

OFFICE OF COUNTY ENGINEER
RAMSEY COUNTY, MINN.

PLAN

Survey

DALE STREET

From Lar penteur To T. H. #36

Road Acc't. No. 62-653-01

Date Filed 4-28-64

DR. 10
File BK. 101

1
DALE ST.

Larpenteur to "B"

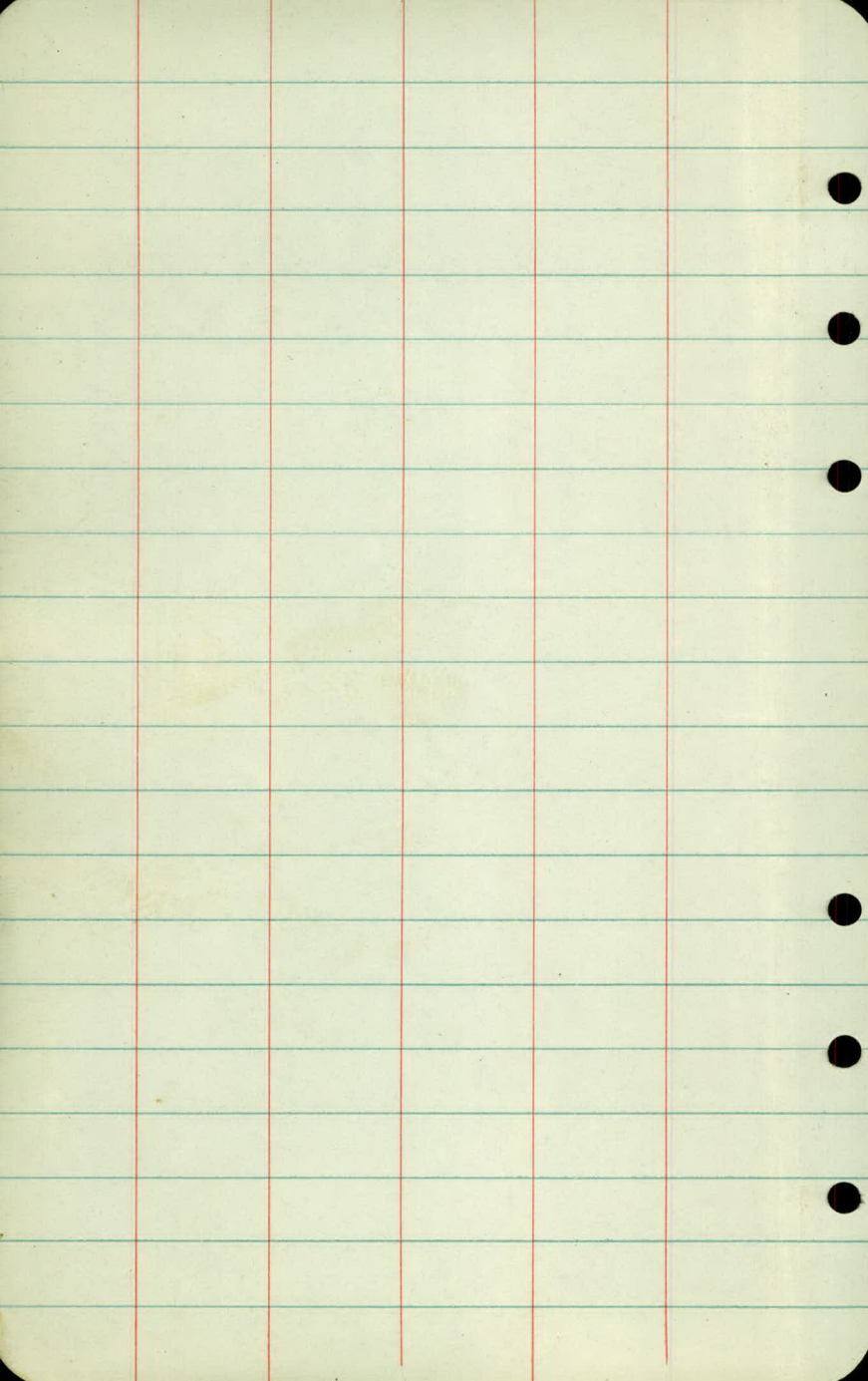
CO. RD. "B"

Alinement 2-

ROSELAWN

Arch

LARPEMTER



Dec. 6, 1963

2.

Alinement

Sta Point Δ Lt. Δ Rt.

8+59.79

6+54.0

6+53.04

5+69.15

4+20.3 P.O.T.

0+00 S.W. Cor. Sec. 13-29-23

Dec. 6, 1963

3

±

Spike

Iron

33'

Iron

Iron

9.7 Br H
12.1 2 1/2
0 147.66

95

West

□ Pillar

81.70
89° 47' 22 1/2"

Center
Signal
Light

36.62

Brass
Mont.

63.38'

Hyd

Sta Point Δ Lt. Δ Rt.

26+11.78 P.I. $0^{\circ}35'$

18+71.51

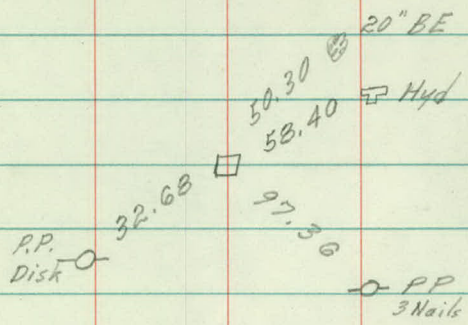
14+34.64

11+61.8

FK
JS
FS
PS
RB

Dec 9, 1963
~~E~~

4



Mont.

Spike

Spike

Spike

33'

Sta Point Δ Lt. Δ Rt

33 + 99.58 1 km

+98.66 P.O.T.

Dec. 10, 1963

5

Iron 0 33'

R.R. spike

Sta Point ΔL ΔR

52+36.56 P.I.

0°02'

37+24.38 P.O.T.

Dec. 11, 1963

6

±

PP

○

53.09

Hyd

±

48.00

± Co. Rd. "B"

PK
17.12
PK

○

Manhole

38.18
~~33.22~~

48.58
~~41.55~~

PP
DISC

PP
○

#629

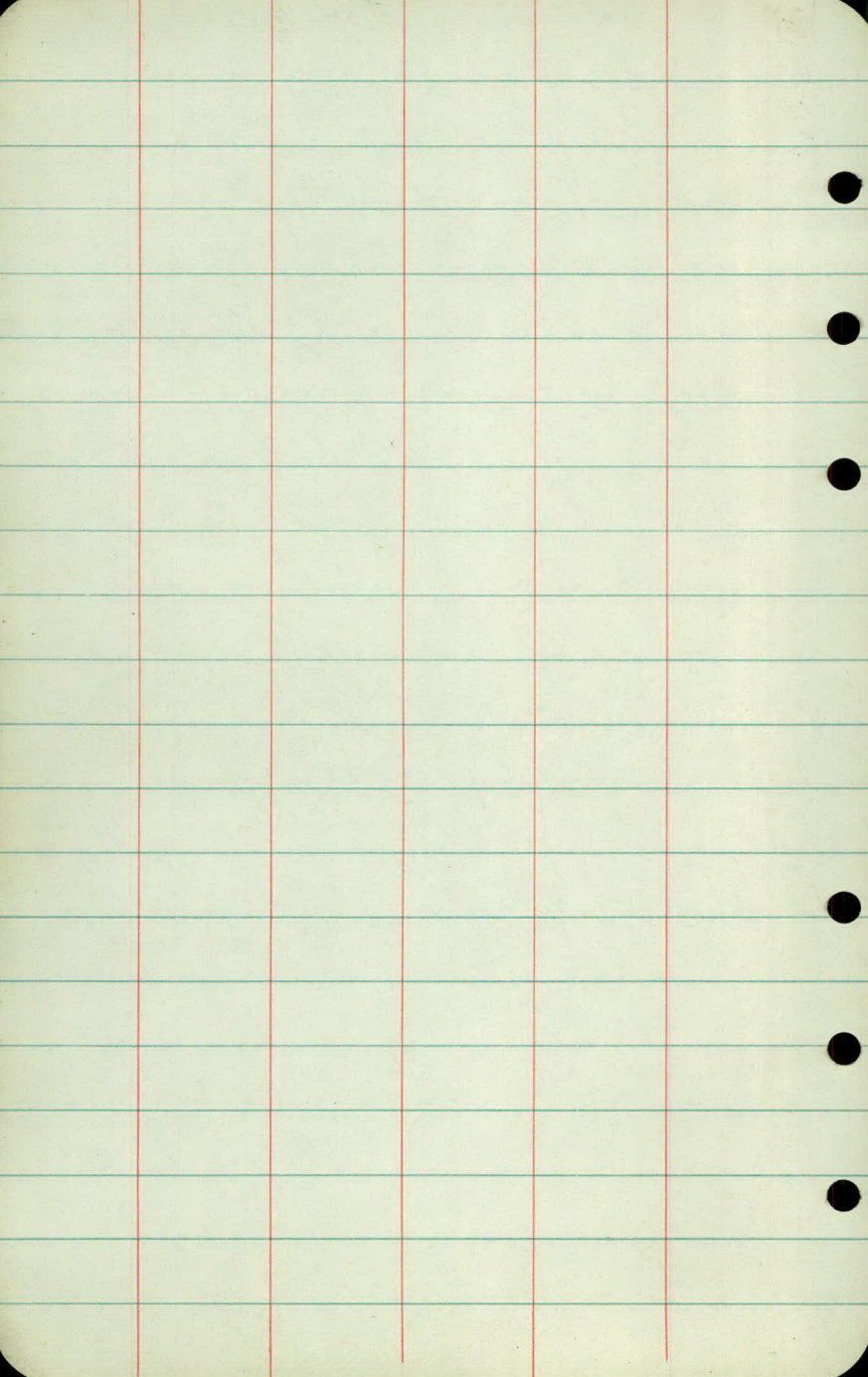
Stryer

65.58'

PK Nail

68.73

±



FK
JS
FS
DS
TL

Feb. 13, 1964

1

Topography

N.W. Cor Dale & Larpenteur

Base Line
Section on opposite

+53 SE Cor Gar
122

+146 ER
30.5

+53 Cor. BT & 7
40.5 + 166

+142 BR
40.5

2+100

+09 BR
30.5

+14 ER
40.5

+16 SW Cor Bldg
72.5

+36 Corners of Conc
40.5

+149 ER
30.5

+21 Cor Conc
68

+33 5' Walk
68

+36.4 6' Walk
67

+113 SE Cor Bldg
173

+113 Cor Bldg
103

+26 Crosspool
16A

+32 BT
169 + 189

+20 W50
167

+23 Tank Cover
117

+109 PP
142

+109 BT
162

+09 Cor Conc
75

+109 Cor BT 4.5' Walk
83

+109 Cor Conc
103

+15 Tank Cover
117

+108 W. E Island
53.2

+10 Angle in Conc
52

+104 Cor BT
325

+106 FOR
37

+105 Cor Conc
40.5

1+100

+100 B.R.
30.5

+100 Cor Conc
75

+80 Cor Conc
44

+conc. base
Ctr 4' Sign

+93 E. E Island
61

+96 Tank Cover
98

+74 35

+160 PP
34.5

+166 Tell Booth
42.5

+157 Signal
34.5

+55 Pull Box
36.5

+71 Edge B.T.
47

Curb

+51 41.5

+156 Curb
48.0

+152 Curb
35.5

OR

+72.5 29.4

+162 BR
30.5

Mont

+100

6100

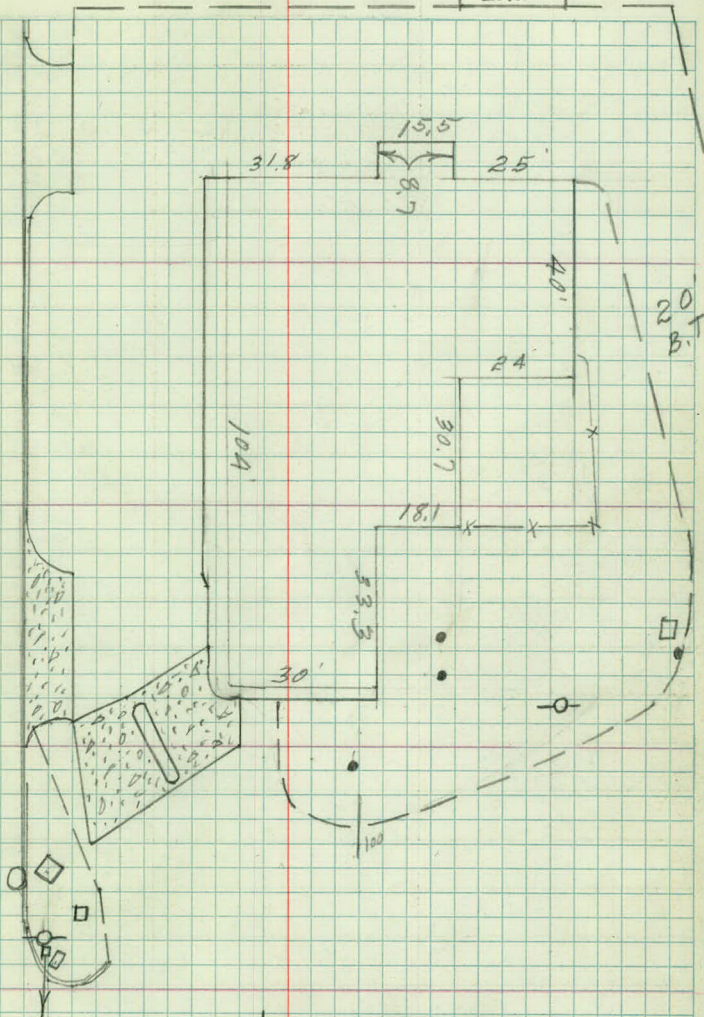
→ 2

NS EW
Ga 20.2 x 22.2

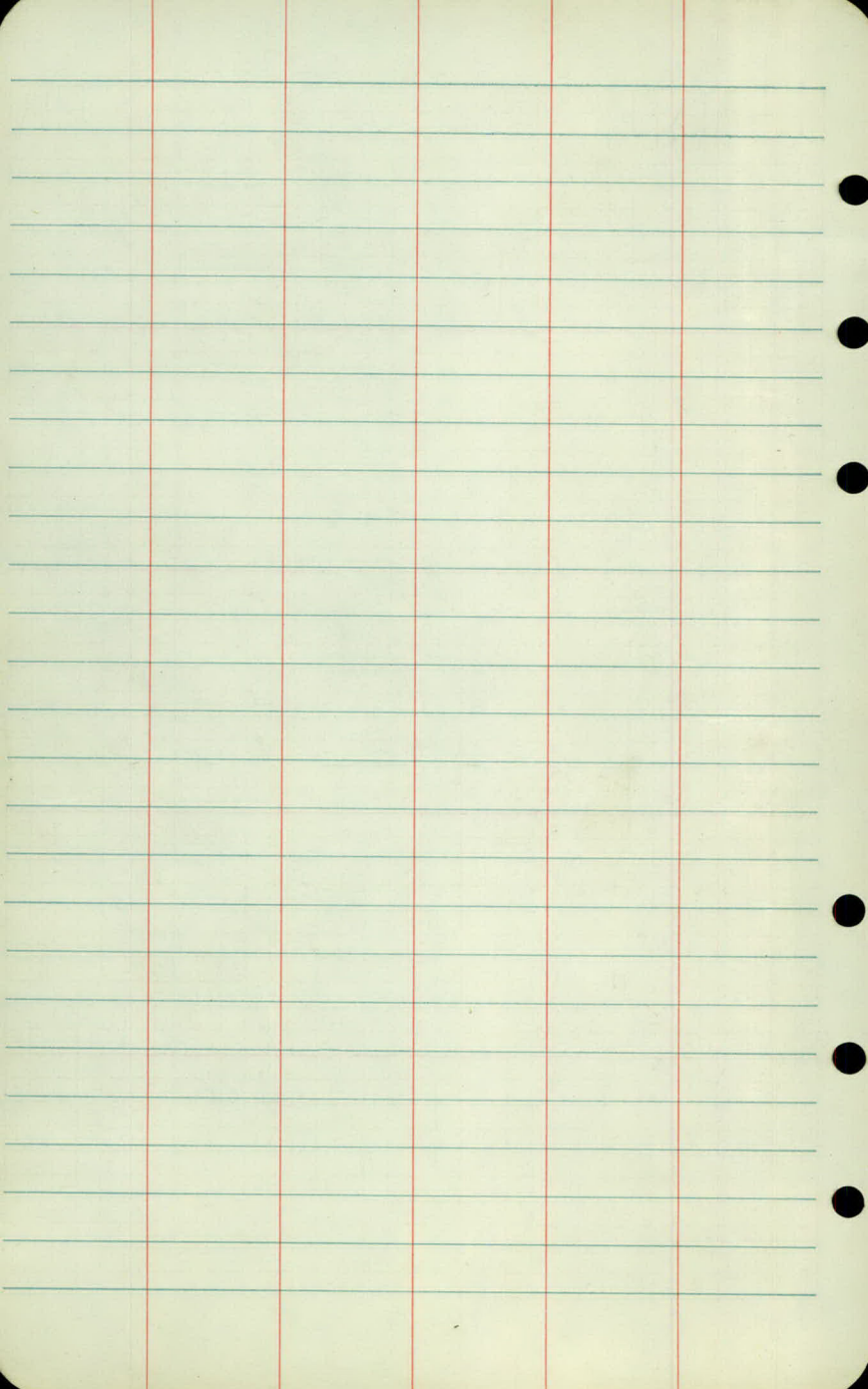
20.2

2

Section line A



± Date St



Dec. 12, 1963

7

TOPOGRAPHY

£

10" S.P.
+45 45

PP
+22 32

Fe
+100 33

4" W
+94 31

30" M
+69 41

8" E
+49 41

MH
+21 32.7

28" M
+30 41

Road
69 - 29

Fe
+100 33

24" M
+92 41

Curb at Pillar
+69 59

W. Dept. Mast
+91 28

MH (w)
+64 46

MH
+62 20

26" E
+82 58

Pillar
+75 54

Gate V
+58 28

B. Fe
+78 33

Ch. 7" R Curb
+45 27

T. Post
+41 66

D-X Sign
+34 75

PP
+74 31.4

Pillar 22x
+75 33

PP
+33 61

Brick MH
+70 39.4

Signal
+32 58

Rd
+55 4

Strip PP
+59 31

Sig. Cont. Box
+60 30

End Conc
+30.7 Lt

End Conc
+31.2 Rt

E. R.C.
+42 56

Gate V
+30 9

MH
+15 16.5

Red. Sig. Button
+41 26

B. R.C.
+25.5 41

Por
+36 51

Edge Header
+100 40.7 - 42.7

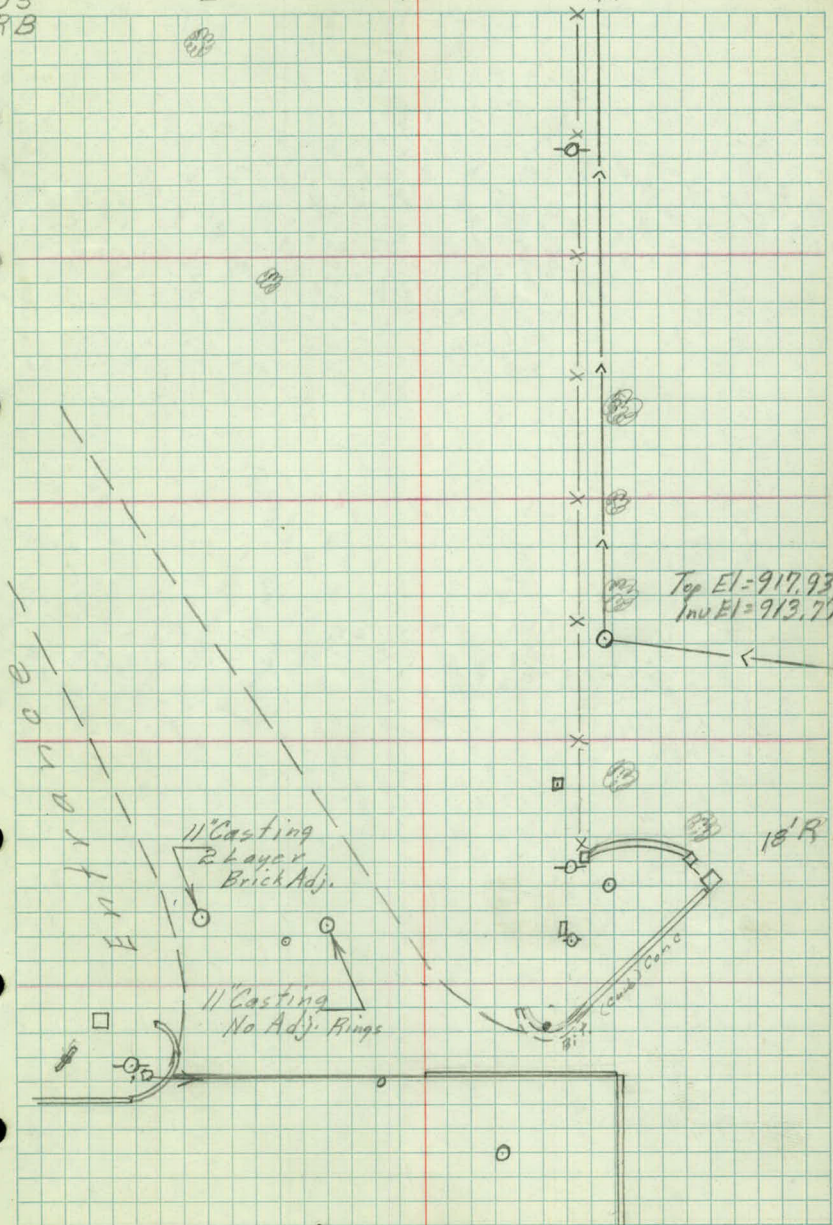
0

3

27

 $\mathcal{L}$

Rt.



Rt.

5

$$\frac{\text{Fe}}{32.5}$$

+84 SEC Ho
107

$$+96 \frac{10'' E.}{72}$$

+94 NW Gr Crypt
50

483 SECOR Fire
Place 46

467 $\frac{2''}{1}P$

$$+ 74 \cdot \frac{x - Fe}{26 - 32.5}$$
$$+ 62 \frac{1'' P}{1}$$

• Sk. Cor No
+24 76

$$\begin{array}{r} +53 \quad 6^{\circ}\text{E} \\ \hline 38 \end{array}$$
$$+66 \frac{1''P}{4}$$
$$+19 \cdot \frac{2^{\text{nd}} \text{ Apple}}{25}$$
$$+15 \cdot \frac{PP}{1}$$
$$\frac{415 \text{ E.Fe}}{12}$$

461 $\frac{1}{4}$

+14 Hedge 3451

+02 Clothes Pole
23

$$+10 \frac{1''P}{18}$$

4	+04 $\frac{2''P}{16}$	+09 $\frac{4-1''\text{Apk Fe}}{5-413.22}$	$\frac{32.5}{32.5}$
---	-----------------------	---	---------------------

+99 $\frac{3''NP}{9}$

$$+92 \frac{4'' \text{ N.P.}}{9}$$
$$+75 \cdot \frac{8''M}{15}$$

181	Wood Rail Fe
	11.2 - 30.4
No	(Cor.)

+68 $\frac{PP}{32}$

457 SECor No
56

46 + \$30 Walk
45

+54 $\frac{4 \text{ Locusts}}{34}$

+34 End 9 Conc Ent

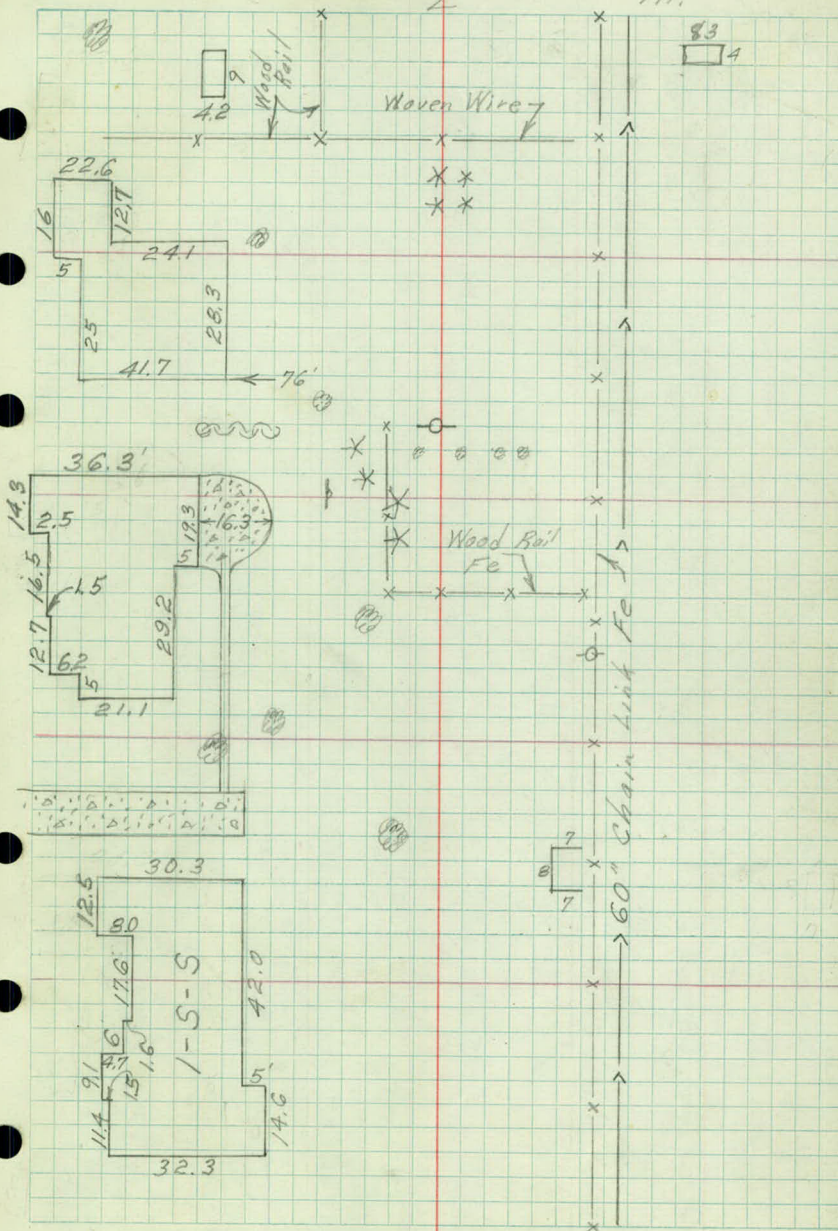
48. 7" Catalpa
47

$$+29 \frac{S.P. 18''}{9}$$

4/19 SW. Co. Utility
Shelter 23

3				1 e
				32.5

+64 SE Cor Ho
36.3



£

$$\begin{array}{r}
 +45 \frac{26^{\circ}0}{32} \\
 +50 \frac{20^{\circ}0}{58} \\
 +35 \frac{8^{\circ}0}{77} \\
 +15 \frac{18^{\circ}0}{23}
 \end{array}$$

7

$$+100 \frac{\text{End Woods}}{1 \rightarrow \text{RT}}$$

$$+82 \frac{\text{Woods}}{1}$$

$$+56 \frac{36^{\circ}W}{16}$$

$$+59 \frac{\text{Cor Woods}}{42}$$

$$+12 \frac{\text{Cor Woods}}{10}$$

$$\begin{array}{r}
 6 \\
 +89 \frac{16^{\circ}0}{1} \\
 +17 \frac{14^{\circ}0 \text{ CH}}{33} +69 \frac{8^{\circ}BE}{30} +83 \frac{8^{\circ}0}{24} \\
 +35 \frac{E. Hedge}{40} +47 \frac{6^{\circ}BE}{19} +36 \frac{\text{Unlabeled}}{44 \text{ SE Cor}} \\
 +26 \frac{Tw 12^{\circ} CH}{35} +34 \frac{6^{\circ}BE}{22} +26 \frac{\text{Hedge}}{11-23 \text{ (Cor)}}
 \end{array}$$

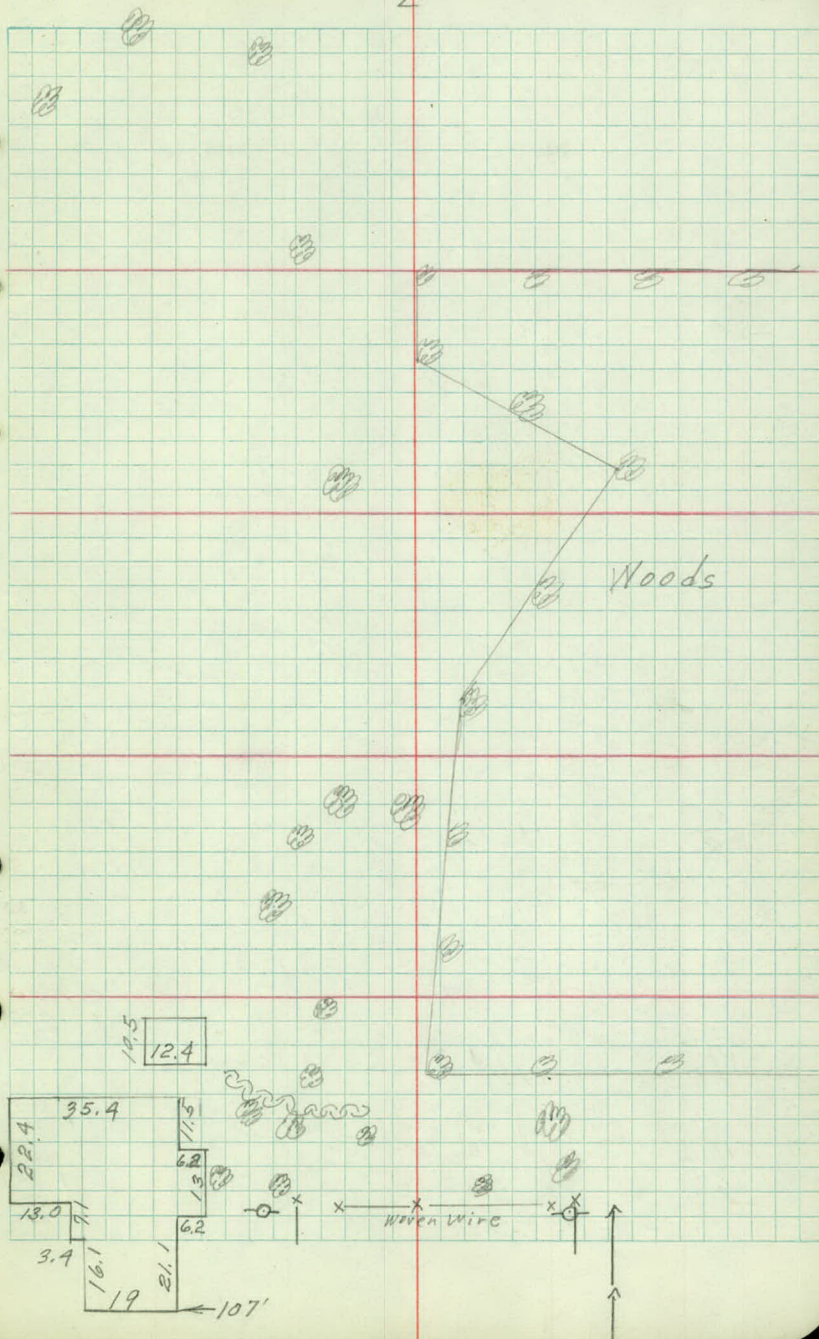
$$\begin{array}{r}
 +13 \frac{12^{\circ}CH}{42} +23 \frac{6^{\circ}BE}{26} +21 \frac{4^{\circ}BE}{10} \\
 +11 \frac{8^{\circ}CH}{29} +16 \frac{34^{\circ}0}{31}
 \end{array}$$

$$\begin{array}{r}
 +34 \frac{\text{Bay Woods}}{\text{RT. 2} \rightarrow} \\
 +26 \frac{Tw 8^{\circ}0}{29}
 \end{array}$$

$$\begin{array}{r}
 +08 \frac{E. Fe}{25} +07 \frac{X-Fe}{17-28} +11 \frac{4^{\circ}W}{13} \\
 5 +06 \frac{PP}{32} +08 \frac{E. Fe}{32.5} +06 \frac{PP}{32}
 \end{array}$$

Dec. 12, 1963

10



10

Lt

E

Rt

$$+43 \frac{\text{Woods}}{65}$$

$$+30 \frac{\text{Woods}}{2}$$

$$+20 \frac{\text{B. Woods}}{20}$$

9

$$+79 \frac{18''0}{72}$$

$$+65 \frac{3-4''0}{70}$$

$$+60 \frac{\text{X.Fc}}{34}$$

$$+55 \frac{1''NP}{36}$$

$$+45 \frac{1''NP}{36}$$

$$+50 \frac{1''WP}{44}$$

$$+41 \frac{2''WP}{44}$$

$$+13 \frac{26''0}{54}$$

$$+36 \frac{2''NP}{36}$$

8

$$+07 \frac{3''Appl}{76} \quad +07 \frac{\text{SECOND HILLY}}{104}$$

$$+92 \frac{\text{Tw } 16''0}{66}$$

$$+96 \frac{16''0}{83}$$

$$+72 \frac{6''E}{45}$$

$$+67 \frac{18''0}{67}$$

$$+67 \frac{12''0}{59}$$

$$+58 \frac{16''0}{82}$$

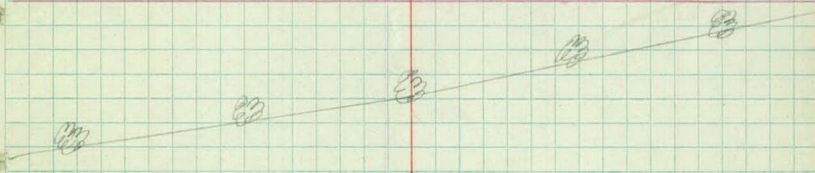
FK
JS
FS
DS
RB

Lt.

Dec. 12, 1963
± Dec. 17, 1963 Rt.

11

Woods



Chain Link 7



N 10.25
E 11.1W



Lt.

E

Rt.

+17 $\frac{12''P}{71}$

12

+84 $\frac{\text{Begin Woods}}{\text{Lt + Rt}}$ +69 $\frac{\text{Row 3 Pine}}{\leftarrow 58}$ +79 $\frac{12''P}{54}$ +51 $\frac{14''P}{76}$ +42 $\frac{12''P}{62}$ +43 $\frac{6''P}{74}$ +35 $\frac{13''O}{56}$ +02 $\frac{\text{End Woods}}{\leftarrow 14}$

11

+93 $\frac{\text{Cor. Woods}}{7}$ +40 $\frac{\text{End Woods}}{19-74}$

10

Lt.

Dec. 17, 1963

12

Rt.

Pine Forest

WOODS

WOODS



15

Lt. $\frac{Fe}{0.5}$ $\frac{Woods}{6}$ Rt. 6

14

+100 $\frac{Fe Cor}{0.5}$ $\frac{Woods}{10}$

+83 $\frac{Woods}{13}$

+57 $\frac{Woods}{34}$

+40 $\frac{Woods}{91}$

+105 $\frac{Woods}{2}$

+100 $\frac{Fe Cor}{0.5}$

13

+88 $\frac{End Woods}{100 - 40}$

Lt

E

Rt

17

$$\frac{Fe}{0.5}$$

$$\frac{Woods}{2}$$

$$\frac{NE Co Ho}{+54 \quad 77}$$

16

$$\frac{Fe}{0.5}$$

$$\frac{Woods}{2}$$

$$\frac{SE Co Ho}{+83 \quad 79}$$

$$\frac{+59 \quad Woods}{2}$$

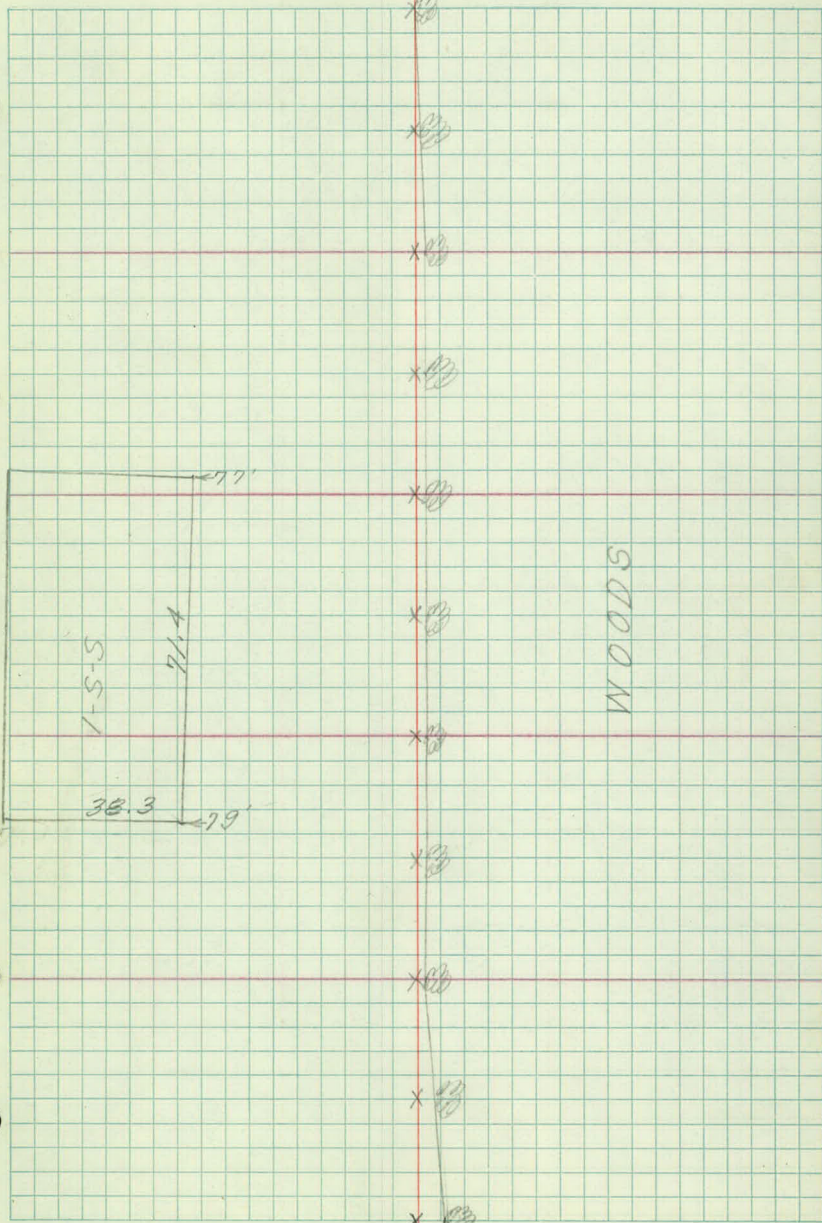
15

Lt.

