3}{29}$ $\frac{15.5}{16}$ $\frac{14.4}{9}$ 14.0 $\frac{14.5}{8}$ $\frac{14.5}{13}$ $\frac{15.9}{17}$ $\frac{15.3}{35}$

$\frac{15.3}{33}$ $\frac{14.6}{24}$ $\frac{6.8}{12}$ 6.3 $\frac{6.7}{13}$ $\frac{13.2}{21}$ $\frac{12.7}{33}$

Spk in 12" Tree 30' Rt. 574. 26 + 38

$\frac{17.3}{33}$ $\frac{15.9}{24}$ $\frac{10.0}{14}$ $\frac{8.7}{9}$ 8.5 $\frac{8.9}{11}$ $\frac{15.2}{21}$ $\frac{15.4}{33}$

Outlet = 18.0
27

$\frac{16.4}{28}$ = Invert.

$\frac{16.6}{35}$ $\frac{15.9}{20}$ $\frac{10.0}{12}$ 9.3 $\frac{9.9}{12}$ $\frac{16.5}{21}$ $\frac{16.2}{33}$

$\frac{11.8}{33}$ $\frac{12.4}{17}$ $\frac{9.2}{11}$ 8.4 $\frac{9.1}{12}$ $\frac{14.6}{21}$ $\frac{14.9}{33}$

$\frac{8.4}{33}$ $\frac{9.6}{14}$ $\frac{8.1}{11}$ 7.5 $\frac{8.2}{10}$ $\frac{10.7}{17}$ $\frac{9.8}{24}$ $\frac{8.2}{33}$

$\frac{2.3}{33}$ $\frac{3.1}{27}$ $\frac{7.9}{19}$ $\frac{8.1}{14}$ $\frac{7.4}{11}$ 6.7 $\frac{9.6}{14}$ $\frac{5.0}{19}$ $\frac{4.6}{28}$ $\frac{3.0}{33}$

$\frac{0.4}{33}$ $\frac{0.5}{28}$ $\frac{6.4}{18}$ $\frac{5.7}{11}$ 5.1 $\frac{5.5}{11}$ $\frac{5.7}{17}$ $\frac{0.3}{25}$ + 2.3
Above H.I.

$\frac{0.6}{33}$ $\frac{0.0}{27}$ $\frac{5.5}{20}$ $\frac{5.1}{12}$ 4.5 $\frac{4.8}{10}$ $\frac{4.7}{17}$ + 2.0 + 3.1
Above H.I.

$\frac{0.5}{33}$ $\frac{0.5}{27}$ $\frac{4.4}{21}$ $\frac{4.7}{11}$ 4.4 $\frac{4.7}{9}$ $\frac{3.7}{17}$ $\frac{0.2}{24}$ + 1.1 + 1.3
Above H.I.

$\frac{3.6}{33}$ $\frac{4.7}{11}$ 4.4 $\frac{4.7}{9}$ $\frac{4.0}{17}$ $\frac{0.0}{24}$ + 1.5
Above H.I.

$\frac{5.2}{33}$ $\frac{5.6}{14}$ $\frac{4.6}{12}$ 4.3 $\frac{4.4}{14}$ $\frac{2.0}{27}$ $\frac{1.5}{33}$

Sta.	+	H.I.	-	Red.	Elev.
33		911.72			06.82

+50					06.82
-----	--	--	--	--	-------

34					06.72
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+50					06.02
-----	--	--	--	--	-------

35					04.82
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+50					03.32
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36	0.67	906.49	10.90	910.82	01.12
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+50					98.59
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37					96.29
----	--	--	--	--	-------

+50					93.59
-----	--	--	--	--	-------

+	Cross Drain				
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38					91.29
----	--	--	--	--	-------

+50					89.29
-----	--	--	--	--	-------

P.M.	8.11	901.44	8.11	893.38	893.33
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6/5/26

$\frac{6.4}{33} \quad \frac{6.6}{15} \quad \frac{5.7}{12} \quad 4.9 \quad \frac{5.3}{12} \quad \frac{5.2}{20} \quad \frac{3.2}{33}$

$\frac{7.6}{33} \quad \frac{6.3}{14} \quad \frac{5.4}{12} \quad 4.9 \quad \frac{5.3}{15} \quad \frac{4.2}{19} \quad \frac{3.8}{33}$

$\frac{6.8}{33} \quad \frac{5.7}{18} \quad \frac{6.4}{14} \quad \frac{5.7}{11} \quad 5.0 \quad \frac{5.6}{15} \quad \frac{2.7}{20} \quad \frac{2.2}{33}$

Above H.I.

$\frac{6.2}{33} \quad \frac{6.2}{27} \quad \frac{5.0}{21} \quad \frac{7.1}{14} \quad \frac{6.2}{10} \quad 5.7 \quad \frac{6.3}{15} \quad \frac{0.0}{24} \quad \frac{+0.5}{33}$

Above H.I.

$\frac{3.6}{33} \quad \frac{2.8}{30} \quad \frac{6.7}{25} \quad \frac{8.2}{14} \quad \frac{7.5}{11} \quad 6.9 \quad \frac{7.3}{7} \quad \frac{7.4}{17} \quad \frac{3.4}{25} \quad \frac{+5.0}{33} \quad \frac{+5.0}{34}$

Above H.I.

$\frac{3.2}{40} \quad \frac{3.2}{34} \quad \frac{8.5}{31} \quad \frac{9.7}{23} \quad \frac{9.8}{14} \quad \frac{7.0}{7} \quad 8.4 \quad \frac{7.2}{14} \quad \frac{5.1}{28} \quad \frac{+8.0}{59} \quad \frac{+8.9}{50}$

$\frac{7.4}{33} \quad \frac{11.6}{30} \quad \frac{12.0}{14} \quad \frac{11.1}{10} \quad 10.4 \quad \frac{11.7}{15} \quad \frac{9.4}{24} \quad \frac{1.9}{32} \quad \frac{1.9}{36}$

$\frac{8.6}{33} \quad \frac{7.2}{24} \quad \frac{3.7}{13} \quad \frac{3.3}{7} \quad 2.9 \quad \frac{3.4}{10} \quad \frac{3.7}{14} \quad \frac{2.1}{20} \quad \frac{1.3}{33}$

$\frac{11.8}{33} \quad \frac{11.5}{22} \quad \frac{6.1}{13} \quad 5.2 \quad \frac{6.0}{13} \quad \frac{9.1}{19} \quad \frac{8.9}{28} \quad \frac{7.9}{33}$

$\frac{11.5}{33} \quad \frac{11.9}{20} \quad \frac{8.5}{13} \quad 7.7 \quad \frac{8.6}{11} \quad \frac{14.8}{23} \quad \frac{15.8}{38}$

12.8

13.7

$\frac{7.8}{33} \quad \frac{9.5}{25} \quad \frac{12.3}{19} \quad \frac{10.6}{14} \quad \frac{10.5}{10} \quad 10.2 \quad \frac{11.0}{14} \quad \frac{11.5}{21} \quad \frac{12.9}{33}$

On Pavement

$\frac{9.6}{33} \quad \frac{9.8}{27} \quad \frac{12.5}{17} \quad 12.2 \quad \frac{13.2}{29} \quad \frac{13.3}{33}$

901.46

+55

89.26

4.38 893.23 12.61 888.85

+64¹ Edge of Pavement 4.40 88.83

+78⁷² 4.22 89.01

+78²² Q. T. H. #1 4.22 89.01

+92 Edge of Pavement 4.40 88.83

39 88.53

+80 87.43

+50 86.73

40 85.53

+50 83.83

3.54 896.03 10.74 882.49

41 82.33

3.54 10.74 882.49

+32 81.63

+ Cross Drain

+40 81.53

on Pavement.

11.4	12.4		13.0	13.2
<u>33</u>	<u>17</u>	12.2	<u>21</u>	<u>33</u>

OUT.

On Pavement

40	40.2		42.2	5.2	5.5
<u>33</u>	<u>22.7</u>	4.22	<u>22.7</u>	<u>30</u>	<u>33</u>

3.10	3.56		5.20	6.18
<u>100</u>	<u>50</u>	4.22	<u>50</u>	<u>100</u>

On Pavement

3.70	4.24		5.1	7.0	7.6
<u>33</u>	<u>13.2</u>	4.7	<u>17</u>	<u>23</u>	<u>33</u>

5.8	5.8		6.3	7.4	7.3	4.2	5.4
<u>33</u>	<u>15</u>	5.8	<u>11</u>	<u>13</u>	<u>14</u>	<u>20</u>	<u>33</u>

9.5	7.3	6.8		7.2	8.7	7.9	7.7	3.2
<u>33</u>	<u>21</u>	<u>15</u>	6.5	<u>10</u>	<u>13</u>	<u>17</u>	<u>22</u>	<u>33</u>

9.8	10.4	7.9	8.2	8.0		8.7	10.1	10.4	2.3
<u>33</u>	<u>30</u>	<u>21</u>	<u>16</u>	<u>12</u>	7.7	<u>11</u>	<u>14</u>	<u>23</u>	<u>33</u>

17.0	16.3	10.2		9.9	13.6	12.1
<u>33</u>	<u>25</u>	<u>13</u>	9.4	<u>9</u>	<u>14</u>	<u>33</u>

Bottom of Ditch.

13.0	13.0	9.6	7.1	9.1	4.2	4.2		4.2	9.0	9.1	7.9
<u>47</u>	<u>43</u>	<u>38</u>	<u>33</u>	<u>23</u>	<u>14</u>	<u>12</u>	3.7	<u>9</u>	<u>14</u>	<u>23</u>	<u>33</u>

7.9	8.3	5.1		4.9	8.5	10.0	8.6
<u>33</u>	<u>22</u>	<u>12</u>	4.4	<u>9</u>	<u>17</u>	<u>24</u>	<u>33</u>

13.7

15.7 = Out lot.

8.3	8.3	6.7	4.5	4.9		5.3	9.8	16.0	15.5	13.0
<u>33</u>	<u>24</u>	<u>18</u>	<u>14</u>	<u>10</u>	4.5	<u>9</u>	<u>17</u>	<u>25</u>	<u>39</u>	<u>42</u>

Sta. + H. I. - Rod. E/ev,

886.03

42

80.93

4.69 885.94 4.74 879.27

+45

81.26

43

81.66

44

81.46

+70

81.16

45

80.96

+75

80.86

46

80.46

47

79.06

48

78.26

+ Cross Brain.

9.90 884.15 11.71 874.25

49

78.05

B.M.

4.73 877.42

50

78.25

6/5/24

Bottom of Dig

5.3	7.0	4.9	5.3		5.7	7.6	9.5	14.5	16.5	16.5	12.5
33	21	14	10	5.1	9	16	23	36	40	50	55

2.0	2.6	5.4	4.2	5.0		5.5	7.4	9.5
33	28	21	15	11	4.7	11	17	33

Above H.I.

11.5	1.5	5.0	5.0	4.4		5.2	6.4	4.6	4.7
33	30	22	18	14	4.3	11	15	26	33

1.2	4.0	5.4	5.0		5.0	5.6	5.7	1.5	1.6
33	28	19	13	4.5	9	12	18	27	33

Above H.I.

1.5	3.9	5.7	5.7	4.8		5.5	5.7	10.5	0.0
33	29	22	19	15	4.8	11	19	26	33

1.4	4.1	6.0	6.0	5.2		5.6	6.3	5.4	2.2	1.2	1.8
33	29	21	19	15	5.0	10	14	18	22	28	33

5.7	6.1	5.5	5.4		5.8	6.5	6.0	5.7
33	19	15	11	5.1	10	13	20	33

8.3	7.3	5.3	5.8		6.0	7.2	8.0
33	17	14	11	5.5	9	14	33

10.4	10.0	7.0	7.4		7.3	11.4	12.2
33	21	15	11	4.9	9	17	33

10.6	10.4	8.1		8.3	10.7	13.7
33	20	13	7.7	10	13	33

15.0

15.4

2.5	7.7	7.1		6.5	9.2	7.7
33	22	14	6.1	9	15	33

Spk. in T.P. Nt. Sta. 50+18.

8.8	8.5	7.0	6.3		6.2	7.9	8.4
33	20	18	14	5.9	10	15	33

884.15

51 78.8

52 81.1

53 83.6

T.P. 12.44 896.51 0.28 883.87

54 87.8

+50 89.5

55 91.3

56 94.8

T.P. 8.82 904.54 1.59 895.72

+58 96.5

57 97.9

+35 99.5

+46 99.9

T.P. 1.89 902.65

T.P. 6.00 921.59 +11.05 915.59

+51²⁰ Top of Mail 18.9

$\frac{7.5}{33} \quad \frac{7.2}{19} \quad \frac{6.1}{15} \quad 5.4 \quad \frac{5.4}{9} \quad \frac{6.0}{13} \quad \frac{5.6}{22} \quad \frac{5.2}{33}$

$\frac{5.2}{33} \quad \frac{5.2}{18} \quad \frac{3.8}{14} \quad 3.1 \quad \frac{5.1}{9} \quad \frac{3.4}{14} \quad \frac{3.2}{33}$

$\frac{3.3}{33} \quad \frac{3.2}{19} \quad \frac{1.4}{14} \quad 0.6 \quad \frac{0.6}{9} \quad \frac{0.7}{13} \quad \frac{1.3}{15} \quad \frac{1.0}{33}$

$\frac{13.3}{33} \quad \frac{11.6}{18} \quad \frac{7.4}{14} \quad 8.5 \quad \frac{8.9}{7} \quad \frac{8.3}{14} \quad \frac{7.2}{29} \quad \frac{6.8}{33}$

Above H.I.

$\frac{10.1}{33} \quad \frac{8.0}{23} \quad \frac{7.4}{14} \quad \frac{7.5}{11} \quad 6.8 \quad \frac{7.1}{8} \quad \frac{6.9}{14} \quad \frac{2.7}{20} \quad \frac{0.2}{25} \quad \frac{1.0}{33}$

Above H.I.

$\frac{7.8}{33} \quad \frac{7.0}{30} \quad \frac{4.1}{19} \quad \frac{5.4}{14} \quad \frac{5.7}{11} \quad 5.0 \quad \frac{5.5}{7} \quad \frac{5.1}{14} \quad \frac{0.3}{23} \quad \frac{+10.2}{37} \quad \frac{+11.6}{46}$

Above H.I.

Above H.I.

$\frac{0.5}{33} \quad \frac{+1.0}{37} \quad \frac{+1.0}{22} \quad \frac{1.8}{14} \quad \frac{2.1}{12} \quad 1.5 \quad \frac{2.0}{12} \quad \frac{1.0}{17} \quad \frac{+5.5}{29} \quad \frac{+13.0}{37} \quad \frac{+13.5}{40}$

Above H.I.

$\frac{6.7}{33} \quad \frac{4.8}{24} \quad \frac{8.6}{18} \quad \frac{8.9}{13} \quad \frac{8.5}{12} \quad 8.0 \quad \frac{8.5}{10} \quad \frac{9.5}{12} \quad \frac{6.1}{19} \quad \frac{+4.4}{34} \quad \frac{+5.7}{41}$

Above H.I.

$\frac{2.3}{33} \quad \frac{2.0}{29} \quad \frac{0.7}{14} \quad \frac{0.9}{23} \quad \frac{6.9}{15} \quad 6.6 \quad \frac{6.4}{9} \quad \frac{0.0}{16} \quad \frac{+2.3}{21} \quad \frac{+3.2}{33}$

Above H.I.

