

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN Survey

Old Snelling Avenue

From T. H. No. 51 To T. H. No. 96

Road Acc't. No. 76 Turnback

Date Filed _____

File 105

KP
W.S
D.S

3-7-72
CLOUDY & COOL
19° AND FALLING

SETTLEMENT OF SNELLING AVE

ELEVATIONS TAKEN WEEKLY ON
AN AREA SURROUNDS MH 16A. THE CONCRETE IN
THIS AREA WAS REMOVED IN ORDER TO
ACCOMMODATE SEWER INSTALLATION AND
REPLACED. IT SEEMS THIS AREA IS SETTLING
AT THE PRESENT TIME. FIFTEEN SPOTS WERE
MARKED ON THE E AND DRIVING LANES AND
ELEVATIONS TAKEN ON EACH SPOT. PURPOSE IS
TO KEEP RECORDS SO THAT ANY LARGE SETTLEMENT
CAN BE REPAIRED BY CONTRACTOR WHO DID SAID
SEWER WORK AND CONCRETE REPLACEMENT. AREA
COVERED IS JUST SOUTH OF R.R. BRIDGE (50'±).
ALSO HAVE AN AREA AT STATION 240 WHICH
IS SETTLING. CONTRACTOR NOT RESPONSIBLE AS
THEY PAVED OVER EXISTING CONCRETE. SPOTS 16-30
ON FOLLOWING PAGES

A
R
E
A

O
F

S
E

T

T
L

E

M

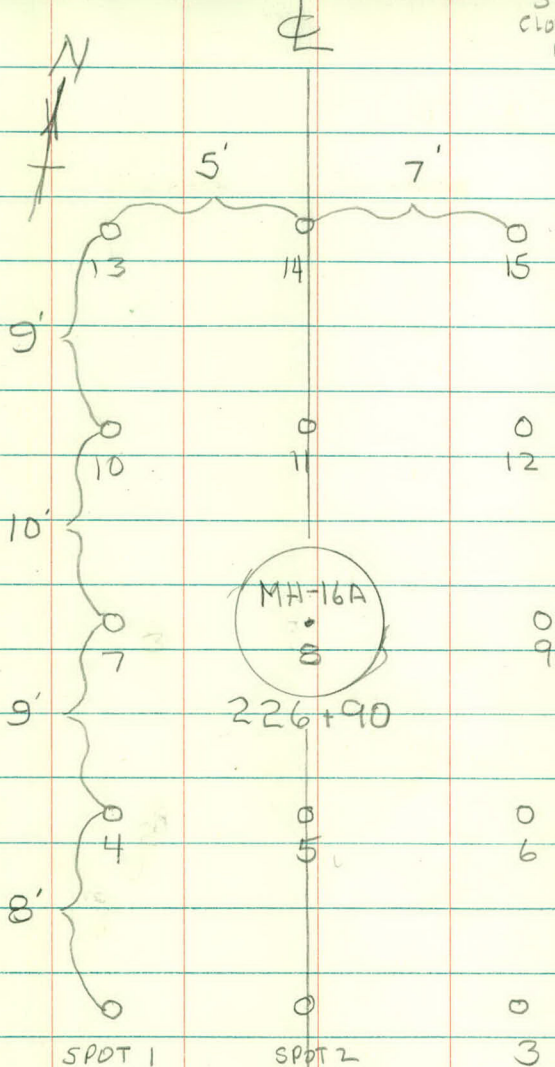
E

N

T

KP
WS
DS

3-7-72 2
CLOUDY & COLD
19° DROPPING



STA + T - ELEV.

BM 5.76 90354

897.78

#1 5.30 898.24

2 5.16 88.38

3 5.24 88.30

4 5.51 88.03

5 5.39 88.15

6 5.47 88.07

7 5.68 87.86

8 5.64 87.90

9 5.62 87.92

10 5.74 87.80

11 5.68 87.86

12 5.70 87.84

13 5.84 87.70

14 5.79 87.75

15 5.81 87.73

BM 5.24 898.30

LT

E

RT

3

LOWER RAIL W. SIDE E RR BRIDGE

STA	+	π	-	ELEV
BM	98.64	9 108.64		100.00
16	5.02		5.02	⁴ 107.62
17			4.68	⁴ 108.96
18			4.62	⁵ 104.02
19			5.08	⁴ 107.56
20			4.78	⁴ 108.86
21			4.75	⁴ 108.89
22			5.15	⁴ 108.49
23			4.88	⁴ 108.76
24			4.85	⁴ 108.79
25			5.25	⁴ 108.39
26			4.98	⁴ 108.66
27			4.95	⁴ 108.69
28			5.34	⁴ 108.30
29			5.04	⁴ 108.60
30	5.02		5.02	⁴ 108.62

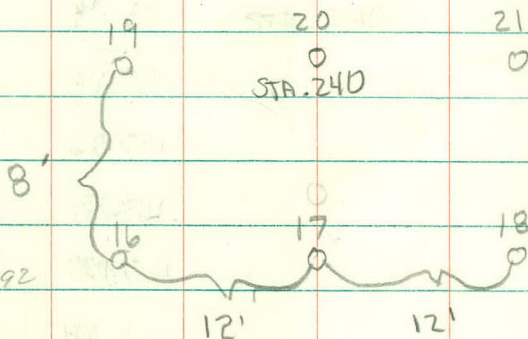
LT 12' 7 MAR 1972 4
RT 12'

SPIKE IN P.P. STA 240+75 ± (RT)

Station	28	29	30
240+24	0	0	0

Station	25	26	27
240+16	0	0	0

Station	22	23	24
240+08	0	0	0



239+92

STA	+	π	-	ELEV.
BM	6.10	903.88		897.78
#1			5.57	898.21 ³¹
#2			5.44	8.44
#3			5.53	8.35
#4			5.77	8.11
#5			5.66	8.22
#6			5.74	8.14
#7			5.96	7.92
* #8			5.85	8.03
#9			5.90	7.98
#10			6.03	7.85
#11			5.96	7.92
#12			5.98	7.90
#13			6.11	7.77
#14			6.08	7.80
#15			6.09	7.79
BM			6.72	897.16
				897.16

LT

13 MAR 1972 5.
± SUNNY 40° RT

LOWER RAIL W. SIDE ± PP BRIDGE

$$\begin{array}{r} 897.16 \\ 6.65 \\ \hline 903.81 \end{array}$$

SPIKE IN PP RT STA 226+50±

11

11

STA	+	π	-	ELEV
BM	10.42	110.42		100.00
#16			5.65	104.77
#17			5.35	105.07
#18			5.34	105.08
#19			5.72	104.70
#20			5.45	104.97
#21			5.46	104.96
#22			5.80	104.62
#23			5.57	104.85
#24			5.67	104.75
#25			5.90	104.52
#26			5.67	104.75
#27			5.67	104.75
#28			5.97	104.45
#29			5.72	104.70
#30			5.75	104.67
BM			5.31	105.11

LT

13 MAR 1972 6.
RT

SPIKE IN PP RT STA 240+75⁺

TOP PK @ STA 239

STA	+	π	-	ELEV.
BM	6.67	903.83		897.16

#1			5.62	898.21 1.1
#2			5.48	8.35
#3			5.58	8.25
#4			5.81	8.02
#5			5.69	8.14
#6			5.78	8.05
#7			5.99	7.84
#8			5.88	7.95
#9			5.93	7.90
#10			6.06	7.77
#11			6.00	7.83
#12			6.02	7.81
#13			6.17	7.66
#14			6.12	7.71
#15			6.13	7.70

BM			5.53	897.77	897.78
			6.05		897.78

KP
WS
DS

LT

£

20 MAR 1972
SUNNY 50° RT

7

SPIKE IN PP RT 226+50[±]

6.05

903.83

5.53

.52

5.45

898.38

897.78

.60

LOWER RAIL W. SIDE £ RR BRIDGE

"

"

"

STA	+	π	-	ELEV.	
BM	10.38	110.38			100.00
#16			5.66	104.72	
#17			5.37	5.01	
#18			5.32	5.06	
#19			5.71	4.67	
#20			5.45	4.93	
#21			5.44	4.94	
#22			5.77	4.61	
#23			5.54	4.84	
#24			5.56	4.82	
#25			5.87	4.51	
#26			5.64	4.74	
#27			5.65	4.73	
#28			5.95	4.43	
#29			5.70	4.68	
#30			5.72	4.66	
			5.78		
			5.32		
BM			5.30	105.08	105.11

20 MAR 1972

LT

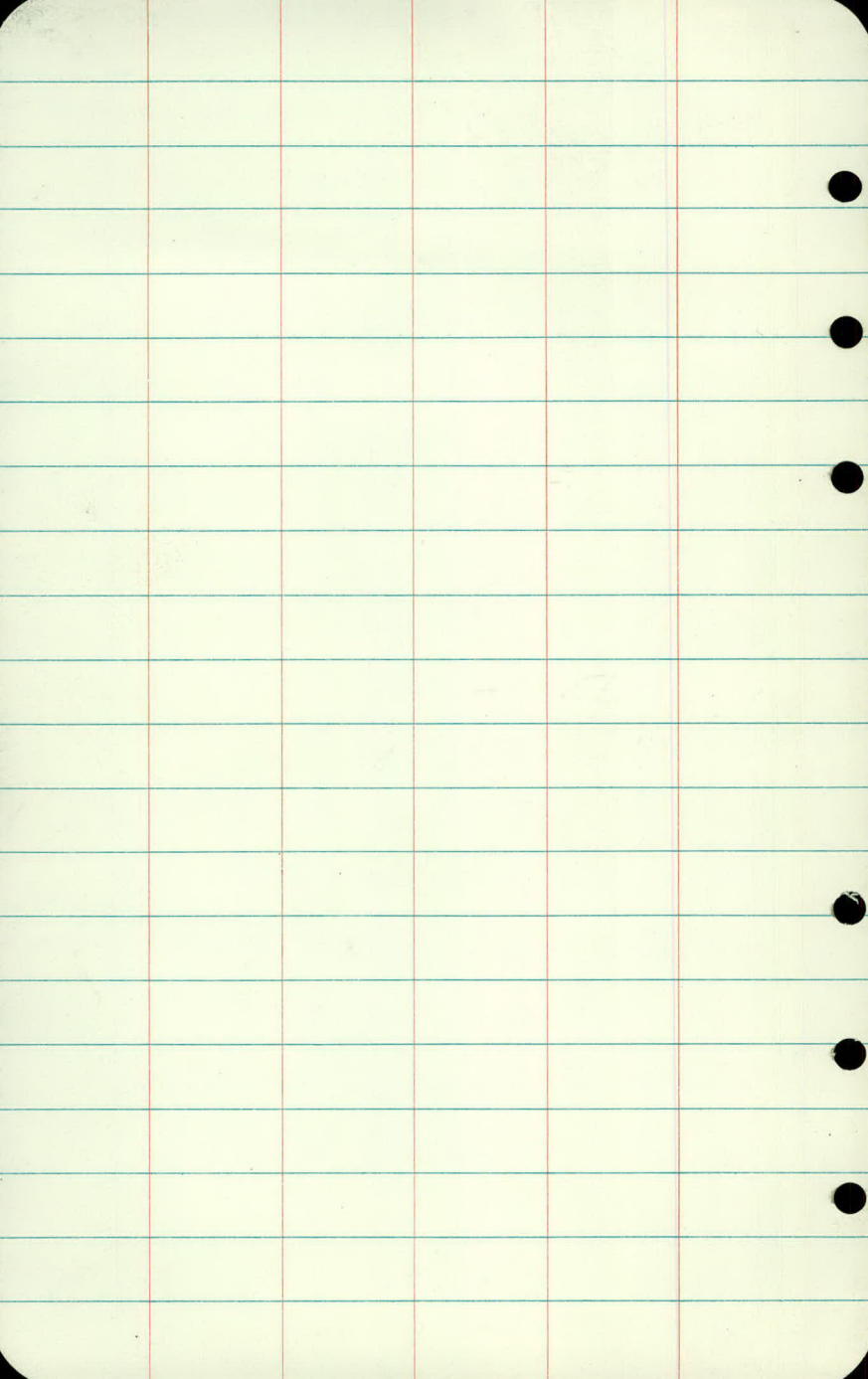
±

RT

8

SPIKE IN PP RT STA 240+75±

TOP PR ± STA 239



W.S
D.S

321-72 9
TUESDAY

SETTLEMENT GRADES

STA.	+	π	-	ELEV.
BM	6.37	904.15 904.05		897.78
SPOT. 1			5.95	898.20
2			5.82	8.33
3			5.91	8.24
4			6.04	8.11
5			6.02	8.13
6			6.11	8.04
7			6.32	7.83
8			6.21	7.94
9			6.26	7.89
10			6.40	7.75
11			6.33	7.82
12			6.36	7.79
13			6.50	7.65
14			6.46	7.69
15			6.48	7.67
T.P.			6.99	897.16 897.06

897.16

LT

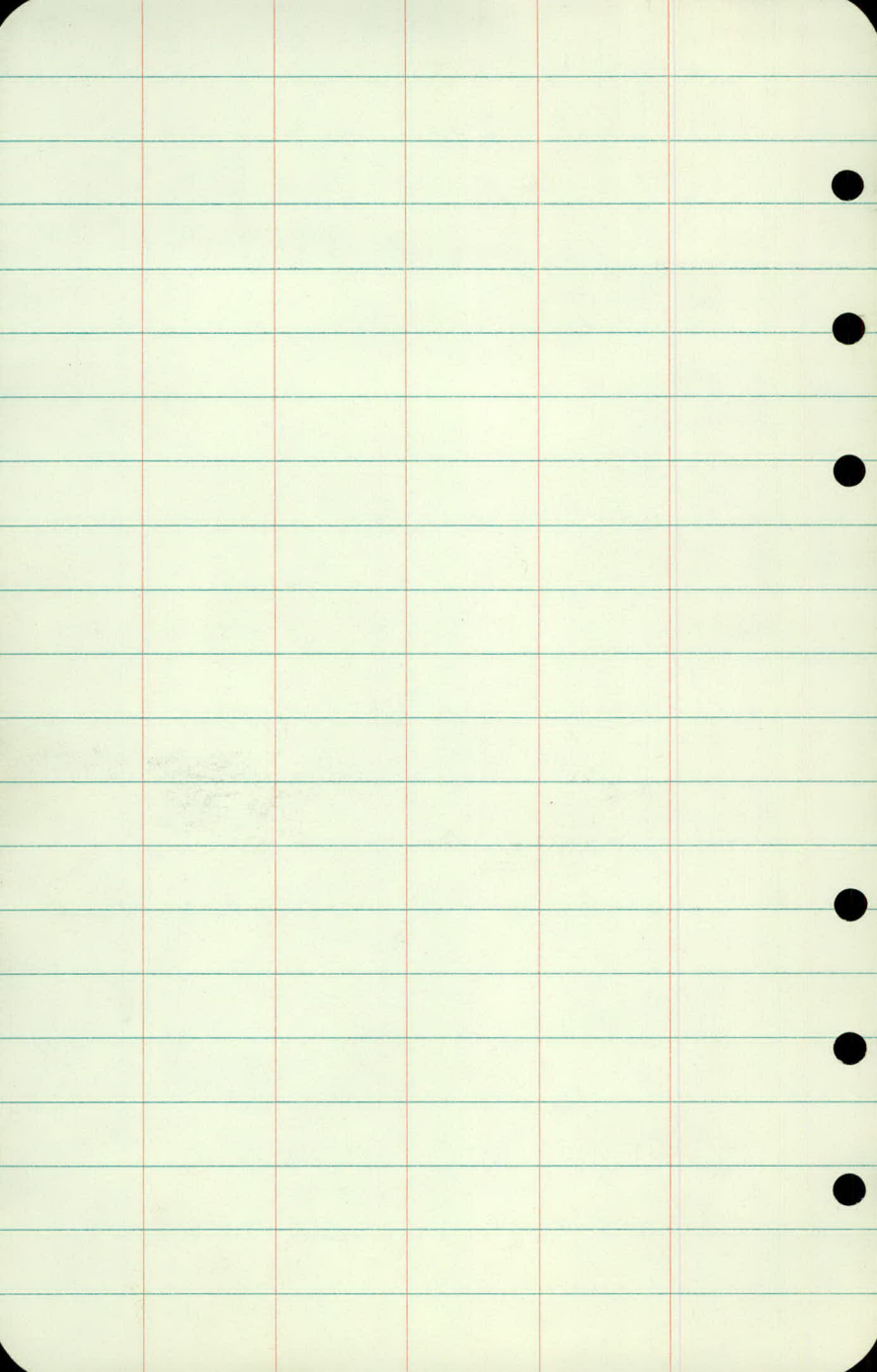
£

RT.

10

LOWER RAIL W. SIDE £ R.R. BRIDGE

P.P. - SE (100') OF R.R. BRIDGE



KP
WS
DS
DK

28 MARCH 1972

1.

SNELLING AVENUE

62-676-01 CTB

SETTLEMENT GRADES

STA	+	$\bar{A}$	-	ELEV.
BM	6.24	904.02		(897.78)

#1			5.84	8.18
----	--	--	------	------

#2			5.71	8.31
----	--	--	------	------

#3			5.80	8.22
----	--	--	------	------

#4			6.03	7.99
----	--	--	------	------

#5			5.91	8.11
----	--	--	------	------

#6			5.99	8.03
----	--	--	------	------

#7			6.22	7.80
----	--	--	------	------

#8			6.11	7.91
----	--	--	------	------

#9			6.16	7.86
----	--	--	------	------

#10			6.29	7.73
-----	--	--	------	------

#11			6.23	7.79
-----	--	--	------	------

#12			6.25	7.77
-----	--	--	------	------

#13			6.40	7.62
-----	--	--	------	------

#14			6.36	7.66
-----	--	--	------	------

#15			6.37	7.65
-----	--	--	------	------

BM			6.84	897.18 (897.16)
----	--	--	------	-----------------

LT

£

28 MAR 1972

2

RT

LOWER RAIL W. SIDE £ RR BRIDGE

SPIKE IN PP RT STA 226+50±

STA	+	π	-	ELEV.	
BM	10.67	110.67			(100.00)
#16			5.99	4.68	
#17			5.70	4.97	
#18			5.69	4.98	
#19			6.03	4.64	
#20			5.76	4.91	
#21			5.74	4.93	
#22			6.09	4.58	
#23			5.85	4.82	
#24			5.86	4.85	
#25			6.19	4.48	
#26			5.94	4.73	
#27			5.94	4.73	
#28			6.26	4.41	
#29			6.00	4.67	
#30			6.02	4.65	
BM			5.61	105.06	(105.11)

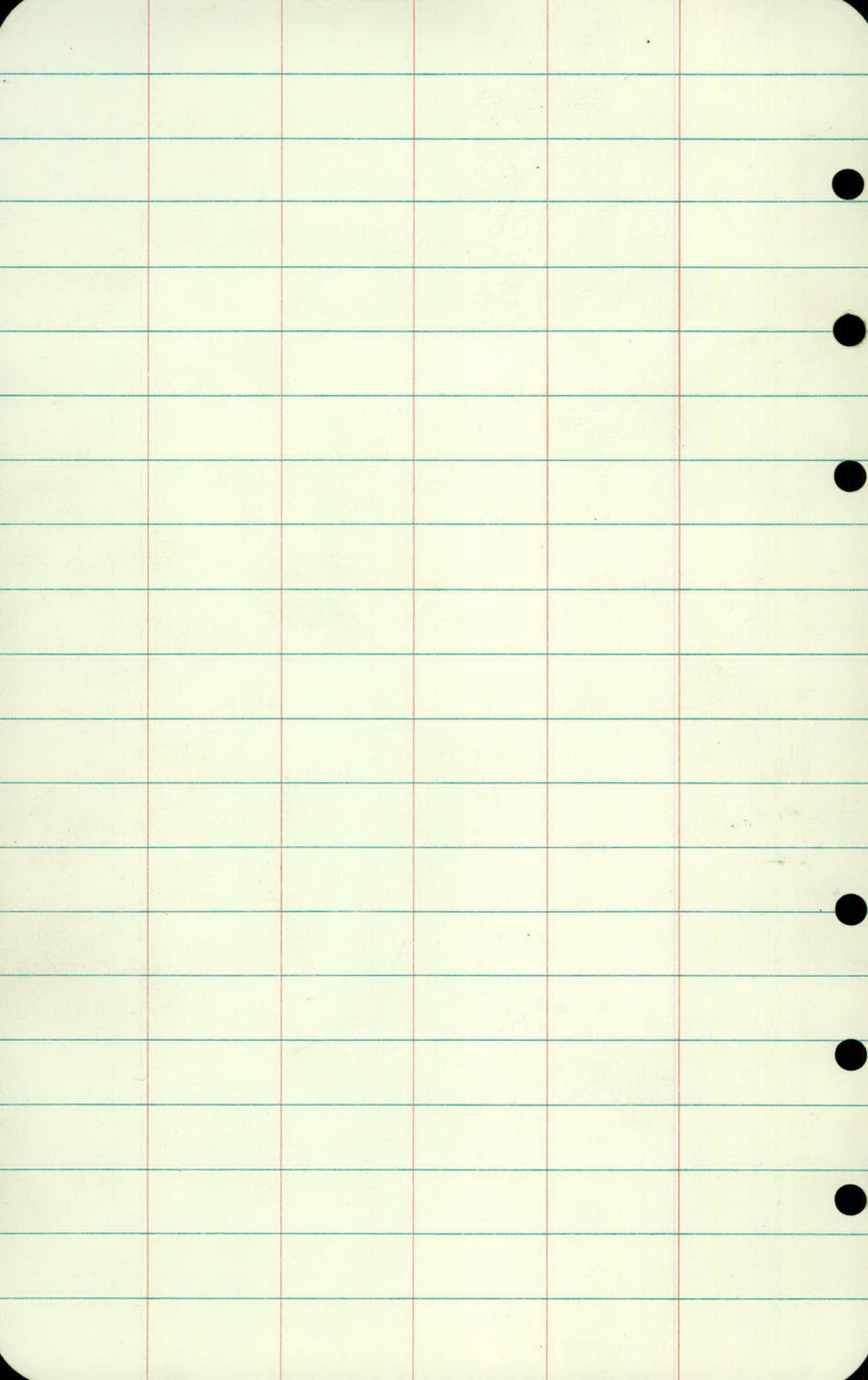
LT

E

28 MAR. 1972, 3,
RT

SPIKE IN PP RT STA 240+75⁺

TOP PK E STA 239



D, R
L, P, D
D, S

APRIL 4, 1972

SNELLING AVE

62-676-01 CTB

SETTLEMENT GRADES

STA	+	Δ	-	ELEV
B.M	6.34	904.12		897.78
# 1			5.99	8.13
# 2			5.85	8.27
# 3			5.94	8.18
# 4			6.16	7.96
# 5			6.05	8.07
# 6			6.12	8.00
# 7			6.34	7.78
# 8			6.23	7.89
# 9			6.29	7.83
# 10			6.43	7.69
# 11			6.36	7.76
# 12			6.38	7.74
# 13			6.53	7.59
# 14			6.48	7.64
# 15			6.50	7.62
B.M			6.95	897.17
				897.16

APRIL 4-1972

LT

♀

RT

LOWER RAIL W. SIDE ♀ R.R. BRIDGE

SPIKE IN P.P. RT STA 226+50

+

STA	+	π	-	ELEV
B.M	10.57	110.57		(100.00)
# 16			5.93	4.64
# 17			5.65	4.92
# 18			5.58	4.99
# 19			5.97	4.60
# 20			5.71	4.86
# 21			5.68	4.89
# 22			6.02	4.55
# 23			5.78	4.79
# 24			5.78	4.79
# 25			6.11	4.46
# 26			5.86	4.71
# 27			5.86	4.71
# 28			6.18	4.39
# 29			5.92	4.65
# 30			5.94	4.63

B.M		553	105.04	(105.11)
-----	--	-----	--------	----------

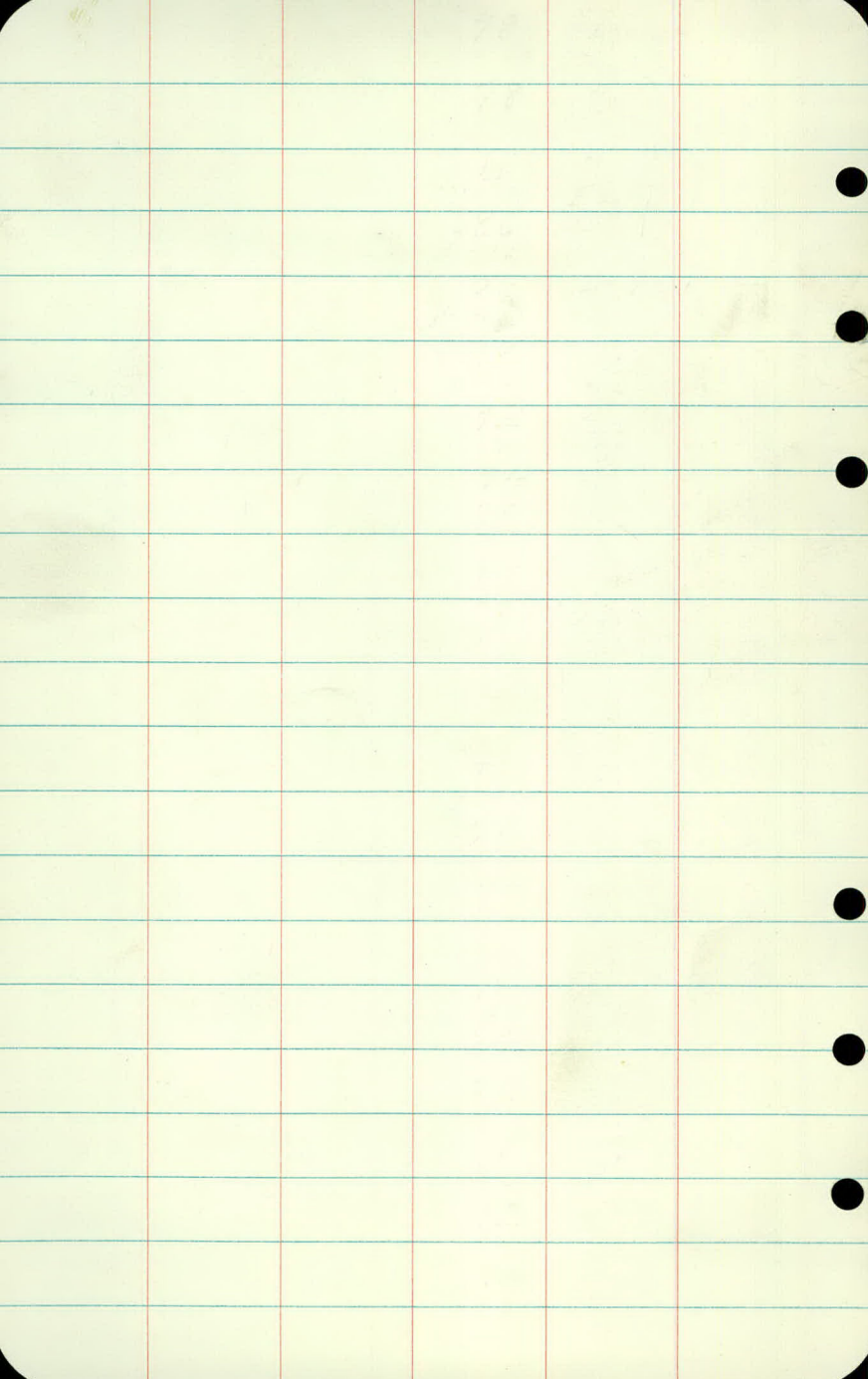
LT

¢

RT

SPIKE IN P.P RT STA 240+75 ⁺₋

TOP P.K ¢ STA 239



RG
DK

April 11, 1972
Cldy 36°
pg 1 of 3

Snelling Ave.

62-676-01 CTB

Settlement Grades

Sta	+	π	-	ELV
BM	6.93 ⁵	904.21 ⁵		897.78
#1			6.12	
#2			5.99	
#3			6.08	
#4			6.29	
#5			6.18	
#6			6.24	
#7			6.45	
#8			6.34	
#9			6.40	
#10			6.53	
#11			6.47	
#12			6.50	
#13			6.63	
#14			6.59	
#15			6.60	
BM			7.04 ³	897.17 ² 897.16

April 11, 1972

2 of 3

Top lower step W. side E RR Bridge

Spike in PP Rt Sta 226+50

Sta	+	π	-	ELV
BM	10.23	110.23		100.00
#16			5.64	
#17			5.35	
#18			5.275	
#19			5.67	
#20			5.40	
#21			5.36	
#22			5.71	
#23			5.46	
#24			5.45	
#25			5.79	
#26			5.525	
#27			5.52	
#28			5.84	
#29			5.59	
#30			5.605	
BM			5.205	105.025 105.11 ?

April 11, 1972

3 of 3

Spike in PP Rt Sta 240+75 ±

Top PK nail R Sta 239

Sta	+	π	-	EIV
BM	6.84	904.62		897.78
#1			6.60	
#2			6.49	
#3			6.57	
#4			6.73	
#5			6.63	
#6			6.69	
#7			6.87	
#8			6.75	
#9			6.83	
#10			6.96	
#11			6.90	
#12			6.94	
#13			7.06	
#14			7.01	
#15			7.05	
BM			7.45	897.17 897.16

R6
GA
DK

April 27, 1972
Cldy 44°

Top lower step or curb W side of RR Bridge

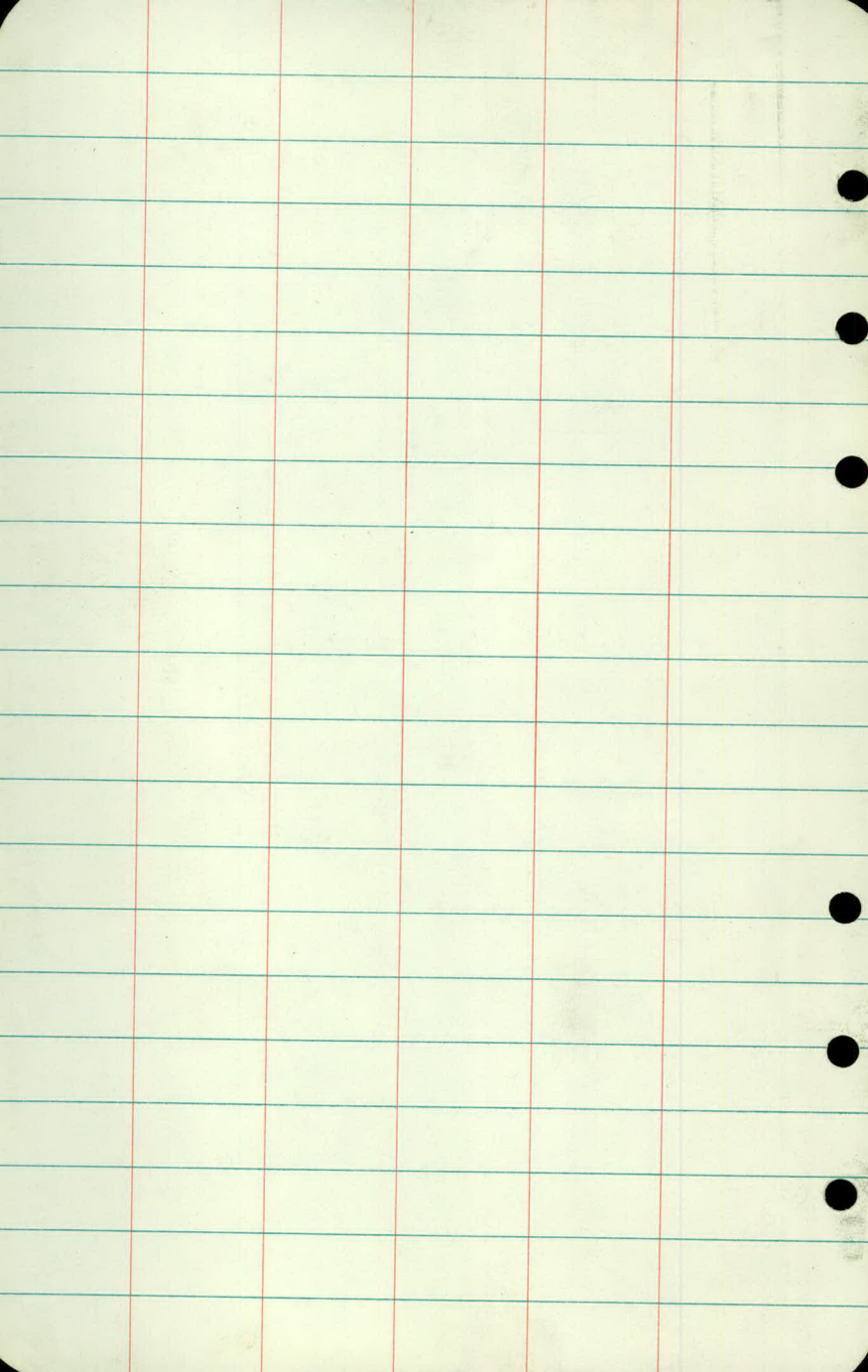
Spike in PP RT Sta 226+50

Sta	+	T	-	ELV	
BM	10.87	110.87		100.00	assumed
#16			6.34		
#17			6.05		
#18			5.94		
#19			6.36		
#20			6.08		
#21			6.03		
#22			6.38		
#23			6.13		
#24			6.10		
#25			6.45		
#26			6.17		
#27			6.17		
#28			6.48		
#29			6.24		
#30			6.25		
BM			5.86	105.01	105.11

April 27, 1972
Cldy 94°

Spike in PP Rt Sta 240+75±

Top PK nail & Sta 239± (Questionable)



76 TURNBACK
OLD STH # 51 (SNELLING AVE.)
NEW STH # 51 - STH # 96

ALINEMENT

STH 96

STH # 494

CO RD F

CO RD E2

VALENTINE
LAKE

500 LINE RR

Johanna Blvd. CO RD F

New STH 51

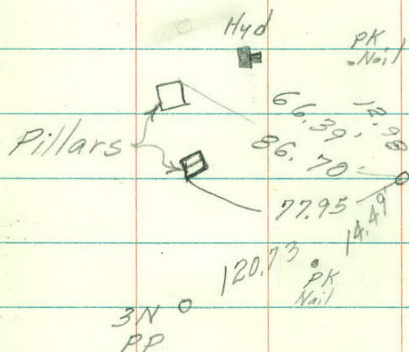


STA	Point	ΔLT	ΔRT	Curve data
+14.85	PT	9°02		
191		8°44		
+50		7°44		$\Delta 1804'$
190		6°44		D 4°
+50		5°44		T 227.76
189		4°44		L 451.67
188+90.95	PI			R 1432.69
+50		3°44		
188		2°44		
+50		1°44		
187		0°44		
186+63.18	PC	0°00		
171+38.78	P.O.T.	≠ SBL NEW SNELLING		

FK
RG
DR

6-5-1970

2



Iron pin

Sta Point Δ Lt. Δ Rt.

216+68.68

E Co Rd "E"

P.K. Nail

STA	Point	ΔL	ΔR	Curve data
+73.12			$3^{\circ}36.75'$	
+50			$3^{\circ}23'$	
222			$2^{\circ}53'$	
+50			$2^{\circ}23'$	$\Delta 7^{\circ}13.5$
221			$1^{\circ}53'$	$D 2^{\circ}$
220+92.83	PI		$7^{\circ}13.5$	$T 180.91$
+50			$1^{\circ}23'$	$L 361.25$
220			$0^{\circ}53'$	$R 2864.93$
+50			$0^{\circ}23'$	
219+11.92	PC		$0^{\circ}00'$	
216+68.68	PI			

LT

£

RT

4

$\frac{3N}{TP}$ -

165.17'

$\frac{3N}{TP}$ -

30.87'

35.55'

$\frac{3N}{PP}$ -

Drill Hole

168.36'

$\frac{3N}{PP}$ -

STA	POINT	ΔLT	ΔRT	CURVE DATA
+76.27	PT	19°40'		
+50		19°00.6'		
237		17°45.6'		
+50		16°30.6'		
236		15°15.6'		
+50		14°00.6'		Δ 39°20'
235		12°45.6'		D 5°00' Lt
+50		11°30.6'		T=409.68'
234		10°15.6'		L 786.67'
+99.28	PI	39°20'		R 1146.28
+50		9°00.6'		
233		7°45.6'		
+50		6°30.6'		
232		5°15.6'		
+50		4°00.6'		
231		2°45.6'		
+50		1°30.6'		
230		0°15.6'		
229+89.60	PC	0°00'		

LT

£

RT

5

FT 0.67 longer

3N
PP 27.33' 12.84'

Guy Wire
at ground

iron

Sta Point Δ -Lt Δ Rt.

+73.23	P.T.	34° 22' 30"
+50		33° 12.8'
255		30° 42.8'
+50		28° 12.8'
54		25° 42.8' $\Delta = 68^\circ 45'$
+50		23° 12.8' $\frac{1}{2}\Delta = 34^\circ 22' 30''$
53		20° 42.8' $D = 10^\circ 00' R$
252+78.17	P.I.	$T = 392.44'$
+50		- 18° 12.8' $L = 687.50$
52		- 15° 42.8' $R = 573.686$
+50		✓ 13° 12.8'
51		✓ 10° 42.8' 687.50
+50		8° 12.8'
50		5° 42.8'
+50		3° 12.8'
49		0° 42.8'
248+85.23	P.C.	0° 00'

23.48

5003 chords
5000/1645 = 5000/45

June 29, 1970

6

10
50/100
10 15'

spike

253.02'

3N
5" Box Elder

16.89

3N
8" POP 2.53'

Iron

T = 392.45
L = 687.50

Sta Point ΔL ΔR

+56.76 P.T. $12^{\circ}07'15''$

+50 $11^{\circ}57.1'$

269 $10^{\circ}42.1$

+50 $9^{\circ}27.1$

$\Delta = 24^{\circ}14'30''$

268 $8^{\circ}12.1'$

$\frac{1}{2}\Delta = 12^{\circ}07'15''$

+50 $6^{\circ}57.1'$

$D = 5^{\circ}00'44''$

267+18.11 P.I. $24^{\circ}14'30''$

$T = 246.18'$

267 $5^{\circ}42.1$

$L = 484.83'$

+50 $4^{\circ}27.1$

$R = 1146.28$

266 $3^{\circ}12.1$

+50 $1^{\circ}57.1'$

265 $0^{\circ}42.1$

264+71.93 P.C. $0^{\circ}00'$

FK
JT
DR

7-8-70

7

Top
- 3N
PP

80.92'

27.63 3N / 1000
5 Tie
8" Willow

Sta Point Δ Lt. Δ Rt.

+16.43 P.T.

$2^{\circ} 46'$

289

$2^{\circ} 36.1' \Delta = 5^{\circ} 32'$

+50

$2^{\circ} 06.1' \frac{1}{2} \Delta = 2^{\circ} 46'$

288

$1^{\circ} 36.1' D = 2^{\circ} 00' \text{ Rt.}$

287+78.22 P.I.

$5^{\circ} 32' T = 138.45'$

+50

$1^{\circ} 06.1' L = 276.66'$

287

$0^{\circ} 36.1' R = 2864.93$

+50

$0^{\circ} 06.1'$

286+39.77 P.C.

$0^{\circ} 00'$

FK
JT
DR

July 9, 1970

8

PK nail

Sta Point Δ Lt. Δ Rt.

+02.31 P.T. $19^{\circ}15'$

312 $19^{\circ}11.5'$

+50 $17^{\circ}56.5'$

311 $16^{\circ}41.5'$

+50 $15^{\circ}26.5'$

310 $14^{\circ}11.5'$

+50 $12^{\circ}56.5'$

$\Delta = 38^{\circ}30'$

9 $11^{\circ}41.5'$

$\frac{1}{2}\Delta = 19^{\circ}15'$

+50 $10^{\circ}26.5'$

$D = 5^{\circ}00' Lt$

308+32.61 P.I. $38^{\circ}30'$

$T = 400.30'$

$\Delta = 00.30'$
308 $9^{\circ}11.5'$

$L = 770.00'$

+50 $7^{\circ}56.5'$

$R = 1146.28'$

307 $6^{\circ}41.5'$

+50 $5^{\circ}26.5'$

306 $4^{\circ}11.5'$

+50 $2^{\circ}56.5'$

305 $1^{\circ}41.5'$

+50 $0^{\circ}26.5'$

304+32.31 P.C. $0^{\circ}00'$

$\frac{770}{211+02.31}$

FK
JT
GA

July 10, 1970

9

• spike

123.50'

• PK nail

82.85'

• on TH #10

Sta Point ΔL ΔR

+22.66 P.T. $1^{\circ}32'30''$

326 $1^{\circ}25'42''$

+75 $1^{\circ}18.2'12''$

+50 $1^{\circ}10.7'$

+25 $1^{\circ}03.2'$ $\Delta = 3^{\circ}05'00''$

325 $0^{\circ}55.7'$ $\frac{1}{2}\Delta = 1^{\circ}32'30''$

+75 48.2 $D = 1^{\circ}00'$

324+6848 P.I. $T = 154.15$

+50 40.7 $L = 308.33'$

+25 33.2 $R =$

324 25.7

+75 18.2

+50 10.7

+25 $0^{\circ}03.2'^{12}$

323+1433 P.C. $0^{\circ}00'$

FK
PK
CM
BP
CP

August 26, 1970

Sta Point ΔL ΔR

36 + 76.82

+76.82 P.T. $24^{\circ}14'$

+50 $22^{\circ}53'33''$

36 $20^{\circ}23'33''$

$\Delta = 48^{\circ}28'$

+50 $17^{\circ}53'33''$

$\frac{1}{2}\Delta = 24^{\circ}14'$

35 $15^{\circ}23'33''$

$D = 10^{\circ}00'$

+50.05 P.I.