Dec. 13, 1963

Rt

14



20 Lt. $\frac{Read}{75-33}$ $\frac{Fe}{2}$ $\frac{Woods}{50}$ Rt.

+94 $\frac{Woods}{100}$

+70 End Nursery
22 - 7

+28 $\frac{GP}{49}$

19 $\frac{Berm}{Read}$ Nursery $\frac{Fe}{0.2}$ $\frac{Woods}{120}$
67 50-8

+80 $\frac{26^0}{4}$

+82 $\frac{MH}{59}$

+64 $\frac{4^0P}{72}$

+53 $\frac{4^0P}{60}$

+50 $\frac{Woods}{110}$

+25 Begin Nursery
55-9

+44 $\frac{4^0P}{61}$

+45 $\frac{26^0}{85}$

+14 $\frac{Cor Woods}{2}$

+100 $\frac{B. Woods}{108}$

+19 $\frac{12^0 WP + Cor Woods}{16}$

$\frac{Woods}{2}$ $\frac{Fe}{0.5}$

+100 $\frac{14^0 WP + E. Woods}{60}$

18

Dec. 17, 1963

15

Rt. 100

Lt.

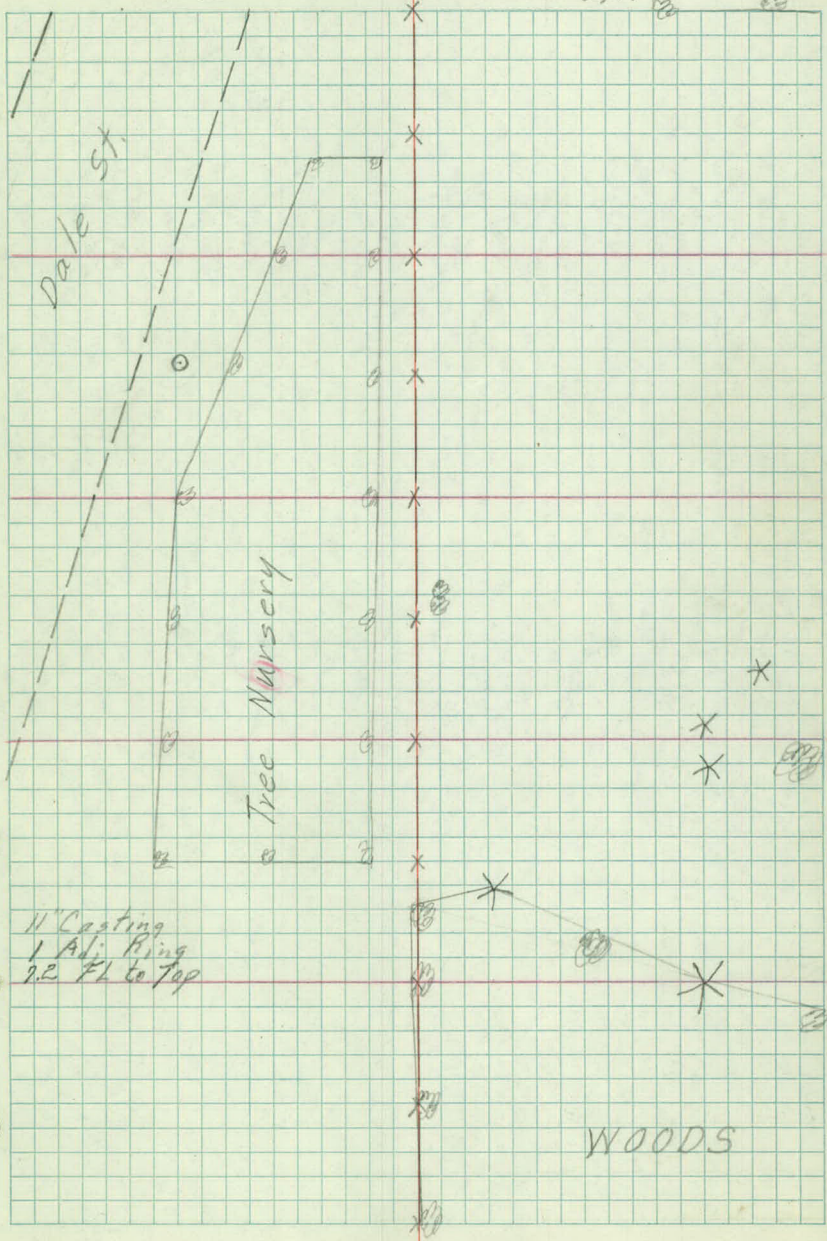
4

Date St.

Tree Nursery

11" Casting
1 Adj. Ring
2.2 FL to Top

WOODS



LT.

£

Bt.

$$\begin{array}{r} 14' A_{11} \\ + 40 \frac{14''}{43} \\ \hline 132 \frac{E.7 R_{100}}{50} \end{array}$$

$$\begin{array}{r} 14'' P \\ + 40 \frac{14''}{29} \\ \hline 107 \frac{14''}{85} \end{array}$$

$$\begin{array}{r} 12'' P \\ + 10 \frac{12''}{49} \\ \hline 103 \frac{12''}{49} \end{array}$$

$$\begin{array}{r} 2 E_{11} \\ + 16 \frac{2 E_{11}}{16} \\ \hline 16 \end{array}$$

$$\begin{array}{r} Fe \\ 41 \end{array}$$

$$\begin{array}{r} R_{100} \\ 27-9 \end{array}$$

$$\begin{array}{r} Fe \\ 30 \end{array}$$

$$\begin{array}{r} 22 \end{array}$$

$$\begin{array}{r} 184 \text{ MH} \\ +63 \text{ Tw 6 WP} \\ \hline 247 \end{array}$$

$$\begin{array}{r} 160 \text{ Woods} \\ +64 \\ \hline 224 \end{array}$$

150	PP 41	150	R. Tie MO	140	GP TO
146	R. Fe 49	123	Woods 33		
51	Begin 7-pine shrubs 57				
21		Road 43-4	Fe 10	Woods 29	

	+56	MH					
		12.5					
+33	Arche		+57	55	+73	10" WP + Cor Woods	
68					24	→ 95	
	+24	GP					
		12			+27	4" WP + Cor Woods	
					48	→ 100	

20

Dec. 17, 1963

16

Lt

Rt.

1-S-B+5
24.5
29.4

60" W. W. →

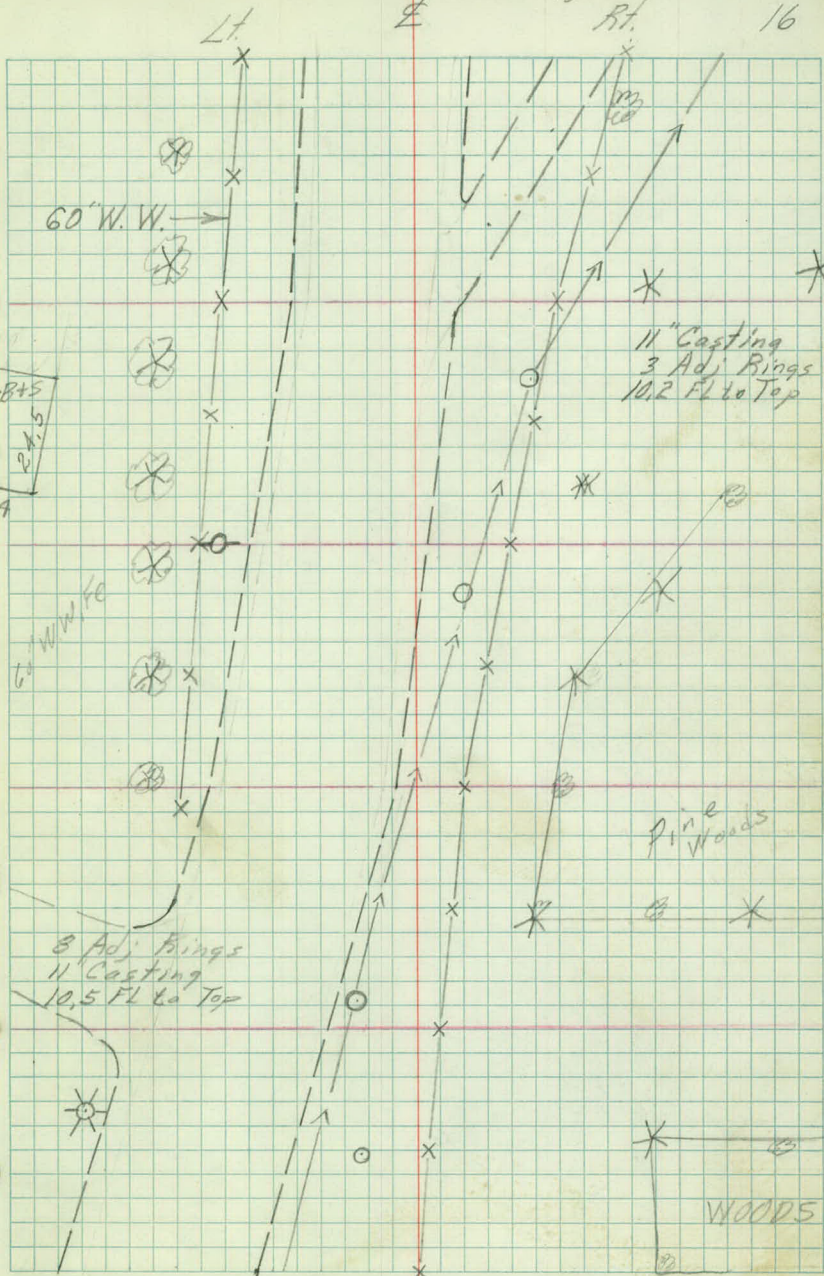
11" Casting
3 Adj. Rings
10.2 FL to Top

6" W. W. Fe

Pine Woods

8 Adj. Rings
11" Casting
10.5 FL to Top

WOODS



25

Lt. Fe 36 Road 17-19 Fe 46 Rt.

PP
+45 27

+07 16" A
64

24

Fe 33 Road 18 18 Fe 49

+9 Tw 14" A
75

+80 4" A
54

+80 3-A BE
39

Basin Broken
+67 34 Fe

+71 26" O
64

+50 14" A
49

+50 Tw 14" A
60

+42 14" A
51

+28 4" P_{an}
59

+33 A P_{an}
65

+42 14" A
48

23

Road
20 15 Fe 39

+Ent
60

+86 E Fe
43

+89 MH
87

PP
+86 27

+82 GP
23

+72 4" B
42

+74 4" B
43

L Fe
+70 35

+65 B Fe
34

+56 L Fe
45

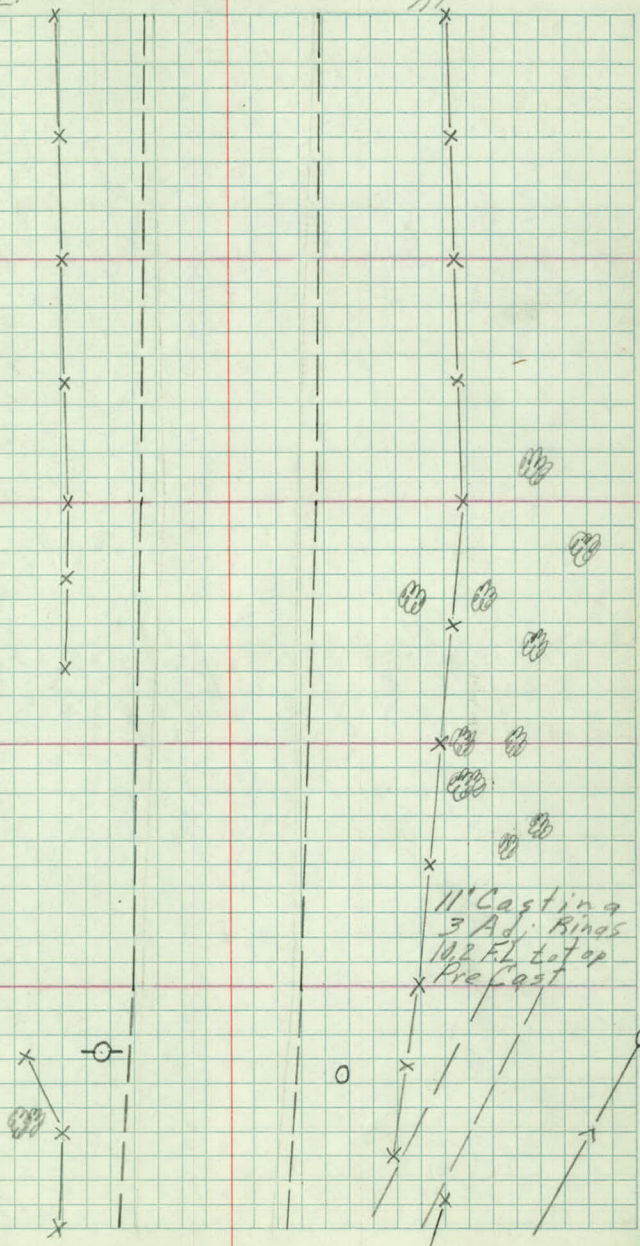
FK
JS
FS
DS
RB

Dec. 23, 1963

17

Lt

Rt



Lt.

±

Rt.

+42 14' 36"

+32 3' 69"

+35 14' 36"

+21 3' 56"

+14 E.E. 24' CM

+30 Pine Bu

+14 L. Wall

Fe Road
37 18-21

+17 Wall

+96 EEnt

+64 SW Cur Ho

+83 R. Tr

+11 EEnt

+56 E.R.

+69 W.E. 24' CM

+79 4' 50"

+45 POR

+82 2' 63"

+51 18' 44"

+70 10' 33"

+51 18' 54"

+50 L. Linc

+35 H. 35"

+54 30' BE

+34 8' E/m

+30 POR

+31 E. Linc

+10 Fe. Cor.

+21 BR

Road
16

26

+94 Arc Light

+99 ER

+91 PP

+90 POR

+79 Fe Cor

+73 POR

+42 BR

25

Lt.

Fe.

$$\begin{array}{r} \text{Road} \\ 22-23 \end{array}$$

Rt.

30

40

22-23

$$+15 \frac{PP}{29}$$

$$\begin{array}{r} \text{Pine Tree Fe Road} \\ 73 \quad 36 \quad 22-23 \end{array}$$

29

$$+82 \frac{4-4" BE}{44}$$

28

$$\begin{array}{r} \text{Fe Road} \\ 36 \quad 21 \quad 23 \end{array}$$

$$+68 \frac{PP}{29}$$

$$+61 \frac{12"E}{37}$$

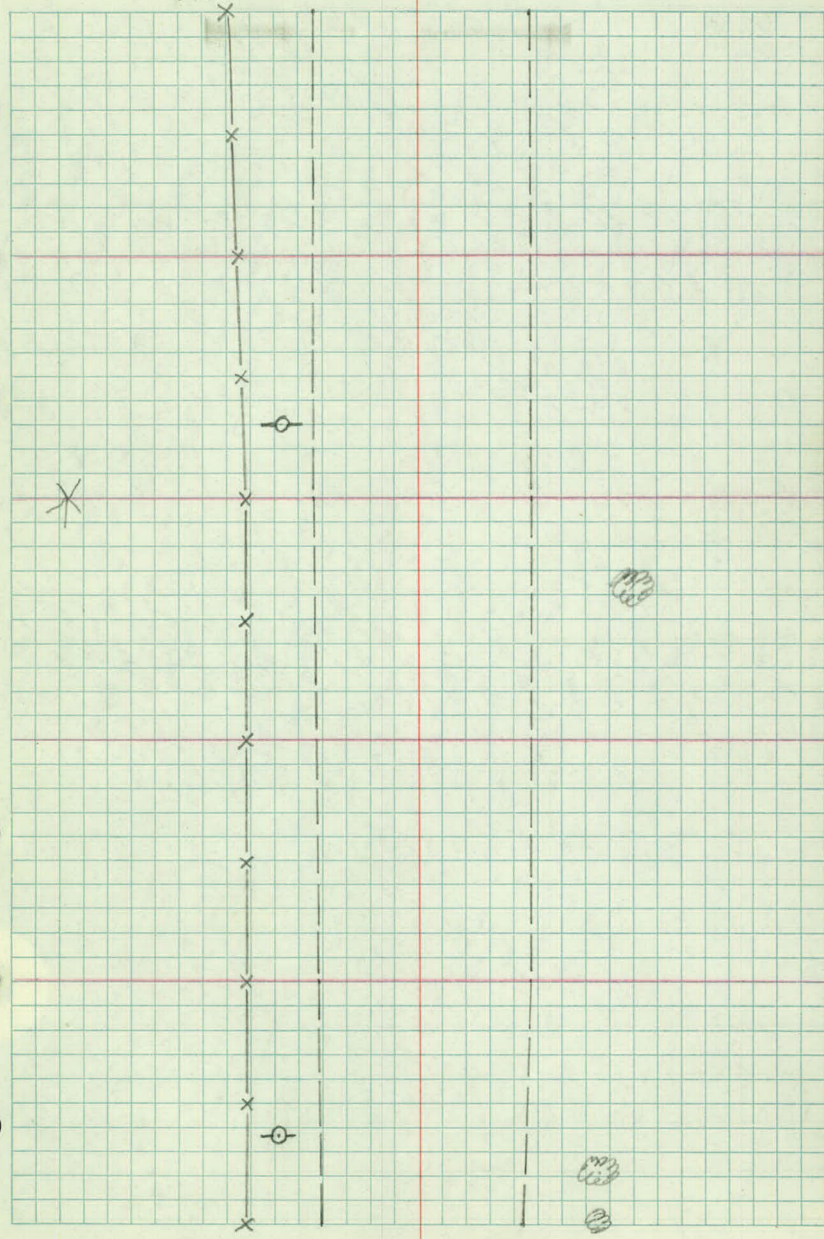
$$+51 \frac{4"E}{37}$$

Dec. 23, 1963

19

Lt.

Rt



Lt

£

Rt

+109 $\frac{PP}{29}$ +28 $\frac{Hqd}{46}$ +21 $\frac{ER}{21}$ 32 Pines Fe
66 40Road
23+20 $\frac{BR}{36}$ +88 $\frac{£ Ent}{70}$ +72 $\frac{BR}{20}$ +88 $\frac{ER}{48}$ +50 $\frac{£2' Walk}{45}$ +40 $\frac{N.W. Cor Ho}{22}$ +40 $\frac{Walk}{68}$ +18 $\frac{Angle in House}{77}$

31

Fe
43Road
22 21+61 $\frac{PP}{29}$ +85 $\frac{S.W. Cor Ho}{72}$ +57 $\frac{PP}{55}$

30

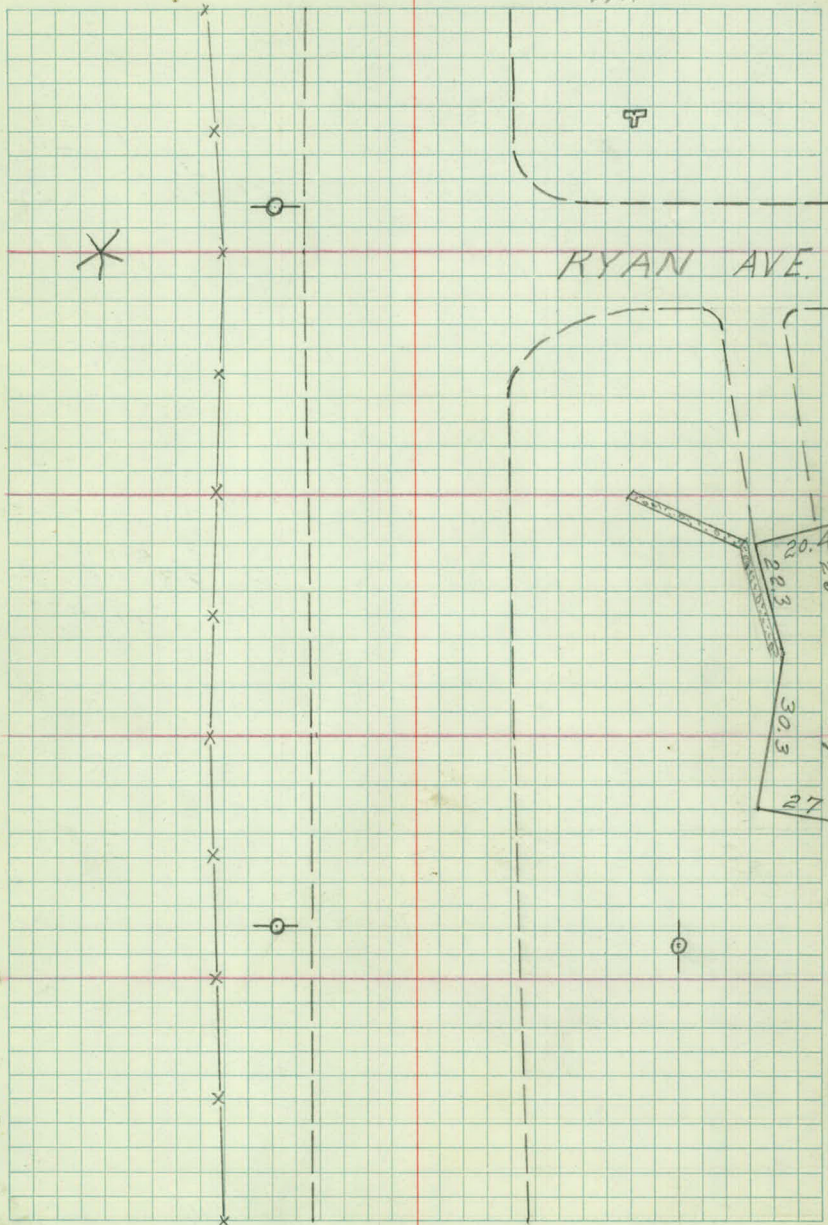
FK
DS
RB

Dec. 31, 1963

20

Lt.

Rt.



35

Lt.

$$\begin{array}{r} \text{Road} \\ 18 \end{array}$$

Rt

$$\begin{array}{r} \text{PP} \\ +170 \end{array}$$

$$\begin{array}{r} \text{WSO} \\ +66.5 \end{array}$$

$$\begin{array}{r} \text{GV} \\ +84 \end{array}$$

$$\begin{array}{r} \text{BR} \\ +94 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +69 \end{array}$$

$$\begin{array}{r} \text{BR} \\ +53 \end{array}$$

$$\begin{array}{r} \text{GP} \\ +64 \end{array}$$

$$\begin{array}{r} \text{Albivida} \\ +47 \end{array}$$

$$\begin{array}{r} \text{Albivida} \\ +37 \end{array}$$

$$\begin{array}{r} \text{2" Pine} \\ +36 \end{array}$$

$$\begin{array}{r} \text{Albivida} \\ +32 \end{array}$$

$$\begin{array}{r} \text{3" Pine} \\ +22 \end{array}$$

$$\begin{array}{r} \text{NWCov Ho} \\ +28 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 20 \end{array}$$

$$\begin{array}{r} \text{4" Pine} \\ +03 \end{array}$$

$$\begin{array}{r} \text{E. Wall} \\ +82 \end{array}$$

$$\begin{array}{r} \text{E. Walk} \\ +82 \end{array}$$

$$\begin{array}{r} \text{E. Conc Ent} \\ +75 \end{array}$$

$$\begin{array}{r} \text{SWCov Ho} \\ +70 \end{array}$$

$$\begin{array}{r} \text{PP} \\ +54 \end{array}$$

33

$$\begin{array}{r} \text{Pines} \\ 70 \end{array}$$

$$\begin{array}{r} \text{Fe} \\ 47 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 22 \end{array}$$

$$\begin{array}{r} \text{SW Cov Ho} \\ +66 \end{array}$$

$$\begin{array}{r} \text{E. All Ent} \\ +50 \end{array}$$

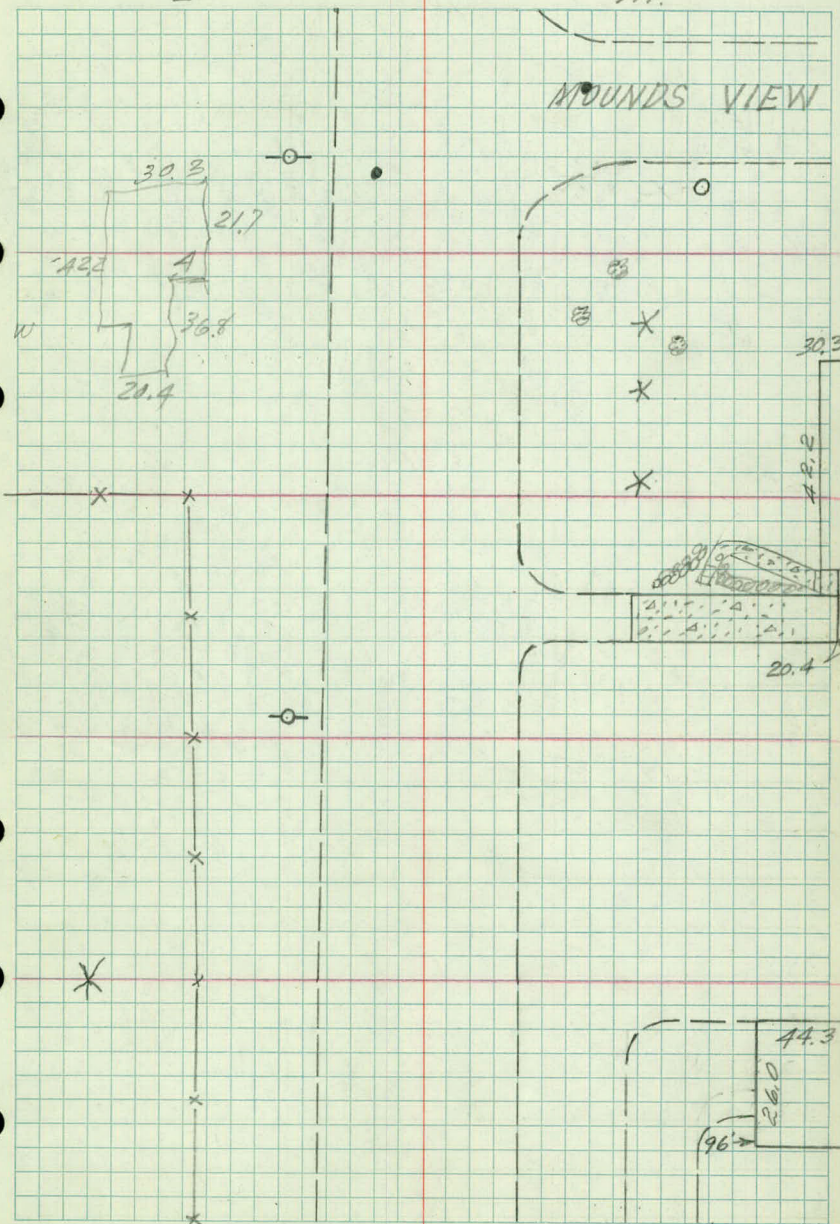
Dec. 31, 1963

21

Lt.

Rt.

MOUNDS VIEW



Lt.

E

Rt.

+40 $\frac{BR}{37}$ +37 $\frac{1" Maple}{33}$ +25 $\frac{SE Cor Ho}{66}$ +16 $\frac{3" P}{55}$ +15 $\frac{PP}{28}$

37

Road
18+11 $\frac{E.R.}{40}$ +81 $\frac{4" CE}{35}$ +99 $\frac{PP}{87}$ +80 $\frac{E.R.}{18}$ +71 $\frac{Hyd}{45}$ +89 $\frac{BR}{18}$ +94 $\frac{4" Ash}{54}$ +59 $\frac{RTic}{40}$ +92 $\frac{8" E}{51}$ +65 $\frac{BR}{39}$ +85 $\frac{Bush}{67}$ +50 $\frac{MH}{79}$ +54 $\frac{SW Cor Ho}{93}$ +40 $\frac{18" W}{71}$ +35 $\frac{E.R.}{48}$ +97 $\frac{BM}{26.7}$ +14 $\frac{BR}{20}$

36

Road
18-18+97 $\frac{PP}{29}$ +96 $\frac{PP}{51}$ +45 $\frac{1" W.P.}{43}$ +41 $\frac{SE Cor Ho}{67}$ +32 $\frac{SW Cor Ho}{101}$ +13 $\frac{E 18' Ent}{17}$ +05 $\frac{E.R.}{20}$

35

+02 $\frac{SE Cor Ho}{67}$ +03 $\frac{Hyd}{29}$

FK
JS
FS
DS
RB

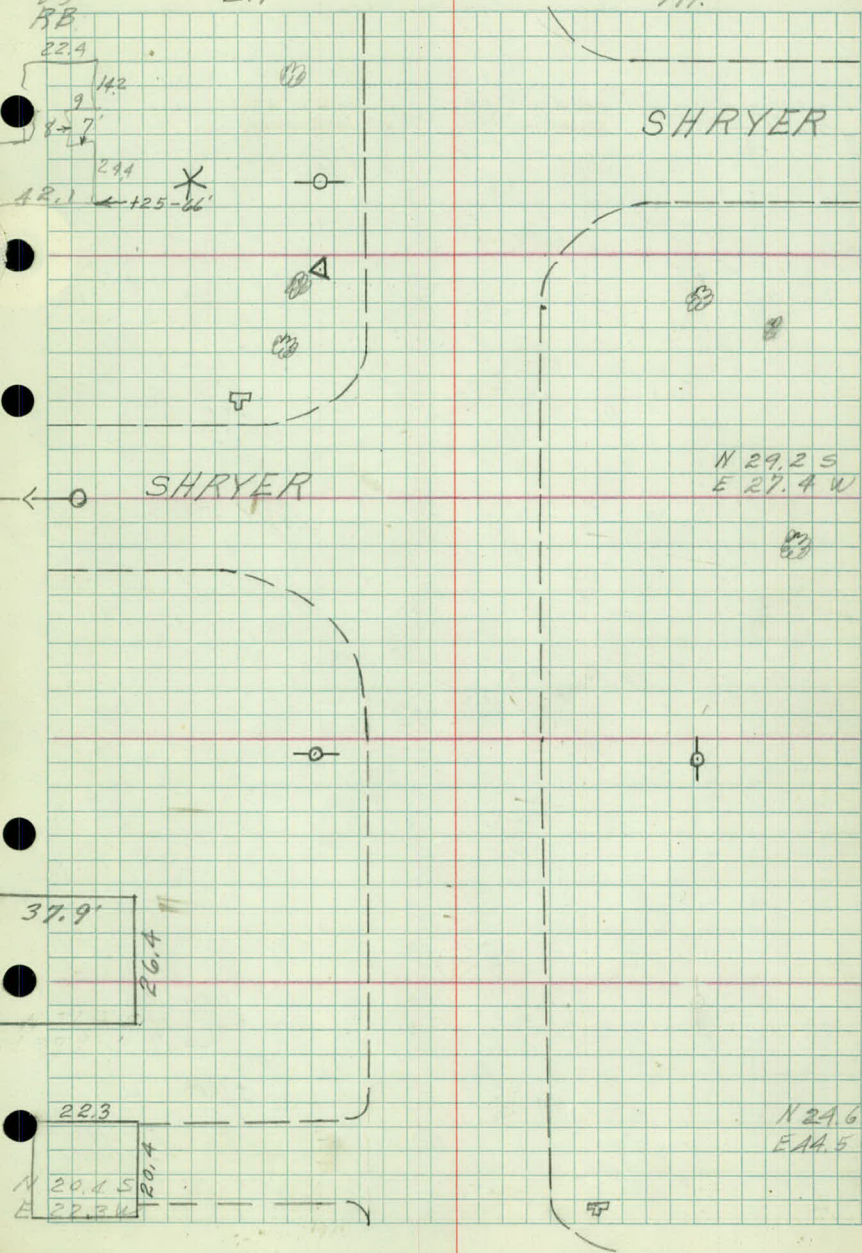
Jan 2, 1964

22

Lt.

E

Rt.



40 Lt. $\frac{Road}{18-21}$ Rt.

193 $\frac{SEC. Ho}{28}$ 195 $\frac{12" C.H.}{60}$

159 $\frac{12" C.A.}{48}$ 173 $\frac{PP}{28}$ 155 $\frac{ER}{18}$

147 $\frac{Hyo}{45}$ 125 $\frac{MH}{43}$ 138 $\frac{BR}{36}$

39 113 $\frac{ER}{30}$ Road 20.5 106 $\frac{MH}{24}$

197 $\frac{B.R.}{18}$ 198 $\frac{1" P}{45}$

133 $\frac{PP}{28}$ 156 $\frac{Road}{19.5}$ 166 $\frac{SW. Cor. Ho}{100}$

116 $\frac{4" C.E.}{46+58}$ 144 $\frac{Ent}{28}$ 132 $\frac{PP}{28}$

38 130 $\frac{30" C.H.}{94}$ 111 $\frac{16" W.}{76}$ 123 $\frac{14" L.P.}{29}$

17 $\frac{Road}{18}$ 182 $\frac{SW. Cor. Ho}{100}$

184 $\frac{2" P}{41}$ 185 $\frac{4" Elm}{65}$ 179 $\frac{1" M.}{32}$

164 $\frac{Ent}{28}$ 156 $\frac{ER}{18}$ 173 $\frac{Lilac}{72}$

Jan. 2, 1964

23

Lt.

Rt.

24.3

N 24.3 S
E 61.9 W

T

11" Casting
No Adj. Rings
FL to Top = 8.18'

11" Casting
No Adj. Rings
FL to Top = 8.00'
*

E 28.8 W
N 34.4 S

N 30.0 S
E 24.2 W

Lt.

E

Rt.

+30 $\frac{SE \text{ Cor Ho}}{79}$ +38 $\frac{4" A}{32}$ +27 $\frac{PP}{28}$ +25 $\frac{12" S.M.}{43}$

42

Road
19 17+94 $\frac{MH}{16}$ +80 $\frac{B. Lilac}{29}$ +96 $\frac{E. Lilac}{28}$ +98 $\frac{8" P}{31}$ +76 $\frac{26" BE}{31}$ +71 $\frac{12" \times 4" M. Culv.}{26}$ +63 $\frac{Honey S.}{36}$ +71 $\frac{SW Cor Ho}{48}$ +54 $\frac{13" BE}{36}$ +67 $\frac{4" Ash}{33}$ +45 $\frac{Honey S.}{41}$ +51 $\frac{15" BE}{37}$ +30 $\frac{E 12" Ent}{28}$ +26 $\frac{SE \text{ Cor Ho}}{80}$ +29 $\frac{E Ent}{26}$ +39 $\frac{Lilac}{35}$ +17 $\frac{Lilac}{35}$ +12 $\frac{PP}{28}$ +09 $\frac{F. Ent}{31}$

41

Road
18 22+00 $\frac{18" O}{35}$ +99 $\frac{PP}{49}$ +99 $\frac{Hedge}{37 \rightarrow}$ +86 $\frac{3" Ash}{33}$ +70 $\frac{SE \text{ Cor Ho}}{78}$ +63 $\frac{MH}{17.5}$ +77 $\frac{18" Cor Ho}{40}$ +95 $\frac{E. Hedge}{34}$ +62 $\frac{8" Ent}{38}$ +50 $\frac{E Ent}{28}$ +47 $\frac{12" E}{39}$ +46 $\frac{B. Hedge}{33}$ +39 $\frac{E-Fg}{45}$ +42 $\frac{SW \text{ Cor Ho}}{68}$ +17 $\frac{16" E}{35}$ +31 $\frac{E Ent}{27}$

40

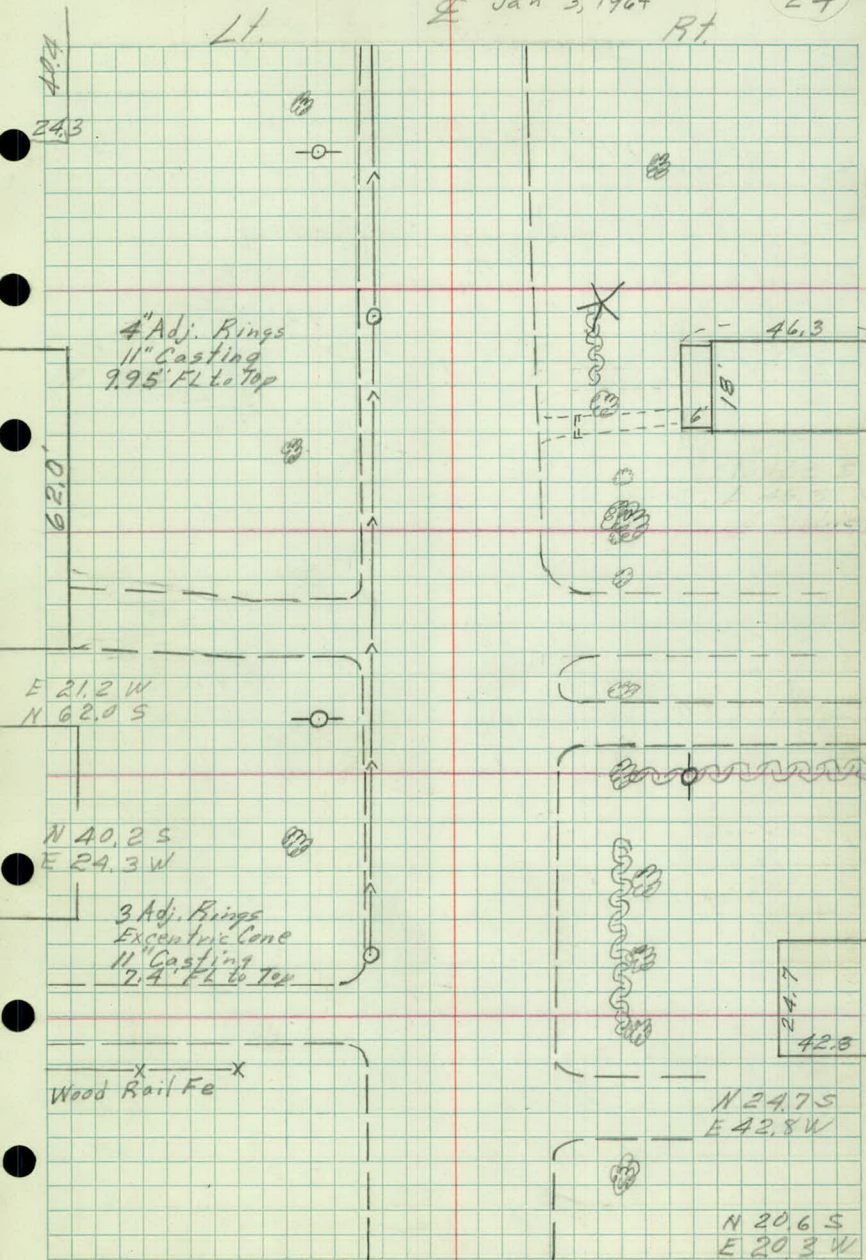
+00 $\frac{SW \text{ Cor Garage}}{97}$

Jan. 2, 1964
Jan 3, 1964

24

Lt.