Above H.I.

$\frac{16.7}{33} \quad \frac{+5.5}{26} \quad \frac{+2.2}{17} \quad \frac{5.0}{8} \quad 5.0 \quad \frac{4.8}{6} \quad \frac{4.2}{8} \quad \frac{+3.0}{18} \quad \frac{+7.6}{30} \quad \frac{+7.6}{33}$

$\frac{+12.5}{26} \quad \frac{+12.5}{33}$

$\frac{+12.5}{33} \quad \frac{+12.5}{26} \quad \frac{+13.3}{12.7} \quad \frac{+11.0}{12.7} \quad \frac{+11.0}{11} \quad \frac{1.8}{10} \quad \frac{3.2}{8} \quad \frac{4.1}{6} \quad 4.4 \quad \frac{4.1}{4} \quad \frac{5.2}{8} \quad \frac{1.8}{10} \quad \frac{+11.0}{11} \quad \frac{+11.0}{12.7} \quad \frac{+12.5}{12.7}$

On Rock.

$\frac{2.69}{100} \quad \frac{2.70}{50} \quad 2.69 \quad \frac{2.85}{50} \quad \frac{3.02}{100}$

Sta.	+	H.I.	-	Red.	F/cu
		921.59			
+56 ¹⁰		Top of Nail		2.69	18.9
+65 ³⁵	"	"	"	2.66	18.93
+70 ²⁵	"	"	"	2.64	18.93
T.P.	1.14	903.79	18.94	902.65	902.65
+74				3.4	900.4
58				3.6	90.2
B.M.			2.66	901.13	901.17
+50				5.3	98.5
59				6.6	97.2
+56 ⁶⁵				7.2	96.6
+61				7.3	96.5
+64				7.4	96.4
60				7.7	96.1
59+78		Cross Drain			
60+60				7.7	96.1

6/4/22

$\frac{2.68}{100}$ $\frac{2.68}{50}$ 2.69 $\frac{2.85}{50}$ $\frac{3.02}{100}$

$\frac{2.68}{100}$ $\frac{2.64}{50}$ 2.64 $\frac{2.91}{50}$ $\frac{3.11}{100}$

$\frac{2.68}{100}$ $\frac{2.63}{50}$ 2.64 $\frac{2.89}{50}$ $\frac{3.11}{100}$

On Rock

$\frac{1.1}{10}$ $\frac{3.6}{8}$ 3.4 $\frac{2.9}{7}$ $\frac{2.0}{9}$ $\frac{1.1}{10}$

Above H.I.

Above H.I.

$\frac{+5.5}{33}$ $\frac{+4.0}{22}$ $\frac{+1.7}{14}$ $\frac{3.6}{9}$ 3.3 $\frac{1.2}{15}$ $\frac{+1.2}{33}$

Spk in T.P. on Co. Rd. R. 50 East of N.P. Ry. R.R. Timber Bridge # 17

$\frac{7.5}{33}$ $\frac{6.0}{17}$ $\frac{5.1}{15}$ $\frac{5.5}{11}$ 5.3 $\frac{5.6}{7}$ $\frac{6.5}{20}$ $\frac{8.1}{27}$ $\frac{9.0}{33}$

$\frac{8.7}{33}$ $\frac{8.9}{27}$ $\frac{8.4}{22}$ $\frac{7.0}{17}$ $\frac{6.8}{13}$ $\frac{6.4}{7}$ 6.6 $\frac{6.9}{7}$ $\frac{7.4}{14}$ $\frac{7.1}{20}$ $\frac{7.7}{28}$ $\frac{7.1}{32}$ $\frac{7.1}{33}$

$\frac{11.6}{33}$ $\frac{11.6}{29}$ $\frac{12.2}{28}$ $\frac{12.2}{26}$ $\frac{11.1}{20}$ $\frac{7.9}{13}$ 7.2 $\frac{7.5}{12}$ $\frac{7.6}{27}$ $\frac{7.4}{33}$

$\frac{11.5}{33}$ $\frac{11.5}{27}$ $\frac{12.4}{24}$ $\frac{12.4}{23}$ $\frac{11.4}{23}$ $\frac{10.4}{17}$ $\frac{8.7}{13}$ $\frac{7.9}{9}$ 7.3 $\frac{7.7}{13}$ $\frac{7.8}{25}$ $\frac{8.0}{33}$

$\frac{11.5}{33}$ $\frac{11.5}{27}$ $\frac{12.5}{24}$ $\frac{12.5}{24}$ $\frac{11.6}{23}$ $\frac{10.4}{17}$ $\frac{8.1}{11}$ 7.4 $\frac{7.9}{13}$ $\frac{8.3}{20}$ $\frac{10.4}{28}$ $\frac{10.7}{33}$

$\frac{11.5}{33}$ $\frac{11.5}{21}$ $\frac{10.7}{19}$ $\frac{9.0}{14}$ $\frac{8.4}{11}$ 7.7 $\frac{8.4}{10}$ $\frac{9.4}{14}$ $\frac{12.4}{19}$ $\frac{12.5}{21}$ $\frac{11.6}{22}$ $\frac{11.7}{33}$

$\frac{12.7}{20}$ $\frac{12.6}{20}$

$\frac{7.4}{33}$ $\frac{7.4}{29}$ $\frac{7.5}{16}$ $\frac{8.9}{14}$ $\frac{8.5}{11}$ 7.7 $\frac{8.5}{10}$ $\frac{7.7}{13}$ $\frac{11.5}{18}$ $\frac{12.4}{19}$ $\frac{12.4}{21}$ $\frac{11.6}{22}$ $\frac{11.8}{33}$

Sta.	+	H.I.	-	Red	Elev.
		903.79			

61				7.2	96.6
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T.P.	7.18	904.01	6.94	896.83	
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+50				7.1	96.9
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62				6.9	97.1
----	--	--	--	-----	------

63				5.2	98.8
----	--	--	--	-----	------

+28				4.9	99.1
-----	--	--	--	-----	------

+74 Cross Drain

64				3.2	00.8
----	--	--	--	-----	------

T.P.	12.50	914.28	2.23	901.78	
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65				2.4	05.9
----	--	--	--	-----	------

66				3.2	11.1
----	--	--	--	-----	------

+50				0.5	13.8
-----	--	--	--	-----	------

T.P.	12.29	925.67	0.90	913.38	
------	-------	--------	------	--------	--

67				9.3	16.4
----	--	--	--	-----	------

+50				7.3	18.4
-----	--	--	--	-----	------

68				5.4	20.3
----	--	--	--	-----	------

$\frac{9.1}{33}$ $\frac{9.1}{30}$ $\frac{8.9}{17}$ $\frac{8.0}{12}$ 7.2 $\frac{7.8}{10}$ $\frac{8.4}{14}$ $\frac{10.9}{18}$ $\frac{11.5}{18}$ $\frac{11.5}{20}$ $\frac{11.0}{21}$ $\frac{11.0}{33}$

$\frac{10.4}{33}$ $\frac{10.0}{29}$ $\frac{8.8}{17}$ $\frac{7.8}{12}$ 7.1 $\frac{7.5}{10}$ $\frac{6.5}{13}$ $\frac{7.5}{14}$ $\frac{9.2}{18}$ $\frac{10.7}{19}$ $\frac{10.7}{21}$ $\frac{9.0}{22}$

$\frac{11.5}{33}$ $\frac{11.0}{31}$ $\frac{10.2}{18}$ $\frac{8.6}{15}$ $\frac{7.7}{12}$ 6.7 $\frac{7.2}{9}$ $\frac{7.6}{14}$ $\frac{7.8}{18}$ $\frac{10.9}{19}$ $\frac{10.9}{20}$ $\frac{9.3}{21}$ $\frac{8.3}{24}$

$\frac{10.5}{33}$ $\frac{9.3}{18}$ $\frac{5.9}{11}$ 5.2 $\frac{5.6}{11}$ $\frac{5.4}{14}$ $\frac{8.5}{19}$ $\frac{8.4}{20}$ $\frac{8.4}{21}$ $\frac{7.4}{23}$ $\frac{5.1}{30}$ $\frac{5.1}{33}$

$\frac{10.7}{33}$ $\frac{10.1}{30}$ $\frac{9.4}{21}$ $\frac{8.5}{18}$ $\frac{5.8}{12}$ 4.9 $\frac{5.4}{9}$ $\frac{5.2}{13}$ $\frac{8.6}{18}$ $\frac{9.5}{21}$ $\frac{9.5}{22}$ $\frac{8.2}{23}$ $\frac{7.5}{33}$

Invert = $\frac{10.1}{24}$

$\frac{10.6}{27}$ = Out Let

$\frac{9.6}{33}$ $\frac{9.2}{29}$ $\frac{8.0}{18}$ $\frac{4.2}{12}$ $\frac{3.9}{11}$ 3.2 $\frac{3.9}{10}$ $\frac{4.3}{12}$ $\frac{8.9}{20}$ $\frac{9.7}{22}$ $\frac{9.9}{24}$ $\frac{9.5}{27}$ $\frac{9.0}{33}$

$\frac{16.9}{33}$ $\frac{16.8}{27}$ $\frac{15.5}{20}$ $\frac{9.0}{11}$ 8.4 $\frac{9.3}{11}$ $\frac{15.9}{24}$ $\frac{18.7}{33}$

$\frac{7.5}{33}$ $\frac{7.8}{27}$ $\frac{6.7}{24}$ $\frac{6.0}{14}$ $\frac{4.0}{12}$ 3.2 $\frac{3.9}{12}$ $\frac{11.3}{25}$ $\frac{11.3}{33}$

$\frac{2.1}{33}$ $\frac{2.0}{24}$ $\frac{0.8}{24}$ $\frac{0.7}{13}$ $\frac{1.2}{11}$ 0.5 $\frac{1.1}{11}$ $\frac{1.4}{14}$ $\frac{7.0}{28}$ $\frac{7.2}{33}$

$\frac{6.4}{33}$ $\frac{6.8}{21}$ $\frac{9.7}{14}$ $\frac{9.8}{7}$ 9.3 $\frac{9.8}{9}$ $\frac{10.0}{24}$ $\frac{9.2}{27}$ $\frac{10.2}{33}$

$\frac{0.2}{33}$ $\frac{0.5}{28}$ $\frac{7.3}{15}$ $\frac{7.7}{9}$ 7.3 $\frac{7.8}{10}$ $\frac{7.2}{18}$ $\frac{5.5}{20}$ $\frac{5.5}{25}$ $\frac{2.1}{29}$ $\frac{2.7}{33}$

Above H. I

$\frac{12.9}{33}$ $\frac{12.2}{30}$ $\frac{4.8}{17}$ $\frac{6.2}{9}$ 5.4 $\frac{5.9}{9}$ $\frac{5.6}{14}$ $\frac{13.8}{30}$ $\frac{13.6}{33}$

Sta.	+	M.I.	-	Ro-1.	Elev.
		925.67			
69		✓		1.5	24.2
T.P.	10.21	934.38	1.50	✓ 924.17	
70				6.3	28.1
+50				5.3	29.1
71				4.5	29.9
+50				4.1	30.3
72				4.5	29.9
+75				4.7	29.7
73				4.7	29.5
+40				5.0	29.4
74				4.7	29.7
+35				4.8	29.6
+45				4.8	29.6
75				4.9	29.5

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Above H.I.

$$\begin{array}{r} 14.7 \\ 33 \end{array} \begin{array}{r} 14.7 \\ 27 \end{array} \begin{array}{r} 0.8 \\ 15 \end{array} \begin{array}{r} 2.1 \\ 9 \end{array}$$

1.5

$$\begin{array}{r} 2.0 \\ 9 \end{array} \begin{array}{r} 1.7 \\ 14 \end{array}$$

Above H.I.

$$\begin{array}{r} 16.1 \\ 29 \end{array} \begin{array}{r} 16.0 \\ 33 \end{array}$$

$$\begin{array}{r} 0.4 \\ 33 \end{array} \begin{array}{r} 1.4 \\ 25 \end{array} \begin{array}{r} 6.5 \\ 16 \end{array} \begin{array}{r} 6.8 \\ 10 \end{array}$$

6.3

$$\begin{array}{r} 7.0 \\ 14 \end{array} \begin{array}{r} 1.0 \\ 24 \end{array} \begin{array}{r} 1.4 \\ 33 \end{array}$$

Above H.I.

$$\begin{array}{r} 0.3 \\ 33 \end{array} \begin{array}{r} 0.0 \\ 24 \end{array} \begin{array}{r} 4.9 \\ 16 \end{array} \begin{array}{r} 5.7 \\ 11 \end{array}$$

5.3

$$\begin{array}{r} 5.8 \\ 11 \end{array} \begin{array}{r} 4.2 \\ 18 \end{array} \begin{array}{r} 0.4 \\ 22 \end{array} \begin{array}{r} 1.8 \\ 24 \end{array} \begin{array}{r} 10.8 \\ 33 \end{array}$$

$$\begin{array}{r} 0.4 \\ 33 \end{array} \begin{array}{r} 2.2 \\ 17 \end{array} \begin{array}{r} 5.1 \\ 12 \end{array}$$

4.5

$$\begin{array}{r} 5.1 \\ 12 \end{array} \begin{array}{r} 4.8 \\ 15 \end{array} \begin{array}{r} 0.6 \\ 22 \end{array} \begin{array}{r} 0.0 \\ 33 \end{array}$$

$$\begin{array}{r} 1.7 \\ 33 \end{array} \begin{array}{r} 4.2 \\ 12 \end{array}$$

4.1

$$\begin{array}{r} 4.8 \\ 10 \end{array} \begin{array}{r} 5.2 \\ 14 \end{array} \begin{array}{r} 1.7 \\ 21 \end{array} \begin{array}{r} 1.8 \\ 33 \end{array}$$

$$\begin{array}{r} 1.5 \\ 33 \end{array} \begin{array}{r} 4.0 \\ 21 \end{array} \begin{array}{r} 4.8 \\ 11 \end{array}$$

4.5

$$\begin{array}{r} 5.2 \\ 12 \end{array} \begin{array}{r} 4.7 \\ 19 \end{array} \begin{array}{r} 2.0 \\ 21 \end{array} \begin{array}{r} 1.8 \\ 33 \end{array}$$

$$\begin{array}{r} 5.8 \\ 33 \end{array} \begin{array}{r} 5.7 \\ 18 \end{array} \begin{array}{r} 5.2 \\ 9 \end{array}$$

4.7

$$\begin{array}{r} 5.2 \\ 11 \end{array} \begin{array}{r} 5.8 \\ 33 \end{array}$$

$$\begin{array}{r} 6.0 \\ 33 \end{array} \begin{array}{r} 6.2 \\ 22 \end{array} \begin{array}{r} 5.3 \\ 10 \end{array}$$

7.9

$$\begin{array}{r} 5.2 \\ 12 \end{array} \begin{array}{r} 6.4 \\ 18 \end{array} \begin{array}{r} 7.2 \\ 28 \end{array} \begin{array}{r} 7.1 \\ 33 \end{array}$$

$$\begin{array}{r} 5.0 \\ 33 \end{array} \begin{array}{r} 6.2 \\ 15 \end{array} \begin{array}{r} 5.5 \\ 12 \end{array}$$