$T = 257.90'$

+50 $12^{\circ}53'33''$

$L = 484.67'$

34 $10^{\circ}23'33''$

$R =$

+50 $7^{\circ}53'33''$

33 $5^{\circ}23'33''$

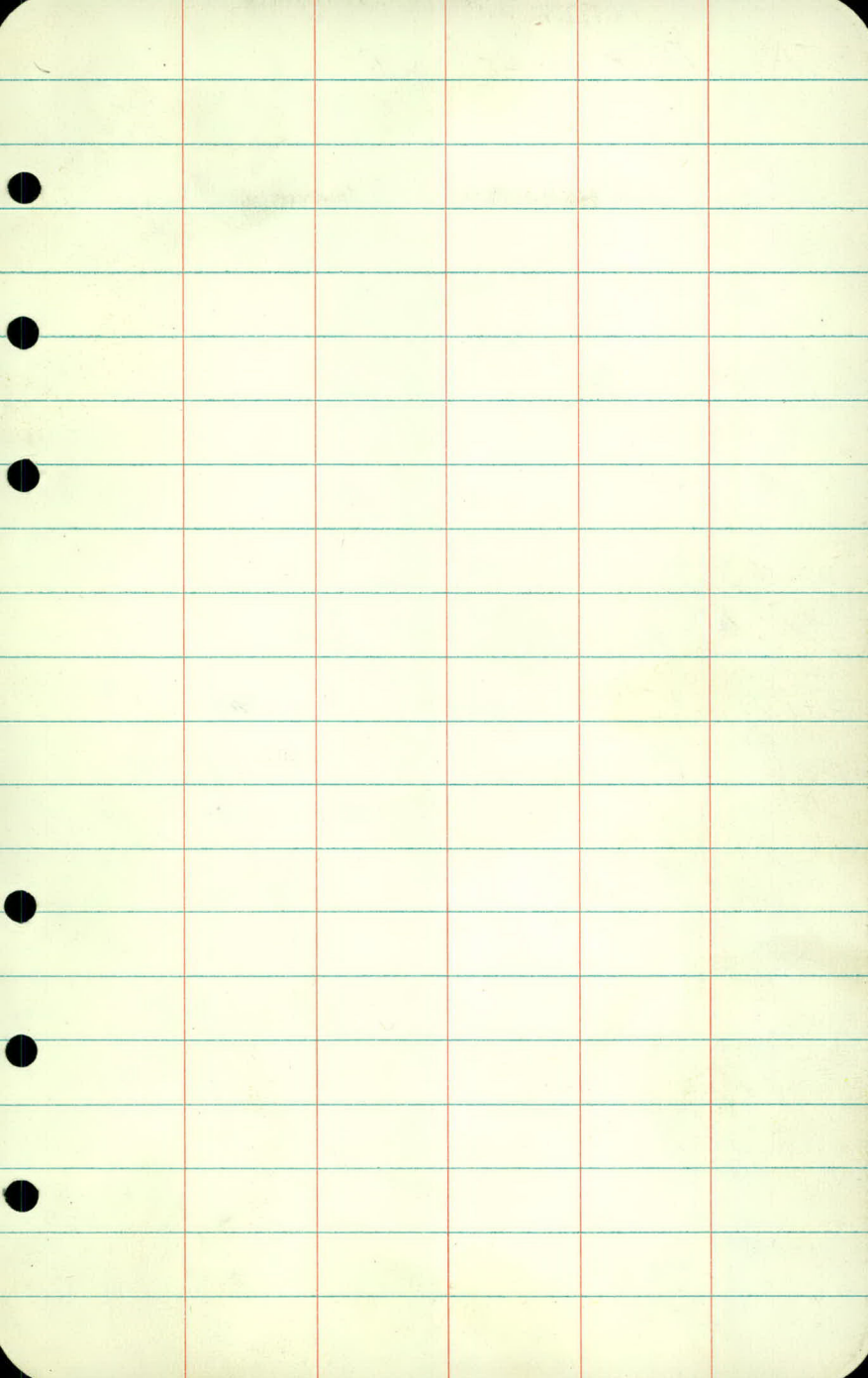
+50 $2^{\circ}53'33''$

32 $0^{\circ}23'33''$

331 + 92.15 PC $0^{\circ}00'$

252.90

50.05



STA

Point $\triangle \angle +$ ΔRT

337+77.93

PI

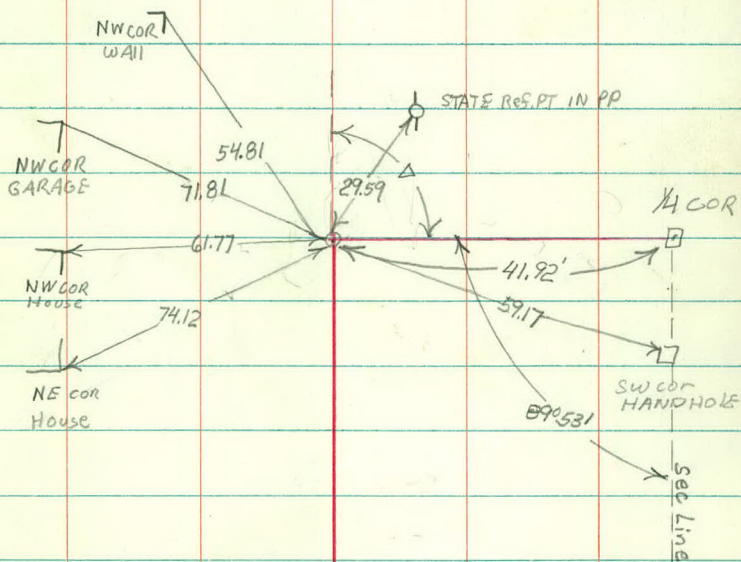
$$\Delta = 90^{\circ} 06' 00''$$

PK
CM
CP
BP

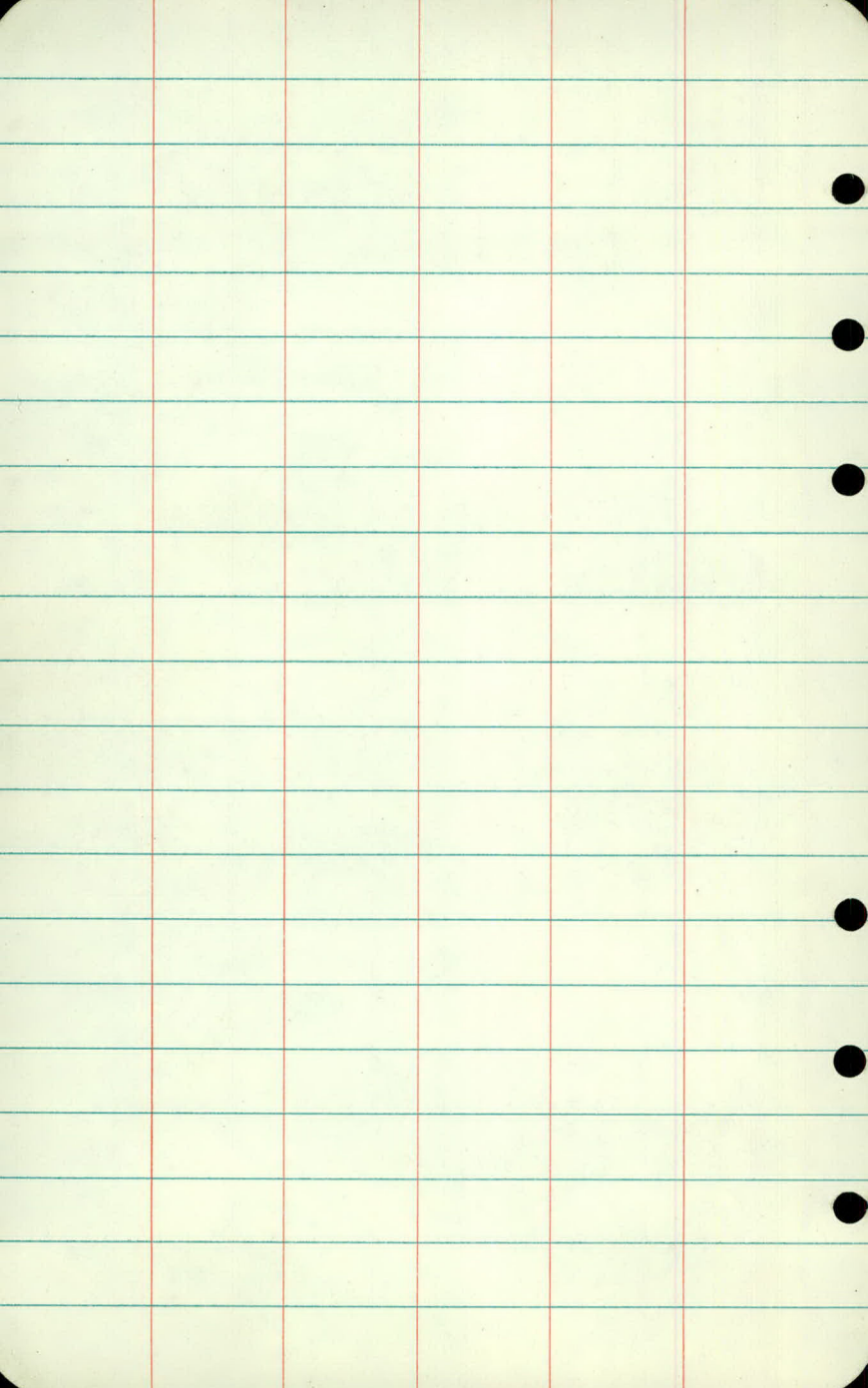
LT

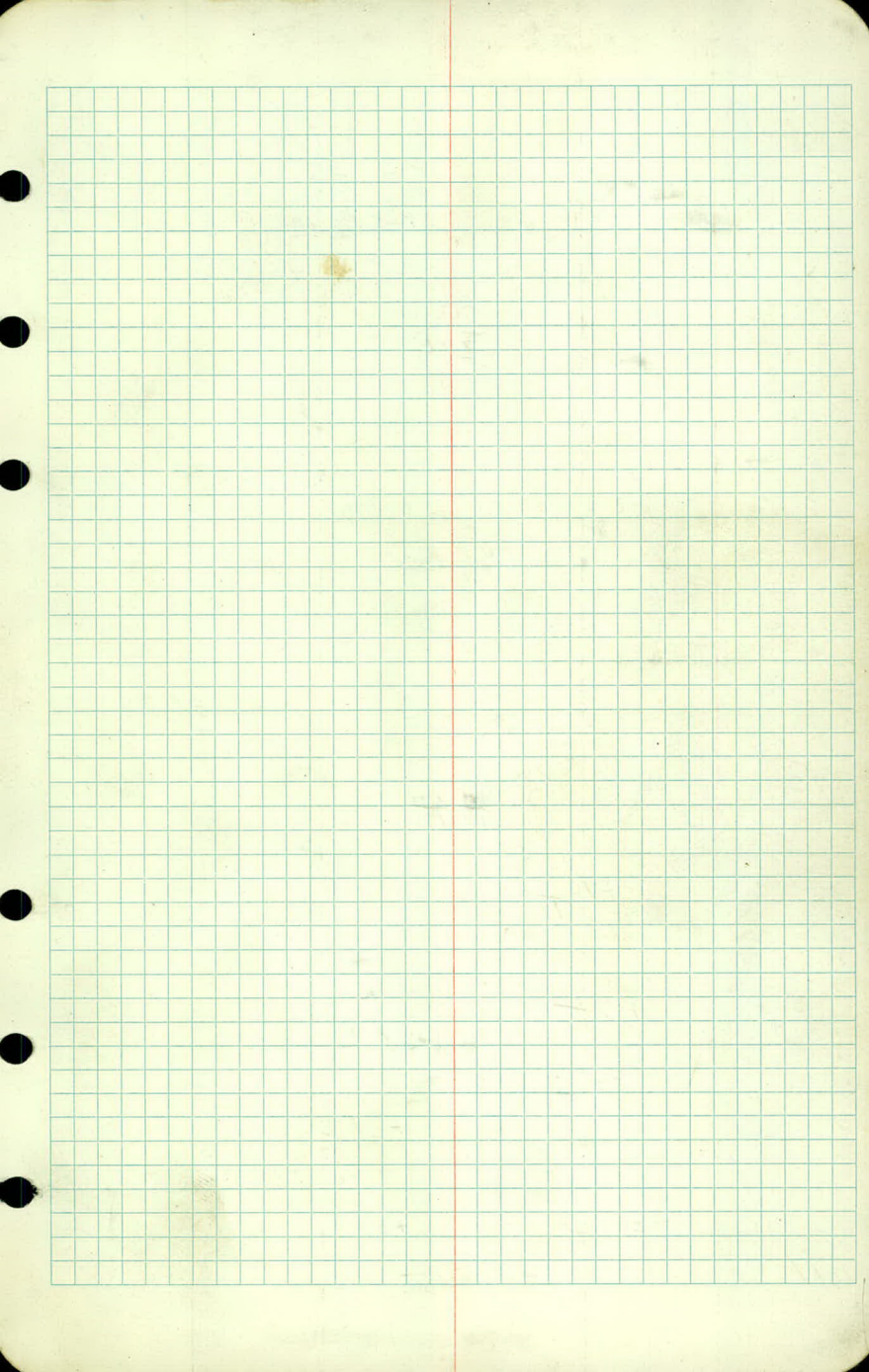
E

Aug 27 '70
RT



36 + 76.82





+50

L+

Φ

RT

+44 POR
49

+30 ER & BR
90

+20 Apron
60

+17 BR
110

173

B.I.T B.I.T
12 12

+50

B.I.T B.I.T
12 12

172

B.I.T B.I.T
12 12

+94 CONC CURB B.I.T CONC
61 78 14 29

+76 ER
11

+50

+58 POR
12

+56 CONC

+37 CONC Curb
16 35

+43 BR
25

+21 ER
24

+17 CONC

+16 ER & BR
26

+12 B.I.T
50

+12 CONC
39

+10 BR
64

+7 POR
44

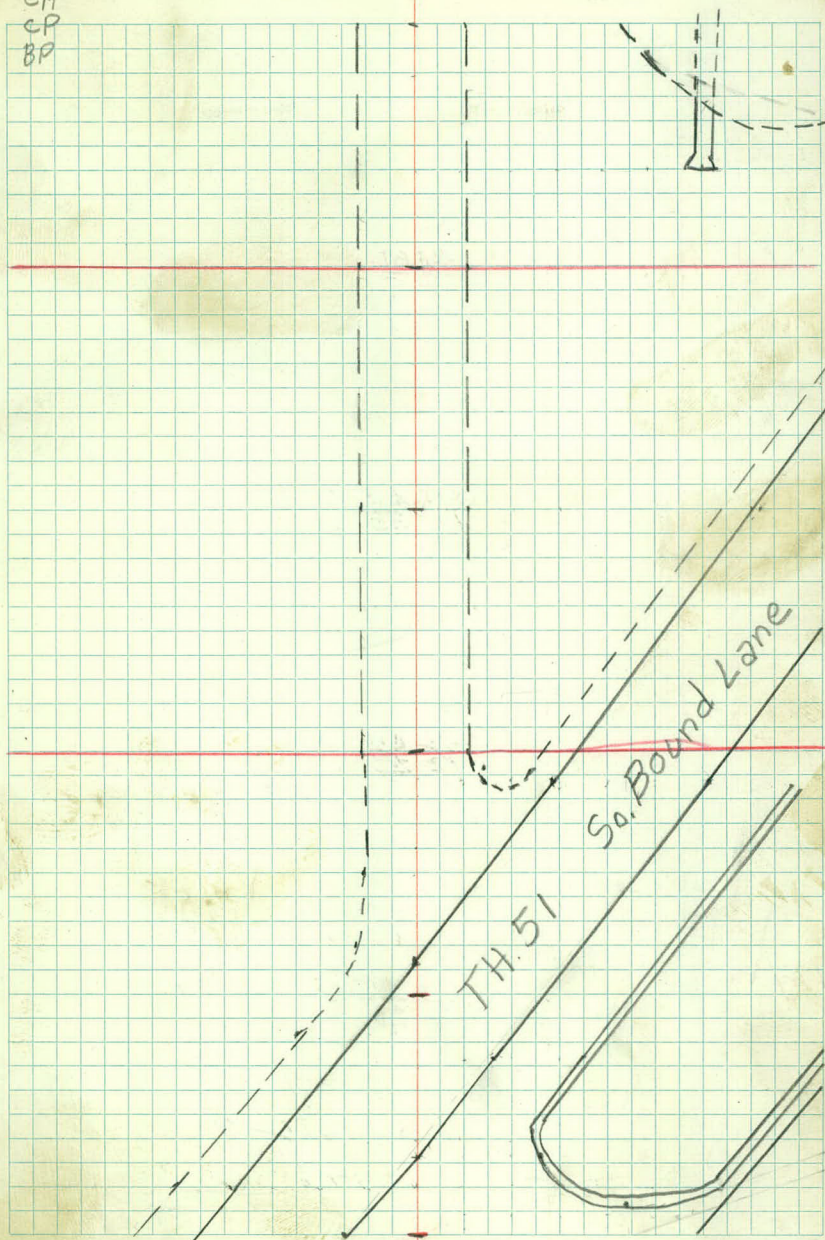
171

CONC
15

+4 CONC
55

PK
CM
CP
BP

June 29 '70 1



176

Lt

Q

Rt

$$+91 \frac{18'' \text{CM}}{32}$$

$$\frac{\text{B.I.T}}{12} \frac{\text{B.I.T}}{15}$$

$$+65 \frac{13' \text{BIT ENT} + 85 \text{ Range tie To ENT}}{42}$$

$$+78 \frac{\text{PP}}{54}$$

+50

$$\frac{\text{B.I.T}}{12} \frac{\text{B.I.T}}{17}$$

$$+38 \frac{\text{HYD}}{41}$$

$$+33 \frac{18' \text{CMP}}{31}$$

$$+38 \frac{\text{WSO}}{39}$$

175

$$\frac{\text{B.I.T}}{12} \frac{\text{B.I.T}}{20}$$

+50

$$\frac{\text{B.I.T}}{12} \frac{\text{B.I.T}}{22}$$

174

$$\frac{\text{B.I.T}}{12} \frac{\text{B.I.T}}{26}$$

+50

$$+67 \frac{\text{APRON}}{74}$$

$$+66 \frac{\text{BIT}}{74}$$

22, 12, 44

$$+56 \frac{\text{POR}}{74}$$

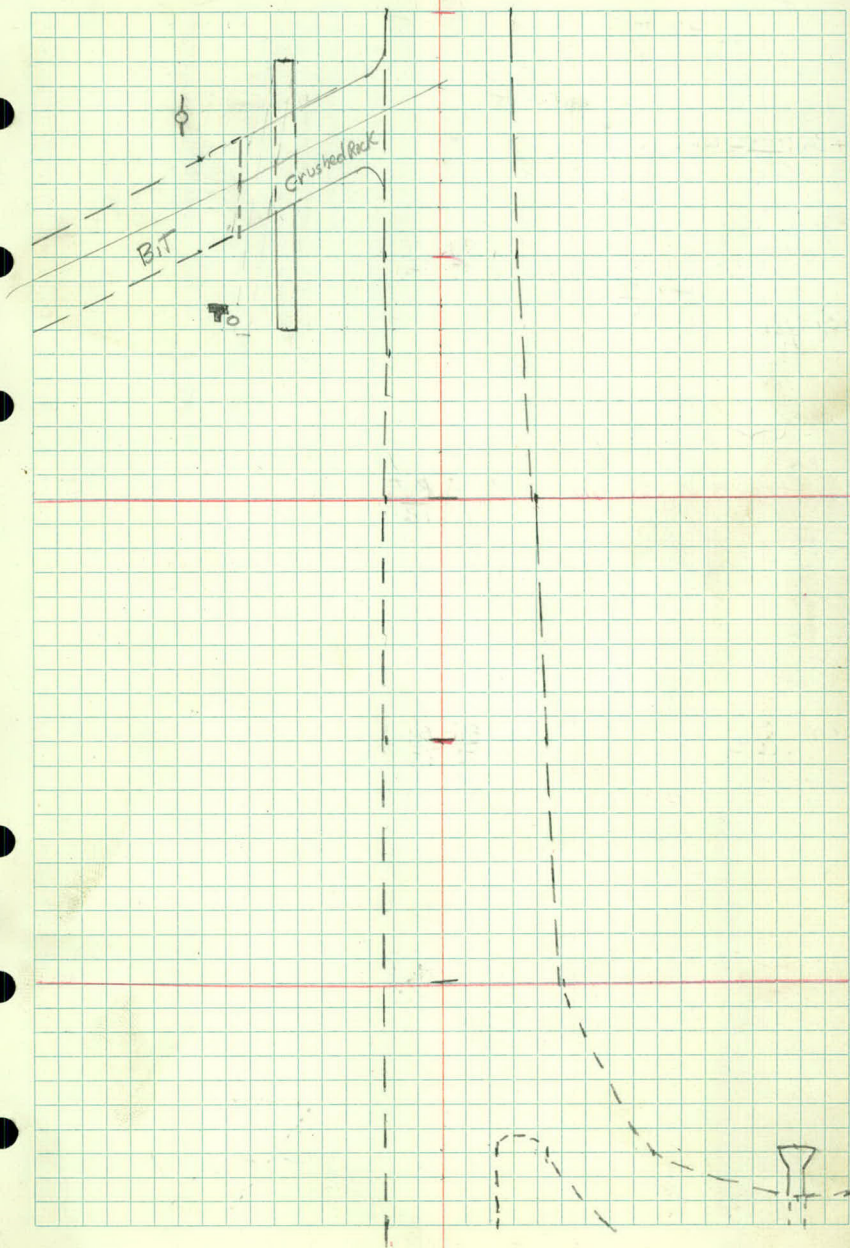
$$+57 \frac{\text{POR}}{100}$$

LT

£

RT

2



+50

LT

$\frac{B.T}{13}$

RT

+47 $\frac{22' ENT}{51}$ (4x4x7)
+34 $\frac{Cor Bldg}{51}$

+33 $\frac{B.T}{12}$

+34 $\frac{Fence wire}{51}$

178

$\frac{B.T}{12}$ $\frac{B.T}{13}$

+81 $\frac{Bush}{B1}$

+50

$\frac{B.T}{12}$

+38 $\frac{B.T}{12}$ +38 $\frac{PP}{50}$

177

$\frac{B.T}{12}$ $\frac{B.T}{12}$

+64 $\frac{E. Wing W.}{30}$

+64 $\frac{E. Wing W.}{27}$

+57 $\frac{Range Tie Totals}{17}$

+50 +56 $\frac{Wing W.}{18}$ +56 $\frac{Cor Br.}{17}$

+56 $\frac{Cor Bridge}{17}$ +56 $\frac{Wing W.}{18}$

+33 $\frac{Cor Bridge}{17}$

+33 $\frac{Wing W.}{19}$ +33 $\frac{Cor Bridge}{19}$

+33 $\frac{Wing W.}{18}$

+26 $\frac{E. Wing W.}{30}$

+26 $\frac{E. Wing W.}{30}$

176

$\frac{B.T}{12}$ $\frac{B.T}{15}$

June 30 1970 3

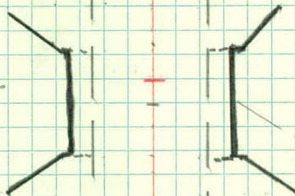
PK
CM
CP
BP

CRushed Rock ent.

w w w w w



NO APPARENT
Ditch



Existing Ditch

181

LT

$$\frac{B,T}{11} \quad \frac{B,T}{13}$$

RT

+50

$$+41 \frac{PP}{45}$$

$$+41 \frac{B,T}{10}$$

$$\frac{B,T}{14}$$

180

$$+90 \frac{ENT}{48}$$

$$+82 \frac{Post}{48}$$

$$+77 \frac{Post}{28} +82 \frac{Post}{39}$$

$$+69 \frac{Conc Fence}{51}$$

$$+69 \frac{H.V.D.}{25}$$

$$+69 \frac{B,T}{11}$$

$$+69 \frac{W.S.O.}{23}$$

$$\frac{B,T}{11} \quad \frac{B,T}{13}$$

+50

$$\frac{Fence}{51}$$

$$\frac{B,T}{11} \quad \frac{B,T}{13}$$

179

$$\frac{Fence}{51}$$

$$\frac{B,T}{12} \quad \frac{B,T}{13}$$

$$+91 \frac{PP}{47}$$

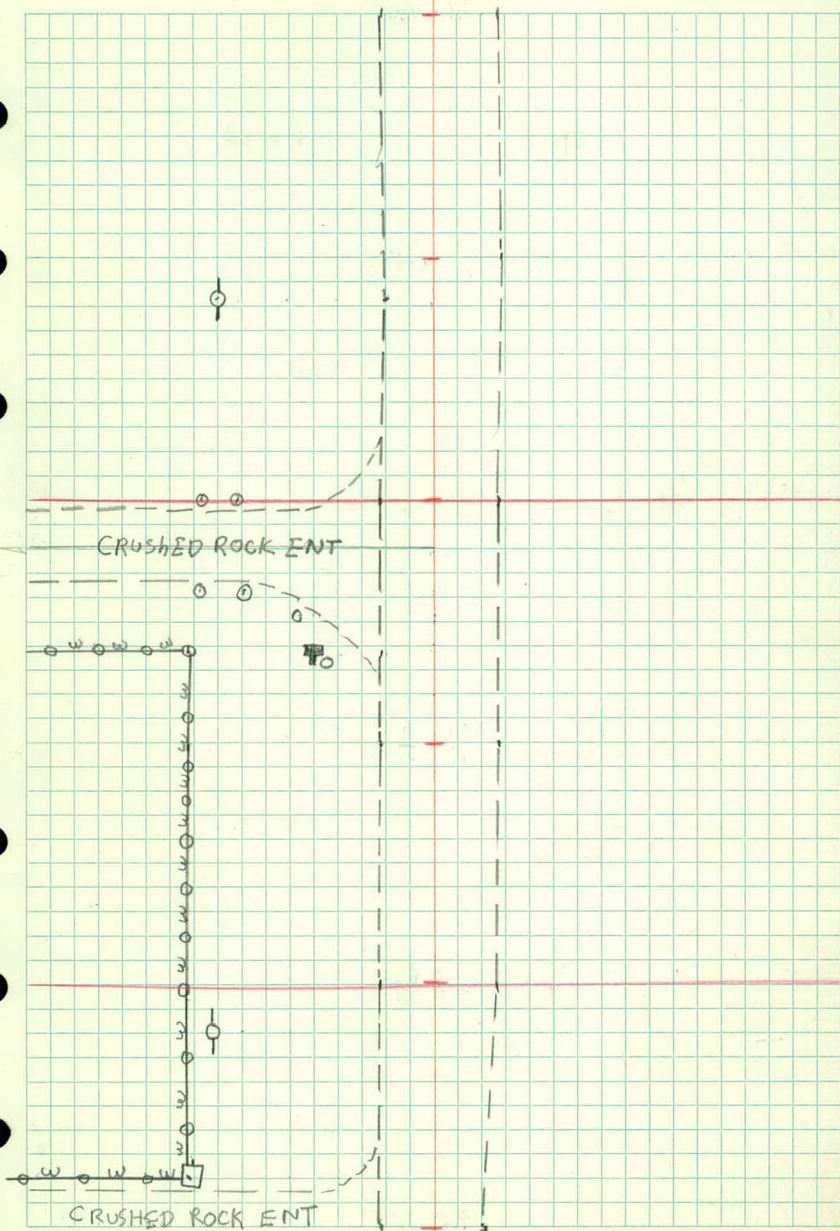
$$+64 \frac{B. Fence}{51}$$

$$+60 \frac{(4 \times 4 \times 7) Conc Pillar}{51}$$

$$+60 \frac{Fence}{51}$$

+50

$$\frac{B,T}{12} \quad \frac{B,T}{12}$$



+50

L+

$\frac{B.T}{11}$ $\frac{B.T}{14}$

R+

+37 $\frac{PP}{41}$

+37 $\frac{B.T}{11}$

183

$\frac{B.T}{11}$ $\frac{B.T}{14}$

wooded Area
26—

+50

+07 Beg Wooded AREA
26—

182

+86 $\frac{PP}{43}$

$\frac{B.T}{11}$ $\frac{B.T}{14}$

+50

$\frac{B.T}{12}$ $\frac{B.T}{14}$

181

$\frac{B.T}{11}$ $\frac{B.T}{13}$

①

WOODED
AREA

②

186

LT

$$\frac{B_1T}{10} \quad \frac{B_1T}{15}$$

RT

+50

Row Pine
55

$$\frac{B_1T}{10} \quad \frac{B_1T}{15}$$

$$+22 \frac{ER}{15}$$

$$+09 \frac{16"CM}{44}$$

$$+01 \frac{POR}{28}$$

$$+99 \frac{BR}{47}$$

$$+82 \frac{E \text{ Commings}}{24}$$

$$+68 \frac{ER}{50}$$

$$+60 \frac{POR}{32} \quad +57 \frac{16"CM}{42}$$

+50

+48 RANGETIC
TO ENT

$$+38 \frac{BR}{14}$$

$$+35 \frac{END \text{ woods}}{42}$$

$$+19 \frac{HYD}{24}$$

$$+19 \frac{WSO}{22}$$

$$+19 \frac{Beg \text{ Row } 8' \text{ Pine}}{55}$$

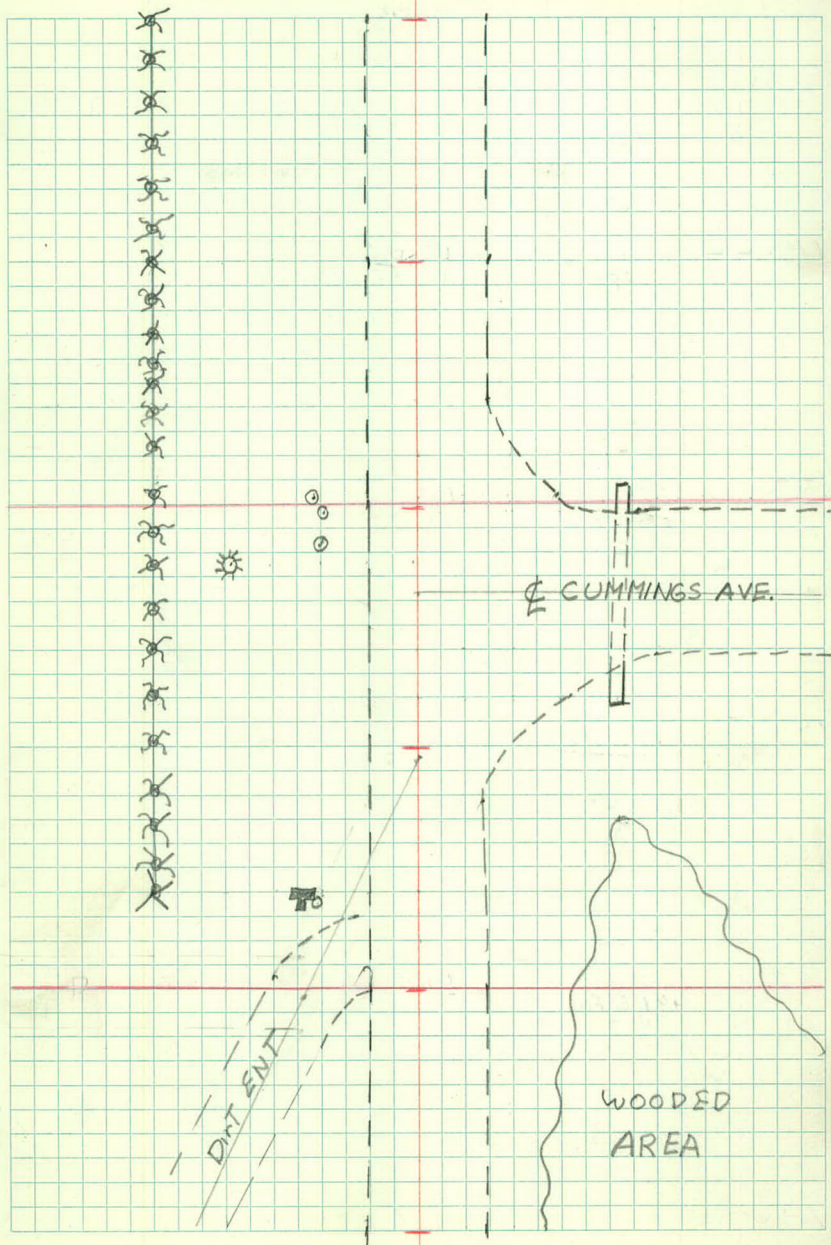
184

$$+98 \frac{E \text{ 18' ENT}}{24}$$

$$\frac{B_1T}{10} \quad \frac{B_1T}{14}$$

+50

$$\frac{B_1T}{11} \quad \frac{B_1T}{14}$$



+50

LT
Row Pine
60

¢
B.T. B.T.
11 12

RT
Beg Woods
70 —

188

+92 PP
54

B.T. B.T.
11 14

+95 2" Pine
69

+79 2" Pine
68

+65 2" Pine
67

+50

Row Pine
52

B.T.
10

+53 ¢ 12' ENT
64

+34 3" Pine
66

187

B. Row 8" Pine
53

B.T. D.T.
10 14

¢ 13' ENT
23

+72 ¢ 20' ENT +68 Rgth
55 To ENT

+50

+49 E. Row Pine
55

B.T. B.T.
9 15

+38 PP
38

186

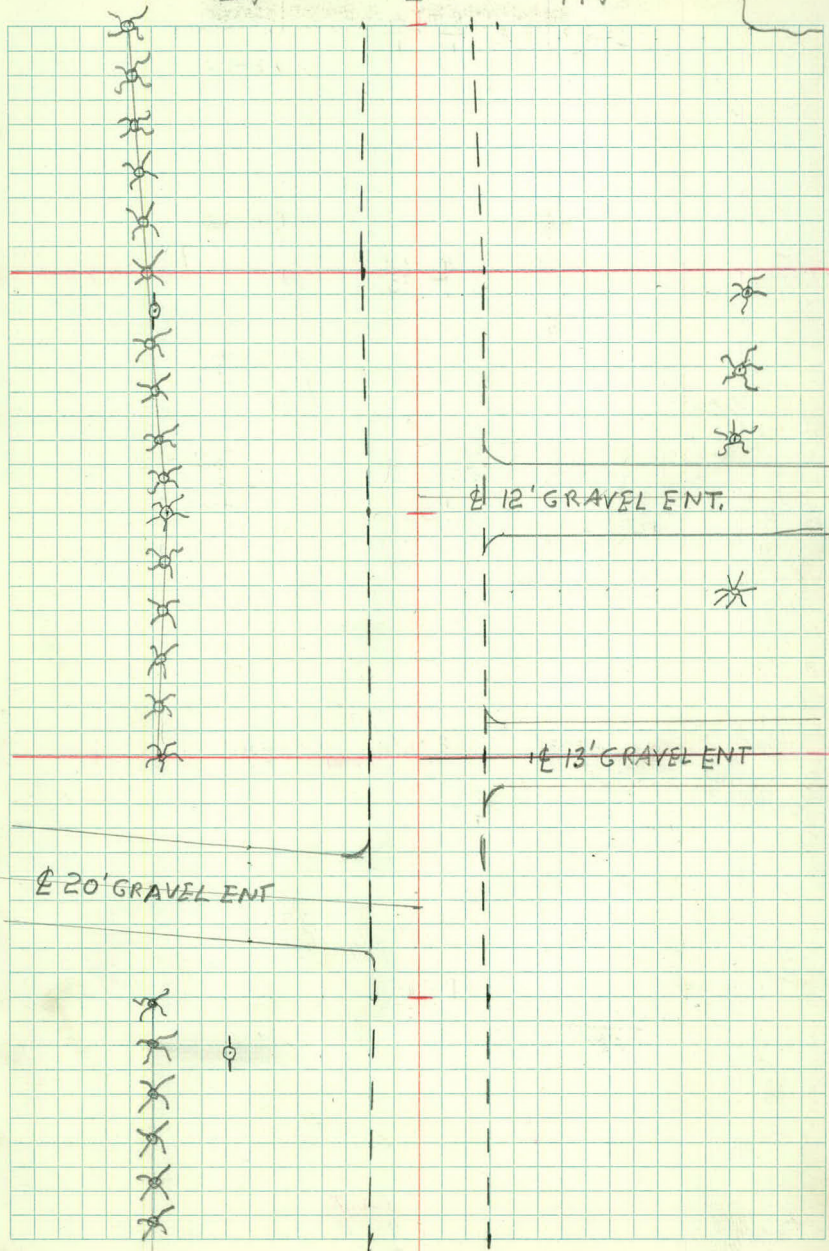
B.T. B.T.
10 15

LT

¢

RT

7



191

L+

$$\begin{array}{r} \text{B.T.} \\ 14 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 11 \end{array}$$

R+

$$+95 \frac{PP}{40}$$

$$+85 \text{ END Woods}$$

$$60-80$$

$$+75 \frac{36" \text{ Asp}}{50} +03 \frac{\text{woods}}{46-100+}$$

$$+74 \frac{28" \text{ Asp}}{70}$$

+50

$$\begin{array}{r} \text{B.T.} \\ 13 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 12 \end{array}$$

$$+48 \frac{\text{woods}}{42-75}$$

$$+38 \frac{\text{END Woods}}{42-75}$$

$$+10 \frac{\text{Beg Woods}}{45} +10 \frac{18" \text{ CMP}}{35}$$

$$+38 \frac{24" \text{ cotton wood}}{42}$$

190

$$\begin{array}{r} \text{B.T.} \\ 13 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 11 \end{array}$$

$$\frac{\text{woods}}{35}$$

$$+73 \frac{18" \text{ CMP}}{38}$$

+50

+39 PP

$$\begin{array}{r} \text{B.T.} \\ 10 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 12 \end{array}$$

$$\frac{\text{woods}}{37}$$

$$+20 \frac{\text{Stone } 2.5 \times 2.5 \text{ pillar}}{54}$$

$$+34 \frac{15" \text{ CMP}}{34}$$

$$+38 \frac{\text{HYD}}{25}$$

$$+38 \frac{\text{WSD}}{22}$$

$$+15 \frac{12" \text{ ENT}}{53} +13 \text{ Range Tie to ENT}$$

$$+03 \frac{\text{Stone } 2.5 \times 2.5 \text{ pillar}}{56}$$

$$\begin{array}{r} \text{B.T.} \\ 12 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 13 \end{array}$$

$$15" \text{ CM}$$

$$32$$

$$+91 \frac{\text{E. Row Pine}}{60}$$

$$+87 \frac{\text{HYD}}{38}$$

$$+87 \frac{\text{WSD}}{41}$$

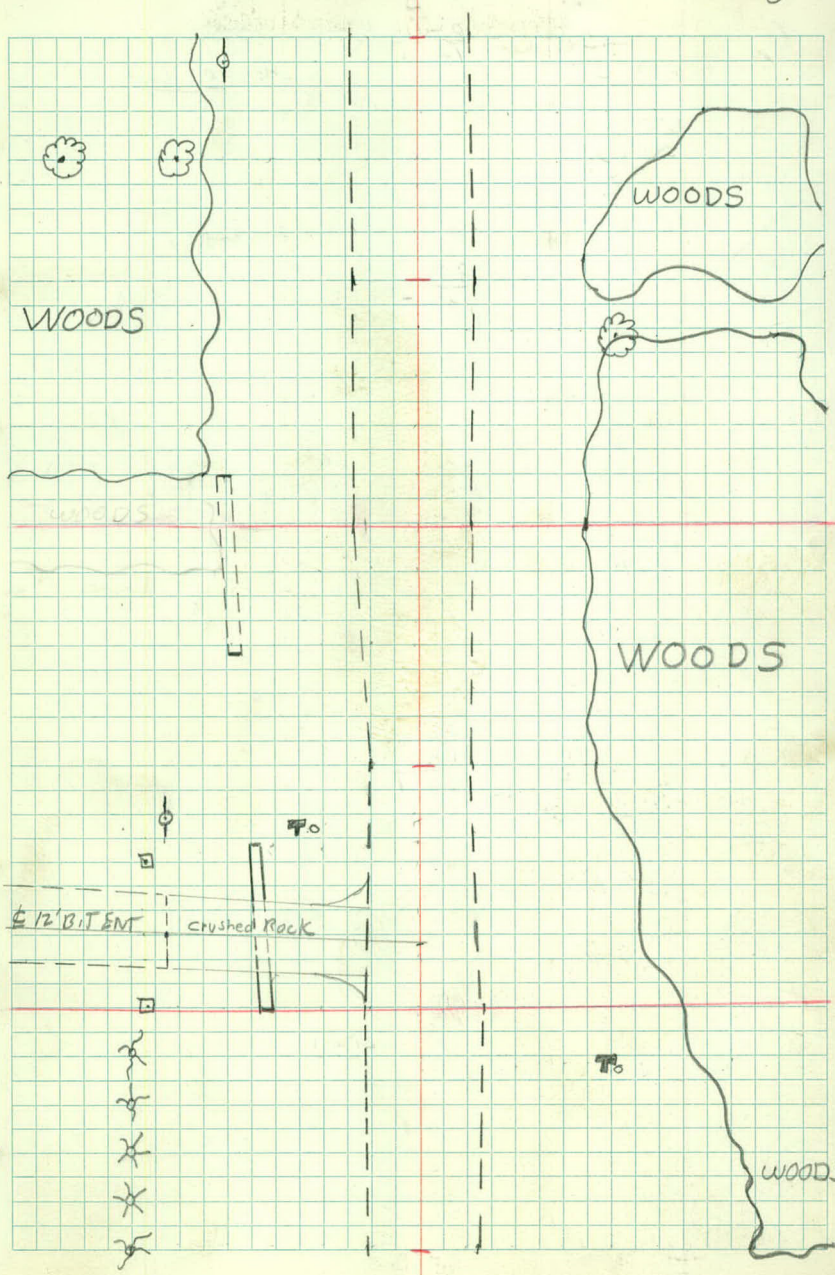
189

+50

$$\frac{\text{Row of Pine}}{60}$$

$$\begin{array}{r} \text{B.T.} \\ 11 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 12 \end{array}$$

$$\frac{\text{Beg Woods}}{70}$$



$$+50 \quad \begin{array}{r} \text{LT} \\ \text{WOODS} \\ 55 \end{array}$$

$$\text{B.T.} \quad \begin{array}{r} \text{14} \end{array}$$

RT

$$+40 \text{ ER} \\ 10$$

$$+20 \text{ WSO} \\ 26 \\ +13 \text{ WSO} \\ 24 \\ +10 \text{ WSO} \\ 27$$

$$+13 \text{ POR} \quad +17 \text{ HYD} \\ 18 \quad 91 \\ +10 \text{ BR} \quad +16 \text{ WSO} \\ 33 \quad 90$$

193

$$\text{B.T.} \\ 14$$

$$+84 \text{ ER} \\ 35$$

$$+97 \text{ \& Glenarden ch} \\ 35$$

+50

$$+40 \text{ PP} \\ 41$$

$$\text{WOODS} \\ 56$$

$$\text{B.T.} \\ 13$$

$$+79 \text{ POR} \\ 20 \\ +57 \text{ 1" Maple} \\ 50 \\ +43 \text{ BR} \\ 11$$

$$+17 \text{ \& 10' GRAV. ENT.} \\ 38$$

$$+20 \text{ 1" Maple} \\ 52$$

192

$$\text{WOODS} \\ 40 \\ +77 \text{ RANGE 1/2} \\ \text{TO ENT}$$

$$\text{B.T.} \\ 13$$

$$\text{B.T.} \\ 10$$

$$+83 \text{ 2" Pine} \quad +83 \text{ 2" Pine} \\ 40 \quad 46 \\ +71 \text{ 1" Ash} \\ 60 \\ +61 \text{ 1" OAK} \\ 49 \\ +52 \text{ STUMP} \quad +52 \text{ 1" Ash} \\ 43 \quad 33 \\ +42 \text{ 1" Ash} \\ 33 \\ +40 \text{ STUMP} \\ 43$$

+50

$$\text{B.T.} \\ 12$$

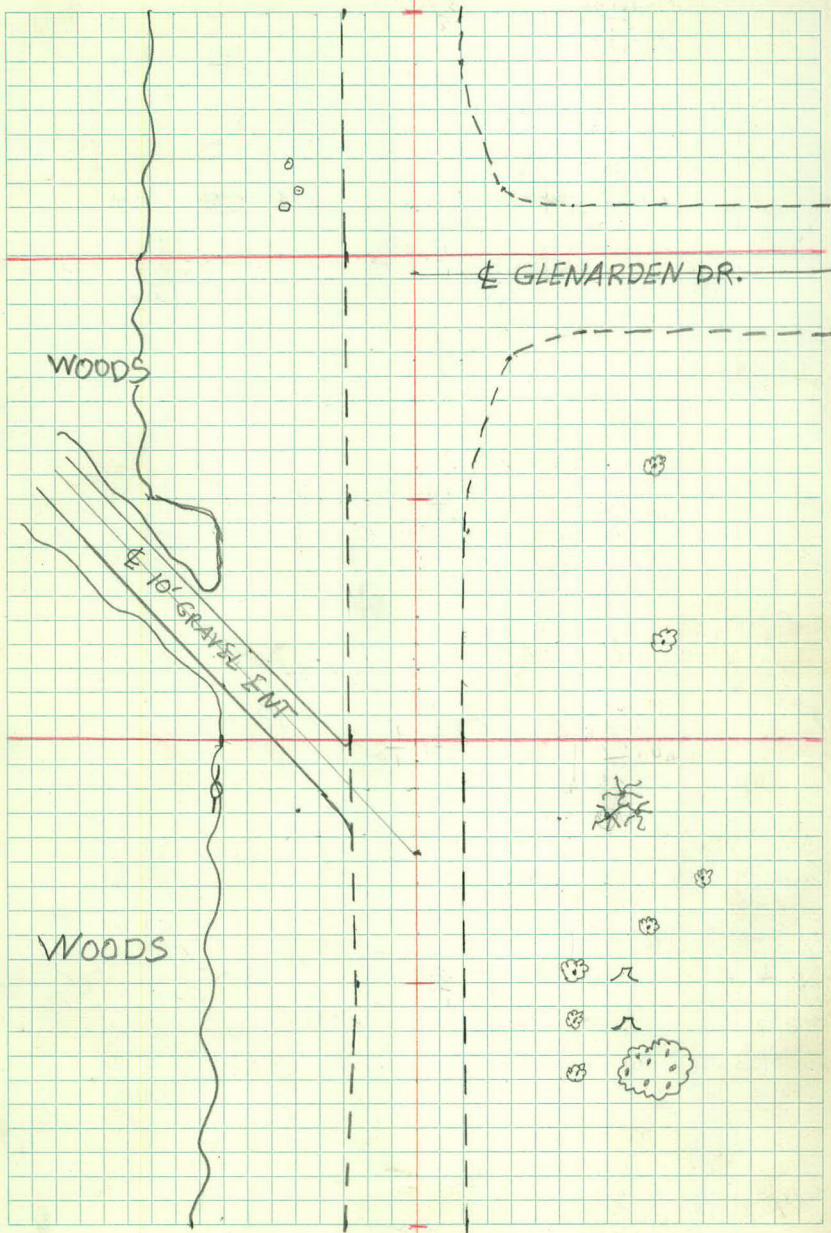
$$+31 \text{ 1" Ash} \quad +31 \text{ 7" Ash} \\ 33 \quad 43-51$$

191

$$\text{WOODS} \\ 46$$

$$\text{B.T.} \\ 14$$

$$\text{B.T.} \\ 11$$



196

LT
WOODS
54
+82 PP
41
+75 15' CMP
38

BIT BIT
13 11

R7
Shoreline
45

+93 24' willow
40

+79 36" cottonwood
30

+55 15' gravel ENT
33

+72 36" cottonwood

+50

+49 RANGELAND
TO ENT

BIT
13

+60 36" cottonwood shoreline
30 44

+50 36" cottonwood
27

+32 15' CMP
31

+10 WOODS
52

WOODS
55

BIT
13

BIT
11

Shoreline
45

195

+69 36" cottonwood
34

+50

+40 14" OAK WOODS
57 57

BIT
13

BIT
11

+62 Shoreline
47

+59 36" cottonwood
34

+15 20" OAK
57

+25 Shoreline
47

+9 HYD +9 WSO
27 25

+02 PP
42
WOODS
57

BIT
13

BIT
11

+20 4" Elm
29

Shoreline
57

194

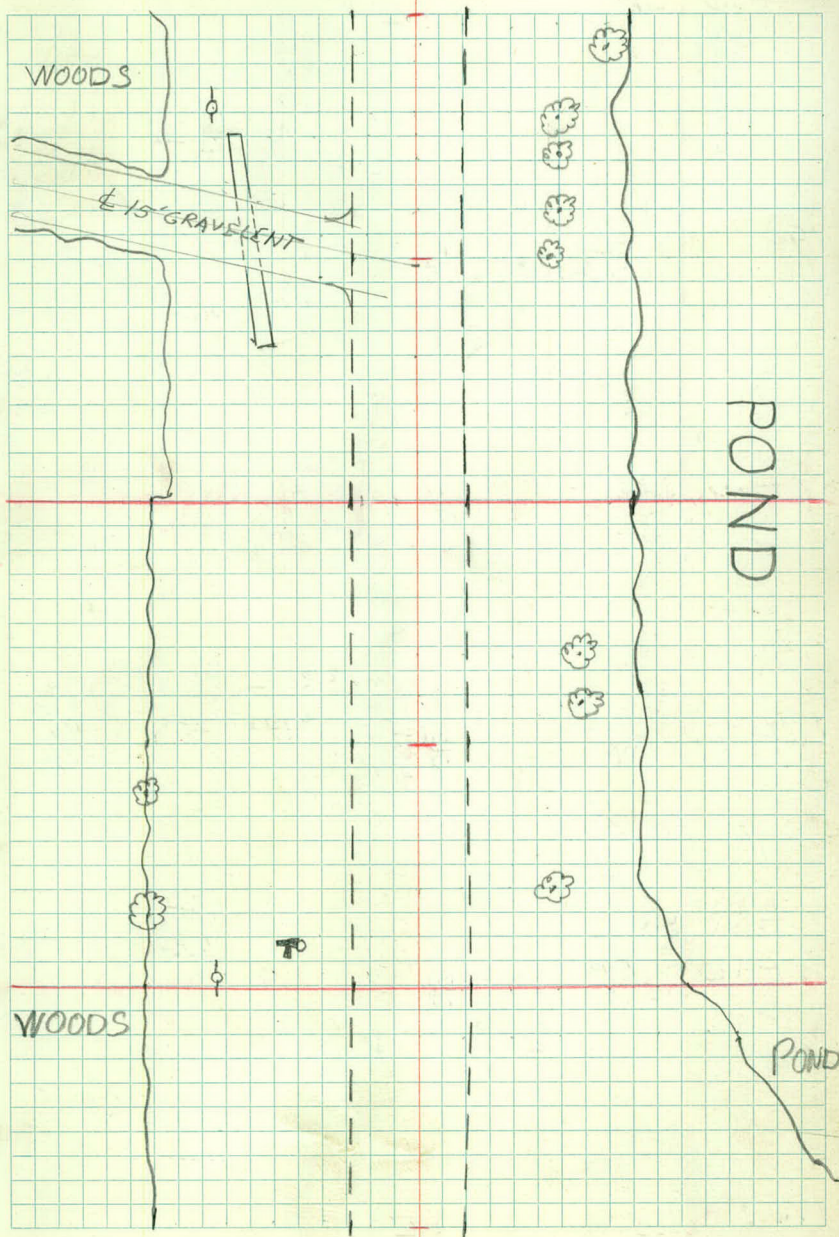
+88 Shoreline
67

+60 Shoreline
105

+50

WOODS
55

BIT BIT
14 10



+50 LT E RT

+48 $\frac{490}{26}$ +49 $\frac{BR}{12}$

+32 $\frac{16}{86}$ cottonwood

-136 $\frac{2}{42}$ OAK +47 $\frac{7}{44}$ OAK

198

+11 $\frac{Twins 8" Elm}{55}$
+99 $\frac{Quad 8" OAK}{75}$

B.T B.T
13 12

+99 Trip 4" poplar
44

+78 $\frac{Box Elm 4"}{39}$

+82 $\frac{36" ELM}{61}$

+65 $\frac{Twins 12" willow}{39}$

+70 $\frac{12" willow}{42}$

+50

+40 $\frac{PP}{42}$

B.T
13

+1/2 $\frac{ABANDONED}{56}$ sewer

+46 shoreline
61-90
+40 $\frac{8" willow}{47}$

+19 $\frac{9" willow}{42}$

+43 $\frac{Twins willow}{49}$

+28 $\frac{shoreline}{59}$

+36 $\frac{cottonwood}{40}$

+129 $\frac{Twins 12" willow}{34}$

+12 $\frac{shoreline}{57}$

+104 $\frac{Trip 8" willow}{47}$

+7 $\frac{8" willow}{47}$

+8 $\frac{24" cottonwood}{55}$

197

B.T B.T
13 11

+6 $\frac{Poplar}{32}$ +12 $\frac{Poplar}{39}$

+44 shoreline

+78 $\frac{18" willow}{41}$

+85 $\frac{10" willow}{45}$

+9 $\frac{4 1/4" willow}{44}$

+71 $\frac{8" willow}{40}$

+75 $\frac{6" cottonwood}{44}$

+66 $\frac{6" Poplar}{44}$

+70 $\frac{12" cottonwood}{44}$

+62 $\frac{2" willow}{38}$

+63 $\frac{2" Poplar}{45}$

+63 $\frac{2" Poplar}{30}$

+68 $\frac{36" cottonwood}{79}$

+52 $\frac{18" willow}{40}$

+59 $\frac{4" Poplar}{42}$

+50

B.T
13

+42 $\frac{Twins 24" cottonwood}{30}$

+39 $\frac{10" willow}{40}$

+39 $\frac{10" Poplar}{41}$

+22 $\frac{36" cottonwood}{36}$

+13 $\frac{24" willow}{38}$ +17 $\frac{37" cottonwood}{31}$

+25 woods
100

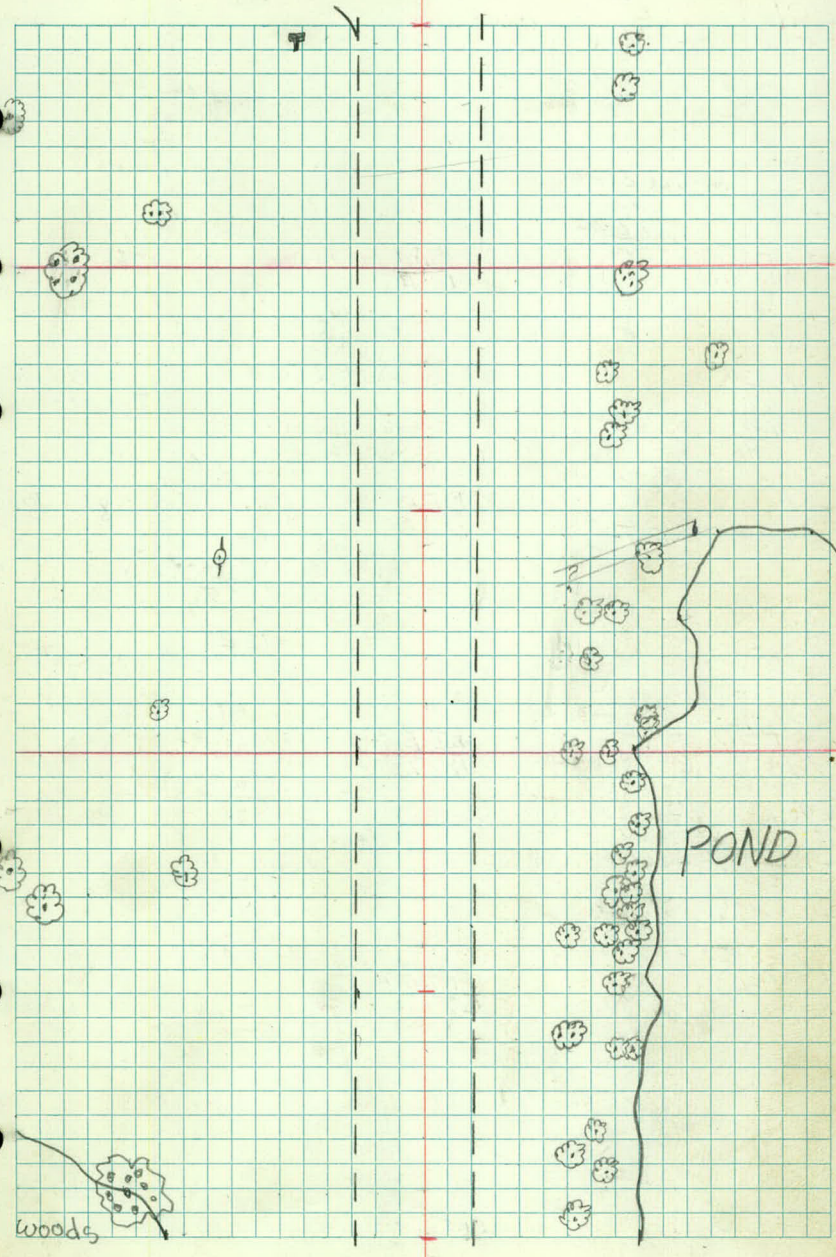
+09 $\frac{9 oak trees}{63}$
woods
54

196

B.T B.T
13 11

+04 $\frac{36" cottonwood}{32}$

Shoreline
45



woods

POND

201

LT

BIT BIT
11 14

RT

+83 $\frac{2'' \text{ Spruce}}{75}$

+82 $\frac{10'' \text{ Ash}}{80}$

+92 $\frac{12'' \text{ Oak}}{85}$

+65 $\frac{2'' \text{ Spruce}}{75}$

+51 $\frac{2'' \text{ Spruce}}{74}$

+50

BIT +52 $\frac{\text{Quad 4'' Ash}}{79}$
11 13 PP

+36 ER
14

+25 POR
16

+35 $\frac{2'' \text{ Spruce}}{75}$

+4 PP
41

+6 $\frac{2'' \text{ Spruce}}{74}$

+16 $\frac{2'' \text{ Spruce}}{74}$

+24 BR
36

200

+00 $\frac{2'' \text{ Pine}}{71}$

+92 $\frac{2'' \text{ Pine}}{73}$ ✓

BIT BIT
12 13

+00 $\frac{\text{SKILLS}}{28}$

+90 R & Tie to 8 =

+88 ER
31

+83 POR
20

+72 BR
13

+50

+52 $\frac{2'' \text{ Pine}}{75}$ ✓

BIT BIT
12 13

+46 $\frac{\text{Twins 8'' Password}}{88}$

+40 $\frac{2'' \text{ Pine}}{77}$ ✓

+47 $\frac{2'' \text{ Pine}}{80}$

+13 $\frac{2'' \text{ Pine}}{86}$ ✓

+20 $\frac{2'' \text{ Pine}}{83}$ ✓

+29 $\frac{2'' \text{ Pine}}{79}$ ✓

+410 $\frac{1'' \text{ Pine}}{92}$

+5 ER
12

+6 $\frac{2'' \text{ Pine}}{87}$ ✓

+05 $\frac{\text{SKILLS}}{12}$

199

15 $\frac{1'' \text{ Pine}}{71}$ ✓

+83 BR
33

BIT BIT
12 12
+93 POR
18

+76 $\frac{\text{SKILLS}}{115}$ ✓

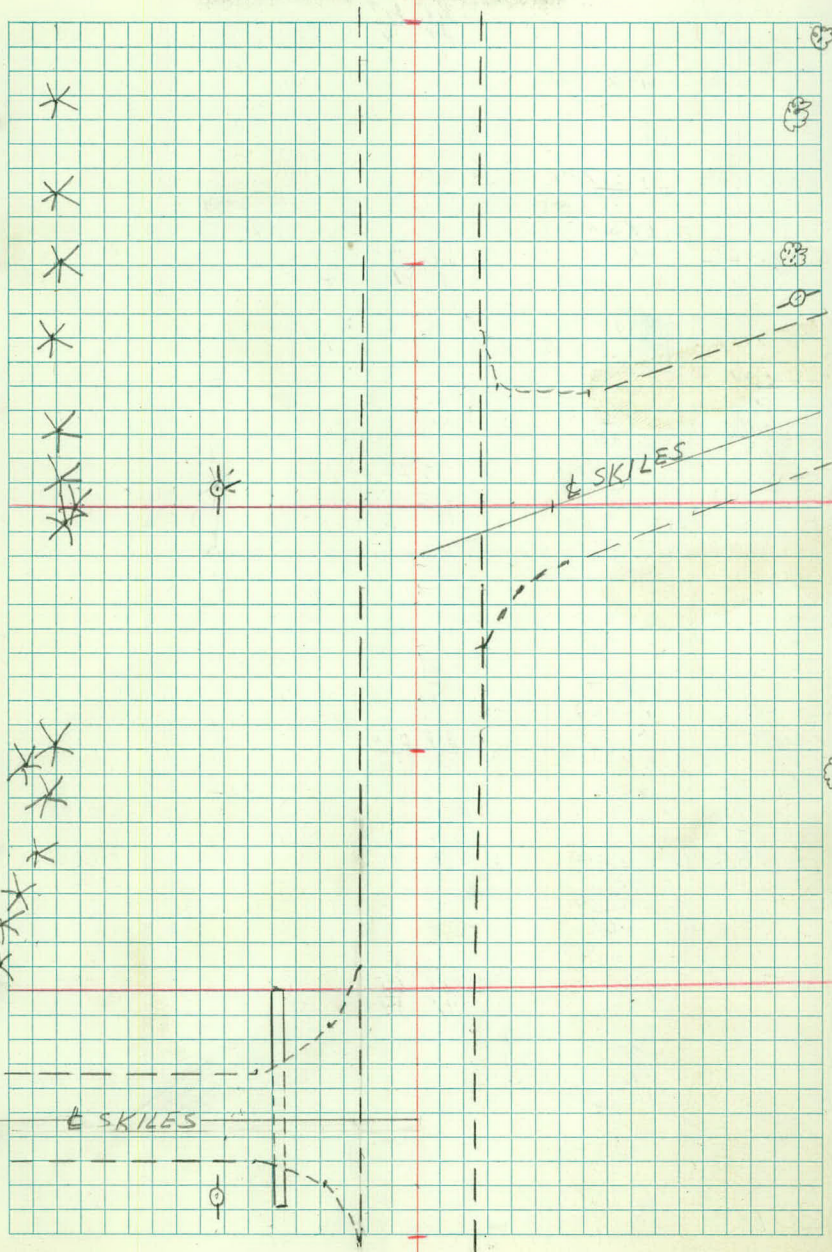
+65 ER
33

+60 POR
19

+50

+58 PP
42

156 $\frac{\text{ENRASH}}{28}$ BIT
12 12



+50

LT

¢

RT

B.I.T. B.I.T.
10 14+27 $\frac{2'' \text{Pine}}{43}$ +34 $\frac{2'' \text{Maple}}{43}$ +19 $\frac{2'' \text{Pine}}{43}$ +24 $\frac{12'' \text{Oak}}{71}$ +22 $\frac{2'' \text{Pine}}{43}$ +30 $\frac{\text{WSD}}{85}$ +2 $\frac{2'' \text{Pine}}{43}$ +7 $\frac{2'' \text{Pine}}{43}$ +14 $\frac{2'' \text{Pine}}{43}$ +18 $\frac{\text{ER}}{15}$ +30 $\frac{14 \text{ D}}{87}$ +6 $\frac{\text{POR}}{20}$ +10 $\frac{\text{BIR}}{37}$ 203 +98 $\frac{3'' \text{Pine}}{43}$ +12 $\frac{2'' \text{Pine}}{44}$ B.I.T. B.I.T.
10 15+91 $\frac{\text{Forest Lane}}{33}$ +86 $\frac{\text{R. 21 E Forest Lane}}{37}$ +86 $\frac{3'' \text{Pine}}{44}$ +12 $\frac{2'' \text{Pine}}{44}$ +73 $\frac{1'' \text{Pine}}{49}$ +80 $\frac{3'' \text{Pine}}{49}$ +66 $\frac{\text{PP}}{41}$ +88 $\frac{\text{ER}}{31}$ +57 $\frac{5'' \text{Oak}}{77}$ +58 $\frac{3'' \text{Oak}}{77}$ +60 $\frac{\text{100 Oak}}{77}$ +74 $\frac{\text{POR}}{21}$ +74 $\frac{18'' \text{CM}}{34}$ +55 $\frac{9'' \text{Oak}}{76}$ +69 $\frac{\text{OK}}{14}$

+50

B.I.T. B.I.T.
11 14+45 $\frac{10'' \text{Oak}}{76}$ +18 $\frac{1'' \text{Maple}}{65}$ +11 $\frac{2'' \text{Pine}}{67}$ +14 $\frac{2'' \text{Pine}}{65}$ +105 $\frac{2'' \text{Maple}}{64}$ +102 $\frac{2'' \text{Pine}}{64}$ +2 $\frac{2'' \text{Pine}}{66}$

202

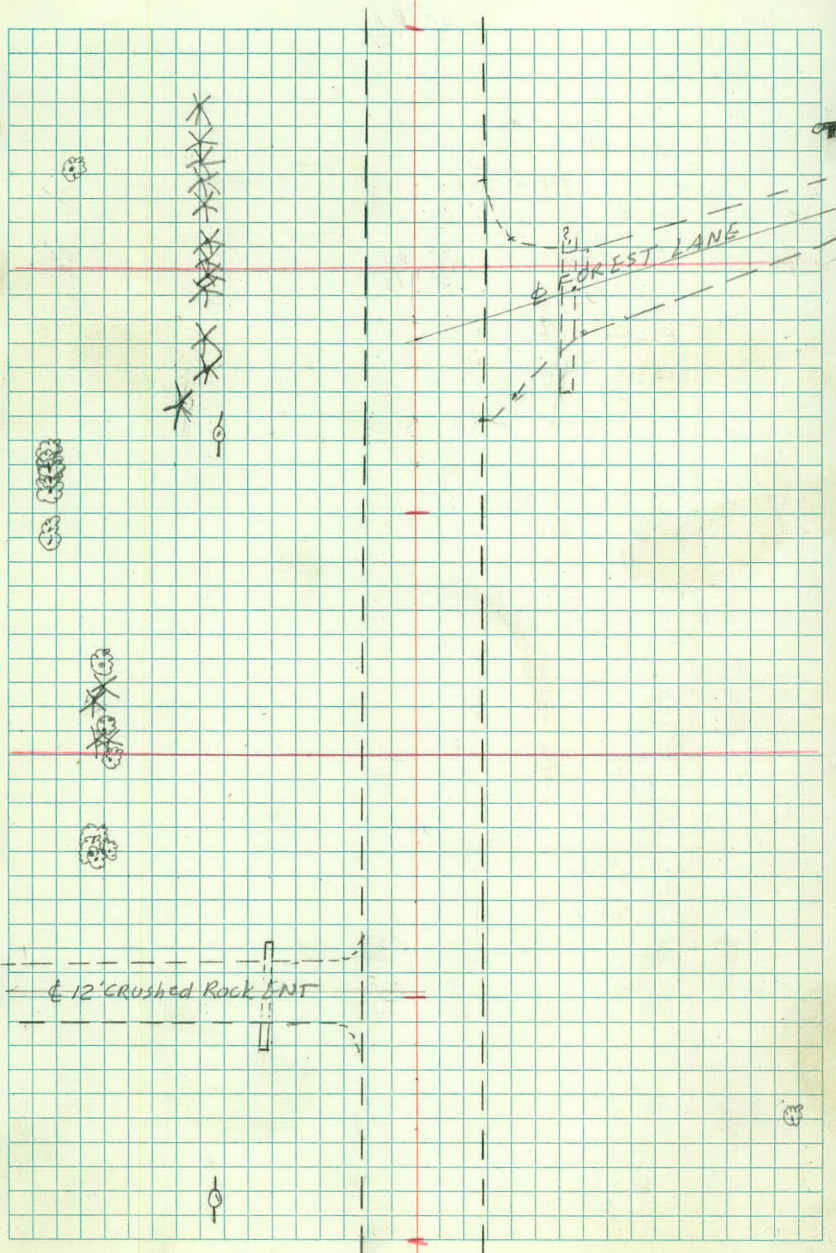
B.I.T. B.I.T.
11 14+99 $\frac{2'' \text{Pine}}{64}$ +82 $\frac{14'' \text{Oak}}{67}$ +78 $\frac{14'' \text{Oak}}{66}$ +79 $\frac{14'' \text{Oak}}{67}$ +79 $\frac{14'' \text{Oak}}{64}$ +62 $\frac{\text{CMP 12''}}{30}$

+50

B.I.T. B.I.T.
11 14+51 $\frac{\text{ENT}}{12' \text{ C.R.}}$ +39 $\frac{\text{CMP}}{31}$ +24 $\frac{3'' \text{Oak}}{77}$

201

+9 $\frac{\text{PP}}{41}$



206

LT

$$\begin{array}{r} \text{BIT} \\ 10 \end{array} \quad \begin{array}{r} \text{BIT} \\ 15 \end{array}$$

RT

+92 RT To

Arden PL

+87 $\frac{1}{2}$ Arden PL+75 $\frac{1}{2}$ ER

36

+68 Por

20

+50

+52 $\frac{1}{2}$ BR

10

$$\begin{array}{r} \text{BIT} \\ 10 \end{array} \quad \begin{array}{r} \text{BIT} \\ 15 \end{array}$$
+42 $\frac{3}{4}$ willow

50

+32 $\frac{2}{4}$ willow

68

+21 $\frac{3}{4}$ willow

50

205

+02 $\frac{1}{2}$ OAK

88

+89 Trip 8" OAK

85

$$\begin{array}{r} \text{BIT} \\ 10 \end{array} \quad \begin{array}{r} \text{BIT} \\ 15 \end{array}$$

+69 Twin 6" Oak

82

+40 Twin 10" OAK

77

+50

+50 Twin 8" OAK

80

+43 $\frac{5}{8}$ willow

54

+40 PP

41

+19 $\frac{1}{2}$ willow

54

+12 $\frac{5}{8}$ OAK 10"

80

$$\begin{array}{r} \text{BIT} \\ 10 \end{array} \quad \begin{array}{r} \text{BIT} \\ 14 \end{array}$$

204

+88 $\frac{1}{2}$ Birch

55

+65 $\frac{4}{8}$ Pine

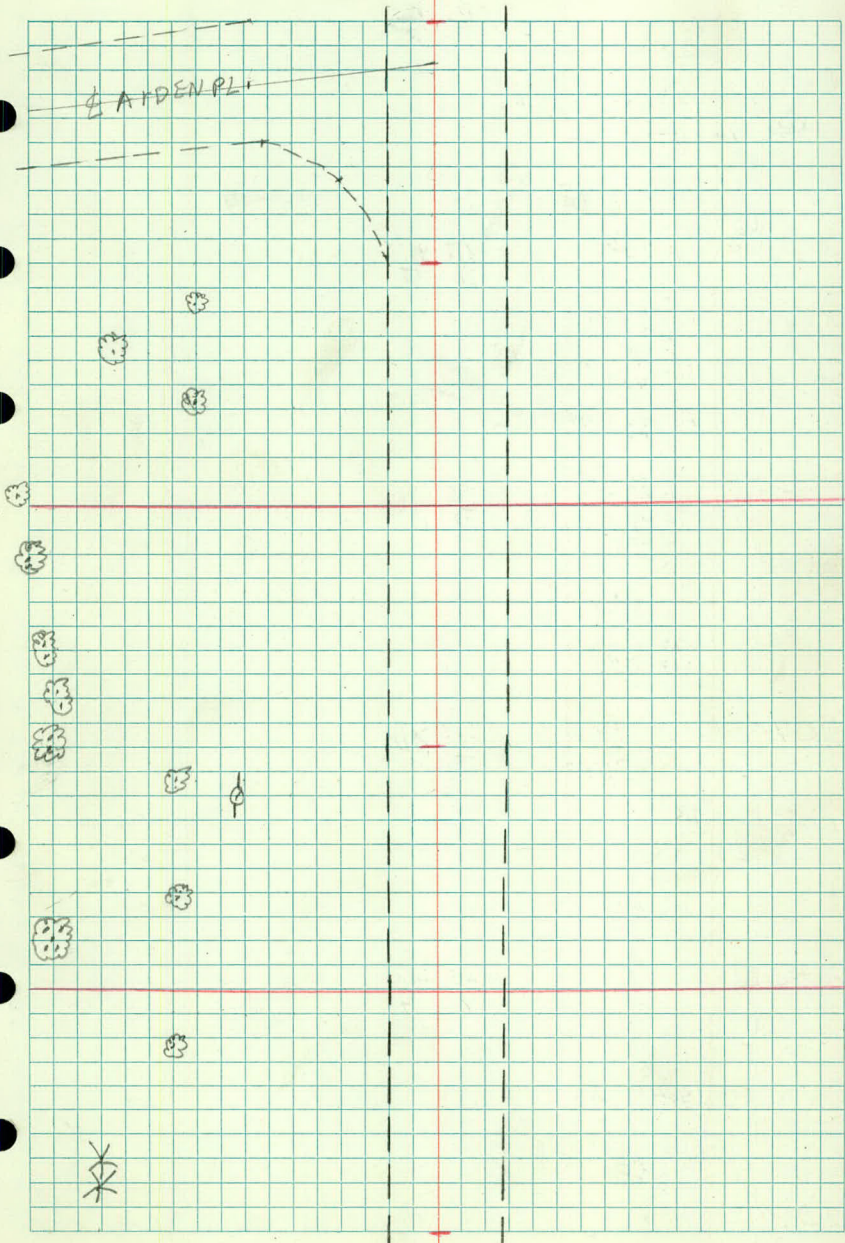
70

+50

+59 $\frac{4}{8}$ Pine

70

EARDEN PL.