Rt.



45

Lt.

$$\begin{array}{r} \text{Road} \\ 19 \ 15 \end{array}$$

Rt.

$$\begin{array}{r} \text{MH} \\ +39 \ 16 \end{array}$$

$$\begin{array}{r} \text{SE Cor Ho} \\ +95 \ 80 \end{array}$$

$$\begin{array}{r} \text{Ent} \\ +48 \ \text{RT} \end{array}$$

$$\begin{array}{r} \text{3" M} \\ +88 \ 54 \end{array}$$

$$\begin{array}{r} \text{PP} \\ +84 \ 28 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +62 \ 20 \end{array}$$

$$\begin{array}{r} \text{PP} \\ +36 \ 28 \end{array}$$

$$\begin{array}{r} \text{B.R.} \\ +45 \ 39 \end{array}$$

$$\begin{array}{r} \text{RTie} \\ +29 \ \text{S.S. Street} \end{array}$$

$$\begin{array}{r} \text{BR} \\ +5 \ 20 \end{array}$$

$$\begin{array}{r} \text{ER} \\ +17 \ 42 \end{array}$$

$$\begin{array}{r} \text{W.S.O.} \\ +04 \ 8 \end{array}$$

44

$$\begin{array}{r} \text{Hqd} \\ +00 \ 38 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 19 \ 16 \end{array}$$

$$\begin{array}{r} \text{PP} \\ +61 \ 28 \end{array}$$

$$\begin{array}{r} \text{Tw-4" BE} \\ +33 \ 55 \end{array}$$

$$\begin{array}{r} \text{RHe} \\ +53 \ \text{Ho} \end{array}$$

$$\begin{array}{r} \text{SE Cor Ho} \\ +33 \ 71 \end{array}$$

$$\begin{array}{r} \text{Trip-6" S.P.P.} \\ +18 \ 58 \end{array}$$

43

$$\begin{array}{r} \text{Road} \\ 18 \ 16 \end{array}$$

$$\begin{array}{r} \text{Ent} \\ +64 \ \text{Lt} \end{array}$$

$$\begin{array}{r} \text{Wall} \\ +56 \ 59 \end{array}$$

Jan 2, 1964
Jan 3, 1964

Rt.

25

Lt.

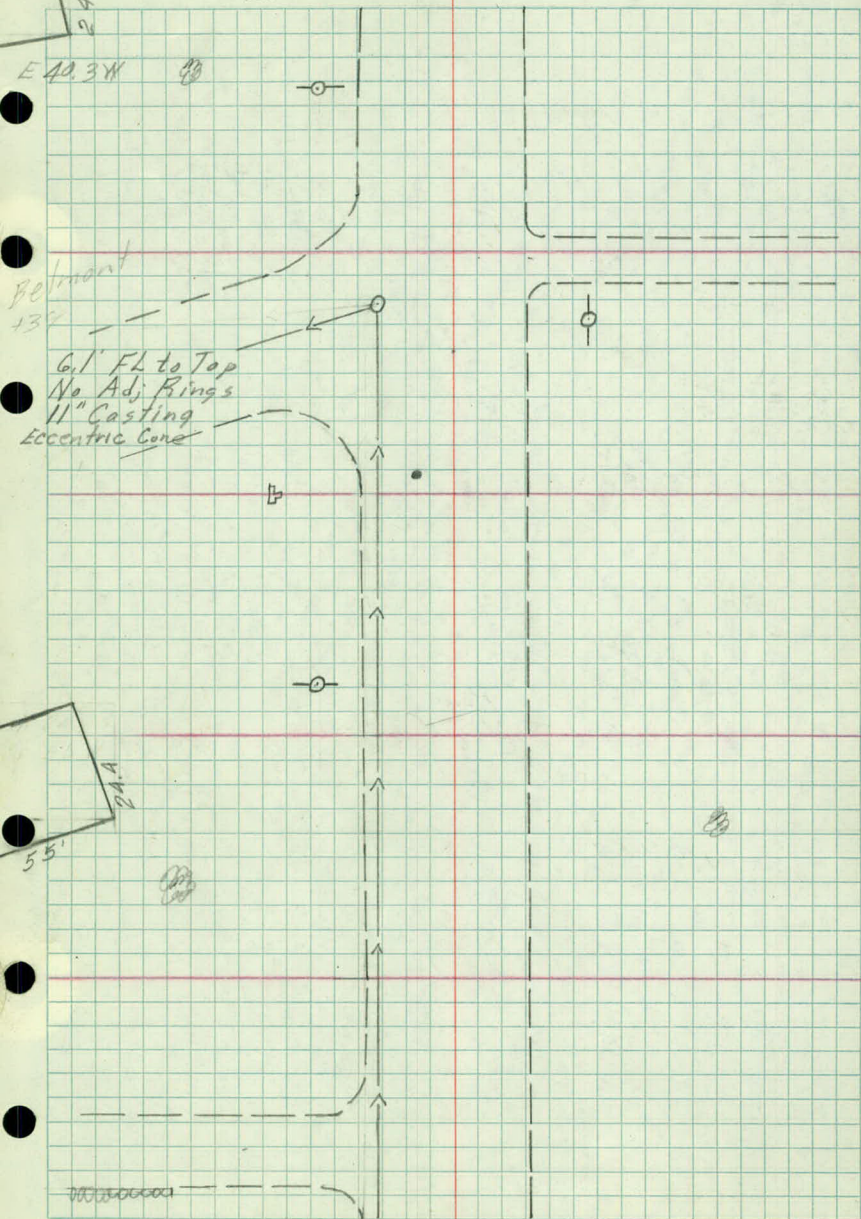
2A.3

E 40.3 W

Belmont
132

6.1' FL to Top
No Adj Rings
11" Casting
Eccentric Cone

2A.4
55'



Lt.

E

Rt.

+36 $\frac{PP}{27}$ +44 $\frac{MH}{18}$ +30 $\frac{ER}{38}$ +12 $\frac{PP}{28}$ +25 $\frac{E Hedge}{35}$

47

+10 $\frac{BR}{18}$ Road
18 15+21 $\frac{NW Cor Ho}{73}$ +94 $\frac{Cedar Busk}{43}$ +86 $\frac{Tr 4" LP}{39}$ +82 $\frac{4" LP}{43}$ +79 $\frac{8" Apple}{59}$ +52 $\frac{SEC. Ho}{80}$ +86 $\frac{2" P}{56}$ +74 $\frac{B. Hedge}{35}$ +72 $\frac{4" BE}{42}$ +44 $\frac{2" M}{50}$ +73 $\frac{STP}{34}$ +56 $\frac{6" BE}{68}$ +56 $\frac{10" M}{59}$ +56 $\frac{4" BE}{46 \& 51}$ +06 $\frac{3" Pine}{66}$ +56 $\frac{R. Tie}{ENT}$ +51 $\frac{E End}{28}$ +10 $\frac{PP}{28}$ +40 $\frac{PP}{28}$

46

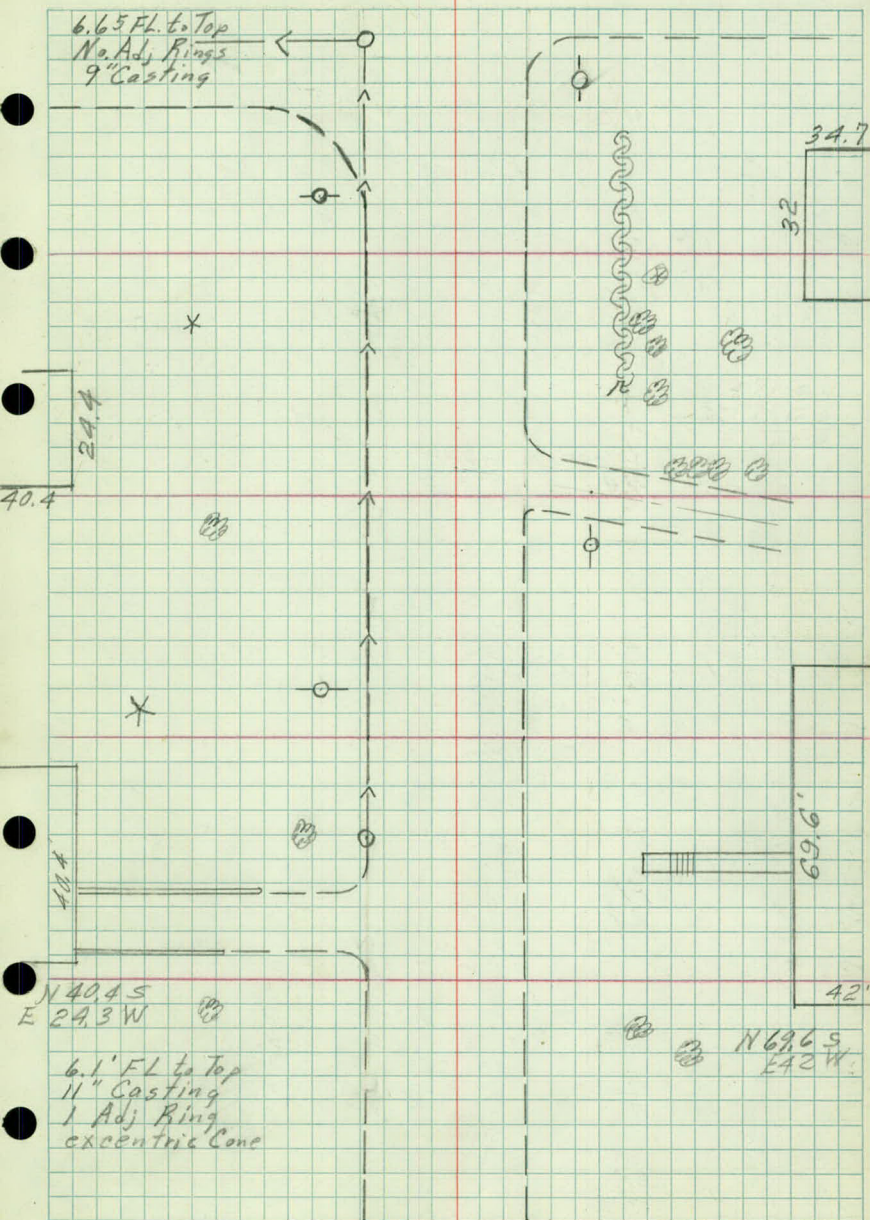
Road
18 14+80 $\frac{4" Ash}{33}$ +56 $\frac{E. Wall}{48}$ +62 $\frac{E. Ent}{41}$ +68 $\frac{E. Wall}{41}$ +53 $\frac{SEC. Ho}{79}$ +74 $\frac{4 Wood Steps + 10.11}{39}$ +44 $\frac{4" Elm}{31}$ +79 $\frac{MH}{78}$ +45 $\frac{Bldg}{71}$ +41 $\frac{14" BE}{37}$ +12 $\frac{R. Tie}{Ho}$ +35 $\frac{Trip 14" BE}{49}$

45

Lt.

Jan 2, 1964
Jan 3, 1964 Rt.

26



50

Lt.

$$\begin{array}{r} \text{Road} \\ 18 \ 19 \end{array}$$

Rt.

$$+52 \begin{array}{l} \text{MH} \\ 33 \end{array}$$

$$+89 \begin{array}{l} \text{PP} \\ 28 \end{array}$$

$$+10 \begin{array}{l} \text{L. Pop} \\ 65 \end{array}$$

$$+26 \begin{array}{l} \text{Hbber-Sign} \\ 37 \end{array}$$

$$+10 \begin{array}{l} \text{PP} \\ 28 \end{array}$$

$$+06 \begin{array}{l} \text{1" Pines} \\ 52-61+70 \end{array}$$

$$+9 \begin{array}{l} \text{Lilac} \\ 108 \ 44 \end{array}$$

$$\begin{array}{r} \text{Road} \\ 21 \ 20 \end{array}$$

$$+79 \begin{array}{l} \text{1" P} \\ 68 \end{array}$$

$$+79 \begin{array}{l} \text{1" P} \\ 46 \end{array}$$

$$+65 \begin{array}{l} \text{Conc Ent} \\ 21 \end{array}$$

$$+53 \begin{array}{l} \text{2" P} \\ 44 \end{array}$$

$$+53 \begin{array}{l} \text{1" P} \\ 58 \end{array}$$

$$+54 \begin{array}{l} \text{2" P} \\ 33 \end{array}$$

$$+09 \begin{array}{l} \text{SEC. Ho} \\ 78 \end{array}$$

$$+33 \begin{array}{l} \text{5" Ash} \\ 32 \end{array}$$

$$+09 \begin{array}{l} \text{PP} \\ 28 \end{array}$$

$$+24 \begin{array}{l} \text{W. Birch} \\ 51 \end{array}$$

48

$$\begin{array}{r} \text{Road} \\ 20 \ 17 \end{array}$$

$$+91 \begin{array}{l} \text{4" Ash} \\ 64 \end{array}$$

$$+81 \begin{array}{l} \text{Pine} \\ 50 \end{array}$$

$$+87 \begin{array}{l} \text{Pine} \\ 44 \end{array}$$

$$+85 \begin{array}{l} \text{SW Cor Ho} \\ 98 \end{array}$$

$$+81 \begin{array}{l} \text{Pine} \\ 44 \end{array}$$

$$+67 \begin{array}{l} \text{Hyd} \\ 46 \end{array}$$

$$+73 \begin{array}{l} \text{ER} \\ 21 \end{array}$$

$$+58 \begin{array}{l} \text{BR} \\ 38 \end{array}$$

$$+59 \begin{array}{l} \text{2 20' Ent} \\ 26 \end{array}$$

Jan 2, 1964
 Jan 3, 1964

27

Lt.

Rt.

12.59 FL to Top
 11" Casting
 No Adj Rings
 Eccentric

4.3' Cone
 2.7' Ring

8.6 B.4		
0.12	0.01	0.14
10.1	0.0	0.0
10.2	0.0	0.0
10.7	0.0	0.0
10.7	0.0	0.0

N 62.5
 E 24.3 W

N 35.8 S
 E 37.4 W

Lt.

£

Rt.

1

+36.5 $\frac{MH}{2}$ +37 $\frac{MH}{72}$ +05 $\frac{Cir Apron}{41}$ +15 $\frac{PORT}{39}$ Apr+18 $\frac{ER}{44}$ +08 $\frac{POR}{26}$ +19 $\frac{ER}{52}$ 52 +08 $\frac{PP}{27}$ Road Apron
24+11 $\frac{PP}{33}$ +96 $\frac{BR}{21}$ +94 $\frac{Cir Apron}{34}$ +84 $\frac{BR}{21}$ +35 $\frac{MH}{33}$ +26 $\frac{PP}{28}$ Road
79 20+95 $\frac{W.E. Culvert}{46}$ Buried

50

Jan 2, 1964
Jan 3, 1964

28

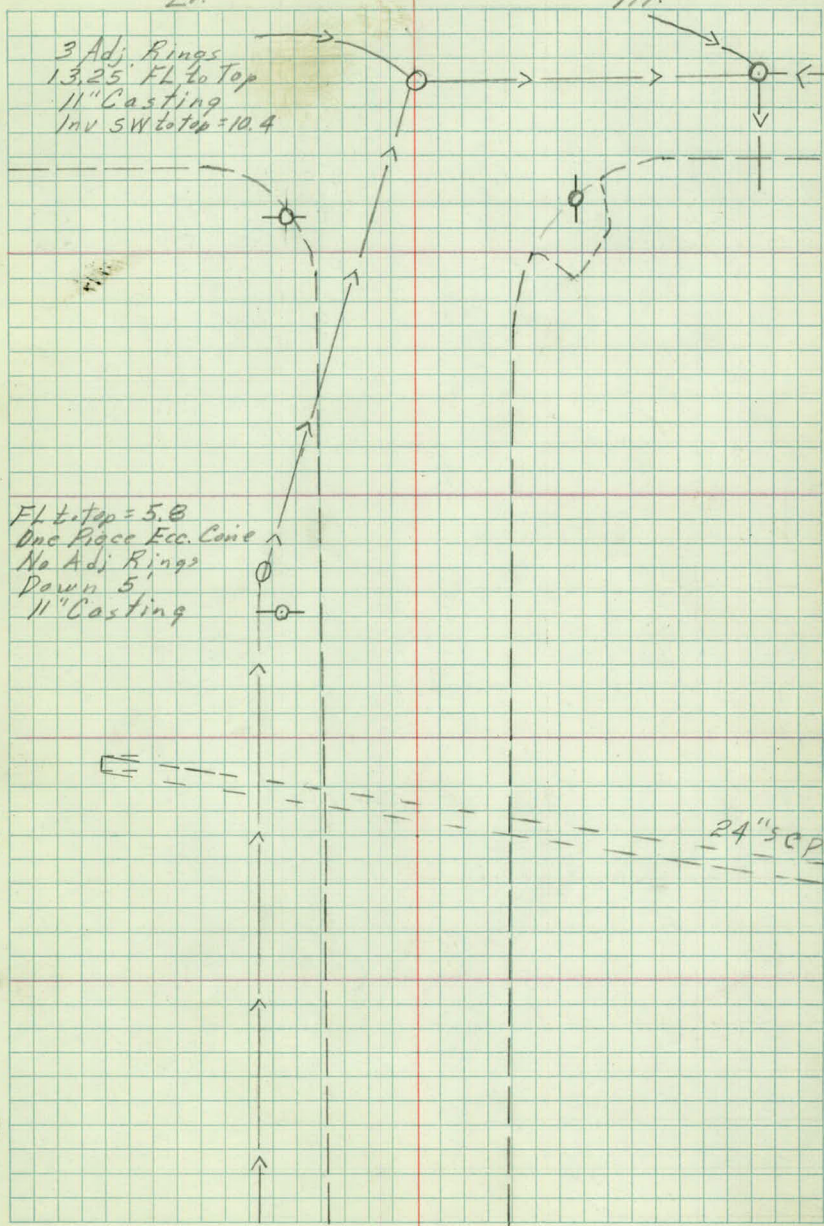
Lt.

Rt.

3 Adj. Rings
13.25' FL to Top
11" Casting
Inv SW to top = 10.4

FL to top = 5.8
One Piece Ecc. Cone
No Adj. Rings
Down 5'
11" Casting

24" SCP



55

Lt

 $\frac{4}{\text{Road}}$
17

Rt

 $\frac{+81}{31}$ Cor Conc

 $\frac{+96}{26}$ SE 15 CM

 $\frac{+96}{27}$ Cor Conc Apron

 $\frac{+58}{31}$ Light S/s

 $\frac{+38}{28}$ B. Grass

 $\frac{+47}{21-32}$ Edge B/L

 $\frac{+109}{28}$ PP

 $\frac{+11}{78}$ S.W. Cor B/L

54

 $\frac{\text{Road}}{17}$
 $\frac{+42}{43}$ Cor Conc

 $\frac{+12}{43}$ B. Conc

 $\frac{+21}{105.5}$ S.W. Cor Sta

 $\frac{+94}{37}$ EC

 $\frac{+84}{33}$ BC

 $\frac{+88}{34}$ Light

 $\frac{+58}{34}$ E. Curb

 $\frac{\text{Curb}}{37}$
 $\frac{+22}{55}$ SE Pump

53

 $\frac{\text{Road}}{17}$
 $\frac{+11}{33}$ BC

 $\frac{+86}{33}$ E. Curb

 $\frac{+77}{29}$ Road

 $\frac{+72}{49}$ B. Curb

 $\frac{+83}{47}$ Light

 $\frac{+84}{18}$ ER

 $\frac{+78}{43}$ Sign

 $\frac{82}{28}$ PP

 $\frac{+65}{22}$ POR

 $\frac{+66}{30}$ POR

 $\frac{+66}{39}$ Hud

 $\frac{+53}{47}$ BR

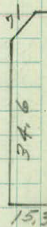
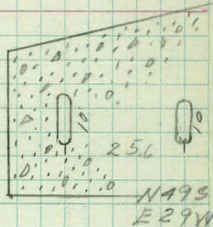
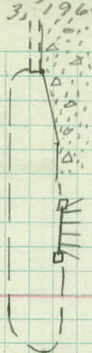
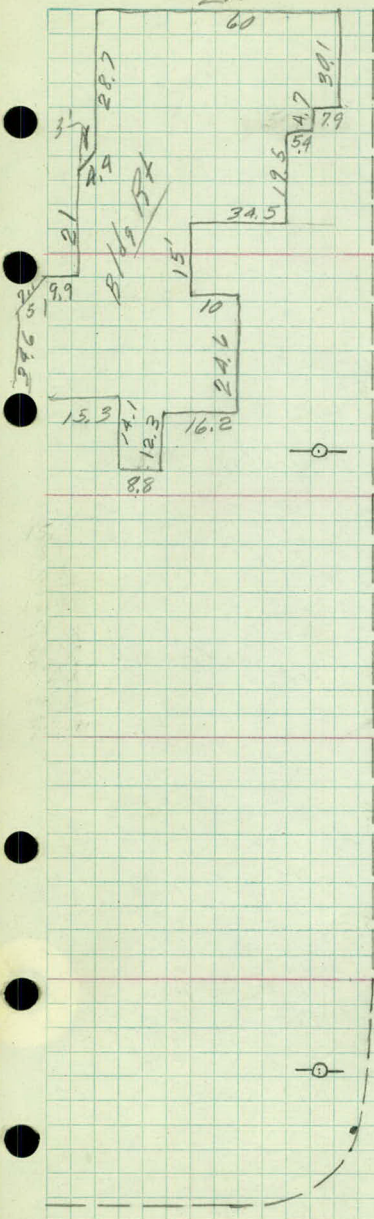
 $\frac{+61}{40}$ BR

 $\frac{+79}{83.5}$ Cor Conc

 $\frac{+91}{93.5}$ P. Island

Jan 2, 1964
Jan 3, 1964

29



Lt

±

Rt

$$+29 \quad \pm \quad \frac{21 \text{ BT Ent } - 293 \text{ pan} \times 29 \text{ cm}}{20} \\ +17 \quad \frac{\text{Cor Parking}}{64}$$

57

$$\frac{\text{BT}}{14 \quad 15}$$

$$+98 \quad \frac{\text{Cor Parking \& P.Curb}}{63}$$

$$+90 \quad \frac{\text{Cor Apt Bldg}}{73}$$

$$+69 \quad \frac{\text{PP}}{28}$$

$$+49 \quad \frac{\text{S.W. Cor Apt}}{73}$$

$$+47 \quad \frac{\text{QV}}{43}$$

$$+36 \quad \frac{\text{X-Fc}}{25}$$

$$+05 \quad \frac{\text{Hyd}}{27}$$

$$+13 \quad \frac{\text{Cor Apt Bldg}}{73}$$

56

$$\frac{\text{BT}}{15-15}$$

$$+72 \quad \frac{\text{Apt Bldg}}{73}$$

$$+56 \quad \frac{\text{E.P.Curb}}{53}$$

$$+38 \quad \frac{\text{PP}}{29}$$

$$+56 \quad \frac{\text{Cor Parking}}{35}$$

$$+28 \quad \frac{\text{NE } 18 \times 32 \text{ CM}}{26}$$

$$+35 \quad \frac{\text{W E } 24 \times 60 \text{ CM}}{33}$$

$$+35 \quad \frac{\text{E.E. } 24 \times 60 \text{ CM}}{27}$$

$$+33 \quad \frac{\text{ER}}{34}$$

$$+28 \quad \frac{\text{POR}}{24}$$

$$+32 \quad \frac{\text{BR}}{19}$$

$$+03 \quad \frac{\text{Cor Cene.}}{27.5}$$

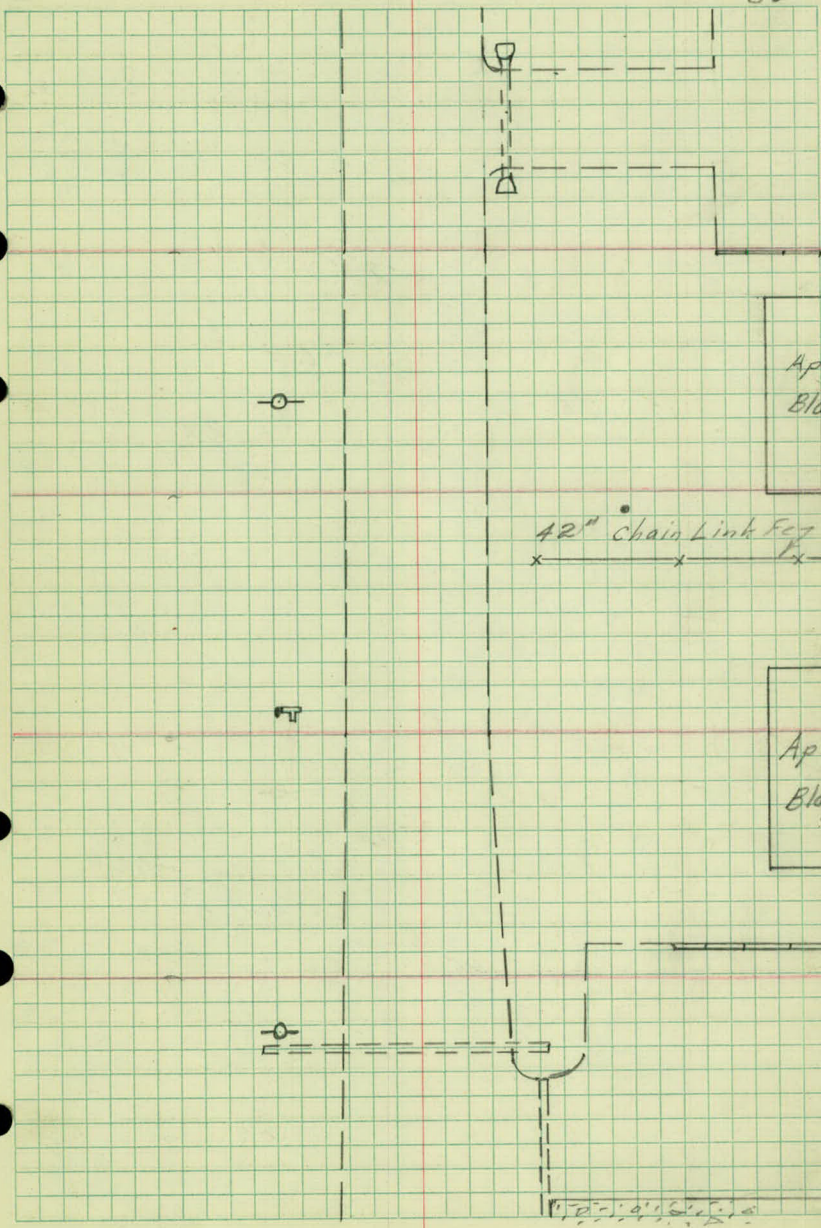
55

FR
JS
FS
TL

Lt

Feb. 20, 1964
Cold Windy 18° Rt

30



60

$$\begin{array}{r} \cancel{4} \\ BT \\ 15-15 \end{array}$$

$$\begin{array}{r} 100 \\ Fc Cor \\ 27 \end{array}$$

(34' W. Aprons)

$$\begin{array}{r} +70 \\ 4" Maple \\ 43 \end{array}$$

$$\begin{array}{r} +73 \\ SE 30' CM \\ 20 \end{array}$$

$$\begin{array}{r} +27 \\ 5" White H. \\ 78 \end{array}$$

$$\begin{array}{r} +33 \\ 4" Maple \\ 43 \end{array}$$

$$\begin{array}{r} +26 \\ MH \\ 50 \end{array}$$

$$\begin{array}{r} +13 \\ 6" Ash \\ 56 \end{array}$$

$$\begin{array}{r} +26 \\ PP \\ 28 \end{array}$$

$$\begin{array}{r} +08 \\ 14" Catt. \\ 40 \end{array}$$

$$\begin{array}{r} +145 \\ Hyd \\ 27.5 \end{array}$$

$$\begin{array}{r} +05 \\ E Hedge & L. 1/2 c \\ 28 \end{array}$$

59

$$\begin{array}{r} BT \\ 15-13 \end{array}$$

$$\begin{array}{r} +00 \\ X-FC \\ 29.5 \end{array}$$

$$\begin{array}{r} +44 \\ PP \\ 45 \end{array}$$

$$\begin{array}{r} +39 \\ Arc Lt. \\ 19 \end{array}$$

$$\begin{array}{r} +29 \\ GV \\ 43 \end{array}$$

$$\begin{array}{r} +10 \\ Cor Apt \\ 73 \end{array}$$

58

$$\begin{array}{r} +00 \\ PP \\ 28 \end{array}$$

$$\begin{array}{r} BT \\ 15-14 \end{array}$$

$$\begin{array}{r} +69 \\ Cor Apt \\ 73 \end{array}$$

$$\begin{array}{r} +60 \\ Cor Parkins & P.S. \\ 64 \end{array}$$

~~2~~ Feb 24 1964

31

B. T. Gu Her

37.5

30.5

48" Ornamental Iron

Apt.
Bldg.

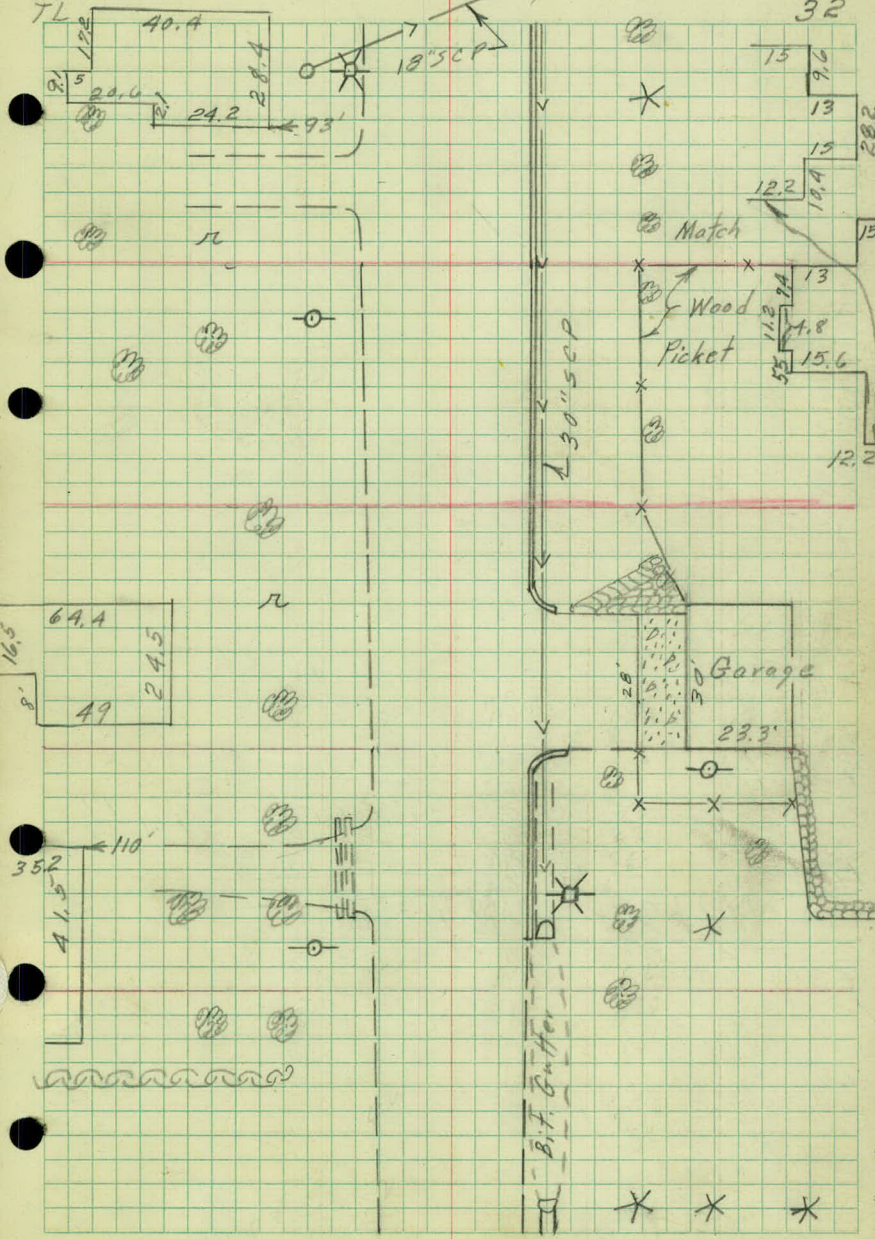
4

131 $\frac{24^{\circ}E}{74}$ 140 $\frac{CB}{30}$ 140 $\frac{Arc LT}{21}$
 127 $\frac{SE Cor Ho}{93}$ 134 $\frac{8^{\circ}P}{41}$ 149 $\frac{10^{\circ}CE}{40}$
 106 $\frac{18^{\circ}E m}{24}$ 117 $\frac{E 10' Ent}{29}$ 121 $\frac{12^{\circ}CE}{40}$
 105 $\frac{STP}{50}$ 100 $\frac{NW Cor Ho}{72}$ 108 $\frac{10^{\circ}P}{42}$
 62 Road 18 16.5 100 $\frac{Fe Cor}{39}$
 199 $\frac{16^{\circ}E m}{41}$
 166 $\frac{16^{\circ}E}{42}$
 150 $\frac{Fe Cor}{40}$ 136 $\frac{Fe Cor}{46}$
 140 $\frac{Cor Wall}{42}$
 189 $\frac{PP}{29}$ 129 $\frac{Cor Wall}{25}$
 178 $\frac{20^{\circ}CE}{69}$ 186 $\frac{18^{\circ}CE}{50}$
 147 $\frac{24^{\circ}M}{34}$
 109 $\frac{24^{\circ}M}{36}$ 131 $\frac{STP}{37}$ 133 $\frac{ER}{16.5}$
 105 $\frac{Cor Ho}{58}$ 128 $\frac{B.O.}{22}$ 116 $\frac{E Ent Circ}{39}$
 61 Road 17 100 $\frac{ER}{29}$ 100 $\frac{Cor Gor.}{19}$
 180 $\frac{NE Cor Barn}{110}$ 196 $\frac{BR}{16.5}$ 196 $\frac{PP}{54}$
 187 $\frac{N 1/2-2-15'X22'CM}{22}$ 188 $\frac{Fe Cor}{39}$ 194 $\frac{4^{\circ}M}{34}$
 168 $\frac{24^{\circ}M}{55}$ 196 $\frac{24^{\circ}M}{36}$ 178 $\frac{4^{\circ}M ad}{64}$
 167 $\frac{24^{\circ}M}{34}$ 172 $\frac{Light Pls}{23}$ 123 $\frac{2^{\circ}P}{50}$
 165 $\frac{2-15'X22'CM (S-End)}{21}$ 164 $\frac{4^{\circ}M ad}{37}$ (30' SCF)
 159 $\frac{PP}{28}$ 161 $\frac{B.P. 6 1/2}{16.5}$ 161 $\frac{S.E. Apron}{19 (6')}$
 143 $\frac{32^{\circ}M}{49}$ 143 $\frac{28^{\circ}M}{34}$ 149 $\frac{6^{\circ}Flan}{36}$
 132 $\frac{E Hedge}{34}$ 155 $\frac{E Fe}{36.5}$ 165 $\frac{Cor Wall}{75}$
 60 106 $\frac{4^{\circ}Pine}{38, 54 47.5}$

FK
JS
DS
TL

Feb 24, 1964
Cloudy Cold 15°

32



65

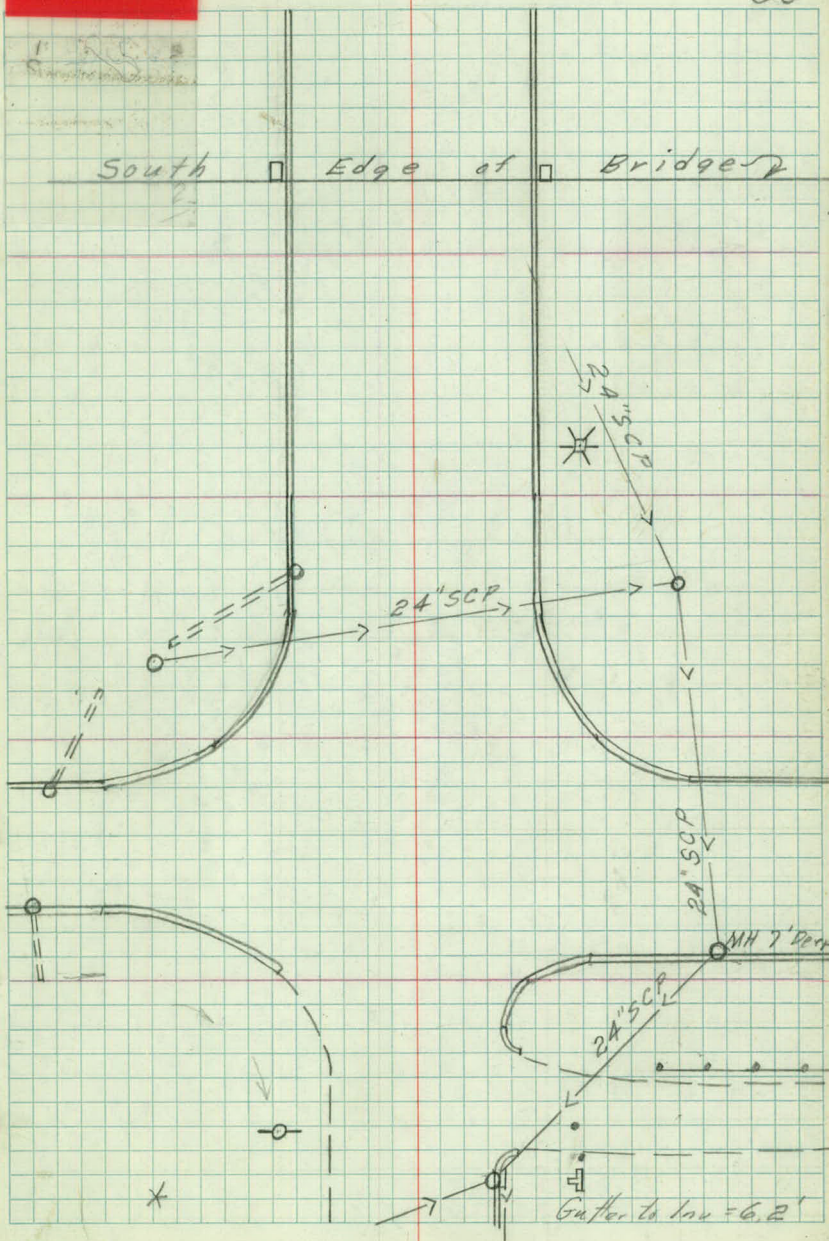
Curb
25.6 25.6+65 $\frac{\text{Pier}}{28}$ +65 $\frac{\text{Pier}}{28}$ +10 $\frac{\text{Arc Lt}}{36}$ Curb
25.9 25.6+85 $\frac{\text{CB}}{25}$ +76 $\frac{\text{ER}}{26}$ +66 $\frac{\text{CB}}{5A}$ +69 $\frac{\text{NE 12 CM}}{52}$ +82 $\frac{\text{CB}}{55}$ +48 $\frac{\text{POR}}{42}$ +65 $\frac{\text{NE 12 CM}}{93}$ +40 $\frac{\text{BR}}{65}$ +60 $\frac{\text{NE 12 CM}}{66}$ +80 $\frac{\text{ER}}{26}$ +39 $\frac{\text{CB}}{77}$ +50 $\frac{\text{POR}}{38}$ +41 $\frac{\text{BR}}{67}$ +15 $\frac{\text{CB}}{80}$ +100 $\frac{\text{SE 12 CM}}{78}$ +40 $\frac{\text{CB}}{96}$ +14 $\frac{\text{ER}}{66}$ +105 $\frac{\text{ER}}{37}$ +106 $\frac{\text{CB}}{63}$ +102 $\frac{\text{B. Conc. Cutler}}{28}$ +100 $\frac{\text{Curb}}{23}$