5.0

$$\begin{array}{r} 5.6 \\ 12 \end{array} \begin{array}{r} 7.1 \\ 17 \end{array} \begin{array}{r} 7.9 \\ 33 \end{array}$$

$$\begin{array}{r} 6.8 \\ 33 \end{array} \begin{array}{r} 6.1 \\ 17 \end{array} \begin{array}{r} 5.2 \\ 12 \end{array}$$

4.7

$$\begin{array}{r} 5.1 \\ 12 \end{array} \begin{array}{r} 4.9 \\ 33 \end{array}$$

$$\begin{array}{r} 9.5 \\ 33 \end{array} \begin{array}{r} 8.1 \\ 18 \end{array} \begin{array}{r} 5.5 \\ 19 \end{array} \begin{array}{r} 5.3 \\ 9 \end{array}$$

4.8

$$\begin{array}{r} 5.1 \\ 10 \end{array} \begin{array}{r} 5.1 \\ 33 \end{array}$$

$$\begin{array}{r} 9.9 \\ 33 \end{array} \begin{array}{r} 8.6 \\ 18 \end{array} \begin{array}{r} 5.8 \\ 13 \end{array} \begin{array}{r} 5.3 \\ 9 \end{array}$$

4.8

$$\begin{array}{r} 5.2 \\ 13 \end{array} \begin{array}{r} 7.2 \\ 21 \end{array} \begin{array}{r} 6.8 \\ 33 \end{array}$$

$$\begin{array}{r} 9.5 \\ 33 \end{array} \begin{array}{r} 7.6 \\ 20 \end{array} \begin{array}{r} 5.7 \\ 14 \end{array} \begin{array}{r} 5.4 \\ 10 \end{array}$$

4.9

$$\begin{array}{r} 5.3 \\ 9 \end{array} \begin{array}{r} 5.6 \\ 19 \end{array} \begin{array}{r} 11.0 \\ 22 \end{array} \begin{array}{r} 11.1 \\ 33 \end{array}$$

Sta.	T	H.I.	-	Prod.	Elev
		734.38			
76		✓		4.9	29.5
T.P.	8.21	737.32	5.27	✓ 729.11	
77				8.2	29.1
78				7.2	30.1
79				5.7	31.6
+50				5.1	32.2
80				4.5	32.8
B.M.			1.58	✓ 735.74	
81				2.8	34.52
+40				2.7	34.6
82				2.8	34.5
+40				2.7	34.6
83		✓		2.8	34.5
T.P.	3.40	737.69	3.03	✓ 734.29	
+50				3.3	34.4
84				3.9	33.8

$$\begin{array}{r} 80 \\ 33 \end{array} \quad \begin{array}{r} 7.9 \\ 18 \end{array} \quad \begin{array}{r} 5.4 \\ 13 \end{array} \quad \begin{array}{r} 5.4 \\ 9 \end{array} \quad 4.9 \quad \begin{array}{r} 5.3 \\ 10 \end{array} \quad \begin{array}{r} 5.7 \\ 13 \end{array} \quad \begin{array}{r} 7.5 \\ 18 \end{array} \quad \begin{array}{r} 7.9 \\ 33 \end{array}$$

$$\begin{array}{r} 10.7 \\ 33 \end{array} \quad \begin{array}{r} 10.4 \\ 17 \end{array} \quad \begin{array}{r} 8.8 \\ 12 \end{array} \quad \begin{array}{r} 8.6 \\ 6 \end{array} \quad 8.2 \quad \begin{array}{r} 8.7 \\ 12 \end{array} \quad \begin{array}{r} 11.1 \\ 19 \end{array} \quad \begin{array}{r} 11.5 \\ 33 \end{array}$$

$$\begin{array}{r} 8.4 \\ 33 \end{array} \quad \begin{array}{r} 8.6 \\ 17 \end{array} \quad \begin{array}{r} 7.4 \\ 12 \end{array} \quad \begin{array}{r} 7.5 \\ 8 \end{array} \quad 7.2 \quad \begin{array}{r} 7.6 \\ 10 \end{array} \quad \begin{array}{r} 7.8 \\ 14 \end{array} \quad \begin{array}{r} 8.7 \\ 14 \end{array} \quad \begin{array}{r} 8.5 \\ 33 \end{array}$$

$$\begin{array}{r} 4.8 \\ 33 \end{array} \quad \begin{array}{r} 5.8 \\ 15 \end{array} \quad \begin{array}{r} 6.1 \\ 9 \end{array} \quad 5.7 \quad \begin{array}{r} 6.1 \\ 11 \end{array} \quad \begin{array}{r} 6.3 \\ 14 \end{array} \quad \begin{array}{r} 6.0 \\ 19 \end{array} \quad \begin{array}{r} 5.6 \\ 33 \end{array}$$

$$\begin{array}{r} 4.1 \\ 33 \end{array} \quad \begin{array}{r} 5.7 \\ 18 \end{array} \quad \begin{array}{r} 5.9 \\ 15 \end{array} \quad \begin{array}{r} 5.6 \\ 8 \end{array} \quad 5.1 \quad \begin{array}{r} 5.6 \\ 12 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad \begin{array}{r} 4.9 \\ 33 \end{array}$$

$$\begin{array}{r} 3.0 \\ 33 \end{array} \quad \begin{array}{r} 2.9 \\ 18 \end{array} \quad \begin{array}{r} 5.0 \\ 15 \end{array} \quad \begin{array}{r} 5.0 \\ 11 \end{array} \quad 4.5 \quad \begin{array}{r} 5.1 \\ 15 \end{array} \quad \begin{array}{r} 4.8 \\ 14 \end{array} \quad \begin{array}{r} 4.6 \\ 33 \end{array}$$

SPK. in T.P. 30' 14.549. 80+10.

$$\begin{array}{r} 1.4 \\ 33 \end{array} \quad \begin{array}{r} 1.2 \\ 18 \end{array} \quad \begin{array}{r} 3.0 \\ 15 \end{array} \quad \begin{array}{r} 3.6 \\ 12 \end{array} \quad 2.8 \quad \begin{array}{r} 3.4 \\ 13 \end{array} \quad \begin{array}{r} 2.1 \\ 17 \end{array} \quad \begin{array}{r} 1.6 \\ 33 \end{array}$$

$$\begin{array}{r} 2.2 \\ 33 \end{array} \quad \begin{array}{r} 1.9 \\ 18 \end{array} \quad \begin{array}{r} 3.4 \\ 14 \end{array} \quad \begin{array}{r} 3.5 \\ 11 \end{array} \quad 2.7 \quad \begin{array}{r} 3.4 \\ 14 \end{array} \quad \begin{array}{r} 2.9 \\ 27 \end{array} \quad \begin{array}{r} 2.0 \\ 33 \end{array}$$

$$\begin{array}{r} 4.0 \\ 33 \end{array} \quad \begin{array}{r} 4.0 \\ 15 \end{array} \quad \begin{array}{r} 3.5 \\ 12 \end{array} \quad 2.8 \quad \begin{array}{r} 3.5 \\ 11 \end{array} \quad \begin{array}{r} 4.8 \\ 18 \end{array} \quad \begin{array}{r} 4.9 \\ 29 \end{array} \quad \begin{array}{r} 4.2 \\ 33 \end{array}$$

$$\begin{array}{r} 3.0 \\ 33 \end{array} \quad \begin{array}{r} 3.8 \\ 20 \end{array} \quad \begin{array}{r} 3.3 \\ 14 \end{array} \quad 2.7 \quad \begin{array}{r} 3.4 \\ 12 \end{array} \quad \begin{array}{r} 5.1 \\ 19 \end{array} \quad \begin{array}{r} 4.4 \\ 30 \end{array} \quad \begin{array}{r} 4.4 \\ 33 \end{array}$$

Above H.I.

$$\begin{array}{r} +1.5 \\ 33 \end{array} \quad \begin{array}{r} +1.1 \\ 25 \end{array} \quad \begin{array}{r} 3.1 \\ 18 \end{array} \quad \begin{array}{r} 3.1 \\ 8 \end{array} \quad 2.8 \quad \begin{array}{r} 3.7 \\ 13 \end{array} \quad \begin{array}{r} 0.5 \\ 14 \end{array} \quad \begin{array}{r} 1.0 \\ 33 \end{array}$$

Above H.I.

Above H.I.

$$\begin{array}{r} +3.2 \\ 35 \end{array} \quad \begin{array}{r} +3.2 \\ 33 \end{array} \quad \begin{array}{r} 2.3 \\ 27 \end{array} \quad \begin{array}{r} 2.5 \\ 22 \end{array} \quad \begin{array}{r} 3.7 \\ 8 \end{array} \quad 3.3 \quad \begin{array}{r} 3.9 \\ 13 \end{array} \quad \begin{array}{r} +1.3 \\ 22 \end{array} \quad \begin{array}{r} +0.9 \\ 33 \end{array}$$

Above H.I.

$$\begin{array}{r} +2.5 \\ 35 \end{array} \quad \begin{array}{r} +2.5 \\ 33 \end{array} \quad \begin{array}{r} 2.2 \\ 29 \end{array} \quad \begin{array}{r} 4.5 \\ 20 \end{array} \quad \begin{array}{r} 4.4 \\ 9 \end{array} \quad 3.9 \quad \begin{array}{r} 4.6 \\ 14 \end{array} \quad \begin{array}{r} +0.6 \\ 22 \end{array} \quad \begin{array}{r} 0.0 \\ 33 \end{array}$$

Sta.	+	H. I.	-	Ref.	Elev.
		937.69			
+60				5.2	32.5
85				5.8	31.9
T.P.	3.45	934.03	7.11	930.58	
+65				4.1	29.9
86				5.3	28.7
+50				7.0	27.0
87				8.4	25.6
+35				9.2	24.8
+47				9.6	24.4
T.P.	4.00	924.97	11.04	922.97	
88				3.7	23.3
+47				5.0	22.0
89				4.4	20.6
+58	Cross Drain				
90				7.2	19.8

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<u>1.8</u>	<u>1.4</u>	<u>4.0</u>	<u>5.9</u>		<u>5.7</u>	<u>5.3</u>	<u>5.9</u>
33	22	20	14	5.2	14	19	33

<u>6.9</u>	<u>5.6</u>	<u>6.0</u>	<u>6.1</u>		<u>6.8</u>	<u>6.6</u>	<u>5.3</u>	<u>5.3</u>
33	17	13	10	5.8	14	19	22	33

Nail in T.P. Lt. 519. 85130.

80	5.3	4.9	5.3	<u>4.6</u>		<u>4.5</u>	<u>5.3</u>	<u>1.2</u>
33	17	17	14	10	4.1	14	21	33

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<u>11.3</u>	<u>9.7</u>	<u>8.7</u>	<u>5.8</u>		<u>5.6</u>	<u>5.6</u>	<u>2.8</u>	<u>2.8</u>
33	30	27	11	5.3	11	17	31	33

<u>13.9</u>	<u>12.2</u>	<u>11.6</u>	<u>9.8</u>	<u>9.2</u>	<u>7.6</u>		<u>7.6</u>	<u>8.1</u>	<u>6.9</u>	<u>6.2</u>
33	30	24	20	15	12	7.0	15	16	24	33

<u>11.3</u>	<u>10.8</u>	<u>10.2</u>	<u>9.1</u>		<u>8.9</u>	<u>8.5</u>	<u>7.0</u>	<u>7.0</u>
33	26	14	14	8.4	13	17	31	33

<u>8.6</u>	<u>8.7</u>	<u>9.7</u>		<u>9.8</u>	<u>8.8</u>	<u>8.7</u>	<u>8.1</u>
33	17	12	9.2	13	18	29	33

<u>12.6</u>	<u>12.6</u>	<u>10.9</u>	<u>10.1</u>		<u>10.0</u>	<u>9.0</u>	<u>9.0</u>
33	31	20	13	9.4	13	17	33

<u>6.6</u>	<u>4.6</u>	<u>4.2</u>		<u>4.4</u>	<u>2.7</u>	<u>1.4</u>	<u>1.4</u>
33	19	11	3.7	13	18	32	33

<u>4.6</u>	<u>5.5</u>	<u>5.3</u>	<u>5.5</u>		<u>5.6</u>	<u>6.8</u>	<u>6.7</u>
33	28	17	12	5.0	11	16	33

<u>11.5</u>	<u>10.9</u>	<u>6.8</u>		<u>6.9</u>	<u>11.3</u>	<u>11.7</u>
33	17	11	6.4	11	20	33

<u>15.3</u>
27

<u>15.6</u>
24

<u>12.1</u>	<u>11.0</u>	<u>8.5</u>	<u>5.6</u>		<u>7.9</u>	<u>11.6</u>	<u>12.0</u>
33	20	14	10	7.2	13	21	33

Sta.	+	H. I.	-	Prod.	L/cv
		726.77			

71				7.3	19.7
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72				6.0	21.0
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T.P.	7.85	731.03	5.79	721.18	
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73				6.7	24.3
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74				3.1	27.9
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+70				0.7	30.3
-----	--	--	--	-----	------

T.P.	11.11	741.41	0.73	730.30	
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75				10.2	31.2
----	--	--	--	------	------

+77				7.4	32.0
-----	--	--	--	-----	------

76				7.3	34.1
----	--	--	--	-----	------

77				4.2	37.2
----	--	--	--	-----	------

78				1.8	39.6
----	--	--	--	-----	------

T.P.	2.10	742.85	0.64	740.75	
------	------	--------	------	--------	--

79				3.5	39.4
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100				4.4	38.5
-----	--	--	--	-----	------

101				5.6	37.3
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$\frac{11.7}{33}$	$\frac{11.7}{20}$	$\frac{9.0}{15}$	$\frac{7.9}{10}$		$\frac{8.3}{12}$	$\frac{12.3}{20}$	$\frac{12.4}{33}$
-------------------	-------------------	------------------	------------------	--	------------------	-------------------	-------------------

$\frac{12.2}{33}$	$\frac{12.0}{21}$	$\frac{6.6}{12}$		$\frac{6.7}{12}$	$\frac{12.0}{21}$	$\frac{12.3}{33}$
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$\frac{15.1}{33}$	$\frac{13.8}{23}$	$\frac{7.3}{12}$		$\frac{7.4}{11}$	$\frac{14.3}{23}$	$\frac{15.6}{33}$
-------------------	-------------------	------------------	--	------------------	-------------------	-------------------

$\frac{13.2}{33}$	$\frac{11.6}{24}$	$\frac{5.7}{13}$		$\frac{5.8}{13}$	$\frac{13.2}{29}$	$\frac{13.8}{33}$
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$\frac{9.4}{33}$	$\frac{7.5}{25}$	$\frac{1.4}{13}$		$\frac{1.5}{13}$	$\frac{7.3}{33}$
------------------	------------------	------------------	--	------------------	------------------

$\frac{15.7}{33}$	$\frac{14.5}{21}$	$\frac{10.4}{14}$	$\frac{10.1}{13}$	$\frac{10.7}{11}$	10.2	$\frac{10.7}{13}$	$\frac{10.0}{16}$	$\frac{10.2}{21}$	$\frac{14.4}{33}$
-------------------	-------------------	-------------------	-------------------	-------------------	--------	-------------------	-------------------	-------------------	-------------------

$\frac{11.7}{33}$	$\frac{10.7}{26}$	$\frac{7.5}{19}$	$\frac{7.9}{10}$		$\frac{7.8}{14}$	$\frac{7.9}{21}$	$\frac{7.4}{24}$	$\frac{7.4}{33}$
-------------------	-------------------	------------------	------------------	--	------------------	------------------	------------------	------------------

Above H.I.