+50 LT

BIT
11

RT
BIT
97-69

+28 OAK
+37 72 OAK
+18 71
+12 85 OAK +16 86 OAK
+05 80 OAK
+00 3 OAKS 18"

+18 Berry Tree
+08 Berry Tree

208 87 PP +89 70 +94 2" Gum 75 +97 Berry Tree 44 BIT BIT
+90 3" Plum 73 +85 Berry Tree 49 +85 Russian Olive GB 14
+73 Russian Olive 2" 64 +77 2" Plum 66 +82 Russian Olive GB
+69 Russian Olive 2" 64 +73 Berry Tree 44
+57 Quad 4" OAK 62 +68 9" OAK 88

BIT
44-68

+87 ER 14 +78 HYD 84 +78 WSO 81
+78 BIT 40-67
+66 POR 30

+50 Berry Tree 34 BIT 10

+31 15 ENT 34
+19 20" OAK 82

+17 PP 58

+29 ER 49
+11 POR 32

207 +94 20" OAK 88 BIT BIT
+80 18" OAK 89 +83 10' Drive BIT 10 14
+82

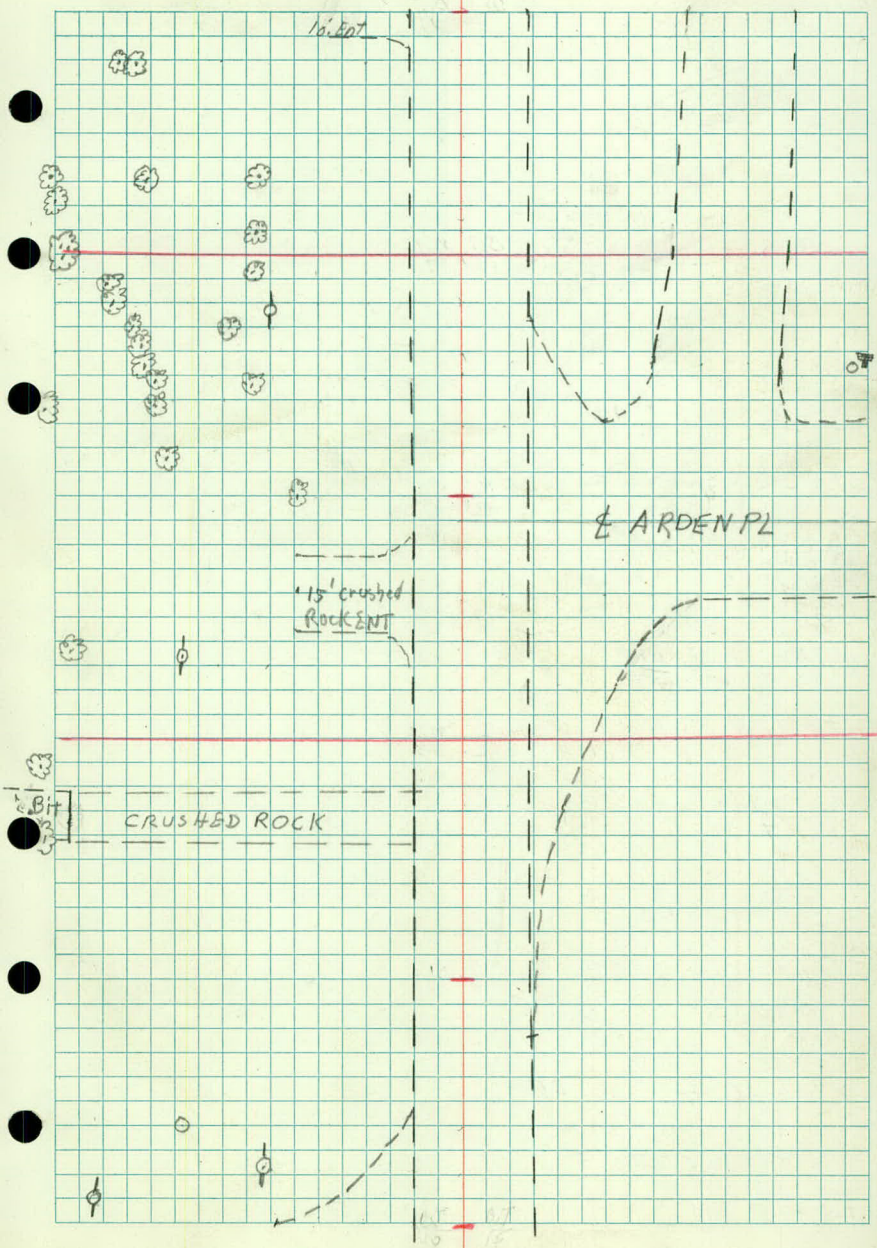
+86 POR 21

+50 +39 24" OAK 94 BIT BIT
10 14

+39 BR 14

+21 Air Raid pole 58 +22 ER 10
+05 PP 77 +12 PP 41

206 38 +07 POR 23 BIT BIT
10 15



211

LT

L

RT

$$\begin{array}{r} \text{B.T.} \\ 12 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 13 \end{array}$$

$$\begin{array}{r} \text{B.T.} \\ 54-73 \end{array}$$

$$+82 \frac{8'' \text{ OAK}}{62}$$

$$+54 \frac{\text{WSD}}{27} \quad +54 \frac{\text{HYD}}{24}$$

+50

$$+49 \frac{6'' \text{ OAK}}{82}$$

$$\begin{array}{r} \text{B.T.} \\ 12 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 13 \end{array}$$

$$\begin{array}{r} \text{B.T.} \\ 50-69 \end{array}$$

$$+98 \frac{12'' \text{ OAK}}{95}$$

$$+43 \frac{20'' \text{ OAK } 8''}{79}$$

$$+18 \frac{\text{GAS VALVE}}{30}$$

$$+12 \frac{9'' \text{ OAK}}{81}$$

$$+13 \frac{3'' \text{ OAK}}{89}$$

$$\begin{array}{r} \text{E18' Drive} \\ 0985 \end{array}$$

$$210 \quad +97 \frac{20'' \text{ OAK } 8''}{92}$$

$$\begin{array}{r} \text{B.T.} \\ 12 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 13 \end{array}$$

$$\begin{array}{r} \text{B.T.} \\ 50-71 \end{array}$$

$$+88 \frac{11'' \text{ OAK}}{97} \quad +98 \frac{24'' \text{ OAK } 8''}{60}$$

$$+71 \frac{20'' \text{ OAKS } 8''}{75} \quad +87 \frac{3'' \text{ OAKS } 8''}{73}$$

$$+67 \frac{20'' \text{ OAKS } 7''}{82}$$

$$+67 \frac{\text{PP}}{40}$$

$$+1298 \frac{30'' \text{ OAK}}{98}$$

+50

$$\begin{array}{r} \text{B.T.} \\ 12 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 13 \end{array}$$

$$\begin{array}{r} \text{B.T.} \\ 98-69 \end{array}$$

$$+37 \frac{20'' \text{ OAKS } 4''}{64}$$

$$+35 \frac{2'' \text{ OAK}}{99}$$

$$+14 \frac{18'' \text{ OAK}}{74} \quad +26 \frac{10'' \text{ ENT}}{70}$$

209

$$+89 \frac{24'' \text{ OAK}}{77}$$

$$\begin{array}{r} \text{B.T.} \\ 12 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 13 \end{array}$$

$$\begin{array}{r} \text{B.T.} \\ 48-69 \end{array}$$

$$+72 \frac{10'' \text{ ENT}}{97}$$

$$+65 \frac{20'' \text{ OAKS}}{74}$$

$$+52 \frac{10'' \text{ ENT}}{27}$$

+50

$$\begin{array}{r} \text{B.T.} \\ 11 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 14 \end{array}$$

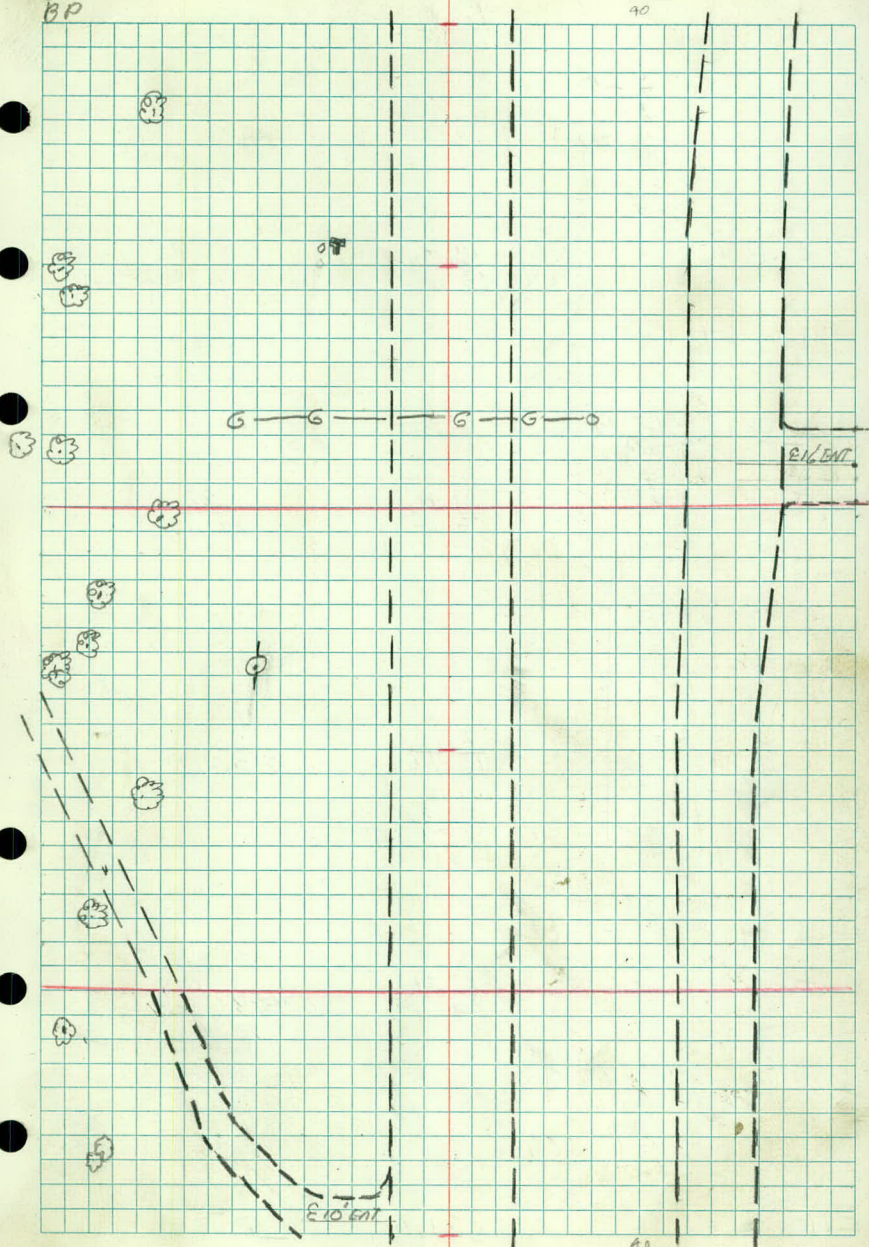
$$\begin{array}{r} \text{B.T.} \\ 47-69 \end{array}$$

PK
CP
BP

July 9 '70

16

40



+50

LT

2

B.T B.T
13 14

RT

+24 8" OAK
93

+12 PP
40

+10 7" OAK
69

213

B.T
13 15

+84.4" OAK
92

+18 6" OAK
66

+66 5" OAK
62

+15 15" OAK
80

+51 3 OAKS 3"
60

+55 10" OAK
93 B.T
13 13

+50

+47 10" OAK
79

+31 8" OAK
97

+24 8" OAK
94

+27 GAS

+10 10" OAK
86

B.T
94-112

+24 10" OAK
77

+25 B.T
82-100

+27 10" OAK
88

+10 10" OAK
86

212

+00 2 OAKS 6"
60

+81 18" OAK
80

B.T
12 13

B.T
69-91

+50

B.T B.T
12 13

B.T
60-78

+31 8" OAK
92

+34 PP
41

+45 4 10" ENT
91

+21 4 OAKS 10"
75

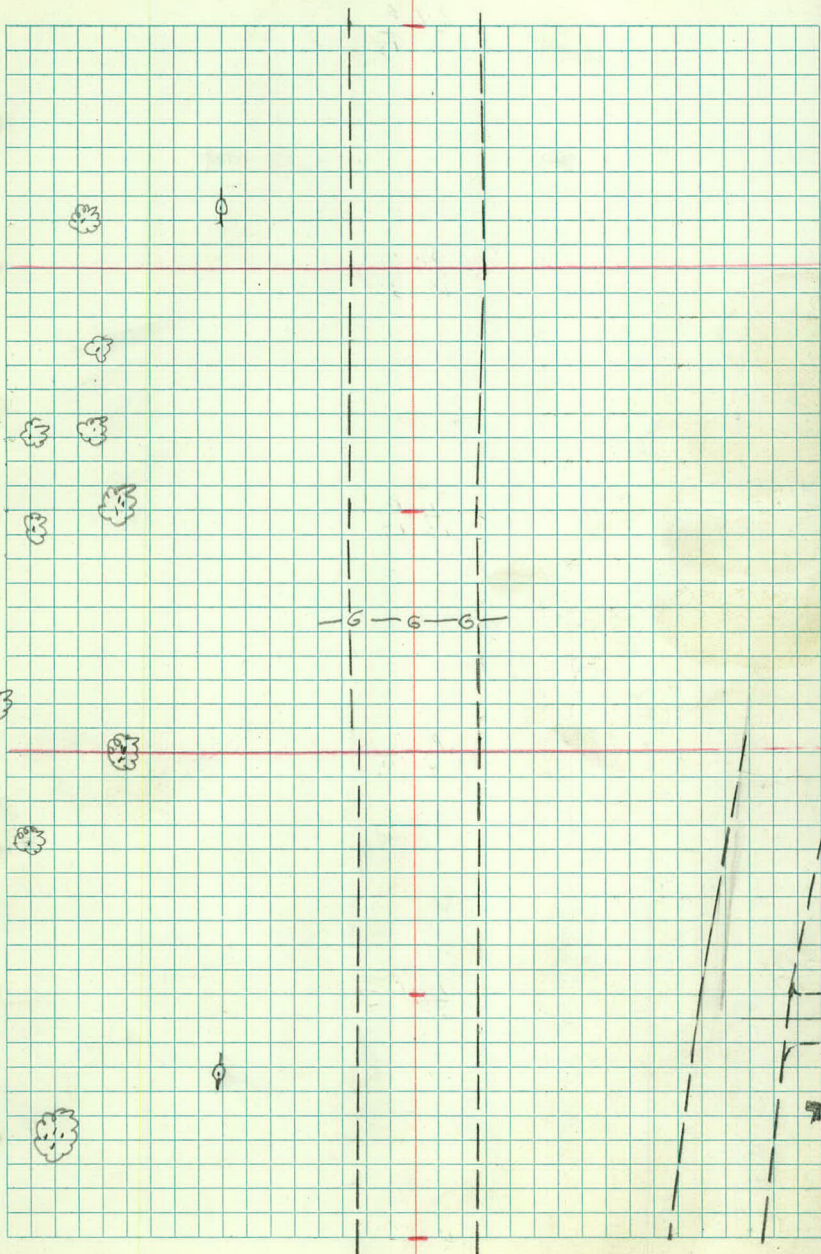
+27 HID
85

+17 2" Pine
94

211

B.T B.T
12 13

B.T
54-73



216

LT

$$\frac{B.T}{16} \frac{B.T}{13}$$

RT

$$\frac{4-6" OAL}{101}$$

+50

$$\frac{B.T}{15} \frac{B.T}{14}$$

215

$$\frac{B.T}{13} \frac{B.T}{14}$$

$$+67 \frac{PP}{40}$$

+50

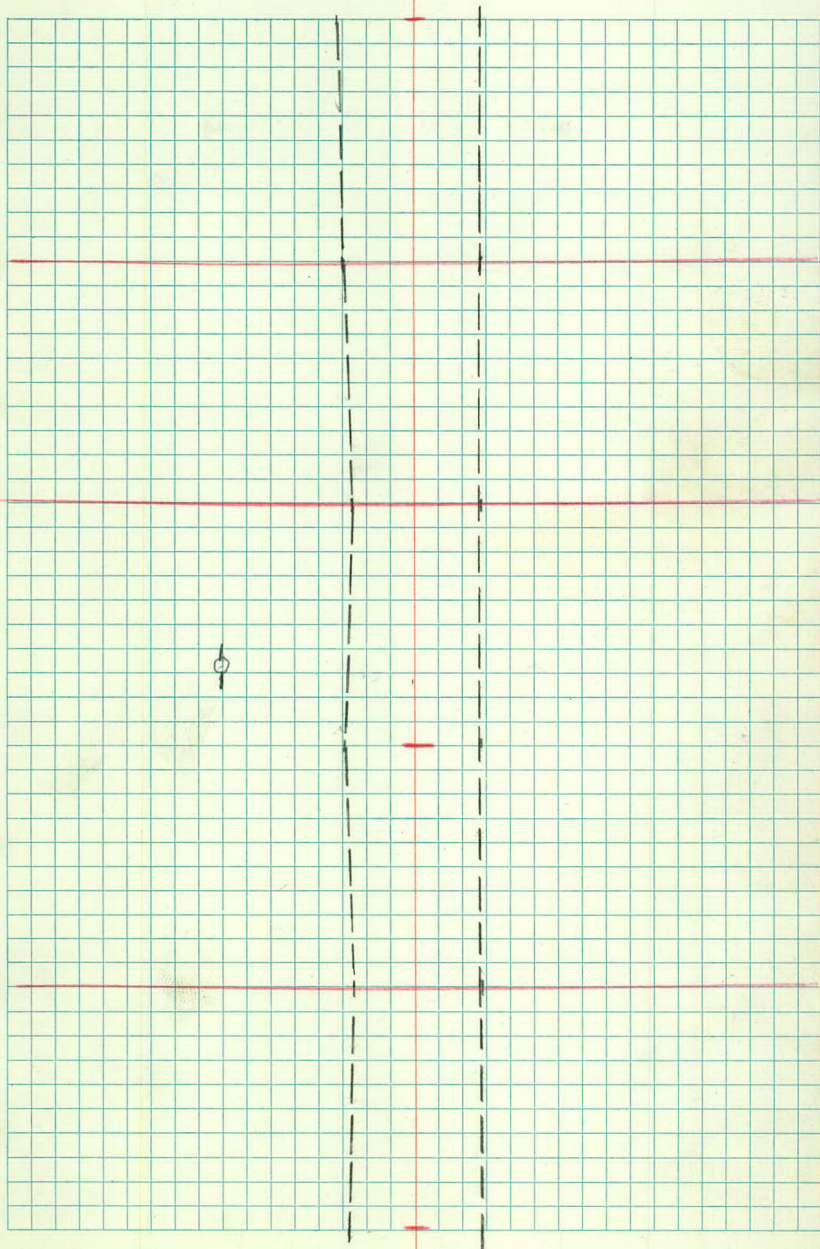
$$\frac{B.T}{14} \frac{B.T}{14}$$

214

$$\frac{B.T}{13} \frac{B.T}{14}$$

+50

$$\frac{B.T}{13} \frac{B.T}{14}$$



+50

LT

¢

RT

CONC
13

CONC
13

CONC
18

BIT
54

+34 G.P.
21

+35 PP
51

+23 Sign Post
61

+10 Guard Post
22

218

CONC
14
CO
11

CONC
32

CONC
13

BIT
65

+98 GARD POST
22 +91 PP
37

+82 BIT
67 +90 MH
56

+90 CONC
E-36

+73 BR
59

+77 ER
92

+77 12" CH
58

+62 ER
13

+62 B CONC.
13

+62 CONC
A-49

+50

+47 ER
76

+57 COR BIT
87

CONC
2055

+38 POR
71

+30 PP
104

+29 GAS VALVE
80

+25 CONC
36-76

+29 BR (ENT)
71

+38 12" CH
77

+36 POR
32

+9 BIT
100

+12 CONC
46-84

217

BR
79 +7 POR
55

CONC
51-91

+75 CONC
75-

+69 BIT
83

+58 ER
40

+50

+48 END APRON
42

BIT
31 BIT
37

+48 CONC
101

+44 MH
78

+44 Vent
79

+46 MH Bell Tell
65

+36 ARC Light pole
42

+42 Control Box
77

+41 PP
41

+38 POR
25

+31 BIT
98

+24 GAS VALVE
31

+32 END APRON 18" RCD
35

+30 POR
22

+22 GAS VENTS
33

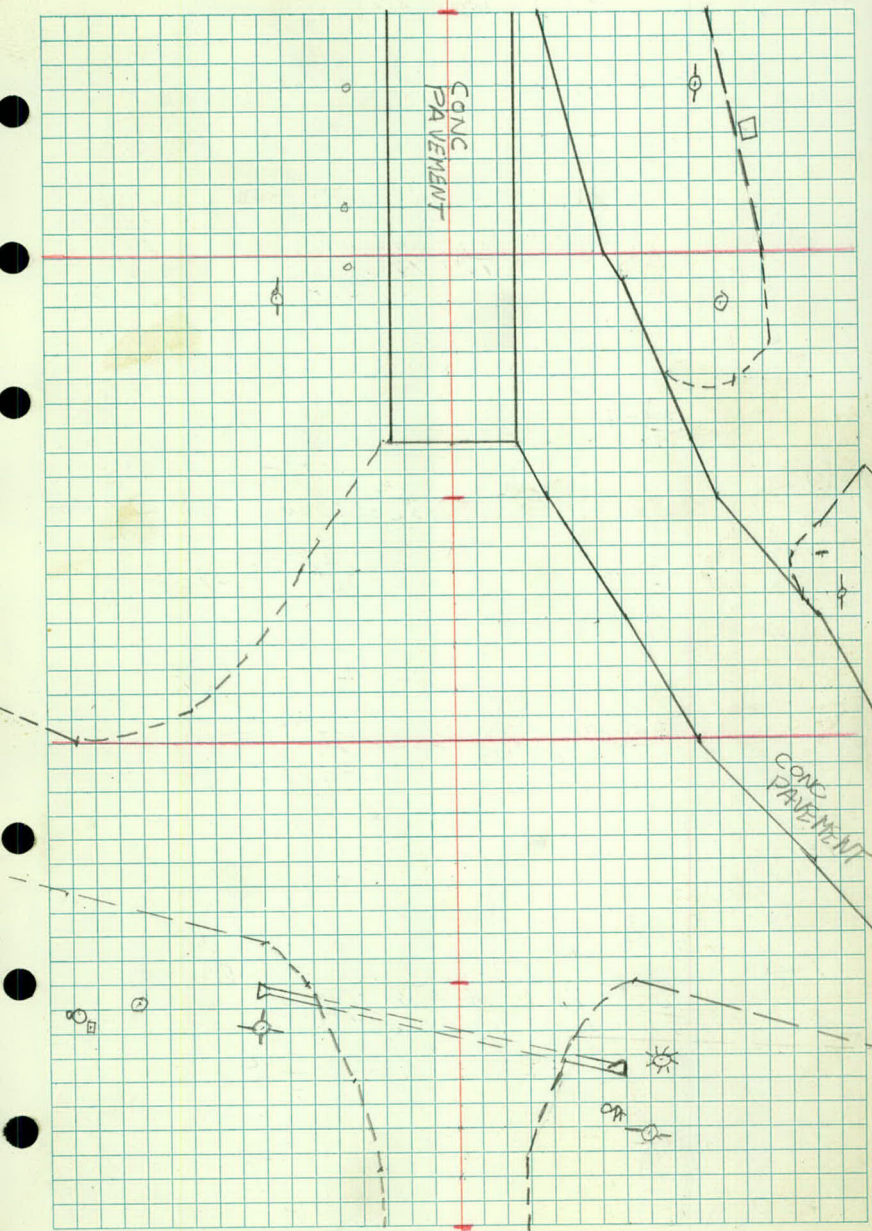
+28 POR
21

216

+13 BR
17

+19 PP
40

+14 BR
19



221

LT
 $\frac{\$10'ENT}{83}$

CONC CONC
 $\frac{13}{14}$ $\frac{14}{19}$

RT

+93 PP
 $\frac{3}{1}$

+50

+30 $\frac{10'OAK}{52}$

CONC CONC
 $\frac{14}{14}$ $\frac{14}{14}$

+25 $\frac{\$10'ENT}{80}$

+930" OAK
 $\frac{87}{1}$

220

$\frac{\$10'ENT}{72}$ CONC CONC
 $\frac{14}{13}$ $\frac{13}{13}$

+93" Spruce +162 Pines
 $\frac{57}{68}$

+996" OAK
 $\frac{42}{1}$

+90 3" PINE +90 4" Spruce
 $\frac{80}{58}$

+82 8" P. Maple +78 6" PINE
 $\frac{68}{81}$

+50

$\frac{\$10'ENT}{55}$

CONC CONC
 $\frac{14}{13}$ $\frac{13}{13}$

+51 12" Pine +57 SW COR HOUSE
 $\frac{62}{92}$

+34 9" Pine 9" PINE +44 9" PINE
 $\frac{65}{55}$ $\frac{55}{55}$

+32 $\frac{12"CM}{27}$

+34 9" Pine 6" PINE 2" Pine
 $\frac{97}{88}$ $\frac{27}{27}$

+27 $\frac{\$10'ENT}{46}$

+27 PP
 $\frac{35}{1}$

+32 MH
 $\frac{33}{1}$

+17 1/2" ENT +21 ENT +24 18" CM
 $\frac{35}{13}$ $\frac{13}{25}$

+12 $\frac{\$30'ENT}{27}$

+5 PP +9 D. Hedge
 $\frac{42}{72}$

219

$\frac{\$10'ENT}{46}$ CONC CONC
 $\frac{15}{13}$ $\frac{13}{13}$

B.T B.T
 $\frac{66}{40}$

+88 $\frac{12"CM}{27}$

+71 $\frac{\$10'ENT}{65}$

+97 B.T
 $\frac{100}{1}$

+14 $\frac{\$10'ENT}{85}$

+84 CONC
 $\frac{14}{1}$

+79 4" Beech
 $\frac{59}{1}$

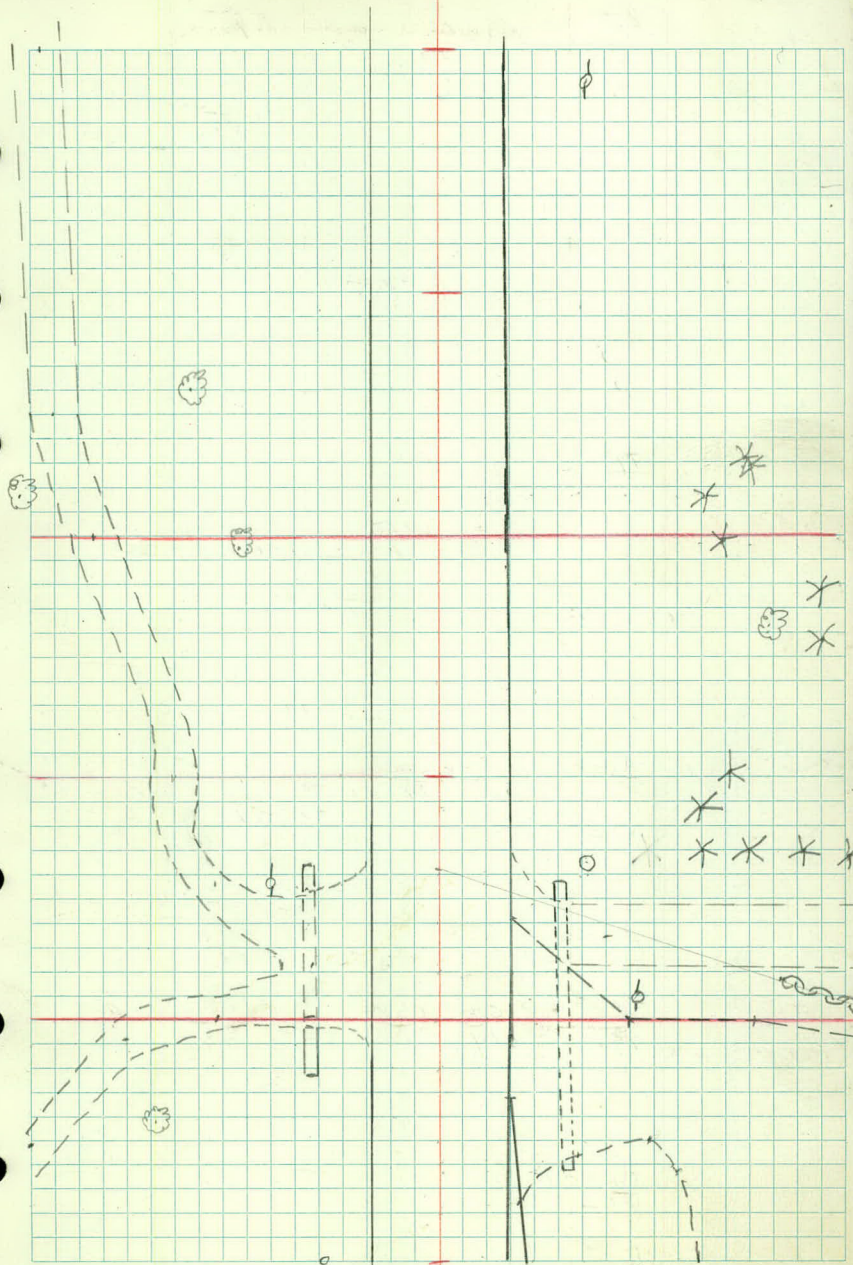
+75 B.T +72 B.T
 $\frac{44}{28}$

+50

+56 G.P.
 $\frac{23}{1}$

+69 B.T +68 18" CM
 $\frac{50}{27}$ $\frac{27}{27}$

+62 BR
 $\frac{17}{1}$



+50

LT Pond
44

£

RT

+33 3/4 Cottonwood
39

+25 POND
46

+16 STUMP POND
46

POND 48
GARDN. 19

+84 POND
51

+61 B. GOARDRAIL
19

+55 TP
30

+50 POND FILL
70 51

+31 FILL AREA 56
+37 POND 70

+14 4" OAK 46
+25 Twin 4" OAK 44

+42 Woods 79-100
+42 Dead 24" OAK
+232" OAK 41
+13 10" OAK 60
+107 Woods 57
+26 2" OAK 41
+20 12" OAK 45
+02 1" OAK 40

+100 4" OAK 40
+00 B. Fence 56
+83 4" OAK 48
+74 JRW Marker 51
+75 Fence Woods 57

CONC 14
CONC 14
+982" OAK 43

WOODS 64

+39 Spillway 1425

+35 Spillway 20-26

+208 Spillway 14

+42 PP 32

+25 5" OAK 46

+16 8" OAK 55

Fence, woods 59

+98 MH 17

+79 Fence Woods 59

+50

FILL AREA 79-

CONC 14

CONC 14

Fence, woods 59

+29 D. Fence B. Woods 10" OAK 59

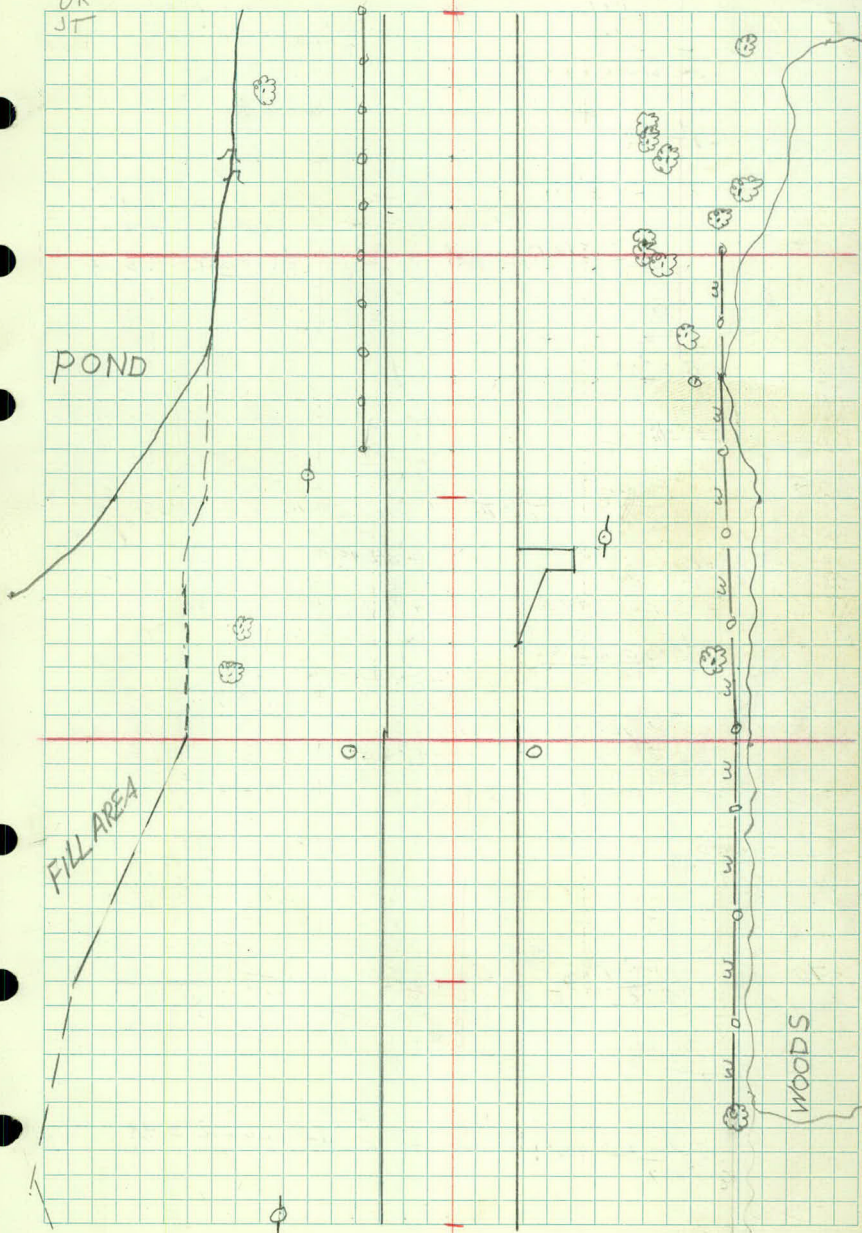
+06 EDGE FILL AREA 88-

+02 PP 36

221

July 13 '70 2/

PK
BP
DR
JT



226

LT Pond 34 G.R. Conc 19 14 14 19 RT Pond 60
 +97 28" willow & 4 Stumps 41
 +75 Pond 36

+62 TP 26 +60 Pond 25 63 170 Dead 10" OAK 63
 +50 Pond 38 14" willow 38 +53 Pond 40
 +43 Stump 37 12" willow 39 +43 PP 43 +40 10" OAK 68 - B. Woods

+29 QUAD 8" willow 37 +282" ASH 53
 +3 Turn 10" willow Pond 38 +19 8" Pine 65 +24 Hedge 63 +26 4" ASH 56
 +108 8" Pine 62 +8 Hedge 62

225

POND 38 G.R. Conc 19 14 14 19 +96 8" PINE 59 +96 4" ASH 55
 +85 POND 38 +84 10" Pine 54 +84 Lilac Hedge 52
 +75 4" Cottonwood 33 +71 18" OAK 54
 +69 20" Dead willow 39 +58 B. Lilac Hedge 54 +63 2" Poplar 33 39
 +61 18" CM 28 +61 5" T 19

+50 POND 38 +48 E. B. TENT 45

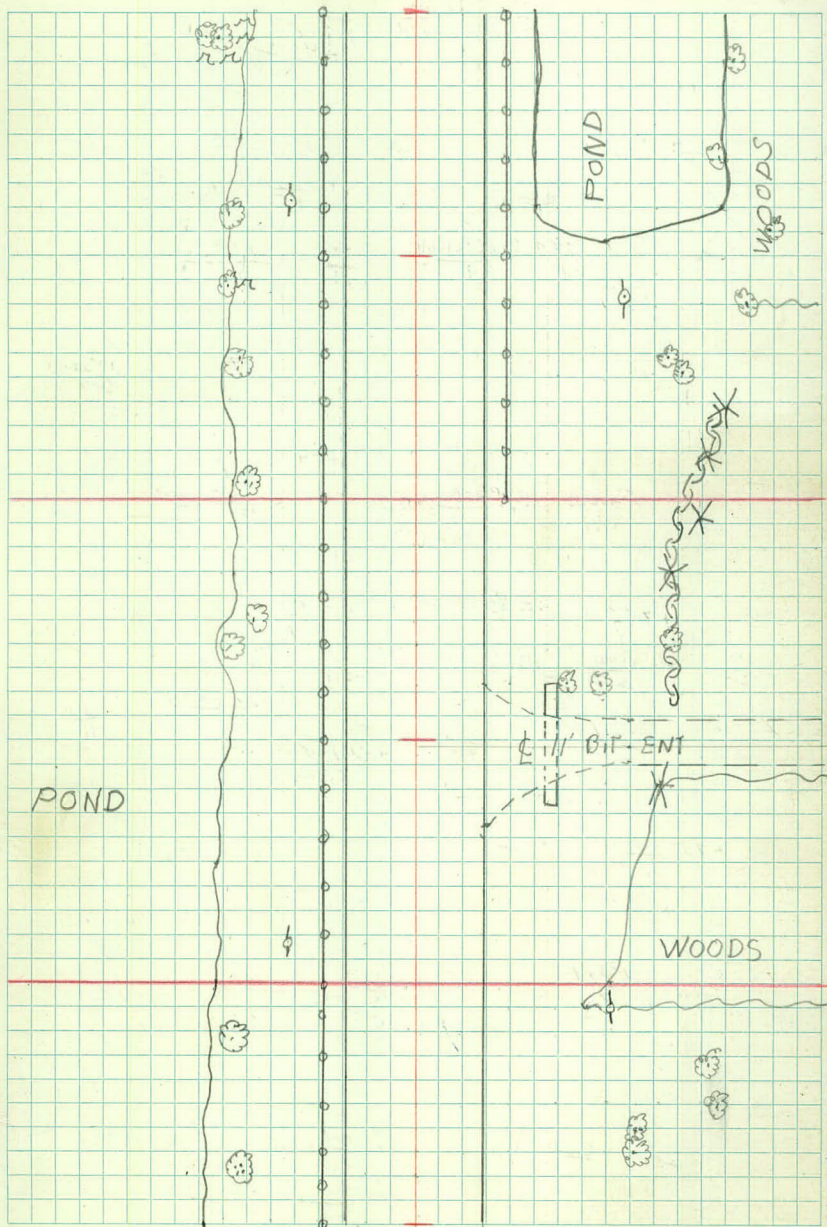
+25 POND 41 +33 E.T 14 +37 18" CM 28 +41 10" Pine Woods 52
 +10 TP 27

224

POND 42 G.R. Conc 19 14 14 19 WOOD 41
 +88 8" OAK 38 +95 PP 41 +95 37 - 100+
 +75 POND 43

+162 Dog & 8" willow 37 +74 18" OAK 63 +83 18" OAK 62
 +65 10" OAK 46 +70 Turn 5" OAK 46

+50



+50 LT

GR
18

CONC
13 14

RT

+46 PP
46

+34 Low Area
44

+43 PP
25
+25 Low Area
51

+23 B. Guard Rail
18

+22 B. GR
19
+5 25 Ash -1"
45

228

+87 Conc Embankment
29

+83 Piller base
16

+00 Brick Ret Wall
24

+76 Tracks

+00 Brick Ret Wall
23

+87 Conc Embankment

+83 Piller Base
17

+50

+50 Conc Embankment
29

+16 Piller Base
16
+16 Conc
14 14

+61 Tracks

+54 B. Piller Base
17

+50 Conc Embankment
30

+22 Pond
56-100+
+15 PP
25

+24 PP
84
+16 Pond
34

+26 Brick Ret Wall
25

+16 E. Guard Rail
19
+04 Spillway
19-26

+25 PP
44

+18 Pond
40
+12 Pond
32

+36 B. Brick Ret Wall
26

+16 Pond
81
+16 E. Guard Rail
20

+7 Pond
91

227

Pond
35

GR Conc
19 14 14

GR
19 14 14

Pond
28

+87 PP
44

+75 Pond
31

+85 Spillway
14

+50

Pond
32

+46 Stump
40

+25 Pond
33

+55 18" Oak
73

+41 4" Oak
68

+29 Dead 6"
62

+25 Dead 6"
62

+13 Dead 4" Oak
56

+10 Pond
32-60

+62 5" Oak
73

+49 4" Oak
77

+32 Dead 12"
55

+25 Pond
30-58

+15 Dead 4" Oak
65

+10 Pond
60

+44 Pond
29 59

+44 Dead Trees
55

+37 10" Oak
78

+25 Pond
30-58

+15 Dead 4" Oak
65

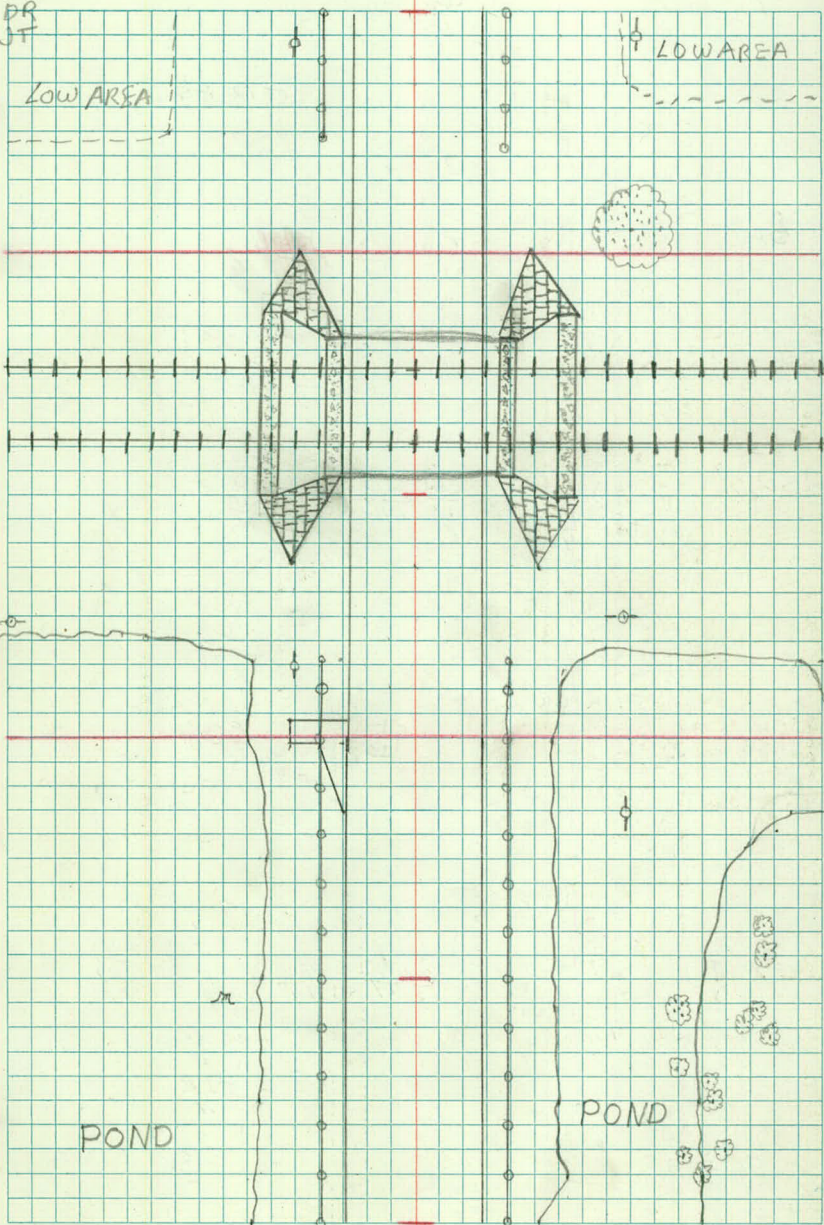
+10 Pond
60

226

PK
CP
BP
BR
JT

July 14 '70

23



231

LT

$\downarrow$
 $\frac{\text{Conc}}{13}$
 $\frac{\text{Conc}}{14}$

RT

$\downarrow$
 $+98 \frac{\text{GR}}{20}$
 $+90 \frac{\text{Fence}}{51}$

+50

$\downarrow$
 $\frac{\text{Conc}}{13}$
 $\downarrow$
 $\frac{\text{Conc}}{14}$
 $\downarrow$
 $\frac{\text{GR}}{20}$

$+35 \frac{\text{Fence}}{51}$
 $+22 \frac{\text{PP}}{46}$
 $\frac{51}{37}$
 $\frac{12}{37}$

230

$\downarrow$
 $+91 \frac{\text{PP}}{40}$

$\downarrow$
 $\frac{\text{Conc}}{13}$
 $\frac{\text{Conc}}{14}$
 $\frac{\text{GR}}{19}$

$\downarrow$
 $+99 \frac{\text{Fence}}{51}$
 $+80 \frac{\text{Low area}}{38}$

$\downarrow$
 $+50$
 $+54 \frac{\text{E. GR}}{19}$

$\downarrow$
 $\frac{\text{GR}}{20}$
 $+40 \frac{\text{Fence}}{50}$
 $+40 \frac{\text{Low Area}}{37}$

229

$\downarrow$
 $+07 \frac{\text{Spillway}}{14-27}$

$\downarrow$
 $+03 \frac{\text{Spillway}}{20-27}$

$\downarrow$
 $+89 \frac{\text{B. Spillway}}{13}$

$\downarrow$
 $+59 \frac{\text{Low Area}}{63}$

$\downarrow$
 $+58 \frac{\text{Low Area}}{51}$

+50

$\downarrow$
 $\downarrow$
 $\downarrow$
 $\frac{\text{GR}}{18}$
 $\frac{\text{Conc}}{13}$
 $\frac{\text{Conc}}{14}$

$\downarrow$
 $\frac{\text{GR}}{18}$

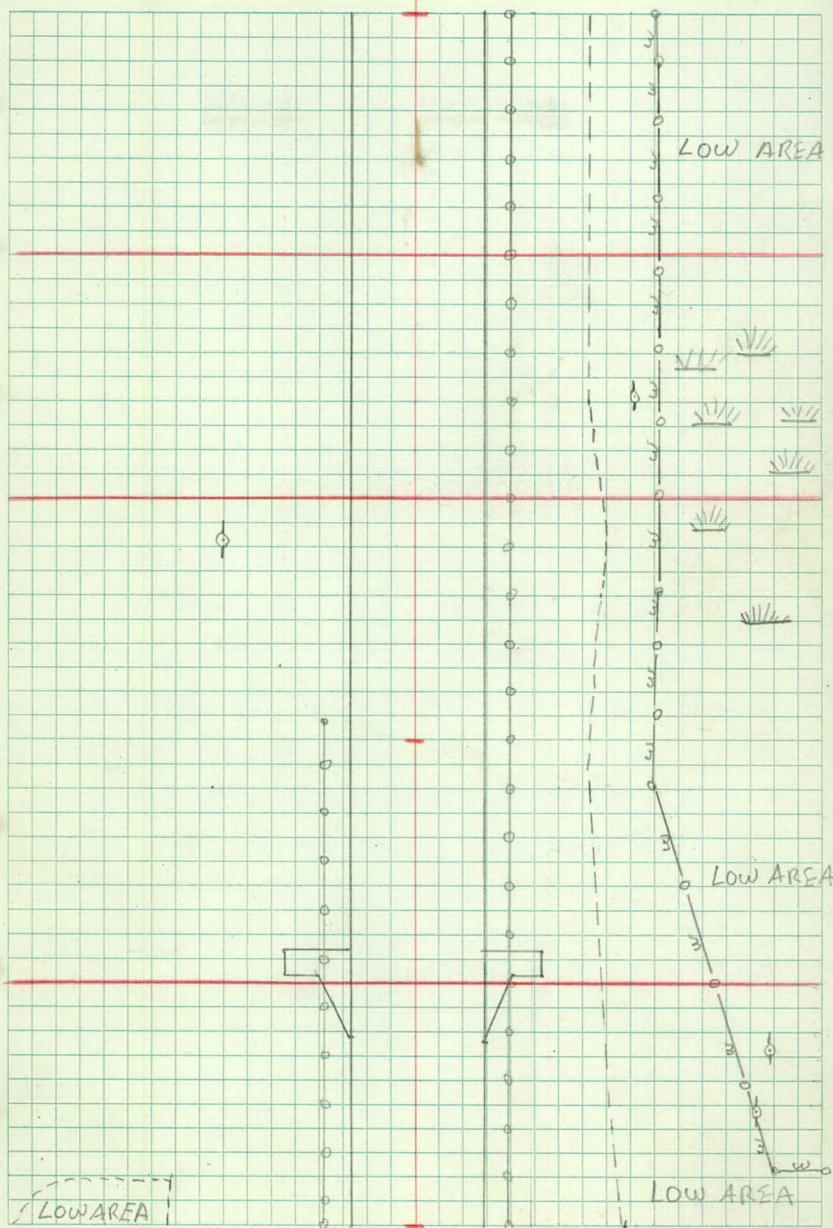
$\downarrow$
 $+07 \frac{\text{Spillway}}{14-27}$
 $+03 \frac{\text{Spillway}}{20-27}$
 $+88 \frac{\text{Spillway}}{14}$