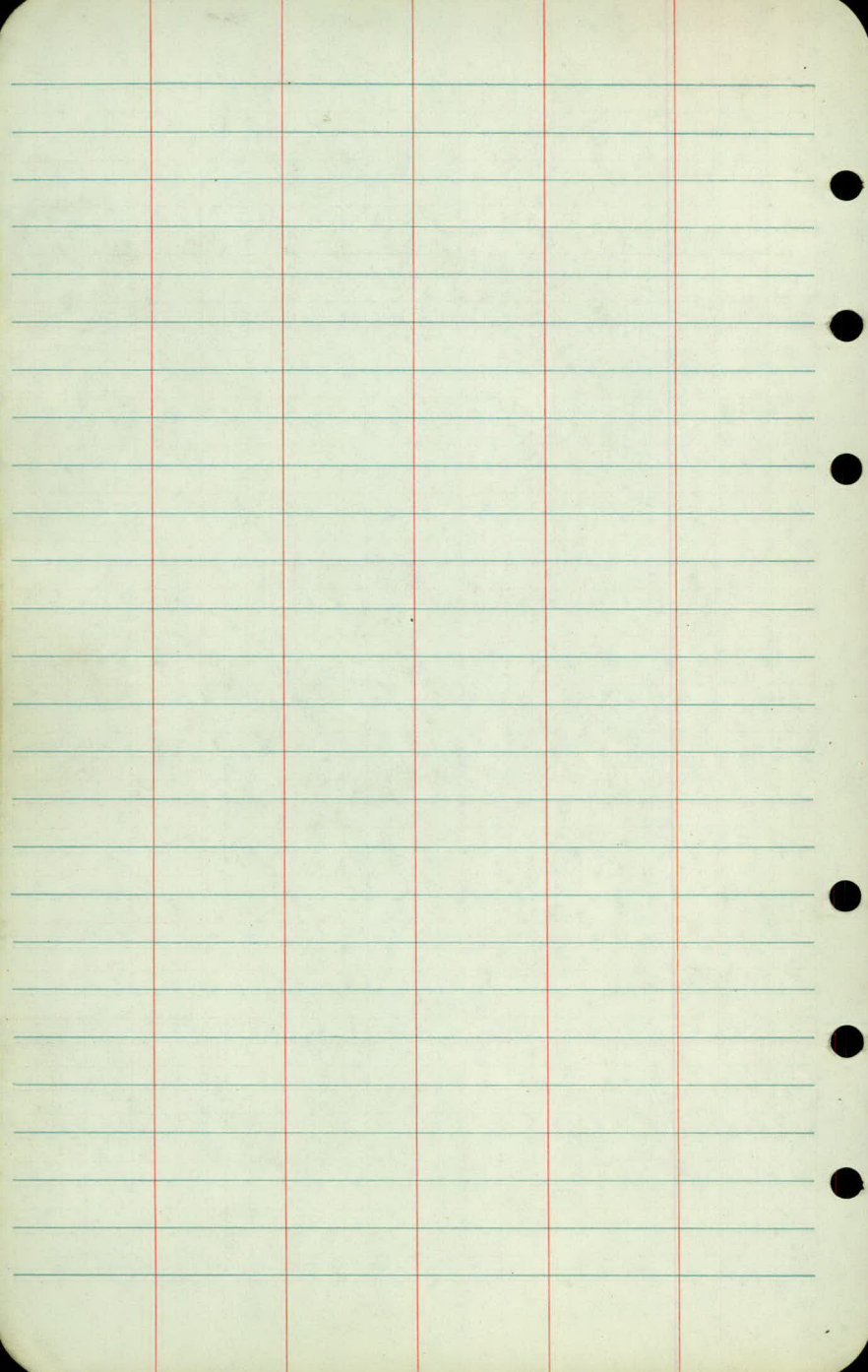
63

+70 $\frac{\text{GV}}{33}$ +82 $\frac{\text{BGR}}{51}$ +63 $\frac{\text{GV}}{35}$ +85 $\frac{\text{BR}}{22}$ +91 $\frac{\text{ER}}{18}$ +82 $\frac{\text{BR}}{18}$ +64 $\frac{\text{ER}}{21}$ +69 $\frac{\text{PP}}{29}$ +58 $\frac{\text{CB Pipe}}{16-19}$ +61 $\frac{\text{BR}}{16.5}$ +56 $\frac{2" P}{34}$ +59 $\frac{\text{Hyd}}{34}$

Feb 24, 1964

33





RP
FS

22 APRIL 1964
SUNNY 50°

WM
+L

DALE ST

LARPENTEUR AVE TO STH #36

PULL-Box Locations

1400

+50

+36.5 Pull Box
55.4

+40 Pull box
28

0400

22 APRIL 1964

Lt

£

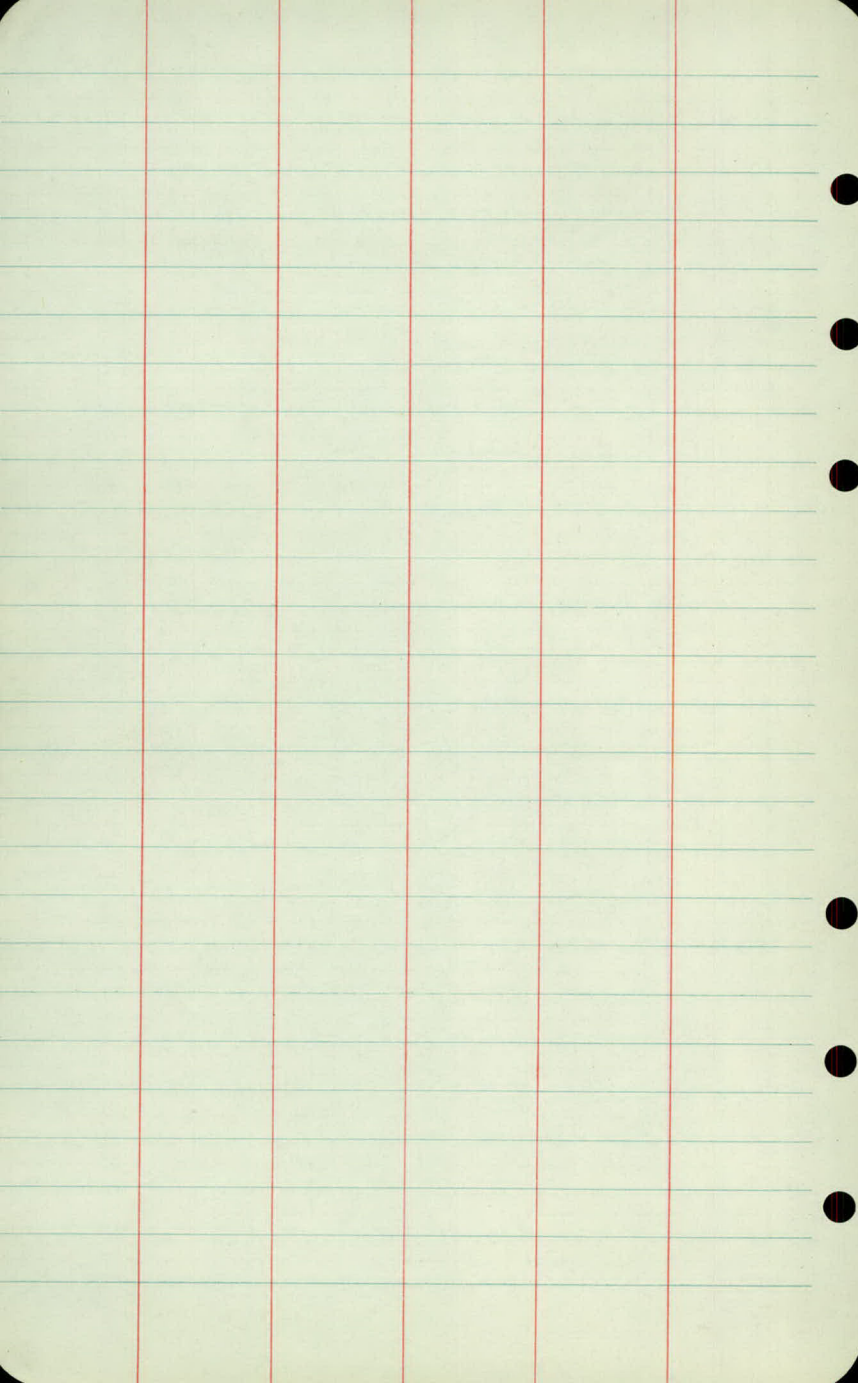
RT

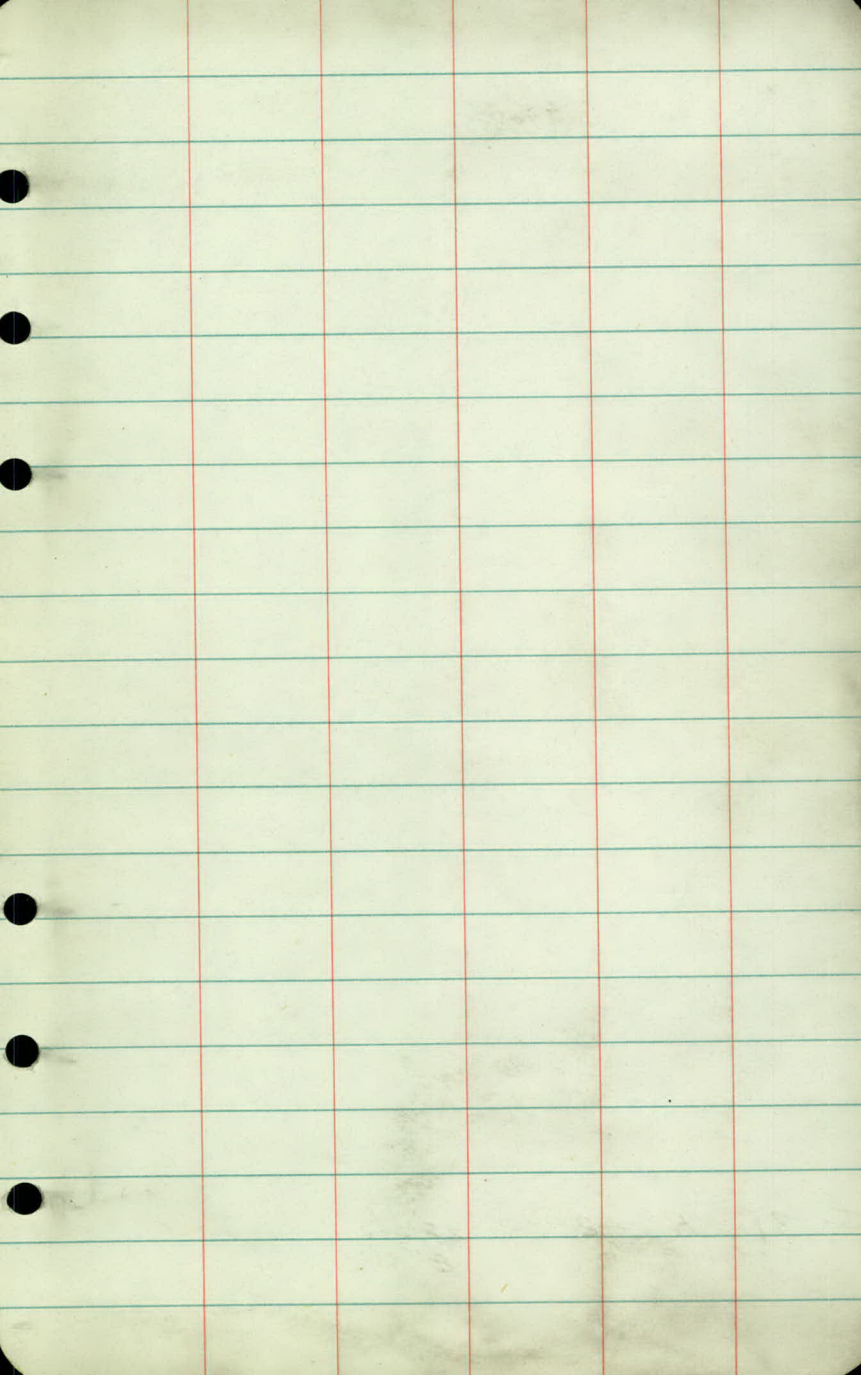
-

-

D

□





54 31 Rt 42' = Possible End Sewer
8" Vit. Pipe

7+47

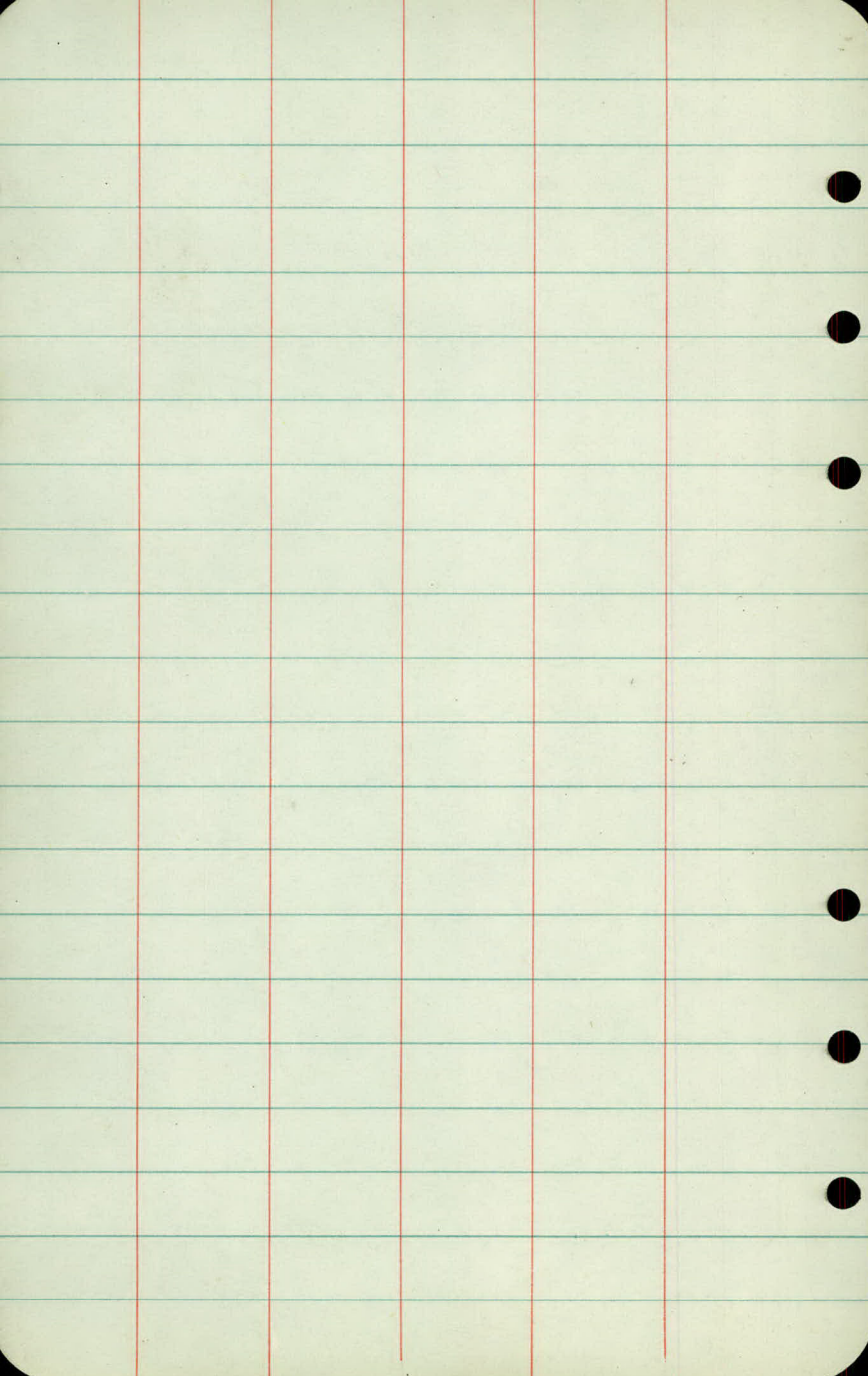
38.60

42.5
10" W.B.
Base

Iron

42.6

7+00.



FA
LB
BZ
FK

August 8, 1963

1

Dale Street

Larpenteur to A²

x-sections

2 pages

Sta	+	π	-	Elev
-----	---	-------	---	------

BM	6.14	899.05		892.91
----	------	--------	--	--------

$\pm$ Present Dalc		7.1	892.0	
--------------------	--	-----	-------	--

16+57

71

1586

5.98

12.6

16+22

15+86

August 8, 1963

It

£

Rt 2

Walk at NW Cor Ho # 1822

at £ Pineview Ct.

92.5	92.4	90.7	89.4	90.6
6.6	6.7	8.4	9.7	8.5
76.5	72.5	45	16	
Ho	"			

Door House on East side

83.2+

87.3	85.8	85.2	85.2	86.2
SS 11.8	13.3	13.9	13.9	12.9
H.O. 68	52	30	8	
78.6				

S'ite + π - Elev.

BM 3.84 925.26

(921.42)

2

+70

3

+24

+63

4+00

+11

+30

FK
LB
BZ
FK

August 9, 1963

3

Top Hyd S.W. Cor Dale & Larp.

18.6

6.7

Fe

30

21.3

40

38

Cor. House

5.19.9

5.4

Fe

30

21.4

3.9

Cor Ho

21.6

3.7

20.3

50

21.9

3.4

Cor Ho

21.5

3.8

Cor Ho

Sta + x - Elev

925.26

+59

5

+18 End Fe Rt

4+00 ϕ 4.8 920.5

BM 4.17 921.30 917.13

T.P. 8.57 912.73 912.79

August 9, 1963

4

Lt

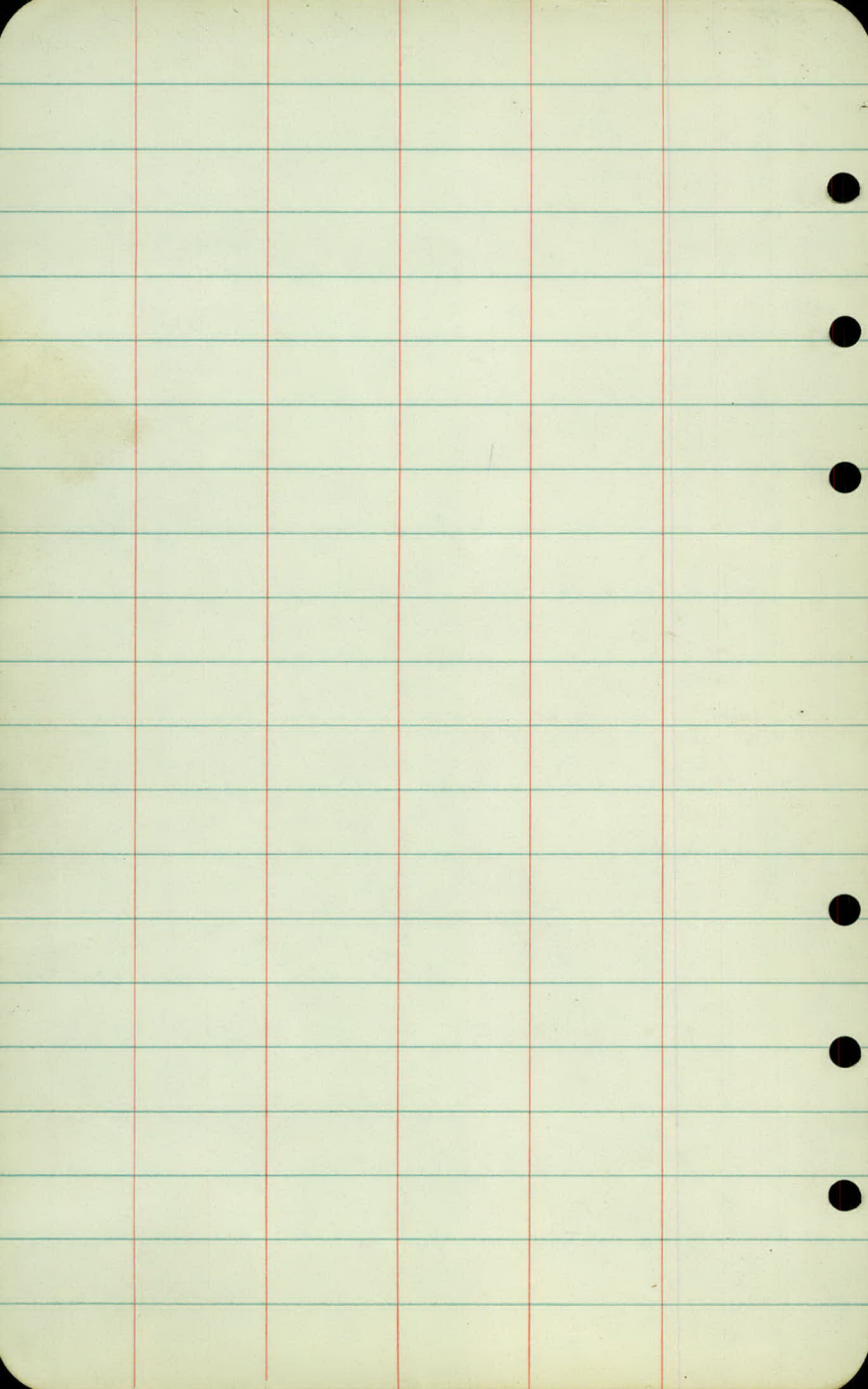
RT

30.21.5
3.8

19.4
5.9

912.79
8.57
921.36
4.17
925.53

Iron pin at Ec Post



FK
JS
FS
DS

Feb. 3, 1964

1

X-sections

Sta + π - Elev.

BM 1.69 923.24

(921.55)

18.83

0+00

4.41

+15 MH 17' RT

4.62 18.62 ✓

+30.5

+55 G.V. 44' LT

4.65 18.59

✓

+58 G.V. 28' LT

4.46 18.78

+59 G.V. 33' LT

4.39 18.85

+61

✓

+67 MH 35' LT

4.31 18.93 ✓

Feb. 3, 1964
Clear Cool 20° 2

Top Hyd S.W. Cor. Dale + Larpenteur

18.32	18.40	18.49	18.53	18.64 ✓	18.48	18.42	18.0	18.0
4.92	4.84	4.75	4.71	4.60	4.76	4.82	5.2	5.2
50	35	20	9		20	40	61	70
			G.V.					
18.27	18.23	18.13	18.29					
4.97	4.51	5.11	4.45					
G	C	G	C					
61		72						
18.7	18.85 ✓	18.78 ✓	18.7	18.5	18.1	17.7	18.24	18.2
4.5	4.39	4.46	4.5	4.7	5.1	5.5	5.00	5.0
57	46	24	12		15	24	33	50
	MH	M.H					Cond	
							Curb	
19.2								
40								
75								

Sta + π - Elev.

923.24

1

+50

2

T.P. 6.53 925.71 4.06 919.18

+50

3

+50

Feb. 3, 1964

Lt

E

3

19.1 18.4

19.2

18.7

18.5

17.6 ✓

17.6

17.3

18.1

41	48	40	45	47	5.6	5.6	5.9	5.1
75	52	43	27	25		8	25	33

19.9

19.0

18.2

18.0

17.1 ✓

16.9

17.0

18.0

3.3	4.2	5.0	5.2	6.1	6.3	6.2	5.2
75	54	44	26		15	26	33

19.5

19.3

18.7

18.9

17.6 ✓

17.5

17.4

18.5

3.7	3.9	4.5	5.3	5.6	5.7	5.8	4.7
73	54	30	19		11	27	33

Nail in PP 32' Rt Sta 2+

21.1

21.1

20.5

19.5

19.6

18.8 ✓

18.4

18.3

18.5

19.3

4.6	4.6	5.2	6.2	6.1	6.9	7.3	7.4	7.2	6.4
46	35	29	27	15		14	24	30	33

21.5

21.2

20.5

19.8 ✓

19.5

19.7

20.1

4.2	4.19	5.2	5.9	6.2	6.0	5.6
42	36	21		17	26	33

House Walk

21.5

21.6

21.2

21.1

20.8

20.7 ✓

20.4

20.5

20.6

4.2	4.11	4.5	4.6	4.9	5.0	5.3	5.2	5.1
50	44	40	27	5		7	24	33

Conc

Sta + π - Elev.

925.71

4

+50

5

+20

✓

T.P. 4.75 917.48 12.98 912.73 912.73

+32

Feb. 3, 1964

Lt.

L

Rt

4

22.07

21.88

21.2

21.1

20.6

20.5

20.5

3.64 3.83 4.5 4.6 5.1 5.2 5.2

51 37 28 15 16 33

Conc

21.4

20.9

20.6

20.5

20.6

20.9

4.3 4.8 5.1 5.2 5.1 4.8

62 40 21 19 33

19.2

19.0

18.4

18.0

18.1

18.8

19.1

19.9

6.5 6.7 7.3 7.7 7.6 6.9 6.6 5.8

52 43 25 21 14 25 33

17.1

16.7

16.7

17.1

17.4

17.4

16.9

16.4

8.6 9.0 9.0 8.6 8.3 8.3 8.8 9.3

50 37 17 5 17 25 31

17.4

16.6

8.3 9.1

50 43

16.8

16.7

14.9

14.9

14.3

13.3

14.1

12.1

0.7 0.8 2.6 2.6 3.2 4.2 3.4 5.4

58 37 22 11 31 51 75

Sta + π - Elev.

917.48

5 + 50

+ 69

6

✓

+ 39

TP 0.56 904.48 13.56 903.92

TP 4.13 894.84 13.77 890.71

+ 39

1378

Feb. 3, 1964

LH

R

RT

5

14.0	12.9	10.5	08.0	08.0	08.9	08.1	06.4	06.5	05.8
3.5	4.6	7.0	9.5	9.5	8.6	9.4	11.1	11.0	11.7
75	48	41	31	17		14	33	52	75

13.8	13.0	09.3	04.2	01.5	01.8	09.9	08.9	08.6	08.2
3.7	4.5	8.2	13.3	16.0	15.7	17.6	18.6	18.9	19.3
75	55	43	32	25		19	34	49	68

01.5	08.9	02.9	00.6	01.0	01.1	00.7
10.0	18.6	24.6	26.9	26.5	26.4	26.8
44	32	22	13.9	13.5	15	34

12.3	13.2	09.7
5.2	4.3	27.8
55	75	75

13.1	09.9	04.6	06.1	00.6
5.4	7.6	12.9	21.4	26.9
75	65	54	43	33

08.8	06.1	05.7	05.7	06.2	06.4	06.2
6.0	8.7	9.1	9.1	8.6	8.4	8.6
27	11	21	38	58		75

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		894.84		
--	--	--------	--	--

6 +54				
-------	--	--	--	--

✓				
---	--	--	--	--

+86				
-----	--	--	--	--

7				
---	--	--	--	--

T.P.	13.28	904.49	4.13	890.71
------	-------	--------	------	--------

+50				
-----	--	--	--	--

T.P.	11.98	913.06	3.41	901.08
------	-------	--------	------	--------

+71				
-----	--	--	--	--

Feb. 3, 1964

LT

♀

RT

6

94.2	85.1	84.6	84.5	84.5	84.5	85.0	85.2
0.6	9.2	10.2	10.3	10.3	10.3	9.8	9.8
46.	35	28	15		16	30	51

99.4	90.1					85.5
+4.6	+6.3	S.S.				9.3
55	59					75

94.3	88.9	85.5	84.3	84.1	84.2	84.8	84.7	85.1	84.5
0.5	5.9	9.3	10.5	10.7	10.6	10.8	10.1	9.2	8.3
75.	64	52	33	18		12	29	54	75

90.3	87.0	85.6	84.1	84.8	85.1	85.7	85.1	86.3	87.1
4.5	7.8	9.2	10.2	10.0	9.7	9.1	9.7	8.5	7.7
75	68	55	31	12		24	37	60	75

94.6	94.6	97.4	97.3	95.8	95.3	95.7	95.1	94.2	94.2
5.9	5.9	7.1	7.2	8.7	9.2	8.8	9.4	10.3	10.3
75	63	40	24	12		25	49	69	75

02.6	02.3	02.4	02.1	01.1	00.3	00.2	99.4	98.9
10.5	10.8	10.7	11.0	12.0	12.8	12.9	13.7	14.2
51	42	30	17		24	47	67	75

03.2	03.4							
9.9	9.7							
6.8	7.5							

Sta	+	+	-	Elev.
-----	---	---	---	-------

		913.06		
--	--	--------	--	--

7+98				
------	--	--	--	--

✓				
---	--	--	--	--

8				
---	--	--	--	--

✓				
---	--	--	--	--

T.P.	12.72	923.81	1.97	911.09
------	-------	--------	------	--------

+20				
-----	--	--	--	--

+45				
-----	--	--	--	--

Feb. 3, 1964

11

2

AT 7

10.4 . 09.9 . 09.0 . 08.1 . 07.6 ✓ . 06.6 . 05.1 . 03.4 . 03.1

27 3.2 4.1 5.0 5.5 6.5 8.0 9.5 10.0
55 43 34 15 25 47 65 75

11.3

11.6

1.8 1.5
65 75

✓

15.0

10.7

09.4

08.3

07.9 ✓

07.0

05.6

03.9

03.4

11.9 2.8 3.7 4.8 5.2 6.1 7.5 9.2 9.7
55 43 34 15 25 47 65 75

15.1

16.3

+2.0 +3.2
65 75

16.8

15.3

13.5

12.3

11.2

09.5

07.6

05.9

05.4

7.0 8.5 10.3 11.5 12.6 14.3 16.2 17.9 18.4
75 60 39 20 ✓ 22 43 65 75

19.3

18.0

16.7

15.5

13.6

11.3

08.4

07.9

4.5 5.8 7.1 8.3 10.2 12.5 15.2 15.9
75 54 36 20 ✓ 19 38 50

06.7

07.0

17.1 16.8
75 70

Sta + π - Elev.

923.81

8+60

3.30
2.4
T.P.

6.68 917.13 (917.13)

BM 9.48 923.36

(913.88)

T.P.

6.23 917.13

9+00

9.6

+32

TP 2.39 913.40 12.05 911.31 Spike at 9+00

TP 1.15 903.89 10.96 902.74

+65

✓

12.58
2.4
9.8

FK T
JS T
DS 6
FS C

Lt.

Feb. 3, 1964
Feb. 4, 1964

Rt. 8

20.6	19.2	17.3	15.1	13.3	10.8	08.8	07.8
3.2	4.6	6.5	8.7	10.5	13.0	14.9	16.0
75	56	34	14		18	34	44

07.1	07.1
16.7	16.7
75	62

Iron Pin at End Fe,

Top N.E. Cor. Garage Stoop Conc. Ho # 1766 Date

Iron Pin at Fe Post

18.1	17.2	15.8	13.9	12.5	11.3	09.9	08.7	08.9
5.3	6.2	7.6	9.5	10.9	12.1	13.5	14.7	14.5
75	67	50	35	18		31	59	75

13.9	12.6	11.2	09.5	08.7	07.4	07.3	06.3	05.6	05.3
9.5	10.8	12.2	13.9	14.7	16.0	16.1	17.1	17.8	18.1
75	60	45	33	18		21	40	53	75

01.3	08.8	08.1	07.5	07.1	06.6	07.0	07.4	08.5	00.0
26	5.1	5.8	6.4	6.8	7.3	6.9	6.5	5.4	3.9
68	49	39	28	13		16	28	46	58

01.9
2.0
75

700.7
32
75

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		903.89		
--	--	--------	--	--

				9.8
--	--	--	--	-----

9+85				
------	--	--	--	--

10				
----	--	--	--	--

✓				
---	--	--	--	--

+19				
-----	--	--	--	--

✓				
---	--	--	--	--

+53				
-----	--	--	--	--

T.P.	11.55	913.30	2.14	901.75
------	-------	--------	------	--------

Feb. 4, 1964

LT

2

9

897.9	90.5	95.7	92.8	91.5	90.2	90.19	89.2	89.8	91.2	94.2
6.0	7.4	8.2	11.1	12.4	13.7	14.7	14.1	12.7	9.7	
75	63	52	35	17		13	28	49	75	

903.8	93.4	91.6	90.2	89.1	88.6	87.7	87.1	87.1	87.4
0.1	0.5	12.3	13.7	14.8	15.3	16.2	16.8	16.8	16.5
75	70	47	31	16		15	35	53	69

87.3
16.6
75

92.9	90.9	89.1	88.1	88.0	87.9	88.0	87.7
11.0	13.0	14.8	15.8	15.9	16.0	15.9	16.2
75	57	33	15		20	37	54

87.0
16.9
75

87.2
16.7
67

95.4	93.9	92.1	90.7	91.0	92.0	94.1	93.6	92.9
5.5	10.0	11.8	13.2	12.9	11.9	9.8	10.3	11.2
75	60	38	17		12	31	54	75

Sta	+	π	-	Elev
-----	---	-------	---	------

913.30

11

2.4

BM

5.27 908.03

+23

+45

+61 See Page #51 for X-sec.

+79

BM	0.48	908.51	5.27	908.03
----	------	--------	------	--------

12

T.P.	1.92	897.93	12.50	896.01
------	------	--------	-------	--------

+35

T.P.	0.52	885.24	13.21	884.72
------	------	--------	-------	--------

T.P.	1.15	873.21	13.18	872.06
------	------	--------	-------	--------

FR
JS
FS
DS

Lt

Feb. 4, 1964
Feb. 6, 1964
Rt 10

06.1	04.8	03.1	01.7	01.7	02.1	02.5	02.4	02.3
72	85	102	116	116	112	108	109	110
75	59	37	17	✓	15	42	62	75
Bent Spike in 10" Elm 56' Lt Sta 11+28								

07.7	06.7	06.2	05.8	05.8	06.3	06.0	05.9	05.6
56	66	71	75	75	70	73	74	77
75	57	40	18	✓	23	48	68	75

04.5	05.3	04.1	04.8	07.8	08.8	09.1	08.7	08.3	08.1
88	80	72	65	55	45	42	46	50	52
75	63	47	35	17	✓	22	42	69	75

09.8	01.8	04.4	05.8	07.3	08.5	08.9	08.4	08.3	08.4	08.7
135	115	89	75	60	48	46	49	50	49	46
75	57	41	25	12	✓	22	32	45	61	75
Bent Spike in 10" Elm 56' Lt Sta 11+28										

08.5	06.2	08.0	00.2	02.1	02.8	02.6	03.3	04.6
14.8	12.3	10.5	8.3	6.4	5.7	5.9	5.2	3.9
75	57	36	13	✓	17	33	55	75

07.1	07.8	09.9	03.1	04.7	06.0	06.4	07.2	08.6
20.8	20.1	18.0	14.8	13.2	11.9	11.5	10.7	8.3
75	58	35	15	✓	14	34	52	75
± 35 Spike								

Sta + π - Elev.

873.21

12+62

NE 00

+74

SE 20

755
227
513

13

33
27
2

+50

14

+35

TP 13.46 884.44 2.23 870.98

Feb. 6, 1964

11

RT 11

69.0	68.8	68.1	68.1	68.9	71.4	73.8	75.8	79.2
4.2	4.4	5.1	5.1	4.3	1.8	10.6	12.6	6.0
75	64	43	20	✓	12	35	54	75

68.9	67.8	68.1	67.5	67.0	67.0	69.0	71.7	73.7
4.3	5.4	5.1	5.7	6.2	6.2	4.2	1.5	10.5
75	60	41	20	✓	30	41	57	75

67.9	67.6	67.7	66.9	66.6	66.0	65.7	66.1	66.7
5.3	5.6	5.5	6.3	6.6	7.2	7.5	7.1	6.5
75	62	42	18	✓	21	42	66	75

68.7	68.0	67.5	67.2	67.2	66.0	65.4	65.4	66.0
4.5	5.2	5.7	6.0	6.0	7.2	7.8	7.8	7.2
75	53	32	14	✓	4	17	40	59

70.7	70.0	68.8	69.3	68.6	67.6	67.1	67.2	67.8
2.5	3.2	4.4	3.9	4.6	5.6	6.1	6.0	5.4
75	53	28	4	✓	8	22	43	62

72.4	72.3	71.6	71.0	70.7	71.2	70.9	69.8	69.3
0.8	0.9	1.6	2.2	2.5	2.0	2.3	3.4	3.9
75	70	48	38	10	5	✓	6	23

Spike 2 14+34.64

67.3
5.94
75

Sta + π - Elev.

884.44

14 + 62

✓

15

✓

T.P. 10.25 894.28 0.41 884.03

+50

1.26 893.02 (893.06)

FA
FS
DS
WS

Feb. 7, 1964

44

RY

12

74.4.

74.2.

74.1.

74.2.

74.5.

74.7.

72.9.

72.1.

71.9.

10.0
52

10.2
40

10.3
17

10.2
7

9.9

10.7
5

11.5
13

12.3
30

12.5
48

74.9.

9.5
75

69.5.

71.4.