$\frac{+3.1}{35}$	$\frac{+3.1}{33}$	$\frac{+1.1}{29}$	$\frac{1.6}{25}$	$\frac{5.2}{21}$	$\frac{6.8}{14}$	$\frac{7.8}{9}$	7.3	$\frac{8.0}{10}$	$\frac{7.4}{13}$	$\frac{0.8}{23}$	$\frac{+2.0}{35}$	$\frac{+3.6}{37}$	$\frac{+3.4}{40}$
-------------------	-------------------	-------------------	------------------	------------------	------------------	-----------------	-------	------------------	------------------	------------------	-------------------	-------------------	-------------------

$\frac{+17.9}{55}$	$\frac{+17.9}{52}$	$\frac{18.7}{52}$	$\frac{0.0}{21}$	$\frac{5.3}{14}$	$\frac{4.5}{10}$	4.2	$\frac{4.5}{10}$	$\frac{4.0}{13}$	$\frac{1.0}{23}$	$\frac{+11.0}{44}$	$\frac{+17.3}{48}$	$\frac{+17.3}{50}$
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$\frac{+11.7}{42}$	$\frac{+11.7}{39}$	$\frac{+6.8}{50}$	$\frac{+4.5}{24}$	$\frac{1.3}{14}$	$\frac{2.2}{9}$	1.8	$\frac{2.0}{9}$	$\frac{1.0}{13}$	$\frac{0.0}{14}$	$\frac{+3.0}{23}$	$\frac{+6.3}{50}$	$\frac{+12.5}{39}$	$\frac{+12.5}{42}$
--------------------	--------------------	-------------------	-------------------	------------------	-----------------	-------	-----------------	------------------	------------------	-------------------	-------------------	--------------------	--------------------

$\frac{5.1}{33}$	$\frac{2.6}{25}$	$\frac{3.0}{23}$	$\frac{5.6}{16}$	$\frac{5.7}{10}$	5.5	$\frac{3.9}{9}$	$\frac{3.5}{10}$	$\frac{3.4}{15}$	$\frac{2.1}{18}$	$\frac{3.0}{25}$	$\frac{4.4}{33}$
------------------	------------------	------------------	------------------	------------------	-------	-----------------	------------------	------------------	------------------	------------------	------------------

$\frac{7.6}{33}$	$\frac{7.4}{27}$	$\frac{8.6}{19}$	$\frac{4.8}{13}$	4.4	$\frac{4.7}{9}$	$\frac{4.4}{12}$	$\frac{9.0}{23}$	$\frac{9.6}{33}$
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$\frac{11.7}{33}$	$\frac{11.7}{26}$	$\frac{10.4}{18}$	$\frac{6.2}{12}$	5.4	$\frac{6.1}{13}$	$\frac{10.6}{20}$	$\frac{11.7}{33}$
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Sta.	+	H.I.	-	Roof	Flex.
		942.85			
102				6.2	36.7

+ Cross Drain

103				6.6	36.3
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T.P.	11.15	946.20	7.80	935.05	
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104				8.4	37.6
-----	--	--	--	-----	------

105				6.7	39.5
-----	--	--	--	-----	------

104				2.6	43.6
-----	--	--	--	-----	------

137				0.1	46.1
-----	--	--	--	-----	------

T.P.	6.11	951.71	0.60	945.60	
------	------	--------	------	--------	--

146 ⁸	Edge of Pavement	4.78			46.93
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136 ⁸	Q. of Pavement	4.70			47.0
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146 ⁸	Edge of Pavement	4.73			46.98
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B.M.	4.51	951.49	4.69	947.02	946.98
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173				4.6	46.9
-----	--	--	--	-----	------

782				4.4	47.1
-----	--	--	--	-----	------

107				4.1	47.4
-----	--	--	--	-----	------

T.P.	10.42	961.23	0.88	950.61	
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6/10/24

11.2	11.2	10.3	7.0		6.7	10.4	11.0
<u>33</u>	<u>29</u>	<u>19</u>	<u>12</u>	6.2	<u>12</u>	<u>20</u>	<u>33</u>

1093

11.5

8.8	10.0	9.8	7.3		7.0	8.9	9.4	9.0	10.0	9.7
<u>33</u>	<u>24</u>	<u>14</u>	<u>12</u>	6.6	<u>12</u>	<u>16</u>	<u>22</u>	<u>24</u>	<u>25</u>	<u>33</u>

14.2	13.7	9.6		9.4	13.4	14.0
<u>33</u>	<u>20</u>	<u>12</u>	8.6	<u>12</u>	<u>20</u>	<u>33</u>

13.1	11.4	8.1	7.5		7.4	10.4	11.7	11.7
<u>33</u>	<u>19</u>	<u>13</u>	<u>10</u>	6.7	<u>13</u>	<u>20</u>	<u>31</u>	<u>33</u>

5.3	5.3	3.3	3.0		3.4	5.1	6.0	6.0
<u>33</u>	<u>17</u>	<u>12</u>	<u>8</u>	2.4	<u>14</u>	<u>20</u>	<u>25</u>	<u>33</u>

1.9	1.9	2.1	0.5		0.3	1.4	2.4	3.1	3.2
<u>33</u>	<u>31</u>	<u>21</u>	<u>18</u>	0.1	<u>21</u>	<u>24</u>	<u>29</u>	<u>30</u>	<u>34</u>

4.96		4.49
<u>33</u>	4.78	<u>33</u>

4.99		4.19
<u>50</u>	4.70	<u>50</u>

5.00		4.45
<u>33</u>	4.73	<u>33</u>

Spl. in T.P.H. 112 at Int. of Co. Rd. "D" & White Bear Rd. #18
 N.E. Cor. Co. Rd. "D" &
 White Bear Rd.

4.8	4.9		4.5	4.8	4.5	4.6
<u>33</u>	<u>20</u>	4.6	<u>15</u>	<u>25</u>	<u>29</u>	<u>33</u>

5.9	5.4	4.8		4.8	4.9	4.8	5.5
<u>33</u>	<u>22</u>	<u>13</u>	4.4	<u>13</u>	<u>19</u>	<u>22</u>	<u>33</u>

4.0	4.8	4.9	4.4		4.5	4.4	4.0	4.1
<u>33</u>	<u>23</u>	<u>14</u>	<u>12</u>	4.1	<u>13</u>	<u>19</u>	<u>24</u>	<u>33</u>

Sta.	T	H.I.	-	Reel	F104
		966.23			
108				9.7	51.5
	+55			8.4	52.8
109				6.7	54.5
	+70			4.9	56.3
110				4.6	56.6
	+65			3.9	57.3
111				3.5	57.7
	+44			3.1	58.1
112				1.9	59.3
113				0.7	60.5
T.P.	3.92	964.46	0.69	960.54	
	+27			3.7	60.8
114				3.7	60.8
115	+40			4.2	60.3

6/11/24

<u>8.0</u>	<u>8.0</u>	<u>9.6</u>	<u>10.2</u>	<u>10.4</u>		<u>10.1</u>	<u>10.2</u>	<u>8.7</u>
<u>33</u>	<u>27</u>	<u>19</u>	<u>11</u>	<u>8</u>	<u>7.7</u>	<u>12</u>	<u>21</u>	<u>33</u>

<u>9.1</u>	<u>8.3</u>	<u>9.0</u>		<u>9.2</u>	<u>7.2</u>
<u>33</u>	<u>24</u>	<u>10</u>	<u>8.4</u>	<u>14</u>	<u>33</u>

<u>8.1</u>	<u>7.7</u>	<u>6.3</u>	<u>6.0</u>	<u>7.6</u>		<u>7.2</u>	<u>7.4</u>	<u>7.8</u>	<u>7.4</u>	<u>5.8</u>	<u>5.3</u>
<u>33</u>	<u>25</u>	<u>22</u>	<u>17</u>	<u>12</u>	<u>6.7</u>	<u>12</u>	<u>15</u>	<u>17</u>	<u>19</u>	<u>21</u>	<u>33</u>

<u>4.2</u>	<u>3.8</u>	<u>4.3</u>	<u>5.7</u>		<u>5.3</u>	<u>5.2</u>	<u>3.9</u>	<u>4.0</u>
<u>33</u>	<u>24</u>	<u>14</u>	<u>13</u>	<u>4.9</u>	<u>11</u>	<u>17</u>	<u>20</u>	<u>33</u>

<u>3.8</u>	<u>3.2</u>	<u>3.7</u>	<u>5.4</u>	<u>5.3</u>		<u>5.0</u>	<u>5.0</u>	<u>3.5</u>	<u>3.6</u>
<u>33</u>	<u>26</u>	<u>17</u>	<u>14</u>	<u>9</u>	<u>4.6</u>	<u>10</u>	<u>14</u>	<u>19</u>	<u>33</u>

<u>5.7</u>	<u>5.4</u>	<u>5.9</u>	<u>5.7</u>	<u>4.5</u>	<u>4.4</u>		<u>4.5</u>	<u>5.1</u>	<u>4.1</u>	<u>4.2</u>
<u>33</u>	<u>19</u>	<u>18</u>	<u>14</u>	<u>13</u>	<u>9</u>	<u>3.9</u>	<u>10</u>	<u>15</u>	<u>20</u>	<u>33</u>

<u>6.0</u>	<u>5.7</u>	<u>4.4</u>	<u>4.1</u>		<u>4.0</u>	<u>4.8</u>	<u>6.3</u>	<u>6.5</u>
<u>33</u>	<u>14</u>	<u>12</u>	<u>9</u>	<u>3.5</u>	<u>10</u>	<u>13</u>	<u>17</u>	<u>33</u>

<u>5.0</u>	<u>5.5</u>	<u>5.8</u>	<u>3.7</u>	<u>3.7</u>		<u>3.8</u>	<u>4.6</u>	<u>7.7</u>	<u>8.7</u>	<u>8.8</u>
<u>33</u>	<u>27</u>	<u>14</u>	<u>11</u>	<u>9</u>	<u>3.1</u>	<u>10</u>	<u>13</u>	<u>17</u>	<u>25</u>	<u>33</u>

<u>2.8</u>	<u>3.1</u>	<u>3.4</u>	<u>2.2</u>	<u>2.4</u>		<u>2.4</u>	<u>2.8</u>	<u>5.8</u>	<u>6.2</u>
<u>33</u>	<u>25</u>	<u>16</u>	<u>12</u>	<u>9</u>	<u>1.9</u>	<u>10</u>	<u>13</u>	<u>20</u>	<u>33</u>

<u>0.2</u>	<u>0.6</u>	<u>0.6</u>	<u>1.3</u>	<u>0.8</u>	<u>1.2</u>		<u>1.6</u>	<u>2.2</u>	<u>3.7</u>	<u>4.7</u>
<u>33</u>	<u>24</u>	<u>17</u>	<u>14</u>	<u>13</u>	<u>9</u>	<u>0.7</u>	<u>12</u>	<u>16</u>	<u>19</u>	<u>33</u>

Above H.I.

<u>10.2</u>	<u>0.2</u>	<u>4.2</u>	<u>4.3</u>		<u>4.4</u>	<u>5.0</u>	<u>4.6</u>	<u>4.6</u>	<u>4.0</u>	<u>4.1</u>
<u>33</u>	<u>22</u>	<u>17</u>	<u>10</u>	<u>3.7</u>	<u>12</u>	<u>19</u>	<u>21</u>	<u>24</u>	<u>24</u>	<u>33</u>

Above H.I.

Above H.I.

<u>13.0</u>	<u>12.3</u>	<u>3.4</u>	<u>4.4</u>		<u>4.7</u>	<u>3.4</u>	<u>0.0</u>	<u>11.6</u>	<u>14.0</u>	<u>14.0</u>
<u>33</u>	<u>29</u>	<u>20</u>	<u>12</u>	<u>3.7</u>	<u>13</u>	<u>20</u>	<u>25</u>	<u>26</u>	<u>31</u>	<u>33</u>

<u>0.0</u>	<u>0.3</u>	<u>3.8</u>	<u>4.9</u>		<u>5.0</u>	<u>3.0</u>	<u>15.0</u>	<u>14.7</u>	<u>13.8</u>
<u>33</u>	<u>26</u>	<u>20</u>	<u>18</u>	<u>4.2</u>	<u>11</u>	<u>19</u>	<u>29</u>	<u>32</u>	<u>33</u>

Sta.	+	H.I.	-	Red.	Elev.
		964.46			
115				5.3	59.2
+29				5.9	58.6
T.P.	5.22	960.34	7.32	955.14	
116				3.2	57.2
117				4.4	56.0
+74				4.8	55.6
118				4.9	55.5
+35				5.2	55.2
+74				5.5	54.9
119				5.8	54.6
+29				6.5	53.9
120				7.2	53.2
+25				7.7	52.7
+43				8.6	51.8
T.P.	5.64	956.61	9.39	950.97	

6/11/23

1.8 2.5 5.2 5.4 6.0 5.8 6.0 6.1 6.0 6.6 7.1 7.0
33 26 22 19 18 12 5.3 10 14 18 20 28 33

6.0 6.7 6.5 6.3 6.6 7.1 7.5 12.1 13.0
33 18 15 10 5.9 11 13 18 23 33

7.9 7.9 8.4 3.5 3.9 15.6 16.0
33 26 21 11 3.2 11 33 36

8.7 8.8 6.0 5.0 5.0 15.3 15.5
33 19 15 12 4.4 11 31 33

8.7 8.8 5.7 5.3 5.5 6.0 7.4 7.8 8.5
33 20 15 11 4.8 11 14 17 29 33

8.3 8.6 7.6 5.8 5.4 8.9
33 26 17 14 4.9 10 33

5.5 5.5 6.2 5.8 5.8 6.3 6.1 3.7 5.6
33 20 17 12 5.2 10 13 14 20 33

2.3 2.6 2.0 2.5 5.8 6.2 6.6 6.2 5.9 1.5 2.0
33 29 27 22 17 13 5.5 13 15 16 23 33

1.0 1.6 6.0 6.2 6.5 6.6 3.4 3.1 3.4
33 23 17 12 5.8 12 17 23 30 33

0.0 0.0 6.3 6.6 6.9 7.0 7.0 5.6 4.9
33 28 24 17 11 6.5 11 19 23 33

4.0 3.2 3.5 7.7 7.6 7.6 7.3 6.7 2.4 2.4
33 26 22 17 12 7.2 9 12 15 22 33

6.6 4.5 4.7 8.1 8.4 8.0 7.6 1.4 1.8
33 25 23 16 13 7.7 9 12 22 33

11.5 10.2 9.1 9.0 9.2 8.9 8.3 8.1 6.9 6.6 6.6
33 20 14 12 8.6 9 11 12 14 14 28 33

Sta. + H.I. - Red. Elev.
956.61

121 5.5 51.1

B.M. 8.57 947.02

+38 6.0 50.6

122 4.5 50.1

123 5.2 51.4

+46 4.2 52.4

+70 3.5 53.1

124 2.6 54.0

+36 0.9 55.7

T. P. 12.31 968.52 0.40 956.21 956.27

125 11.4 57.1

+34 10.3 58.2

126 8.4 59.9

+50 4.6 61.9

T. P. 10.47 974.83 4.34 964.14

127 11.0 63.8

2/11/25

9.1 8.4 9.0 8.7 6.2 6.0 6.0 6.4 7.2 7.5
33 24 24 20 14 11 5.5 9 13 15 33

Spk. in T. 12 30 17.5 5.4 1.21 + 6.5

12.1 7.6 7.0 8.9 9.3 9.1 8.0 6.6 6.5 6.4 7.1 8.4 8.4 8.5 9.0
33 27 24 24 23 20 17 14 11 6.0 9 12 15 19 23 33

16.0 15.8 8.3 7.0 7.5 15.1 15.3
33 27 17 13 6.5 11 24 33

11.3 10.5 10.0 5.9 5.8 6.0 6.4 7.5 7.6 7.3 7.4
33 26 21 13 12 5.2 11 13 15 22 28 33

Above H.I.