$\downarrow$
 $+86 \frac{\text{PP}}{74}$

$\downarrow$
 $+73 \frac{\text{PP}}{71}$

$\downarrow$
 $+62 \frac{\text{Fa Cor}}{75}$

$\downarrow$
 $+62 \frac{\text{Fence}}{75-100+}$



LT

2

RT

+50

CONC CONC
13 14

✓
+29 $\frac{PP}{44}$

233

CONC CONC
14 13

✓ End
FE
00 51

✓ End
L Area
+00 $\frac{95}{103}$
✓ Cotton wood
+00

+50

CONC CONC
14 13

+50 $\frac{FE}{50}$ +50 $\frac{L Area}{77}$

✓ Tel.
+20 $\frac{E.H.}{19}$

232

End
CONC. Spillway
+8826

Edge
Spillway
-85 19-260 Beg
Spillway
+71 $\frac{13}{13}$

CONC CONC
14 13

✓ L Area
+100 $\frac{60}{78}$
✓ FE
+92 $\frac{51}{51}$

✓ PP
+70 $\frac{96}{96}$

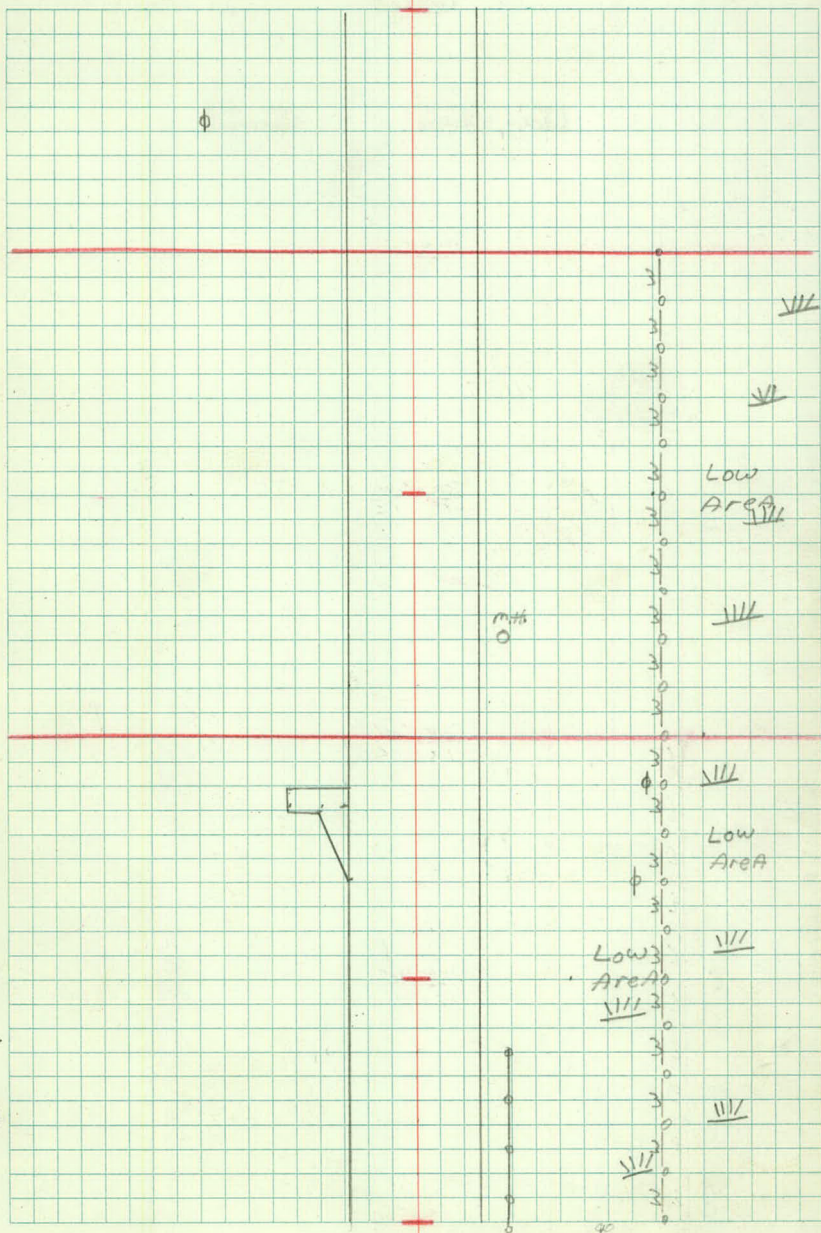
+50

CONC CONC
14 13

✓ L AREA
+50 $\frac{32}{32}$

✓ End
C.R.
+35 $\frac{19}{19}$

231



236

LT

E

RT

I

$$\begin{array}{ccccccc}
 +00 & \downarrow & & & & +00 & \downarrow \\
 \text{G.R.} & & \text{Conc} & \text{Conc} & & \text{G.R.} & +00 \\
 19 & & 13 & 14 & & 19 & \text{Fe} \\
 & & & & & & 51
 \end{array}$$

+50

$$\begin{array}{ccccccc}
 +50 & \downarrow & & & & -50 & \downarrow \\
 \text{G.R.} & & \text{Conc} & \text{Conc} & & \text{G.R.} & +50 \\
 19 & & 13 & 14 & & 19 & \text{Fe} \\
 & & & & & & 52
 \end{array}$$

$$\begin{array}{c}
 \text{Beg} \\
 \text{GR} \\
 +19 \quad 19
 \end{array}$$

$$\begin{array}{c}
 +32 \quad \text{PP} \\
 46
 \end{array}$$

235

$$\begin{array}{ccccccc}
 +00 & \downarrow & & & & +00 & \downarrow \\
 \text{End} & & \text{Conc} & \text{Conc} & & \text{G.R.} & +00 \\
 \text{Spillway} & & 13 & 14 & & 19 & \text{Fe} \\
 24 & & & & & & 51 \\
 & & \downarrow & & & & \\
 & & \text{Spillway} & & & & \\
 & & +19 \quad 20 & & & &
 \end{array}$$

$$\begin{array}{c}
 \downarrow \text{PP} \\
 +85 \quad 29
 \end{array}$$

$$\begin{array}{c}
 \text{Beg} \\
 \text{Spill} \\
 +81 \quad 13
 \end{array}$$

+50

$$\begin{array}{ccccccc}
 & & \downarrow & & & +50 & \downarrow \\
 & & \text{Conc} & \text{Conc} & & & \text{G.R.} \\
 & & 13 & 14 & & & 19
 \end{array}$$

$$\begin{array}{c}
 \downarrow \text{Beg} \\
 +92 \quad \text{G.R.} \\
 19
 \end{array}$$

$$\begin{array}{c}
 \downarrow \text{Beg} \\
 +25 \quad \text{Fe} \\
 51
 \end{array}$$

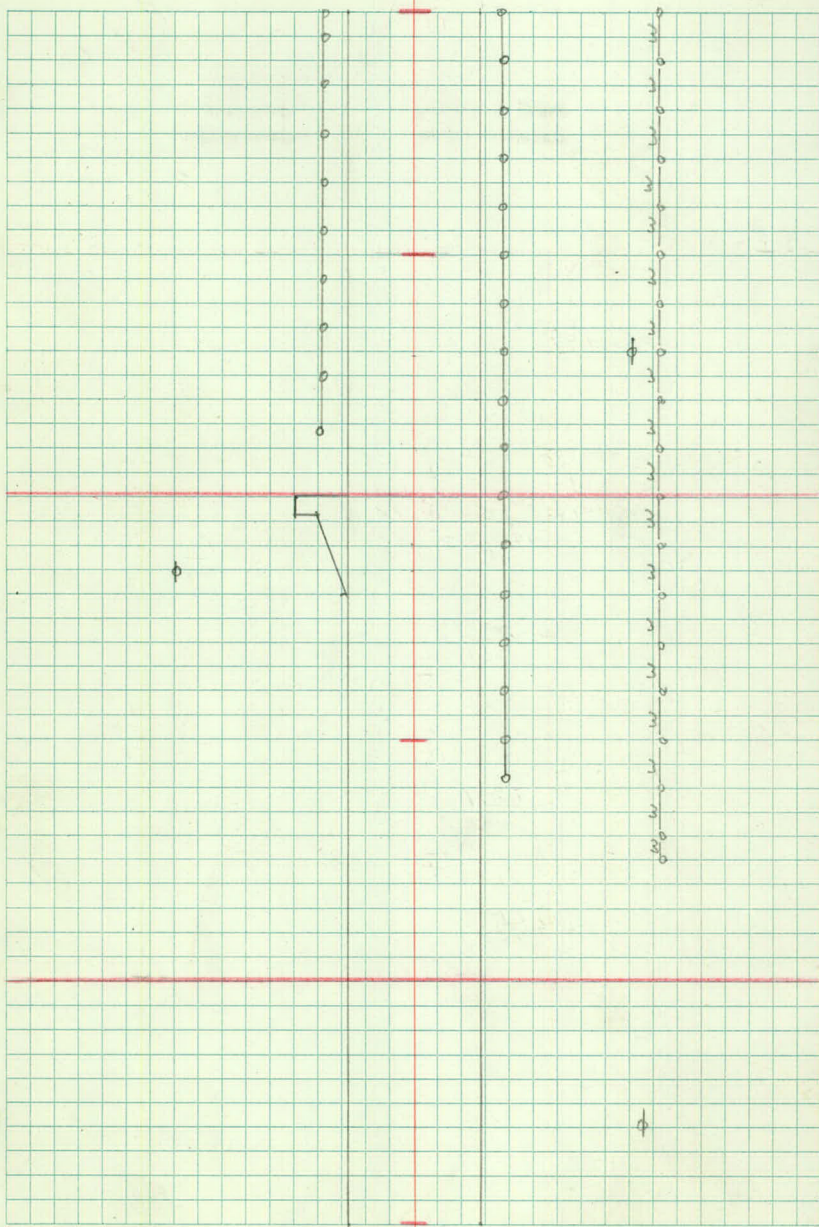
234

$$\begin{array}{ccccccc}
 & & \downarrow & & & & \\
 & & \text{Conc} & \text{Conc} & & & \\
 & & 13 & 14 & & &
 \end{array}$$

$$\begin{array}{c}
 \downarrow \\
 +72 \quad \text{PP} \\
 47
 \end{array}$$

+50

$$\begin{array}{ccccccc}
 & & \downarrow & & & & \\
 & & \text{Conc} & \text{Conc} & & & \\
 & & 13 & 14 & & &
 \end{array}$$



+50

LT

↓
conc conc
13 14

RT

↓
+50 Fe
51

238

↓
conc conc
13 14

↓
+100 Fe
51

↓ P.P.
+64 20

↓ End
+62 15

↓
+54 20

↓ End
+52 25

+50

↓
+99 20

↓
conc conc
13 14

↓
+50 Fe
51

↓
+93 13

↓
+44 P.P.
46

↓
+12 38

↓
+07

237

↓
conc conc
13 14

↓
+100 Fe
52

↓
+83 35

↓
+82 20

↓
+67

↓
+54 25

+50

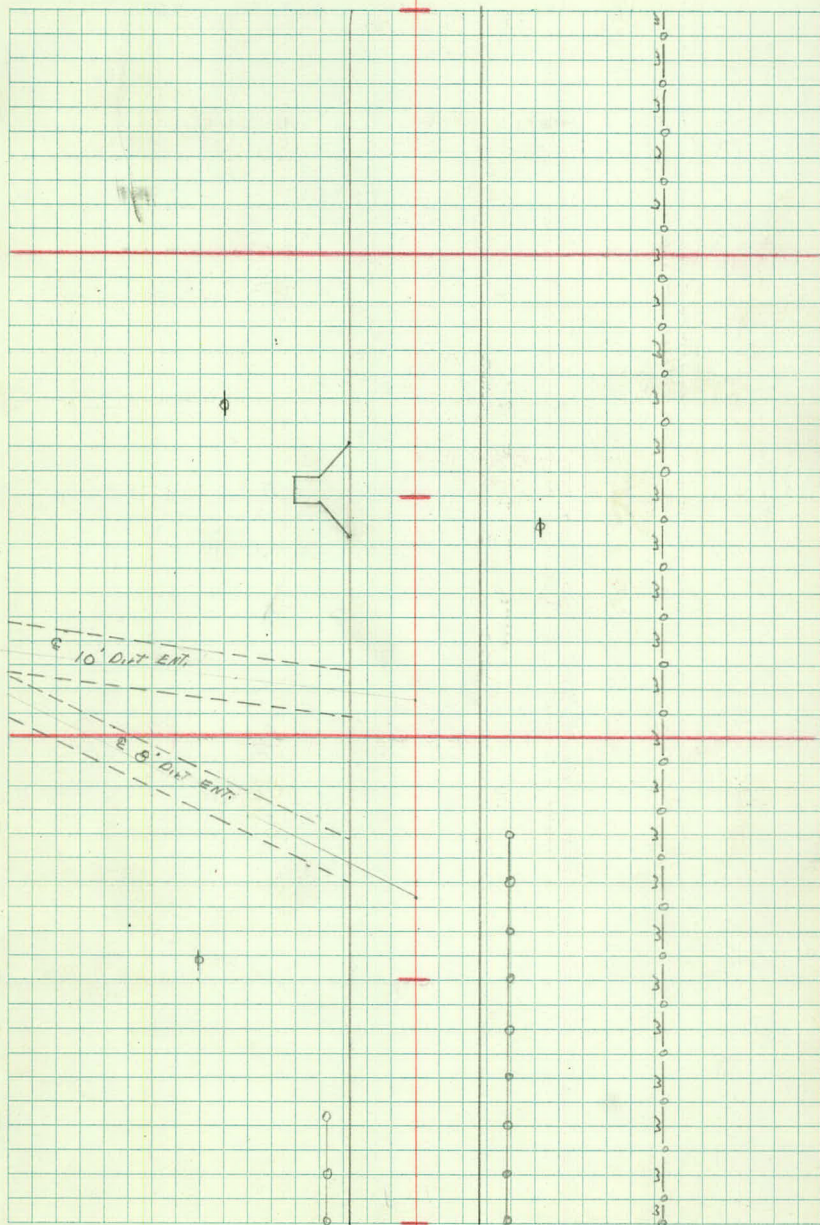
↓
conc conc
13 14

↓
+50 G.B.
19

↓
+23 18

236

↓
conc conc
13 14



241

LT

↓

RT

$\frac{\text{conc}}{13}$
 $\frac{\text{conc}}{14}$
 $\frac{\text{Fence}}{52}$
 $\frac{\text{Swamp}}{54}$

↓
 +60 $\frac{3' \text{ cotton wood}}{40}$

+50

$\frac{\text{Fence}}{51}$
 ↓
 +47 $\frac{\text{Swamp}}{51}$
 $\frac{\text{END woods}}{4-51}$

+25 $\frac{\text{Fence}}{50}$
 $\frac{\text{Woods}}{50-81}$
 $\frac{\text{Swamp}}{81}$

240

$\frac{\text{conc}}{13}$
 $\frac{\text{conc}}{14}$
 $\frac{\text{Fence}}{51}$
 $\frac{\text{woods}}{56}$

↓
 +86 $\frac{\text{TP}}{40}$

+50

$\frac{\text{conc}}{13}$
 $\frac{\text{conc}}{14}$
 +61 $\frac{\text{Fence}}{51}$
 $\frac{\text{TP}}{53}$
 $\frac{\text{woods}}{99}$

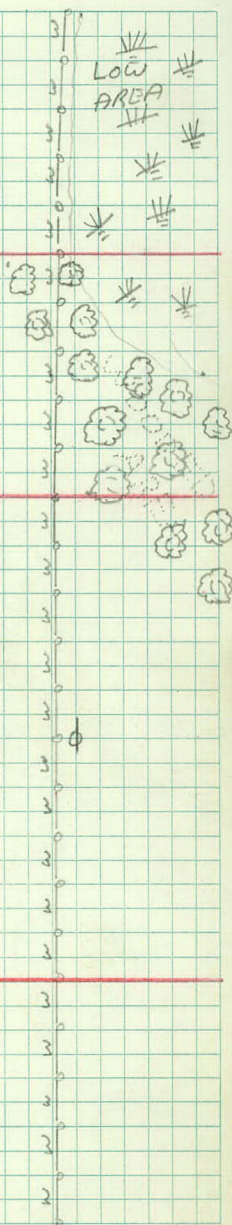
239

$\frac{\text{conc}}{14}$
 $\frac{\text{Fence}}{51}$

+50

$\frac{\text{conc}}{13}$
 $\frac{\text{conc}}{14}$

LOW
AREA



+50

LT

↓
B.T. B.T.
14 13

RT
Swamp
59

↓
+10 TP
40

243

↓
+64 18" CMP
45

↓ ↓ ↓ ↓
conc conc E. Fence Swamp
14 14 51 50
+92 B. 1/2" B.T. overlay
on Conc. Pavement

+50

↓
+39 18" CMP
45

↓
conc
14

↓ ↓ ↓ ↓
+60 conc E. Fence PP Swamp
14 51 55 52

↓
+37 MH
17

242

↓ ↓ ↓ ↓
conc conc Fence Swamp
14 14 53 60

↓
+72 2" OAK
49

↓ ↓ 39 Trees
+58 E Row Trees
48

+50

↓ ↓ ↓ ↓
conc conc Fence Swamp
14 13 55 58

↓
+31 TP
41

↓
B. Row of 2" OAKS
48

↓
conc
14

241

END CONC.
 1/2" Bit Overlay
 2 on CONC.

18" CMP

1/4"

Low
AREA

Low
AREA

246

LT

Low Area

45-70

G.R

19

E

B.T

13

JRT

D. Brush Area

+97⁴⁸ Dense Brush Area

46

+82 E. Swamp

47-100+

+50

B. Low Area

48-55

B.T

14

B.T

13

+63 PP

58

+58 Swamp

46

+26^J B. GUARD Rail

19

+25^J Swamp

50

245

B.T

14

B.T

14

+96^J 4" Elm

75

Swamp

74

+50

+60 PP

41

B.T

14

B.T

14

+45^J Twin 3" willow

50

Swamp

87

+42^J 6" willow

52

244

B.T

14

B.T

13

Swamp

90

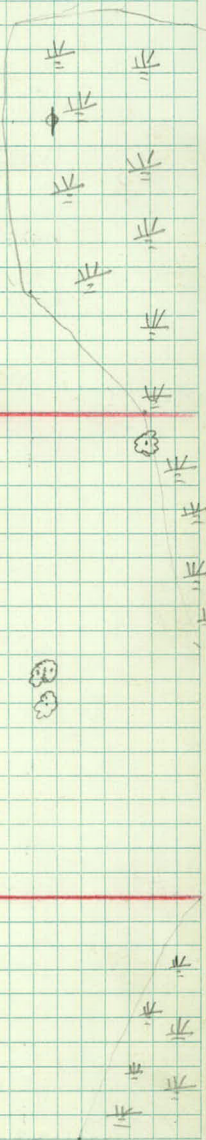
+50

+50 Swamp

59



DENCE Brush
AREA



LT

E

RT

+50

+37 ✓ Low Area +43 L. Area 14 13 +48 PP +414" Poplar
 44 72 57 89
 +35 42" RCP +30 Ditch
 44 44
 +33 QUAD cottonwood +33 42" RCP +37 42" RCP
 41 43 43
 +31 42" RCP +35 R.T. to Ditch
 44

248

↓ Low Area ↓ GR ↓ B.T ↓ B.T ↓ Ditch
 44 19 14 13 46

↓
+64 TP
 40

+50

✓ ↓ Low Area ✓ ↓ GR ✓ ↓ B.T ✓ ↓ B.T ↓ Ditch
 49 19 13 13 46

247

↓ Low Area ↓ GR ↓ B.T ↓ B.T
 48 19 14 13

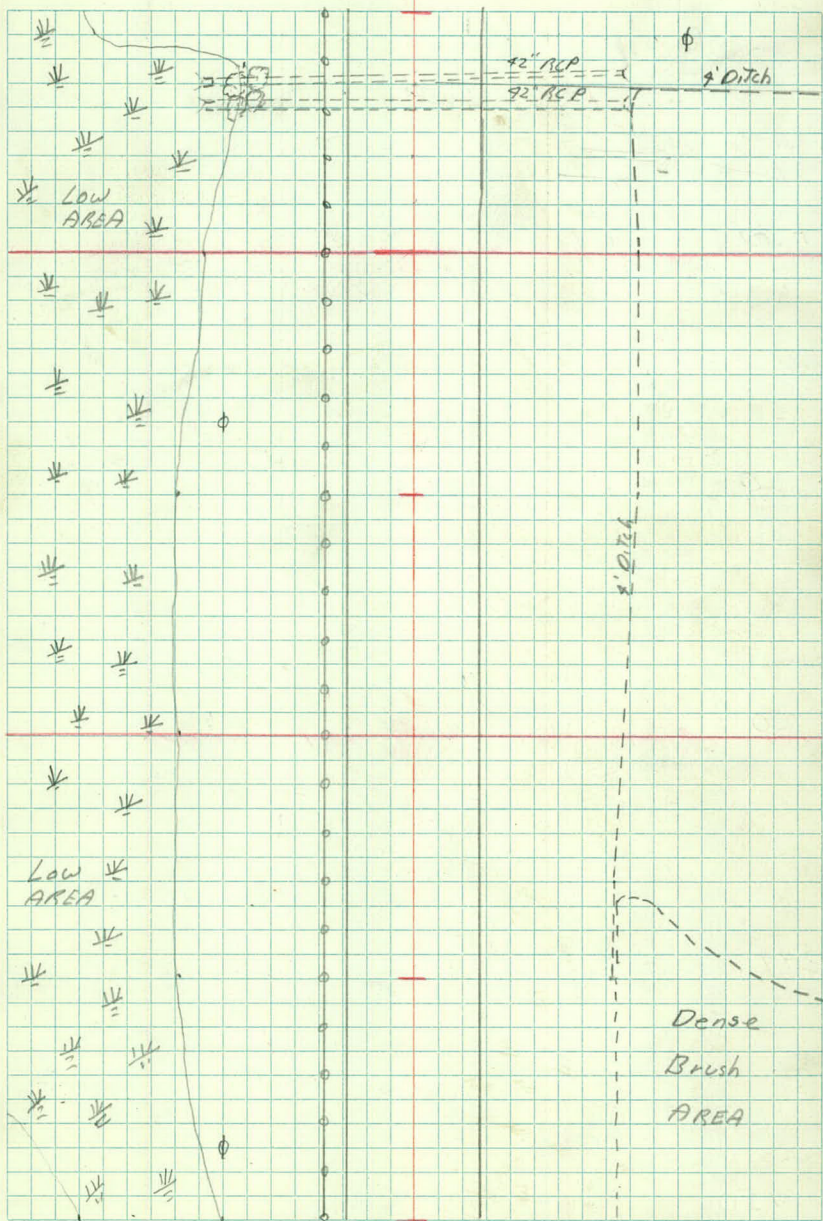
↓
+64 E. Dense BRUSH ↓ Ditch
 42-50 42

+50

↓ Low Area ↓ G.R. ↓ B.T ↓ B.T ↓ Dense Brush Area ↓ Ditch
 48 - 100+ 19 14 13 42 - 90 42 +

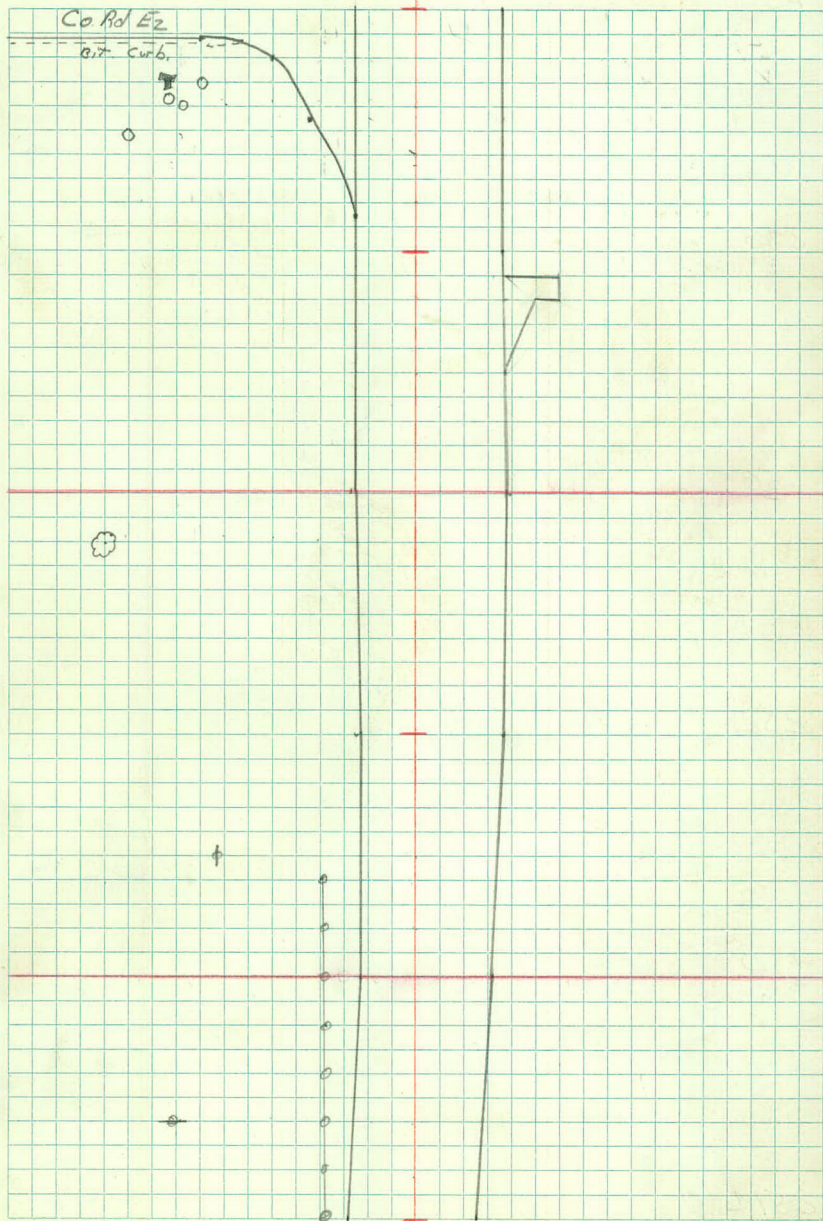
↓
+16 TP
 41
 ↓
 GR
 19

246



Co Rd E2

0.7 curb



+50

LT ✓
Brush AREA✓
BIT BIT↓ RT.
D.B. AREA↓
Shoreline+47 Trip 4' Willow 58
38

13 17

44

86

+133 Low A. +33 58
58-100

58-100

+24 E Willow 2"
43

253

↓
Low Area
50↓
BIT BIT
13 17↓
DRAINAGE ↓ Shoreline
+91 Shoreline Takeout twice
87+85 D.B. AREA
69

+50

↓
Low Area woods
70-80 80↓
BIT
13↓
D.B. Area
57

252

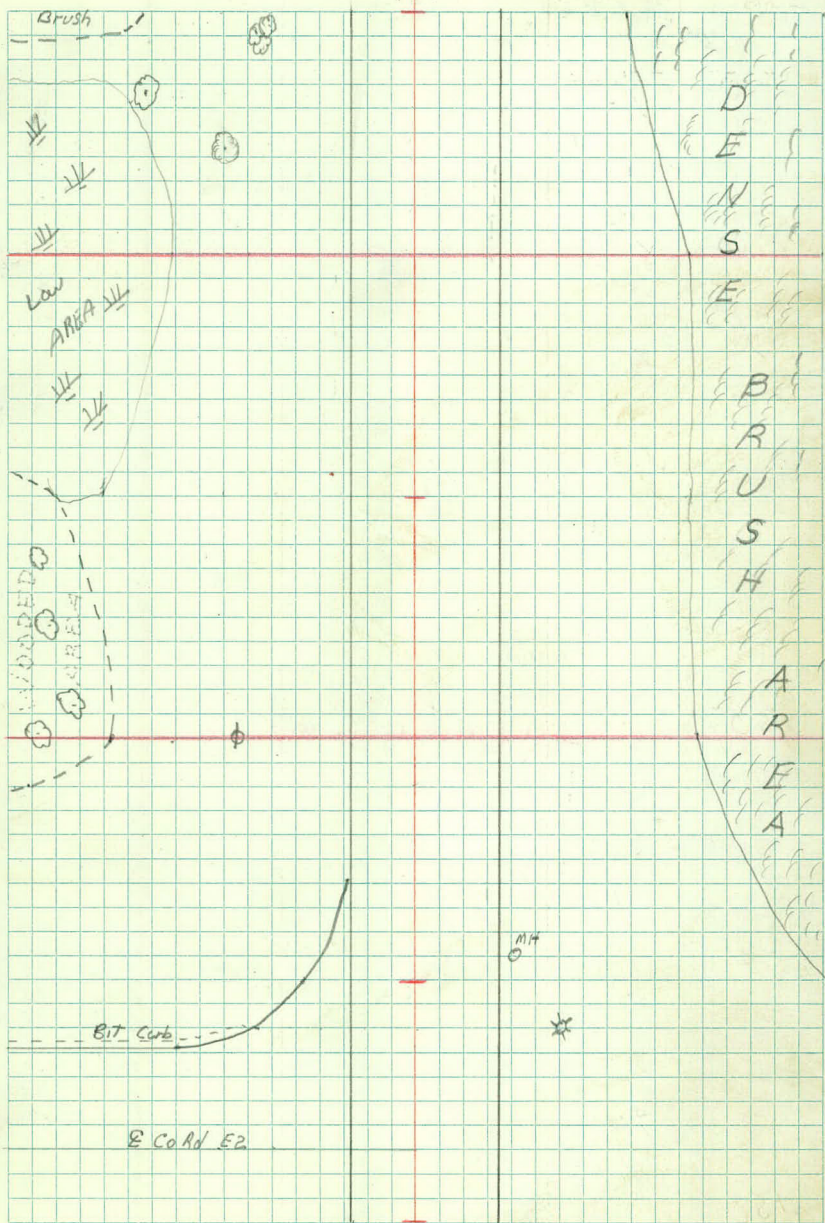
↓
PP wood
38 63↓
BIT conc
13 17↓
D.B. AREA
58+90 B. Woods
81-100+↓
+71 ER
14+61 MH
20

+50

↓
PORB
23conc
17↓
D.B. AREA
90+90 POR E.B. CORB
34↓
+37 BR
49+40 Arc Light Pole
30↓
+15 ER
41

251

D



256

✓ LT
30" OAK
 74

£
B.I.T CANC
 14 14

RT

✓
 +80 10" Cottonwood
 57

✓
 +75 E. D.B. AREA
 98

+50

✓
 +45 20" OAK
 90

✓
B.I.T B.I.T
 14 16

✓
D.B. AREA
 78

+25 TP
 47

✓
 +20 14" OAK
 88

✓
P55
 +94 18" OAK
 92

✓
 +96 24" OAK
 60

✓
B.I.T B.I.T
 14 16

✓
D.B. AREA
 39

✓
Shoreline
 117

✓
 +79 12" OAK
 71

✓
 +78 5" OAK
 77

✓
 +68 10" OAK
 85

✓
 +12 OAK
 82

✓
 +66 18" OAK
 67

+50

✓
 +30 6" Cottonwood
 55

✓
B.I.T
 13

✓
B.I.T
 17

✓
D.B. Area
 40

✓
Shoreline
 67

✓
 +30 TRIP. 6" Cottonwood
 85

✓
 +32 PP
 62

✓
 +18 SP.
 96

✓
 254 E. D.B. AREA
 57-70

✓
B.I.T
 13

✓
B.I.T
 17

✓
D.B. AREA
 40

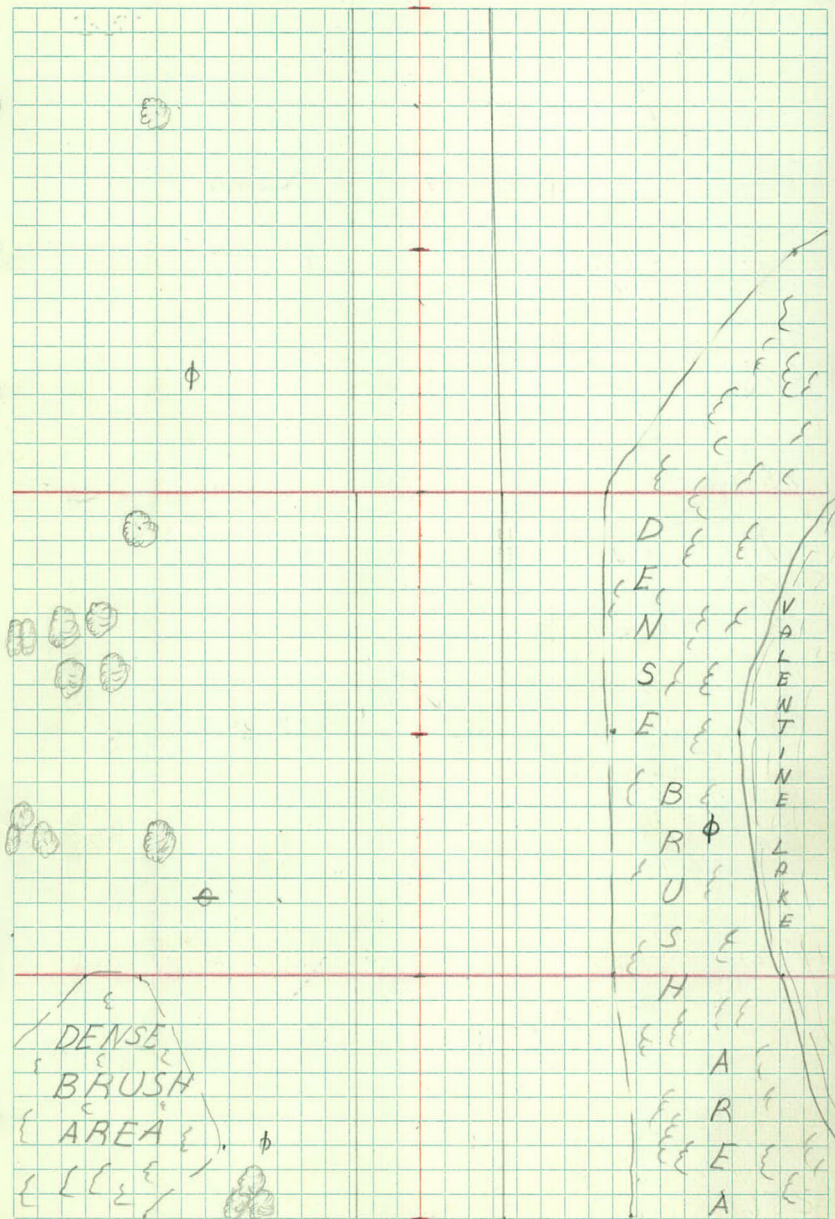
✓
Shoreline
 76

✓
 +69 D.B. AREA
 42

✓
 +68 TP
 37

+50

✓
 +55 TRIP 4" willow
 38



+50

LT

£

RT.

D.O AREA

conc
14

↓
15" OAK
+30
73

↓
2" PP
+37
60

↓ End
Sumac
+38
94-52

↓
9" OAK
+18
53

258

↓
Trip 3" OAK
+58
46

↓
Sumac
+73
13-14

✓
D. B. AREA

114

↓
6" OAK
+75
75

↓
PP
+82
46

↓
Trip 2" OAK
+73
58

↓
2" Poplar
+70
60

↓
3" OAK
+73
59

↓
4" Poplar
+77
60

↓
2" OAK
+67
59

↓
2" Poplar
+65
59

↓
5" Poplar
+65
70

+50

Sumac
45-61

conc
14

✓
D. B. AREA

91

↓
132 24" OAK
72

↓
SUMAC
+32
47-62

257

↓
Sumac
46-61

✓
conc
13

✓
conc
14

✓
D. B. AREA

97

↓
Sumac
+75
46-65
+71
46

↓
4" Poplar
+62
30

+50

✓
conc
14

✓
PP
+44
74

↓
1" OAK
+35
72

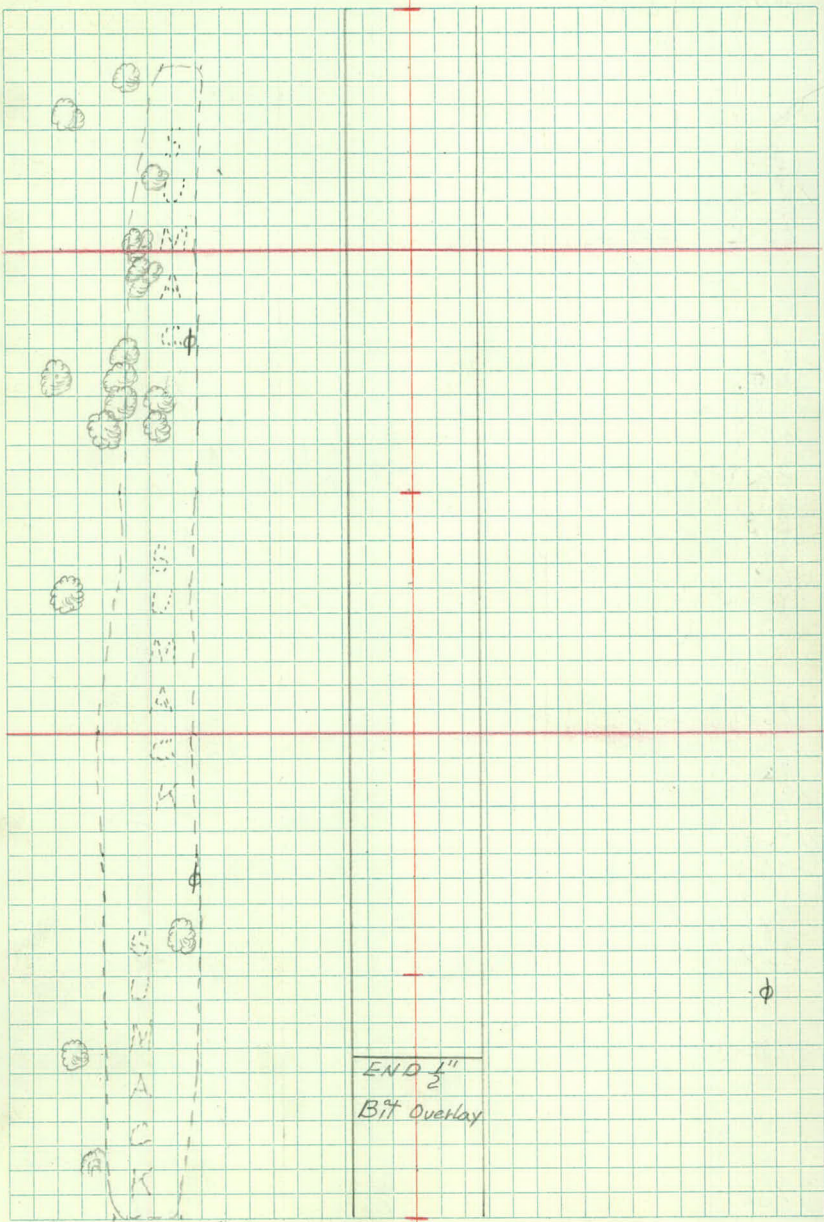
↓
+33 END 1/2" Bit overlay

↓
Berry Bush
+13
67

256

↓
Sumac
49-63

Sumac
47-63



END 1/2
Bit Overlay

261

LT ✓
Fence
45

✓ E ✓
BIT BIT
13 14

RT ✓
Shoreline
42

+50

✓
Fence
46

✓
BIT BIT
13 14

✓
Shoreline
43

✓ MH
+21 33

✓
+16 TP, E.B. Barred Cable
45

✓
260 Fence
45

✓
+11 4 willows 3"
44
BIT BIT Trip 4" Pop Shoreline
13 14 51 52

✓ 12" OAK +55 76
✓ 14" OAK +56 67
✓ 55" B.G. CL Fence 90
+50 +51 14" OAK 58
+53 20" OAK 79

✓
BIT
13.5

✓
Shoreline
81

✓ 11" OAK +33 77
✓ 11" GAS VENT +34 39
✓ 11" OAK +20 59
✓ 14" OAK +39 72
✓ 32 B. 1/2" BIT Overlay +32 21
✓ 35 GAS VALVE 21

✓ PP
+5 69

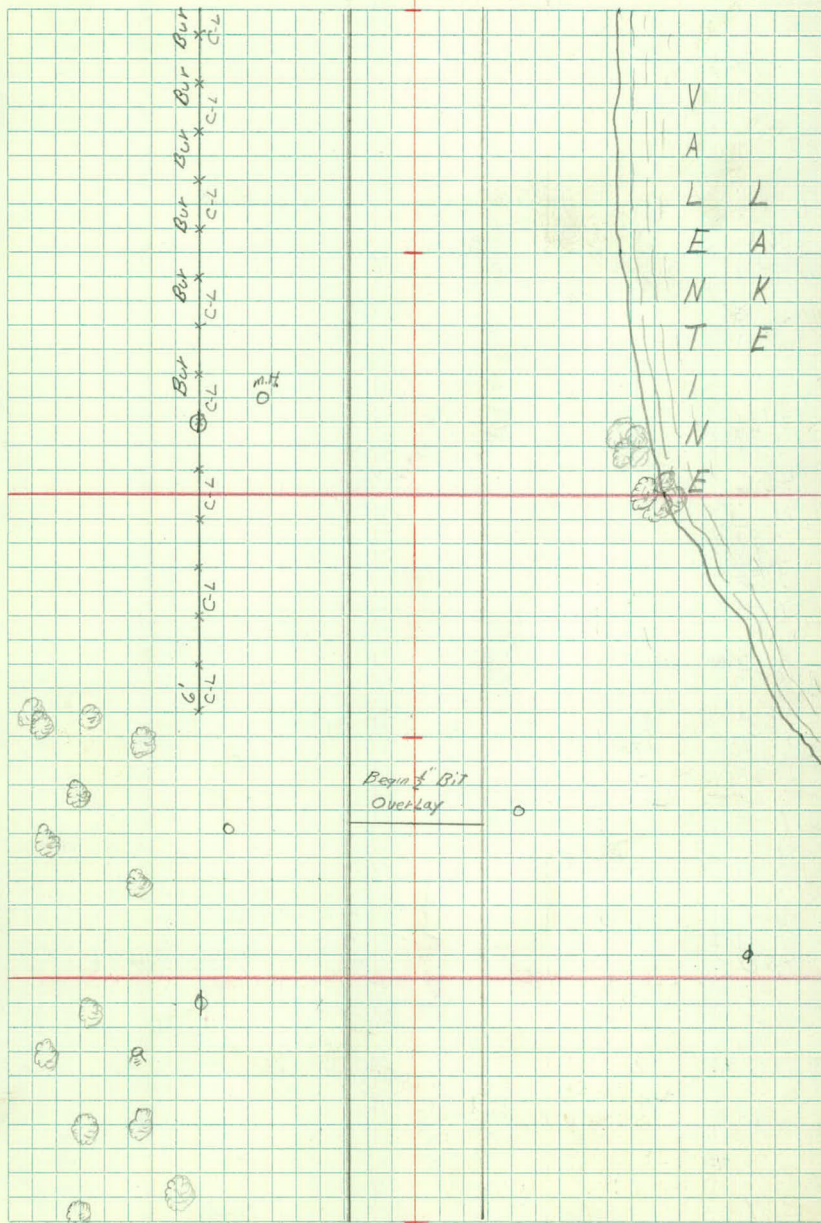
259

✓ PP +95 95
✓ 8" OAK +89 87
✓ 8" OAK +94 69
✓ 8" OAK +69 61
✓ 12" OAK +71 58
✓ 12" OAK +86 77
✓ 12" OAK +55 51
✓ 5' Willow +51 73

✓ Stump Conc Conc
+89 59 73 14
+86 77

✓ P.B. AREA Shoreline
95 100

+50



+50

LT

E

$$\frac{\text{conc}}{14}$$

RT

$$\frac{\text{SL}}{77}$$

$$+98 \frac{\text{Box Elder}}{72}$$

$$+11 \frac{\text{Culvert}}{32} +29 \frac{\text{GOR}}{14}$$

$$+08 \frac{\text{C.B.}}{28}$$

263

$$+00 \frac{\text{POR}}{23}$$

$$\frac{\text{conc}}{14} \frac{\text{conc}}{14}$$

$$\frac{\text{Shoreline}}{75}$$

$$+98 \frac{\text{WSO}}{38}$$

$$+78 \frac{\text{OR}}{62}$$

$$+88 \frac{\text{POR}}{37}$$

+50

$$+57 \frac{\text{C.CORR}}{70}$$

$$+45 \frac{\text{RTTOR}}{70-100}$$

conc

$$\frac{\text{Shoreline}}{69}$$

$$+37 \frac{\text{ER}}{43}$$

$$+41 \frac{\text{NECORR}}{82}$$

$$+25 \frac{\text{POR}}{26}$$

$$+25 \frac{\text{WSO}}{41}$$

$$+18 \frac{\text{AROC light pole}}{44} +18 \frac{\text{BRT To 12'cm}}{44}$$

$$+17 \frac{\text{BARRON 24'cm}}{31}$$

+20 E. 1/2" B.T overlay

$$+36 \frac{\text{RCP}}{32}$$

$$+11 \frac{\text{14'cmp}}{83}$$

$$+9 \frac{\text{RT to 18'cmp}}{14}$$

$$+67 \frac{\text{Shoreline}}{66}$$

$$+02 \frac{\text{RCP}}{32}$$

$$+01 \frac{\text{BR}}{14}$$

262

$$+98 \frac{\text{SECORR}}{97}$$

$$\frac{\text{B.T}}{14} \frac{\text{B.T} + 01}{14}$$

$$+30 \frac{\text{RCP \& 6' Ditch}}{30}$$

$$+86 \frac{\text{12'cmp}}{51}$$

$$+77 \frac{\text{HYD}}{40}$$

$$+72 \frac{\text{WSO}}{35}$$

$$+80 \frac{\text{18'cmp}}{46}$$

$$+91 \frac{\text{Shoreline}}{57}$$

$$+69 \frac{\text{E.C.L Fence}}{45}$$

$$+67 \frac{\text{PP}}{63}$$

+50

$$\frac{\text{Fence}}{45}$$

$$\frac{\text{Buried cable}}{42}$$

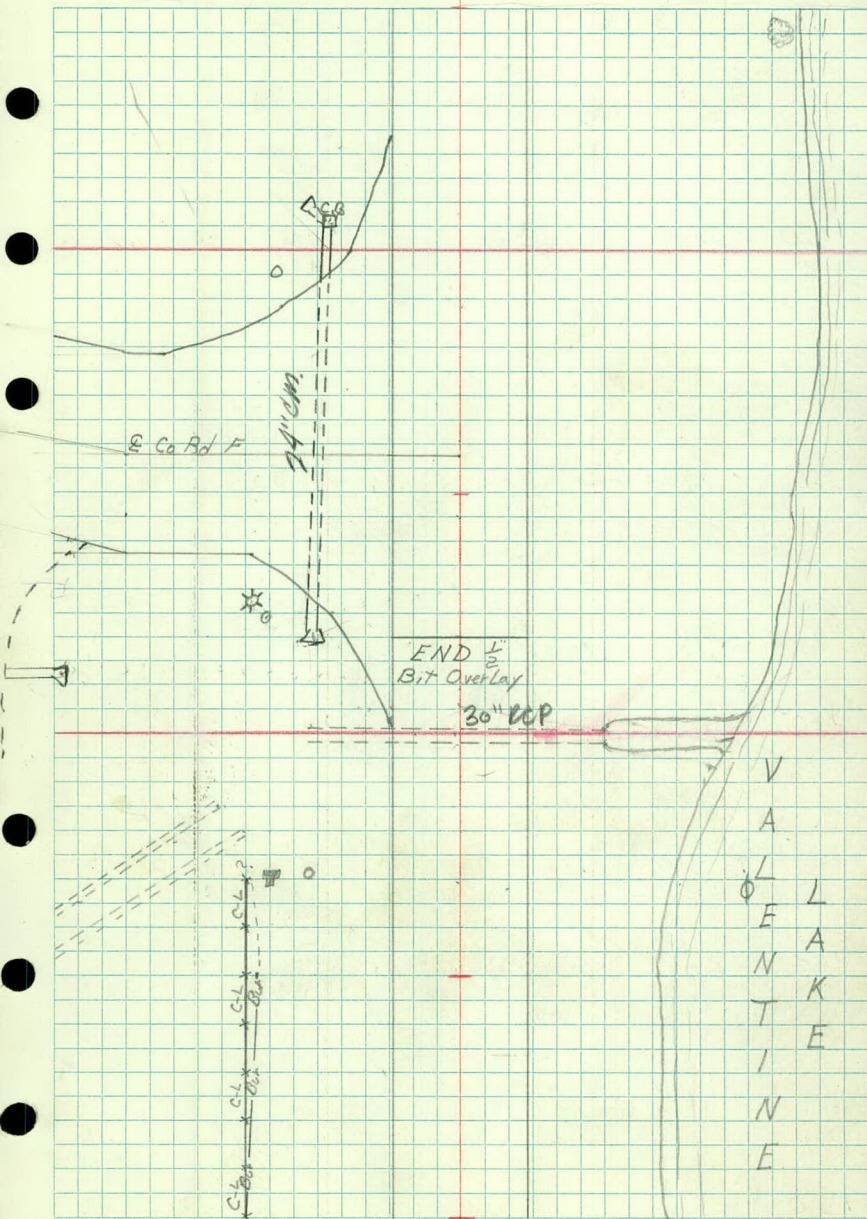
$$\frac{\text{B.T}}{13} \frac{\text{B.T}}{14}$$

$$\frac{\text{Shoreline}}{41}$$

261

$$\frac{\text{B.T}}{14}$$

$$\frac{\text{Shoreline}}{42}$$



266 LT Brush & Trees CONC CONC GR RT Shoreline
 49-82 14 13 18 51

+83 Brush & Trees
 48

+75 TP
 42

+67 MH
 17

+50 Brush & Trees CONC CONC GR Shoreline
 42-71 14 13 19 57

+25 Brush & Trees
 47-71

+03 SP. Way
 14

265 Brush & Trees CONC CONC GR Shoreline
 47-87 14 13 18 61

+93 SP. Way +95 SP. Way
 20-26 20-26

+84 B. SP. Way
 14

+75 Brush & Trees
 48-87

+50 Brush & Trees CONC CONC GR Shoreline
 55-87 14 13 18 64

+35 Brush & Trees
 56-87

+23 Plum Tree
 65

+36 PIP
 58

+14 B. Brush & Trees +14 Plum Tree
 68-87 66

+22 B. Guard Rail
 19

264 CONC CONC Shoreline
 +99 CP 14 14 69
 45

+50 CONC
 14
 July 14, 70 C. Pearson

July 16 1970

38

PK
CP
BP

DR
JT

V

A

L

E

M

7

1

M

E

L

A

K

E

+50

LT

Fence
67Conc
14Conc
14

RT.