14.9 12.0
75 58

79.1.

78.6.

79.2.

79.8.

78.9.

78.8.

78.1.

78.3.

78.0.

5.3
32

5.8
26

5.2
8

4.6
4

5.5

5.6
5

6.3
17

6.1
28

6.4
40

79.2.

79.4.

5.2
57

5.0
75

75.4.

76.7.

77.5.

9.0
75

7.7
65

6.9
51

TOP STAKE # 15739

84.1.

83.6.

83.9.

83.8.

84.8.

84.5.

84.7.

84.2.

84.3.

10.2
45

10.7
28

10.4
18

10.5
8

9.5

9.8
3

9.6
7

10.1
12

10.0
23

83.9.

84.1.

84.5.

81.7.

82.6.

83.8.

10.4
57

10.2
71

9.8
75

12.6
75

11.7
56

10.5
39

N.E. COR. LOWER STEP 140 # 1822 (BACK)

Sfa + π - e/ev

B.M. 1.98 895.04

893.06

16

+24

✓

+4/2

✓

+6.3

Feb. 7, 1964

Lt

Q

Rt

13

N.E. COR. LOWER STEP HO # 1822 (Back End)

87.3.	86.6	86.1	85.5	85.3	86.0	87.4	87.7	87.6	87.0	86.1	85.4
77	84	89	9.5	97	9.0	76	73	74	8.0	8.9	9.6
78	69	53	33	11	6	✓	5	15	31	51	75

86.7	86.5	86.1	86.1	87.1	89.0	88.9	89.2	88.7	87.4	86.2
8.3	8.5	8.9	8.9	7.9	6.0	6.1	5.8	6.3	7.6	8.8
65	58	36	14	7	6.0	5	10	13	28	47

8.8									84.5	85.4
8.2									10.5	9.6
78									15	62
HO.										

91.0	90.4	89.5	89.3	89.8	90.6	89.9	89.0	88.0	86.7	85.6
40	46	5.5	5.7	5.2	4.4	5.1	6.0	7.0	8.3	9.4
69	53	34	12	7	4.4	5	15	29	41	55

91.4									88.4	
3.6									11.6	
78									75	
HO.										

92.3	91.3	90.2	89.5	90.9	90.4	89.8	86.3	84.8	82.4
2.1	3.2	4.8	5.5	4.1	4.6	6.2	8.7	10.2	12.6
75	54	31	15	✓	6	21	38	53	75

Sta + π - elev

895.04

17

+25

+75

1.27 893.77

893.75

T.P 4.96 891.60 8.40 886.64

+55

+83

18

Feb. 7, 1964

LT

£

RT

14

90.7	90.2	89.3	89.4	90.5	89.6	85.9	83.4	82.2	80.5
4.3	4.8	5.7	5.6	4.5	5.4	9.1	11.6	12.8	14.5
75	51	28	6	✓	9	33	52	63	75

88.8	88.2	88.7	88.7	90.0	88.2	84.5	80.9	78.0
5.2	5.8	6.3	6.3	5.0	6.8	10.5	14.1	17.0
75	53	31	8	✓	13	31	51	75

M.H. N. RIM 100' LT

ROCK 17+90 LT 30'

89.6	88.6	84.7	84.7	87.3	86.7	84.9	82.2	78.6	78.0	77.4
2.0	3.0	3.9	3.9	4.3	4.9	6.7	9.4	13.0	13.6	14.2
75	56	44	32	15	✓	6	21	40	55	75

89.7	88.3	87.1	85.5	85.0	83.7	82.1	80.9	79.3	78.5	78.4
1.9	3.3	4.5	6.1	6.6	7.9	9.5	10.7	12.3	13.1	13.2
75	60	51	32	12	4	✓	13	34	57	75

90.0	88.1	86.2	84.8	84.5	83.6	82.4	81.1	79.9	79.9	80.3	80.5
1.6	3.5	5.4	6.8	7.1	8.0	9.2	10.5	11.7	11.7	11.3	11.1
75	62	50	32	13	3	✓	14	30	48	62	75

Sta + π - elev

891.60

18+17

+50

+75

T.P. 10.47 897.79 4.28 887.32

19

+38

18+88⁺ MH 65' Lt

8.78

89.01

FK
JS
DS

Feb. 10, 1964
Feb. 10, 1964
Clear Cool 15°

LT

RT

15

89.6	88.4	84.6	84.9	84.2	83.3	82.6	82.3	82.8	81.7	81.6
2.0	2.2	5.0	6.7	7.4	8.3	9.0	9.3	8.8	9.9	10.0
75	65	50	29	11		14	33	41	61	75

71.6	89.4	87.3	86.6	85.4	86.1	86.4	86.1	85.4	84.5	83.6	82.8
0.0	2.2	4.3	5.0	6.2	5.5	5.2	5.5	6.2	7.1	8.0	8.8
75	65	52	36	18	8		14	28	47	60	75

94.1	89.9	88.4	87.6	87.0	86.4	87.0	86.0	84.8	83.7	84.1	84.4
12.5	1.7	3.2	4.0	4.6	5.2	4.6	5.6	6.8	7.9	7.5	7.2
75	64	55	40	25	5		9	24	51	65	75

TOP NAIL 18+71.52

91.6	88.0	87.1	86.6	85.9	85.5	84.8	84.6	84.5	85.0
8.2	9.8	10.7	11.2	11.9	12.3	13.0	13.2	13.3	12.3
54	36	21	6		10	17	32	56	75

93.1	93.4	93.7
4.7	4.4	4.1
62	70	75

93.3	93.4	89.7	88.1	87.9	87.6	86.6	86.0	85.6	85.4
4.5	4.4	8.1	9.7	9.9	10.2	11.2	11.8	12.2	11.9
54	53	41	22	7		12	29	50	67

93.6	93.6	85.8
4.2	4.2	12.0
70	75	75

Sta + π - elev

897.79

19+72

✓

20

✓

+31

12.56

1.96

15.6

✓

Feb. 10, 1994

Lt				Rt			
92.9	90.5	90.0	89.8	89.9	91.2	88.2	87.9
4.9	7.3	7.8	8.0	7.9	8.6	9.6	9.9
42	33	19	5		2	9	27

92.6	93.2	93.1				86.4	86.1
5.2	4.6	4.7				11.4	11.7
43	61	75				75	61

92.3	92.6	91.2	90.5	89.1	89.1	87.5	87.0	85.6	84.6
5.5	5.2	6.6	7.3	8.7	8.7	10.3	10.8	12.2	13.2
32	31	24	13	5		11	26	43	61

92.7	92.7	92.9	92.8					84.5
5.1	5.1	4.9	5.0					13.3
51	65	74	75					75

92.4	92.0	92.3	90.2	89.8	86.9	85.6	85.3	84.0	82.2
5.4	5.8	5.5	7.6	10.0	10.9	12.2	12.5	13.8	15.6
40	22	20	11	4		7	20	26	41

92.3	92.2	92.5	94.2	94.9			90.4	91.1
5.5	5.6	5.3	3.6	2.9			2.4	6.7
53	61	62	69	75			7.5	52.5

79.8
 18.0
 75
 59
 20.5
 17.3
 59
 20.5
 17.3
 59

Sta + π - Elev.

892.79

20+72

✓

+55 MH 122+

5.84 91.95 - TOP
- $\frac{10.50}{81.45}$ INV.

21

✓

+36

✓

✓

Feb. 10, 1964

LT

2

81

17

92.0.

91.9.

92.1.

91.8.

91.1.

90.1.

89.5.

89.2.

85.6.

83.8.

5.8 5.9 5.7 6.0 6.7 7.7 8.3 10.6 12.2 14.0
30 11 9 7 6 5 9 27 41

91.9.

92.2.

92.4.

78.1.

80.0.

81.9.

5.9 5.6 5.4
42 71 75

19.7 17.8 15.9
75 65 52

92.1.

91.7.

92.0.

91.9.

92.1.

91.5.

89.9.

87.7.

87.0.

84.0.

5.7 6.1 5.8 5.9 5.7 6.3 7.9 10.1 10.8 13.8
44 42 21 4 3 10 15 27 41

92.7.

93.6.

78.1.

80.9.

5.1 4.2
51 75

19.7 16.9
75 59

92.1.

92.0.

91.7.

91.8.

92.0.

91.9.

92.2.

91.1.

88.3.

5.7 5.8 6.1 6.0 5.8 5.9 5.6 6.7 9.5
40 36 34 18 2 3 7 18

94.6.

95.5.

95.5.

80.3.

82.5.

84.7.

86.0.

3.2 2.3 2.3
55 69 75

12.5 15.3 13.1 11.8
53 43 27 27

76.2.

21.6
75

Sta + π - Elev

897.79

21+60

✓

+86

✓

TP 4.73 897.96 4.56 893.23

13.36
0.38

20+67 Profile N. Curb Pineview Court

Feb 10, 1964

14

BT

18

92.3.

92.1.

91.7.

91.8.

92.1.

91.9.

92.2.

91.4.

89.8.

5.5 5.7 6.1 6.0 5.7 5.9 5.6 6.4 8.0
35 30 29 12 8 9 12 20

93.1.

93.5.

94.6.

96.5.

96.5.

75.4.

79.4.

81.8.

83.4.

88.1.

4.7 4.3 3.2 1.3 1.3 22.4 18.4 16.0 14.4 9.7
37 40 45 62 75 75 60 42 40 25

93.7.

92.4.

92.1.

91.7.

92.0.

92.2.

92.2.

92.6.

92.0.

90.5.

91.23.

4.1 5.4 5.7 6.1 5.8 5.6 5.6 5.2 5.8 7.3 6.56
39 33 29 28 11 7 8 12 21 24
MH 22/14

96.2

97.4

98.4

73.1.

76.8.

78.8.

80.8.

84.7.

88.2.

1.6 0.4 +0.6 2.47 2.10 1.90 1.70 1.31 9.6
47 64 75 75 65 52 47 37 28

21+81-22.81 Ho

94.78

93.34

92.49

92.23

91.93

3.18 4.62 5.47 5.73 6.03
115 90 70 Curb 50
Curb 60 Curb

95.19.

2.77
122

Curb = 6 "Bit"

Sta + π - Elev.

897.96

22.

✓

+94

✓

✓

+41

✓

✓

Feb. 10, 1964

2

14

15

19

95.0	92.1	91.6	92.0	92.25	92.3	92.7	91.6	90.6
3.0	5.9	6.4	6.0	5.71	5.7	5.3	6.4	7.4
41	27	26	10		8	9	15	22

97.3.
 0.7
 58

97.4
 +.46
 75

76.9
 21.1
 58

78.3
 19.7
 53

84.1
 13.9
 40

87.6
 10.4
 31

74.3
 23.7
 68

77.9
 26.1
 81

66.6
 31.4
 105

64.8
 32.2
 114

62.1
 35.9
 153

63.4
 34.6
 133

94.4	91.3	91.3	92.0	92.5	92.6	92.2	92.6	91.8	87.8	86.6
3.6	6.7	6.7	6.0	5.5	5.4	5.8	5.4	6.2	10.2	11.4
36	22	20	19	8		11	12	16	24	35

96.4
 1.6
 49

97.9
 0.1
 67

98.8
 +.05
 75

74.8
 23.2
 68

78.6
 19.4
 57

82.3
 15.7
 46

85.6
 12.4
 40

73.7
 24.3
 72

71.3
 26.7
 83

70.2
 27.8
 95

67.2
 30.8
 109

Sta + π - Elev.

897.96

22+66

✓

✓

+91 MH RT

23.46 74.50

23

✓

✓

Feb. 10, 1964

LA

51

20

90.7.	90.7.	92.3.	92.8.	93.0.	92.5.	93.0.	92.4.	92.1.	92.8.
7.3	7.3	5.7	5.2	5.0	5.5	5.0	5.6	5.9	9.2
30	27	23	12		12	13	16	20	27

92.6.	93.6.	95.8.	98.3.
5.4	4.4	2.2	10.3
32	35	49	75

84.3.	84.5.	85.0.	86.1.
13.7	13.5	13.0	11.9
46	40	35	32

100.	81.2.	79.9.	76.9.	72.4.
28.0	168	18.1	21.1	25.6
100	51	55	67	86

90.5.	90.5.	91.8.	93.0.	93.5.	93.9.	93.4.	93.8.	93.2.	88.5.
7.5	7.5	6.2	5.0	4.5	4.1	4.6	4.2	4.8	9.5
39	37	30	21	15		14	15	19	28

91.6.	93.2.	94.7.	96.3.
6.4	4.8	3.3	1.7
43	55	61	75

80.1.	81.6.	81.7.	84.3.
17.9	16.4	16.3	13.7
70	62	53	38

76.0.	73.8.	71.9.
22.0	24.2	26.1
80	91	110

Sta	+	π	-	Elev.
-----	---	-------	---	-------

Sta	+	π	-	Elev.
		897.96		

Sta	+	π	-	Elev.
23+33				

Sta	+	π	-	Elev.
23+33				
✓				

Sta	+	π	-	Elev.
✓				

Sta	+	π	-	Elev.
+63				

Sta	+	π	-	Elev.
✓				

Sta	+	π	-	Elev.
✓				

Sta	+	π	-	Elev.
TP	6.41	902.94	1.43	896.53

Sta	+	π	-	Elev.
✓				

Feb. 10, 1964

LH

£

RT

21

92.6	94.2	94.8	94.4	95.1	94.6	95.0	93.9	90.3	86.0
5.4	3.8	3.2	3.6	2.9	3.4	3.0	4.1	7.7	12.0
28	22	18.6	17.6		16	17	21	29	37

91.4	91.2	90.4	90.4	91.9	79.5	79.5	80.6	83.3
6.6	6.8	7.6	7.6	6.1	18.5	18.5	17.4	14.7
36	44	48	50	57	82	73	57	44

94.2	79.2	77.8	76.9
3.8	18.8	20.2	21.1
75	90	100	110

93.0	94.3	96.0	96.7	96.1	96.7	96.0	96.4	95.9	95.5	94.7
5.0	3.7	2.0	1.3	1.9	1.3	2.0	1.6	2.1	2.5	3.3
30	27	21	18	17		16	17	19	21	23

92.0	90.6	90.2	90.2	91.0	81.5	82.3	82.9	83.8	90.3
6.0	7.4	7.8	7.8	7.0	16.5	15.7	15.1	14.2	7.7
38	50	56	57	68	53	50	47	44	32

Ditch

91.3	81.3	79.7	78.8	78.6
6.7	16.7	18.3	19.2	19.4
75	60	69	79	93

Before T.P. 21.6 20.5 19.6 130 114 100

Sta + π - Elev.

902.94

24

✓

✓

7.95

2.85

5.1

(13.1)

+36

Feb 18, 1964

£

RT 22

97.4	98.1	98.5	98.1	98.67	97.7	98.2	97.8	96.5
5.5	4.8	4.4	4.8	4.27	5.2	4.7	5.1	6.4
26	20	17	16		17	18	19	25

96.0	94.7	93.5	91.4	89.8	85.6	86.9	89.6	94.5
6.9	8.2	9.4	11.5	13.1	17.3	16.0	13.3	8.4
30	33	40	53	65	48	43	37	28

90.3	89.8	84.6	83.3	81.5	81.0	79.7
12.6	13.1	18.3	19.6	21.4	21.9	23.2
100	84	55	70	79	88	100

97.5	900.0	900.5	900.1	900.5	99.4	99.8	99.3	97.9
5.4	2.9	2.4	2.8	2.4	3.5	3.1	3.6	5.0
28	19	17	16		17	18	19	24

94.4	92.6	90.9	89.4	85.9	84.8	88.6	90.5	93.8
8.5	10.3	12.0	13.5	17.0	16.1	14.3	12.4	9.1
34	44	57	65	57	52	46	39	31

88.5	85.4	84.0	82.4	81.2
14.4	17.5	18.9	19.5	21.7
75	67	81	93	100

Sta + π - Elev.

902.94

24+63

✓

✓

T.P. 7.67 909.52 1.09 901.85 07

BM 2.19 909.44 2.27 907.25 (907.25)

25

1315

✓

23

8.9	11.9	13.8	14.2	16.6	15.2	15.1	12.8
35	52	68	75	76	64	55	46
94.0.	91.0.	89.1.	88.7.	86.3.	87.7.	87.8.	90.1.

85.3	84.7
17.6	18.2
89	100

11.9	8.4	5.8	5.2	5.7	5.1	6.3	6.0	6.5	6.9	11.2
32	25	19	17	16	19	19	20	22	24	32
97.5	91.0	93.6	94.2	93.7	94.3	93.1	93.4	92.9	92.5	98.2

95.0 -	91.1 -	90.0	88.1	92.9 -	93.7 -	92.6 -	93.6 -	96.0 -
14.4	5	16.2	6.2	8	16.5	15.7	16.8	15.8
36	42	48	60	75	62	56	46	38

	24.0	23.0	22.1
10.5	98	89	
100	77	69	

JK

Sta + Δ - Elev

909.44

25+30

✓

✓

+60

✓

+80

FK
JS
DS

Feb. 15, 1964
Clear Cool Windy

20°

RH 24

03.9' 14' 05.8'

06.2'

05.7'

06.1'

05.8'

04.9'

05.0'

04.4'

04.1'

55 36 32 37 33 36 45 44 50 53
25 18 16 15 9 20 21 22 25

900.4' 98.4' 97.1' 95.3'

✓

02.1'

99.9'

900.4'

03.0'

9.0 11.0 12.3 14.1
31 35 41 53

7.3 10.0 9.0 6.4
50 42 36 29

890.4' 92.6' 93.7'

900.7'

899.9'

19.0 16.8 15.7
100 81 69

8.7 9.5
63 75

03.6' 06.5' 07.4' 08.2' 07.7'

08.0'

07.5'

06.4'

06.0'

06.4'

06.3'

5.8 2.9 2.0 1.2 1.7 1.4 1.9 3.0 3.4 3.0 3.1
33 25 19 16 15 13 28 30 38 45

01.4' 99.2' 97.1' 96.1'

✓

05.3'

05.5'

06.1'

8.0 10.2 12.3 13.3
37 50 63 75

4.1 3.9 3.3
75 62 48

04.6' 06.8' 08.8' 09.5' 08.9'

09.2'

08.6'

07.2'

07.7'

06.4'

06.1'

4.8 2.6 0.6 10.1 0.5 0.2 0.8 2.2 1.7 3.0 3.3
35 31 19 16 15 23 45 48 57 75

03.0' 01.4' 99.2' 97.1'

✓

6.4 8.0 10.2 12.3
42 49 60 75

Sta + π - Elev

909.44

BM 728 914.53 2.19 907.25 907.25

BM 54 Con
Dale A2

26 S Edge Rd Rt

+11.5 ϕ St Rt

+24

Lt

Feb. 11, 1964

±

R1 25

05.6°	09.0°	10.0°	10.4°	09.9°	14.39°	10.0°	09.2°	08.5°	07.6°	07.4°
8.9	5.5	4.5	4.1	4.6	4.14	4.5	5.3	6.0	6.9	7.1
32	25	19	17	15		16	31	51	71	75

03.5°	02.0°	01.3°	09.4°
11.0	12.5	13.2	15.1
38	47	59	75

04.8°	09.9°	11.0°	10.5°	11.0°	10.6°	09.7°	08.5°	07.6°
9.7	4.6	3.5	4.0	3.5	3.9	4.8	6.0	6.9
33	24	16	15		15	33	54	74

03.2°	01.4°	00.4°		01.0°	03.6°	06.2°
11.3	13.1	14.1		13.5	10.9	8.3
43	60	75		200	150	100

06.1°	07.3°	11.4°	11.8°	11.3°	11.7°	11.3°	10.3°	08.9°	07.7°	06.8°
8.4	7.2	3.1	2.7	3.2	2.8	3.2	4.2	5.6	6.8	7.7
34	30	24	16	15.5		15	29	48	65	75

08.2°	06.8°	04.7°	03.0°
6.3	7.7	9.8	11.5
38	50	67	75

Sta + π - Elev

914.53

26 +35

✓

+44

✓

T.P. 7.04 918.47 3.10 911.43

+55

1949

✓

✓

Feb. 11, 1964

Lt.

Rt.

26

088°

11.9°

12.3°

11.9°

12.3°

11.8°

10.6°

11.0°

12.1°

57

26

2.2

2.6

2.2

2.7

3.9

3.5

2.4

36

26

17

16

15

33

44

57

06.8°

04.9°

02.6°

13.0°

12.9°

77

96

11.9

1.5

1.6

47

59

75

75

71

089°

12.2°

12.8°

12.3°

12.8°

12.2°

11.4°

11.3°

11.7°

56

2.3

1.7

2.2

1.7

2.3

3.1

3.2

2.8

38

27

17

16

16

26

34

50

07.6°

04.2°

02.7°

12.7°

12.2°

6.9

9.3

11.8

1.8

2.3

40

55

75

75

64

07.7°

12.6°

13.4°

12.8°

13.5°

13.1°

12.7°

12.9°

15.0°

15.8°

10.8

5.9

5.1

5.7

5.0

5.4

5.8

5.6

3.5

2.7

35

25

17

16

13

22

24

31

43

05.2°

04.9°

02.5°

91.7°

15.6°

15.6°

13.3

23.6

26.0

26.8

2.9

2.9

40

55

72

85

75

55

90.9°

27.6

120

Sta + π - Elev.

918.47

26 + 78

120

✓

+80

✓

+87

✓

✓

Feb. 18/1964

05.72	07.2	12.5	14.1	13.5	14.2	13.9	13.6	14.6	15.4
12.75	11.3	60	44	50	43	46	49	39	3.1
40	37	30	17	16		14	23	28	32
FL245M									
93.6	92.3	92.5	92.1	97.1	✓		16.5	16.6	16.2
249	262	260	264	214			20	1.9	23
52	63	78	94	100			75	55	43

05.3	08.4	12.6	14.6	13.9	14.8	14.5	14.4	14.1	14.7
132	10.1	5.9	3.9	4.6	3.7	4.0	4.1	4.4	3.8
41	37	32	17	16		12	21	24	29
9010	9007	9032	9059	9050	✓	899.8	917.4	16.8	15.8
17.5	17.8	15.3	12.6	13.5	18.7	11.1	1.7	2.7	
48	57	61	62	70	100	75	55	37	

11.0	13.7	15.0	14.4	15.1	14.9	14.9	14.5	14.5
7.5	4.8	3.5	4.1	3.4	3.6	3.6	4.0	4.0
37	31	17	16		11	16	25	32

07.5	04.7	03.5	901.9	899.8	✓	17.3	16.9	15.4
11.0	13.8	15.0	16.6	18.7		1.2	1.6	3.1
55	75	80	81	89		75	67	49

895.0
23.5
100

899.1
19.4
93

01.3
17.2
90

Sta + π - Elev.

915.47

27+00

✓

✓

+16

✓

✓

BM 12.08 925.78 477 913.70 (913.70)

Feb. 15, 1964

44

84 28

11.6	14.2	15.7	15.1	15.82	15.7	15.3	15.0	15.7
6.9	4.3	2.8	3.4	2.65	2.8	3.2	3.5	2.8
35	27	18	17		15	26	38	60

08.7	06.5	09.1	07.9
9.8	12.0	19.4	20.6
52	53	67	79

✓

16.3
2.2
75

01.4	02.1	09.6
17.1	16.4	18.9
100	95	89

15.5	16.3	16.7	16.0	16.9	16.4	16.4	14.17	14.2
3.0	2.2	1.8	2.5	1.6	2.1	2.1	4.30	4.3
29	19	18	17		15	22	24	27

25

✓

12.3	09.5	08.8	06.8	07.3	16.8	16.8	18.2	17.9
6.2	9.0	9.7	11.7	11.2	1.7	1.7	0.3	0.6
36	40	44	49	54	49	42	34	32

02.9	05.1	07.5	09.3
15.6	13.4	11.0	9.2
100	86	67	55

Top Hyd NE Cor Daley A2

17.3	19.7	20.0	19.8	17.2
1.2	1.2	1.5	1.3	1.3
Wall	Wall	Wall	Wall	75
52	65			

Sfa + π - Elev.

^{.78}
925.89

27+30

✓

+55

✓

28

223

1354
22
11.3

✓

JP 13.54 ^{.09} 937.16 2.23 ^{.55} 923.62

FX
JS
DS
FS

Feb. 13, 1964

2+

4

RT

29

15.6	17.0	17.3	16.7	17.7	17.0	15.8	17.4	19.5	19.2
10.2	8.8	8.5	9.1	8.1	8.8	10.0	8.4	6.3	6.6
32	21	19	18		14	23	26	34	47

13.7	12.6	11.3	10.1	9.5	✓	22.9	22.2	21.4
12.1	13.2	14.5	15.7	16.3		2.9	3.6	4.4
37	46	58	69	75		75	68	54

16.4	17.2	18.1	18.6	17.9	19.1	18.4	17.4	18.7	20.7	23.0
9.4	8.6	7.7	7.2	7.9	6.7	7.4	8.4	7.1	5.1	2.8
44	37	22	20	19		15	23	27	33	38

15.0	15.8	12.4	✓	24.5	24.1	23.9
10.8	12.0	13.4		1.3	1.7	2.4
56	66	75		75	65	52

23.0	20.2	20.7	20.0	20.7	21.5	20.7	20.0	20.7	24.9	28.4
2.8	5.6	5.1	5.8	5.1	4.3	5.1	5.8	5.1	0.9	12.6
31	24	21	20	14		16	23	27	35	43

23.6	22.4	22.9	22.9	19.1	19.9	31.1	29.7	28.8
2.2	3.4	2.9	2.9	6.7	5.9	15.3	13.9	13.0
36	42	51	61	69	75	75	65	55

Sta + π - Elev

^{.09}
~~937.76~~

11.3

28+17

72
57

✓

+ 30

✓

+ 40

✓

12.83

0.37

12.46

Feb. 13, 1964

Lt

2

RT

30

26.4	21.3	21.5	20.9	21.8	22.5	21.6	20.7	21.4	22.7
10.7	15.8	15.6	16.2	15.3	14.6	15.5	16.4	15.7	14.4
36	25	22	21	13		15	23	26	31

✓

25.7	25.2	24.3	23.6	34.4	33.6	31.5	31.7	29.6	26.0
11.4	11.9	12.8	13.5	27	35	5.6	5.4	7.5	11.1
42	60	72	75	75	68	51	46	41	35

28.0	22.2	21.8	21.6	22.5	23.1	22.3	21.4	22.4	24.5	27.7
9.1	14.9	15.3	15.5	14.6	14.0	14.8	15.7	14.7	12.6	9.4
36	25	22	21	13		14	24	27	38	49

✓

28.0	27.9	26.3	25.5	35.1	35.5	34.1	31.8
9.1	9.2	10.8	11.6	20	1.6	3.0	5.3
50	61	68	75	75	69	59	58

25.1	23.3	22.2	22.9	23.7	22.8	22.1	23.1	25.1
12.0	13.8	14.9	14.2	13.4	14.3	15.0	14.0	12.0
29	26	21	15		14	23	26	32

✓

29.2	28.3	28.5	27.2	26.6	34.6	35.6	35.5	32.2	27.2
7.9	8.8	8.6	9.9	10.5	2.5	1.5	1.6	4.9	9.9
37	51	62	69	75	75	64	52	45	37

Sta + π - Elev

937.^{.09}16

28+72

✓

+87

✓

29

✓

Feb. 13, 1964

✓

B1 31

26.0	24.5	24.1	24.8	25.7	24.7	24.0	24.8	30.6
11.1	12.6	13.0	12.3	11.4	12.4	13.1	12.3	6.5
29	24	21	14		15	23	26	37

✓

30.2	29.3	29.0	28.6	27.5	27.3	37.5	38.0	40.9	35.7
6.9	7.8	8.1	8.5	9.6	9.8	10.4	10.9	13.8	1.4
36	41	51	61	70	75	75	69	58	47

29.6	28.8	26.3	24.7	25.9	26.5	25.6	24.8	25.7	27.9
7.5	8.3	10.8	12.4	11.2	10.6	11.5	12.3	11.4	9.2
36	32	27	21	11		15	24	26	40

✓

28.9	29.0	29.1	28.1	27.5		37.4	35.0	32.3
8.2	8.1	8.0	9.0	9.6		10.3	2.1	4.8
41	50	60	67	75		75	66	57

29.1	27.5	25.7	25.3	26.5	27.1	26.6	25.4	26.7	28.3	30.4
8.0	9.6	11.4	11.8	10.6	10.0	10.5	11.7	10.4	8.8	6.7
32	28	24	21	11		11	24	27	45	59

✓

30.2	29.0	29.1	28.8	27.9	27.0		34.6	33.3
6.9	8.1	8.0	8.3	9.2	10.1		2.5	3.8
36	41	50	61	66	75		75	71

Sta + π - Elev

^{.09}
937.16

29+20

✓

+54

127
128

✓

+79

Feb. 13, 1964

17

4

32

31.5	30.0	27.8	26.7	27.9	28.4	27.9	26.7	27.6	29.5	30.8
56	71	93	104	92	87	92	104	95	76	63
37	31	26	22	12		11	23	26	39	50

30.3	30.5	30.2	28.7	27.7		33.5	33.1	37.0
6.8	6.6	6.9	8.4	9.4		3.6	4.0	0.1
42	52	63	69	75		75	67	60

34.6	33.1	29.8	28.8	29.7	30.4	29.7	28.8	29.4	29.8	34.6
25	40	73	83	74	67	74	83	77	73	25
37	33	28	22	13		11	22	25	31	36

33.1	32.9	32.1	30.3		38.7	38.8	38.5	37.1
4.0	4.2	5.0	6.8		11.6	11.7	11.4	10
43	54	63	75		75	66	50	40

35.0	34.1	31.2	30.1	31.1	31.8	31.4	30.5	31.6	32.6	35.4
21	30	59	70	60	53	57	66	55	45	17
39	32	25	22	11		10	22	25	31	35

34.0	33.6	32.7	31.9	30.9		40.2	39.9	39.0	37.3
3.1	3.5	4.4	5.2	6.7		13.1	12.8	11.9	10.2
45	54	64	67	75		75	62	53	40

Sta + π - Elev

^{.09}
937.16

30+00

✓

T.P. 12.82 ^{.54} 949.58 0.37 ^{.72} 936.79

12.5

54

54

+22

✓

+66

BM

184

974.75

Feb. 13, 1964

11

A

RT

33

38.7-	35.6-	32.5-	31.3-	32.5-	33.1-	32.4-	31.8-	32.6-	33.7-	36.0-
11.6	1.5	4.6	5.8	4.6	4.0	4.7	5.3	4.5	3.4	1.1
40	32	26	22	10		12	22	25	33	40

34.6-	36.3-	35.6-	34.4-	33.8-	40.8-	40.4-	39.6-	38.0-
0.5	0.8	1.5	2.7	3.3	13.7	13.3	12.5	10.9
47	55	65	68	75	75	64	53	42

41.0-	37.5-	33.7-	32.5-	33.6-	34.2-	33.6-	32.7-	33.5-	34.7-
8.5	12.0	15.8	17.0	15.9	15.3	15.9	16.8	16.0	14.8
42	35	27	23	13		11	22	24	34

39.3-	38.0-	36.9-	36.0-	41.4-	41.2-	40.1-	38.5-	36.7-
10.2	11.5	12.6	13.5	8.1	8.3	9.4	11.0	12.8
48	61	69	75	75	67	55	46	39

42.0-	39.7-	35.7-	35.0-	36.1-	36.7-	36.2-	35.4-	36.0-	37.3-
7.5	9.8	13.8	14.5	13.4	12.8	13.3	14.1	13.5	12.2
40	34	25	23	12		11	22	24	33

44.1-	42.9-	41.9-	40.9-	39.9-	43.0-	42.6-	41.8-	40.0-
5.4	6.6	7.6	8.6	9.6	6.5	6.9	7.7	9.5
44	49	59	68	75	75	68	53	43

Sta + π - Elev

~~949.58~~

31

69

✓

+50

✓

BM 6.84 954.56 1.84 947.74 ^{.70} 947.72

+68 S. Gutter Ryan Ave.

✓

Feb. 3, 1964

LT

+

RT 34

40.5	37.3	36.8	37.8	38.6	38.2	37.1	38.2	39.2	41.5
9.0	12.2	12.7	11.7	10.9	11.3	12.4	11.3	10.3	8.8
31	24	22	13		10	21	23	32	4

45.6	44.5	43.7	42.5	41.6	✓	44.34	43.8	42.9
3.9	5.0	5.8	7.0	7.9		5.20	5.7	6.6
42	47	50	67	75		Walt	63	50
						74		

45.7	47.7	40.5	40.0	40.8	41.2	40.8	40.0	40.8	42.0	43.92
3.8	1.8	9.0	9.5	8.7	8.3	8.7	9.5	8.7	7.5	5.62
46	38	25	22	12		10	20	23	34	Walt
										44

49.6	43.0	41.4	✓	49.6	44.0
4.9	6.5	8.1		4.9	5.5
61	65	75		75	57

Top Hyd NECu Ryan + Dole St.

49.4	42.6	41.9	42.6	43.2	42.9	42.2	42.8	43.7
5.2	12.0	12.7	12.0	11.4	11.7	12.4	11.8	10.9
40	27	23	14	12.4	8	22	36	57

47.3	45.7	44.4	41.9	✓	44.7
7.3	8.9	10.2	12.7		9.9
46	60	65	75		74

Sta + π - Elev.

954.56

32 3' S. of Approx $\perp$ Ryan Ave

✓

+20 N. Gutter Ryan Ave.

✓

BM 11.18 958.90 6.84 947.72

+50

FK
JS
DS

Feb. 13, 1964
Feb. 14, 1964

BT 35

49.3	43.1	42.5	43.3	43.9	43.9	42.9	43.5	44.6
5.3	11.5	12.1	11.3	10.7	11.2	11.7	11.1	10.0
40	26	23	13		9	19	40	62

47.7	46.7	44.6	43.2			47.0	46.38
6.9	7.9	10.0	11.4			7.6	8.18
47	58	66	75			100	88

50.0	49.8	44.6	43.3	44.1	44.8	44.3	43.8	43.8	44.4
4.6	4.8	10.0	11.3	10.5	9.8	10.3	10.8	10.8	10.2
40	38	27	23	14		10	20	40	61

48.1	47.2	45.6	43.9			45.2
6.5	7.4	9.0	10.7			9.4
46	60	65	75			75

Top Hyd NE Cor Dale & Ryan Ave.

47.0	45.4	44.7	46.5	46.1	45.5	44.7	45.4	46.7
11.9	13.5	14.2	13.4	12.8	13.4	14.2	13.5	12.2
29	25	23	12		10	20	22	35

51.4	50.6	50.0	48.8	48.2	47.7	45.3	45.1	45.9
7.5	8.3	8.9	10.1	10.7	11.2	13.6	13.8	13.0
41	47	60	70	75	75	66	61	49

Sta + π - Elev

958.90

32+80

✓

33

✓

BM 11.17 958.89 11.17 947.73 (947.72)

T.P. 12.69 961.73 9.85 949.04

+20

✓

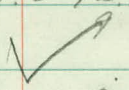
Feb. 14, 1964

2+

#

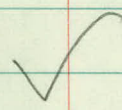
RY 36

49.1	47.1	46.1	46.8	47.3	46.8	46.9	46.7	47.9
9.8	11.8	12.8	12.1	11.6	12.1	13.0	12.2	11.0
31	25	22	11			20	22	36



55.5	54.4	54.2	53.5	53.0	46.8	45.5	45.7	47.4
3.4	4.5	4.7	5.4	5.9	12.22	13.4	13.2	11.5
44	49	61	69	75	Gar. Apron 95	75	55	49

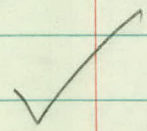
58.6	48.2	47.0	47.6	48.1	47.9	46.7	47.4	48.6
0.3	10.7	11.9	11.3	10.8	11.5	12.2	11.5	10.3
48	25	22	11		12	20	24	37



57.5	57.2	55.5		49.0	49.3	49.3
1.4	1.7	3.4		9.9	9.6	9.6
54	68	75		75	67	50

Top Hy. NE, Cor. Ryan Ave

60.2	49.1	47.6	48.2	48.7	48.1	47.3	48.0	49.0
1.5	12.6	14.1	13.5	13.0	13.6	14.4	13.7	12.7
50	26	22	12		12	20	25	34



59.3	58.4	57.5		51.0	50.7	49.7
2.4	3.3	4.2		10.7	11.0	12.0
54	68	75		75	64	50

Sta + π - Elev.

96173

33+55

✓

+81 N Edge Ent Rt

✓

+96

✓

Feb 18, 1964

2

84

37

60.9.

49.8.

48.6.

49.2.

49.8.

49.4.

48.8.

49.2.

49.7.

0.8

11.9

13.1

12.5

11.9

12.3

12.9

12.5

12.0

51

23

22

12

11

20

23

39

59.4

58.4

57.9

51.9

50.5

2.3

3.3

3.8

9.8

11.2

58

70

75

75

56

61.1

50.6

49.3

49.8

50.4

49.9

49.4

49.7

50.3

0.6

11.1

12.4

11.9

11.3

11.8

12.3

12.0

11.4

49

24

20

11

12

21

26

37

59.9

58.4

52.47

51.90

51.29

50.55

1.8

3.3

9.26

9.83

10.44

11.18

56

75

84

75

60

cinc

Gar,

44

60.4

51.7

49.7

50.2

50.7

50.2

49.7

50.5

52.4

1.3

10.0

12.0

11.5

11.0

11.5

12.0

11.2

9.3

48

26

20

11

12

20

23

32

59.6

58.4

57.8

58.6

58.3

57.8

56.5

54.7

2.1

3.3

3.9

21

24

39

52

7.0

57

69

75

40

75

71

60

47

77

Sta + x - Elev.

961.73

34

✓

BM 3.64 959.28 6.07 955.66 (955.64)

+19

✓

+44

✓

166 W50 9' Lt. 2.52 51.76

Feb. 14, 1964

✓

RT 38

54.8.	51.9.	49.8.	50.2.	50.8.	50.3.	49.9.	50.7.	53.1.
6.9	9.8	11.9	11.5	10.9	11.4	11.9	11.0	8.6
35	27	20	11		11	20	24	35

✓

58.0.	56.9.	55.5.		58.3.	56.7.	55.4.
37	4.8	6.2		34	50	63
47	59	75		25	61	52

Top Hy d NE Cor Mounds View + Date St

52.2.	51.9.	51.5.	50.3.	50.6.	51.2.	50.5.	50.2.	51.1.	51.3.	54.5.
7.1	7.4	7.8	9.0	8.7	8.1	8.8	9.1	8.2	8.0	4.8
60	47	26	21	14		14	19	21	25	44

✓

52.0.		58.3.	57.4.
7.3		1.0	1.9
75		75	65

51.8.	51.5.	51.5.	50.8.	51.1.	51.7.	51.2.	50.7.	51.6.	53.2.
7.5	7.8	7.8	8.5	8.2	7.6	8.1	8.6	7.7	6.1
65	50	23	20	13		12	20	23	38

✓

51.8.		57.2.	55.9.
7.5		2.1	3.4
75		75	56

Sta + π - Elev.