6.6 5.5 4.9 4.6 5.5 5.0 4.6 4.4 4.9 + 2.6 + 2.6
33 38 27 24 21 14 4.2 9 11 17 28 33

3.0 1.7 4.5 4.1 3.8 3.9 + 4.5 + 4.5
33 25 19 12 3.5 9 18 30 33

Above H.I.

+ 2.8 7.1 1.6 2.3 3.6 3.2 3.0 2.8 3.6 3.6 + 2.4 + 2.4
33 27 22 20 18 12 2.6 10 14 17 19 28 33

Above H.I.

+ 0.1 + 0.5 0.0 1.6 1.5 1.2 0.8 + 2.0 + 3.4
33 24 20 17 12 0.9 9 12 25 33

8.4 7.2 11.8 12.0 11.9 12.3 11.6 5.0 4.1 4.6
33 24 17 12 11.4 10 14 17 25 29 33

12.0 9.6 9.6 10.9 10.9 11.0 11.0 10.5 2.0 1.5
33 25 20 14 12 10.3 10 13 16 26 33

13.8 12.3 10.0 9.1 9.2 9.3 5.7 4.6
33 23 14 10 8.6 9 14 24 33

9.2 7.7 7.3 7.1 7.0 7.4 2.3 1.6
33 14 11 6.4 10 14 14 24 33

11.5 11.2 11.5 11.6 11.3 11.9 11.9 6.8 5.7
33 21 11 11.0 10 14 15 17 24 33

Sta. + H.I. - Ref. Elev.

974.83

+50

7.5

65.3

128

8.2

66.6

+50

7.1

67.7

129

6.2

68.6

+50

5.4

69.4

130

5.1

69.7

+50

4.8

70.0

131

4.3

70.5

+50

3.6

71.2

132

2.9

71.9

+50

2.5

72.3

133

2.1

72.7

T.P.

8.24

981.22

1.85

972.98

+35

7.4

73.6

6/11/26

<u>9.8</u>	<u>9.2</u>	<u>11.5</u>	<u>11.5</u>	<u>10.9</u>	<u>10.8</u>	<u>10.0</u>		<u>9.8</u>	<u>9.9</u>	<u>10.3</u>	<u>10.6</u>	<u>6.3</u>	<u>5.5</u>
33	25	22	18	16	14	11	9.5	10	13	14	16	22	33

<u>8.9</u>	<u>8.2</u>	<u>10.1</u>	<u>10.8</u>	<u>8.7</u>		<u>8.5</u>	<u>8.9</u>	<u>6.2</u>	<u>6.1</u>
33	24	21	16	10	8.2	9	15	20	33

<u>7.2</u>	<u>6.5</u>	<u>10.0</u>	<u>7.9</u>	<u>7.8</u>		<u>7.1</u>	<u>7.1</u>	<u>6.9</u>	<u>4.6</u>	<u>4.1</u>
33	26	21	16	11	7.1	7	14	17	21	33

<u>5.2</u>	<u>5.2</u>	<u>7.0</u>	<u>9.1</u>	<u>8.3</u>	<u>7.9</u>	<u>6.6</u>		<u>6.6</u>	<u>6.2</u>	<u>3.2</u>	<u>2.9</u>
33	32	25	21	19	15	11	6.2	11	15	21	33

<u>4.8</u>	<u>4.8</u>	<u>8.4</u>	<u>8.2</u>	<u>7.2</u>	<u>6.5</u>	<u>6.0</u>		<u>5.9</u>	<u>6.8</u>	<u>3.0</u>	<u>2.0</u>
33	31	24	21	18	15	11	5.4	12	15	19	33

<u>6.3</u>	<u>6.2</u>	<u>6.5</u>	<u>6.9</u>	<u>6.9</u>	<u>5.8</u>		<u>5.4</u>	<u>5.8</u>	<u>4.0</u>	<u>3.7</u>
33	25	22	21	17	11	5.1	10	16	19	33

<u>7.6</u>	<u>7.4</u>	<u>7.2</u>	<u>6.6</u>	<u>5.3</u>		<u>5.1</u>	<u>5.0</u>	<u>5.8</u>	<u>5.2</u>
33	29	23	21	11	4.8	10	15	16	33

<u>7.4</u>	<u>7.0</u>	<u>5.0</u>	<u>4.6</u>		<u>4.8</u>	<u>4.7</u>	<u>5.7</u>	<u>5.7</u>
33	24	13	9	4.3	10	14	17	33

<u>7.1</u>	<u>6.6</u>	<u>6.6</u>	<u>6.6</u>	<u>4.3</u>	<u>4.1</u>		<u>4.0</u>	<u>4.4</u>	<u>4.9</u>	<u>4.4</u>
33	27	23	19	13	10	3.6	10	14	16	33

<u>5.2</u>	<u>5.1</u>	<u>5.6</u>	<u>5.5</u>	<u>3.7</u>	<u>3.2</u>		<u>3.4</u>	<u>4.4</u>	<u>4.1</u>	<u>4.2</u>	<u>4.4</u>
33	26	23	17	14	10	2.9	13	14	22	25	33

<u>5.4</u>	<u>4.8</u>	<u>5.1</u>	<u>3.0</u>	<u>3.0</u>		<u>3.1</u>	<u>3.0</u>	<u>3.1</u>	<u>2.6</u>	<u>3.1</u>
33	23	19	14	9	2.5	10	12	20	22	33

<u>4.0</u>	<u>3.2</u>	<u>2.4</u>		<u>2.4</u>	<u>2.0</u>	<u>1.0</u>	<u>0.3</u>	<u>0.2</u>
33	20	11	2.1	11	13	15	22	33

<u>9.7</u>	<u>9.2</u>	<u>8.3</u>	<u>7.9</u>	<u>8.3</u>		<u>7.8</u>	<u>6.3</u>	<u>5.4</u>	<u>5.5</u>
33	19	16	14	12	7.4	10	14	22	33

Sta. + H. I. - Rod. Elev.
981.22

185 7.1 74.1

134 7.0 74.2

+60 6.7 74.5

135 6.7 74.5

+44 6.5 74.7

136 6.4 74.8

+12 Cross Drain

137 5.2 76.0

+44 4.4 76.8

T.I. 12.57 987.89 3.90 777.32

138 12.1 77.8

+50 10.9 79.0

139 9.5 80.4

+50 8.7 81.2

$\frac{7.4}{33}$	$\frac{7.3}{25}$	$\frac{6.9}{16}$	$\frac{8.2}{14}$	$\frac{7.7}{11}$	7.1	$\frac{7.9}{11}$	$\frac{7.5}{14}$	$\frac{7.6}{22}$	$\frac{7.2}{33}$
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$\frac{6.3}{33}$	$\frac{6.1}{28}$	$\frac{5.9}{23}$	$\frac{6.7}{21}$	$\frac{6.9}{16}$	$\frac{7.8}{13}$	7.0	$\frac{7.6}{9}$	$\frac{7.7}{13}$	$\frac{6.4}{17}$	$\frac{6.1}{22}$	$\frac{5.7}{33}$
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above H.I.

$\frac{5.0}{33}$	$\frac{4.8}{24}$	$\frac{5.4}{22}$	$\frac{5.1}{16}$	$\frac{6.7}{14}$	$\frac{7.3}{11}$	6.7	$\frac{7.0}{11}$	$\frac{6.7}{13}$	$\frac{5.8}{15}$	$\frac{5.0}{17}$	$\frac{7.1}{24}$	$\frac{7.2}{33}$
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$\frac{5.5}{33}$	$\frac{6.6}{22}$	$\frac{7.0}{20}$	$\frac{7.7}{17}$	$\frac{7.8}{15}$	$\frac{7.5}{11}$	6.7	$\frac{7.4}{10}$	$\frac{7.0}{18}$	$\frac{2.6}{25}$	$\frac{2.6}{33}$
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$\frac{12.0}{33}$	$\frac{12.3}{27}$	$\frac{11.4}{19}$	$\frac{7.1}{11}$	6.5	$\frac{6.8}{10}$	$\frac{7.3}{15}$	$\frac{7.7}{14}$	$\frac{7.1}{27}$	$\frac{6.8}{33}$
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$\frac{12.5}{33}$	$\frac{12.8}{22}$	$\frac{7.1}{11}$	6.4	$\frac{7.3}{12}$	$\frac{12.0}{22}$	$\frac{12.0}{26}$	$\frac{12.0}{33}$
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$\frac{12.8}{23}$

$\frac{13.0}{18}$

$\frac{6.7}{33}$	$\frac{6.7}{29}$	$\frac{8.4}{22}$	$\frac{8.0}{17}$	$\frac{6.5}{15}$	$\frac{5.7}{12}$	5.2	$\frac{5.9}{8}$	$\frac{5.6}{10}$	$\frac{7.1}{14}$	$\frac{8.7}{25}$	$\frac{8.5}{33}$
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$\frac{5.3}{33}$	$\frac{5.1}{27}$	$\frac{6.0}{17}$	$\frac{4.8}{14}$	$\frac{4.9}{10}$	4.4	$\frac{5.0}{9}$	$\frac{5.7}{13}$	$\frac{5.6}{22}$	$\frac{5.7}{33}$
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$\frac{17.4}{33}$	$\frac{17.3}{28}$	$\frac{16.7}{19}$	$\frac{12.6}{11}$	12.1	$\frac{12.6}{9}$	$\frac{12.4}{10}$	$\frac{11.9}{21}$	$\frac{11.7}{23}$	$\frac{11.0}{33}$
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$\frac{16.5}{33}$	$\frac{15.5}{27}$	$\frac{14.6}{19}$	$\frac{11.4}{11}$	10.9	$\frac{11.4}{11}$	$\frac{11.0}{15}$	$\frac{10.2}{17}$	$\frac{9.2}{22}$	$\frac{7.7}{33}$
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$\frac{14.8}{33}$	$\frac{13.4}{26}$	$\frac{12.5}{18}$	$\frac{10.8}{13}$	$\frac{10.3}{12}$	7.5	$\frac{9.9}{9}$	$\frac{10.1}{14}$	$\frac{9.3}{21}$	$\frac{9.6}{23}$	$\frac{8.6}{33}$
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$\frac{12.3}{33}$	$\frac{11.6}{26}$	$\frac{11.1}{16}$	$\frac{9.0}{11}$	8.7	$\frac{9.6}{8}$	$\frac{9.2}{10}$	$\frac{11.5}{17}$	$\frac{11.7}{25}$	$\frac{11.4}{33}$
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Sta. + H.I. - Ref. Elev

989.89

140

7.7

82.2

+50

6.7

83.2

141

5.4

84.5

T.P.

7.70

994.78

2.81

987.08

+67

8.2

86.6

142

7.8

87.0

+60

7.0

87.8

143

6.4

88.4

+75

5.5

89.3

144

5.3

89.5

+68

5.1

89.7

145

4.8

90.0

+50

4.4

90.4

B.M.

3.65

994.82

3.65

991.13

991.17

11.1 10.7 7.7 8.4 8.3 7.6 7.6 7.4 7.5
33 27 17 12 7.7 12 14 19 21 33

8.6 7.7 7.3 7.0 7.0 7.3 7.0 6.6 7.1 5.6 4.1 4.5
33 24 17 17 11 4.7 8 12 14 17 21 23 33

5.5 4.6 4.3 5.7 6.0 5.7 5.7 5.0 2.2 2.1 2.2
33 26 21 18 12 5.4 8 12 15 20 25 33

6.2 5.4 5.4 8.0 8.7 7.0 8.5 8.0 2.4 2.7 2.2
33 27 21 18 12 8.2 11 13 14 24 27 33

4.8 4.6 4.9 7.8 8.3 8.4 8.1 3.0 3.2 3.2
33 27 22 17 13 7.8 8 14 22 25 33

5.8 5.9 6.3 7.1 7.4 7.6 7.5 6.8 6.7 7.1 6.8
33 26 20 18 12 7.0 10 15 17 21 27 33

5.6 5.6 6.2 6.7 6.7 6.8 6.8 2.9 8.0 7.7
33 24 19 12 4.4 9 12 14 21 33

2.2 2.1 3.3 3.5 5.9 5.8 6.1 6.3 4.9 5.4 5.3
33 28 25 23 18 12 5.5 11 17 20 23 33

2.1 2.5 3.7 3.8 5.5 5.5 5.7 5.9 6.2 5.2 5.8 6.1
33 28 26 23 17 12 5.3 7 12 16 18 24 33

3.2 3.4 4.5 5.1 5.1 5.2 7.0 7.0 10.0 10.0
33 27 25 21 12 5.1 9 13 17 25 33

4.0 4.1 4.7 4.7 5.0 5.3 5.6 6.7 7.4 8.4 8.6
33 27 20 14 11 4.8 8 13 14 20 25 33

2.4 2.5 3.2 4.1 4.1 4.5 5.0 4.7 4.8 6.3
33 27 22 19 15 11 4.4 7 9 13 33

SpK in T.P.H. 18329 on Co. Rd. "D" 1 mile W. of F.C. Line #19.

SpK in T.P. Rt. Sta. 145+70.

Sta. + H.I. - Rod. Elev.

994.82

146

4.0

90.8

+70

3.2

91.6

147

3.6

91.2

+32

3.5

91.2

148

3.6

91.2

T.P.

5.41

996.39 ✓

3.84

990.98 ✓

+30

5.1

91.3

149

5.0

91.4

150

4.4

91.8

+54

4.8

91.6

151

4.9

91.5

152

3.1

93.3

+50

1.9

94.5

T.P.