+31 20" OAK
69+47 Twin 8" Elm
60+21 1" Pine
59+26 Twin 8" Elm
61

268

4" OAK
66Fence
64Conc
14Conc
14+89 E. GR
19+107 8" Elm
61+10 Twin 6" Willow
105+90 30" OAK
72+83 1" Pine
68+72 Fecor
96+78 Fecor
61+72 11" Elm
61+64 18" CM
27

+50

E 8' DIRT FENCE Fence Conc Conc Trip 7" Willow GR Shoreline
96 14 13 67 18 73+33 18" OAK
91+36 Trip 7" Willow
61+25 IP
37+27 18" CM
27+32 Fewer wood
94-100++14 5" Willow 5"
57

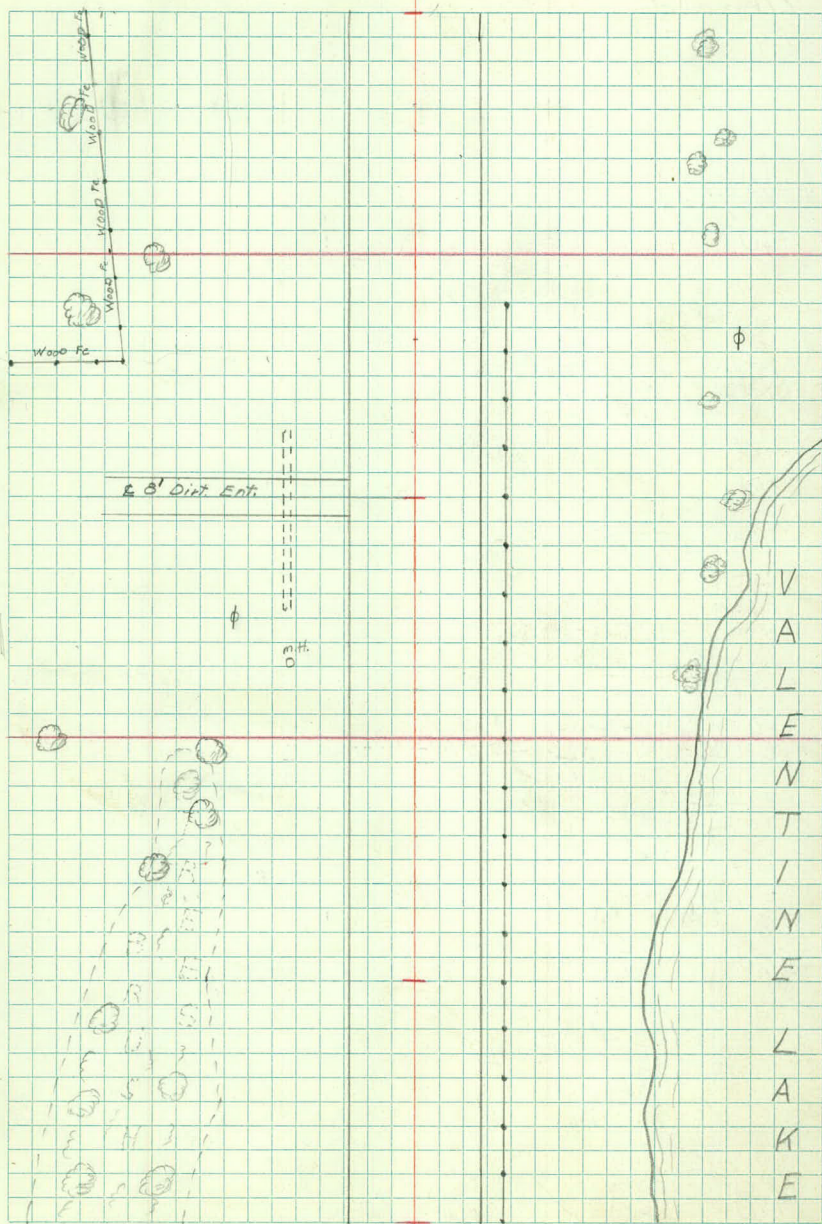
267

+16 1" Pine
27+02 Twin 16" OAK
78 ConcConc GR
13 19Shoreline
59+99 3" Pine END Brush
44+86 3" Pine
45+75 Brush +75 10" OAK
40-54 54

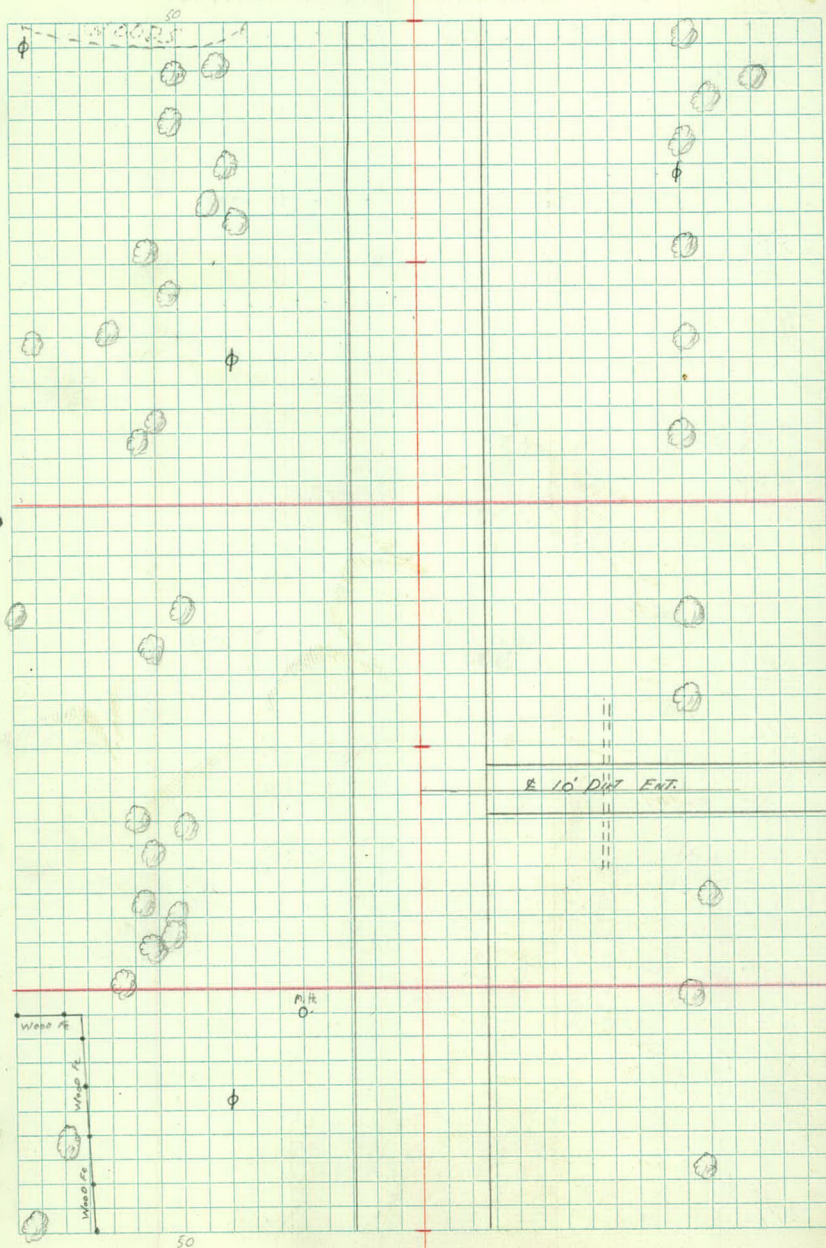
+50

Brush & Trees
43Conc
14Conc
13GR
18Shoreline
47+25 Brush & Trees
41

266



271	woods	LT	RT
+95 PP	36-82	conc 14	conc 14
			+98 6" Elm
+92 5" Popel	+90 5" Oak		+88 6" Apple
	52		+85 Russian olive
+66 3" Popel	+71 2" Popel	twine 52	+76 2" Elm
	46		53
+54 2" Popel	+61 2" Popel	+64 2" Popel	+67 PP
	57	39	54
+50	+52 S. Ecor House	conc 13	conc 14
	107		+54 2" Elm
			54
+45 5" Cot. Tanwood	+47 2" Cottonwood		
	58	65	
+31 TP	+35 36" Oak		+35 6" Elm
	39		54
	+14 2" Popel	+17 2" Popel	+15 6" Elm
270	59	50	54
		conc 14	conc 14
+97 IRON PAST			
	87		+78 7" Elm
			55
+79 20" Oak	+80 1" Popel		
	85	50	
+73 5" Cottonwood			+59 12" Elm
	56		37
+50			+62 8" Elm
+37 4" Willow		conc 14	conc 14
	60		+41 10" ENT DIRT
+31 3" Cottonwood	+35 4" Willow		34
	56	51	
+25 18" Oak	+13 2" Popel	+18 6" Willow	+21 6" Elm
	72	51	58
+11 2" Popel			+24 12" Elm
	44		37
+8 1" Popel	+10 2" Popel	conc 14	conc 14
	64	57	6" Elm
269			55
+90 FESOR			
	72-100		
+77 TP	+98 MH		
	40	25	
+70 30" Oak			
	75		
+52 14" Oak			+64 8" Elm
	83		58
+50			



+50

LT

woods
97conc
14

&

conc
14

RT

woods
46-100+

273

woods
78-100+conc
14conc
14woods
54-100++86 8" willow
40+78 8" Popel
56

+50

+40 woods
39-70-100++06 24" Oak
107+05 PP
83+05 TP
38

272

woods
38-80conc
14conc
14+48 Bit
53-66-86+43 14" Elm
48+21 12" Elm
47+06 Bit
14+06 BR
34+10 Bit
47-71conc
14conc
14+90 Por
39+97 Big ENT
34

+71 RT to ENT

+86 Bit
14+78 14" CM
35+76 10" Elm
51+86 Bit
50-71

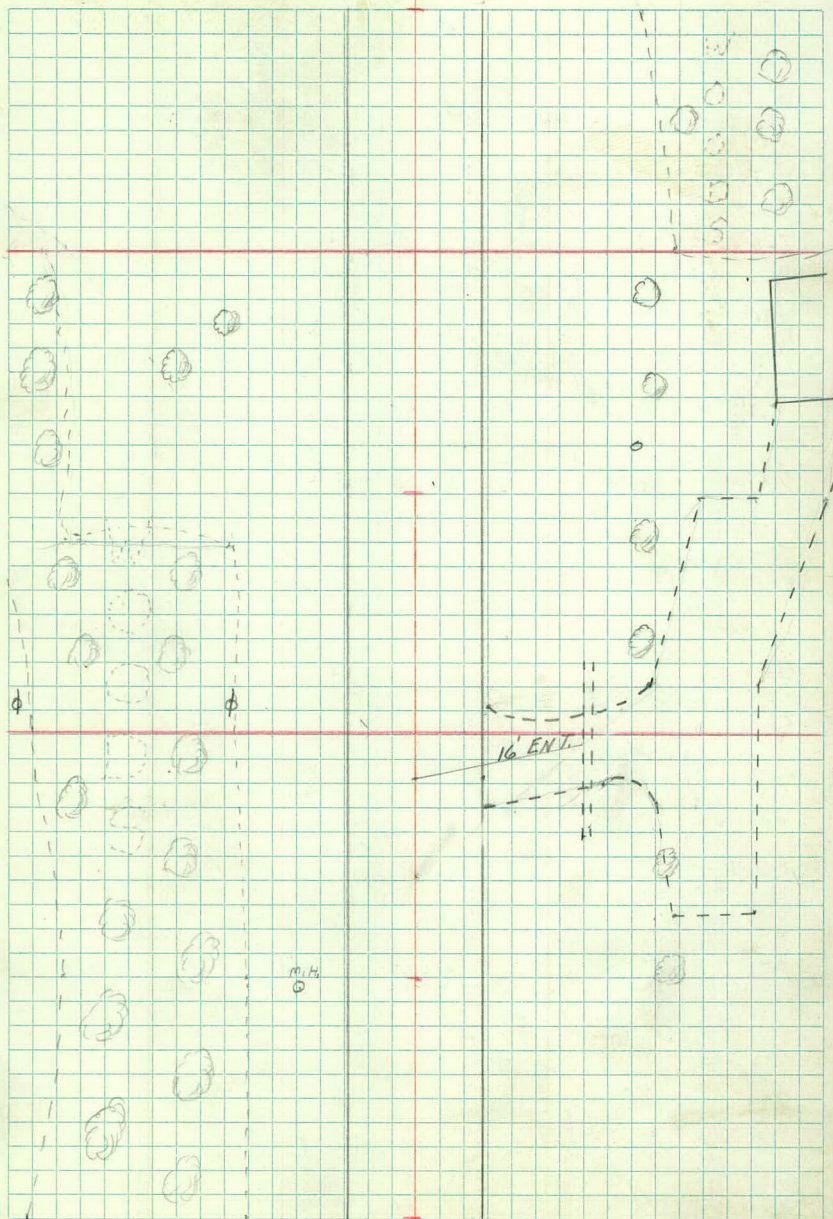
+51

SE cor swimming pool
88+63 Bit
54-74

+50

woods
2-74
+49 MH
25conc
13conc
1453 8" Elm
53+34 Tri 8" Oak
87

271



L7

C

RT.

276 +99 $\frac{4}{46}$ VALENTINE

BIT

Shoreline

+94 RT TO $\frac{4}{46}$ RA +81 $\frac{14}{14}$ (End Conc)

54

+89 $\frac{14}{14}$ +77 $\frac{4'' \text{ willow}}{77}$ +84 $\frac{BR}{26}$ +87 $\frac{8'' \text{ willow}}{54}$ +57 $\frac{1.4'' \text{ willow}}{70}$ +64 $\frac{BR}{14}$ +50 +60 $\frac{5'' \text{ willow } 2''}{61}$ DIT DIT
14 14

Shoreline

43

+49 $\frac{\text{Twin } 2'' \text{ willow}}{52}$ 275 +6 $\frac{PO}{38}$ +24 $\frac{7'' \text{ Poplar}}{40}$

+25 Shoreline

+90 $\frac{2 \text{ Dead } 12' \text{ oak}}{72}$ +90 $\frac{10' \text{ oak}}{69}$ Conc Conc
14 14+8 $\frac{1.4''}{27}$ Shoreline
+88 $\frac{\text{Good } 12'' \text{ cottonwood}}{66}$ 55+81 $\frac{\text{Dead } 12' \text{ oak}}{57}$ +95 $\frac{13 \frac{1}{2}'' \text{ B.T. over } 14''}{14}$ +64 $\frac{10' \text{ oak}}{85}$

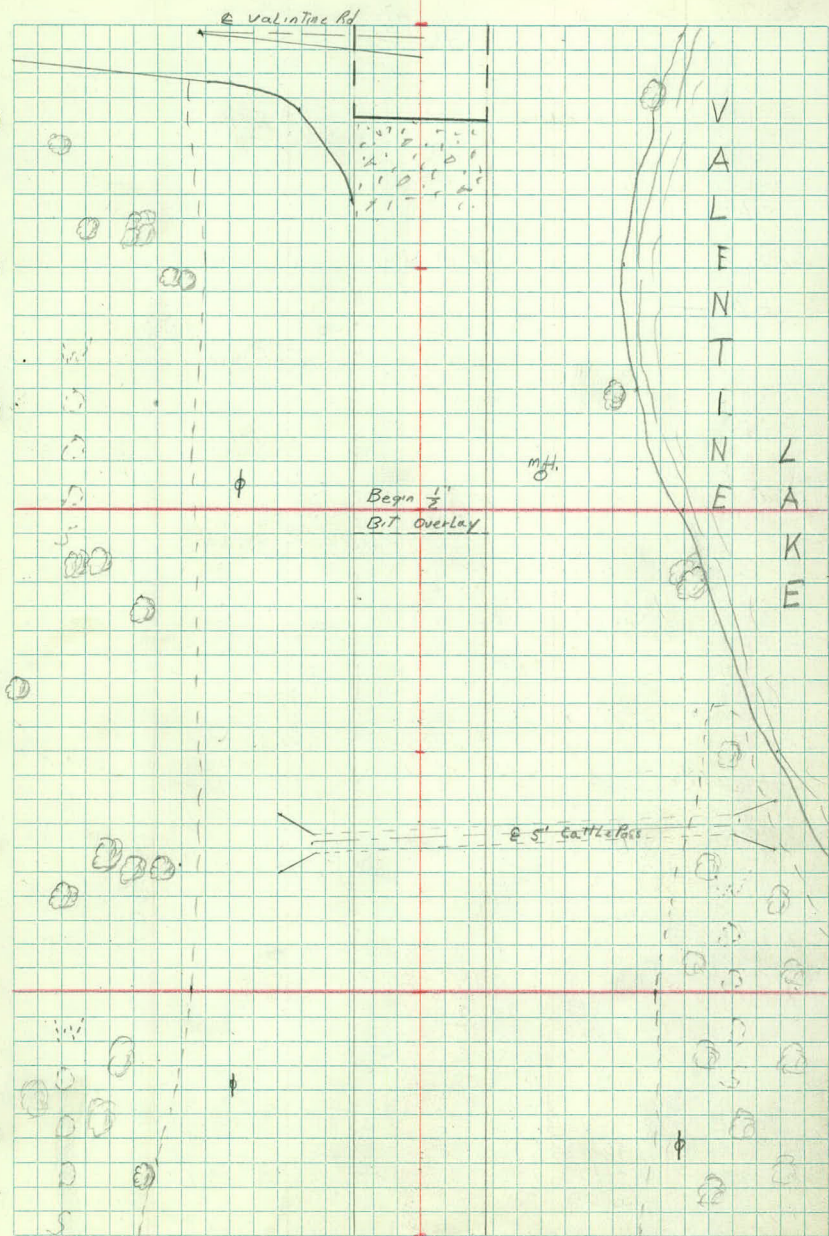
+50

Conc Conc
14 14+57 $\frac{F. woods}{52-79}$

+66 Shoreline

+37 $\frac{\text{wing wall}}{29}$ +46 $\frac{12'' \text{ Twin oak } 14''}{54}$ +40 $\frac{\text{wing wall}}{74}$ +36 $\frac{1 \text{ cut } 10' \text{ post}}{67}$ +25 $\frac{\text{wing wall}}{29}$ +31 $\frac{1.5'' \text{ cattle pass}}{22}$ +30 $\frac{\text{wing wall}}{74}$ Shoreline
100+29 $\frac{15' \text{ oak Sward}}{67}$ +21 $\frac{15' \text{ oak}}{76}$ +28 $\frac{5'' \text{ Basswood}}{54}$ +28 $\frac{12' \text{ elm}}{55}$ 277 woods
47-100+Conc
14woods
48-100++81 $\frac{TP}{35}$ +63 $\frac{6'' \text{ Poplar}}{59}$ +63 $\frac{\text{woods}}{59-100+}$ +68 $\frac{PP}{52}$ +66 $\frac{PP}{87}$

273 +50



LT.

E

RT.

+50

+43 IRON POST
83B.T B.T
12 13+29 Twins 14" cottonwood
76
+21 10" willow
77+9 20' OAK
75

278

B.T B.T
12 12+90 14" OAK +95 PP
91 39+80 STUMP
99Shoreline
110+65 STUMP
82

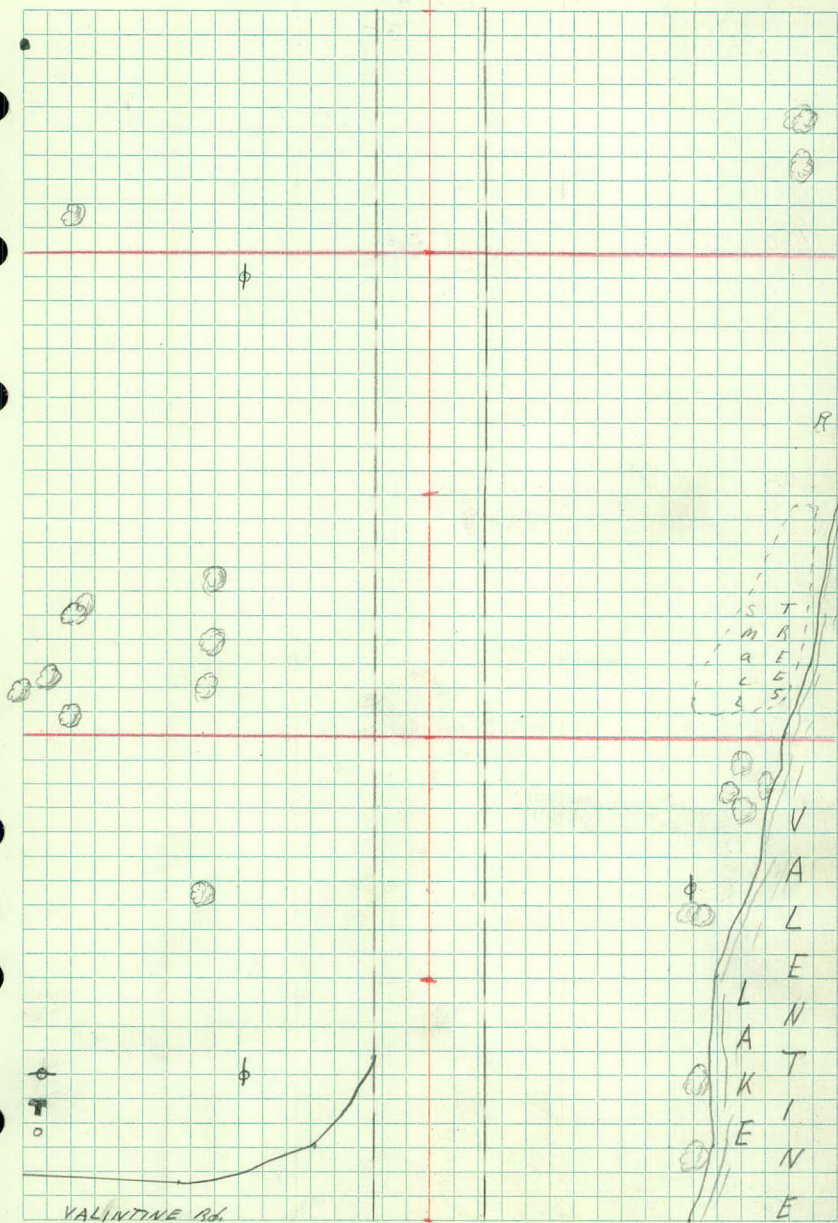
+50

B.T
12+26 Twins 5" OAK +34 2" Cottonwood
76 47+47 Small Trees
78-80Shoreline
82+12 6" OAK +20 2" Cottonwood
81 47+10 6" OAK +12 2" Cottonwood
86 47+8 Small Trees
60-79+13 Shoreline
79277 +05 2" Cottonwood
76B.T B.T
12 12+95 6" Aspen
64Shoreline+97 8" OAK
100+87 1" Elm
62+90 6" willow
72+85 6" Aspen
64+67 PP
54+69 2" Cottonwood
47+64 Twins 2" poplar
54

+50

B.T B.T
12 13Shoreline
60+32 PP
39
+34 ER +32 PP
12 81
+15 FOR 120 HYD
24 83+30 trip 4" willow
56+7 BR +19 W50
52 83+15 8" willow
56+15 Shoreline
57

276



L+

C

Rt.

281

$$\begin{array}{r} \text{B.T. B.T.} \\ 17 \quad 17 \end{array}$$

$$+81 \quad \begin{array}{r} \text{B.T.} \\ 17 \quad 17 \end{array}$$

$$+82 \quad \begin{array}{r} \text{Bush} \\ 62 \end{array}$$

$$+79 \quad \begin{array}{r} \text{B.T.} \\ 15 \end{array} +72 \quad \begin{array}{r} \text{Bush} \\ 70 \end{array}$$

$$+54 \quad \begin{array}{r} \text{HPD} \\ 39 \end{array}$$

+50

$$+49 \quad \begin{array}{r} \text{B.T.} \\ 14 \end{array} \quad \begin{array}{r} \text{B.T.} \\ 15 \end{array}$$

+7

280

$$+99 \quad \begin{array}{r} \text{B.T. ENT} \\ 39 \end{array} \quad 96 \text{ RT ENT} \quad \begin{array}{r} \text{B.T. B.T.} \\ 14 \quad 13 \end{array}$$

$$+92 \quad \begin{array}{r} \text{E. Woods} \\ 59-100+ \end{array}$$

Conc & Rock

$$+71 \quad \begin{array}{r} \text{Mailbox} \\ 29 \end{array} \text{ STAND}$$

$$+67 \quad \begin{array}{r} \text{PP} \\ 39 \end{array}$$

$$+74 \quad \begin{array}{r} \text{BP} \\ 59 \end{array}$$

$$\begin{array}{r} \text{woods} \\ 60 \end{array}$$

$$+61 \quad \begin{array}{r} \text{Rock wall} \\ 55-100+ \end{array}$$

+50

$$+51 \quad \begin{array}{r} \text{B.T. ENT} \\ 63 \end{array}$$

$$\begin{array}{r} \text{B.T.} \\ 12 \end{array}$$

$$\begin{array}{r} \text{woods} \\ 75 \end{array}$$

$$+41 \quad \begin{array}{r} \text{Rock wall} \\ 63-100+ \end{array}$$

$$+27 \quad \begin{array}{r} \text{Rock Yard decoration} \\ 77 \end{array}$$

$$+27 \quad \begin{array}{r} \text{B Woods} \\ 83-100+ \end{array}$$

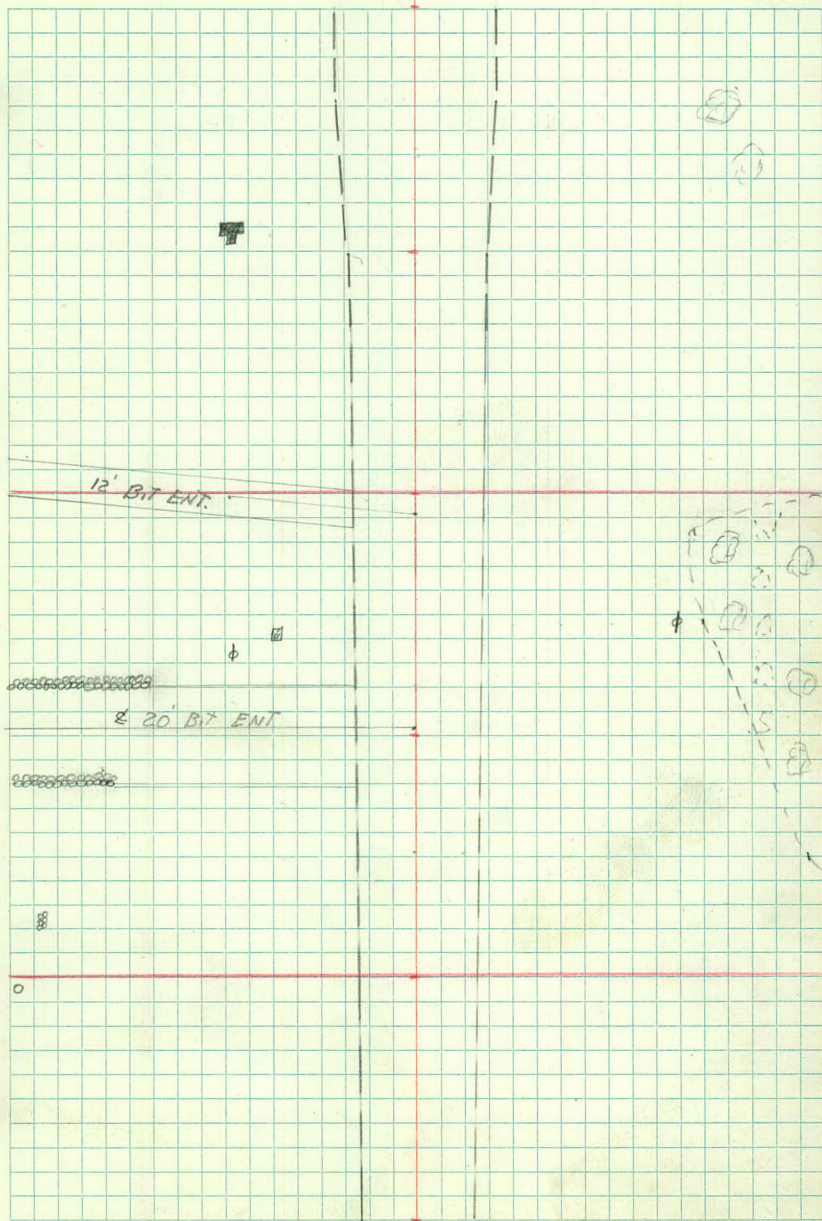
$$+11 \quad \begin{array}{r} \text{Silver maple} \\ 90 \end{array}$$

279

$$\begin{array}{r} \text{B.T. B.T.} \\ 12 \quad 12 \end{array}$$

$$+98 \quad \begin{array}{r} \text{water service} \\ 83 \end{array}$$

+50



LT.

C

RT.

+50

CURB B.T B.T
22 17 17

CURB
22

+40 Embankment +45 wingwall
61 65

+29 wingwall
65
+24 Ret wall
60

+35 Ret wall +37 Ret wall
28 61

+27 Ret wall +25 Embankment
28 60

+13 Piller +28 Piller
50 30

+04 Piller +20 Piller
30 30

283

CURB B.T B.T
22 17 17

CURB
22

+88 Ret wall +96 Piller
28 30

+88 Piller
30

+89 Embankment +92 Ret wall
61 61

+77 Ret wall +81 Ret wall
60 36

+84 PP +85 wingwall
39 66

+69 wingwall +73 Embankment
65 60

+82 CURB +65 TP
26 40

+60 CURB
23

+50 +64 B CONC CURB
29

+53 B CONC CURB
26

B.T B.T
17 17

+25 Fence RT Fence 45
77

+21 4" Cottonwood
79

+10 APRON +6 12 3" Cottonwood
45 53

282

+103 Apron 30" RCP
55

B.T B.T
17 17

+98 NH
36

+98 4" Cottonwood
69

+60 PP
53

+52 Bush
56

+50

B.T B.T
17 17

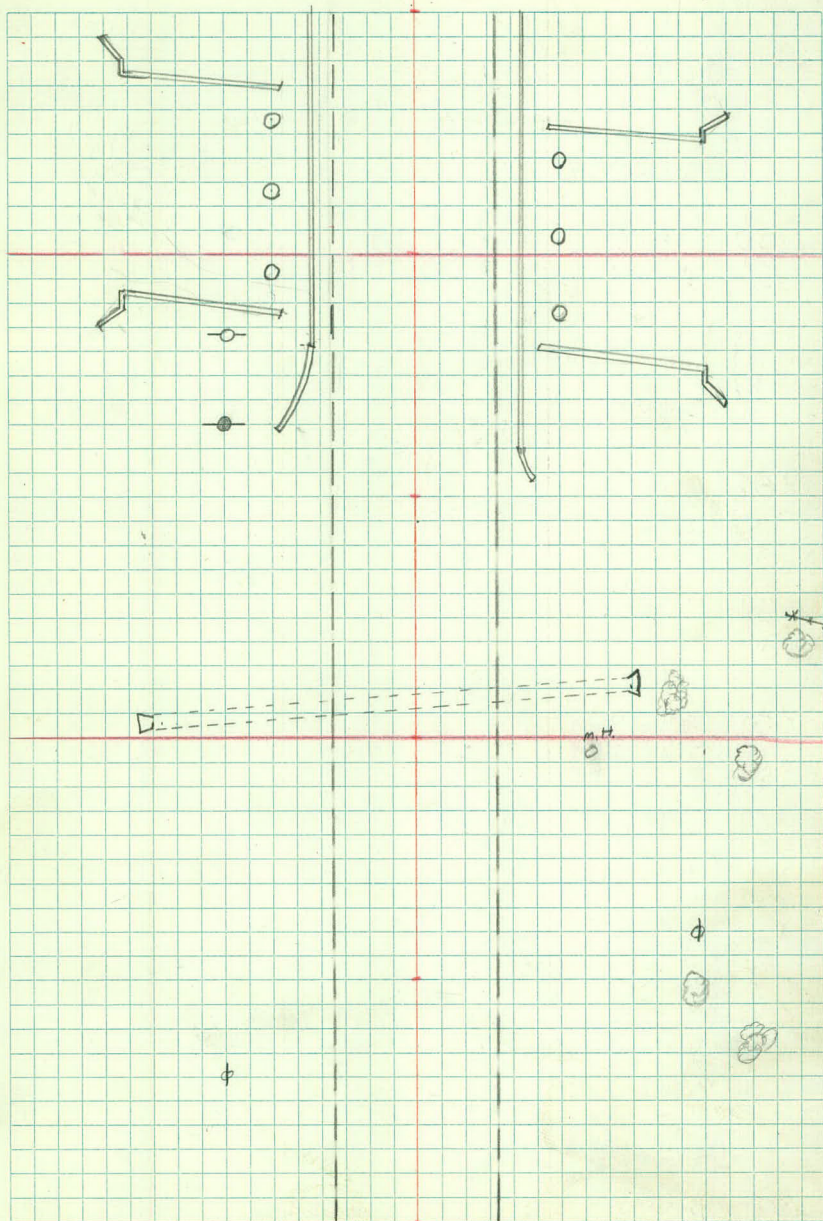
+30 PP
48

+38 5 willow 10"
67

281

7-20-70

45



LT.

E

RT

286

$$\begin{array}{r} \text{Fence E} \\ 99 \end{array}$$

$$\begin{array}{r} \text{B.I.T} \\ 12 \end{array} \quad \begin{array}{r} \text{B.I.T} \\ 12 \end{array}$$

+50

$$\begin{array}{r} \text{B.I.T} \\ 13 \end{array} \quad \begin{array}{r} \text{B.I.T} \\ 12 \end{array}$$

$$+21 \quad \begin{array}{r} \text{B.I.T} \\ 13 \end{array}$$

285

$$\begin{array}{r} \text{B.I.T} \\ 13 \end{array}$$

$$+86 \quad \begin{array}{r} \text{B.I.T} \\ 13 \end{array}$$

+50

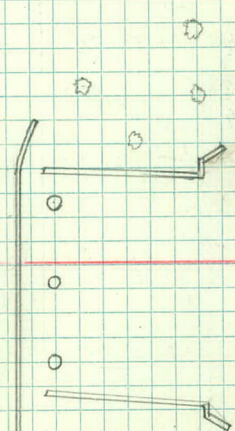
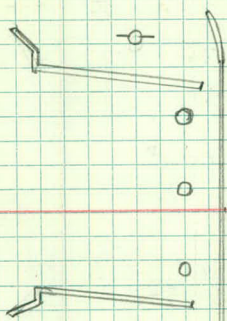
+38 wing wall 66	+36 PP 40	+42 CURB 25	+37 Bosh 36	+48 Bosh 59	+27 Bosh 56	+35 Bosh 60
+30 Ret wall 61	+33 Embankment 61	+32 CURB 22	+29 CURB 26	+26 Bosh 47	+24 wing wall 65	
+26 Ret wall 27	+20 Pillar 30		+20 CURB 22	+20 Ret wall 27	+19 Embankment 60	
+5 Pillar 30			+13 Pillar 30		+18 Ret wall 60	

284

+88 Pillar 30	CURB 22	B.I.T 12	B.I.T 12	CURB
+84 Ret wall 61		+81 Ret wall 12	+96 Pillar 30	
+78 wing wall 66	+82 Embankment 61	+80 Pillar 30	+70 Embankment 61	
+81 Ret wall 28		+73 Ret wall 27	+71 Ret wall 61	
+50		+66 wing wall 66		

7-20-70

46



+50

LT,

✓
B.I.T
12 13

RT

288

✓
B.I.T
12 13

✓
+95 $\frac{1}{2}$ C.R. ENT
85 21'

+79 $\frac{PP}{40}$

+69 $\frac{3}{4}$ " Pine +68 $\frac{1}{2}$ C.R. ENT
71 53 21'

+50

B.I.T B.I.T
12 12
+44 $\frac{1}{4}$ " Pine
87

+43 $\frac{1}{2}$ C.R. ENT
38 21'

+26 $\frac{B.I.T}{29}$ +45 RT Jo ENT

(NSP)
+07 $\frac{1}{4}$ "

+20 $\frac{B.I.T}{46}$ B.I.T
+16 $\frac{64}{64}$

287 +96 $\frac{CMP}{37}$ Por 10
R.T. = +80 +84 $\frac{1}{2}$ 10' B.I.T ENT
48 +94 $\frac{1}{2}$ 24 90 40

+00 $\frac{53}{53}$ Por
+93 $\frac{24}{24}$ Por 36 +93 $\frac{58}{58}$ Por 72

+71 $\frac{15" CM}{39}$ +73 $\frac{Por}{33}$
+67 $\frac{1}{2}$ F. Fence 67 $\frac{23}{23}$ Por
+55 $\frac{BR}{12}$

+74 $\frac{BR}{12+80}$ B. Fence 78
+75 $\frac{Fence}{86}$ +75 $\frac{1}{2}$ B.I.T ENT 16'
100
+67 $\frac{3}{4}$ " Pine
70

+50

Fence
62

B.I.T
12

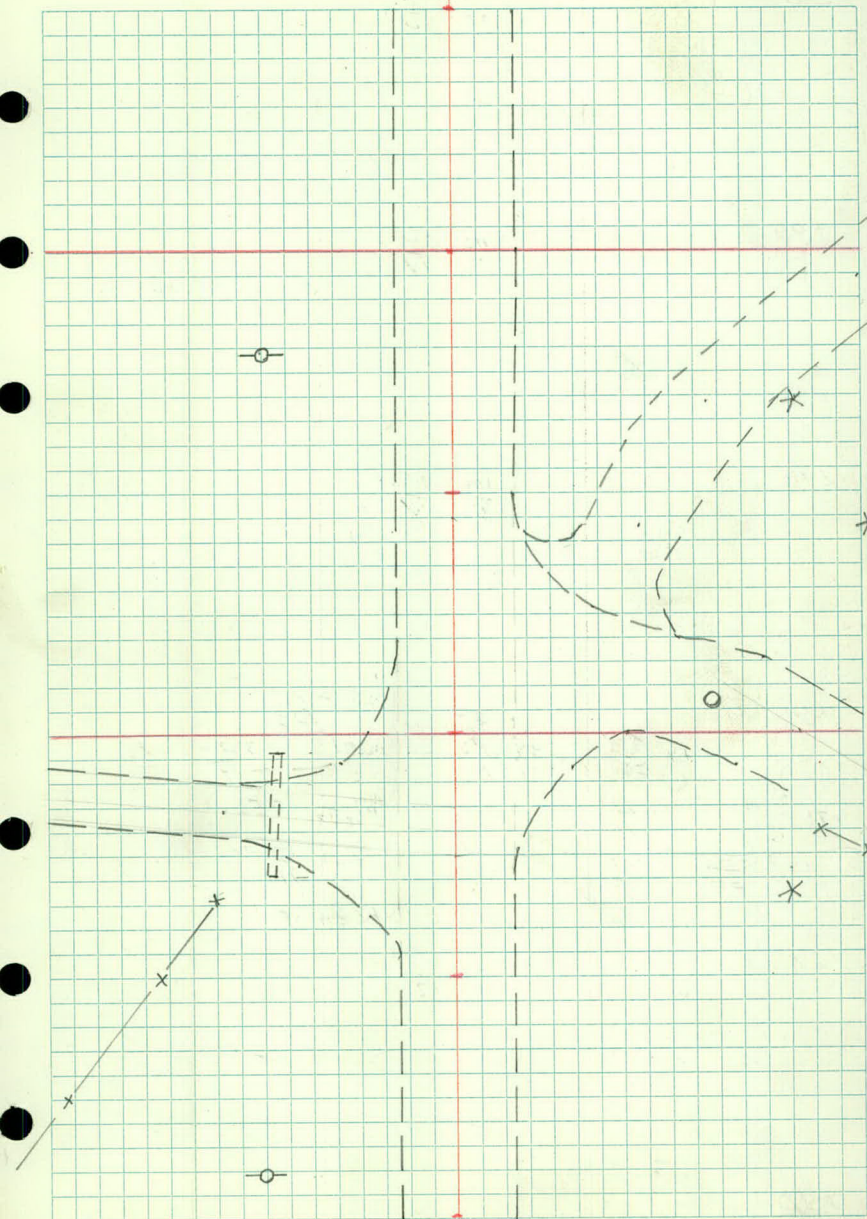
+25 Fence
82

+9 $\frac{PP}{40}$

286

7-20-70

47



LT.

2

RT.

291

✓
CONC 13
✓
CONC 14

✓
+91 PP
37

✓
+82 RW Marker
85

✓
+69 PP
54

+50

✓
CONC 13
✓
CONC 14

290

✓
CONC 13
✓
CONC 14

+50

✓
+49 GP
70

✓
+49 GP
37

✓
CONC 13

✓
+53 PP
103
✓
+48 PP
54
✓
+41 PP
103

✓
+48 Pole Brace
74

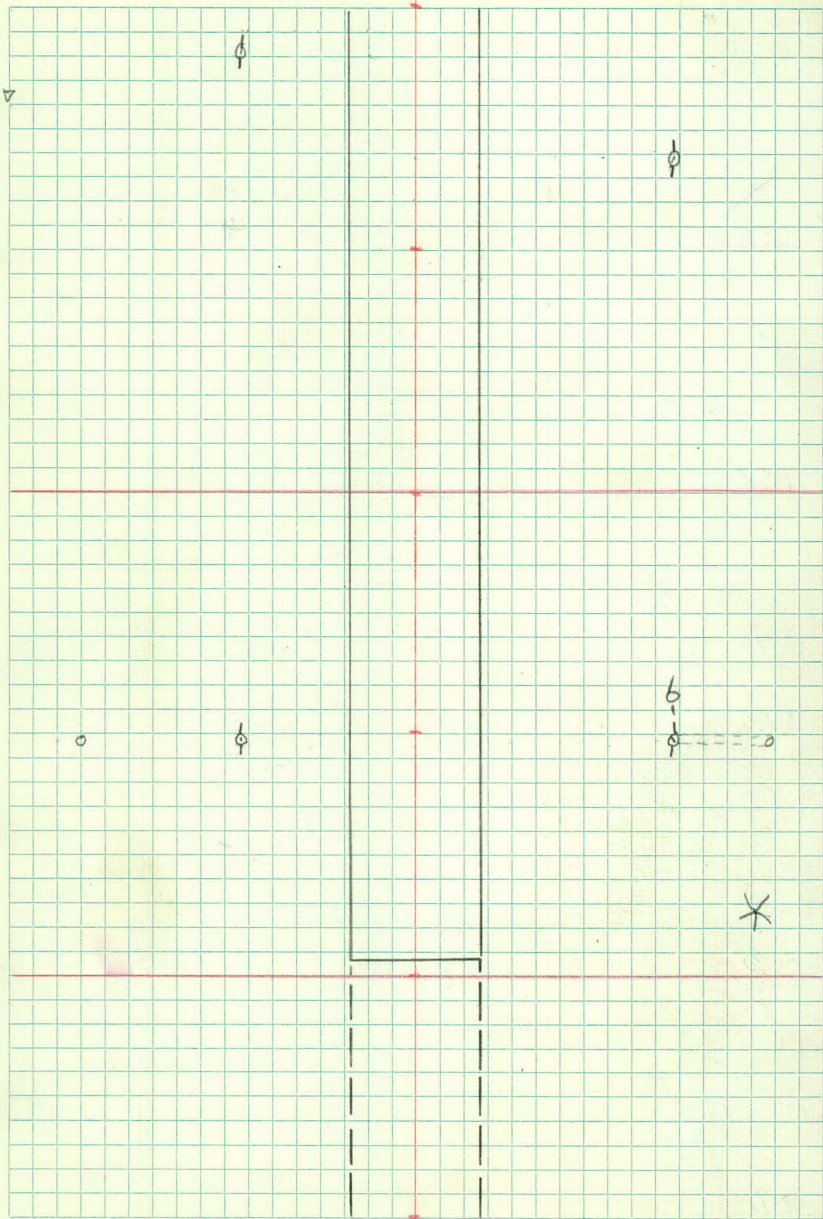
✓
CONC 14
✓
CONC 13

✓
+13 3" Pipe
71

+63 B. Conc Pavement

289

+50



LT.

E

RT.

+50

$$\begin{array}{r} \text{conc} \quad \text{conc} \\ 14 \quad 14 \end{array}$$

293

$$\begin{array}{r} \checkmark \quad \checkmark \\ \text{conc} \quad \text{conc} \\ 13 \quad 14 \end{array}$$

$$\begin{array}{r} \downarrow \quad \text{PP} \\ +77 \quad 54 \end{array}$$

+50

$$\begin{array}{r} \downarrow \quad \downarrow \\ \text{conc} \quad \text{conc} \\ 13 \quad 14 \end{array}$$

$$\begin{array}{r} \downarrow \\ +26 \quad \text{PP} \\ 37 \end{array}$$

292

$$\begin{array}{r} \downarrow \quad \downarrow \\ \text{conc} \quad \text{conc} \\ 14 \quad 14 \end{array}$$

$$\begin{array}{r} \downarrow \\ +57 \quad \& \text{Dist} \quad 12' \\ \hline 14-100+ \end{array}$$

+50

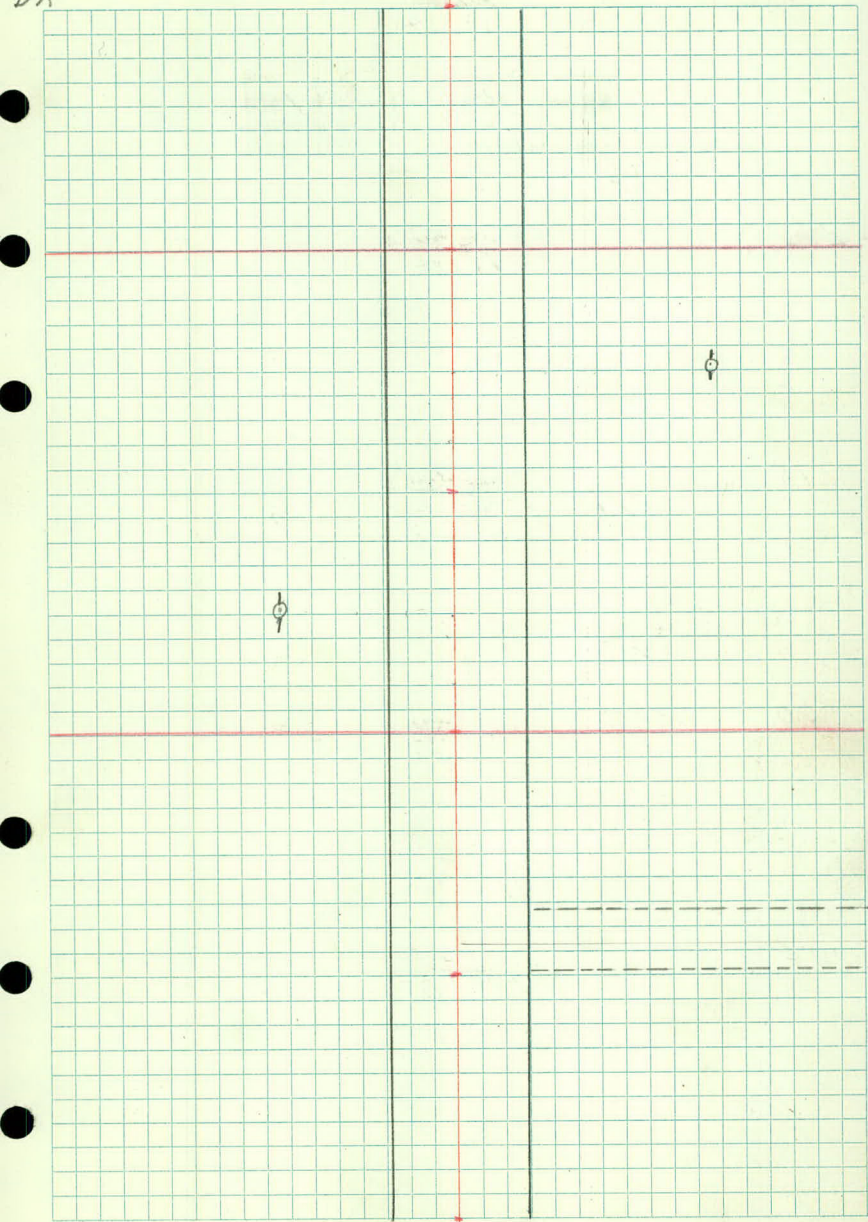
$$\begin{array}{r} \downarrow \quad \downarrow \\ \text{conc} \quad \text{conc} \\ 14 \quad 14 \end{array}$$

291

FH
CP
BP
DR

7-20-70

49



L7

E

Rt.

296

$$\begin{array}{r} \downarrow \quad \downarrow \\ \text{B.T.} \quad \text{B.T.} \\ 14 \quad 14 \end{array}$$

$$\begin{array}{r} \checkmark \\ +97 \quad \text{Bush dump} \\ 95 \end{array}$$

+70 Beg. B.T. overlay

$$\begin{array}{r} \checkmark \\ 8'' \text{ Cottonwood} \\ +69 \quad 67 \end{array}$$

+50

$$\begin{array}{r} \checkmark \quad \checkmark \\ \text{Conc} \quad \text{Conc} \\ 13 \quad 14 \end{array}$$

$$\begin{array}{r} \checkmark \\ +50 \quad \text{E2' Ditch} \\ 82 \end{array}$$

295

$$\begin{array}{r} \downarrow \\ \text{P.P.} \\ +97 \quad 38 \end{array}$$

$$\begin{array}{r} \downarrow \\ \text{NE Cor Amphouse} \\ +91 \quad 70 \end{array}$$

$$\begin{array}{r} \downarrow \\ \text{SE Cor Amphouse} \\ +73 \quad 70 \end{array}$$

$$\begin{array}{r} \downarrow \quad \downarrow \\ \text{Conc} \quad \text{Conc} \\ 13 \quad 14 \end{array}$$

$$\begin{array}{r} \downarrow \quad \downarrow \\ +00 \quad \text{Endwood} \quad +00 \quad \text{E2' Ditch} \\ 77-85 \quad 91 \\ \downarrow \quad \downarrow \\ +89 \quad \text{P.P.} \\ 57 \\ \downarrow \quad \downarrow \\ +73 \quad \text{Woods} \\ 75-100+ \end{array}$$

+50

$$\begin{array}{r} \downarrow \quad \downarrow \\ \text{Conc} \quad \text{Conc} \\ 13 \quad 13 \end{array}$$

$$\begin{array}{r} \downarrow \\ \text{B. woods} \\ +42 \quad 100 \end{array}$$

294

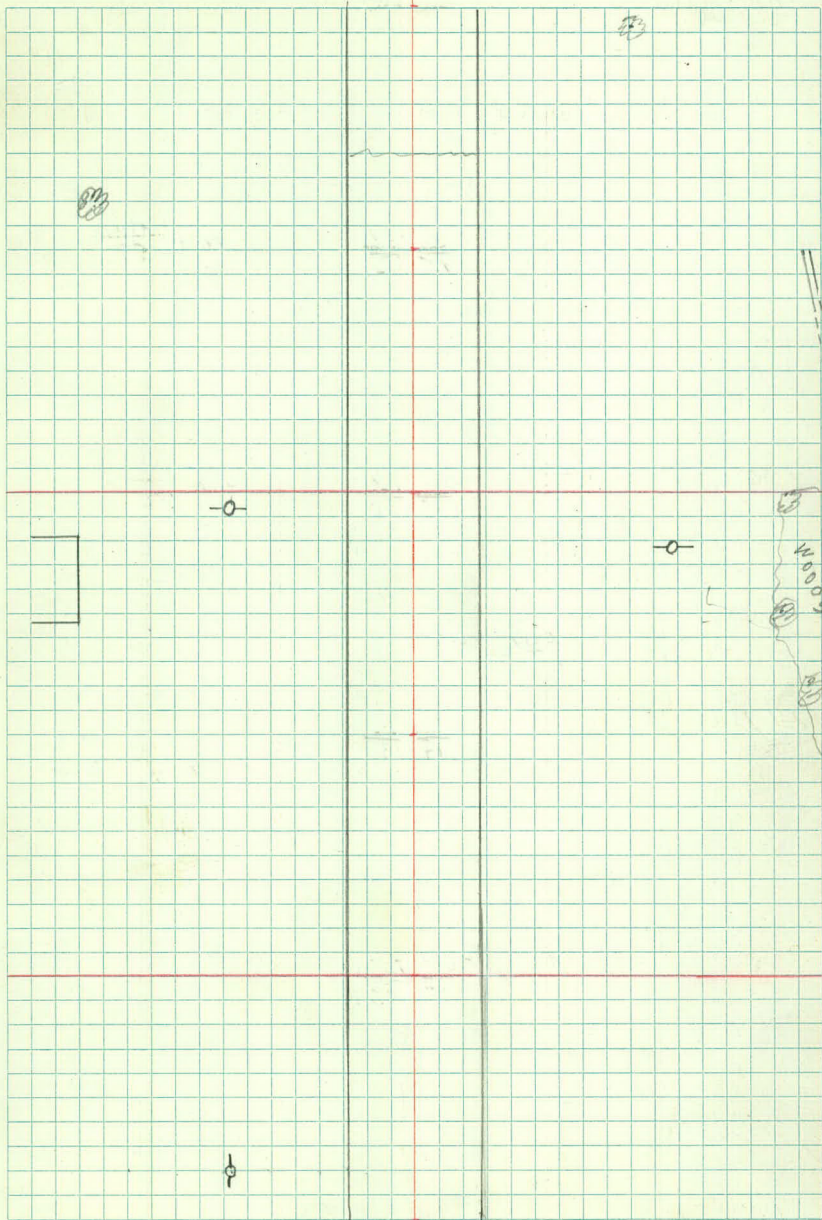
$$\begin{array}{r} \downarrow \quad \downarrow \\ \text{Conc} \quad \text{Conc} \\ 14 \quad 14 \end{array}$$

$$\begin{array}{r} \downarrow \\ 60 \quad \text{PP} \\ 38 \end{array}$$

+50

7-20-70

50



+50

LT ✓
E Ditch
96

E
BIT
15 12

RT ✓
E Ditch
94

298

✓ E Ditch
+100 94

✓ ✓
BIT BIT
15 12

✓ E Ditch
+100 99

✓ P.P.
+92 29

+50

✓ E Ditch
+50 93

✓ ✓
BIT BIT
15 13

✓ E Ditch
+50 98

297

✓ End Low Area
+5 79
✓ E Ditch
+100 92

✓ ✓
BIT BIT
14 13

✓ AP
+93 59

✓ 3" Ash
+79 71

✓ 3" Ash
+79 91

✓ Low Area A
+84 60-108
✓ Low Area A
+61 59-106
✓ Below Area
+46 81

✓ E Ditch
+93 45

✓ 3" Ash
+57 73

✓ 36" R.C.P.
+57 47

+50

✓ E Ditch
+50 94

✓ ✓
BIT BIT
14 13

✓ 10' DIRT RD
+38 47

✓ P.P.
+139 39
✓ 24" RCP
+8 36-100
✓ 36" 12" Cotton
+23 77

✓ 36" RCP
+15 49

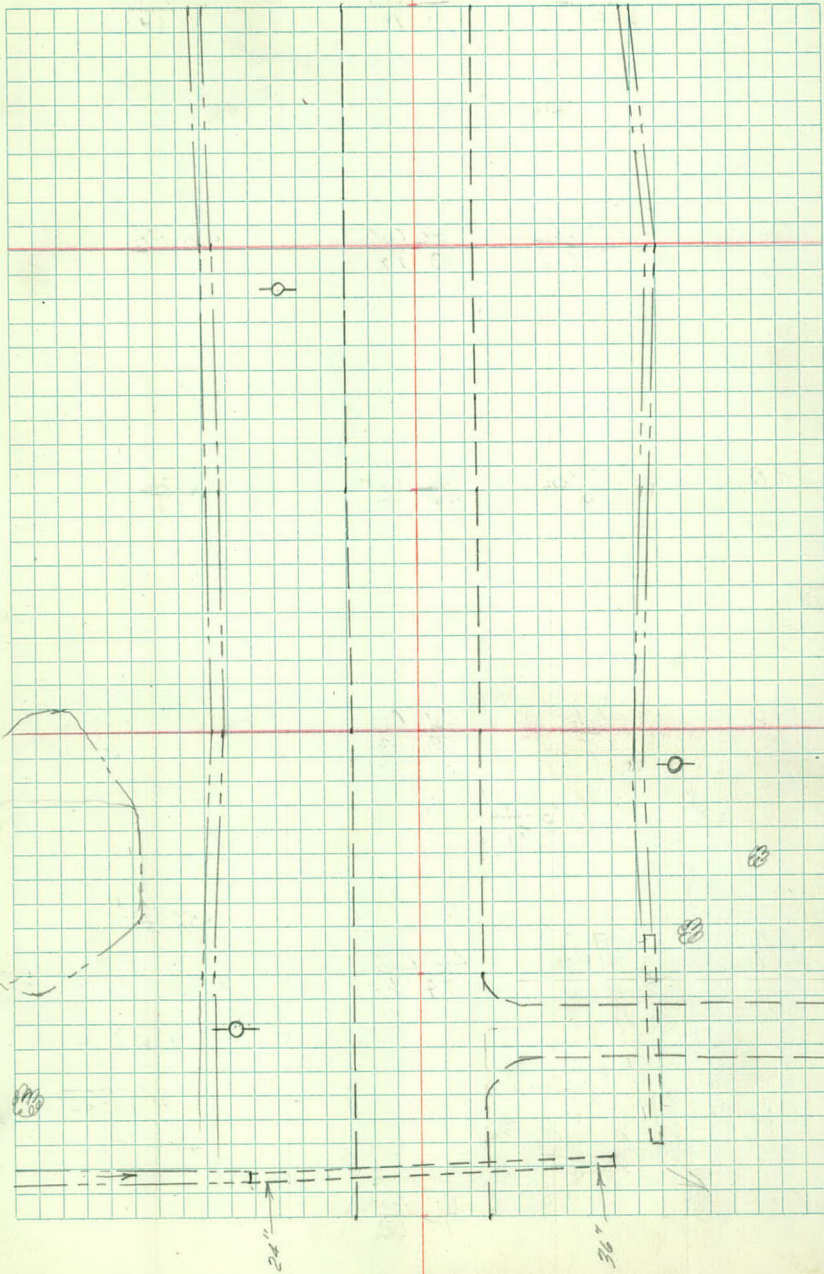
✓ 36" RCP
+11 90

296

✓ ✓
BIT BIT
14 14

7-20-70

51



RT

E

LT

301

$$\begin{array}{r} \text{E Ditch} \\ 91 \end{array}$$

$$\begin{array}{r} \text{Cox Conc} \\ 13 \quad 14 \end{array}$$

$$\begin{array}{r} \text{E Ditch} \\ 39 \end{array}$$

$$+83 \frac{PP}{42}$$

+50

$$\begin{array}{r} \text{E Ditch} \\ 41 \end{array}$$

$$\begin{array}{r} \text{Cox Conc} \\ 13 \quad 14 \end{array}$$

$$\begin{array}{r} \text{E Ditch} \\ 39 \end{array}$$

300

$$\begin{array}{r} \text{E Ditch} \\ 41 \end{array}$$

$$\begin{array}{r} \text{Cox Conc} \\ 13 \quad 14 \end{array}$$

$$\begin{array}{r} \text{E Ditch} \\ 38 \end{array}$$

+87 End Bit Overlay

+50

$$\begin{array}{r} \text{E Ditch} \\ 39 \end{array}$$

$$\begin{array}{r} \text{BIT BIT} \\ 13 \quad 14 \end{array}$$

$$\begin{array}{r} \text{E Ditch} \\ 42 \end{array}$$

$$+38 \frac{PP}{41}$$

299

$$+100 \text{ E Ditch} \\ 41$$

$$\begin{array}{r} \text{BIT BIT} \\ 14 \quad 13 \end{array}$$

$$+100 \text{ E Ditch} \\ 42$$

$$\downarrow \text{End Spill} \\ +76 \frac{15}{15}$$

$$\downarrow \text{Spillway} \\ +60 \frac{21-28}{21-28}$$

$$+56 \frac{B \text{ Spill}}{15-28}$$

+50

$$\begin{array}{r} \text{BIT BIT} \\ 15 \quad 12 \end{array}$$

$$+103 \frac{PP}{52}$$

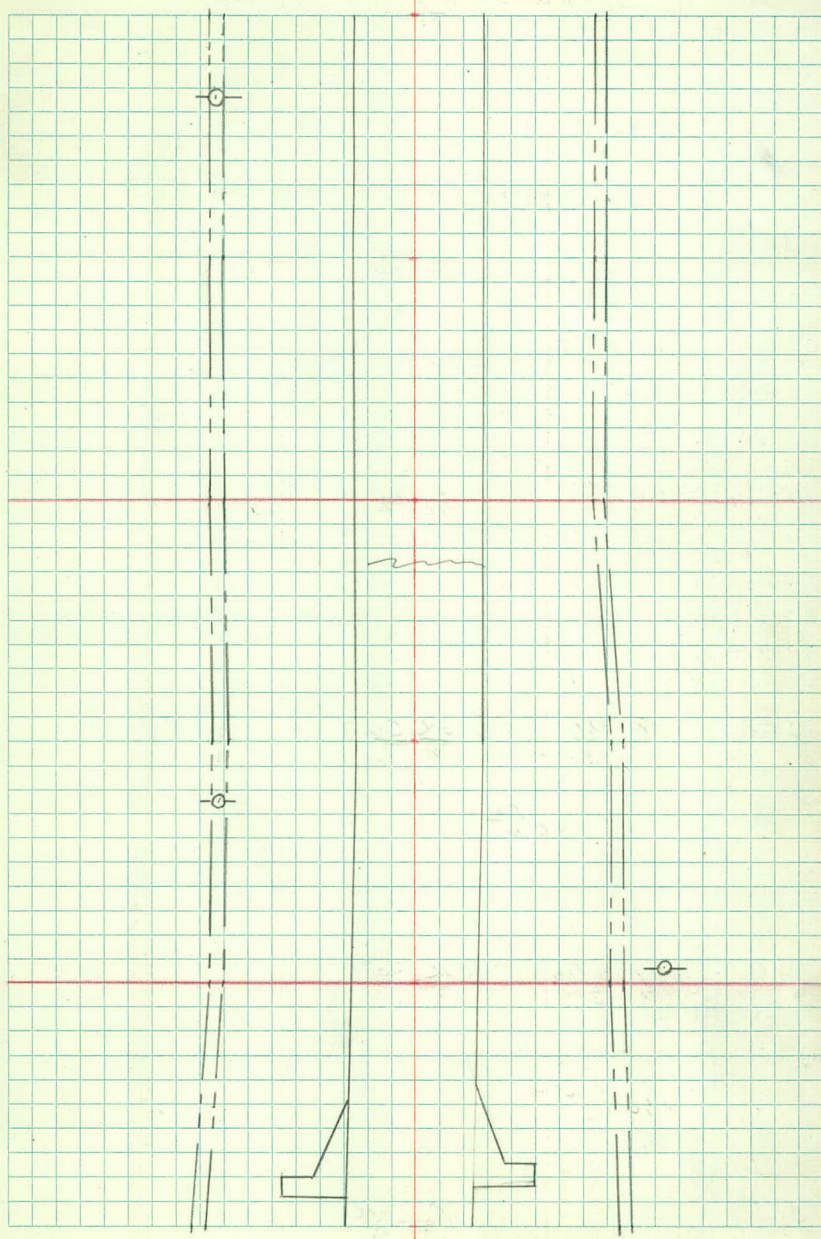
$$\downarrow \text{End Spill} \\ +78 \frac{12}{12}$$

$$\downarrow \text{Spillway} \\ +61 \frac{18-25}{18-25}$$

$$\downarrow \text{B Spill} \\ +58 \frac{12-25}{12-25}$$

7-20-70

52



RT
CT

E

RT RT

+50

L.A. Conc Conc
30-70 14 14

197 $\frac{1'' \text{ Pine}}{91}$ +20 $\frac{\text{End Spill.}}{14}$

Spillway
+03 20-26

B. Spill.

+00 14-26

303

L.A. Conc Conc
+00 30-62 14 14

+86 $\frac{\text{P.P.}}{93}$ $\frac{\text{Beg. Conc. A}}{36-58}$ 18 CMP

+72 $\frac{\text{Twins Oak}}{62}$ 778 92

+72 $\frac{12'' \text{ Oak}}{88}$ +74 $\frac{\text{Twins Oak}}{65}$ +57 $\frac{12'' \text{ Oak}}{89}$ +79 $\frac{12'' \text{ Oak}}{89}$ +57 $\frac{60 \text{ Beg. Drive}}{90}$ 776 92