959.28

34+69 Gutter Line Rt

+84 $\pm$ Rt

✓

+95

35

+22

Feb. 14, 1964

LT

RT

39

52.3	52.0	52.0	52.1	51.3	51.7	52.0	51.8	51.5	51.8	52.6	53.0
70	73	73	72	8.0	7.6	7.3	7.5	7.8	7.5	6.7	6.7
75	62	43	24	20	13	9	19	40	63	75	

52.2	52.3	52.3	51.7	51.9	52.3	51.9	51.9	51.9.5	52.4
7.1	7.0	7.0	7.6	7.4	7.0	7.4	7.4	7.33	6.9
57	40	23	20	13	12	23	W50	52	

52.4									
69									
75									

52.3	52.6	52.2	52.2	51.8	52.1	52.4	52.0	52.0	52.1	52.5	53.1
70	6.7	7.1	7.1	7.5	7.2	6.9	7.3	7.3	7.2	6.8	6.2
75	57	42	24	19	13	11	21	33	52	75	

52.7	52.5	52.3	52.1	51.9	52.1	52.4	52.1	52.0	52.6.8	53.5	54.1	54.1
6.6	6.8	7.0	7.2	7.4	7.2	6.9	7.2	7.3	6.6	5.8	52.4	
75	58	44	25	19	13	10	22	W50	48	63	75	

52.5	52.5	52.4	52.1	52.3	52.6	52.3	52.1	53.1	55.2	57.3
6.8	6.8	6.9	7.2	7.0	6.7	7.0	7.2	6.2	4.1	2.0
60	46	27	19	13	10	18	22	36	57	

52.73										
6.55										
66										

Conc Approx

58.0

7.3

75

Sta	+	x	-	Elev.
-----	---	---	---	-------

				959.28
--	--	--	--	--------

35+45				
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✓				
---	--	--	--	--

+85				
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✓				
---	--	--	--	--

36				
----	--	--	--	--

✓				
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Feb. 14, 1964

Lt.

4

BT 40

52.6.	52.7.	52.1.	52.2.	52.7.	52.5.	52.3.	53.2.	54.1.	54.3.
6.7	6.6	7.2	7.1	6.6	6.8	7.0	6.1	5.2	3.0
42	23	19	12		10	17	20	26	41



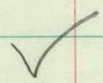
52.8.
6.5
59

52.9.
6.4
67
110

59.3.
0.0
75

58.1.
1.2
57

52.4.	52.4.	52.5.	52.0.	52.2.	52.5.	52.3.	52.1.	53.1.	53.8.	54.5.
6.9	6.9	6.8	7.3	7.1	6.8	7.0	7.2	6.2	5.5	2.8
53	35	21	19	12		9	17	20	26	46



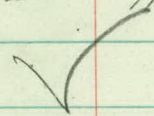
52.18.
7.10
69
conc

52.2.
7.1
75

59.4.
10.1
75

58.5.
0.8
65

52.2.	52.6.	52.5.	51.9.	52.1.	52.4.	52.2.	51.9.	52.9.	53.6.	57.8.
7.1	6.7	6.8	7.4	7.2	6.9	7.1	7.4	6.4	5.7	1.5
46	29	21	20	12		11	18	20	28	40



52.2.
7.1
61

52.15.
7.13
69
conc

52.2.
7.1
75

58.8.
0.5
75

58.9.
0.4
70

58.8.
0.5
50

Sta + π - Elev.

959.28

36+35

✓

+50

✓

+59 WSO 42' Lt 7.80 51.48

+65

✓

Feb. 14, 1964

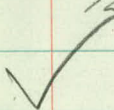
Lt.

~~2~~

RT

41

51.4.	51.6.	51.6.	51.7.	52.0.	52.1.	51.9.	51.6.	52.4.	52.8.	58.4.
79	77	77	76	73	72	74	77	69	65	09
75	60	45	28	14		12	18	24	28	42



58.4.	58.5.
09	0.8
75	59

51.1.	51.38.	51.6.	51.7.	51.8.	51.8.	52.0.	51.7.	51.4.	52.1.	52.4.	58.2.
8.2	7.9	7.7	7.6	7.5	7.5	7.3	7.6	7.9	7.2	6.9	1.1
100	78	63	41	24	14		11	19	23	28	41

MH



58.3	58.5
1.0	0.8
75	61

51.2.	51.3.	51.3.	51.3.	51.4.	51.6.	51.8.	51.5.	51.3.	51.9.	52.3.	58.1.
8.1	8.0	8.0	8.0	7.9	7.7	7.5	7.8	8.0	7.4	7.0	1.2
75	68	49	34	19	12		11	18	21	26	41



58.4.	58.4.
0.9	0.9
75	62

Sta + Δ - Elev.

959.28

36+95

✓

37

✓

BM

7.74 951.54

BM

0.78

955.23

4.82

954.46

954.45

+04

✓

Feb. 14, 1964

Lt.

Rt. 42

52.0.	51.6.	51.1.	50.8.	51.3.	51.0.	50.7.	51.3.	51.8.	54.1.
7.3	7.7	8.2	8.5	8.0	8.3	8.6	8.0	7.5	5.2
47	28	19	17		12	18	22	28	34

52.2.	52.06.	52.1.
7.1	7.22	7.2
64	70	75

Conc

57.7.	57.5.	57.2.
1.6	1.8	2.1
75	64	42

52.2.	52.0.	51.5.	51.0.	50.7.	51.2.	50.8.	50.7.	51.5.	52.9.
7.1	7.3	7.8	8.3	8.6	8.1	8.5	8.6	7.8	6.4
63	46	28	20	17		13	21	27	36

52.06.	52.1.
7.22	7.2
70	75

55.6.	55.5.	54.6.
3.7	3.8	4.7
75	71	53

Hyd NW. Cor S Pryor & Dale St.

52.1.	52.0.	51.5.	51.0.	50.6.	51.2.	50.7.	50.6.	51.6.	52.6.	53.1.
3.1	3.2	3.7	4.2	4.6	4.1	4.5	4.6	3.6	2.6	2.1
65	49	29	20	17		12	24	32	49	65

52.05.	52.1.
3.18	3.1
20	75

53.5.
1.7
75

Sta + π - Elev.

955.23

37+12

✓

+24 $\pm$ Shyer

✓

+40

+35 W 50 33' RT 4.68 50.55

+67

Feb. 14, 1964

11.

2

81

43

51.4	50.7	50.4	50.6	50.9	50.7	50.6	51.3	52.3
3.8	4.5	4.8	4.6	4.3	4.5	4.6	3.9	2.9
28	18	17	10		9	19	35	51

51.9	52.1	52.1	52.2
3.3	3.1	3.1	3.0
43	56	68	75

53.1	52.2	52.9
2.1	2.0	2.3
75	72	64

52.06	51.8	51.4	52.9	50.1	50.6	50.4	50.3	50.8	52.0	53.0
3.17	3.4	3.8	4.3	5.1	4.6	4.8	4.9	4.4	3.2	2.2
62	45	30	19	17		9	14	27	47	67

52.0	52.0
3.2	3.2
67	75

53.2	53.8	53.9	53.3
2.0	1.4	1.3	1.9
200	150	100	75

51.91	51.7	51.0	50.5	49.7	50.2	50.0	49.8	50.4	51.3	52.3
3.32	3.5	4.2	4.7	5.5	5.0	5.2	5.4	4.8	3.9	2.9
Walk 46	28	20	17		✓	11	17	35	50	75

51.3	50.6	49.5	49.0	49.3	49.6	49.2	49.8	49.2	50.1	51.2
3.9	4.6	5.7	6.2	5.9	5.6	6.0	6.4	6.0	5.1	4.0
52	38	24	17	10		9	18	22	34	53

51.63
3.60
595 conc

51.9	51.6
3.3	3.6
75	67

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		955.23		
--	--	--------	--	--

37+75				
-------	--	--	--	--

✓				
---	--	--	--	--

38				
----	--	--	--	--

✓				
---	--	--	--	--

+32				
-----	--	--	--	--

✓				
---	--	--	--	--

Feb. 14, 1964

Lt

LT

RT

44

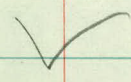
50.8.	49.4.	48.8.	49.0.	49.4.	48.9.	48.5.	49.1.	49.6.
4.4	5.8	6.4	6.2	5.8	6.3	6.7	6.1	5.6
33	20	16	11		10	17	18	26



51.4.	51.5.	51.7.
3.8	3.7	3.5
49	64	75

52.0.	52.0.	51.7.	51.4.
3.2	3.2	3.5	3.8
75	64	50	33

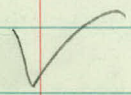
50.5.	49.8.	48.1.	48.3.	48.7.	48.1.	47.8.	48.3.	48.2.	51.3.
4.7	5.4	7.1	6.9	6.5	7.1	7.4	6.9	7.0	3.9
41	27	17	11		11	18	21	27	35



51.0.	51.4.
4.2	3.8
58	75

51.4.	51.3.
3.8	3.9
75	51

50.5.	50.2.	49.5.	48.5.	47.2.	47.7.	47.1.	46.6.	47.1.	47.9.	51.4.
4.7	5.0	5.7	6.7	8.0	7.5	8.1	8.6	8.1	7.3	3.8
75	64	44	25	17		11	18	20	28	37



51.7.	51.5.
3.5	3.7
75	54

Sta + + - Elev.

955.23

38+40

✓

+55

✓

39

✓

BM 223 949.43 8.00 947.23 947.20

Feb. 14, 1964

2

RT

45

49.7.

14

48.6.

46.9.

47.1.

47.4.

46.9.

46.4.

46.8.

48.1.

49.0.

5.5

6.6

8.3

8.1

7.8

8.3

8.8

8.4

7.1

6.2

43

26

17

11

11

18

30

51

67

✓

50.1.

50.4.

5.1

4.8

61

75

49.5.

5.7

75

49.9.

49.1.

48.1.

46.3.

46.5.

47.0.

46.4.

46.0.

46.3.

47.5.

48.9.

5.3

6.1

7.1

8.9

8.7

8.2

8.8

9.2

8.9

7.7

6.3

56

38

26

17

11

10

18

19

32

48

✓

50.1.

5.1

75

50.0.

5.2

75

49.8.

5.4

67

48.0.

46.3.

44.6.

44.8.

45.2.

44.8.

44.6.

45.0.

46.5.

7.2

8.9

10.6

10.4

10.0

10.4

10.6

10.2

8.7

42

27

17

12

12

18

21

32

✓

48.3.

48.9.

6.9

6.3

59

75

49.8.

5.4

75

49.5.

5.7

58

48.4.

6.8

43

Top Hyd. N.W. Cor. Skillman & Pale

Sta + π - Elev.

949.43

39+06

✓

+16 S. Gutter Line

✓

+24 $\angle$ Sk. Man

+35 WSO 44' Lt 5.34 44.09

+45 WSO 45' Lt 5.10 44.33

Feb. 14, 1964

FL 46

47.2.	47.3.	46.3.	44.4.	44.9.	44.5.	44.3.	44.7.	44.95.
2.2	2.1	3.1	5.0	4.5	4.9	5.1	4.7	4.48
57	41	21	17		11	19	20	MH 23



48.1.
1.3
75

49.2.
0.2
75

48.9.
0.5
59

48.4.
1.0
40

45.6.
3.8
27

44.7.	44.5.	44.2.	44.1.	44.6.	44.1.	43.8.	44.2.	44.8.	44.0.
4.7	4.9	5.2	5.3	4.8	5.3	5.6	5.2	4.6	0.4
75	55	36	17		12	20	22	26	37

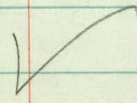


47.2.
2.2
75

47.6.
1.8
68

48.0.
1.4
47

44.6.	44.6.	44.42.	44.1.	43.9.	44.3.	44.0.	43.5.	43.8.	44.5.	48.4.
4.8	4.8	5.01	5.3	5.5	5.1	5.4	5.9	5.6	4.9	1.0
75	67	44 MH	32	16		11	20	21	27	39



44.6.
4.8
100

44.5.
4.9
150

43.8.
5.6
200

46.1.
3.3
75

46.5.
2.9
63

47.1.
2.3
48

Sta + π - Elev.

949.43

39+39

✓

BM 0.81 948.01 2.23 947.20 (947.20)

+53

✓

+81

✓

47

49.2	49.9	46.1	47.2
5.2	4.5	3.3	2.2
75	59	44	36

94.7	94.0	93.3	92.8	93.0	93.3	93.0	92.6	93.0	93.4
3.3	4.0	4.7	5.2	5.0	4.7	5.0	5.4	5.0	4.6
60	35	20	18	12		12	19	22	27

450.

3.0
7.5

43.5	43.8	44.5	46.1
4.5	42.35	1.9	
75	63.47	35	

44.1.	42.8.	42.1.	41.6.	41.8.	42.2.	41.9.	41.6.	42.0.	42.0.
3.9	5.2	5.9	6.4	6.2	5.8	6.1	6.4	6.0	6.0
35	27	19	18	12		12	20	22	26

44.8

A.S.S.

46.1.

Ab. 7.

A close-up of a handwritten lowercase letter 'v' on lined paper. The letter is formed with two strokes, starting from the middle line, going down to the bottom line, and then up to the middle line. The paper has a red vertical margin line and blue horizontal lines.

42,9.

43.0.

433.

43.9.

32	25	19	13
40	45	60	75

429.	430.	433.	439.
51	50	47	41
75	52	38	33

Sta + π - E/

948.01

39+89

✓

40

✓

+22

✓

Feb 18, 1964

Lt

L

Rt 48

42.3.

41.8.

41.3.

41.5.

41.9.

41.6.

41.3.

41.6.

41.4.

42.0.

5.7
25

6.2
19

6.7
18

6.5
12

6.1
11

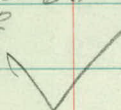
6.4
11

6.7
21

6.4
22

6.6
27

6.0
36



45.4.

46.2.

41.7.

41.6.

41.6.

2.6
45

1.8
60

6.3
75

6.4
64

6.4
52

45.4.

41.9.

41.3.

40.7.

41.0.

41.4.

41.1.

40.9.

41.3.

41.2.

41.5.

2.6
48

6.1
25

6.7
20

7.3
17

7.0
12

6.6
11

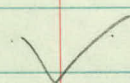
6.9
20

7.1
22

6.7
26

6.8
35

6.5



46.0.

46.9.

41.0.

41.5.

2.0
60

1.1
75

7.0
75

6.5
50

43.9.

41.0.

40.2.

39.9.

40.0.

40.5.

40.2.

40.4.

40.5.

41.0.

41.1.

4.1
41

7.0
26

7.8
20

8.1
17

8.0
12

7.5
20

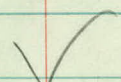
7.8
22

7.6
31

7.5
39

7.0
54

6.9



46.0.

46.8.

59.9.

40.2.

2.0
60

1.2
75

8.1
75

7.8
63

Sta + π - Elev

948.01

40+50 $\neq$ Ent Lt.

✓

+50 60' Lt

43 943.7

+50 35' Lt

66 941.4

} Cement
Block
carb.

+65

✓

41

✓

BM 6.78 944.90 9.89 938.12

Feb. 17, 1964

LT

✓

RT 49

43.6.	40.3.	39.1.	38.7.	39.3.	38.9.	38.5.	38.5.	39.2.	40.0.
44	77	89	93	8.7	9.1	9.5	9.5	88	8.0
60	23	20	16		21	24	26	31	38

45.0.

3.0
75

✓

40.1.

40.03

40.0

7.9 7.98 8.0
68 59 51
40 Conc

44.5.

43.3.

41.6.

39.9.

38.1.

38.7.

37.9.

36.9.

36.9.

37.8

3.5	4.7	6.4	8.1	9.9	9.3	10.1	11.1	11.1	10.2
60	45	35	27	18		22	24	26	28

45.1

2.9
75

✓

39.4.

39.3.

39.1.

38.7

8.6 8.7 8.9 9.3
67 59 48 34
40

44.8.

44.6.

42.6.

38.0.

36.7.

37.4.

36.9.

36.4.

35.5.

34.73

3.2	3.4	5.4	10.0	11.3	10.6	11.1	11.6	12.5	11.79
75	60	42	25	19		12	22	24	26

40

✓

35.8.

36.1.

36.6.

37.1.

36.8.

35.5

12.2	11.9	11.4	10.9	11.2	12.5
75	66	53	39	28	26

Sta + π - Elev.

94490

41+05 Ent Rt

✓

+30 Ent Rt & Lt

✓

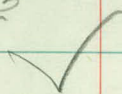
+42

✓

Feb. 17, 1964

84 50

42.1	36.3	36.6	36.8	37.2	36.8	36.3	36.2	35.8	34.8
2.8	8.6	8.3	8.1	7.7	8.1	8.6	8.7	9.1	10.1
40	69	18	12		11	21	26	29	41



42.4
1.5
50

44.5
0.4
75

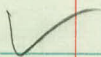
31.9
130
75

32.3
126
65

33.5
114
55

42.97	41.7	38.3	35.7	35.8	36.2	35.7	35.0	34.5	33.1
1.93	3.2	6.6	9.2	9.1	8.7	9.2	9.9	10.4	11.8
79	65	38	21	12		15	24	30	44

conc
Apron



31.8
131
75

32.3
126
58

42.0	39.8	36.7	35.1	35.3	35.7	35.1	34.6	33.8	33.5
2.9	5.1	8.2	9.8	9.6	9.2	9.8	10.3	11.6	11.4
65	40	26	19	12		13	23	24	26



40.9
4.0
75

31.6
133
75

32.3
126
54

32.8
121
50

33.3
116
41

34.0
109
30

Sta + π - Elev

944.90

41+72

✓

42

✓

T.B.M

12.06 932.84 (932.84)

BM 3.19 911.22

(908.03)

11+61

11 Φ 9.46 901.76

T.B.M. 6.16 939.00

(932.84)

42+14

Feb. 17, 1964

14

2

St. 51

39.5° 35.1° 33.9° 34.1° 34.5° 33.9° 33.5° 33.7° 33.5°

54 28 110 108 104 110 114 112 114
39 26 19 13 12 18 19 20

40.3°

41.4°

42.1°

32.1°

32.28°

32.6°

4.6 3.5 2.8
45 62 75

12.8 12.62 12.3
40 42 36

47 Conc Walk

33.6°

33.0°

32.8°

32.8°

33.3°

32.9°

33.0°

32.6°

32.1°

11.3 11.9 12.1 12.1 11.6 12.2 11.9 12.3 12.8
26 19 18 12 17 18 21 22

35.9°

38.0°

39.6°

40.5°

31.1°

31.39°

31.8°

32.2°

32.1°

9.0 6.9 5.3 4.4 13.6 13.5 13.1 12.7 12.8
33 39 50 75 75 63 45 25 24

Top NW Cor Lower Step

Bent Spike in 10" Oak 56' 14" Sta 11428

02.1° 02.6° 03.2° 04.5° 06.5° 08.5° 09.4° 10.1° 09.1° 09.0° 09.2° 09.3°

91 86 80 67 47 27 1.8 1.1 2.1 2.2 20 1.9
100 75 69 53 36 17 21 38 57 75 100

Top NW Cor Lower Step

34.6°

33.2°

32.6°

32.2°

32.2°

32.6°

32.2°

32.5°

31.6°

31.6°

31.5°

4.4 5.8 6.4 6.8 6.8 6.4 6.8 6.5 7.4 7.4 7.5
34 26 20 19 12 17 18 22 24 35

Sta + π - Elev.

939.00

42+14

+26

✓

130
45
85

✓

134
15
11.9

+40

✓

T.P.

0.25

931.17

8.08

930.92

Feb. 17/1964

21

81 52

38.3	37.8	36.9	36.8	35.5	30.6	28.9	27.5	26.5
0.7	1.2	2.1	2.2	3.5	8.4	10.1	11.5	12.5
75	59	56	52	47	47	55	69	75

34.9	32.8	32.3	31.9	31.5	31.6	32.1	31.6	32.0	31.0	28.5
4.1	6.2	6.7	7.1	7.5	7.4	6.9	7.4	7.0	8.0	10.5
51	28	26	20	19	13		17	18	23	30

36.6	36.8	37.7	37.71
2.4	2.2	1.3	1.29
55	58	61	75

23.0	23.0	21.8	26.0
16.0	16.0	17.2	13.0
57	50	41	33

20.8	20.0	20.9
18.2	19.0	18.1
62	70	75

34.3	33.3	31.5	30.8	31.0	31.4	31.0	31.3	31.0	30.5	25.6
4.7	5.7	7.5	8.2	8.0	7.6	8.0	7.7	8.0	8.5	13.4
57	42	25	19	12		17	18	19	27	36

34.45	34.9
4.55	4.1
71	77
Walk	Horse

23.3	20.6	13.9	17.1
15.7	18.4	25.1	21.9
65	59	52	46

16.3	12.7	14.5	12.4
22.7	21.3	24.5	26.6
75	78	91	100

Sta + π - Elev.

931.17

42+63 $\pm$ Ent Lt.

✓

✓

+80

✓

A3

Feb. 15, 1964

LT

Z

BT 53

31.4	31.1	30.3	29.8	30.4	29.8	30.1	28.3	21.5
+0.2	0.1	0.9	1.4	0.8	1.4	1.1	2.9	9.7
42	36	23	17		16	17	27	39

31.9	32.0
+0.7	+0.8
68	77
Gar	

✓

09.0	05.5	07.4	18.2
222	257	238	13.0
68	64	60	46

07.2	09.8	08.4	06.9
240	214	228	24.3
78	84	93	100

31.1	30.9	29.4	29.0	29.1	29.7	28.7	29.2	28.3	19.3	09.6
0.1	1.3	1.8	2.2	2.1	1.5	2.5	2.0	2.9	11.9	21.6
51	28	19	18	16		15	16	20	39	65

✓

33.1
+1.9
75

03.6	04.5	?	05.3	01.9
276	267	27	259	29.3
100	93	87	80	74

30.2	30.0	29.0	28.5	28.1	28.67	27.9	28.3	27.5	18.6
1.0	1.2	2.2	2.7	3.1	2.45	3.3	2.9	3.5	12.6
68	39	27	18	17		15	17	19	40

✓

30.3

0.9
75

01.1	04.5	10.0
30.1	26.7	21.2
100	84	62

Sta + π - Elev

931.17

43+35

✓

+70

✓

44

✓

BM

5.10 926.07

T.P. 236 926.27

7.26 929.91

+04 Gate Valve 7' Lt

Feb 12/1964

21

2

53a

29.2	27.6	27.0	26.6	27.2	26.5	27.1	25.8	24.0
2.0	3.6	4.2	4.6	4.0	4.7	4.1	5.4	7.2
41	26	19	18		13	16	19	24

29.8

1.4
70
40

900.3
30.9
100

06.3
24.9
67

15.9
15.3
42

27.6	26.3	25.2	25.4	24.8	25.8	25.0	25.3	24.2	15.1
3.6	4.9	6.0	5.8	6.4	5.4	6.2	5.9	7.0	16.1
58	41	27	21	19		15	16	20	43

28.1

26.3

3.1
71

4.9
77

04.7
26.5
100

06.5
24.7
82

09.3
21.9
64

22.7	22.9	23.5	23.2	23.7	24.5	23.9	24.2	23.3	22.5	16.4
8.5	8.3	7.7	8.0	7.5	6.7	7.3	7.0	7.9	8.7	14.8
60	39	21	20	12		16	17	22	26	41

22.0

9.2
75

08.1
23.1
100

09.9
21.3
81

12.9
18.8
56

Top Hyd S.W. Cor Belmont Lane & Dale St.

Sta + ~~A~~ - Elev.

926.27

44+18 S. Gutter Belmont

13
5
8

✓

+31

✓

+38

✓

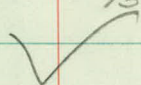
Feb. 12, 1964

21.3	21.8	22.5	23.0	23.8	23.1	23.4	22.3	13.5
50	45	38	33	2.5	3.2	2.9	4.0	12.8
75	52	23	13		16	17	25	50



08.6	10.7
17.7	15.6
100	74

21.2	21.4	21.8	22.1	22.5	23.2	22.5	22.8	21.6	13.3
51	4.9	4.5	4.2	3.8	3.1	3.8	3.5	4.7	13.0
75	65	45	24	13		15	16	25	49



08.8	10.0
17.5	16.3
100	81

21.3	21.1	21.5	21.99	22.2	22.9	22.3	22.4	21.3	19.4	14.7
5.0	5.2	4.8	4.28	4.1	2.4	4.0	3.9	5.0	6.9	11.6
75	61	38	M.H.	13		15	16	21	35	66
			17							



10.0	11.3
16.3	15.0
100	93

Sta + π_1 - Elev.

926.27

44+46 Gutter Lt

✓

+56

✓

+67

✓

Feb. 17, 1964

Lt.

✓

BT 55

21.5	21.6	21.3	21.3	21.9	22.6	21.9	22.0	19.5	16.3
4.8	4.7	5.0	5.0	4.4	3.7	4.4	4.3	6.8	10.0
67	49	35	25	12		15	16	28	51

✓

21.8

4.5
75

09.5

16.8
100

12.2

14.1
78

21.5	21.2	20.8	21.5	22.2	21.8	21.5	21.7	20.7	19.0
4.8	5.1	5.5	4.8	4.1	4.5	4.8	4.6	5.6	7.3
28	23	21	11		10	14	15	19	31

✓

21.9

4.4
42

22.4

3.9
61

22.9

3.4
75

9.6

16.7
100

12.2

14.1
81

14.3

12.0
65

16.5

9.8
50

22.4	21.5	20.9	20.5	21.0	21.7	21.4	21.1	21.3	20.6	19.2
3.9	4.8	5.4	5.8	5.3	4.6	4.9	5.2	5.0	5.7	7.1
37	26	19	18	12		11	15	16	20	27

✓

23.4

2.9
55

23.7

2.6
75

09.1

17.2
77

10.0

16.3
70

11.5

14.8
52

15.4

10.9
37

07.3

19.0
79

07.3

19.0
93

05.9

20.4
100

Sta + π - Elev.

926.27

44+80

✓

45

✓

BM 0.01 926.06 0.20 926.07 (926.05)

+35

13.3

13.6

FK
JS
TL

LT

Feb. 17, 1964
Feb. 18, 1964 RT 56

22.9	20.5	20.3	20.1	20.4	21.2	20.8	20.6	21.0	20.1
3.4	5.8	6.0	6.2	5.9	5.1	5.5	5.7	5.3	6.2
36	26	19	18	12		11	15	16	22

24.2	24.6	24.9		5.3	5.5	8.0	8.7	11.5	15.3
2.1	1.7	1.4		21.0	20.8	18.3	17.6	14.8	11.0
48	65	75		100	81	76	65	48	35

22.9	20.3	19.6	19.3	19.6	20.3	20.0	19.7	20.0	18.8
3.4	6.0	6.7	7.0	6.7	6.0	6.3	6.6	6.3	7.5
38	26	19	18	12		10	15	16	21

24.9	25.0	24.8		4.6	5.6	7.2	10.0	15.1
1.9	1.3	1.5		21.7	20.7	19.1	16.3	11.2
53	70	40		100	83	67	50	33

Top Hyd 81 SW. Cor Belmont Lane

24.2	22.8	19.5	17.9	18.2	18.9	18.2	18.6	17.9	14.5	12.8
1.9	3.3	6.6	8.2	7.9	7.2	7.9	7.5	8.2	11.6	13.3
68	41	23	17	13		14	15	17	31	36

24.4				01.6	04.2	07.4	09.5
1.7				24.5	21.9	18.7	16.6
75				100	80	68	50

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		926.06		
--	--	--------	--	--

45+43				
-------	--	--	--	--

✓				
---	--	--	--	--

+49				
-----	--	--	--	--

+61	2 Ent Lt			
-----	----------	--	--	--

✓				
---	--	--	--	--

+72				
-----	--	--	--	--

+79	M.H 17' Lt			
-----	------------	--	--	--

		9.80		
--	--	------	--	--

			916.26	
--	--	--	--------	--

Feb. 18, 1964

11

2

81 57

22.4	19.8	18.7	17.7	17.9	18.6	17.9	18.4	18.3	17.1
37	6.3	7.4	8.4	8.2	7.5	8.2	7.7	7.8	9.0
41	26	21	18	12		14	15	21	30

23.5

24.0

✓

18.8 9.1 9.5 11.5 12.8

→ 2.6 2.1
59 75

7.3 17.0 16.6 14.6 13.3
75 67 56 50 40

23.8

22.3

18.6

17.7

17.4

18.3

17.6

18.1

17.1

9.4

9.3

2.3	3.8	7.5	8.4	8.7	7.8	8.5	8.0	9.0	16.7	16.8
75	50	43	19	18	✓	14	15	38	57	71

8/dg.

18.78

18.4

18.0

17.2

16.9

17.8

17.1

17.8

16.7

15.4

7.28	7.7	8.1	8.9	9.2	8.3	9.0	8.3	9.4	10.7
Apron	50	33	19	18		14	15	38	42
77									

✓

09.4

09.5

16.7 16.6

71 57

8/dg.

20.4

18.7

17.6

17.0

16.6

17.3

16.8

17.5

16.3

9.6

9.8

5.7	7.4	8.5	9.1	9.5	8.8	9.3	8.6	9.8	16.5	16.3
50	40	28	19	18		14	15	38	57	71

21.0

21.1

✓

→ 5.1 5.0
71 79

Sta	+	π	-	Elev
-----	---	-------	---	------

		926.06		
--	--	--------	--	--

46+00				
-------	--	--	--	--

✓				
---	--	--	--	--

+25				
-----	--	--	--	--

✓				
---	--	--	--	--

+50	±	Ent/RT		
-----	---	--------	--	--

✓				
---	--	--	--	--

T.P.	5.38	921.56	9.88	916.18
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Feb. 18, 1964

LT

£

RT

58

17.8.	16.6.	16.1.	15.5.	16.2.	15.8.	16.3.	15.6.	9.7.
8.3	9.5	10.0	10.6	9.9	10.3	9.8	10.5	16.4
36	26	18	17		14	15	39	55

✓

23.7	24.7							9.5
24	1.4							16.6
60	75							71
								8/19.

20.9	16.1	15.3	14.5	15.2	14.7	15.3	14.9	9.6
5.2	10.0	10.8	11.6	10.9	11.4	10.8	11.2	16.5
43	24	18	17		14	15	41	56

✓

23.1.	23.9.							8.6.
3.0	2.2							9.2.
62	75					55	17.5	16.9
							72	69

21.3.	14.6.	13.9.	13.3.	14.1.	13.6.	13.8.	13.6.	11.8.
48	11.5	12.2	12.8	12.0	12.5	12.3	12.5	14.3
45	24	18	17		14	15	23	45

✓

22.2.	22.4.							7.4
3.9	3.7							9.9
57	75							18.7
								16.2
								75
								58

46 £

Sta + π - Elev.

921.56

46+70

47

✓

+22

✓

BM 0.79 913.12 9.22 912.34 912.33

+31

Feb. 18, 1964

Lt

E

RH

59

22.0'	21.6'	20.7'	14.0'	12.9'	12.4'	13.3'	12.7'	12.9'	12.3'	12.0'	11.7'
40.0	0.9	2.6	8.7	9.2	8.3	8.9	8.7	9.3	9.6	9.9	
77	51	44	25	19	18	14	15	33	61	75	

HO

19.9'	19.5'	12.1'	11.9'	11.3'	12.0'	11.5'	12.1'	11.4'	11.5'
1.7	3.1	9.5	9.7	10.3	9.6	10.1	9.5	10.2	10.1
63	42	24	18	17		14	15	17	30

20.1'									
1.5									
75									

HO 72

11.3'	10.9'	10.2'	10.6'	11.0'	10.7'	11.1'	10.7'	11.3'
10.3	10.7	11.4	11.0	10.6	10.9	10.5	10.9	10.3
38	32	21	12		15	16	19	32

11.9'	12.3'							
9.7	9.3							
61	75							

HO 75 66 47

Top Hyd N.W. Cor. Eldredge & Dale St.

11.1'	10.7'	10.2'	9.9'	10.2'	10.6'	10.6'	10.2'	10.7'	10.1'	10.7'
2.0	2.4	2.9	3.2	2.9	2.5	2.5	2.9	2.4	3.0	2.4
75	62	43	26	11		5	15	16	18	23

11.3'	11.3'	10.8'
1.8	1.8	2.3
75	52	33

Sta + π - Elev.

913.12

47+44

✓

+54 G.V. 44'21"

3.18

909.94

+60

✓

+66 G.V. 45'21"

3.51

909.61

+80

✓

Feb. 15, 1964

LH

£

RT 60

10.8	10.0	09.5a	09.6	10.0	10.1	09.5	09.7	09.2
2.3	3.1	3.53	3.5	3.1	3.0	3.6	3.4	3.9
65	39	MH	13	✓	5	15	16	21
		17						

11.3	11.6	12.0	11.69	10.8		09.0	08.8	09.0
1.8	1.5	1.1	1.43	2.3		4.1	4.3	4.1
86	100	137	159	200		75	53	37
			MH					

10.5	10.2	09.2	08.7	09.3	09.4	08.8	09.1	08.7	08.7
2.6	2.9	3.9	4.4	3.8	3.7	4.3	4.0	4.4	4.4
75	61	34	19		5	15	16	21	43

✓

08.8	08.8
4.3	4.3
75	59

10.6	08.9	07.7	07.9	07.6	08.5	08.1	07.8	08.3	08.0	08.6
2.5	4.2	5.4	5.2	5.5	4.6	5.0	5.3	4.8	5.1	4.5
55	31	21	20	19		11	16	17	18	34

✓

11.6
1.5
75

08.9	08.7
4.2	4.4
75	56

Sta + π - Elev.

913,12

48

✓

+33

✓

+66 E Ent Lt.

Feb. 18, 1964

1+

2

84 61

07.6	06.9	07.1	06.8	07.1	07.7	07.4	07.1	07.5	07.2
55	62	60	63	60	54	57	60	56	59
26	21	20	19	12		10	17	18	19

08.6	10.4	11.9	12.1	09.2	08.7	08.1	07.4
45	27	1.2	1.0	3.9	4.4	5.0	5.7
31	42	66	75	75	57	37	26

08.4	06.4	05.6	05.3	05.7	06.4	06.3	05.9	05.5	05.7	05.4
47	67	75	78	74	67	68	72	76	74	77
32	25	20	19			5	13	18	19	20

10.3	11.2	12.2	12.7	09.0	08.8	08.1	06.9
2.8	1.9	0.9	0.4	4.1	4.3	5.0	6.2
43	52	70	77	75	66	47	28

09.72	07.39	05.37	04.12	03.9	05.1	04.4	03.8	04.1	03.7	04.6
340	573	775	900	92	8.0	8.7	9.3	9.0	9.4	8.5
50	38	30	22	20		13	19	20	21	23

Conc Ent

11.18	12.22	12.68	07.1	05.2	04.9	05.7
194	090	0.44	6.0	79	8.2	24
61	27	29	75	58	39	34

Conc Ent

Apren

Sta + π - Elev.

9/3,12

49

✓

+13

✓

T.P. 3.11 903.93 12.30 900.82

+39

✓

Feb. 18, 1964

Lt.

E

RT

62

037. ⁻	031. ⁻	026. ⁻	030. ⁻	035. ⁻	029. ⁻	022. ⁻	027. ⁻	023. ⁻
9.4	10.0	10.5	10.1	9.6	10.2	10.9	10.4	10.8
27	21	19	13	13	13	19	20	22

065. ⁻	077. ⁻	079. ⁻	084. ⁻	053. ⁻	041. ⁻	040. ⁻	039. ⁻
6.6	5.4	5.2	4.7	7.8	9.0	9.1	9.2
42	54	66	75	75	71	48	29

031. ⁻	023. ⁻	020. ⁻	024. ⁻	029. ⁻	023. ⁻	017. ⁻	022. ⁻	018. ⁻
10.0	10.8	11.1	10.7	10.2	10.8	11.4	10.9	11.3
28	20	19	13	11	19	20	22	

033. ⁻	051. ⁻	064. ⁻	063. ⁻	061. ⁻	039. ⁻	042. ⁻	033. ⁻	033. ⁻	025. ⁻
9.8	8.0	6.7	6.8	7.0	9.2	8.9	9.8	9.8	10.6
33	42	54	70	75	75	62	47	29	29

099.1. ⁻	090.6. ⁻	01.4. ⁻	00.9. ⁻	01.3. ⁻	01.7. ⁻	01.1. ⁻	000.7. ⁻	01.0. ⁻	00.5. ⁻	01.0. ⁻
4.8	3.3	2.5	3.0	2.6	2.2	2.8	3.2	2.9	3.4	2.9
47	28	22	20	13		13	19	20	21	22

099.6. ⁻	099.2. ⁻	000.9. ⁻	01.5. ⁻	01.9. ⁻	01.7. ⁻	01.7. ⁻
5.3	5.7	3.0	2.4	2.0	2.2	2.2
64	75	75	68	57	40	30

Sta + π - Elev.

903.93

49+51

✓

+80

✓

✓

50

TP

0.39

892.67

6.65

897.28

Feb. 18, 1964

BT 63

	8999.	9009.	9014.	9008.	9012.	9006.	9003.	9007.	9001.
4.0	3.0	3.5	3.1	2.7	3.3	3.6	3.2	3.8	
28	22	20	13	12	19	20	22		
899.36.	897.8.	896.6.	895.9.	899.2.	900.4.	901.0.	900.9.	900.7.	
4.57	6.1	7.3	8.0	4.7	3.5	2.9	3.0	3.2	
MH	44	63	75	75	65	54	37	24	
34									
897.9.	898.8.	899.6.	899.3.	899.6.	899.9.	899.4.	899.0.	899.7.	899.4.
6.0	5.1	4.3	4.6	4.3	4.0	4.5	4.9	4.2	4.5
28	27	20	19	13	11	17	18	20	
895.4.	893.5.	892.7.	892.5.	896.5.	898.3.	898.6.	898.9.		
8.5	10.4	11.2	11.4	7.4	5.6	5.3	5.0		
37	61	75	68	65	49	35	26		
896.1.	896.7.	897.9.	898.7.	898.5.	898.9.	898.5.	896.9.	899.3.	
7.8	7.2	6.0	5.2	5.4	5.0	5.4	5.8	5.2	
30	26	24	20	19	11	18	19	23	
93.6	91.5	90.4	90.2	90.0	90.9	93.5	94.5	95.8	
10.3	12.4	13.5	13.7	13.9	13.0	10.4	9.4	8.1	
36	48	65	75	75	69	62	46	36	

Sta + π - Elev.