9.92

1004.23 ✓

2.08

994.31 ✓

153

8.5

95.7

2.5 2.6 3.1 3.7 3.8 4.0 4.5 4.8 6.2 6.3
33 28 22 19 12 10 4.0 8 12 23 33

3.7 3.2 3.6 3.6 3.6 2.2 1.8 2.5
33 27 11 3.2 10 15 18 21 33

5.0 3.9 3.7 4.1 4.1 3.1 2.7 3.5
33 19 11 3.6 10 15 17 22 33

6.4 6.2 4.2 4.2 4.7 4.0 4.2 4.0
33 24 11 3.6 9 14 22 24 33

5.1 5.1 3.9 4.0 5.6 4.1 3.7 1.7
33 24 9 3.6 7 11 13 22 33

5.6 6.0 5.7 5.5 5.1 6.8 6.3 6.3
33 23 12 5.1 7 11 17 23 33

3.7 5.5 5.5 5.5 5.3 8.0 9.5 9.6
33 21 12 5.0 7 12 17 23 33

2.1 2.5 4.6 4.8 5.1 5.6 5.8 5.9
33 27 17 11 4.6 8 19 23 33

4.6 4.8 5.5 5.2 5.2 5.6 5.0 7.5 8.4 8.4
33 27 21 14 11 4.8 7 12 17 24 33

8.0 7.8 6.8 6.0 5.3 5.3 5.6 7.2 10.2 10.3
33 24 22 15 14 12 4.9 11 19 26 33

6.4 6.2 5.4 4.9 4.9 5.6 3.8 3.6 4.3 4.4 4.4
33 28 26 23 17 13 11 3.1 8 21 27 33

3.0 3.0 2.4 3.0 2.4 2.1 2.4 2.4 2.3 0.9 0.2 0.2
33 27 25 18 16 14 12 1.9 8 14 21 25 33

7.4 7.4 9.2 8.7 8.5 9.0 8.5 9.1 9.9 10.1 9.3
33 27 19 16 14 12 6 5.5 8 20 26 33

Sta.	T	H.I.	-	Red.	Lev.
		1004.23			
+41				7.9	96.3
+53				7.7	96.5
154				7.1	97.1
155				6.3	97.9
156				5.2	99.0
157				3.2	1001.0
T.P.	5.40	✓ 1008.92	0.71	✓ 1003.52	
158				4.9	04.0
B.M.	10.99	✓ 1015.35	4.56	✓ 1014.36	
+50				9.8	05.6
159				8.3	07.1
+50				6.4	9.0
160				4.2	11.2
+50				2.3	13.1
T.P.	10.09	✓ 1024.75	0.67	✓ 1014.66	
161				9.5	15.3

6/12/25

4.7 6.4 8.5 7.6 8.4 7.9 8.9 9.2 9.1
 38 35 29 14 12 5 7.9 10 21 33

4.5 5.7 6.4 8.1 8.7 8.0 8.2 7.7 8.5 8.4 6.8 6.8 7.5 8.3
 34 31 25 20 17 13 12 5 7.7 8 12 15 31 27 33

6.3 6.4 7.1 7.7 7.2 7.4 7.1 7.7 7.5 8.3 9.9 10.2
 33 26 21 19 12 11 5 7.1 8 10 20 28 33

6.4 6.4 6.5 6.8 6.8 7.0 9.4 9.8 10.2
 33 30 12 11 6.3 8 12 17 22 33

5.5 5.6 5.2 5.6 5.7 6.1 7.9 7.8 8.3
 33 17 15 11 5.3 7 12 17 21 33

4.1 4.4 4.3 3.6 3.7 3.7 4.3 5.6 6.2 6.5
 33 23 16 14 12 32 7 12 16 24 33

5.8 5.7 5.8 5.1 5.2 5.3 5.1 5.2 6.0 6.2 5.5 6.4
 33 25 17 14 12 4.9 6 8 11 14 17 27 33

Sp. N. in T.P. R+5+9.152+100

10.5 10.1 10.3 10.1 10.2 10.5 9.6 10.0 9.6 9.3
 33 21 18 13 7.8 7 11 14 14 23 33

8.3 8.0 8.5 8.2 8.4 8.7 8.7 8.5 8.4 7.9 8.2
 39 25 23 14 12 8.3 8 10 21 26 28 33

6.0 5.5 6.4 6.3 6.5 6.8 7.0 6.8 6.9 6.3 6.9
 33 25 23 15 14 6.4 11 10 13 24 26 33

4.3 3.9 4.1 4.4 4.5 4.7 3.8 3.4 4.0
 33 27 16 15 4.2 7 11 12 23 33

2.6 2.2 2.7 2.4 2.5 2.6 2.6 2.5 0.6 0.7
 33 25 23 15 14 2.3 8 11 13 15 23

9.1 8.5 9.4 9.8 9.5 10.0 10.0 9.8 9.8 7.1 6.5 7.0
 33 26 23 20 18 15 7.5 7 9 13 15 24 33

Sta.	T	H. I.	-	Red.	Elev.
		1024.75			
+50				7.7	17.1
162				6.2	18.6
+50				4.9	19.9
163				3.4	21.4
+50				2.2	22.6
+58.				2.0	22.8
+80				1.5	23.3
T. P.	11.01	1034.11	165	1023.10	
164				10.3	23.8
+50				9.2	24.9
165				8.4	25.7
166				5.4	28.7
+64				3.8	30.3
167				3.5	30.6

6/15/26

$\frac{5.3}{33} \frac{5.2}{28} \frac{4.4}{26} \frac{4.5}{23} \frac{7.6}{19} \frac{8.2}{14} \frac{8.7}{7.7} \frac{8.1}{8} \frac{8.1}{11} \frac{7.9}{13} \frac{6.0}{16} \frac{5.6}{23} \frac{6.4}{33}$

$\frac{2.3}{33} \frac{2.0}{26} \frac{3.0}{20} \frac{5.8}{18} \frac{6.7}{14} \frac{6.2}{6.2} \frac{6.6}{7} \frac{6.3}{9} \frac{6.7}{12} \frac{6.4}{14} \frac{6.0}{15} \frac{7.6}{33}$

$\frac{1.9}{33} \frac{2.6}{25} \frac{3.6}{17} \frac{4.9}{13} \frac{5.2}{11} \frac{4.9}{4.9} \frac{5.3}{7} \frac{5.0}{10} \frac{5.1}{14} \frac{4.2}{22} \frac{5.5}{33}$

Above H.I.

$\frac{4.5}{33} \frac{4.3}{27} \frac{3.6}{25} \frac{3.9}{11} \frac{3.4}{3.4} \frac{3.8}{8} \frac{3.8}{11} \frac{3.0}{15} \frac{+1.6}{18} \frac{+1.9}{25} \frac{+1.8}{33}$

Above H.I.

$\frac{4.9}{33} \frac{4.5}{27} \frac{2.5}{19} \frac{2.6}{13} \frac{2.2}{2.2} \frac{2.5}{8} \frac{2.0}{12} \frac{+3.2}{18} \frac{+3.7}{33}$

$\frac{4.9}{33} \frac{4.7}{30} \frac{3.0}{21} \frac{2.5}{13} \frac{2.0}{2.0} \frac{2.4}{9} \frac{2.0}{15} \frac{0.6}{33}$

$\frac{5.1}{33} \frac{4.6}{29} \frac{2.6}{19} \frac{2.2}{13} \frac{1.5}{1.5} \frac{1.9}{8} \frac{2.0}{14} \frac{1.3}{19} \frac{0.2}{23} \frac{0.2}{26} \frac{2.0}{33}$

$\frac{14.5}{33} \frac{12.9}{21} \frac{11.1}{14} \frac{10.9}{12} \frac{10.3}{10.3} \frac{10.7}{8} \frac{10.5}{14} \frac{10.5}{18} \frac{11.5}{20} \frac{13.7}{33}$

$\frac{12.5}{33} \frac{11.6}{24} \frac{9.9}{15} \frac{9.2}{9.2} \frac{9.9}{9} \frac{13.6}{15} \frac{19.3}{33}$

$\frac{10.4}{33} \frac{9.8}{23} \frac{8.8}{14} \frac{8.4}{8.4} \frac{9.0}{8} \frac{9.5}{12} \frac{12.0}{18} \frac{16.0}{33}$

$\frac{6.2}{33} \frac{5.6}{28} \frac{5.8}{21} \frac{5.9}{12} \frac{5.4}{5.4} \frac{5.9}{8} \frac{6.8}{12} \frac{13.1}{21} \frac{17.5}{33}$

Above H.I.

$\frac{0.4}{33} \frac{0.4}{29} \frac{+0.5}{26} \frac{3.4}{19} \frac{4.1}{15} \frac{4.0}{12} \frac{3.8}{3.8} \frac{4.3}{9} \frac{4.7}{10} \frac{4.6}{15} \frac{8.5}{24} \frac{12.3}{33}$

Above H.I.

$\frac{+2.6}{33} \frac{+3.0}{30} \frac{2.6}{20} \frac{3.8}{13} \frac{3.5}{3.5} \frac{4.2}{8} \frac{4.2}{13} \frac{2.4}{16} \frac{2.9}{19} \frac{4.9}{25} \frac{8.0}{33}$

Sta.	T	H.I.	-	Red.	Elev.
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1034.11

+22				3.6	30.5
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+42				3.7	30.4
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+69				4.2	29.9
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168				4.8	29.3
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+09				5.1	29.0
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T.P.	1.34	1032.32	3.15	1030.96	
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+50				4.5	27.8
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169				5.8	26.5
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+34				6.7	25.4
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T.P.	2.22	1024.60	9.94	1022.38	
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170				13	23.3
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171				3.8	20.8
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B.M.	8.44	1024.62	8.44	1016.14	1016.16
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172				5.8	18.8
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+50				6.6	18.0
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Above H.I.

$\frac{+4.1}{58}$	$\frac{+0.7}{33}$	$\frac{0.2}{28}$	$\frac{2.5}{21}$	$\frac{4.0}{12}$	3.6	$\frac{4.1}{8}$	$\frac{3.7}{13}$	$\frac{1.3}{18}$	$\frac{1.4}{21}$	$\frac{4.1}{28}$	$\frac{5.3}{33}$
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Above H.I.

$\frac{+4.7}{48}$	$\frac{5.0}{35}$	$\frac{6.6}{20}$	$\frac{4.1}{14}$	$\frac{4.2}{11}$	3.7	$\frac{4.3}{9}$	$\frac{4.1}{14}$	$\frac{0.3}{20}$	$\frac{1.3}{23}$	$\frac{2.0}{26}$	$\frac{3.0}{27}$	$\frac{4.0}{33}$
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Above H.I.

$\frac{+10.0}{52}$	$\frac{+10.1}{50}$	$\frac{+2.0}{39}$	$\frac{0.4}{30}$	$\frac{3.4}{20}$	$\frac{4.5}{11}$	4.2	$\frac{4.9}{9}$	$\frac{4.6}{16}$	$\frac{0.4}{23}$	$\frac{1.9}{29}$	$\frac{2.3}{33}$
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Above H.I.

$\frac{+12.4}{58}$	$\frac{+12.6}{54}$	$\frac{+6.3}{42}$	$\frac{0.5}{28}$	$\frac{1.6}{26}$	$\frac{4.3}{18}$	$\frac{5.3}{12}$	4.8	$\frac{5.6}{10}$	$\frac{5.2}{18}$	$\frac{+0.1}{28}$	$\frac{+0.5}{32}$	$\frac{0.0}{33}$
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Above H.I.

$\frac{+15.6}{54}$	$\frac{+15.7}{52}$	$\frac{+5.0}{38}$	$\frac{0.7}{29}$	$\frac{3.5}{22}$	$\frac{5.5}{12}$	5.1	$\frac{5.9}{9}$	$\frac{6.0}{12}$	$\frac{5.5}{15}$	$\frac{3.9}{25}$	$\frac{0.1}{32}$	$\frac{+0.1}{33}$
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Above H.I.

Above H.I.

$\frac{+15.0}{52}$	$\frac{+15.0}{49}$	$\frac{+11.0}{47}$	$\frac{0.2}{30}$	$\frac{3.8}{23}$	$\frac{4.9}{11}$	4.5	$\frac{5.1}{10}$	$\frac{5.0}{14}$	$\frac{1.8}{24}$	$\frac{0.0}{26}$	$\frac{+3.3}{31}$	$\frac{+4.0}{33}$
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Above H.I.

$\frac{+0.2}{33}$	$\frac{+0.7}{29}$	$\frac{1.4}{17}$	$\frac{5.3}{19}$	$\frac{6.4}{11}$	5.8	$\frac{6.4}{9}$	$\frac{5.4}{13}$	$\frac{+2.1}{30}$	$\frac{+2.1}{33}$
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$\frac{10.1}{33}$	$\frac{10.7}{24}$	$\frac{7.7}{15}$	$\frac{7.2}{10}$	6.9	$\frac{7.5}{9}$	$\frac{7.1}{14}$	$\frac{8.4}{24}$	$\frac{7.9}{33}$
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$\frac{7.4}{33}$	$\frac{8.1}{23}$	$\frac{1.9}{11}$	$\frac{1.7}{9}$	1.3	$\frac{2.0}{9}$	$\frac{2.1}{12}$	$\frac{5.2}{19}$	$\frac{6.3}{25}$	$\frac{5.0}{33}$
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$\frac{13.2}{33}$	$\frac{12.4}{24}$	$\frac{4.3}{11}$	$\frac{4.4}{9}$	3.8	$\frac{4.5}{8}$	$\frac{4.4}{11}$	$\frac{10.0}{20}$	$\frac{10.7}{25}$	$\frac{11.0}{33}$
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SpX. in T.P. #18311 on Co. Rd. "D" 1/2 Mile W. of East Co. Line #20.

SpX. in T.P. #18311 Rt. Sta. 171 + 30.

$\frac{12.4}{33}$	$\frac{11.4}{22}$	$\frac{6.3}{12}$	5.8	$\frac{6.4}{7}$	$\frac{6.4}{9}$	$\frac{12.7}{21}$	$\frac{14.3}{33}$
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$\frac{8.7}{33}$	$\frac{10.1}{18}$	$\frac{7.5}{13}$	$\frac{7.3}{10}$	6.4	$\frac{7.0}{9}$	$\frac{12.0}{19}$	$\frac{13.7}{24}$	$\frac{13.7}{33}$
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Sta. + H.I. - Rod. Elev

1024.62

173 7.1 17.5

+50 7.4 17.2

174 7.4 17.2

T.P. 8.37 1025.23 ✓ 7.74 1016.84 ✓

+50 8.0 17.2

175 8.0 17.2

+50 8.4 16.8

176 9.0 16.2

+50 9.2 16.0

177 8.9 16.3

+40 8.2 17.0

178 6.6 18.6

+50 5.2 20.0

179 4.2 21.0

<u>5.7</u>	<u>6.6</u>	<u>8.0</u>	<u>9.1</u>	<u>9.1</u>	<u>7.7</u>	<u>7.7</u>		<u>7.7</u>	<u>12.6</u>	<u>13.3</u>	<u>13.6</u>
<u>33</u>	<u>27</u>	<u>22</u>	<u>19</u>	<u>15</u>	<u>13</u>	<u>10</u>	7.1	<u>10</u>	<u>18</u>	<u>23</u>	<u>34</u>

<u>2.9</u>	<u>3.4</u>	<u>4.5</u>	<u>7.9</u>	<u>8.0</u>	<u>7.8</u>	<u>8.0</u>		<u>8.0</u>	<u>8.2</u>	<u>10.7</u>	<u>12.7</u>	<u>13.3</u>	<u>13.4</u>
<u>33</u>	<u>24</u>	<u>22</u>	<u>17</u>	<u>15</u>	<u>14</u>	<u>9</u>	7.4	<u>9</u>	<u>12</u>	<u>14</u>	<u>21</u>	<u>25</u>	<u>35</u>

<u>1.0</u>	<u>1.0</u>	<u>3.5</u>	<u>7.7</u>	<u>8.0</u>		<u>8.0</u>	<u>8.0</u>	<u>11.0</u>	<u>12.8</u>	<u>13.3</u>
<u>33</u>	<u>27</u>	<u>20</u>	<u>15</u>	<u>9</u>	7.4	<u>9</u>	<u>12</u>	<u>17</u>	<u>25</u>	<u>33</u>

<u>6.8</u>	<u>6.8</u>	<u>7.9</u>	<u>8.4</u>		<u>8.4</u>	<u>8.9</u>	<u>8.8</u>	<u>10.5</u>	<u>10.5</u>	<u>9.7</u>
<u>33</u>	<u>24</u>	<u>18</u>	<u>10</u>	8.0	<u>10</u>	<u>14</u>	<u>21</u>	<u>23</u>	<u>30</u>	<u>33</u>