12' Drive Conc Conc
+75 90 14 14

15' 72' Drive
+99 100

+00 $\frac{\text{G.R.}}{19}$ $\frac{\text{E. Ditch}}{33}$

+96 $\frac{\text{P.P.}}{56}$ +77 $\frac{12'' \text{ Oak}}{54}$

End Row 4-3" Cotton
+68 $\frac{\text{Willows}}{35}$ +68 92

+762 $\frac{\text{Beg. G.R.}}{19}$

$\frac{\text{E. Ditch}}{33}$

+50

Berry +32 $\frac{\text{P.P.}}{92}$ +32 $\frac{18 \text{ CMP}}{39}$
+14 93 8 +31 $\frac{1'' \text{ Oak}}{83}$
+09 $\frac{\text{Bury B.}}{95}$

$\frac{\text{E. Ditch}}{35}$

302

$\frac{\text{E. Ditch}}{38}$ Conc Conc
14 14

+99 $\frac{\text{Bury B.}}{99}$ +86 $\frac{\text{Bury B.}}{92}$

+78 $\frac{\text{Bury B.}}{99}$ +64 $\frac{\text{Bury Bush}}{90}$

Beg. Row - Willows
+99 33

+50

$\frac{\text{E. Ditch}}{39}$ Conc Conc
13 14

+52 $\frac{3'' \text{ Elm}}{98}$

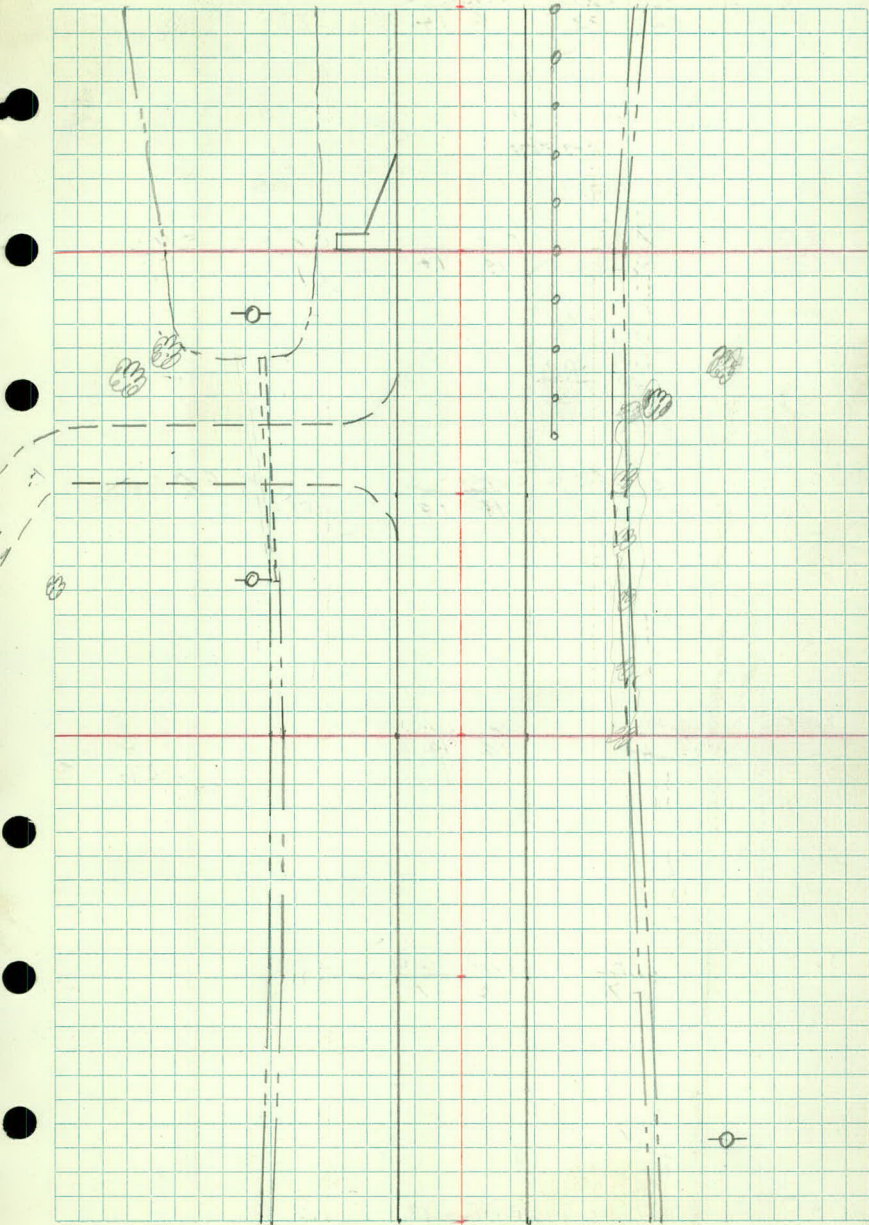
+17 $\frac{\text{P.P.}}{55}$

301

Conc Conc $\frac{\text{E. Ditch}}{40}$
13 14

7-20-70

53



At Lt

E

LT Rt

306

L.A.
28-98
Row Pine
77
Conc Conc
14 14

G.R.
19

+88 92 ^{8" Ash}
+59 82 ^{Row Pine}

+89 ^{Reg. Low Area}
34-54

150

L.A.
32-58
Conc Conc
14 14

G.R.
19

E.Ditch
38

+30 ^{P.P.}
32

305

L.A.
33-60
Conc Conc
14 14

G.R.
19

E.Ditch
38

+90 ^{10 Pine}
93

+50

L.A.
33-78
Conc Conc
14 14

G.R.
18
+95 33 ^{2" Cotton}

+92 32 ^{2" Cotton}

+38 32 ^{2" Cotton}
+36 32 ^{1" Cotton}

+29 ^{E.Ditch}
38

307

L.A.
31-71
Conc Conc
14 14

G.R.
19

E.Ditch
38

+80 ^{P.P.}
43

+64 ^{1" Pine}
92

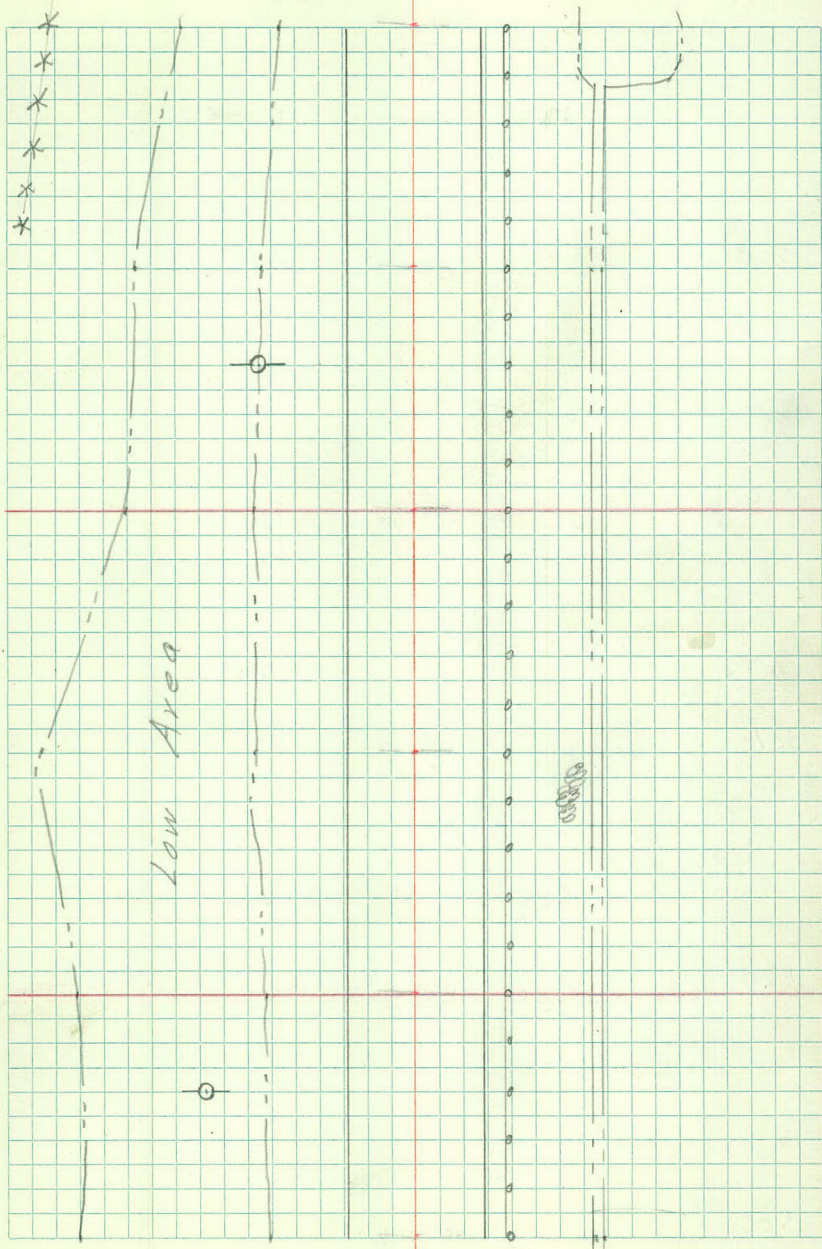
+50

Conc Conc
14 14

G.R.
19

E.Ditch
38

25



+50

RT LT

2

LT RT

End Row
Pine
52

CONC CONC
14 14

G.R.
18

West Edge
Hwy 10
BIT CONC
97 57

+21 PP
90

308

1" Row
Pine
57

CONC CONC
14 14

G.P.
19

West Edge
Hwy 10
BIT CONC
53 63

+50

Row
1" Pine
58

CONC CONC
14 14

G.R. metal
19
+93
End post
G.R.
19
+38

West Edge
Hwy 10
BIT CONC
61 71
End L.A.
+91 36

307

Row
Pine
61

CONC CONC
14 14

G.P. Posts
18

L.A.
29-94

West Edge
Hwy 10
BIT CONC
70 80

+79 PP
47

End L.A.
+79 29

+50

Row
Pine
73

L.A.
25-45

CONC CONC
14 14

G.R. Posts
19

L.A.
32-94

West Edge
Hwy 10
BIT CONC
82 92

Spill.
195 14

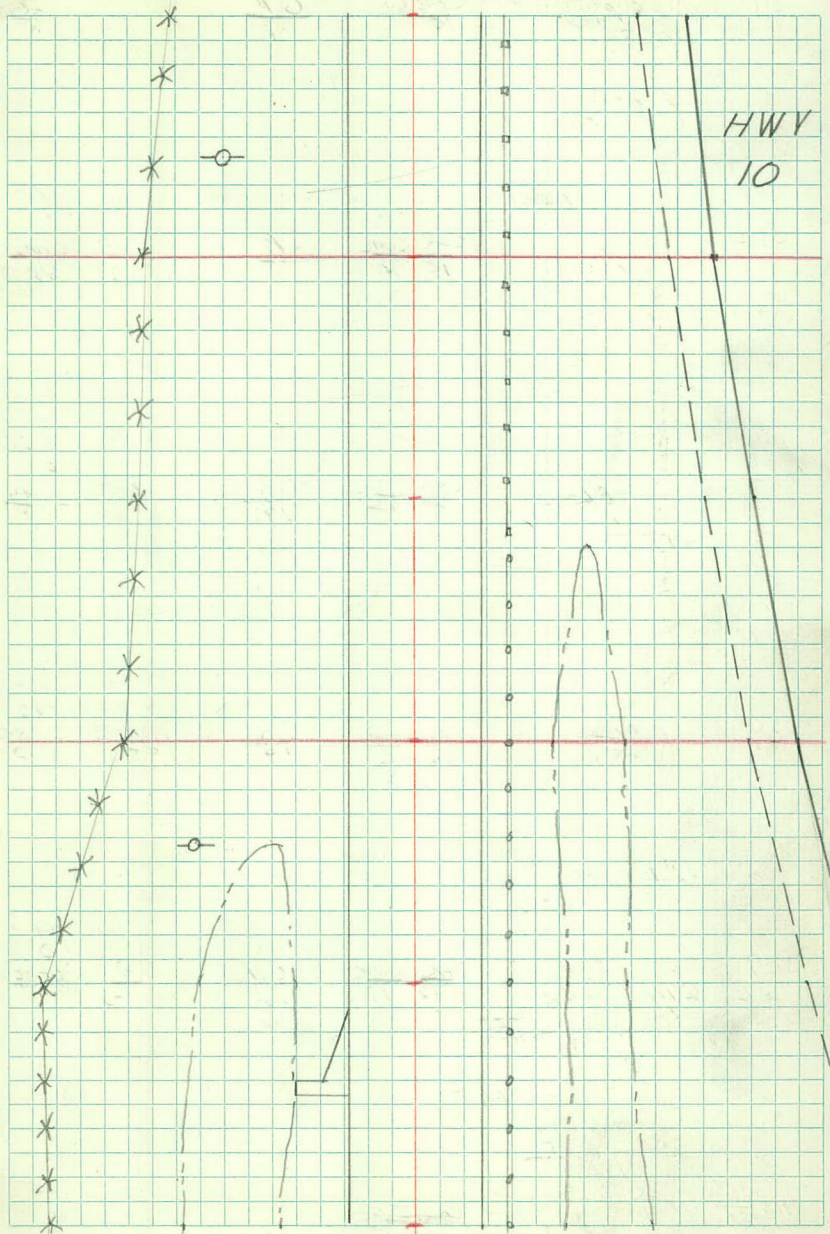
Spillway
+30 19-25

Br & Spill
+27 13-25

306

CONC CONC
19 14

Clear 7-20-70° 55°
Cool 72°



311

RT
LT

E

LT
R*West Edge
Hwy 109" Pine
+96 57Shrubs
+77 46Coac Coac
18 19G.R.
18BIT Coac
90 50S.E. Cor
9x5 Stone Box

+65 79

18" CMP
+69 26E 19'
Gravel
Grille
+51 32

+50

Coac Coac
14 14G.R.
18West Edge
Hwy 10BIT Coac
38 98Cor Grav.
+92 60Cor Grav.
+90 9418" CMP
+137 25Cor Grav.
+8 99Shrub
+28 96Cor Grav.
+6 62

310

AB End spill
14Loac Coac
14 15G.R.
19West Edge
Hwy 10BIT Coac
39 99Spill,
+124-20

P.P.

Beg Spill
14-24

+65 99

+91 1" Maple
62+61 1" Ash
68

+50

Row Pines
+50 Bushes
85Coac Coac
14 14G.R.
19West Edge
Hwy 10BIT Coac
40 50+20 Bay Row
Pines a Berry Bushes
782" Pine
+9 42

309

Coac Coac
19 14G.R.
18West Edge
Hwy 10BIT Coac
93 53

+91 24

E 116' Drive
+77 32Row 3" Pine
74-82

+91 23

16" CMP
+77 41-87

Row Pine

+91 100

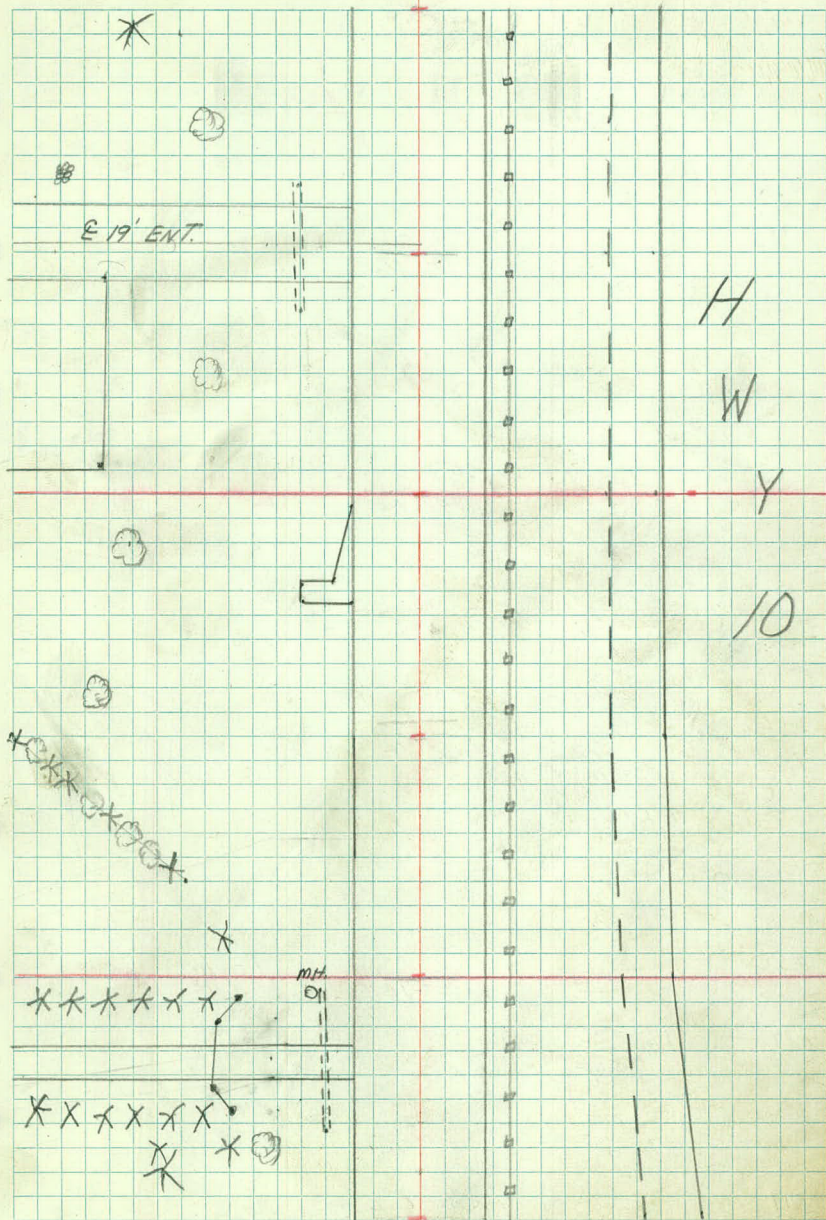
Drive 2" Pine
+65 513" Pine
+65 95Berry Bush
+66 33+67 16" CMP
202" Pine
+58 46

+122 37

16" CMP
+77 413" Pine
+77 39Berry Bush
+77 35

+50

Coac Coac
14 14



RT

E

LT

+50

$\frac{13' \text{ Pine Drive}}{31}$
 $+48$
 CONC CONC
 $\frac{14}{14}$

West Edge
 Hwy 10
 BIT CONC
 $\frac{61}{71}$

$\frac{12' \text{ CMP.}}{23}$
 $+38$

313

CONC CONC
 $\frac{14}{14}$

West Edge
 Hwy 10
 +00 BIT CONC
 $\frac{57}{67}$

+50

CONC CONC
 $\frac{14}{14}$

West Edge
 Hwy 10
 +50 BIT CONC
 $\frac{53}{63}$

$\frac{P.P.}{47}$
 $+37$

312

CONC CONC
 $\frac{14}{14}$

West Edge
 Hwy 10
 +00 BIT CONC
 $\frac{98}{58}$

$\frac{2' \text{ Pine}}{99}$ +89 $\frac{3' \text{ Pine}}{90}$ +83

$\frac{3' \text{ Pine}}{80}$ +82 $\frac{3' \text{ Pine}}{68}$ +81

$\frac{4' \text{ Pine}}{58}$ +80

$\frac{7' \text{ P.P.}}{70}$
 $+52$

+50

CONC CONC
 $\frac{14}{14}$

West Edge
 Hwy 10
 +50 BIT CONC
 $\frac{93}{53}$

$\frac{P.H.}{25}$
 $+28$

$\frac{4-5' \text{ Birch}}{95}$ +23 $\frac{3' \text{ Pine}}{69}$ +16

$\frac{P.P.}{46}$
 $+10$

$\frac{3' \text{ Pine}}{61}$
 $+7$

311

CONC CONC
 $\frac{14}{14}$

E 13' ENT

E 13' ENT

 ϕ

H

W

Y

10

X X X

m.H.
0X
X ϕ

RT,

E

LT,

316

Conc

14 14

B.T.

Conc.

71

81

+51 W.E 26' Arch Apron
65 C.M.

+50

+46 $\frac{PP}{46}$ +30 $\frac{12' C.M.P.}{27}$ +40 $\frac{16' P}{59}$

Flower

Pot

+27 $\frac{38}{38}$ +31 $\frac{NH}{24}$

E 12' B.T. 12" x 30' CM

+17 $\frac{Drive}{31}$ 28

Flow.

Pot

+9 $\frac{39}{39}$

+11 R.T. Drive

315

+00 $\frac{12' C.M.P.}{28}$

Conc

Conc

14

14

W. Edge

Hwy 10

B.T.

Conc

70

80

+65 $\frac{8' Pile}{56}$

W. Edge

Hwy 10

+50

Conc

Conc

14

14

+50

B.T.

Conc

67

77

+05 $\frac{27' Cott.}{56}$

W. Edge

Hwy 10

314

Conc

Conc

14

14

+00

B.T.

Conc

68

74

+88 R.T. to Drive

+79 $\frac{PP}{45}$ +69 $\frac{12' C.M.P.}{23}$

+50

Conc

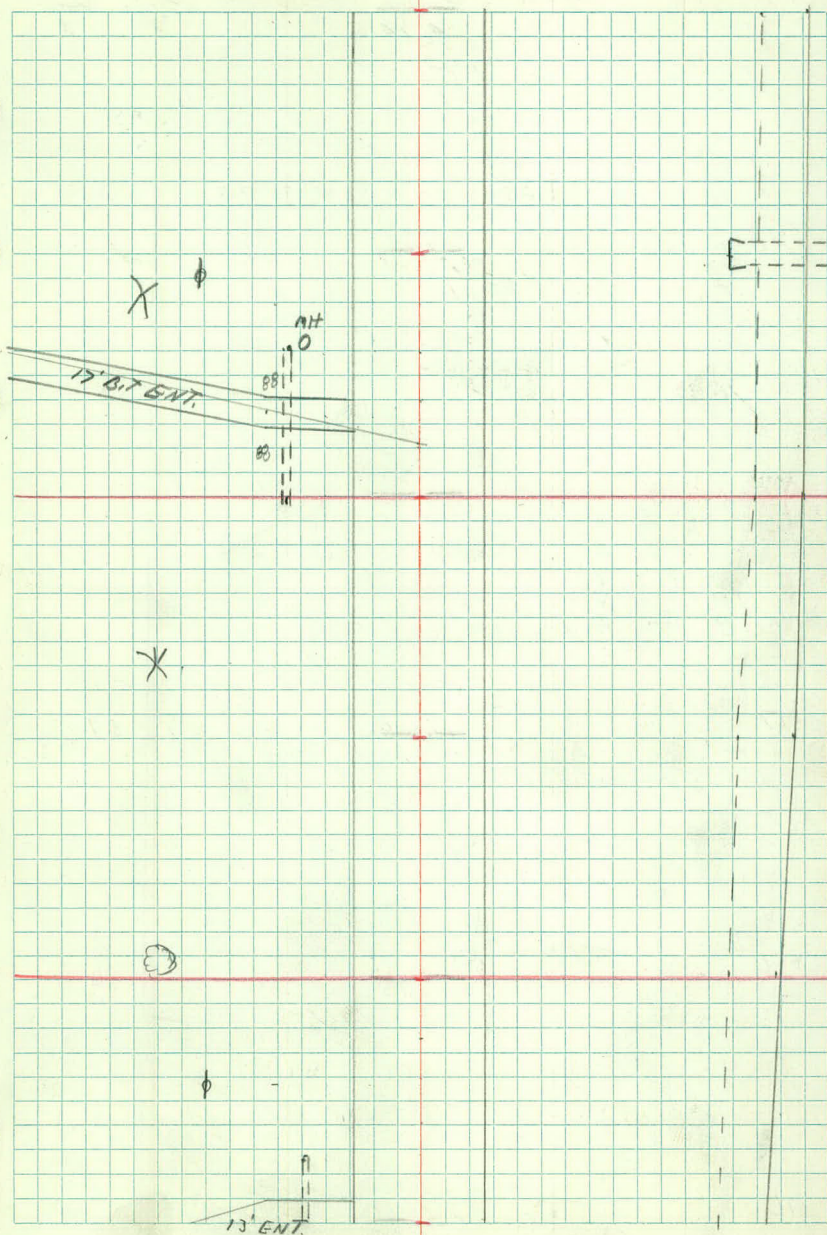
Conc

14

14

7-20-1970

58



RT

E

LT

+50

+37 $\frac{1''P}{61}$ +04 SEC. Ho
120+17 $\frac{2}{19' Ent}$ $\frac{18'' \times 29' CM}{C. Rock}$ 29

318

+88 $\frac{P. Bush}{47}$ +90 $\frac{Conc}{14}$ $\frac{3''P}{61}$ 74GR
19Bit Conc
67 77+83 $\frac{P. Bush}{42}$ +63 $\frac{NE Cor. Ho}{120}$ $\frac{Par. to Rd.}{47}$ +85 Bulber+68 $\frac{10'' W. Birch}{92}$

+50

+57 $\frac{B.G. Rail}{19}$ +25 $\frac{8'' Basswood}{85}$ +08 $\frac{2 8' Ent}{Dirt}$

317

+92 $\frac{PP}{47}$ Conc.
14 13Bit Conc
70 80+88 $\frac{8'' Flow Almond}{86}$ +75 $\frac{18''P}{61}$

+50

316

Conc
14 14Bit Conc
71 81

7-20-1970

59

K

419' ENT.

K K

40' ENT

φ

K

H
W
Y
10

RT

E

LT

321

4' Spillway 19@13.5
+98 20-25

4' Spillway
20-25'

7-2" Cott
+98 79

+50

320

Conc	GR	Bit	Conc
13.5 13.5	19	56	66

PP
+71 45

+50

MH
+32 23

319

Begin Marsh
+00 ← 45

Conc.	GR	Bit	Conc
13.5 13.5	19	62	72

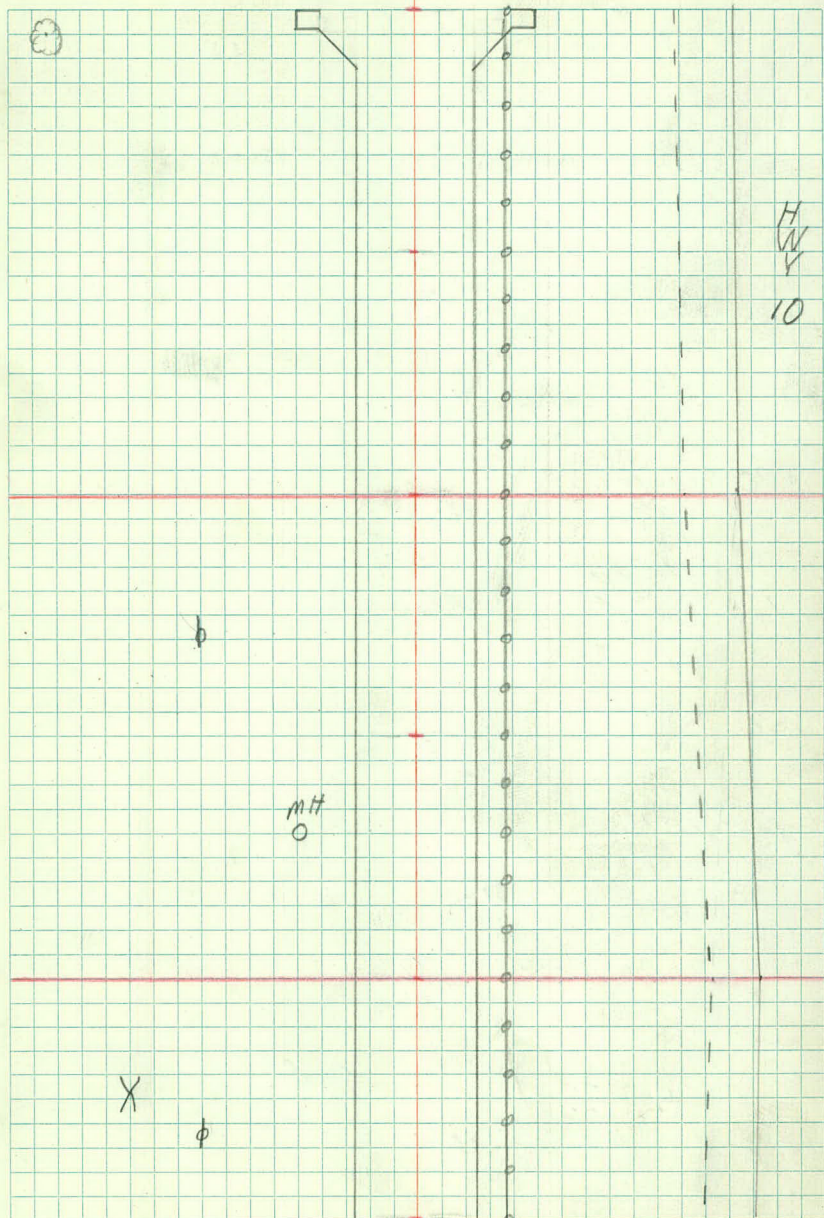
1" P
+78 60

+50

PP
+67 45

7-20, 1970

60



+50

R.T.

£

LT.

+33 MH
24

+26 Begin B 10-24
39

+13 £15 Con. Ent 15" X 33
47 37

+21 End Conc

+21 Begin B 9-24¹⁰
78.0

323

+100 Culv

Conc

Bit

Conc.

+99 Headwall
43-29

13.5 13.5

40

50

+92 Boulder
54

+98 Yard Lt.
57

+64 SE Cor. Ho.
119

+67 2" P
77

+61 PP
56

+53 Lilac
61

+39 1" P
90

+50 1" P
70

+39 3" Cedar
77

322

Conc
13.5 13.5

Bit
46

Conc
56

+77 SE Cor. Ho.
121

+88 £14 Conc Ent 15" X 43' CM
71 35

+50

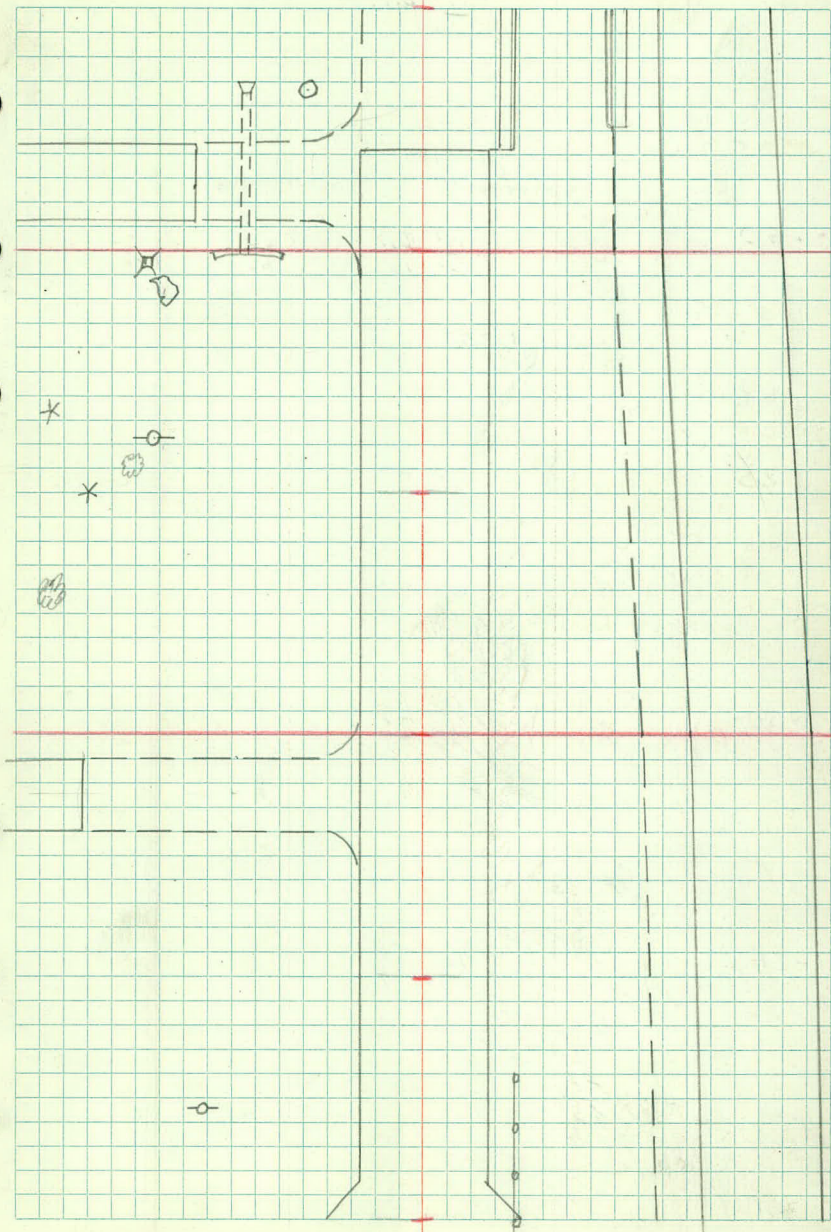
+23 PP
46

+30 E.G.R.
19

321

7-20-1970

61



RT

2

LT

326

Bit	Bit	Curb	Curb	Bit	Conc	Bit
12	16	18	31	33	41-65	60

+75 $\frac{\text{Bit}}{12}$ +66 PP
66

+50

Bit	Bit	Curb	Curb	Bit	Conc	Bit
12	16	18	31	33	41-65	69

+25 $\frac{\text{Bit}}{12}$

From

325

Bit	B-9-24	Curb	Bit	Conc
15	15	28.5	31	39.5

+50

Bit	B-9-24	Curb	Bit	Conc
13.5	16.5	32	34	42

+41 $\frac{\text{PP}}{71}$ +03 $\frac{10" \text{ Maple}}{87}$

from

324

13.0	Curb	Curb	Bit	Conc
17.5	34	37	45	

+85 P. Bush

+85 $\frac{12" \text{ Elm}}{103}$ +94 $\frac{10" \text{ Elm}}{82}$

17.5

34

37

45

+76 $\frac{10" \text{ Maple}}{82}$ +75 $\frac{\text{SE Cor. Ho. #2477}}{121}$ +67 $\frac{\text{P. Bush}}{63}$ +95 $\frac{\text{E 10" Ext + 15" x 36" CM.}}{63}$

38 w Apron

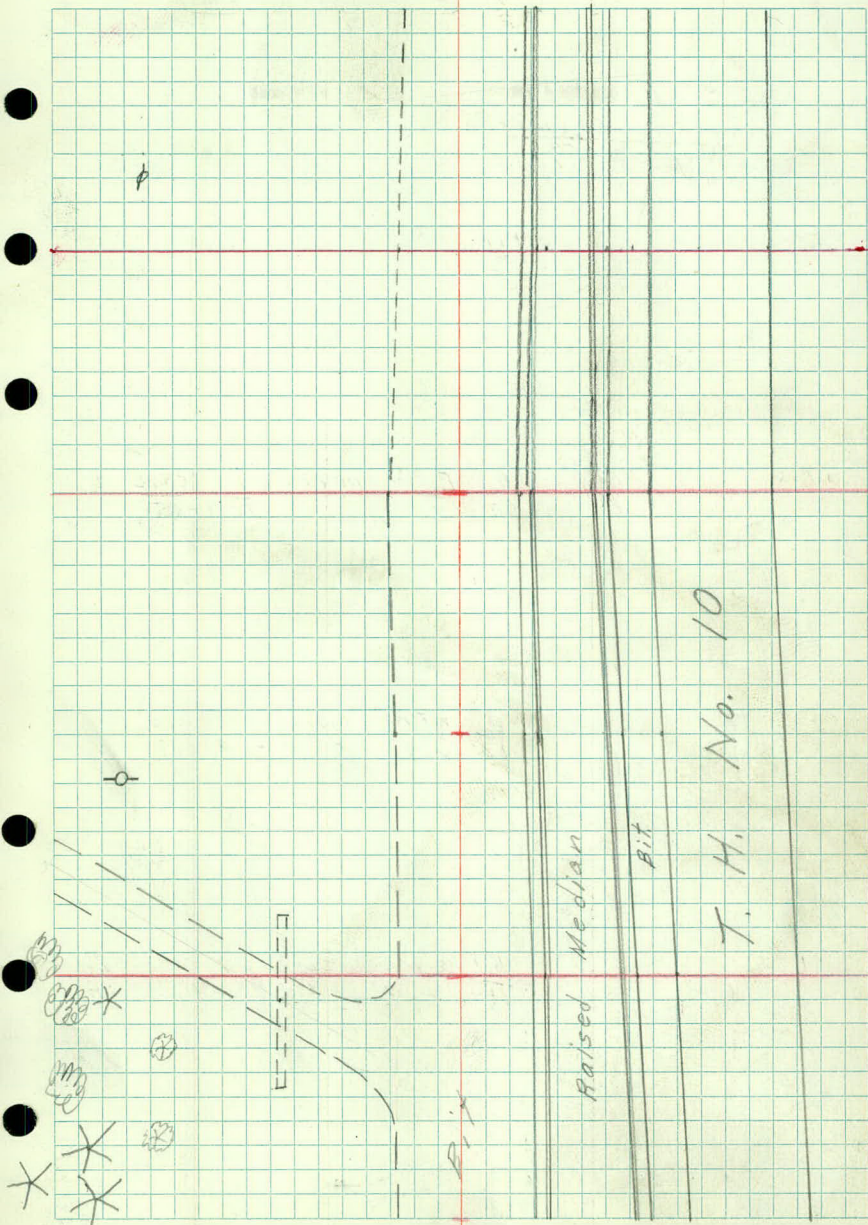
+57 $\frac{8" \text{ P}}{90}$ +64 $\frac{8" \text{ P}}{78}$ +53 $\frac{8" \text{ P}}{77}$ +73 $\frac{\text{RTire}}{\text{Ent}}$ +95 $\frac{4" \text{ P}}{93}$ +99 $\frac{10" \text{ Elm SE 10" Culv}}{100}$

+77

38

7-20-1970

62



<u>B.T</u>	<u>B.T</u>	<u>CORB</u>	<u>CORB</u>	<u>B.T CONC</u>	<u>B.T</u>
12	16	18	30	33 41-65	68

+22 36 RCP E. Apron
59

328

<u>B.T</u>	<u>B.T</u>	<u>CORB</u>	<u>CORB</u>	<u>B.T CONC</u>	<u>B.T</u>
12	16	18	31	33 41-65	68

+50

<u>B.T</u>	<u>B.T</u>	<u>CORB</u>	<u>CORB</u>	<u>B.T CONC</u>	<u>B.T</u>
12	16	18	31	33 41-65	68

327

<u>B.T</u>	<u>B.T</u>	<u>CORB</u>	<u>CORB</u>	<u>B.T CONC</u>	<u>B.T</u>
12	16	18	31	33 41-65	68

+84 PP
60

+50

<u>B.T</u>	<u>B.T</u>	<u>CORB</u>	<u>CORB</u>	<u>B.T CONC</u>	<u>B.T</u>
11	16	18	31	33 41-65	68

326

B.T
12

PK
CM
CP
BP

Aug 26 '70

63

36" B.C.P.

B.T

Raised Median

B.T

T.H. #10

331 $\frac{L+}{45}$
 width Lake Shore Drive = 18'

$\frac{\$}{12}$ $\frac{RT}{16}$ $\frac{CURB}{18}$ $\frac{CURB}{32}$ $\frac{BIT}{34}$ $\frac{CONC}{41-67}$ $\frac{BIT}{69}$

+78 $\frac{L.S. Drive}{45}$

+63 $\frac{B. Hedge}{59}$ +82 $\frac{E. Hedge}{61}$ RT=57

+57 $\frac{L.S. Drive}{41}$ +61 $\frac{E. APRON}{26}$ +62 $\frac{Row trees}{65}$

+50 +57 $\frac{ER LAKE Shore DR}{26}$

+43 $\frac{6" Maple}{78}$

+30 $\frac{ENT}{45}$ +17 $\frac{ENT}{25}$

+19 $\frac{ER Lake Shore Drive}{26}$ +17 $\frac{ENT}{96}$ $\frac{20' BIT ENT}{26}$

+09 $\frac{PP}{44}$

+14 $\frac{18" CHMP APRON}{26}$

+4 $\frac{8" Pine}{58}$ +7 $\frac{4" Pine}{56}$ +8

330 +00 $\frac{4" Pine}{52}$ $\frac{BIT}{12}$ $\frac{BIT}{16}$ $\frac{CURB}{18}$ $\frac{CURB}{31}$ $\frac{BIT}{34}$ $\frac{CONC}{41-66}$ $\frac{BIT}{69}$

+95 $\frac{10" Birch}{52}$

+59 $\frac{Flag Pole}{87}$

+50

+38 $\frac{10" Maple}{86}$

+15 $\frac{4" Pine}{66}$

329 +98 $\frac{4" Pine}{73}$ +98 $\frac{4" Pine}{82}$ $\frac{BIT}{12}$ $\frac{CURB}{16}$ $\frac{CURB}{18}$ $\frac{BIT}{31}$ $\frac{CONC}{35}$ $\frac{BIT}{41-65}$ $\frac{BIT}{68}$

+90 $\frac{8" Elm}{65}$

+91 $\frac{4" Pine}{78}$

+73 $\frac{5" Elm}{84}$

+62 $\frac{PP}{51}$

+64 $\frac{10" Elm}{73}$

+50

+55 $\frac{Twelve 6" Birch}{65}$

PK
CM
GP
RP

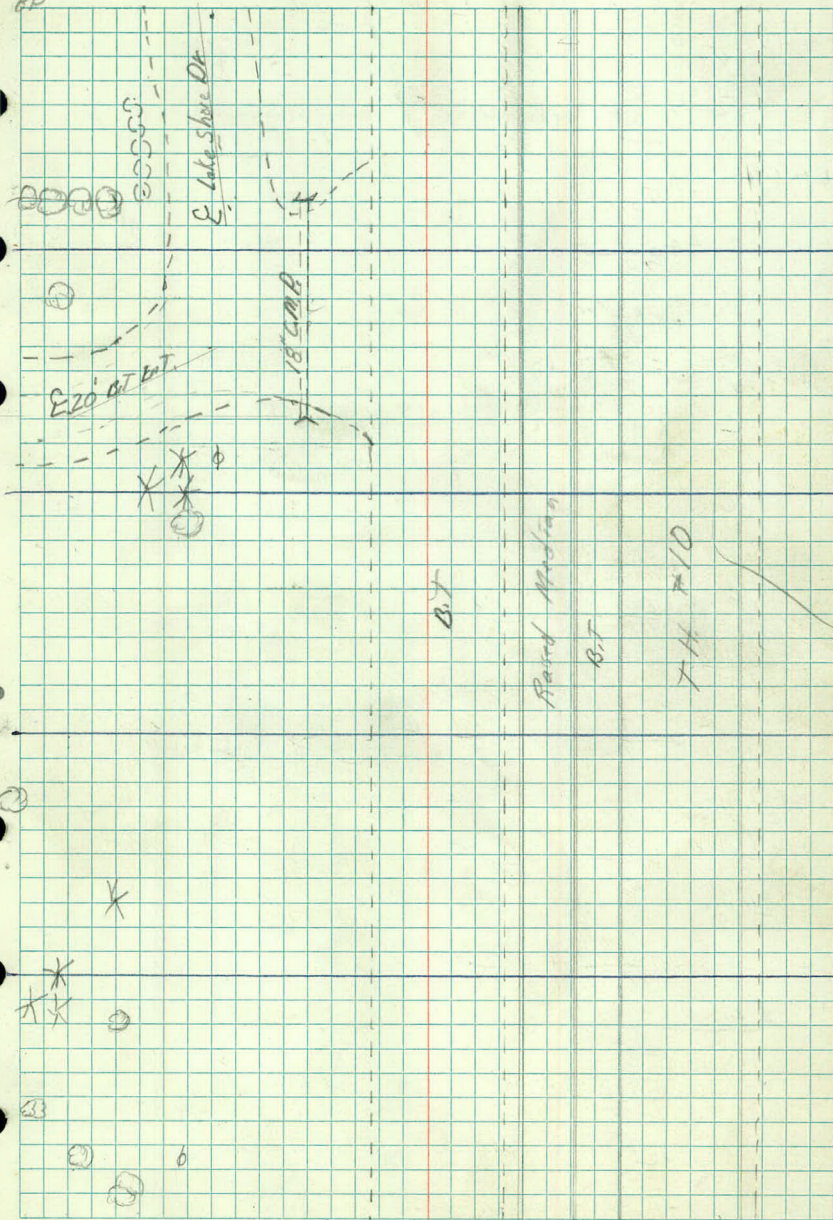
LT

Q

AUG 27 '70

64

Rt



LT & L.S. Drive $\frac{B.T}{12}$ $\frac{B.T}{12}$ $\frac{B.T}{61}$ RT

+44 $\frac{6'' \text{ Pine}}{48}$

+31 $\frac{8'' \text{ Pine}}{52}$ +33 $\frac{8'' \text{ Pine}}{62}$

+18 $\frac{E. Conc}{75}$

+17 $\frac{4'' \text{ Pine}}{59}$ +11 $\frac{2'' \text{ Pine}}{48}$

333 $\frac{\text{L.S. Drive}}{78}$

$\frac{B.T}{13}$ $\frac{B.T}{46}$ $\frac{conc}{56-81}$ $\frac{B.T}{85}$

+97 $\frac{4'' \text{ Pine}}{54}$

+73 $\frac{PP}{34}$ +80 $\frac{3'' \text{ Pine}}{46}$ +80 $\frac{\text{L.S. Drive}}{72}$

+59 $\frac{3'' \text{ Pine}}{53}$ +63 $\frac{3'' \text{ Pine}}{39}$

+50 $\frac{B.T}{13}$ $\frac{B.T}{37}$ $\frac{conc}{47}$

+52 $\frac{\text{L.S. Drive}}{70}$

+25 $\frac{L. Lac}{78}$ +36 $\frac{3'' \text{ Hedge}}{87}$

$\frac{PP}{82}$ +13 $\frac{\text{L.S. Drive}}{61}$ +19 $\frac{3'' \text{ Pine}}{36}$

+06 $\frac{E. Hedge}{78}$ +09 $\frac{3'' \text{ Pine}}{79}$

332 $\frac{\text{L.S. Drive}}{57}$

$\frac{B.T}{12}$ $\frac{B.T}{18}$ $\frac{B.T}{18}$ $\frac{conc}{42-67}$ $\frac{B.T}{69}$
+95 $\frac{E. CURB}{18}$ +25 $\frac{E. CURB}{34}$

+81 $\frac{\text{L.S. Drive}}{52}$

+74 $\frac{6'' Elm}{72}$ +74 $\frac{\text{Hedge}}{72}$ +81 $\frac{PP}{38}$

+34 $\frac{B. Hedge}{68}$

+50 $\frac{MH}{54}$ +51 $\frac{E. Hedge}{67}$ +52 $\frac{8'' Elm}{67}$

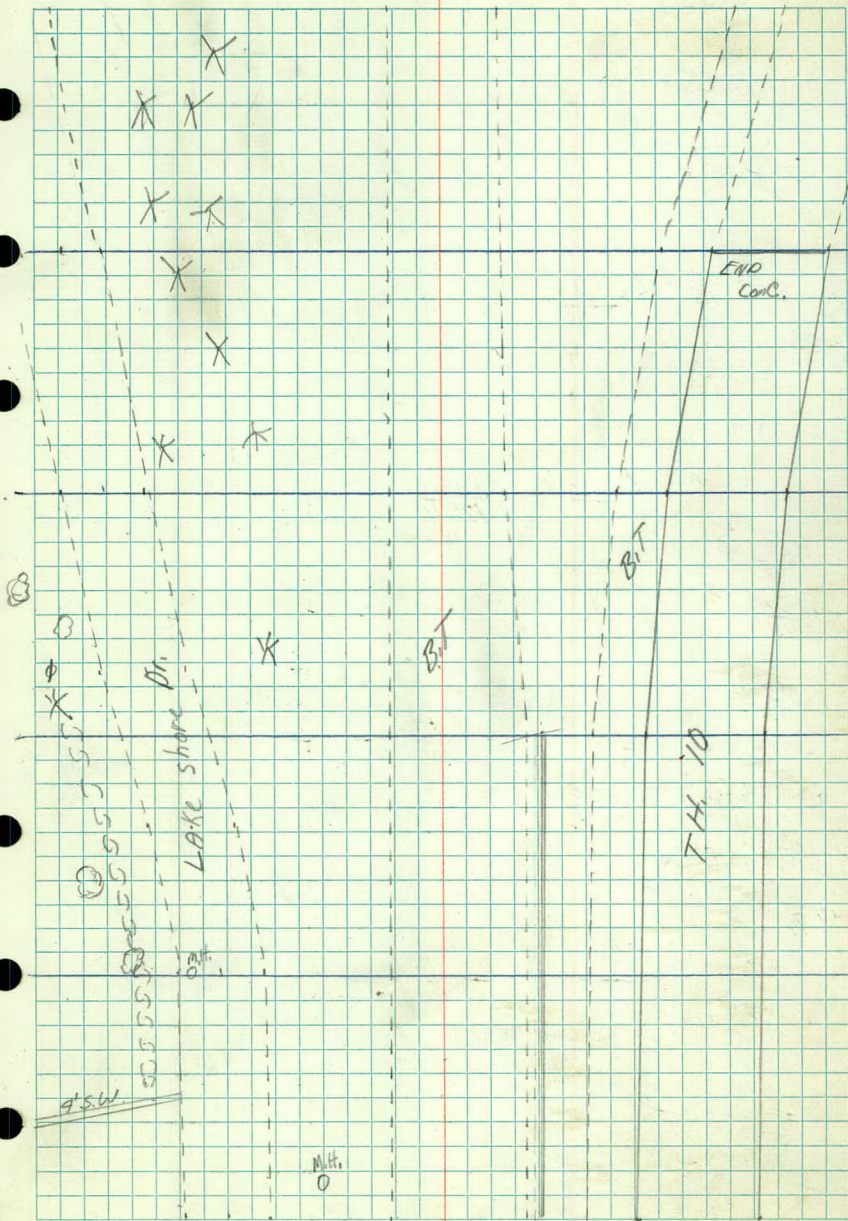
+50 $\frac{\text{L.S. Drive}}{46}$

RT To Walk = 33

+24 $\frac{4'' \text{ side walk}}{61}$ +28 $\frac{B. Hedge}{62}$

+19 $\frac{6'' Elm}{62}$ +9 $\frac{MH}{26}$

331 +4 $\frac{\text{L.S. Drive}}{54}$



336 £ L.S. Drive
65

On B.T
9 15

B.T
59-93
£0.1496

+74 PP
38

+50 6" Pine £ L.S. Drive
48 78

B.T B.T
11 13

B.T
69

+28 6" Pine
48

+08 6" Pine
52

335 +00 6" Pine £ L.S. Drive
40 81

B.T B.T
12 11

B.T
83

+90 6" Pine
55

+80 6" Pine
42

+72 CONTICOL BOX B.T
51 89

+61 GP B.T
44 89

+69 6" Pine
58

+48 PP B.T
43 90

+54 6" Pine +60 6" Pine
60 93

+35 £ L.S. Drive +45 6" Pine
89 96

+18 6" Pine +25 6" Pine
67 99

+4 6" Pine
49

334 £ L.S. Drive

B.T B.T B.T
11 13 79 - 00

+90 6" Pine +94 6" Pine
39 88

+79 6" Pine +71 6" Pine
52 69

+60 6" Pine +69 6" Pine
50 40
+54 6" Pine
65

LAKE SHORE DRIVE

p

B.T

□

o

d

B.I.T
52-76

+33 $\frac{5W}{54}$ cor wall

+16 $\frac{14'CLM}{58}$ +33 $\frac{NW}{54}$ cor wall

+21 $\frac{18'ELM}{3}$ +14 $\frac{SE}{55}$ cor wall

338

+10 $\frac{NE}{5}$ cor wall

+86 $\frac{EDINTENT}{22}$ 22'