892.67

50 + 30

✓

✓

+65

✓

✓

TP 1.01 893.96 3.72 893.95

BM

894.21

Feb. 18, 1964

RT 64

✓

✓

✓

89.9. 95.5. 97.0. 97.3. 97.0. 89.7.5. 97.0. 96.6. 97.0. 91.5.

78 2.2 0.7 0.4 0.7 0.2 0.7 1.1 0.7 6.2
38 28 24 19 18 14 18 22 30

87.0. 85.6. 85.0. 84.8. 89.0. 89.0. 86.9. 86.9.

10.7 12.1 12.7 12.9 8.7 8.7 10.8 10.8
49 66 75 65 54 43 42 40

84.8. 86.1.

12.9 11.6
69 75

89.2. 94.2. 95.3. 95.0. 95.2. 95.7. 95.1. 94.7. 95.3. 95.0.

8.5 3.5 2.4 2.7 2.5 2.0 2.6 3.0 2.4 2.7
36 28 20 19 14 12 18 19 21

84.7. 83.3. 81.8. 81.4. 83.9. 85.3. 86.0. 90.0.

13.0 14.4 15.9 16.3 13.8 12.4 11.7 7.7
44 50 64 75 45 40 35 27

85.1. 84.2. 81.9. 81.5.

12.6 13.5 15.8 16.2
49 57 64 75

51 £

Top Hyd N.E. Cor Dale St. + Co Rd "B"

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		893.96		
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51+00				
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✓				
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+31				
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✓				
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+62				
-----	--	--	--	--

✓				
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Feb. 18, 1964

11

B1 65

90.6 92.5 93.4 93.1 93.4 94.0 93.5 92.1 93.8 93.2

34 1.5 0.6 0.9 0.6 0.0 0.5 0.9 0.2 0.8
32 25 20 19 14 12 19 20 22

87.5 81.6 78.9 78.1 81.0 81.9 84.4 85.8

6.5 12.4 15.1 15.9 13.0 12.1 9.6 8.2
37 47 61 75 75 61 47 34

86.36

90.3 91.6 92.2 91.9 93.0 92.3 92.8 92.6 83.8

7.60 3.7 2.4 1.8 2.1 1.0 1.7 1.2 1.4 10.2
MH 28 22 20 19 19 20 22 34
33

89.6 88.2 84.7 84.4 83.8 83.7 85.9 86.5 83.8

4.4 5.8 9.3 9.6 10.2 10.3 8.1 7.5 10.2
38 48 65 75 75 71 55 41 37

85.9 88.6 91.2 91.6 91.4 92.2 91.7 92.3 92.2 84.4 84.4

8.1 5.4 2.8 2.4 2.6 1.8 2.3 1.7 1.8 9.6 9.6
71 47 23 20 19 20 21 24 37 40

85.4 90.0 90.4 88.8

8.6 4.0 3.6 5.2
75 75 68 44

Sta + π - Elev.

893.96

51+80

✓

52

✓

+21 S. Gutter B

+37 $\neq$ B

Feb. 18, 1964

11

2

Rt

66

86.9	89.2	90.9	91.2	90.9	91.8	91.4	91.9	91.5	91.2
7.1	4.8	3.1	2.8	3.1	2.2	2.6	2.1	2.5	2.8
64	39	25	21	19		20	21	23	34

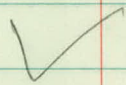


85.9

8.1
7.5

92.3	92.1	90.8	86.7	86.7
1.7	1.9	3.2	7.3	7.3
75	72	50	40	38

89.7	90.2	90.5	90.1	90.8	91.3	91.3	91.2	91.6	91.7
4.3	3.8	3.5	3.9	3.2	2.7	2.7	2.8	2.4	2.3
30	23	21	20	11		12	24	25	27



87.8	86.3	85.6
6.2	7.7	8.4
55	69	75

93.4	92.5	91.5	90.9	91.2
0.6	1.5	2.5	3.1	2.8
75	66	45	34	28

87.7	88.2	88.6	90.1	90.4	91.0	91.2	91.4	91.5	92.0	92.3
6.3	5.8	5.4	3.9	3.6	3.0	2.8	2.6	2.5	2.0	1.7
75	60	41	21	14		12	24	38	61	75

87.1	87.8	88.7	89.5	90.3	90.73	91.2	91.6	92.2	92.57
6.9	6.2	5.3	4.5	3.7	3.23	2.8	2.4	1.8	1.39
100	78	54	23	15	MH	17	31	58	MH



85.5
84.2
8.5
150
98
200

93.2
0.8
99

Sta + π - Elev.

893.96

52+55 N. Gutter line

+63 Gate V. 38' Lt 2.97

+75

✓

53

BM 1.64 895.86 +.27 894.23 (894.22)

+20

✓

FX
JSS
TL

Feb. 18, 1964
Feb. 25, 1964

87.8.	87.9.	88.7.	89.6.	90.1.	90.5.	90.9.	91.3.	91.9.	92.8.
6.2	6.1	5.3	4.4	3.9	3.5	3.1	2.7	2.1	1.2
75	71	49	25	12	12	30	60	89	

87.4.	87.8.	89.2.	89.4.	89.9.	90.4.	90.5.	90.9.	91.6.	91.1.	91.4.
6.6	6.2	4.8	4.6	4.1	3.6	3.5	3.1	2.4	2.9	2.6
75	55	27	20	13	36	11	30	48	48.5	64



92.49
1.47
78
Carb
91.9
2.1
77

87.8.	87.6.	87.7.	89.2.	89.8.	90.5.	90.6.	90.6.	91.3.	91.7.
6.2	6.4	6.3	4.8	4.2	3.5	3.4	3.4	2.7	2.3
75	68	51	23	17	20	41	61	75	

Top Hyd N. E. Cor Dale St. & Co. Rd B

88.6.	89.5.	89.9.	90.0.	90.5.	90.6.	90.7.	91.1.	91.3.
7.3	6.4	6.0	5.9	5.4	5.3	5.2	4.8	4.6
26	21	17	13	13	24	29	37	

87.9.	87.6.	87.8.	87.5.	91.58.	91.12.	91.00.	90.91.
8.0	8.3	8.1	8.4	4.28	4.74	4.86	4.95
38	57	70	75	75	55	43	37

Conc

Sta + π - Elev.

895.86

53+50

✓

+75

✓

54

✓

Feb. 25, 1964

11.

2

RI 68

87.4	88.2	89.6	90.0	90.5	90.6	90.7	91.0	91.04
85	77	6.3	5.9	5.4	5.3	5.2	4.9	4.82
47	28	21	17		12	21	26	36

✓

87.1	87.0				91.56	91.10	90.87	90.8
88	89				4.30	4.76	4.99	5.1
73	75				75	53	42	36

Conc

87.1	88.3	89.5	90.1	90.5	90.5	90.4	90.5	90.9
8.8	7.6	6.4	5.8	5.4	5.4	5.5	5.4	5.0
39	25	20	14		12	23	41	58

✓

86.7	86.5							91.5
9.2	9.4							4.4
57	75							75

86.4	86.6	86.8	89.6	89.9	90.53	90.5	90.4	91.2	92.6
9.5	9.3	9.1	6.3	6.0	5.33	5.4	5.5	4.7	3.3
75	53	34	20	15		12	27	37	54

✓

93.7	93.4
2.2	2.5
75	70

Sta + π - Elev

895.86

54+50

✓

BM 5.61 896.76 4.71 891.15

+88

✓

55

Feb. 25, 1964

£

RT 69

864.	859.	901.	904.	907.	907.	907.	900.	913.
95	100	58	55	52	52	52	59	46
51	33	19	13	11	21	25	32	

861.

9.8

75

Top H₂O Lt Ste

94.33.

939.

925.

1.53 2.0 34

75 74 50

860.

859.

900.

904.

908.

909.

908.

895.

91.30.

923.

10.8	10.9	6.8	6.4	6.0	5.9	6.0	7.3	5.4	6.5
49	32	20	14	11	19	24	31	51	

851.

84.8.

937.

11.7

12.0

31

70

75

75

854.

858.

901.

905.

90.86.

909.

908.

905.

909.

11.4	11.0	6.7	6.3	5.9	5.9	6.0	6.3	5.9
54	32	19	13	11	18	19	27	

846.

84.6.

923.

923.

12.2

12.2

3.5 4.5

66

75

75 49

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		896.76		
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+26				
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✓				
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+35				
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✓				
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+56				
-----	--	--	--	--

Feb. 25, 1964

11

✓

RT 70

85.4.	86.5.	90.6.	90.9.	91.1.	91.0.	90.8.	90.5.	90.5.
11.4	10.3	6.2	6.0	5.7	5.8	6.0	6.3	6.3
37	29	20	15		10	18	20	25

✓

86.1.	86.3.
11.7	10.5
58	75

93.2.	91.8.
3.6	5.0
78	45

83.90.	86.8.	90.7.	91.0.	91.1.	91.1.	90.9.	86.44.	86.4.
12.86	10.0	6.1	5.8	5.7	5.7	5.9	10.32	10.4
33	27	20	14		10	19	27	29
FL24CM							FL24CM	

✓

85.2.	87.4.
11.6	9.4
51	75

93.1.	92.5.	91.4.
3.7	4.3	5.4
75	59	35

86.5.	87.0.	91.0.	91.2.	91.3.	91.3.	91.1.	87.5.	87.5.	91.8.
10.3	9.8	5.8	5.6	5.5	5.5	5.7	9.3	9.3	5.0
48	28	20	14		10	18	25	27	32

✓

87.6.	87.5.
9.2	9.3
71	75

92.0.	92.5.	92.1.
3.8	4.3	4.7
75	58	43

Sta	+	K	-	Elev.
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		896.76		
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56				
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✓				
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+50				
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✓				
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TP	9.67	903.48	2.95	893.81
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57				
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✓				
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Feb. 25, 1964

88.4- 88.4- 91.3- 91.6- 91.9- 91.7- 91.3- 89.0- 89.0- 91.2-
 8.4 8.4 5.5 5.2 9 5.1 5.5 7.8 7.8 5.6
 48 28 19 14 11 17 21 22 25

87.8- 87.6- 96.5- 93.0-
 9.0 9.2 8.3 3.8
 71 75 73 45

88.9- 89.6- 92.1- 92.4- 92.7- 92.6- 92.6- 91.1- 91.1- 92.9-
 7.9 7.2 4.7 4.4 4.2 4.2 5.7 5.7 4.4
 46 30 19 13 11 4 19 21 29

87.9- 87.6- 96.8- 95.8- 93.9-
 8.9 9.2 9.0 1.0 2.9
 65 75 68 60 42

89.1- 89.8- 92.8- 93.3- 93.8- 93.6- 92.0- 92.0- 93.5-
 14.4 12.7 10.7 10.2 9.7 9.9 11.5 11.5 10.0
 51 30 19 13 15 20 22 23

88.3- 88.4- 98.8- 98.5- 97.1- 95.5-
 15.2 15.1 4.7 5.0 6.4 8.0
 69 75 75 63 59 38

Sta	+	X	-	Elev.
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Sta	+	X	-	Elev.
		903.48		

Sta	+	X	-	Elev.
57+19				

Sta	+	X	-	Elev.
✓				

Sta	+	X	-	Elev.
+36				

Sta	+	X	-	Elev.
✓				

Sta	+	X	-	Elev.
+56				

Feb. 25, 1964

11

81 72

89.1-	90.0-	93.1-	93.7-	94.3-	93.9-	94.3-	96.0-	97.2-	97.9-
14.4	13.5	10.4	9.8	9.2	9.6	9.2	7.5	6.3	5.6
54	32	19	13	15	21	40	61	75	

88.4-

15.1
75

89.5-	90.7-	93.7-	94.2-	94.7-	94.4-	94.7-	96.5-	97.2-	97.9-
14.0	12.8	9.8	9.3	8.8	9.1	8.8	7.0	6.3	5.6
52	32	19	13	15	21	41	52	66	

88.9-

14.6
75

88.1-

5.4
75

89.5-	89.9-	91.5-	94.3-	94.8-	95.0-	94.8-	93.7-	93.7-	95.5-
14.0	13.6	12.0	9.2	8.7	8.4	8.5	8.7	9.8	9.8
65	48	28	18	12	11	15	20	22	27

89.3-

14.2
75

99.2-

4.3
75

99.0-

4.5
69

97.7-

5.8
41

Sta	+	π	-	Elev
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Sta	+	π	-	Elev
		903.48		

Sta	+	π	-	Elev
58				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
+40				

Sta	+	π	-	Elev
✓				

Sta	+	π	-	Elev
+58				

Sta	+	π	-	Elev
✓				

Feb. 25, 1964

LT

+

RT 73

92.0.	93.1.	95.8.	96.1.	96.4.	94.0.	94.7.	94.7.	96.9.	98.5.
115	104	77	74	71	75	88	88	71	5.0
46	29	18	12	14	20	22	27	41	

91.2.	90.9.
12.3	12.6
67	75

90.4.	89.9.
31	36
73	60

93.1.	94.4.	97.4.	97.4.	97.6.	97.4.	95.6.	95.6.	97.1.	98.9.
104	9.1	6.1	6.1	5.9	6.1	7.9	7.9	6.4	4.6
46	29	19	13	15	20	22	26	37	

92.7.	92.3.
10.8	11.2
63	75

99.9.	99.6.	99.6.
36	39	39
75	68	47

93.9.	95.1.	97.7.	97.9.	98.2.	98.0.	96.0.	96.0.	97.8.
9.6	8.4	5.8	5.6	5.3	5.5	7.5	7.5	5.7
42	27	19	13	14	21	24	27	

93.4.	92.9.
10.1	10.6
60	75

97.8.	97.3.	97.9.
5.7	6.2	6.1
75	67	45

Sta + π - Elev.

903.48

59

✓

+18

✓

+27 MH 50' Lt 6.49 896.99

BM 9.14 909.64 2.98 900.50

+56

✓

Feb. 25, 1964

14

15

PH

24

91.2	97.3	99.0	99.3	99.5	99.3	99.1	97.6	97.6	98.9
73	62	45	42	40	42	44	59	59	46
40	27	18	13		10	16	19	22	24

94.6	93.6				99.0	98.2	98.0	99.1
89	99				45	53	55	44
61	75				75	64	45	35

96.8	97.8	99.5	900.1	90.2	900.0	899.9	98.0	98.0
67	57	40	34	33	35	36	55	55
42	31	22	13		11	16	18	20

95.2	94.4
83	91
59	75

03.7	02.7	901.3	899.8
102	08	22	37
75	54	37	24

Top Hyd Lt Sta ^{27.5} 59+14.5

97.7	98.9	900.8	01.5	01.6	01.4	01.4	98.7	98.7
11.9	10.7	8.8	8.1	8.0	8.2	8.2	10.9	10.9
48	37	24	13		10	14	19	22

96.1	895.7
13.5	13.9
65	75

05.5	05.34	04.5	03.1	01.5
41	430	51	65	81
H0	70	59	42	25
76				

Sta + π - Elev

909.64

59+98

✓

60

✓

+ 23

✓

Feb. 25, 1964

11

4

25

900.7	01.4	02.5	03.3	03.4	03.3	04.9	03.3	03.4
8.9	8.2	7.1	6.3	6.2	6.3	9.15	6.3	6.2
35	28	21	13		10	21	28	45

0.9	09.8	08.3
8.7	9.8	11.3
39	52	75

04.8	04.1
4.8	5.5
75	65

01.5	01.1	01.5	02.5	03.4	03.5	03.4	03.2	900.5	900.5	02.1
8.1	8.5	8.1	7.1	6.2	6.1	6.2	6.4	9.1	9.1	7.5
37	34	30	22	14		10	14	19	21	21

09.8	08.7
9.8	10.9
58	75

05.5	05.2	04.6	04.1	03.0
4.1	4.4	5.0	5.5	6.6
75	61	44	27	25

03.4	02.3	02.3	03.8	04.4	04.6	04.3	04.2	01.9	01.9	04.3
6.2	7.3	7.3	5.8	5.2	5.0	5.3	5.4	8.2	8.2	5.3
27	26	25	22	14		9	15	19	22	25

02.8	01.2	900.0
6.8	8.4	9.6
38	60	75

06.5	05.8	05.0	04.6
3.1	3.8	4.6	5.0
75	65	48	31

Sta	+	π	-	Elev.
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		909.64		
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60+59				
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✓				
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+70				
-----	--	--	--	--

✓				
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61				
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T.P.	12.62	921.25	1.01	908.63	61 ±
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BM	406	925.00	0.31	920.94	
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1710
510
56

Feb. 25, 1964

Lt.

#

Rt. 76

03.6	03.6	04.2	06.3	06.4	06.0	05.7	03.0	02.9
6.0	6.0	3.4	3.3	3.2	3.6	3.9	6.6	6.7
23	20	16	12		11	14	19	23
04.9	04.5	03.8	03.2		09.1	07.3	06.6	07.0
4.7	5.1	5.8	6.4		0.5	2.3	3.0	2.6
26	41	59	75		75	51	30	26

05.9	03.8	03.8	06.8	06.9	07.0	06.7	06.38	06.93	07.9
3.7	5.8	5.8	2.8	2.7	2.6	2.9	3.26	2.71	1.7
25	23	20	16	12			9	6	39
							17		

04.4	03.5						09.8	08.9
5.2	6.1						10.2	0.7
46	75						67	56

06.2	06.2	08.3	08.4	08.6	08.4	08.43	08.89
3.4	3.4	1.3	1.2	1.00	1.2	1.21	0.75
23	21	16	12		10	18	19
						G	C

07.1	07.0	06.8	06.8				
2.5	2.6	2.8	2.8				
26	42	60	75				

Top Hyd SECov TH #36 + Date ST

Sta + π - Elev.

5.6

925.00

61+00

+27

✓

+41

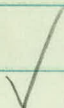
✓

+68

FK
JS
TL

Lt.

Feb. 26, 1964
Cold Clear Windy 5°
Rt. 77



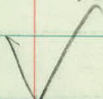
10.36	10.40	11.5	11.7
14.64	14.60	13.5	13.3
38	38	38.5	75
Apron C			

08.0	08.0	09.7	09.8	10.0	09.7	09.6	10.19	09.96
170	170	15.3	15.2	15.0	15.3	15.4	14.81	15.04
24	22	18	13		11	16	C	G
							21	



08.7	08.6	08.4	10.56	10.62	10.5
16.3	16.4	16.6	14.44	14.38	14.5
29	43	57	43	38	35
Ho			Apron Apron		

09.7	09.1	09.1	10.3	10.7	10.2	10.65	14.3	18.4
15.3	15.9	15.9	14.7	14.3	14.8	14.35	10.7	6.6
29	24	21	17	16.5	17	27	38	



09.7	09.3	09.5	21.8	21.6	21.5	19.8
15.3	15.7	15.5	3.2	3.4	3.5	5.2
37	57	75	75	72	68	42

11.7	10.9	10.7	11.9	12.1	11.6	12.12	16.6	20.0
13.3	14.1	14.3	13.1	12.9	13.4	12.88	8.4	5.0
50	29	23	17	16.5	17	29	38	



12.4	24.3	24.27	22.4
13.6	0.7	0.73	2.6
75	74	71	51

Sta + π - Elev

925.00

62

✓

+18. $\pm$ Ent Lt

✓

+39

+48

Feb 26, 1964

£

11

81 78

133.

133.

138.

139.

133.

1380.

210.

233.

11.7

11.7

11.2

11.1

11.7

11.20

4.0

1.7

24

22

18

16.5

17

38

52

14.0.

14.7.

15.5.

16.7.

✓

250

24.95.

11.0

10.3

9.5

8.3

0.0

0.05

29

34

53

75

40

68

76

16.9

16.1

14.9.

14.8.

14.9.

14.4.

14.75

22.4.

24.1.

8.1

8.9

10.1

10.2

10.1

10.6

10.25

26

0.9

62

43

26

17

16.5

17

42

61

✓

17.9.

7.6

75

24.8.

0.2

75

20.9.

18.6.

14.48

15.7

15.9.

15.4.

15.80.

22.2.

24.3.

24.5.

4.1

6.4

10.52

9.3

9.1

9.6

9.20

2.8

0.7

0.5

75

50

CB

18

✓ 16.5

17

40

65

75

31

21.4.

20.6.

19.2

14.8

16.0

16.3.

15.8.

16.22.

22.3.

24.0.

24.3

3.6

4.4

5.8

10.2

9.0

8.7

9.2

8.78

2.7

1.0

0.7

75

64

51

31

18

16.5

17

40

63

75

Sta + π - Elev.

925.00

62+58

✓

BM 7.07 928.01 4.06 920.94 920.94

+65 S Gutter Rt

✓

+85 N. Gutter Rt

Feb. 26, 1964

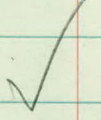
Lt.

£

Rt

79

205.	18.0.	15.3.	16.0.	16.9.	16.7.	16.32.	16.82.	17.5.	19.9.
45	70	97	90	86	8.3	8.68	8.18	75	56
57	45	29	25	19		CB	17.5	24	35
						17			

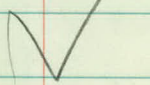


→ 21.5
3.5 3.4
70 75

22.4 20.9
26 4.1
75 55

Top Hyd SE. Cor TH #36 + Dale St.

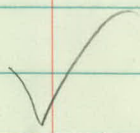
18.3.	16.1.	16.5.	16.7.	17.1.	16.6.	16.6.	18.2.	19.8.
9.7	11.9	11.5	11.3	10.9	11.4	11.4	9.8	8.2
46	28	19	17		17	20	32	47



19.9.
21.1.
21.7.
8.1 6.9 6.3
51 64 75

23.6.
22.0.
21.9.
4.4 6.0 6.6
100 75 69

16.3.	17.2.	17.4.	17.6.	17.8.	17.4.	18.7.	20.6.	22.1.
11.7	10.8	10.6	10.4	10.2	10.6	9.3	7.4	5.9
40	31	24	18		17	33	53	69



16.5.
16.6.
11.5 11.4
70 75

24.0.
22.6.
4.0 5.4
100 75

Sta + π - Elev.

928.01

63

✓

+105.5 Top Carb Rt

✓

+15.5 Gutter Linelt.

+28.5 $\neq$ Approach

Feb. 26, 1964

RT 80

18.3	18.33	18.1	18.3	18.5	18.4	17.65	18.07
9.7	9.68	9.9	9.7	9.5	9.6	10.36	9.94
34	29	24	14		11	G	C
Conc Gutter						20	22

17.4	16.50
10.6	11.51
53	77
FL 12 CM	

19.7	19.5	18.9
8.3	8.5	9.1
75	64	47

18.7	18.7	18.50	18.7	18.8	18.6	18.3	17.8	18.13
9.3	9.3	9.51	9.3	9.2	9.4	9.7	10.2	9.88
39	35	33	13		11	17	27	37
Cmc G								Carb

18.3	18.5
9.7	9.5
56	75

20.28	19.14	18.10	18.61
7.73	8.87	9.91	9.40
100	75	GB	C
62.5			

19.01	18.77	18.76	18.9	19.0	19.2	19.0	18.8	18.9	19.3	20.3
9.00	9.24	9.25	9.1	9.0	8.8	9.0	9.2	9.1	8.7	7.7
100	78	56	27	13		12	25	56	75	100
CB		Gutter								

19.4	19.3	19.3	19.5	19.6	19.7	19.6	19.5	19.3	19.6	20.6
8.6	8.7	8.7	8.5	8.4	8.3	8.4	8.5	8.7	8.4	7.4
100	75	50	25	14		13	25	56	75	100

20.2	21.7
7.8	6.3
150	200

25.5	23.0
2.5	5.0
200	150

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		928.01		
--	--	--------	--	--

63+40.5		Curb Line		
---------	--	-----------	--	--

✓				
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+64				
-----	--	--	--	--

✓				
---	--	--	--	--

+85				
-----	--	--	--	--

Feb. 26, 1964

LT

RT 81

19.91	19.42	19.8	20.0	20.2	20.1	19.8	19.4	19.98
8.10	8.59	8.2	8.0	7.8	7.9	8.2	8.6	8.03
Curb	60	26	14		13	26	57	Curb
65	G							67

19.91	19.30	19.90	20.95	20.16	20.83
8.10	8.71	8.11	7.06	7.85	7.18
76.5	CB	100	100	CB	96
	76.5		Curb	96	Curb

21.1	21.19	20.77	20.9	21.1	20.9	20.46	20.90	20.2	18.3
6.9	6.82	7.24	7.1	6.9	7.1	7.55	7.11	7.8	9.7
32	29.5	29	13		14	28	29	35	57
						G	C		

19.9	16.23	16.4	16.6	17.74	18.3	18.1
8.1	11.78	11.6	11.4	10.27	9.7	9.9
42	55	69	75	93	89	74
	CB			FL 12 CM		

21.8	21.91	21.39	21.8	21.9	21.8	21.5	21.88	21.5	19.9
6.2	6.10	6.62	6.2	6.1	6.2	6.5	6.13	6.5	8.1
29	26	CB	12		13	25	25.5	31	40
	C	26							

21.6	20.1	17.8	17.3	17.8	17.31
6.4	7.9	10.2	10.7	10.2	10.70
34	44	59	75	75	55
					CB

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		928.01		
--	--	--------	--	--

64				
----	--	--	--	--

+50				
-----	--	--	--	--

65				
----	--	--	--	--

		1.9		
--	--	-----	--	--

			26.11	
--	--	--	-------	--

+50				
-----	--	--	--	--

		0.2		
--	--	-----	--	--

			27.81	
--	--	--	-------	--

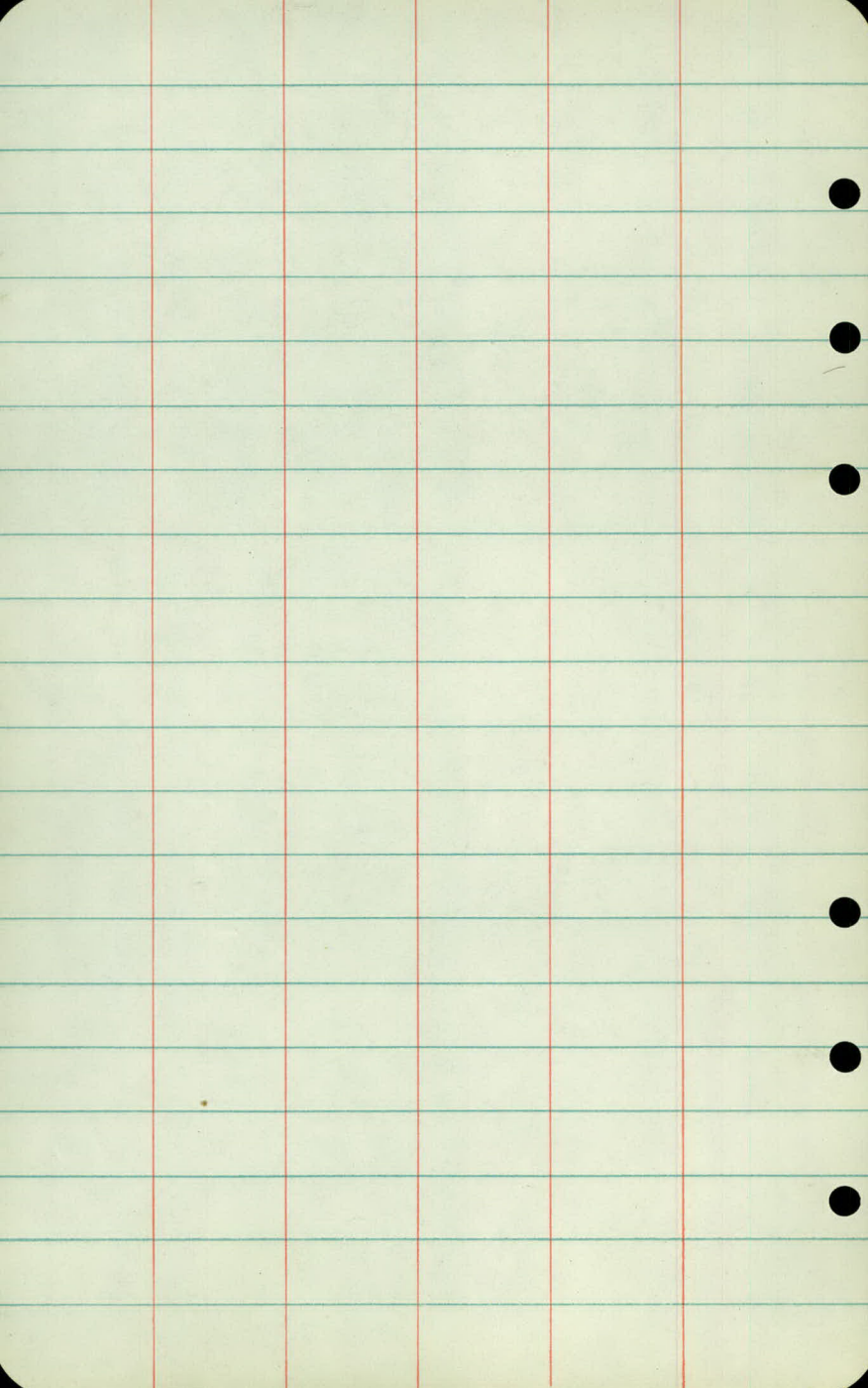
BM				
----	--	--	--	--

		7.07	920.94	
--	--	------	--------	--

Feb 26, 1964

Lt.												RT		82
20.7	22.0	22.45	22.0	22.3	22.5	22.3	22.0	22.47	22.2	19.3				
73	6.0	5.56	6.0	5.7	5.5	5.7	6.0	5.54	5.8	8.7				
50	35	26	25.5	12		13	25	25.5	32	50				
		C						C						
26.5	24.9	24.57	23.7	24.1	24.3	24.2	23.7	24.58	24.8	28.0				
1.5	3.1	3.44	4.3	3.9	3.7	3.8	4.3	3.43	3.2	0.0				
37.5	35	25.5	25	14		11	25	25.5	35	40				

Top Hyd. S.E. Cor TH #36 + Dalest



Dale St

Storm Sewer Elev.

Sta	+	π	-	Elev.
BM	028	921.22		920.94

62+58	In r C.B.Rt	11.15	10.07
-------	-------------	-------	-------

62+40	Top 18" SCP-93 low 1.75	11.05	10.17
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TP	2.03	910.67	12.58	908.64
----	------	--------	-------	--------

60+61	End Apron	7.53	03.14
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60+65	A' North at Culvert	7.36	03.31
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BM		10.14	900.53
----	--	-------	--------

FK
JS
WM

March 30, 1964

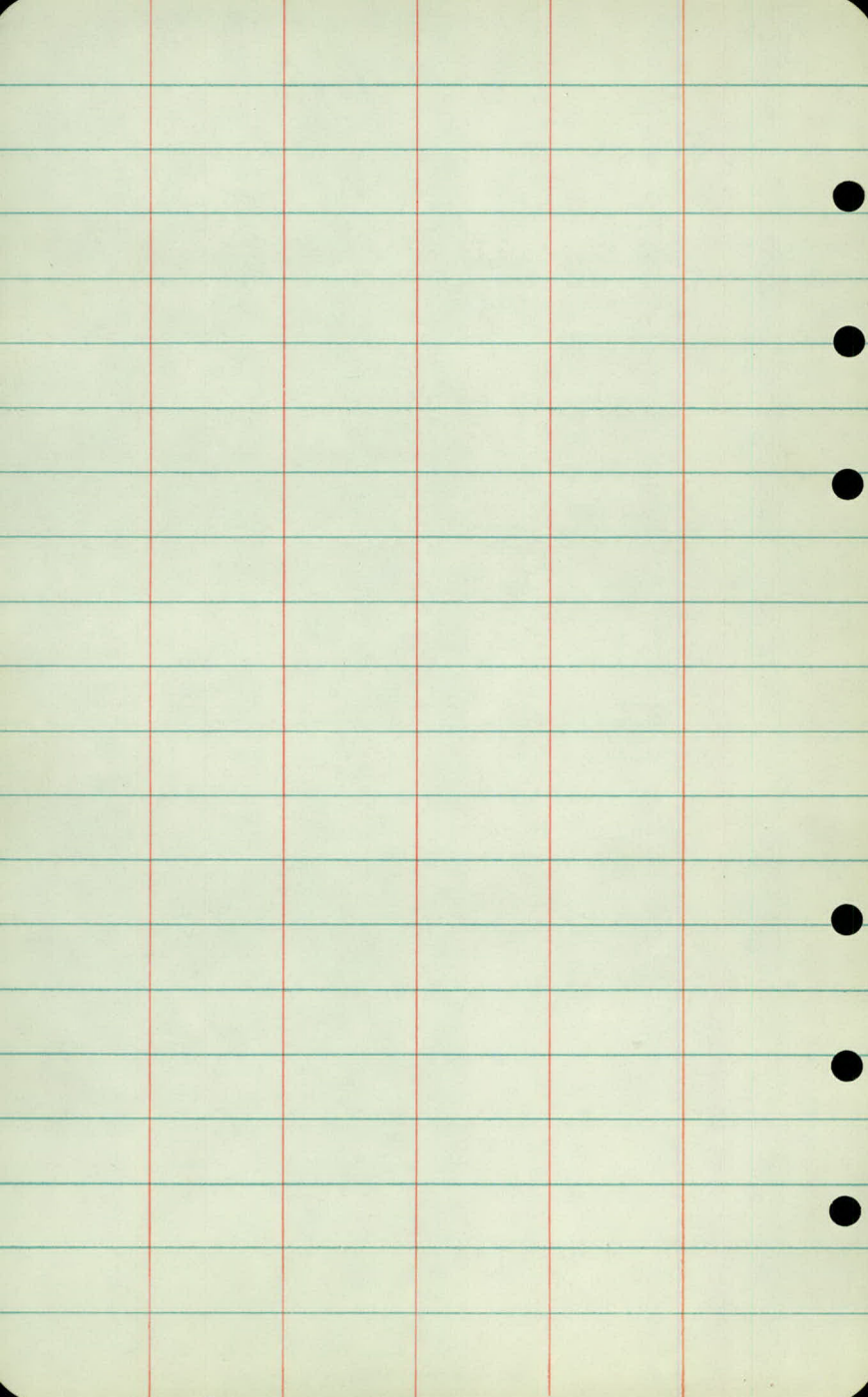
2

Top Hyd

13.8
4.5

9.3

61+00 ~~4~~



March 24, 1964

1

Dale St.

50+80

90°

1+25

22°30'1/2

Rec. 3-24-64

Sta	+	x	-	Elev
BM	0.05	894.26		894.21
TP	1.67	883.62	12.31	881.95
Top W.E. Culvert			7.51	876.11
TP	12.15	894.17	1.60	882.02
0 +50				
TP	0.29	882.58	11.88	882.29
+75				
/				
+25	P.I.			
+50				
+77	End Pipe	±	7.59	874.99

FK
JS
WM

March 24, 1964

2

Top Hyd NE Cor B & Dalest

82.0	84.8	84.3	81.8	84.2	84.0	84.6	83.8
12.2	9.4	9.9	12.4	10.0	10.2	9.6	10.4
40	30	15	10	5		20	40
82.0	81.0	80.6	80.1	81.4	81.2	81.9	
0.6	1.6	2.0	2.5	1.2	1.4	0.7	
30	25	13		17	24	27	
81.2	80.1	79.7	79.6	79.1	79.3	78.3	
1.4	2.5	2.9	3.0	3.5	3.3	4.3	3.5
38	26	13		19	29	35	43
	79.7	78.8	78.8	78.8	78.1	76.8	78.0
	2.9	3.8	3.8	3.8	4.5	5.8	4.6
	32	13		14	25	39	50
81.6	79.0	77.4	77.6	77.5	78.7	76.5	78.8
1.0	3.6	5.2	5.0	5.1	3.9	6.1	3.8
44	27	11		14	23	27	37

Top Conc Pipe

Sta	+	-	Elev.
-----	---	---	-------

		882.58	
--	--	--------	--

2			
---	--	--	--

+50			
-----	--	--	--

3			
---	--	--	--

+50			
-----	--	--	--

4			
---	--	--	--

+20	± Ditch on ±	15.4	867.18
-----	--------------	------	--------

+70	± Ditch ^{on} ±	16.1	866.48
-----	-------------------------	------	--------

TP	13.10	895.34	0.34 882.24
----	-------	--------	-------------

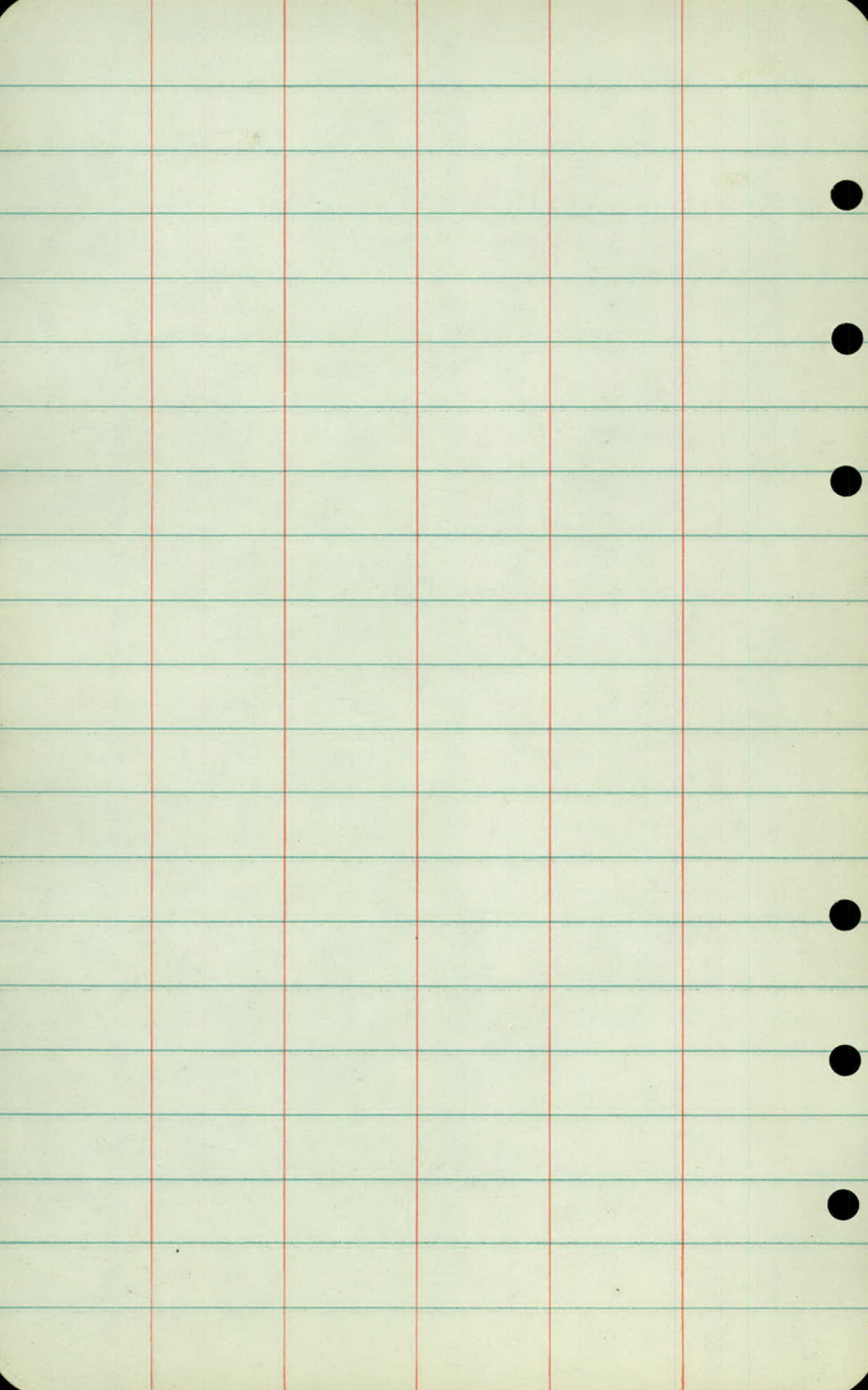
BM		1.13	894.21 (894.21)
----	--	------	-----------------

876.11

March 29, 1964

	LT					RT	3
77.1	76.4	75.5	75.7	75.8	75.7	76.4	78.0
3.5	6.2	7.1	6.9	6.8	6.9	6.2	4.6
35	20	10		13	27	39	50
76.8	75.6	74.2	74.1	74.3	74.9	74.7	76.2
5.8	7.0	8.4	8.5	8.3	7.7	7.9	6.4
31	26	14		10	26	40	50
	75.8	72.7	73.1	72.9	73.0	73.9	
	6.8	9.9	9.5	9.7	9.6	8.7	
	32	18		20	38	50	
73.9	72.6	72.0	71.5	71.4	71.9	72.1	
8.7	10.0	10.6	11.1	11.2	10.7	10.5	
50	33	24	6	5	25	50	
70.7	70.6	70.5	69.7	68.3	69.3	71.4	71.4
11.9	12.0	12.1	12.9	14.3	13.3	11.2	11.2
50	35	15		10	13	17	32

Top Hyd NE Cor. Dale & "B"



Ramsay County

Dale St.