<u>12.0</u>	<u>11.0</u>	<u>8.6</u>	<u>8.4</u>	<u>8.5</u>		<u>8.4</u>	<u>8.9</u>	<u>8.8</u>
<u>33</u>	<u>19</u>	<u>12</u>	<u>10</u>	<u>7</u>	8.0	<u>12</u>	<u>25</u>	<u>33</u>

<u>12.3</u>	<u>11.2</u>	<u>9.2</u>	<u>9.0</u>		<u>8.6</u>	<u>9.6</u>	<u>9.2</u>	<u>8.9</u>
<u>33</u>	<u>14</u>	<u>10</u>	<u>8</u>	8.4	<u>12</u>	<u>18</u>	<u>26</u>	<u>33</u>

<u>12.2</u>	<u>11.9</u>	<u>11.9</u>	<u>10.2</u>	<u>9.7</u>	<u>9.5</u>		<u>9.5</u>	<u>9.8</u>	<u>9.9</u>	<u>10.0</u>
<u>33</u>	<u>25</u>	<u>17</u>	<u>13</u>	<u>10</u>	<u>7</u>	9.0	<u>11</u>	<u>16</u>	<u>26</u>	<u>33</u>

<u>12.2</u>	<u>11.8</u>	<u>11.8</u>	<u>10.1</u>	<u>9.6</u>		<u>9.7</u>	<u>9.7</u>	<u>10.9</u>	<u>10.7</u>
<u>33</u>	<u>25</u>	<u>17</u>	<u>13</u>	<u>8</u>	9.2	<u>10</u>	<u>12</u>	<u>17</u>	<u>33</u>

<u>12.2</u>	<u>11.8</u>	<u>11.6</u>	<u>10.3</u>	<u>9.5</u>		<u>9.1</u>	<u>10.0</u>	<u>10.4</u>	<u>10.3</u>
<u>33</u>	<u>25</u>	<u>17</u>	<u>14</u>	<u>10</u>	8.9	<u>8</u>	<u>14</u>	<u>26</u>	<u>33</u>

<u>12.1</u>	<u>11.8</u>	<u>10.9</u>	<u>9.8</u>	<u>8.9</u>		<u>8.8</u>	<u>9.0</u>	<u>11.1</u>	<u>11.5</u>	<u>10.1</u>	<u>9.9</u>
<u>33</u>	<u>24</u>	<u>16</u>	<u>14</u>	<u>8</u>	8.2	<u>10</u>	<u>13</u>	<u>20</u>	<u>25</u>	<u>28</u>	<u>33</u>

<u>12.5</u>	<u>11.6</u>	<u>10.5</u>	<u>7.6</u>		<u>6.8</u>	<u>6.9</u>	<u>7.4</u>	<u>7.2</u>	<u>5.5</u>	<u>5.2</u>
<u>33</u>	<u>25</u>	<u>16</u>	<u>11</u>	6.6	<u>10</u>	<u>13</u>	<u>15</u>	<u>20</u>	<u>28</u>	<u>33</u>

<u>10.9</u>	<u>10.9</u>	<u>10.2</u>	<u>7.2</u>	<u>6.2</u>	<u>6.0</u>		<u>5.5</u>	<u>5.0</u>	<u>5.7</u>	<u>5.4</u>	<u>6.8</u>	<u>0.0</u>
<u>33</u>	<u>30</u>	<u>27</u>	<u>21</u>	<u>12</u>	<u>10</u>	5.2	<u>11</u>	<u>16</u>	<u>18</u>	<u>22</u>	<u>28</u>	<u>33</u>

above H.S.

<u>8.0</u>	<u>7.2</u>	<u>5.8</u>	<u>5.0</u>	<u>4.5</u>	<u>4.7</u>		<u>4.5</u>	<u>4.3</u>	<u>3.7</u>	<u>2.5</u>	<u>16.6</u>	<u>16.6</u>
<u>33</u>	<u>28</u>	<u>22</u>	<u>18</u>	<u>11</u>	<u>10</u>	4.2	<u>10</u>	<u>14</u>	<u>14</u>	<u>22</u>	<u>33</u>	<u>35</u>

Sta. + H.I. - Rod. Flex.

1025.23

+50 3.4 21.8

180 3.5 21.7

+50 3.4 21.8

T.P. 4.39 1025.71 3.91 1021.32

+80 4.2 21.5

181 4.5 21.2

+71 Cross Drain

182 6.9 18.8

183 7.2 18.5

184 5.9 19.8

185 3.2 22.5

T.P. 9.83 1033.43 2.11 1023.60

+40 9.1 24.3

184 8.3 25.1

+30 7.9 25.5

6/15/20

Above H.I.

Spove H.I.

<u>0.3</u>	<u>+0.2</u>	<u>33</u>	<u>40</u>	<u>3.4</u>	<u>2.9</u>	<u>0.0</u>	<u>+8.5</u>	<u>+12.5</u>	<u>+14.6</u>	
33	30	23	10	3.4	10	11	23	34	37	42

33 30 23 10 3.4 10 11 23 34 37 42

$\frac{+4.3}{.98}$	$\frac{+5.3}{.34}$	$\frac{1.0}{.24}$	$\frac{1.7}{.32}$	$\frac{2.7}{16}$	$\frac{3.5}{13}$	$\frac{3.8}{9}$	3.5	$\frac{3.7}{10}$	$\frac{2.8}{14}$	$\frac{1.3}{.22}$	$\frac{+7.5}{.52}$	$\frac{+5.6}{.36}$
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38 34 24 22 14 13 9 3.5 10 14 22 32 36

of Above H. I.

12.1	12.1	0.9	2.1	3.7	4.2	3.8	4.0	3.6	10.1	10.2	2.1	3.2
23	30	27	23	18	12	10	3.4	10	18	22	24	31

33 30 27 23 18 12 10 3.4 10 18 22 24 31 35

$\frac{4.5}{33} \quad \frac{4.1}{25} \quad \frac{4.9}{23} \quad \frac{4.5}{15} \quad \frac{4.6}{9} \quad 4.2 \quad \frac{4.6}{11} \quad \frac{4.8}{14} \quad \frac{5.4}{14} \quad \frac{5.4}{17} \quad \frac{5.0}{18} \quad \frac{6.7}{28} \quad \frac{6.7}{33}$

33 25 23 15 9 4.2 11 14 14 17 18 28 33

8.0 7.8 6.1 5.9 5.1 5.0 4.9 7.9 9.2 9.5
33 28 23 14 14 9 4.5 12 18 27 33

33 28 29 14 14 9 4.5 12 18 27 33

15.0
29

29

$$\begin{array}{r} 13.0 \\ \hline 38 \end{array}$$

38

$\frac{13.6}{33}$ $\frac{12.7}{21}$ $\frac{7.7}{12}$ $\frac{7.3}{9}$ 6.9 $\frac{7.4}{9}$ $\frac{7.4}{13}$ $\frac{12.4}{20}$ $\frac{13.1}{33}$

33 21 12 9 6 9 9 13 20 33

$\frac{12.8}{33}$ $\frac{12.6}{27}$ $\frac{12.2}{21}$ $\frac{7.8}{12}$ $\frac{7.7}{9}$ 7.2 $\frac{1.8}{9}$ $\frac{7.8}{11}$ $\frac{11.3}{18}$ $\frac{12.0}{25}$ $\frac{12.1}{33}$

33 17 21 12 9 12 9 11 18 25 33

50	50	6.0	7.0	7.9	7.7	6.6	6.4		6.4	6.4	7.0	8.1	8.2	7.2	7.3	7.4	
39	29	26	14	15	14	11	8	5	9	9	12	15	17	19	22	26	33

33 29 24 14 15 14 11 8 5.9 9 12 15 17 19 22 26 30

2.6	2.4	3.2	4.4	6.2	6.2	3.8	3.7			3.7	3.8	4.2	4.6	4.6	3.5	3.2
33	28	26	17	14	15	12	8	5	2	10	12	15	17	19	21	33

33 28 26 17 14 15 12 8 3 2 10 12 15 17 19 21 33

6.9	7.6	8.1	11.1	10.7	9.7	9.3	9.5		9.8	9.7	9.9	10.6	10.1	9.9	9.5	9.5
13	17	18	15	14	12	9	8	9.1	7	12	15	14	18	19	26	33

33 37 18 15 14 12 9 8 9.1 7 12 15 14 18 19 24 30

$\frac{10.5}{33}$ $\frac{10.9}{27}$ $\frac{10.6}{18}$ $\frac{12.1}{17}$ $\frac{11.1}{16}$ $\frac{8.9}{11}$ $\frac{8.9}{8}$ $\frac{8.3}{8.3}$ $\frac{9.0}{10}$ $\frac{9.1}{15}$ $\frac{10.7}{17}$ $\frac{10.8}{26}$ $\frac{10.9}{33}$

33 27 18 19 16 11 8 8.5 10 15 17 26 33

13.0	14.0	11.6	8.5	8.4	8.3	8.2	11.0	11.0	11.1
33	25	18	12	9	9	13	21	26	33

35 25 18 12 9 7.9 9 13 21 26 33

Sta. + H.I. - Rod. Elev.

1033.43

187 6.5 26.9

+50 5.1 28.3

188 3.0 30.4

8.62 1040.55 1.50 1034.93

+50 8.4 32.2

189 7.1 33.5

+50 5.7 34.9

190 5.1 35.5

+55 5.0 35.6

B.M. 5.25 1040.25 5.58 1034.97 1035.00

191 4.7 35.6

+48 2. East Co. Line Rd. 5.2 35.1

B.M. 5.25 1035.00

13.0 12.7 7.0 7.0 7.0 6.6 6.8 9.2 9.1 8.3 8.1
33 25 14 9 6.5 9 10 14 20 21 22 33

10.8 9.9 9.9 5.4 5.6 5.6 5.6 9.2 9.1
33 30 24 14 9 5.1 9 15 23 33

8.8 7.8 6.9 4.2 3.8 3.5 3.6 4.4 4.6 3.7 3.8
33 28 20 15 9 3.0 9 14 15 19 22 33

7.0 8.7 9.4 9.3 9.2 9.0 9.4 4.5 4.4
33 25 21 18 12 8.4 12 14 20 24 33

3.2 3.2 4.4 5.2 7.8 7.8 7.7 7.9 2.1 2.1
33 28 24 23 18 11 7.1 8 17 23 33

0.8 1.0 3.2 3.8 5.9 5.8 6.1 6.4 6.5 2.9 3.0 3.9
33 28 25 23 19 14 11 5.7 10 14 20 27 33

Above H.I.

+1.0 0.1 4.9 5.2 5.6 5.5 5.7 8.5 9.0 9.4
33 25 21 15 5.1 9 11 14 24 28 33

Above H.I.

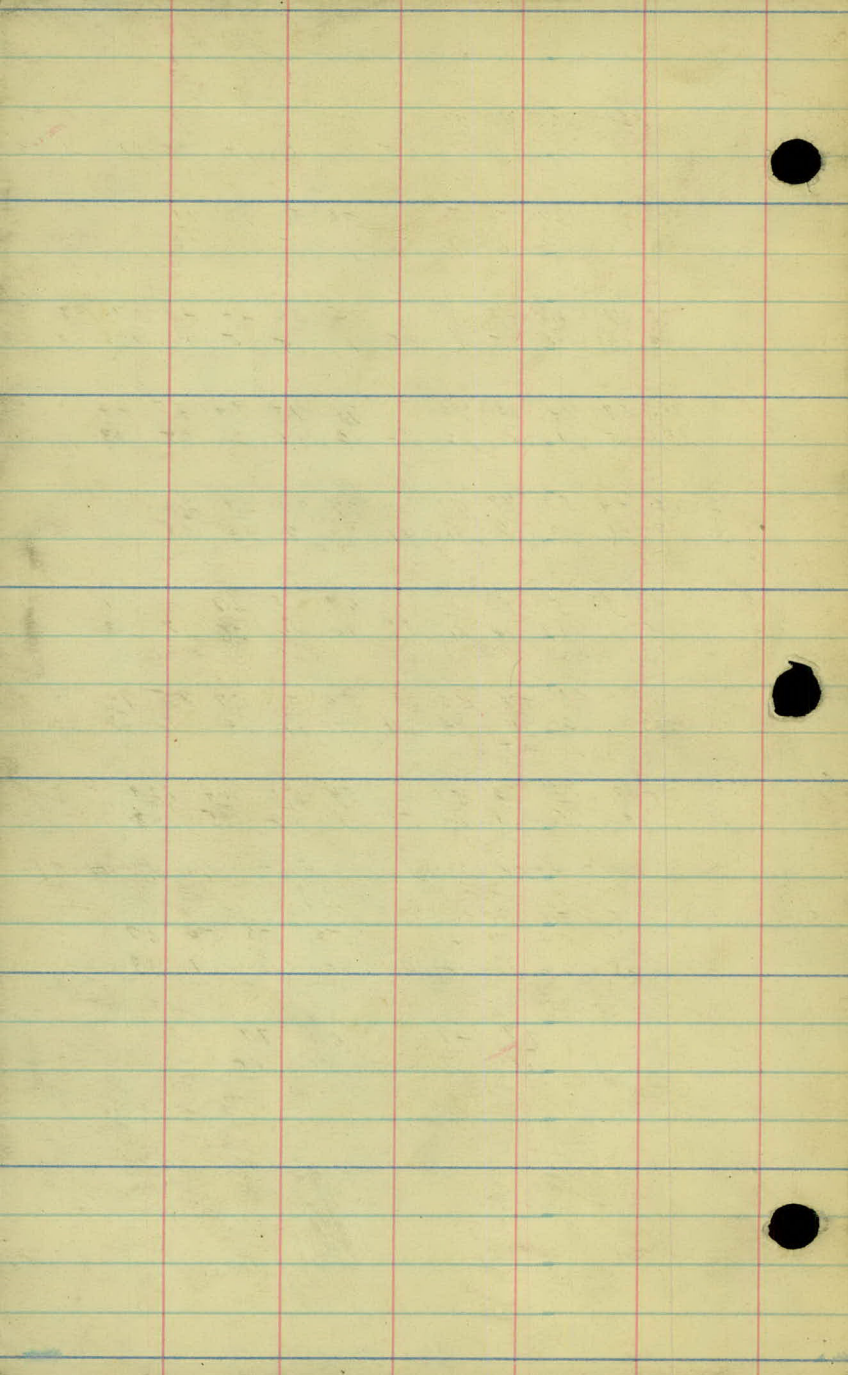
+0.8 0.2 5.2 5.1 5.4 5.6 10.4 12.4
33 25 21 12 5.0 9 14 25 33

Spk. in T.P. #18295 at Int. Co. Rd. "D" & East Co. Line Rd. # 21

Spk. in T.P. Rt. Sta. 190+65.