+78 $\frac{NECOR}{69}$ GARAGE

+67 $\frac{18'ELM}{23}$ +75 $\frac{18'CMP}{14}$

+54 $\frac{NW}{58}$ cor house

+50 $\frac{MH}{04}$

+63 $\frac{B.I.T}{0}$

+72 $\frac{B.I.T}{7}$

+29 $\frac{NE}{59}$ cor house

+30 $\frac{3'PIPE}{56}$

+21 $\frac{3'PIPE}{48}$

+12 $\frac{10'ELM}{77}$

+12 $\frac{10'ELM}{23}$

+12 $\frac{10'ELM}{58}$

$\frac{B.I.T}{7}$

$\frac{B.I.T}{16}$

$\frac{B.I.T}{53-87}$

+90 $\frac{8'APPLE}{36}$

+91 $\frac{8'APPLE}{50}$

+78 $\frac{1'APPLE}{37}$

+65 $\frac{18'CM}{20}$ +76 $\frac{10'APPLE}{49}$

+50

+46 $\frac{ELV.Drive}{19}$

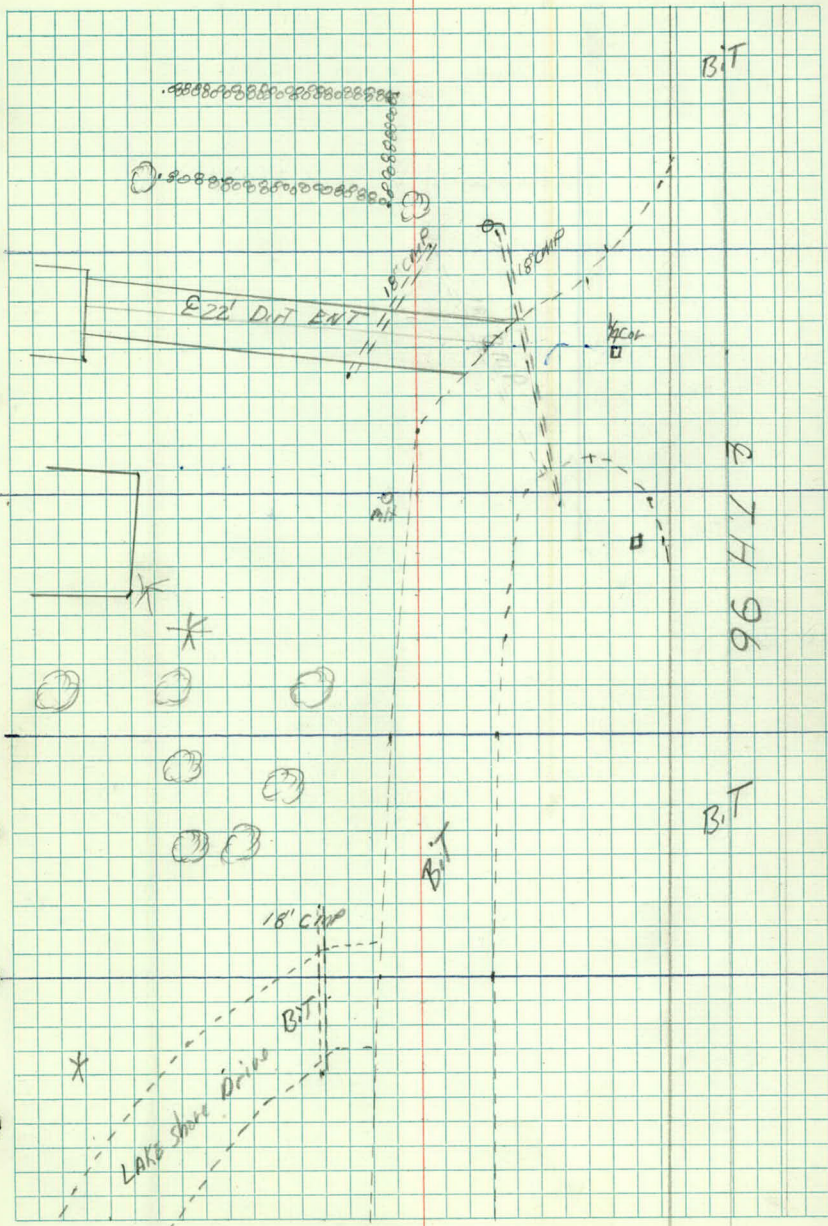
$\frac{B.I.T}{9}$ $\frac{B.I.T}{15}$

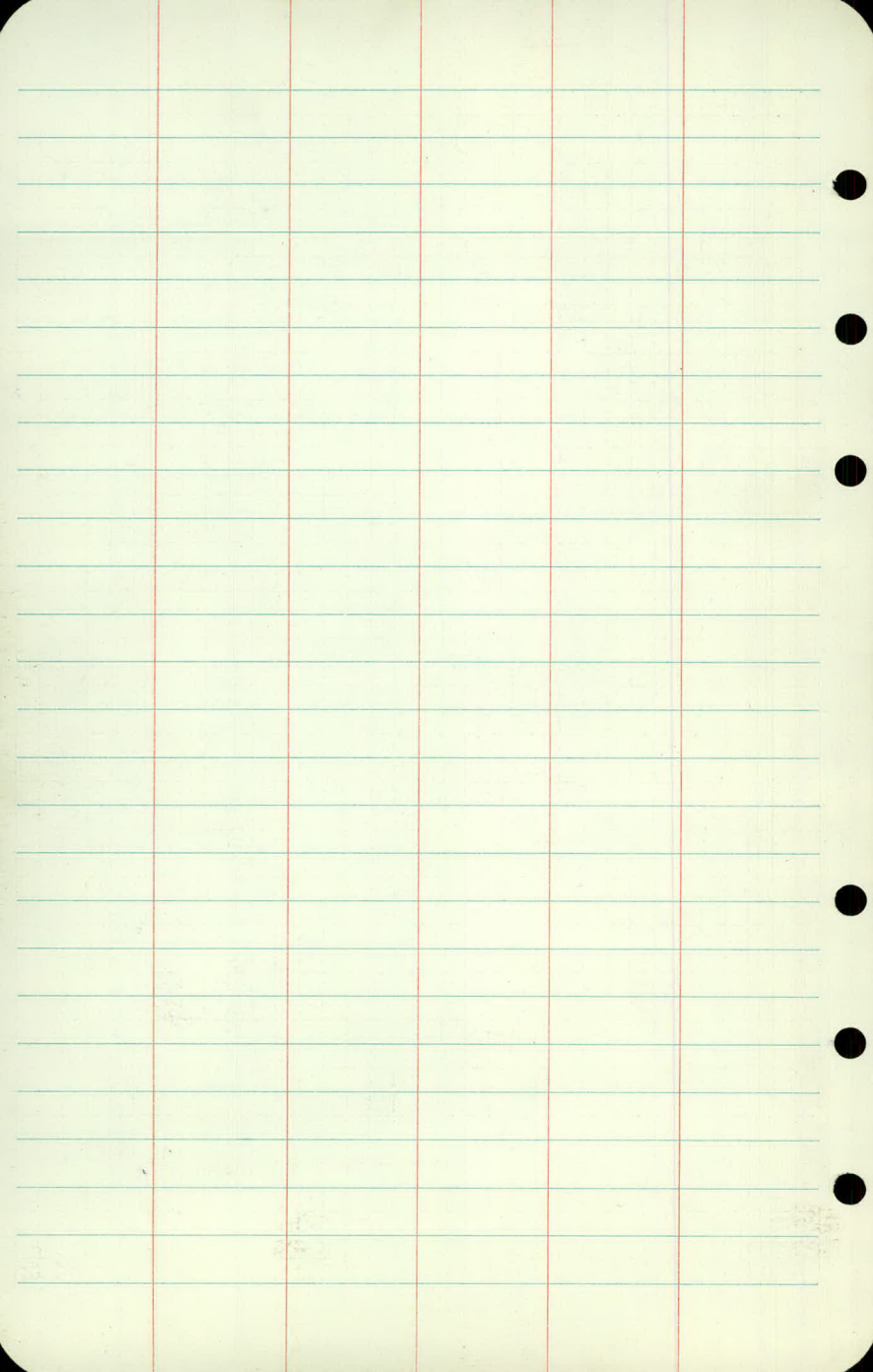
$\frac{B.I.T}{54-88}$

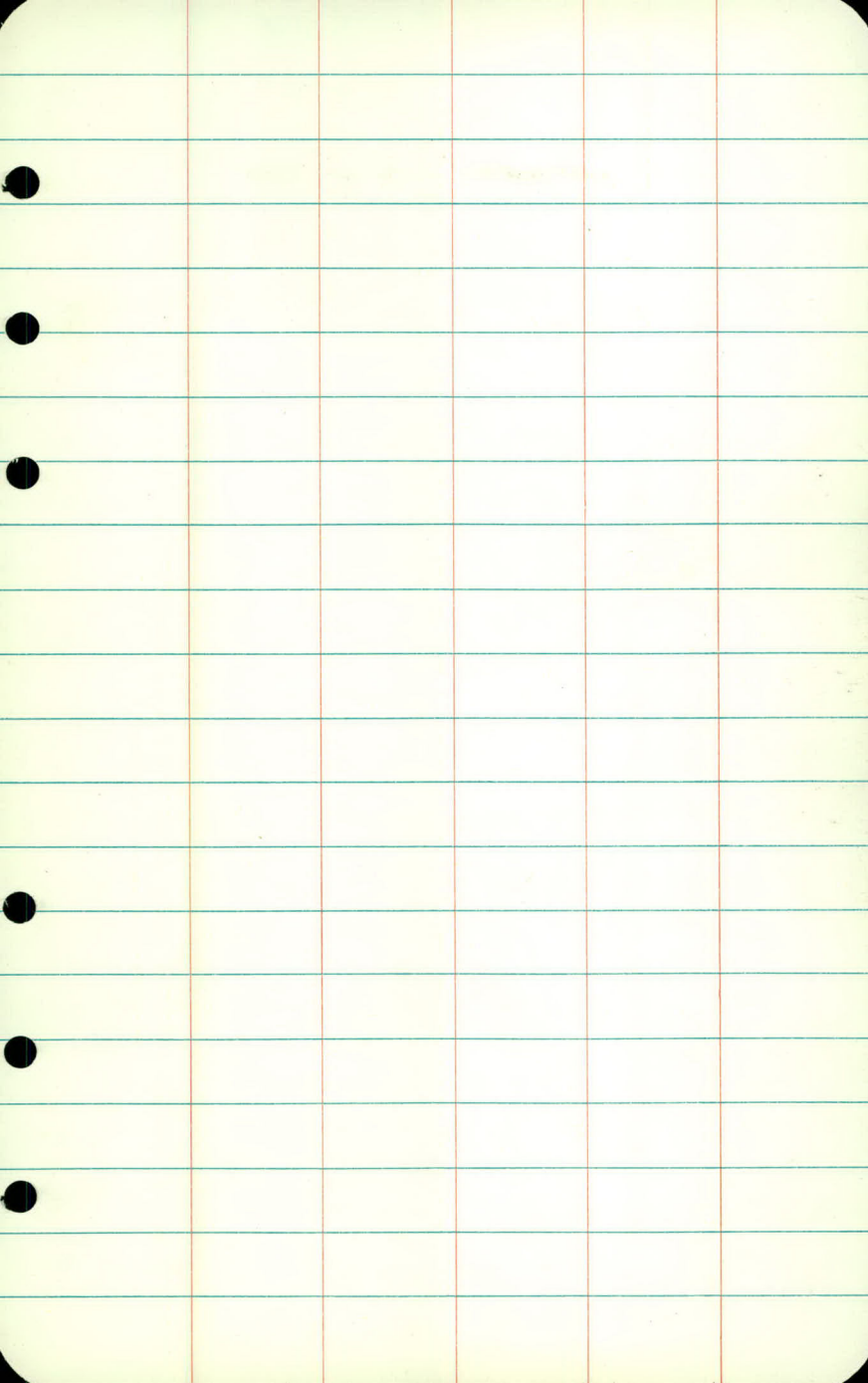
+32 $\frac{ELV.Drive}{42}$ +31 $\frac{18'CMP}{21}$ +32 $\frac{Pipe 2"}{71}$

336

EXTENDED TANGENT







Begin Curb	STA	on the	To STA	End of CURB
------------	-----	--------	--------	-------------

217	217+25	RT	229+25	
-----	--------	----	--------	--

	223+05	LT	238+41	
--	--------	----	--------	--

	217+62	LT	218+64	
--	--------	----	--------	--

	316+47	RT	323+21	
--	--------	----	--------	--

	316+47	LT	323+21	
--	--------	----	--------	--

PK
BP

Sept 18 1970
Clear

1

Total Linear St

Notes:

1200

1398 ✓

Begin Conc Pavement Co RDE

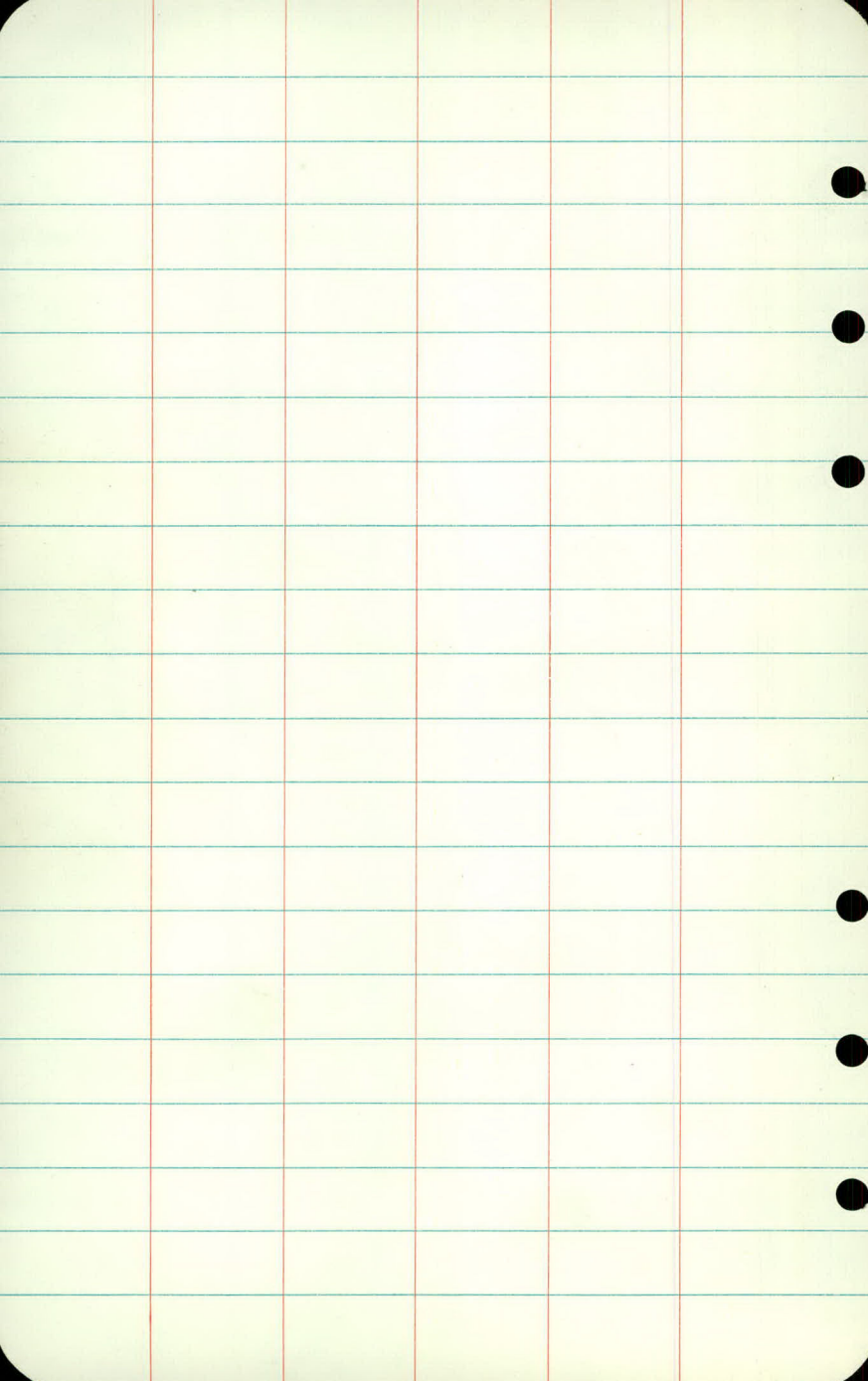
1535

102

674

674

4383



Bridge Elev.

&

RR Track Profile

OLD TH 10

STA 227+75 ±

STA	+	Δ	-	Elev
BM	8.83	906.61		897.78 9.83
TP	12.13	918.04 3.9	0.70	905.91 12.3
TP	5.82	920.47	3.39	914.65 57.82
A	920.47 4.44 916.03		3.47	917.00
B	14.65 3.96 18.61 2.60 16.01		7.09	913.38
C			7.31	913.16
D			3.95	916.52
+E			4.44	916.03
+25			3.30	917.17
+50			3.28	917.19
+75			3.16	917.31

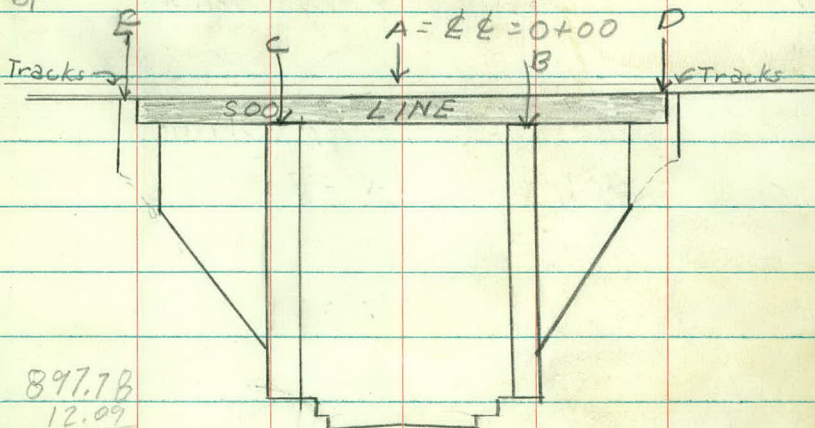
LT

E

RT

June 30 1970

PK
CM
CP
BP

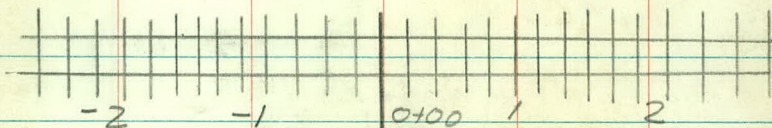


897.78
12.09
909.87
- 4.10
905.77
10.20
915.97
1.32
914.65

SEE NEXT PAGE

E OLD 10

228



227

STA + π - E/ev

920.47

1+00 2.97 917.50

+25 2.79 917.68

+50 2.66 917.81

+75 2.40 918.07

2+00 2.19 918.28

+25 1.98 918.49

+50 1.80 918.67

0-25 3.60 916.87

-50 3.81 916.66

Lt

- E

Rt

A = Top Tracks & E

B = Top East Piller assembly

C = Top W Piller assembly

D = Top East EMBUCKMENT

E = Top W EMBUCKMENT

Note: All shots Taken on top RR tracks

STA	+	π	-	Elev
		920.47		
		1483		
-75		5.64	3.82	916.65
		1.8		
-1+00			3.89	916.58
-25			3.95	916.52
-50			3.93	916.54
-75			3.92	916.55
-2+00			3.91	916.56
-25			3.84	916.63
-50			3.83	916.64
BM			5.59	914.08 (914.03)

Lt

£

RT

22 27

22 47

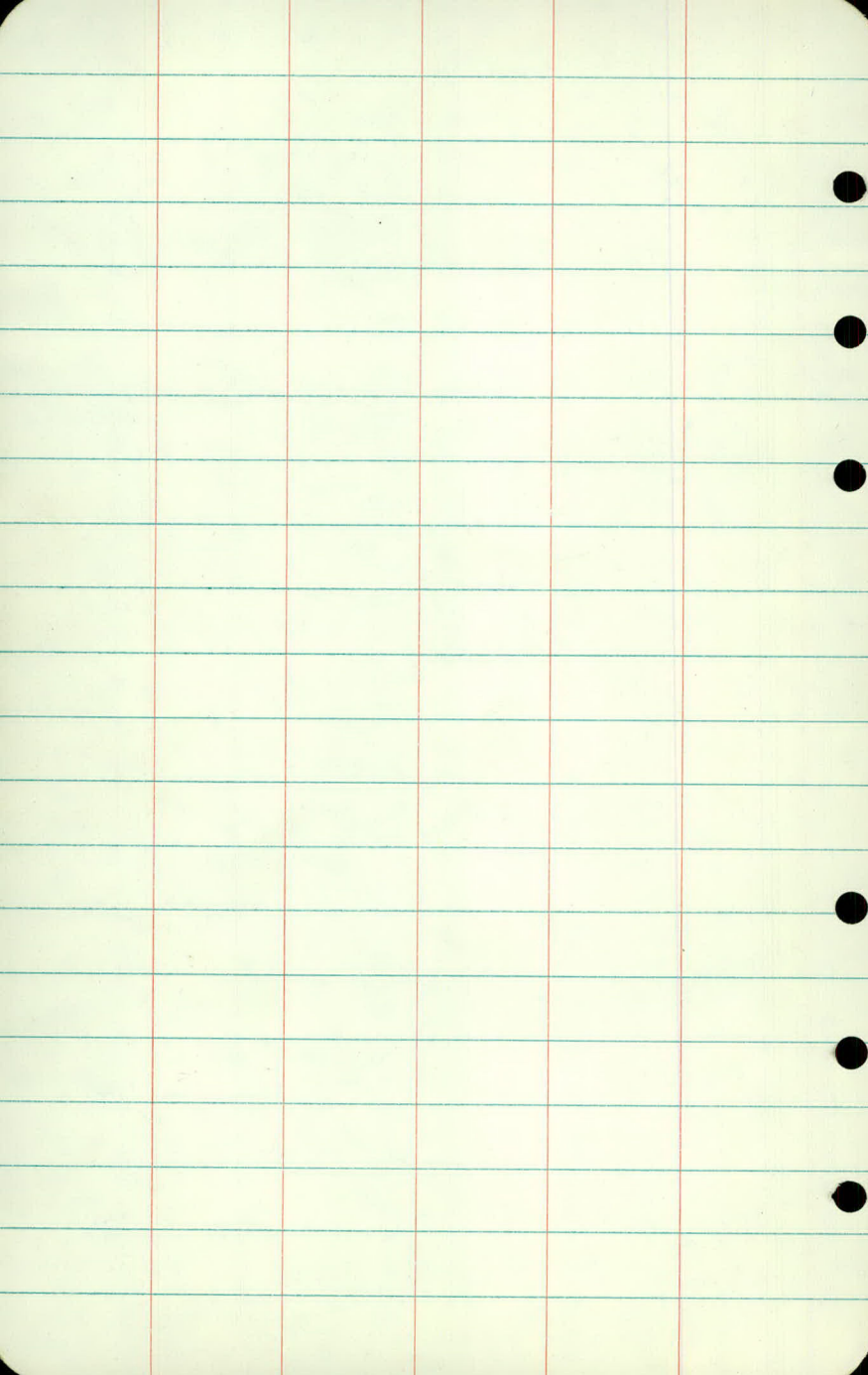
5 16

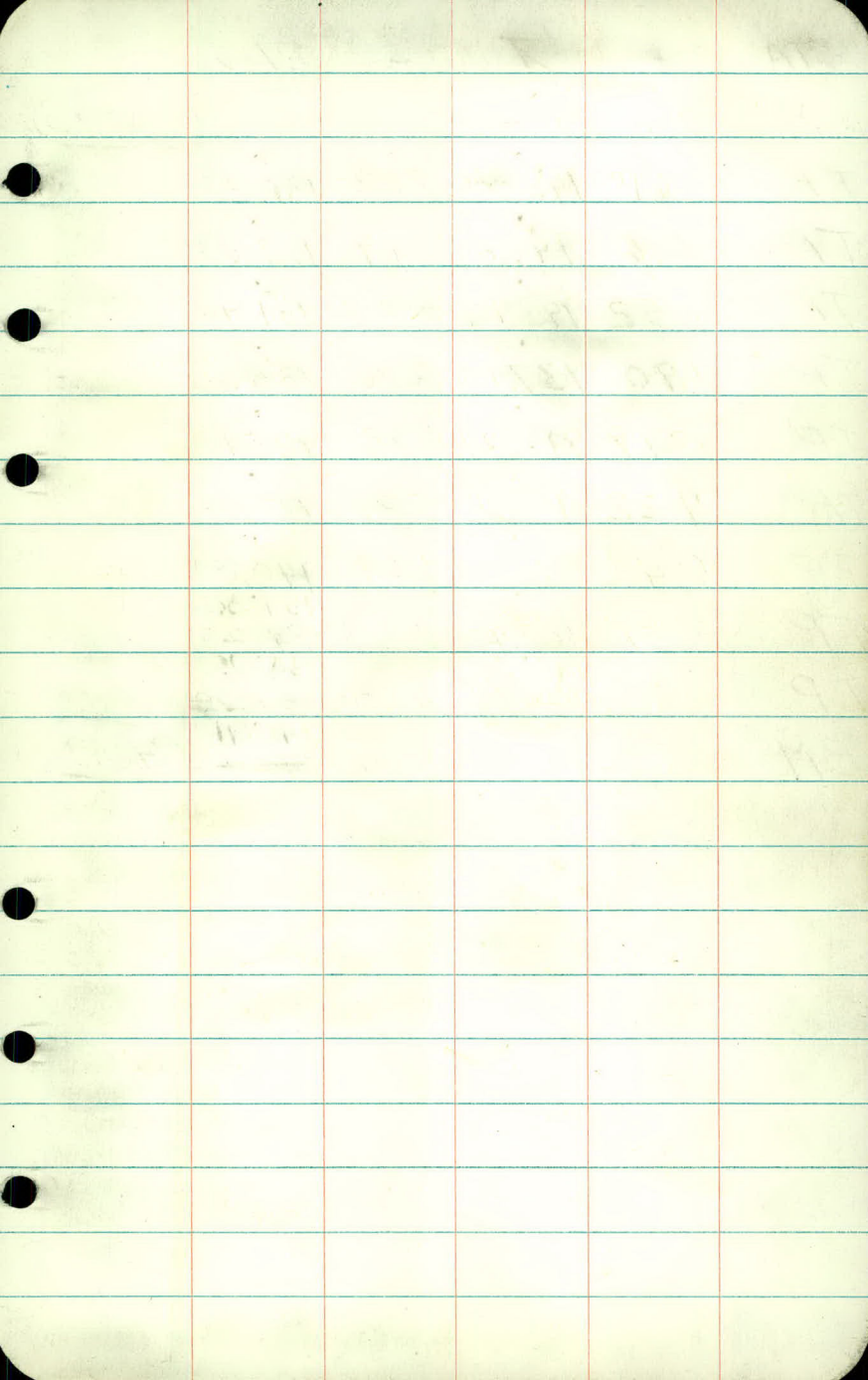
5 16

19 28

19 28

Top West Edge MH STA 219+35 RT
(Long Shot 900+ feet)





STA	+	Σ	-	Elev
BM	2.52	943.42		940.90
TP	6.61	942.84	7.19	936.23
TP	4.16	946.81	0.19	942.65
TP	1.52	943.46	4.87	941.94
TP	1.90	937.10	8.26	935.20
TP	13.19	938.37	11.92	925.18
TP	11.22	943.70	5.89	932.48
TP	6.42	946.43	3.69	940.01
TP	3.57	942.92	7.07	939.35
TP	8.82	943.54	8.20	934.72
BM			2.64	940.90

PK
CM
CP
BP

June 26 '70

Brass Disk SE Cor Wingwall Co Rd E & TH 51

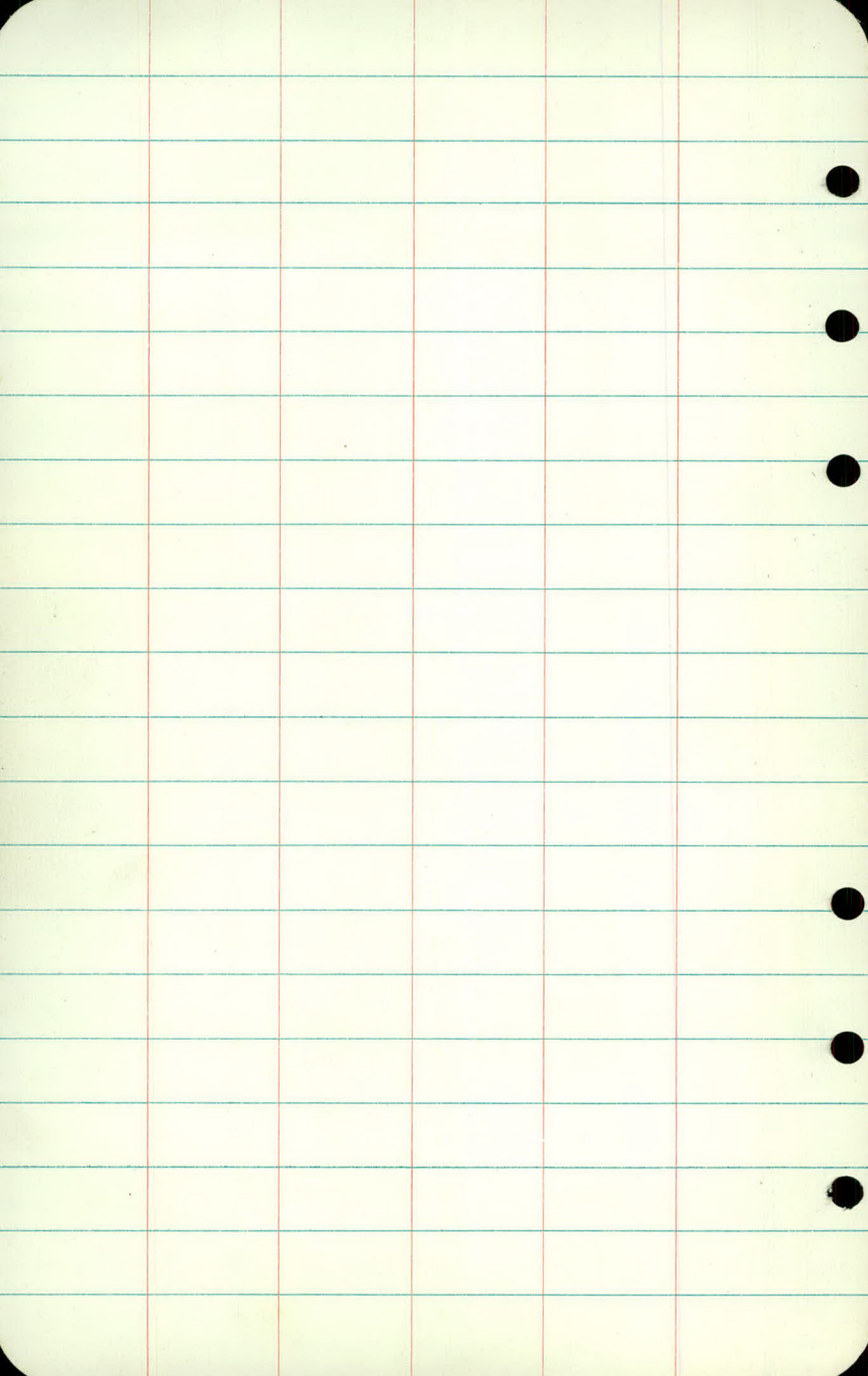
Top Hyd SW cor Co Rd E & TH 51

Top Hyd across from 1464 Co Rd E

Top Hyd NE Cor Co Rd E & Pascal

Top Hyd By 1467 Co Rd E

Spike in Arclight Pole SE cor E & TH 51



L+

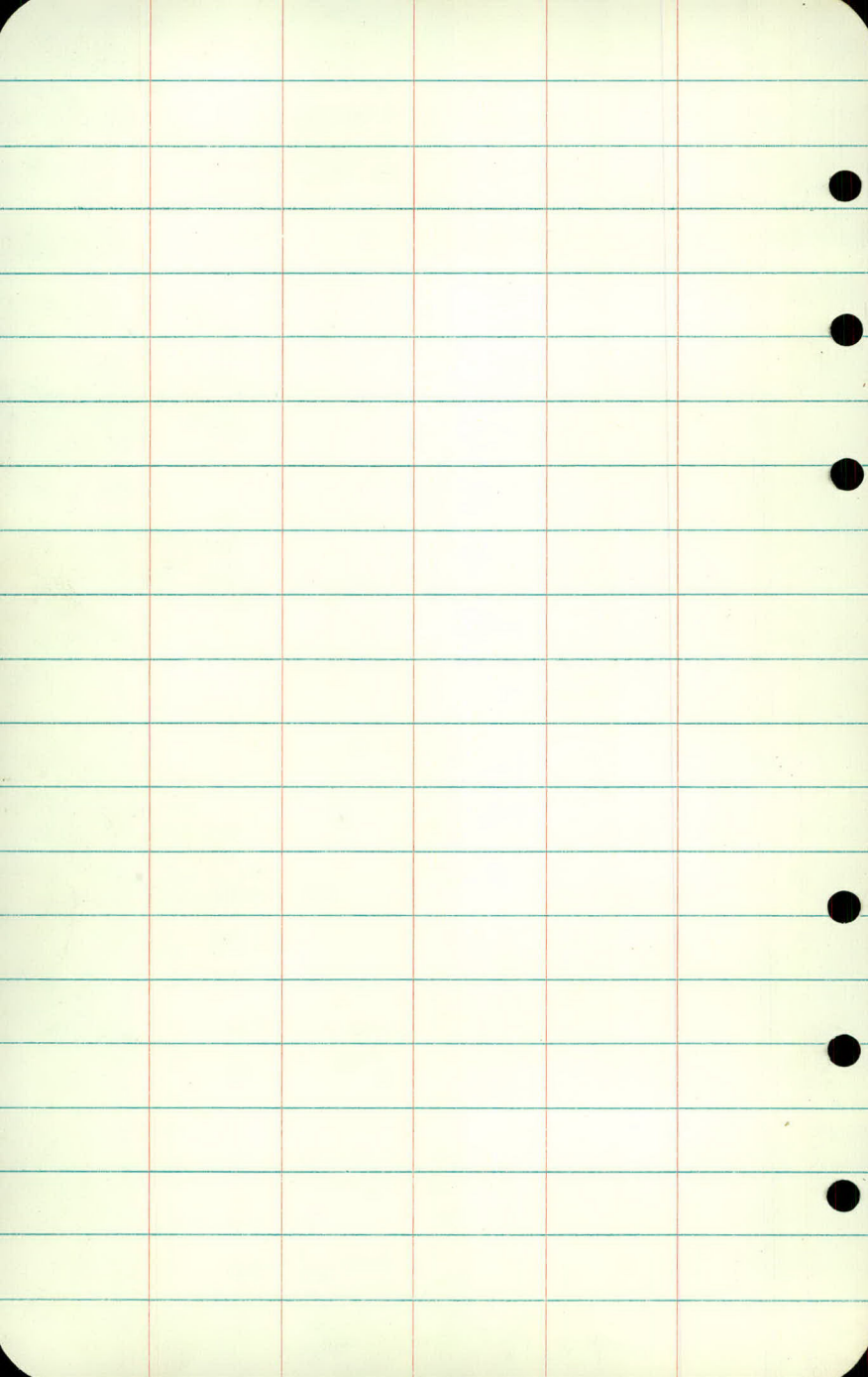
£

R+

STA	+	$\bar{A}$	-	Elev
BM	1.46	889.19		(887.73)
TP	4.90	887.61	6.48	882.71
TP	4.59	889.54	2.66	884.95
TP	5.12	893.34	1.32	888.22
BM			5.12	888.22 (888.25)

Spike in 24" oak at pump pipe outlet
Lake Josephine

SE Cor Top NE Wing wall. bridge Sta 173+50
Top SE Cor West Curb on bridge



SNELLING AVE

Bench Levels
and
Profile

STA + π - Elev

BM 4.52 892.77

888.25

172

+25

+50

+75

173

+25

PK
CM
CP
BP

Lt

£

June 25 70

RT

1

84.67
8.1

84.27
8.5

84.07
8.7

84.27
8.5

84.67
8.1

85.07
7.7

STA + $\bar{T}$ - Elev

892.77

+50

+75

174

+25

+50

+75

LT

£

RT

2

85.67
7.1

86.27
6.5

86.67
6.1

87.07
5.7

87.37
5.4

87.67
5.1

STA + π - Elev

892.77

175

+25

+50

+75

176

+25

Lt

£

Rt

3

87.77
5.0

87.87
4.9

87.97
4.8

87.97
4.8

87.87
4.9

87.97
4.8

STA + π - Elev

892.77

+50

+75

177

+25

+50

+75

Lt

£

Rt

4

88.17
4.6

88.37
4.4

88.77
4.0

89.47
3.3

90.07
2.7

90.67
2.1

STA + π - Elev
892.77

178

TP 10.82 902.09 1.50 891.27

+25

+50

+50

+75

179

+25

Lt

£

RT

5

91.27
1.5

PK STA 178 £

91.89
10.2

92.59
9.5

93.29
8.8

94.09
8.0

94.69
7.4

STA + $\bar{T}$ - Elev

902.09

+50

+75

TP 13.70 911.27 4.52 897.57
180

+25

+50

+75

LT

£

T

RT

6

95.39
6.7

96.09
6.0

Top Hyd STA 179+75 LT

96.47
14.4

97.57
13.7

98.27
13.0

98.97
12.3

STA + $\bar{\pi}$ - Elev

911.27

181

+25

+50

+75

182

+25

LT

£

RT

7

99.67
11.6

900.37
10.9

01.27
10.0

02.04
9.2

02.87
8.4

03.47
7.8

STA	+	π	-	Elev
-----	---	-------	---	------

		911.27		
--	--	--------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

183				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

LT

£

RT

8

~~04.27~~
7.0

~~04.97~~
6.3

~~05.77~~
5.5

~~06.37~~
4.9

~~07.17~~
4.1

~~07.87~~
3.4

STA + π - Elev

911.27

184

TP 9.74 920.91 0.10 911.17

+25

+50

+75

185

+25

Lt

E

Rt

9

184

2.7

08.57

Top Hyd STA 184+20 Lt

25

11.6

09.31

50

10.9

10.01

75

10.2

10.71

185 00

9.5

11.41

25

8.7

12.21

STA + π - Elev

920.91

+50

+75

186

+25

+50

+75

LT

C

RT

10

12.81
8.1

13.51
7.4

14.11
6.8

14.61
6.3

15.01
5.9

15.31
5.6

1

STA

+

π

-

Elev

920.91

187

+25

+50

+75

188

+25

LT

£

RT

11

$$\begin{array}{r} 15.41 \\ 5.5 \end{array}$$

$$\begin{array}{r} 15.51 \\ 5.4 \end{array}$$

$$\begin{array}{r} 15.61 \\ 5.3 \end{array}$$

$$\begin{array}{r} 15.61 \\ 5.3 \end{array}$$

$$\begin{array}{r} 15.61 \\ 5.3 \end{array}$$

$$\begin{array}{r} 15.41 \\ 5.5 \end{array}$$

STA	+	π	-	Elev
-----	---	-------	---	------

		920.91		
--	--	--------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

189				
-----	--	--	--	--

+25				
-----	--	--	--	--

TP	0.63	915.52	6.02	914.89
----	------	--------	------	--------

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

LT

£

RT

12

5.7
15.21

6.0
14.91

6.5
14.41

7.0
13.91

Top Hyd STA 189 + 20 LT

2.2
13.32

2.9
12.62

STA	+	π	-	Elev
-----	---	-------	---	------

		915.52		
--	--	--------	--	--

190				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

191				
-----	--	--	--	--

+25				
-----	--	--	--	--

L+

2

R+

13

$$\begin{array}{r} 12.02 \\ 3.5 \end{array}$$
$$\begin{array}{r} 11.32 \\ 4.2 \end{array}$$
$$\begin{array}{r} 10.72 \\ 4.8 \end{array}$$
$$\begin{array}{r} 10.32 \\ 5.2 \end{array}$$
$$\begin{array}{r} 09.82 \\ 5.7 \end{array}$$
$$\begin{array}{r} 09.52 \\ 6.0 \end{array}$$

STA	+	π	-	Elev
-----	---	-------	---	------

		915.52		
--	--	--------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

192				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

Lt

¢

Rt

14

09.12

6.4

08.92

6.6

08.82

6.7

08.52

7.0

08.22

7.3

07.92

7.6

STA + π - Elev

915.52

193

+25

+50

+75

194

TP 4.33 913.25 6.60 908.92

+25

LT

£

RT

15

07.82
7.7

07.72
7.8

07.52
8.0

07.42
8.1

07.32
8.2

Top Hyd STA 194+05 LT

07.25
6.0

STA + π - Elev

9/3.25

+50

+75

195

+25

+50

+75

L+

-

R+

16

07.15
6.1

07.15
6.1

07.25
6.0

07.25
6.0

07.25
6.0

07.35
5.9

STA + π - Elev

9/3.25

196

+25

+50

+75

197

+25

L+

£

R+ 17

07.45
5.8

07.65
5.6

07.95
5.3

08.35
4.9

08.75
4.5

09.35
3.9

STA + π - Elev

913.25

+50

+75

198

+25

TP 10.12 923.27 0.10 913.15

+50

+75

L+

£

RT

L78

3.09.95
3.3

10.65
2.6

11.45
1.8

12.25
1.0

Top Hyd Sta 1984 45 L+

10.12.94
10.3

13.77
9.5

STA + $\bar{T}$ - Elev

923.27

199

+25

+50

+75

200

+25

Lt

£

Rt

19

14.57
8.7

15.47
7.8

16.57
6.7

17.57
5.7

18.47
4.8

19.37
3.9

STA + π - Elev

923.27

+50

+75

201

+25

TP 11.26 933.23 1.30 921.97

+50

+75

LT

Z

RT

20

2017
3.121.07
2.222.07
1.222.87
0.4

Spike in PP STA 201 + 10 LT

23.83
9.424.73
0.5

STA + T - Elev

933.23

202

+25

+50

+75

203

+25

TP 6.95 938.48
~~6.55~~ ~~938.08~~ 1.70 931.53

Lt

E

RT

21

~~5.0
3.0
3.0
3.0~~

7.6

~~5.0
3.1
3.1
3.1~~

6.8

~~5.0
3.0
3.0
3.0~~

5.9

~~5.0
3.0
3.0
3.0~~

5.0

~~5.0
3.0
3.0
3.0~~

4.0

~~5.0
3.0
3.0
3.0~~

3.3

Top Hyd NE Cor Snelling & Forest Lane

STA	+	π	-	Elev
-----	---	-------	---	------

		938.08		
--	--	--------	--	--

		938.48		
--	--	--------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

204				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

Lt

£

Rt

22

$$\begin{array}{r} 30.78 \\ 7.7 \end{array}$$
$$\begin{array}{r} 31.48 \\ 7.0 \end{array}$$
$$\begin{array}{r} 32.08 \\ 6.4 \end{array}$$
$$\begin{array}{r} 32.58 \\ 5.9 \end{array}$$
$$\begin{array}{r} 33.18 \\ 5.3 \end{array}$$
$$\begin{array}{r} 33.58 \\ 4.9 \end{array}$$

STA + π - Elev

~~938.08~~

938.48

205

+25

+50

+75

206

+25

TP 8.11

942.54

~~942.14~~

4.05

934.43

~~934.03~~

LT

4

RT

23

53.98
4.5

34.38
4.1

34.78
3.7

35.18
3.3

35.48
3.0

35.78
2.7

Spike in AirRaid Sierin STA 206+25 Lt

STA + π - Elev

~~942.14~~

942.54

+50

+75

207

+25

+50

+75

Lt

2

RT

24

36.14
6.4

36.44
6.1

36.74
5.8

36.94
5.6

37.14
5.4

37.44
5.1

STA + T - Elev.

~~942.14~~

942.54

208

+25

+50

+75

209

+25

LT

£

R+

25

37.74
4.8

38.04
4.5

38.34
4.2

38.64
3.9

38.84
~~38.84~~
3.7

39.04
3.5

STA + π - Elev

~~942.14~~

942.54

+50

+75

210

+25

+50

TP

0.72

941.13

~~940.73~~

2.13

940.41

~~940.01~~

+75

LT

L

RT

26

39.24
3.3

39.34
3.2

39.44
3.1

39.54
3.0

39.54
3.0

Top Hyd STA 210 + 60 LT

PK
CM
CP
BP

June 26 '70

39.43
1.7

STA

+

T

-

Elev

941.13

~~940.73~~

211

+25

+50

+75

212

+25

Lx

11

Rx

27

1. 39.43
1. 7

1. 39.33
1. 8

1. 39.23
1. 9

2. 39.03
2. 1

2. 38.83
2. 3

2. 38.53
2. 6

STA	+	π	-	Elev
-----	---	-------	---	------

STA	+	π	-	Elev
		941.13		
		940.73		

STA	+	π	-	Elev
		941.13		
		940.73		
+50				

STA	+	π	-	Elev
		941.13		
		940.73		
+50				
+75				

STA	+	π	-	Elev
		941.13		
		940.73		
+50				
+75				
213				

STA	+	π	-	Elev
		941.13		
		940.73		
+50				
+75				
213				
+25				

STA	+	π	-	Elev
		941.13		
		940.73		
+50				
+75				
213				
+25				
+50				

STA	+	π	-	Elev
		941.13		
		940.73		
+50				
+75				
213				
+25				
+50				
+75				

L+

L

R+

28

38.13
3.0

37.73
3.4

37.23
3.9

36.63
4.5

36.13
5.0

35.53
5.6

STA + π - Elev

941.13
~~940.73~~

214

+25

+50

+75

215

+25

LT

4

RT

29

6.3 34.83

7.1 34.03

7.9 33.23

8.8 32.33

9.8 31.33

11.0 30.13

STA + π - Elev
941.13
~~940.73~~

+50

+75

TP 1.82 932.01 930.19
~~931.61~~ 10.94 ~~929.79~~

216

+25

+50

+75

LT

£

RT

30

88.93

12.2

27.73

13.4

26.51

5.5

25.21

6.8

24.01

8.0

22.91

9.1

STA	+	π	-	Elev
		932.01		
		931.61		

217

+25

+56

+67 CONC Pavement

BM	0.54	925.72	6.84	925.17	924.77	925.18
				4		5.2
				925.17		

+75

218

LT

£

RT

31

21.81
10.2

20.91
11.1

19.91
12.1

19.35
~~12.06~~
12.66

Splice in Arc light Ble cord £ & old 51

18.67
20.5

17.96
7.76

STA + π - Elev

925.72

+25

+50

+75

219

+25

+50

Lt

£

Rt

32

12.16

8.56

16.48

9.24

15.74

9.98

14.91

10.81

14.28

11.44

13.76

11.96

STA + π - Elev

925.72
10.89

+75

220

+25

TP 1.73 9/6.56 10.89 914.83
1.73

+50

+75

221

Lt

E

Rt

33

13.18

12.54

12.61

13.11

12.08

13.64

West Edge Top MH STA 219+35 RT

PK

CM

CP

BP

11.5

June 30 1970

4.97

11.04

5.52

10.47

6.09

10.5

10.5

10.5

10.5

STA + T - Elev

916.56

+25

+50

+75

222

+25

+50

LT

£

RT

34

909.97

6.59

909.39

7.17

908.86

7.70

908.30

8.26

907.71

8.85

908.18

8.38

STA	+	T	-	Elev
-----	---	---	---	------

		916.56		
--	--	--------	--	--

+75				
-----	--	--	--	--

223				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

224				
-----	--	--	--	--

Lt

E

Rt

35

906.60

9.96

906.09

10.47

905.50

11.06

904.97

11.59

904.51

12.05

904.07

12.49

STA + π - Elev

916.56
12 49

+25

+50

TP 2.64 906.71 12.49 904.07
2 64

+75

225

+25

+50

L+

£

R+

36

903.60
12.96

903.12
13.44

STA 224 £

902.40
4.31

901.52
5.19

900.80
5.91

900.20
6.51

STA	+	T	-	Elev
-----	---	---	---	------

906.71				
--------	--	--	--	--

	+75			
--	-----	--	--	--

226				
-----	--	--	--	--

	+25			
--	-----	--	--	--

	+50			
--	-----	--	--	--

	+75			
--	-----	--	--	--

227				
-----	--	--	--	--

L+

£

R+

37

99.56
7.15

99.10
7.61

98.72
7.99

98.48
8.23

98.19
8.52

97.67
9.04

STA + T - Elev

906.71
893

+25

+50

+75 £ £ Bridge

TP 120 898.98 8.93 897.78
✓

228

+25

Lt

£

Rt

38

97.39

9.32

97.05

9.66

90.59

10.12

Top Bottom Step W side of RR Bridge by
Center Pillar → Yellow paint Spot

95.89

3.09

95.16

3.82

STA + π - Elev

898.98

+50

+75

229

+25

+50

+75

Lt

£

Rt

39

94.64
4.34

94.20
4.78

93.72
5.26

93.20
5.78

92.68
6.30

92.23
6.75

STA + T - Elev

898.98

230

+25

+50

+75

231

+25

LT

£

RT

40

91.82

7.16

91.42

7.56

91.00

7.98

90.57

8.41

90.29

8.69

89.96

9.12

STA + π - Elev

898.98
9 87

+50

+75

232

TP 4.87 89398 9.87 889.11
4 87

+25

+50

+75

Lt

£

Rt

41

~~89.60~~

9.38

~~89.55~~

9.43

~~89.49~~

9.49

S.P. Ke in PP STA 232 ± Rt

~~49.32~~

4.66

~~49.18~~

4.80

~~48.99~~

4.99

STA	+	π	-	Elev.
-----	---	-------	---	-------

		893.98		
--	--	--------	--	--

2.33				
------	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

234				
-----	--	--	--	--

+25				
-----	--	--	--	--

LT

E

RT

42

82.82

5.16

80.64

5.34

81.50

5.48

81.38

5.66

81.15

5.83

81.98

6.06

STA	+	$\nearrow$	-	Elev
-----	---	------------	---	------

		893.98		
--	--	--------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

235				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

Lt

2

Rt

43

87.68
6.30

87.48
6.50

87.31
6.67

87.10
6.88

86.97
7.01

86.92
7.06

STA + π - Elev

893.98
6.57

236

+25

+50

+75

237

+25

TP 3.49 890.90 6.57 887.41

Lt

£

Rt

44

~~86.94~~

7.04

~~86.97~~

7.01

~~86.91~~

7.07

~~86.92~~

7.06

~~86.85~~

7.13

~~86.83~~

7.15

Spike in PP STA 237+40± Rt

STA	+	T	-	Elev
-----	---	---	---	------

		890.90		
--	--	--------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

238				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

Lt

Σ

→

RT

45

•
86.75

4.15

•
86.71

4.19

•
86.64

4.26

•
86.55

4.35

•
86.50

4.40

•
86.42

4.48

STA + π - Elev

890.90

239

+25

+50

+75

240

+25

Lt

±

Rt

46

86.27

4.63

86.15

4.75

86.02

4.88

85.87

5.03

85.71

5.19

85.56

5.34

STA + π - Elev

890.90

+50

+75

241

+25

+50

+75

Lt

£

Rt

47

85.46

5.44

85.41

5.49

85.40

5.50

85.32

5.58

85.22

5.68

85.14

5.76

STA + T - Elev

890.90
779

242

+25

+50

+75

243 Begin BIT Pavement

TP 7.04 890.15 7.79 883.11
7.04

+25

Lt

-

T

RT

48

85.12

5.78

85.00

5.90

84.96

5.94

84.86

6.04

84.80

6.10

Spike in PP STA 243+ ± Lt

84.74

5.41

STA + $\bar{A}$ - Elev.

890.15

+50

+75

244

+25

+50

+75

Lt

£

Rt

49

84.71

5.44

84.70

5.45

84.58

5.57

84.38

5.77

84.15

6.00

84.27

5.88

STA	+	π	-	Elev
-----	---	-------	---	------

		890.15		
--	--	--------	--	--

245				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

246				
-----	--	--	--	--

+25				
-----	--	--	--	--

LT

E

RT

50

84.48

5.67

84.51

5.58

84.50

5.57

84.75

5.40

84.82

5.33

84.71

5.44

STA	+	$\uparrow$	-	Elev
-----	---	------------	---	------

		890.15		
--	--	--------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

247				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

LT

2

RT

51

4.77
8

5.38

4.77
8

5.38

4.70
8

5.45

4.57
8

5.58

4.53
8

5.62

4.57
8

5.58

STA + $\bar{A}$ - Elev

890.15
69

248

TP 1.55 891.04 0.66 889.49

BM 11.20 879.84 ~~880.09~~

✓

879.84

TP 0.60 890.09 889.49
60

+25

+50

+75

249

Lt

E

Rt

52

41.73
 81
 5.42

Top Hyd SW Cor Co Rd E² & TH 10

Spike in PP NE Cor TH 10 & E²

PK
 CP
 BP

July 9 '70

Top Hyd SW Cor Co Rd E² & TH 10

41.76
 81
 5.37

41.99
 81
 5.10

41.99
 81
 5.1

45.09
 81
 5.0

STA	+	T	-	Elev
-----	---	---	---	------

		890.09		
--	--	--------	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

250				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

LT

£

RT

53

85.09

5.0

85.09

5.0

84.99

5.1

84.99

5.1

84.99

5.1

84.89

5.2

STA	+	π	-	Elev
-----	---	-------	---	------

		890.09		
--	--	--------	--	--

+ 75				
------	--	--	--	--

251				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

252				
-----	--	--	--	--

LT

E

RT

54

84.89

5.2

84.79

5.3

84.79

5.3

84.69

5.4

84.69

5.4

84.59

5.5

STA + 7 - Elev

890.09

+25

+50

+75

253

+25

+50

LT

Z

RT

55

84.49

5.6

84.49

5.6

84.39

5.7

84.09

6.0

83.99

6.1

83.99

6.1

STA	+	$\bar{\Delta}$	-	Elev
-----	---	----------------	---	------

		890.09		
--	--	--------	--	--

+75				
-----	--	--	--	--

254				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

255				
-----	--	--	--	--

LT

E

RT

56

83.99
6.1

83.79
6.3

83.89
6.2

83.89
6.2

83.79
6.3

83.59
6.5

STA	+	7	-	Elev
-----	---	---	---	------

		890.09		
--	--	--------	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

256				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

LT

Z

RT

57

83.39
6.7

83.39
6.7

83.59
6.7

83.89
6.8

83.19
6.9

Begin Conc
83.05
7.04

STA + 7 - Elev

890.09
134

+75

257

+25

TP 5.72 888.45 7.36 882.73
5/2

+50

+75

258

LT

E

RT

58

82.95

7.14

82.86

7.23

82.78

7.31

82.75

5.70

82.83

5.62

82.81

5.64

STA + π - Elev

888.45

+25

+50

+75

259

+25

+50

LT

£

RT

59

82.77

5.68

82.76

5.69

82.75

5.70

82.67

5.78

82.66

5.79

82.73

5.72

STA	+	+	-	Elev
-----	---	---	---	------

				888.45
--	--	--	--	--------

+75				
-----	--	--	--	--

260				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

261				
-----	--	--	--	--

LT

£

RT

60

82.71
5.74

82.71
5.74

82.65
5.80

82.57
5.88

82.49
5.96

82.37
6.08

STA + Δ - Elev

888.45
478

+25

+50

+75

TP 5.20 888.87 4.78 883.67

262

+25

+50

LT

E

RT

61

82.36

6.09

82.41

6.04

82.39

6.06

Top Hyd STA 261+75.7 LT.

82.35
6.5282.4
3
82.1

82.59

6.28

82.71

6.16

STA + T - Elev

888.87

+75

263

+25

+50

+75

264

LT

£

RT

62

83.5
82.8
82.5
6.02

83.99
82.99
5.88

83.08
83.08
5.79

83.13
83.13
5.74

83.21
83.21
5.66

83.29
83.29
5.58

STA + T - Elev

888.87

+25

+50

+75

265

+25

+50

LT

2

RT

63

83.37

5.50

83.46

5.41

83.51

5.36

83.51

5.30

83.64

5.23

83.76

5.11

STA + π - Elev

888.87
5.90

+75

266

+25

+50

+75

TP 6.16 889.13 5.90 882.97
6.16

267

LT

- 2

RT

64

83.75
8

5.12

83.81
8

5.06

83.86
8

5.01

83.91
8

4.96

84.03
83.93
8

4.84

84.07
8

5.06

STA

+

↑

-

Elev

889.13

+25

+50

+75

268

+25

+50

LT

D

RT

65

84.16
8
4.97

84.38
8
4.75

84.49
8
4.64

84.66
8
4.47

84.7
84.4
84.3

84.83
8
4.30

84.93
8
4.20

STA + $\nearrow$ - Elev

889.13

+75

269

+25

+50

+75

270

LT

4

RT

66

84.93
4.20

85.26
3.87

85.36
3.77

85.45
3.68

85.51
3.54

85.61
3.46

STA + π - Elev

889.13

+25

+50

TP 5.84 892.23 2.74 886.39
5.84

+75

271

+25

+50

LT

-

RT

67

85.80

3.33

85.86

3.27

Spike in PP STA 270+50 $\pm$ RT

86.03

6.20

86.16

6.07

86.28

5.95

86.34

5.89

STA	+	π	-	Elev
-----	---	-------	---	------

		892.23		
--	--	--------	--	--

+75				
-----	--	--	--	--

272				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

273				
-----	--	--	--	--

Lt

d

Rt

68

86.30
5.85

86.43
5.80

86.53
5.70

86.63
5.60

86.67
5.56

86.78
5.45

STA

+

↑

-

Elev

892.23

+25

+50

+75

274

+25

+50

LT

-

RT

69

86.89
8
5.34

86.93
8
5.30

86.99
8
5.24

86.90
8
5.33

87.00
8
5.23

87.03
8
5.20

STA

+

$\bar{A}$

-

Elev

892.23

+75

275

+25

+50

+75

276

LT

4

RT

70

86.93

5.30

87.05

5.18

87.05

5.18

86.94

5.29

86.83

5.40

86.58

5.65

STA + π - Elev

892.23
765

+25

TP 6.27 890.85 7.65 884.58

+50

+75

277

+25

+50

Lt

E

RT

71

86.39

5.84

SPike in PP STA 276 + 25 ± ~~RT~~ Lt

86.31

4.54

86.25

4.6

86.15

4.7

86.05

4.8

85.95

4.9

STA + π - Elev

890.85

+75

278

+25

+50

+75

279

Lt

£

Rt

72

85.75
5.1

85.65
5.2

85.65
5.2

85.65
5.2

85.75
5.1

85.65
5.2

STA	+	π	-	Elev
-----	---	-------	---	------

		890.85		
--	--	--------	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

280				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

TP	10.85	896.90	4.80	886.05
----	-------	--------	------	--------

LT

Ø

RT

73

5.55
5.3

5.55
5.3

5.45
5.4

5.55
5.5

5.25
5.6

5.25
5.6

Top Hyd STA 280+50 ± 1'

STA + π - Elev

896.90

+75

281

+25

+50

+75

282

LT

\$

RT

74

PK
CP
BP

July 10 '70

85.60

11.3

85.60

11.3

85.80

11.1

85.90

11.0

STA	+	$\bar{A}$	-	Elev
-----	---	-----------	---	------

		896.90		
--	--	--------	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

283				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

LJ

4

RT

75

86.20

10.7

86.40

10.5

86.70

10.2

87.10

9.8

87.50

9.4

87.90

9.0

STA + π - Elev

896.90

+75

284

TP 13.46 908.96 1.40 895.50

BM 0.31 908.65 (908.66)

TP 2.25 897.75 (895.50)
2.25

+25

+50

+75

LT

E

RT

76

88.30
8.6

88.70
8.2

Spike in PP 6' North Bridge 9311 ET
Std disk NW cor Bridge 9311 (Traverse Sta)

Spike in PP 6' North Bridge 9311 Lt.
88.05
8.7

88.35
8.4

88.65
8.1

STA + π - Elev
897.75

285

+25

+50

+75

286

TP 7.11 898.64 6.22 891.53

+25

LT

4

RT

77

90.05
89.85

7.7

90.55

7.2

90.25

6.9

91.25

6.5

91.65

6.1

Spike in PP STA 286 +00± LT

92.04

6.6

STA + T - Elev

898.64

+50

+75

287

+25

+50

+75

L+

~~E~~

R+

78

92.34

6.3

92.74

5.9

92.04

5.6

92.24

5.4

92.44

5.2

93.64

5.0

STA + π - Elev

898.64

288

+25

+50

+75

289

+25

LT

£

RT

79

93.74

4.9

93.74

4.9

93.74

4.9

93.84

4.8

94.14

4.5

94.08

4.56

STA	+	$\nearrow$	-	Elev
-----	---	------------	---	------

		898.64		
--	--	--------	--	--

		_{2 1 4}		
--	--	------------------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

290				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

TP	1.96	898.46	2.14	896.50
----	------	--------	------	--------

LT

±

RT

80

94.08

4.56

94.07

4.57

94.02

4.62

94.04

4.60

94.02

4.62

94.02

4.62

Spike in PP STA 290+75± LT

STA + π - Elev

898.46

291

+25

+50

+75

292

+25

LT

2

RT

81

93.95

4.51

93.89

4.57

93.83

4.63

93.87

4.59

93.86

4.60

93.85

4.61

STA + T - Elev

898.46

+50

+75

293

+25

+50

+75

LT

L

RT

82

93.76

4.70

93.76

4.70

93.66

4.80

93.65

4.81

93.60

4.86

~~93.48~~

4.98

STA + π - Elev

898.46

294

+25

+50

+75

TP 1.91 896.09 4.28 894.18
191

295

+25

Lt

£

PT

83

93.40

5.06

93.31

5.15

93.30

5.16

93.20

5.26

Spike in PP STA 294+75±

93.09

3.00

92.99

3.10

STA + Δ - Elev

896.09

+50

+75

296

+25

+50

+75

LT

±

RT

84

92.89
3.20

92.76
3.33

92.79
3.3

92.49
3.6

92.09
4.0

91.59
4.5

STA

+

π

-

Elev

896.09

297

+25

+50

+75

298

+25

LT

E

RT

85

91.19

9.9

90.89

5.2

90.89

5.2

90.69

5.4

90.59

5.5

90.39

5.7

STA + $\bar{I}$ - Elev

896.09

+50

+75

299

+25

T.P. 10.65 898.52 8.22 887.87

+50

+75

Lt

£

RT

86

90.49

5.6

90.69

5.4

90.89

5.2

91.19

4.9

Spike in P.P STA. 299+25 ± Lt.

91.42

7.1

91.62

6.9

STA	+	T	-	Elev
		898.52		
300				
+25				
+50				
+75				
301				
+25				

Lt

£

Rt

87

91.84

6.68

92.20

6.32

92.59

5.93

92.77

5.75

93.01

5.51

93.19

5.33

STA	+	$\bar{T}$	-	Elev
-----	---	-----------	---	------

		898.52		
--	--	--------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

302				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

LT

C

RJ

88

93.[.]56

4.96

93.[.]92

4.60

94.[.]25

4.27

94.[.]62

3.90

95.[.]04

3.98

95.[.]49

3.03

STA + X - Elev

898.52

303

+25

+50

T.P. 11.80 906.27 4.05 899.47

+75

304

+25

LT

L

RT

89

95.95
2.57

96.44
2.08

96.80
1.72

Spike P.P LT STA 303+80±

97.25
9.02

97.54
8.73

97.5
97.2

97.91
8.36

STA + π - Elev

906.27

+50

+75

305

+25

+50

+75

LT

£

RT

90

98.22

8.05

93.61

7.66

99.01

7.26

99.42

6.85

99.81

6.46

900.26

6.01

STA	+	π	-	Elev
-----	---	-------	---	------

		906.27		
--	--	--------	--	--

306				
-----	--	--	--	--

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

307				
-----	--	--	--	--

+25				
-----	--	--	--	--

LT

— 2

RT

91

900.70

5.57

01.07

5.20

01.43

4.84

01.26

4.41

02.30

3.97

02.79

3.48

STA	+	π	-	Elev
-----	---	-------	---	------

		906.27		
--	--	--------	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

308				
-----	--	--	--	--

TP	7.02	913.19	0.10	906.17 702
----	------	--------	------	---------------

+25				
-----	--	--	--	--

+50				
-----	--	--	--	--

+75				
-----	--	--	--	--

LT

E

RT

92

903.23

3.04

03.67

2.60

04.10

2.17

Spike in guard Rail Post STA 307+75± RT

04.40

8.79

04.78

8.41

05.20

7.99

STA + π - Elev.

9/3.19

309

+25

+50

+75

310

+25

L+

£

R+

93

05.69

7.50

06.10

7.09

06.26

6.93

06.72

6.47

07.13

6.06

07.54

5.65

7.1
3
906.8

STA + T - Elev

913.19

+50

+75

311

+25

+50

+75

L+

Σ

R+

94

07.98
5.21

08.42
4.77

08.83
4.36

09.25
3.94

09.66
3.53

10.15
3.04

STA + π - Elev

913.19

45

312

+25

TP

5.99

918.73

~~918.63~~

0.45

912.74

~~912.64~~

+50

+75

313

+25

LT

E

RT

10.49
2.70

10.53
10.2

10.34
2.45

Spike in PP STA 312 + 30 ± LT

11.16
7.57

11.59
7.14

12.00
6.73

12.37
6.36

STA + $\bar{A}$ - Elev

918.73

+50

+75

314

+25

+50

+75

Lt

£

RJ

96

12.73
6.00

13.10
5.63

13.37
5.36

13.61
5.12

13.80
4.93

13.90
4.83

STA + π - Elev

918.73

315

+25

+50

+75

316

+25

LT

£

RT

97

14.04

4.69

14.02

4.71

14.07

4.66

14.04

4.69

13.98

4.75

13.83

4.90

STA + π - Elev

918.73
2.9

+50

+75

TP 0.23 916.48 2.48 916.25

317

+25

+50

+75

Lt

±

Rt

98

13.67
5.06

13.38
5.35

Spike in PP STA 316 + 90 ± LT

13.11
3.37

12.79
3.69

12.43
4.05

12.06
4.42

STA + $\bar{T}$ - Elev

916.48

318

+25

+50

+75

319

+25

LT

2

RT

99

10.63

5.85

11.26

5.22

10.92

5.56

10.66

5.92

10.19

6.29

09.84

6.64

STA + π - Elev

916.48
739

+50

+75

320

TP 6.52 915.61 7.39 909.09

+25

+50

+75

LT

£

RT

100

09.52

6.96

09.31

7.17

£ STA 320

PK
BP
DR
JT

09.01

6.60

July 13 1970

08.82

6.79

08.65

6.96

STA + T - Elev

9/5.61

321

+25

+50

+75

322

+25

LT

£

RT

101

08.71
6.90

908.73
908.4

09.01
6.60

09.28
6.33

09.51
6.10

09.71
5.90

09.81
5.74

STA + $\nearrow$ - Elev

915.61

+50

+75

323

+25

+50

+75

LT

£

RT

102

10.09

5.52

10.31

5.30

10.60

5.01

10.31

4.8

BIT.

11.01

4.6

11.11

4.5

STA + π - Elev

9/5.61

324

+25

+50

+75

325

+25

LT

£

RT

103

11.31
4.3

11.61
4.0

11.91
3.7

12.31
3.3

12.61
3.0

12.81
2.8

STA + $\nearrow$ - Elev

915.61

5.41

+50

+75

326

+25

+50

+75

TP 11.57 921.91 5.21 910.40

11.57

LT

L

RT

104

13.11
2.5

13.51
2.1

13.81
1.8

14.11
1.5

14.41
1.2

14.61
1.0

Spike in PP STA 326+75 ± LT

STA + π - Elev

921.91

327

+25

+50

+75

328

+25

LT

2

RJ

105

14.81

7.1

15.01

6.9

15.21

6.7

15.41

6.5

15.71

6.2

15.91

6.0

STA + T - Elev

921.91

+50

+75

329

+25

+50

+75

Lt

£

Rt

106

16.01

5,9

16.21

5,7

16.41

5,5

16.61

5,3

16.81

5,1

17.01

4,9

STA + T - Elev

921.91
254

330

+25

+50

+75

331

TP 4.36 923.73 2.54 919.37

B'M 1.68 922.05 922.05

LT

E

RT

107

17.21

4.7

17.41

4.5

17.61

4.3

17.81

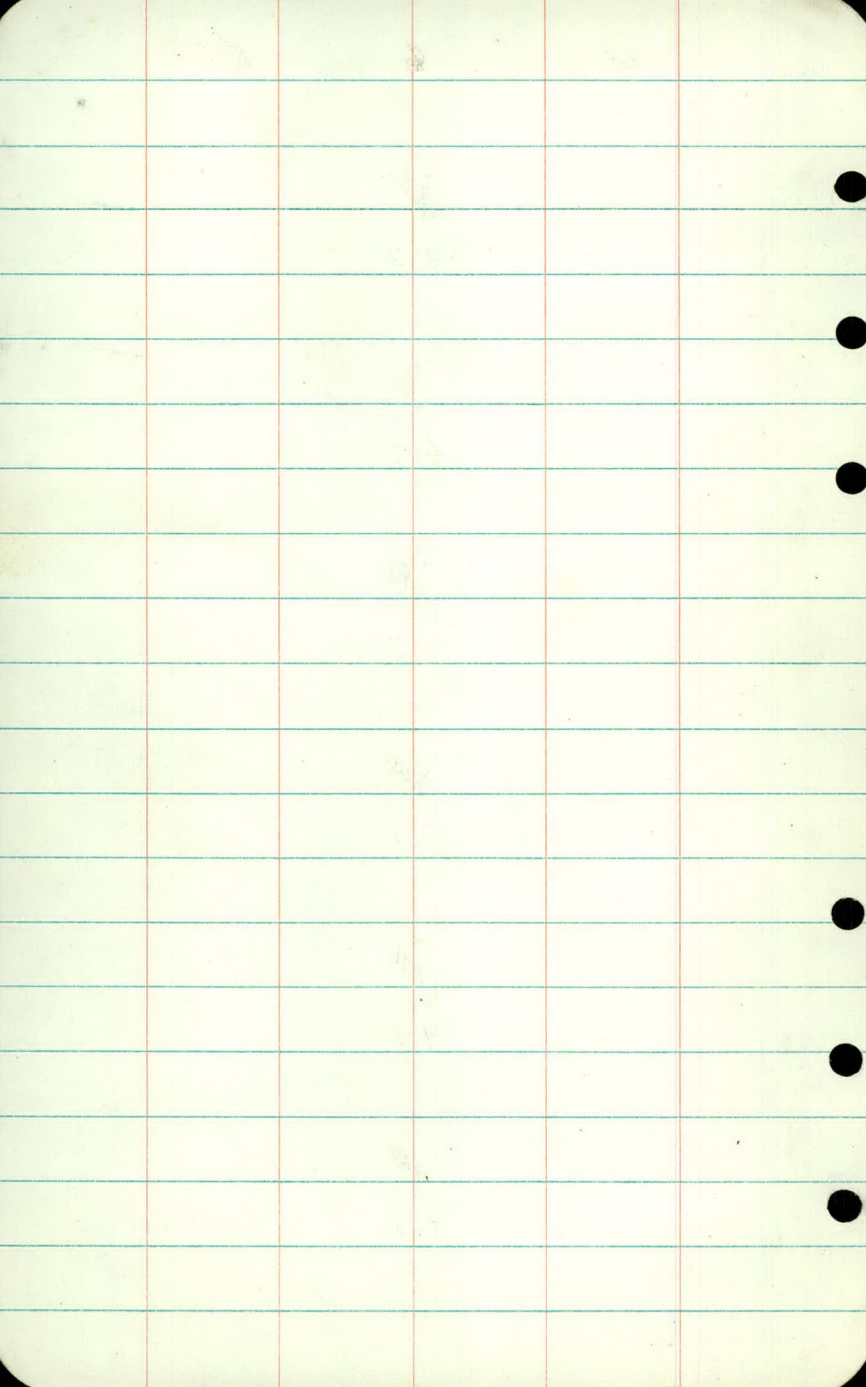
4.1

17.91

4.0

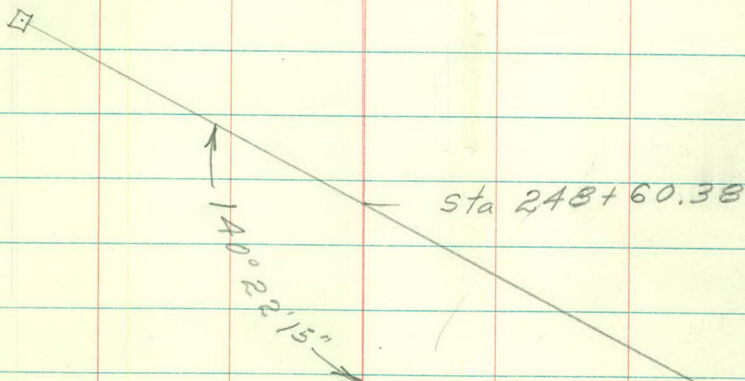
Spike in PP STA 331 + 25 ±

USCE MON NE COR TH 96 ± H 10

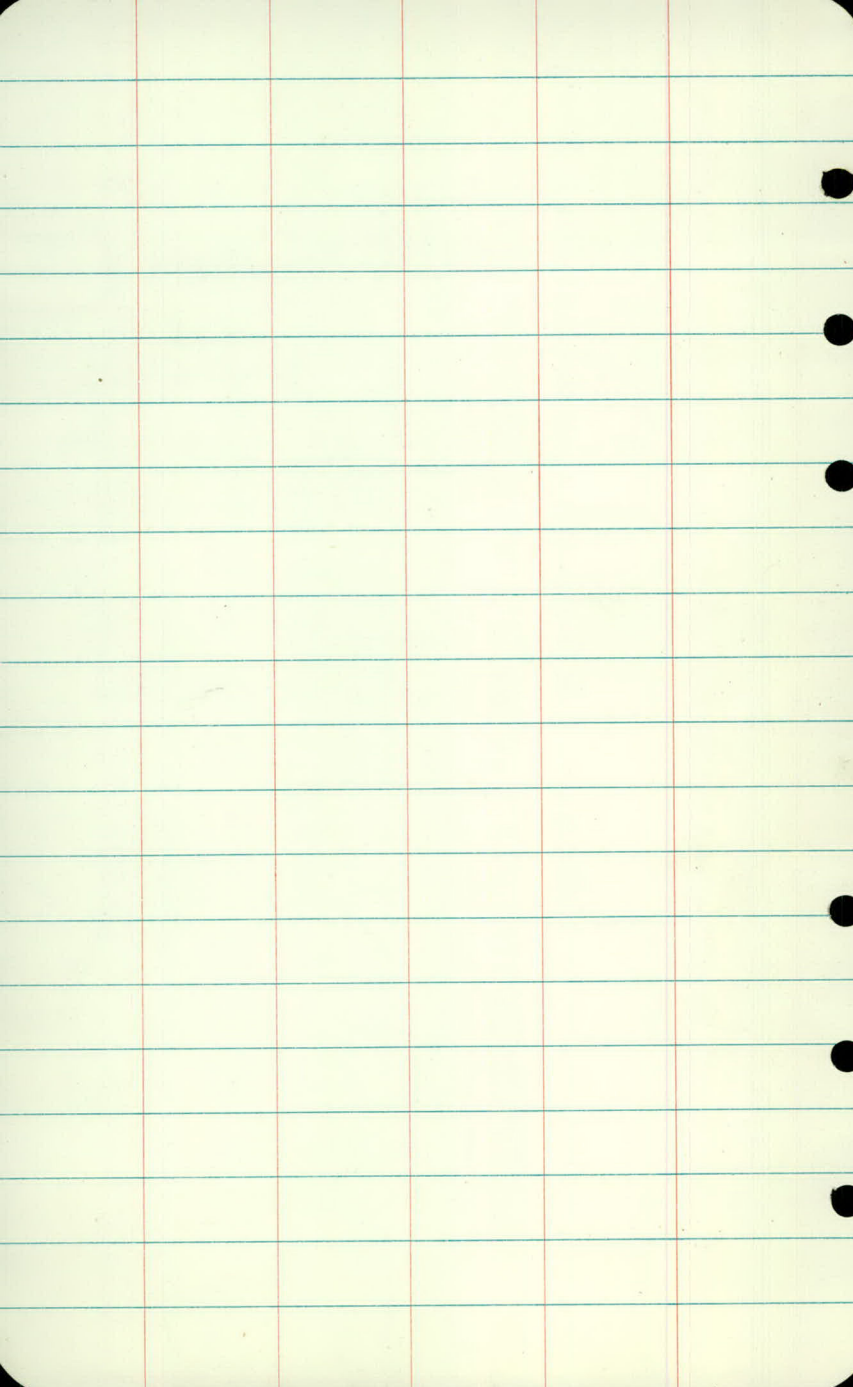


FK
CP
BP
JT
DR

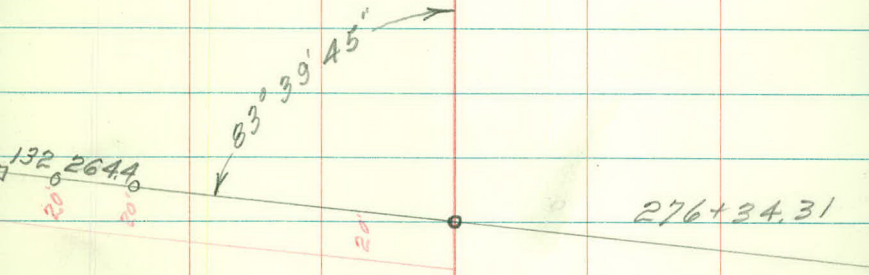
July 22, 1970



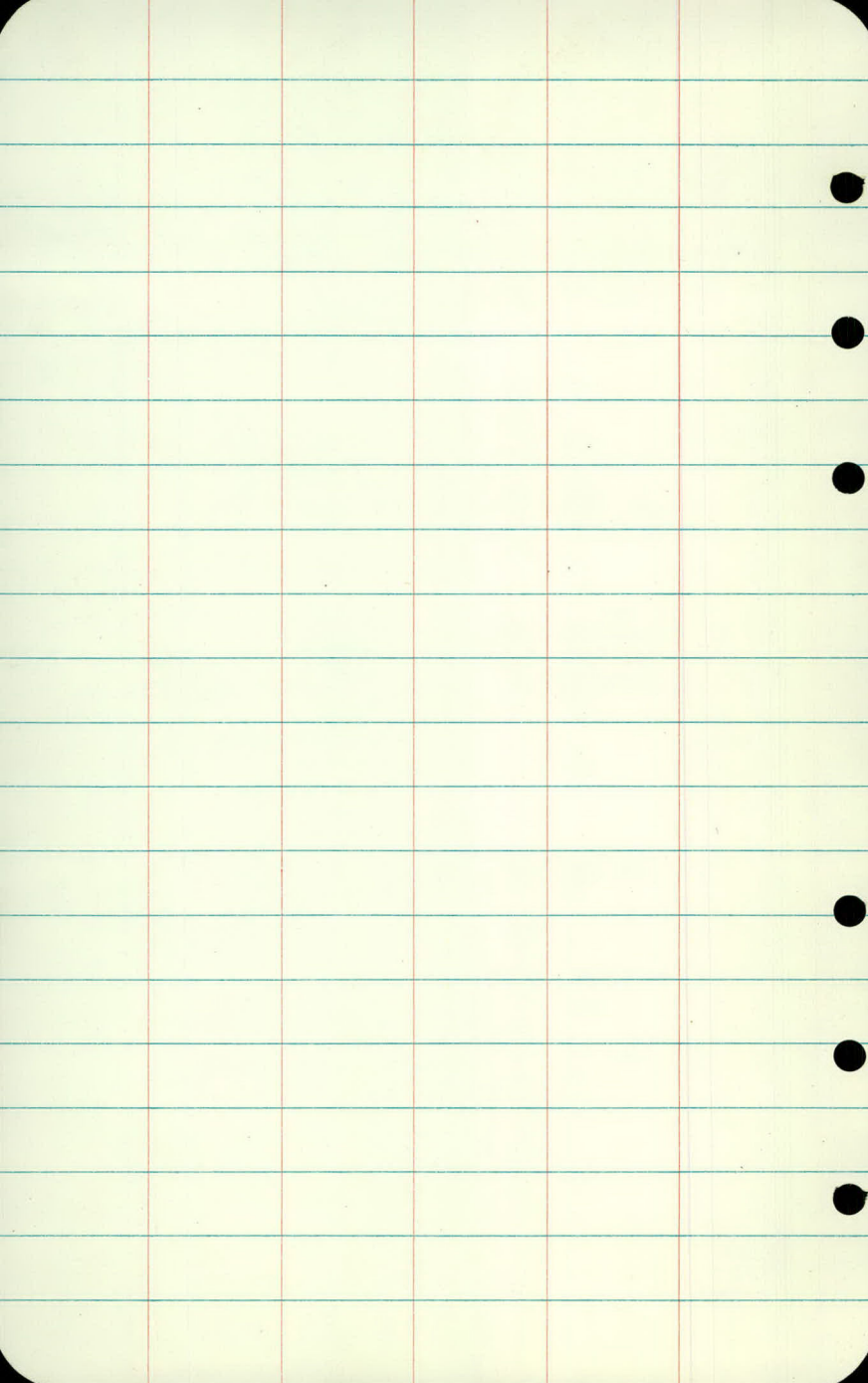
P.I.



P.I.



276



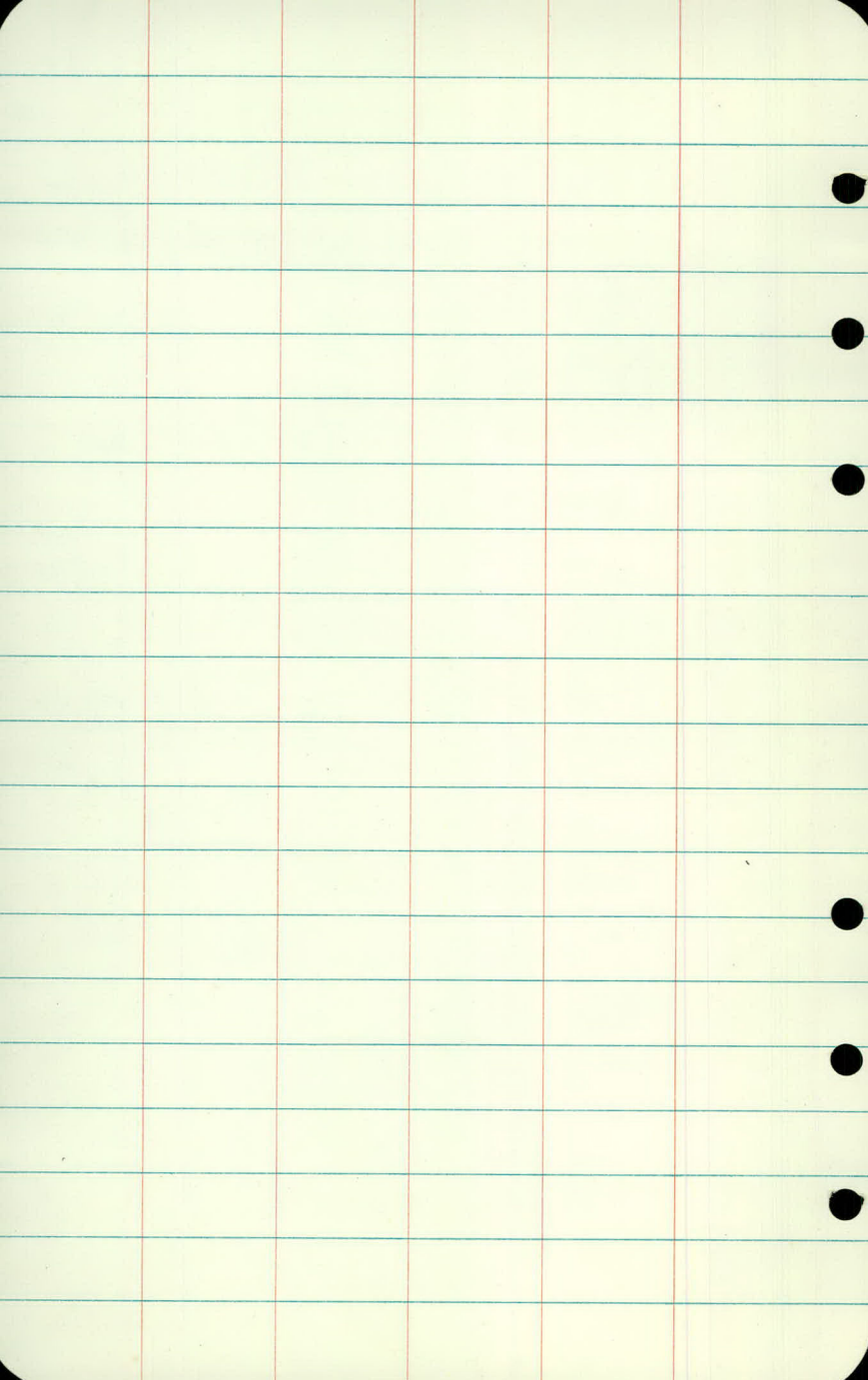
July 24, 1970

0.07 Short of
Previous P.O.T.

Found Drill Hole

Sta 302+76.78

$\leftarrow 89^{\circ} 46' 30'' \rightarrow$



July 24, 1970

1

76 Turnback

Ent. Profile

Sta + π - Elev.

BM 4.65 892.87 888.25

173+58 Turn off #51

BM 11.84 901.71 300 889.87
11.84
901.71

175+66 Ent Lt

✓

TP 6.52 897.95 10.28 891.43 Top Bridge

178+49 Ent Lt

✓

17

179+91 Ent Lt.

BM

0.38

897.57 J.A.
~~907.57~~ 897.57

FK
CP
BP
DR
JT

July 24, 1970

2

17

RT

Top S.E. Corner NE Wing wall Sta 173+50

85.9	85.7	85.2	83.6	83.5
7.0	7.2	7.7	9.3	9.4
	13	28	59	100

Top Hyd by Ho # 3233

90.3	89.0	88.0	87.7	87.9
114	127	137	140	138
59	43	25	13	
B.T.				

92.7	95.3	98.3	900.4	901.3	016.7
9.0	6.4	3.4	1.3	0.4	0.34
79	100	126	150	175	178
Conc ←					

89.1	89.7	90.9	92.1	92.5	92.6
8.9	8.3	7.1	5.9	5.5	5.4
100	78	49	25	12	

88.9	89.2	89.7
9.1	8.8	8.3
130	160	200

95.9	95.9	94.6	96.1	96.6	96.7
4.1	4.1	3.4	1.9	1.4	1.3
103	78	52	29	13	

Sta	+	π	-	Elev.
BM	5.38	916.55		911.17

183+94 Ent Lt

184+82 E Cummings Lane

BM 5.24

T.P. 6.96 921.05 2.46 914.09 Sta 186

186+71 Ent Lt

187+00 Ent Rt

187+50 Ent Rt

BM 7.04 914.01 914.00

BM 4.48 919.37 6.15 914.90 914.89

F
 C
 8
 JT
 DR

July 27, 1970

3

Top Hyd Lt. Sta 184+20

14.7	12.5	10.9	08.7	08.4	08.5
1.9	4.1	6.0	7.9	8.2	8.1
108	80	56	31	11	

10.9	10.0	10.0	08.7	07.7	06.8
5.7	5.8	6.6	7.9	8.9	9.8
14	40	73	106	132	

Top Hyd NE Corner Cummings Lane 4

914.11

13.1	13.7	14.2	14.4	14.9	15.3
8.0	7.4	6.9	6.7	6.2	5.8
110	84	59	32	10	

17.07	16.8	16.1	15.8	15.9	15.5	15.9	15.8	16.1	16.8	17.07
3.98	4.3	5.0	5.3	5.2	5.6	5.2	5.3	5.0	4.3	3.98
102	77	57	32	14		14	32	57	77	102
Conc						Conc				

16.6	16.1	15.7	15.6	16.1	16.5
5.5	5.0	5.4	5.5	5.0	4.6
14	35	53	74	101	

Top Hyd Rt Sta

16.72
 4.33
 112
 Conc

Top Hyd Lt Sta 189+20

Sta	+	π	-	Elev.	
		919.37			
189+15	Ent	Lt.			Top Hyd Rd
BM	0.09	914.09	5.37	914-	Sta
192+06	} Ent Lt				
192+26					
✓					
193+00	£ Glen arden Rd				
BM			5.80	908.29	[±] 908.31
BM	3.34	912.26	5.19	908.90	(908.92)
195+61	Ent	Lt.			
TP	13.34	922.11	3.49	908.77	

July 27, 1970
Rt

4

11.

11.1	11.7	11.9	12.2	13.4	14.1
8.3	77	7.5	72	60	53
150	100	78	50	12	
B.T.			C.R.		

13.0	13.6	14.0
6.4	5.8	5.4
2 Ent	14	
27		

07.8	09.3	11.9	12.6	13.5	13.8
11.6	10.1	7.5	6.8	5.9	5.6
59	44	33	26	14	
2 Ent					

06.2	04.5	02.6
13.2	14.9	16.8
Ent Profile		
73	88	111

13.1	13.0	12.3	11.3	10.4	09.7
6.3	6.4	7.1	8.1	9.0	9.7
9	31	51	76	99	

Top Hyd NE Corner Glenarden Rd & Snelling

Top Hyd 1st Sta 194+05

08.2	08.2	07.7	07.3	07.2	07.2	07.3
4.1	4.1	4.6	5.0	5.1	5.1	5.0
100	91	66	47	28	13	

Sta 197

Sta + π - Elev.

922.11

198+80 Skiles Lane Left

(913.13)

BM

8.97

913.14

Top Hyd Lt MB

200+05 Skiles Lane Rt

✓
BM

12.33

934.30

0.16

921.95

(921.97)

201+51

Ent Lt

✓

202+90

Forest Lane Rt

BM

9.28

940.81

2.77

931.53

(931.53)

July 27, 1970

5

11
 2.8 2.13 19.4 17.7 15.82 14.6 13.9 13.8
 2.7 4.4 6.29 7.5 8.3 8.3
 118 99 82 57 35 15
 MH

18.6 18.4 17.5 16.4 15.19 14.3
 3.5 3.7 4.6 5.7 6.92 7.8
 12 30 54 82 100
 MH

120 12.7
 10.1 9.4
 149 132

Spike in P.P. Lt. Sta 201+10

25.3 24.9 24.5 23.5 22.8 23.9
 9.0 9.4 9.8 10.8 10.5 10.4
 71 60 46 39 11

26.6
 7.7 7.48
 101 104
 Conc Apron

28.8 28.6 27.9 27.4 26.87 26.0
 5.5 5.7 6.4 6.9 7.43 8.3
 15 35 48 6.8 115
 MH
 25.99
 8.31
 131
 MH

Top Hyd N.E. Cor. Forest Lane & Snelling

Sta + π - Elev.

940.81

205+86 Arden Place Lt.

✓

206+83 Ent Lt. C.R.

✓

207+33 Ent Lt.

+40 Arden Place Rt.

BM 8.96 943.39 6.38 934.43 (934.43)

July 27, 1970
Rt.

6

Lt.

33.2 33.55 33.6 34.3 35.1 35.3
76 726 72 65 5.7 5.5
81 56 52 30 10
MH

33.1 32.9 32.0 31.8 31.73
7.7 7.9 8.6 9.0 9.08
100 125 155 175 194
MH

32.0 33.9 34.9 35.0 36.3 36.5
8.6 6.9 5.9 5.6 4.5 4.3
100 83 51 28 11
B;t

31.07
9.74
1.28
conc. Apron

30.6 32.90 34.50 35.60 36.70 37.0
102 7.9 6.3 5.2 4.1 3.8
88 60 45 26 11

37.1 37.0 36.7 36.5 36.3 36.09 35.9
3.7 3.8 4.1 4.3 4.5 4.72 4.9
14 34 54 71 101 114
MH

Spike in Civil Defence Siren Pole Lt 5%
206+25

35.9
4.9
175

Sta + π - Elev.

943.39

208+59

BM.

2.28 941.11

BM.

2.97 940.42 940.41

+80

Ent Lt

209

BM

2.28 941.11

BM

2.97 940.42 940.41

BM 5.80 920.63

914.83

218+87 Ent Rt.

219 Ent Lt. 3.7 14.9 14.91

July 27, 1970

Rt.

7

Lt.

34.5	35.6	36.5	37.8	38.1	38.5
8.9	7.8	6.9	6.2	5.3	4.9
52	41	37	26	12	
Ent					

38.30	37.1	33.9	36.1	37.8	38.3	38.7
11.1	10.3	9.5	7.3	6.2	5.1	4.7
60	52	43	32	24	12	
Ent						

30.0	31.3	35.8	36.8	37.3	38.5	38.8
3.4	12.1	8.2	7.2	6.1	4.9	4.6
65	52	41	31	23	12	

Top Hyd Lt. Sta 210+60

Top West Edge M.H. Rt. Sta 219+35

15.3	15.0	15.4	15.8	16.4	17.2
5.3	5.6	5.2	4.8	4.2	3.4
13	14	36	53	68	

14.8	14.6	14.7	15.1	14.9
5.8	6.0	5.9	5.5	5.7
65	51	31	13	

Sta + π - Elev,

920.63

219+16 Ent Rt

T.P. 9.42 911.21

T.P. 4.36 908.43 904.07

25 $\pm$ 6.90 901.53

254+50

BM 10.31

T.P. 4.30 890.69 886.39

267+46 Ent Lt ?

269+41 Ent Rt

270 $\pm$ 5.35 891.04 5.00 885.69 85.67

Lt

~~£~~ July 23, 1970 Rt 8

14.5	14.2	14.5	15.2	16.8	18.3
6.1	6.4	6.1	5.4	3.8	2.3
13	14	27	53	78	

Spike in P.P. Rt sta

Sta 224 £

03.0	03.0	03.2	03.9	05.4	07.5
5.4	5.4	5.2	4.5	3.0	0.9
13	14	26	50	78	

Spike in P.P. Rt Sta 225

Spike in PP Rt Sta 270+50[±]

81.8	83.7	83.4	83.6	83.4	84.4
59	70	73	71	73	6.3
38	27	24	13.5	13	

86.3	87.6	89.4	90.4
4.4	3.1	1.3	0.3
50	58	68	72

85.4	86.1	85.7	85.5	85.2	85.6	84.5
5.3	4.6	5.0	5.2	5.5	5.2	5.8
14	23	35	50	83	95	

Sta + π - Elev.

891.04

271+98

86.44

BM. 5.34 891.37

886.03

276+04 Valentine Ave 48 85.1

BM 4.67 890.61 5.43 885.94

279+49 Bit Ent Lt.

Lt.

± July 27, 1970
RT

9

86.4	86.3	86.2	85.9	85.9	86.0
4.6	4.7	4.8	5.1	5.1	5.0
	13	28	39	48	62

Ch-T

RT
~~Left~~

Spike in PP. ~~Sta~~ Sta 276+55±

85.1	85.6	85.9	86.5	86.6
6.3	5.8	5.5	4.9	4.8
100	60	33	12	

84.6	84.77	84.8	84.8	85.3
6.8	6.60	6.6	6.6	6.1
150	193	200	250	300

MH

Top Hyd N.W. Corner Valentine Ave & Snelling

87.3	86.0	84.7	84.7	85.2	85.5
3.3	4.6	5.9	5.9	5.4	5.1
66	52	37	26	12	

87.7	90.61
2.9	0.00
84	116

Conc.

Sta + Δ - Elev.

890.61

280+00 Ent Lt.

BM 4.56 886.05 (886.05)

BM 4.60 886.01

BM 6.05 884.56

BM 6.72 898.25 891.53

286+83 Ent Lt

287+07 Ent Rt

287+50 $\neq$ Check 4.82 893.43 93.44

Lt

July 23, 1970
Rt

10

89.5 87.7 86.2 84.9 84.7 85.1 85.3
 11 29 44 57 59 55 53
 79 66 55 42 26 12

Top Hyd Lt Sta 280+50±

Spike in PP Rt Sta 276+55

Spike in P.P. Lt Sta 276+25±

Spike in PP Lt Sta 286±

97.8 97.0 95.7 94.2 92.3 92.7 92.8
 05 13 26 41 60 56 55
 85 79 70 58 41 12

93.1 93.0 92.7 92.98 92.7
 5.2 53 56 5.27 5.6
 12 26 52 75
 NH

Sta	+	π .	-	Elev.
BM	687 3.87	8 895.05		891.18

294+80			5.52	892.53 889.53
--------	--	--	------	-----------------------------

295			4.96	893.09 890.09 (93.09)
-----	--	--	------	-------------------------------------

296			5.31	892.74 889.74 (92.79)
-----	--	--	------	-------------------------------------

BM	6.46	900.93		(894.47)
----	------	--------	--	----------

302+58

302			6.70	894.23 (94.25)
-----	--	--	------	---------------------------

303			4.98	895.95 (95.96)
-----	--	--	------	---------------------------

BM	7.20	913.37		(906.17)
----	------	--------	--	----------

308+84

FX
BP
CP
CM

July 30, 1970

11

Spike in P.P. Lt Sta 294+75[±]

± Double Doors on Pump Ho 70' Lt

Spike in P.P. Lt Sta 303+80[±]

96.9	96.2	95.5	95.5	95.4
4.0	4.7	5.4	5.4	5.5
91	78	60	39	20

spike in
Top Guard Rail post Rt 307+80[±]

07.2	06.4	05.4	05.0	04.6	05.4
6.2	7.0	8.0	8.4	8.8	8.0
76	50	31	15	13	

Bit

Sta + π - Elev.

913.37

310+52 Ent Lt (Bit)

TP 10.60 918.04 5.91 907.46

313 6.07 911.99 12.00

313+52 Ent Lt

314 4.70 913.36 13.37

315+16

TP

+32 4.72 918.00 4.78 913.28

317+07 Ent Lt

318 6.38 911.62 19.63

318+16 Ent Lt

✓
T.P. 6.70 915.54 9.16 908.84

Lt

July 30, 1970

Rt

12

10.2	09.7	08.3	07.8	07.2	06.1
32	37	51	56	62	53
76	54	32	15	13	

S. Edge MH 29' Lt 311+25

10.3	11.0	11.9	12.7	12.6	12.8
28	71	62	54	55	53
75	57	35	18	13	

12.5	13.0	13.5	14.0	14.1
56	51	46	41	40
78	55	30	13	

Rt

MH S. Rim 24' Lt

13.9	13.8	13.4	13.1	13.2	13.0	13.03
42	42	46	49	48	50	497
100	79	54	31	14	13	

11.5	11.2	11.1	11.4	11.8	11.4
65	68	69	66	68	66
75	55	32	13	12	

Beautiful lawn + Ent.

12.0
6.0
100

+32 Lt 24' MH S. Rim

Sta + π - Elev.

915.54

321+89 Ent Lt

✓

323

4.93 910.61

(10.60)

323+13

324+00 in Ent Lt 4.18 911.36

(11.31)

July 30, 1970

13

Lt

£

Rt

07.68	08.3	09.3	09.7	09.5	09.62
7.86	72	62	58	60	5.92
71	46	26	14	13	

conc

07.48	07.44
8.06	8.10
96	100

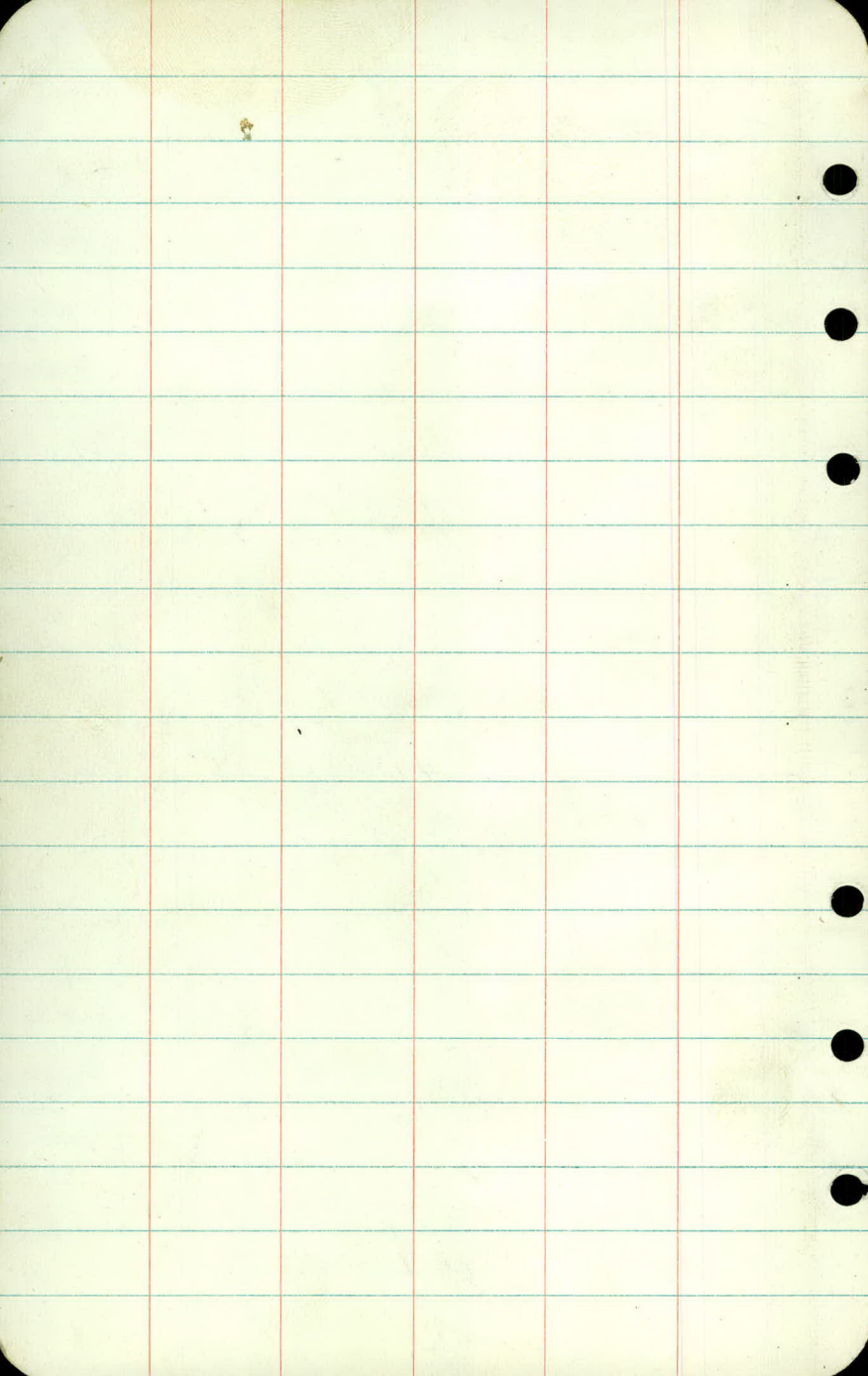
Joint

11.13	10.80	10.6	10.8	10.6
4.41	4.74	4.9	4.7	4.9
76	48	33	14	13

conc Bit

15.3	14.9	14.3	12.9	11.2	11.2	11.36
32.06	1.2	26	4.3	4.3	4.18	
191	73	57	35	15		

Garage



March 10, 1971 1

62-676-01

POND CONTROL

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	5.48	903.67		898.19
----	------	--------	--	--------

$\pm$ Rd + $\pm$ RR		7.08		896.59
---------------------	--	------	--	--------

Ice		9.67		894-
-----	--	------	--	------

Top of Gauge		8.08		895.59
--------------	--	------	--	--------

Stump		9.03		894.64
-------	--	------	--	--------

Water Surface		9.76		893.91
---------------	--	------	--	--------

5.9' Deep & Wet!!!
Frank Fell in

Stump		8.38		895.29
-------	--	------	--	--------

		9.09		894.58
--	--	------	--	--------

"		9.18		894.49
---	--	------	--	--------

Stp East		7.15		896.52
----------	--	------	--	--------

Ice E side		9.67		894-
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BM		5.93		897.74 (897.78)
----	--	------	--	-----------------

FX
KG

March 10, 1971

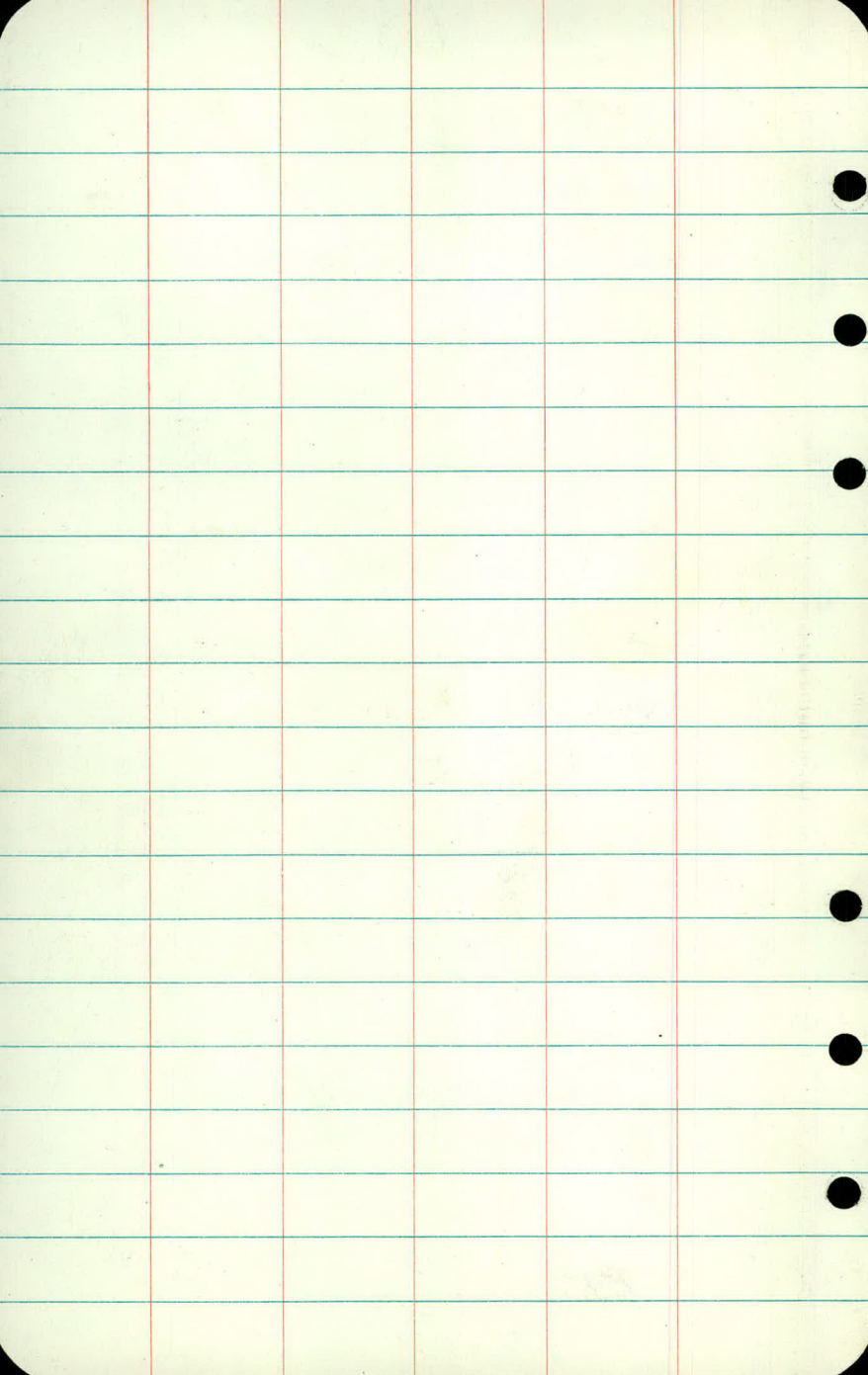
2

Top S.W. Corner 2nd Rail East Side ^{Bridge}

1' Above 1' Mark

I would recommend pond
to be controlled at an elevation
of 89' 3" 00 feet above
sea-level
JF

Spike in PP 200' S of RR E. Side



FK
GA

April 21, 1971

1

76 Turnback

Sta	+	π	-	Elev.
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223		3,25909.34		906.09
-----	--	------------	--	--------

W.S. Pond			13.69	895.65
-----------	--	--	-------	--------

224			5.28	904.06 (904.07)
-----	--	--	------	-----------------

FK
GA

April 21, 1971

2

£

Pond South of R.R. tracks W. of Snelling