2.7 5.4 5.1 4.8 5.2 5.3 5.4 6.7
48 44 28 12 4.7 10 18 29 33

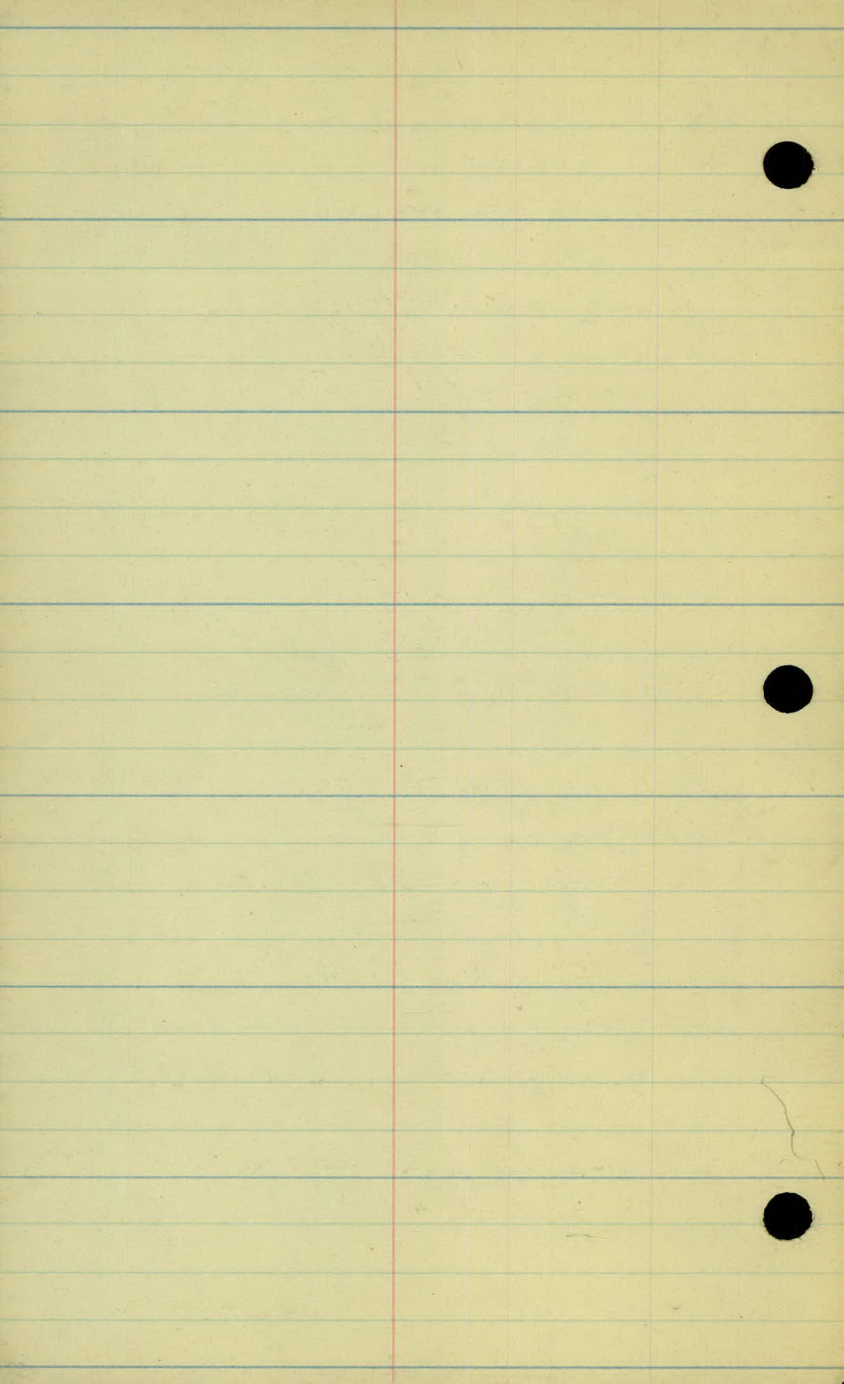
4.9 4.9 6.6 7.7
100 50 52 50 100



PLANS

IN
HANDS

Co. Rd "D"



PLANS-IN-HAND INSP.-
MAINT. PLANS- CO. RD. D.

6-29/26

H.D.K.
M.H.C.

0+20 - No Culv. Reg.-
—

2+16 - F.E. Rt. - P- 12" X 24' C.M. -
—

4+00 - Inp. - 24" X 60' C.M. - Clean Jo. End. -
—

7+20 - F.E. Rt. - No Culv. Reg. - Summit. -
—

9+11 - F.E. Rt. - Inp. - 12" X 24' - Clean. -
—

10+10 - Inp. - 15" X ? C.M. Rem. - P. 24"
—

13+93 - F.E. Rt. - No Culv. Reg. -
—

16+90 - F.E. Rt. - P - 12" X 24' C.M.
—

16 to 19 - Cl. & Gr. 15 Tr.
—

20+77 - F.E. Lt. - P-12" X 24' C.M.
—

23+83 - Inp - 12" X 56' C.M. Rem. - P. - 24"

Used old C.M. for F.E.

26+50 - F.E. Rt. - P - 12" x 24"

27+33 - F.E. - Lt. - No Cul. Reg. -

27+60 - Inp. - 12" x 56' C.M. Rem. - P. 24"
Use old C.M. -

28+55 - Inp. - 12" x 16' - Rem & Rep. - 12" x 24"

31+33 Lt & 31+64 Rt. - No. Cul. Reg. -

33+12 - Rt. & Lt. - P. 2 - 12" x 24' C.M.

37+54 Inp. - 12" x 48' - Rem - P. 24"
Used old C.M.

38+78 - J.T.H. #1 no cul. Reg. -

41+36 - Inp 36" x 50' C.M. Extend. -

45+75 - F.E. Rt & H. - P² 12" x 24' C.M.

48+11 - Inp. - 18" x 44' C.M. - Extend. -

53+75- F.E. Rt. & Lt. - P-12"X24' C.M. Rt. -

—+—

59+50. Rt. - Rt. No Cul. Reg. -

—+—

59+98- Inp. - 12"X40' C.M. - Rem. - P 24"

—+—

63+74 Inp. - 12"X50' C.M. Rem. - P-24"

—+—

66+71- F.E. Lt. - Inp. - 12"X30' C.M. Rem & Rep. -

—+—

71+50 - F.E. Lt. - No Cul. Reg. -

—+—

74+00 F.E. Rt. - No Cul. Reg. -

—+—

82+40. F.E. Rt. - No Cul. Reg. - Summit.

—+—

84+69. F.E. Lt. - P-12"X24' C.M.

—+—

89+58- Inp. - 30"X50' C.M. - Extend

—+—

102+04 Inp. - 18"X40' C.M. Extend.

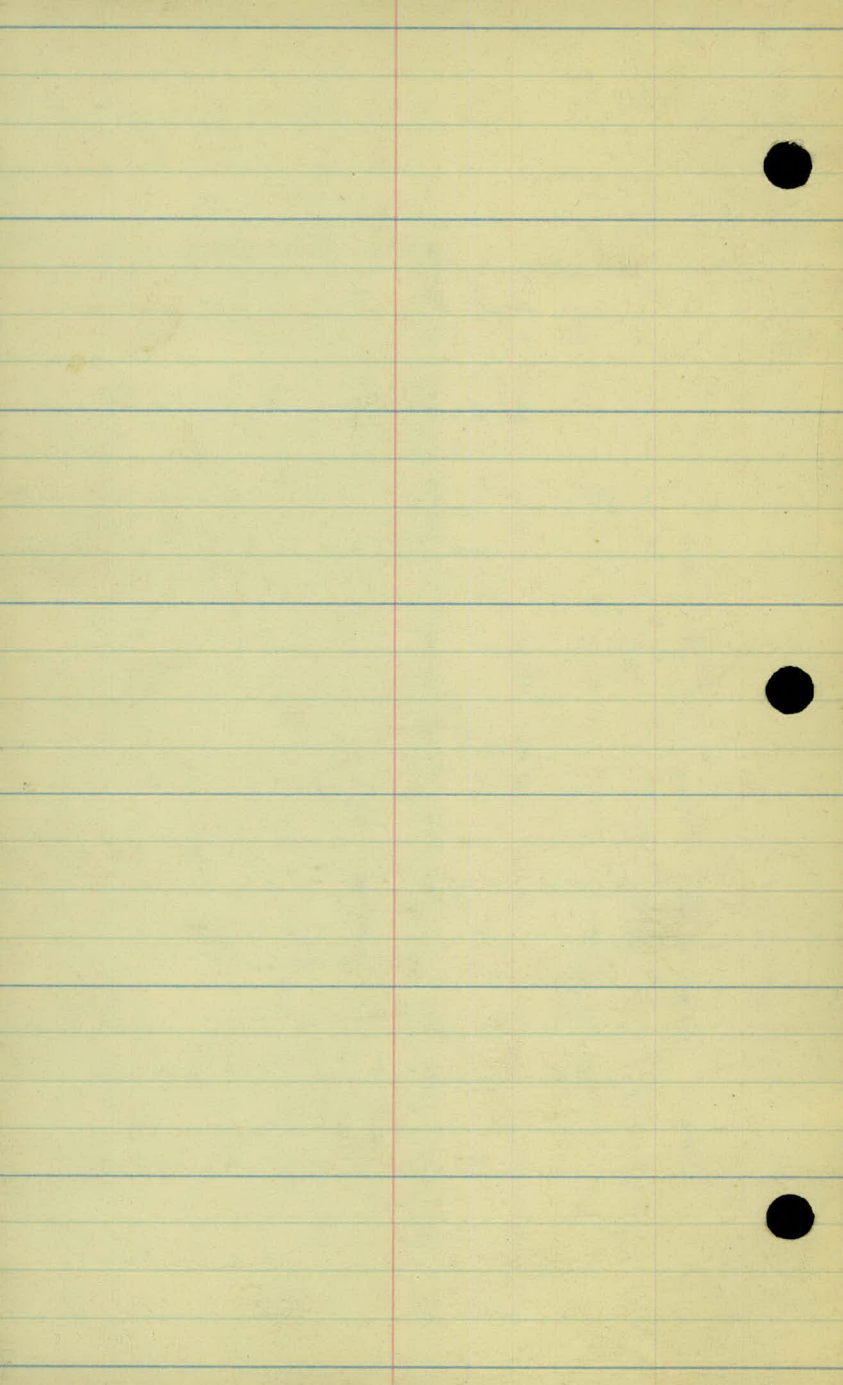
—+—

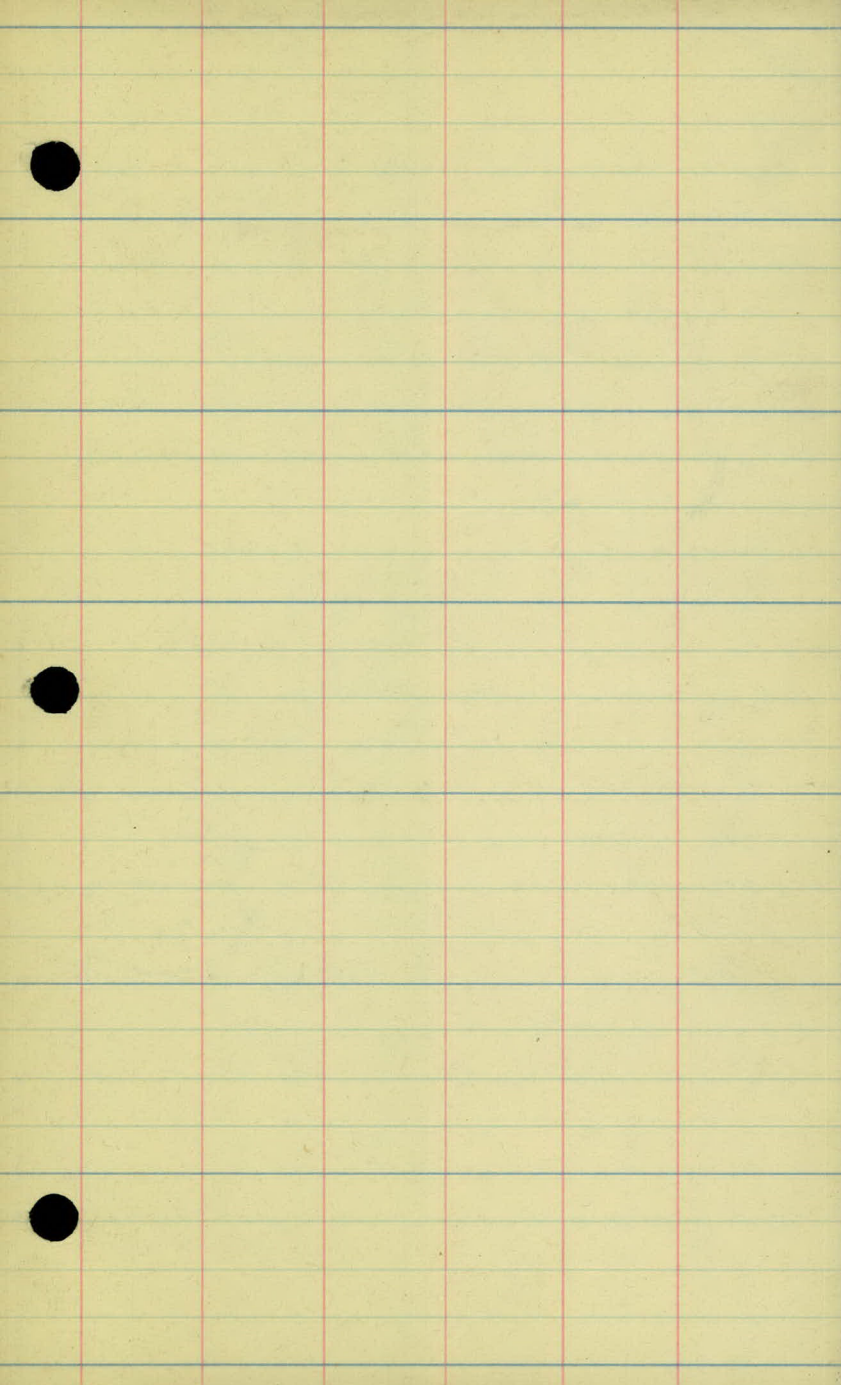
106+58 Rt. Inp. - 24"X40' Ps. - O.K.

—+—

109+60 - Rt. Inp. - 12"X18- Rem & Rep. -

—+—





7/2/26

H.D.V.R.

M.W.C.

112+50 F.E. Lt. P-12"x24"CM.-

115+10 F.E. Rt. P-12"x24"CM.-

116+75 No Cul. Reg. Drain East.

119+00 F.E. - Rt. Inp. - 12"x20" Rem. & Rep.

122+00 P-24" X Drains Lt.-

128+61 F.E. Rt. Inp. - 12"x16"CM. - Rem. & extend
F.E. Lt. P-12"x24"CM.

132+10 F.E. Lt. No Culv. Reg.

132+72 F.E. Rt. P-12"x24"CM.-

136+12 Inp. - 18"x40"CM. - Extend. - Drains Lt.

138+60 Rd. Rt. P-12"x30"CM.-

142+50 F.E. Rt. P-12"x24"CM.

145+50. Rd. Rt. - No Culv. Reg. -
—+—

145+95 - F.E. Lt. - No Culv. Reg. -
—+—

151+82 - F.E. Rt. - P-12" X 24' CM. -
—+—

163+63 - F.E. Rt. - No Culv. Reg. -
—+—

171+50 - P-18" CM. - Drains Rt. -
—+—

174+20 - F.E. - Lt. - No Culv. Reg. -
—+—

Drain back from 174 to 171
—+—

176+13 - F.E. Rt. - P-12" X 24' CM. -
—+—

176+50 - P-18" Cross Drain. -
—+—

178+90 - Double F.E. Lt. - P-12" X 36' CM. -
—+—

181+70 - Inp 18" X 68' CM. Remove
P-24" CM. skew
—+—

184+55 - F.E. Lt. - P-12" X 24' CM.