2+50 - 4

0-4	FS		lt bwn
4-6	SL	sap	" "
6-8	SL	pl	" "

6+55 - 4

0-4	LS		lt bwn
4-12	C	firm	black
12-16	SL	sap	Gray

H2O Table 8.0'

8+60 - 4

0-4	SL	sap	lt bwn
4-8	LFS		" "
8-16	SLT	pl	" "
16-20	SIC		" "

10+25 - 4

0-4	SL	sap	dk gray bwn
4-7	SL	pl	lt "
7-9	VFSL	silly	" "
9-11	SIL	pl	" "
11-12	C	very stiff	Red

11+60 - 4

sample	0-1	SL	PI	dk bwn
1 D	1-14	FS		lt bwn
	14-28	SL	sap1	" "

13+35 - 4

0-4	VFSL	Silty	PI	lt bwn
4-8	VFSL	PI		dk bwn
8-11	SICL			dk bwn
11-12	S			lt "

Dale St.

Sta	+	Δ	-	Elev.
BM	0.10	907.35		907.25
T.P.	0.93	894.81	13.47	893.88
B.M.	0.05	885.63	9.23	885.58
			7.42	878.21 878.16

Rt 70'

24+14.8 ~ 9.00 876.63

24+23.5. 9.23 876.46

24+33.0 6.72 878.91

24+26.6 7.72 877.91

Lt 59'

24+13.5 882.45

24+19 881.90

24+23.5 884.39

24+33 886.36

April 3, 1964

2

Roseville B.M. SE Cor Dale & Roselawn

Nail in NE Side 18" Ash Tree 36

E. Rino M. H.

20

Top 36" Water Main

24 Clay
Drain

Top 20" Water Main

Top 24" Vit. Drain

Top 15" Vit. Drain

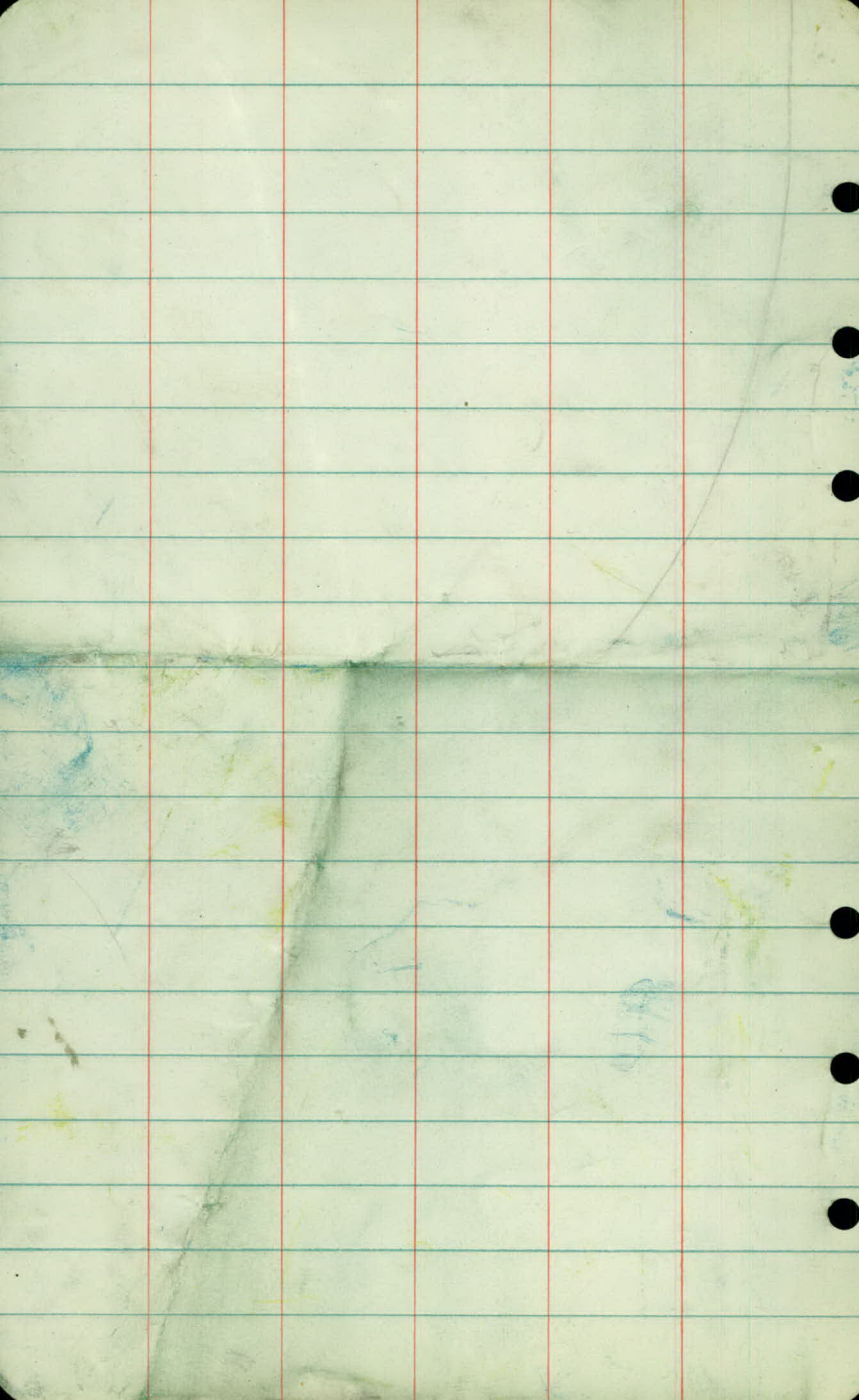
Top 36" Water Main

Water Dept
April 7, 1964

Top 20" Main

Top 15" Drain

Top 24" Drain



1
Dale St

Co Rd "B" X-Sections

5 pages

Sta	+	π	-	Elev.
-----	---	-------	---	-------

BM	0.88	895.09		
----	------	--------	--	--

				894.21
--	--	--	--	--------

0+00				
------	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

/				
---	--	--	--	--

FK
JS
WM

March 25, 1964

Cloudy Cold 10° Windy 2

Top Hyd NE Cor

Date 4 "B"

RA

83.1	83.7	84.2	83.9	84.2	83.7	83.4	80.6	78.8
120	114	109	112	109	114	11.7	14.5	16.3
23	18	16	15		15	20	29	34

80.8	80.4						78.9
14.3	14.7						16.2
33	50						50

84.8	85.4	85.4	85.1	85.3	84.8	84.9	84.6	84.4
10.3	9.7	9.7	10.0	9.8	10.3	10.2	10.5	10.7
19	18	17	16		17	18	19	22

84.8	84.0	84.7				81.0	80.8
10.3	11.1	10.4				14.1	14.3
23	29	50				50	29

86.6	86.5	86.9	86.7	87.0	86.5	86.8	86.2	85.8
8.5	8.6	8.2	8.4	8.1	8.6	8.3	8.9	9.3
34	19	18	17		16	17	19	25

86.2					83.3	83.6	82.5	83.6
8.9					11.8	11.5	12.6	11.5
50					60	50	47	36

Sta + π - Elev.

895.09

1+58

✓

2+00 = $\pm$ Dale St

T.P. 7.37 899.89 2.57 892.52

+42

✓

+53 $\pm$ Eht

March 25, 1964

14

B1

3

87.9	88.4	88.8	88.9	88.9	88.6	88.7	89.2	88.9
7.2	6.7	6.3	6.2	6.1	6.5	6.4	5.9	6.2
50	33	19	10		15	17	18	19

✓

88.7	88.6
6.4	6.5
50	34

91.35	91.5	91.1	91.6	91.8	91.7	91.5	91.7	91.1	90.5
8.54	8.4	8.8	8.3	8.1	8.2	8.4	8.2	8.8	9.4
45	29	27	12		11	20	21	41	45

✓

90.8	90.7
9.1	9.2
45	50

87.4
12.5
50

91.4	91.3	91.8	92.0	92.3	92.2	92.0	92.4	92.1	92.2
8.5	8.6	8.1	7.9	7.6	7.7	7.9	7.5	7.8	7.7
50	34	24	16		10	18	19	20	35

✓

92.0
7.9
50

Sta + π - Elev.

899.89

2+84

✓

3

✓

+20

March 25, 1964

✱

A

92.64

92.5

92.7

92.9

92.6

92.5

92.9

92.5

7.25

7.4

7.2

7.0

7.3

7.4

7.0

7.4

Curb
37

23

15

10

18

19

20

92.2

92.02

91.92

93.8

93.7

93.2

→ 7.7

7.87

7.97

6.1

6.2

6.7

37

43

50

50

38

28

G

conc

93.03

93.3

93.0

93.1

93.2

93.0

92.8

93.2

93.0

93.6

6.86

6.6

6.9

6.8

6.7

6.9

7.1

6.7

6.9

6.3

37

28

23

17

11

18

19

20

31

C

92.6

92.46

92.29

94.1

→ 7.3

7.43

7.60

5.8

37

43

50

50

G

93.56

93.6

93.4

93.6

93.7

93.4

93.2

93.7

93.8

6.33

6.3

6.5

6.3

6.2

6.5

6.7

6.2

6.1

36

29

25

18

11

17

18

24

93.1

92.69

94.9

94.5

→ 6.8

7.20

5.0

5.4

36

50

50

32

Sta + π - Elev.

899.89

3+58

✓

+79

✓

A

✓

BM

4.90 894.99 (895.00)

March 25, 1964

95.75 95.4 94.8 94.4 94.6 94.3 94.1 94.5 96.0

4.14 4.5 5.1 5.5 5.3 5.6 5.8 5.4 3.9

36 32 24 14 11 17 18 29

Conc. Wall

96.07

3.82

50

Conc. Wall

95.9

96.1

4.0

3.8

50

42

95.6 95.5 94.7 94.8 94.9 94.7 94.5 94.9 95.6

4.3 4.4 5.2 5.1 5.0 5.2 5.4 5.0 4.3

33 29 18 12 11 17 18 22

95.7

4.2

50

97.2

97.3

96.4

96.4

2.7

2.6

3.5

3.5

50

42

28

24

96.6 96.2 95.0 95.1 95.3 95.0 94.8 95.2 95.8 96.6

3.3 3.7 4.9 4.8 4.6 4.9 5.1 4.7 4.1 3.3

33 28 17 12 10 17 18 24 38

97.8

2.1

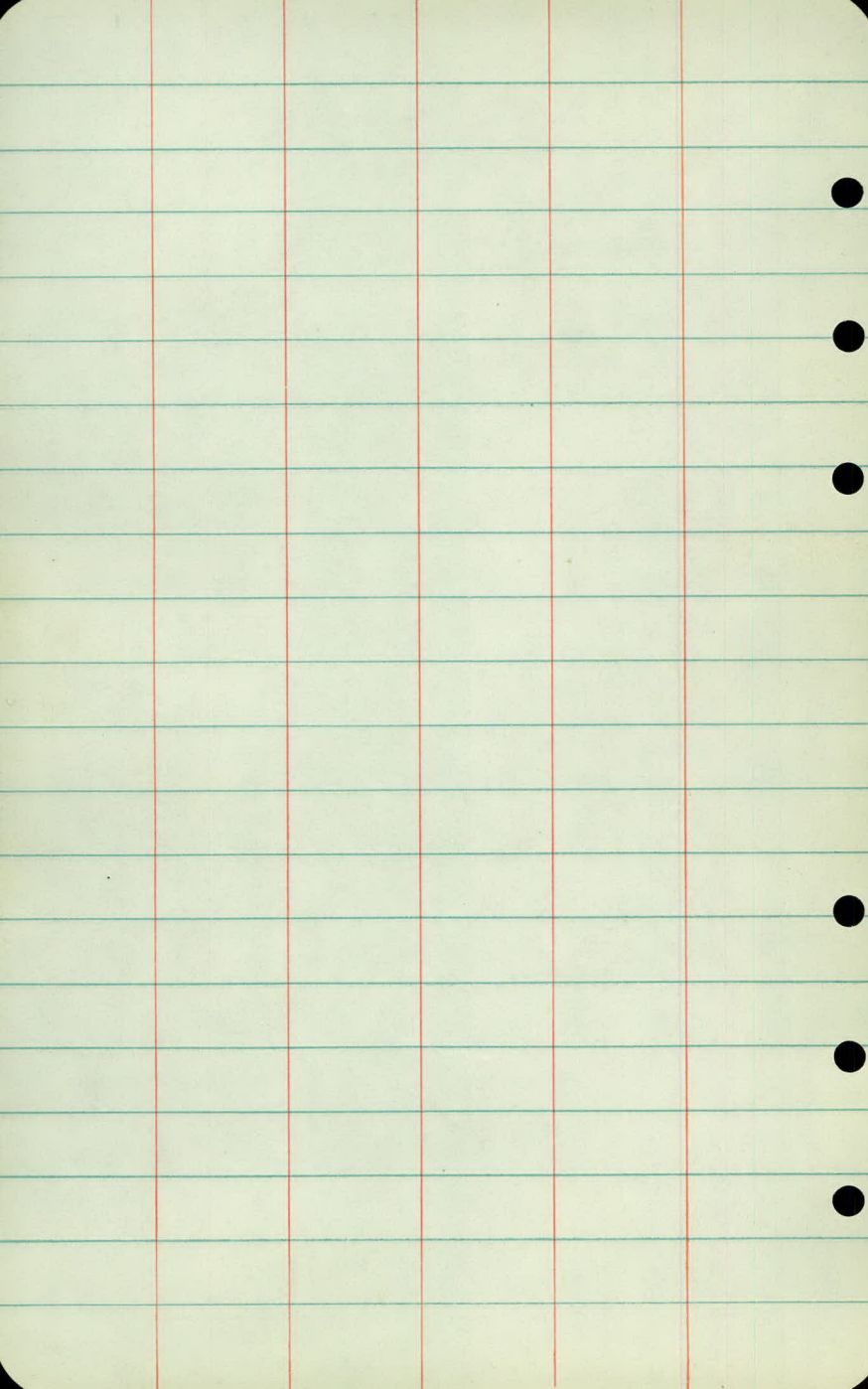
50

96.6

3.3

50

USGS BM



KP
JS
FS
WM
TH

6 APRIL 1964

1.

DALE STREET

LARPEUR AVE TO STH#36

ADDITIONAL X-SECTIONS

2 pages

STA

BM

+
0.0.5
5.0

892.8

π

892.65

897.6

-

ELEV.

92.8
95
87.8

892.6

0.84

891.95

20+41

BM

3.5

89.1
894.1

6 APRIL 1964 2.

£

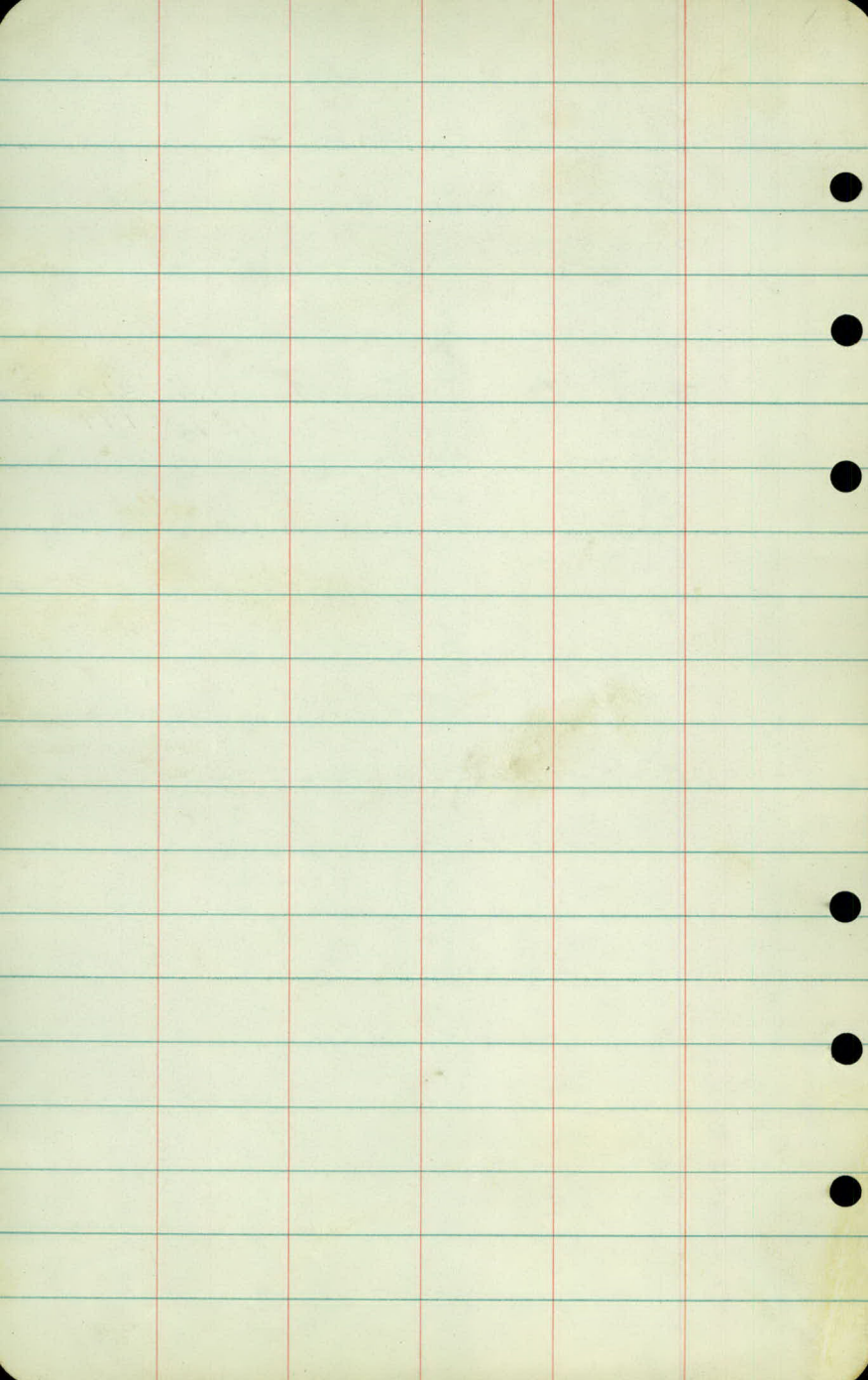
RT

TOP OF ROAD £ STA 20+41

CENTER OF MH 12.5' £ STA 20+56

87.8	875.6	72.1	64.9	64.1	61.6
0.05					
5.0	17.0	20.5	27.7	28.5	31.0
	100	127	150	157	177

TOP NAIL £ STA 20+00



1
Dale St

additional X-sections

Sta	+	π	-	Elev.
BM	0.60	893.66		893.06

TP	0.88	881.52	13.02	880.64
----	------	--------	-------	--------

T.P.	4.96	875.56	10.92	870.60
------	------	--------	-------	--------

13+25

T.P.	11.97	887.13	0.40	875.16
------	-------	--------	------	--------

T.P.	12.78	897.62	2.29	884.84	12+35
------	-------	--------	------	--------	-------

T.P.	12.92	910.09	0.45	897.17
------	-------	--------	------	--------

BM			2.01	908.08	906.03
----	--	--	------	--------	--------

BM	6.00	899.06		893.06
----	------	--------	--	--------

18+50

+53	141' Lt		3.39	95.67
-----	---------	--	------	-------

+62	163' Lt		0.77	98.29
-----	---------	--	------	-------

+88	127' Lt		3.76	95.30
-----	---------	--	------	-------

+89	142' Lt		2.05	97.01
-----	---------	--	------	-------

+89	158' Lt		0.63	98.43
-----	---------	--	------	-------

19

18+90	MH Lt		10.06	89.00
-------	-------	--	-------	-------

FK
WM
TL

March 10, 1964
Clear Cool 30°

Lt Rt 2
Top NE Cor Lower step Ho 1822 (Back Ent)

Top Fe Post 14+72

Top Fe Post 13+23

69.5	68.3	68.2	68.0	67.7	67.1	66.5	66.2	65.7	65.6	65.7
6.1	7.3	7.4	7.6	7.9	8.5	9.	9.4	9.9	10.0	9.9
100	85	65	43	22	5	✓	20	50	78	100

18+50

19+00

Bent 29+20 spike in

Top NE Cor Lower step Ho 1822 (Back Ent)

95.70	95.1	94.9	94.7	94.3	94.3	94.3	94.6	94.4
3.36	4.0	4.2	4.4	4.8	4.8	4.8	4.5	4.7
141	132	123.5	123	108	100	✓	89	88
					Lt		86	86

96.3	95.7	94.5	94.6	94.1	94.2	93.8
2.8	3.4	4.6	4.5	5.0	4.9	5.3
133	123	112	107	106	100	86

Lt

Sta + π - Elev.

899.06

20+20

✓

✓ MH ∇ Pineview Ct. 7.15 891.91 891.95

BM 11.69 912.19

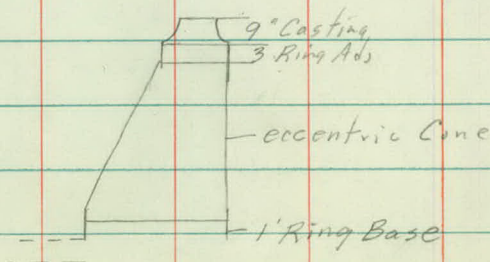
900.50

59+90

58+91 MH 30' Rt 15.33 96.86

61+10

61 ∇ 3.59 08.60



MH 58+91

March 10, 1964

Lt.

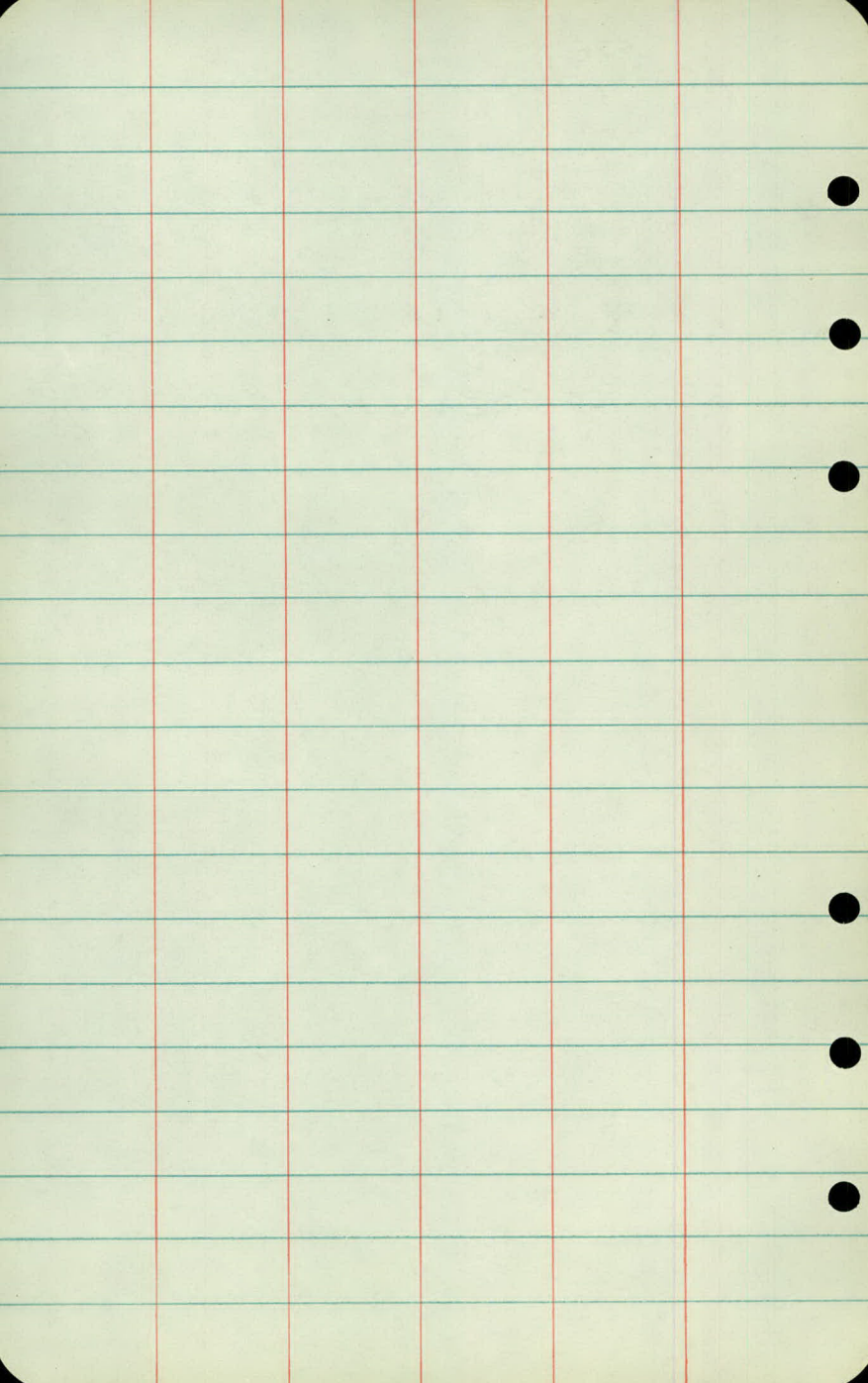
£

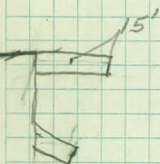
RT 3

92.2	92.4	92.4	90.6	89.1	87.9	87.0	86.0	86.1	85.2
6.9	6.7	6.7	8.5	10.0	11.2	12.1	13.1	13.0	13.9
27	26	23	16	9		3	11	19	24
92.4	92.3	92.7	92.5	95.8	97.5	79.8	80.8	82.3	84.2
6.7	6.8	6.4	6.6	3.3	1.6	19.3	18.3	16.8	14.9
47	67	69	74	81	86	75	65	51	35
£									

Top Hyd Lt Sta 69+15±

03.1	02.8	03.1
9.1	9.4	9.1
	33	43
09.1	10.0	10.45
2.1	2.2	1.74
	33	38.6
		Apron





19

127

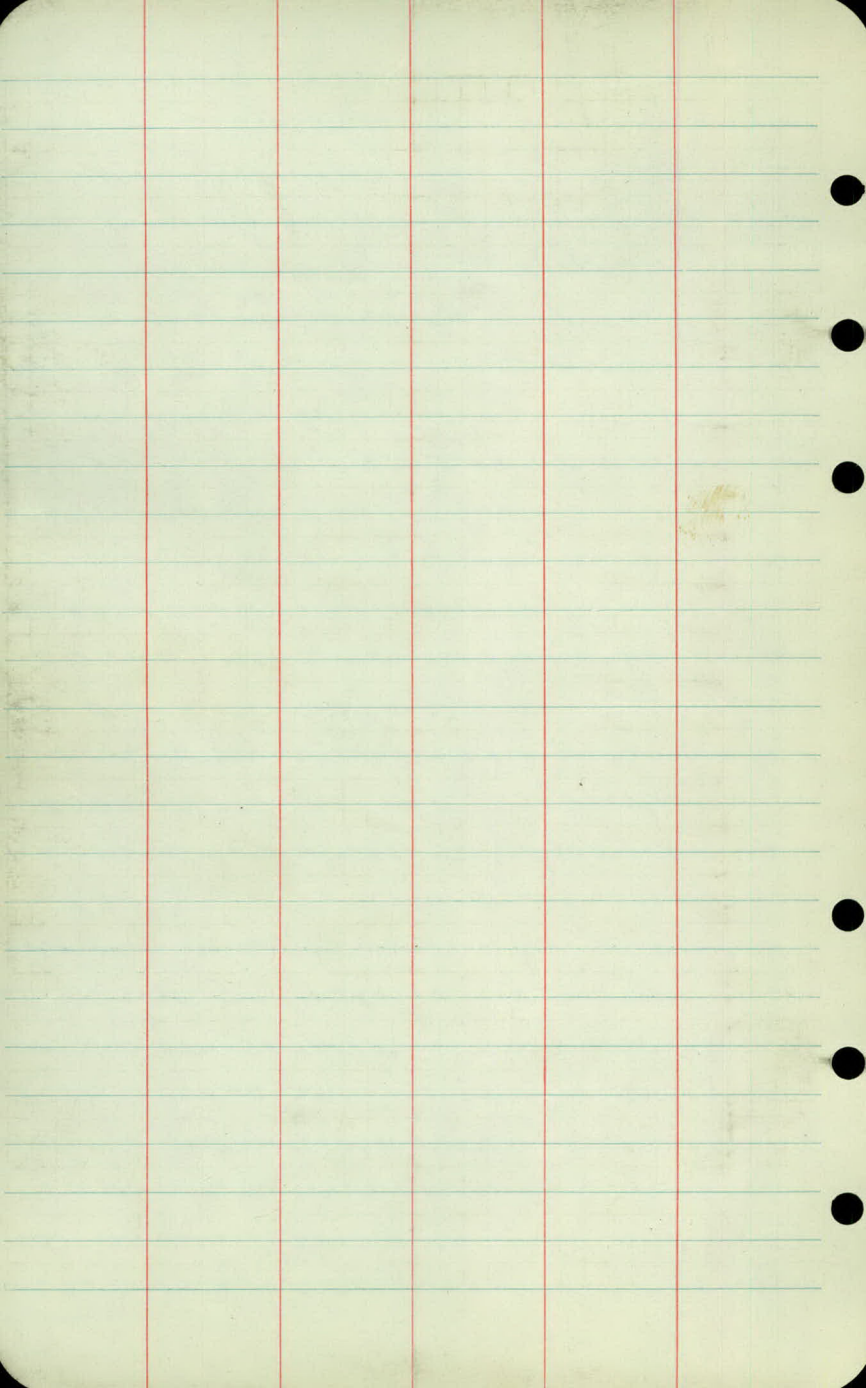
142

+89 - 158 $\neq$ Ent
+88 - 127 End Ent

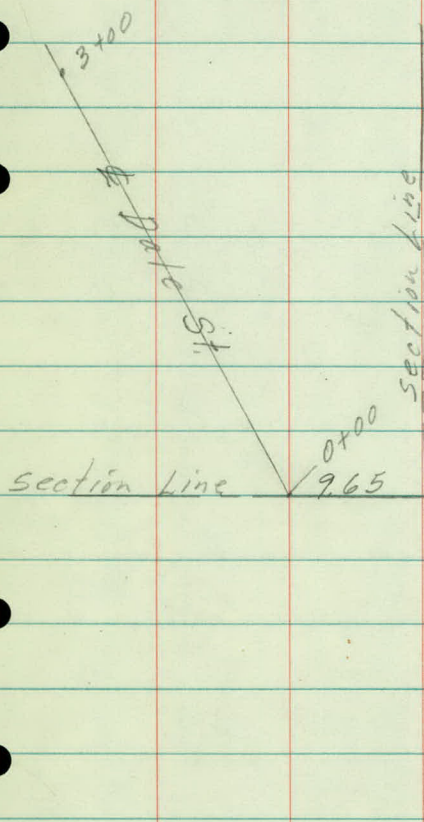
+62 164 $\neq$ Ent
+53 - 142 End Ent

18





Dale St. X-sections



Sta	+	π	-	Elev.
BM	1.05	922.60		921.55

1+00

+50

+25

2

+10

+40

FX
WS
DS
TL

March 5, 1964

Lt

4

RT

2

Top Hyd S.W. Cor Larpenteur & Dale St

19.9	19.4	19.0	19.3	19.2	18.9	18.4	17.9	17.6
2.7	3.2	3.6	3.3	3.4	3.7	4.2	4.7	5.0
50	39	25	16	✓	18	25	39	50
19.5	19.5	19.3	19.1	19.5	19.7	19.0	19.1	18.3
3.1	3.1	3.3	3.5	3.1	2.9	3.6	3.5	4.3
50	46	37	27	16	✓	16	21	27
18.2	18.0	18.2	18.0	18.2	18.0	18.2	18.0	18.2
4.4	4.6	4.4	4.6	4.4	4.6	4.4	4.6	4.4
50	50	50	50	50	50	50	50	50
19.4	19.4	19.5	19.4	19.7	19.9	19.3	19.4	18.9
3.2	3.2	3.1	3.2	2.9	2.7	3.3	3.2	3.7
50	42	30	23	17	✓	16	21	24
19.5	19.6	19.5	19.8	20.1	19.7	19.6	19.3	19.2
3.1	3.0	3.1	2.8	2.5	2.9	3.0	3.3	3.4
50	35	25	17	✓	16	20	27	41
19.8	19.6	19.6	20.0	20.2	19.7	19.7	19.4	19.4
2.8	3.0	3.0	2.6	2.4	2.9	2.9	3.2	3.2
50	34	26	14	✓	16	19	26	42
19.8	19.8	19.9	19.4	20.1	20.5	20.1	19.9	20.4
2.8	2.8	2.7	3.2	2.5	2.1	2.5	2.7	2.2
50	44	32	24	16	✓	15	19	28

Sta + π - Elev.

922.60

2+50

3

Sta 2 on sec Line 5.1

Additional X-Sections

BM 4.94 898.69

893.75

70 D.S.

18+69

✓

✓

Feb. 5, 1964

Lt					Rt				
20.3	20.2	20.3	19.8	20.2	20.5	20.0	20.4	20.2	20.8
2.3	2.4	2.3	2.8	2.4	2.1	2.6	2.2	2.4	1.8
50	43	33	24	17	16	19	28	41	50
21.1	20.8	20.0	20.5	20.8	20.5	20.4	20.6	20.7	21.0
1.5	1.8	2.6	2.1	1.8	2.1	2.2	2.0	1.9	1.6
50	36	26	17	14	16	18	30	41	50

N Rim MH Lt Sta 17+25±

87.6	86.8	85.7	86.6	87.4	86.4	86.4	84.7	84.4
11.1	11.9	13.0	12.1	11.3	12.3	12.3	14.0	14.3
36	22	15	5	6	14	24	45	
87.8	89.6	94.2	94.2	94.0			84.1	83.6
10.9	9.1	4.5	4.5	4.7			14.6	15.1
56	65	77	81	82			75	66

96.2	94.6	94.3	94.1
2.5	4.1	4.4	4.6
136	117	116	99

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		898.69		
--	--	--------	--	--

18+85				
-------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

19				
----	--	--	--	--

+15				
-----	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

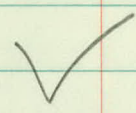
March 5, 1964

11

RT

4

89.3	88.2	87.3	86.7	86.3	85.7	84.6	83.8	84.4
94	10.5	11.4	12.0	12.4	13.0	14.1	14.9	14.3
61	99	32	9		13	25	54	75



94.0	94.1	93.7	94.0	94.1
4.7	4.6	5.0	4.7	4.6
71	75	76	93	100

95.30	94.5	94.3
3.39	4.2	4.4
130	112	111
Cone		

95.6	94.5	94.2	94.2	93.8
3.1	4.2	4.5	4.5	4.9
24	108	107	100	87

93.7	93.6	89.5	87.9	86.8	86.3	85.9	85.0	84.7	85.3
5.0	5.1	9.2	10.8	11.9	12.4	12.8	13.7	14.0	13.4
63	61	52	30	7		11	21	37	55

93.3	93.7	93.9	93.9	94.3
5.4	5.0	4.8	4.8	4.4
65	80	100	102	103

95.7
13.0
75

95.8	94.4
2.9	4.3
118	106

Sta + π - Elev.

898.69

19+34

✓

✓

+72

✓

20

March 5, 1964

B1

5

941	88.9	87.8	87.3	87.6	86.3	85.9	85.4	85.7
8.6	9.8	10.9	11.4	11.1	12.4	12.8	13.3	13.0
45	33	22	4		12	20	42	59

93.4	93.2	93.7	93.6	93.9				86.0
5.3	5.5	5.0	5.1	4.8				12.7
59	58	75	96	97				75

96.4	94.0
2.3	4.7
110	100

93.2	92.7	92.9	90.7	89.9	89.9	88.0	87.9	86.2	86.4
5.5	6.0	5.8	8.0	8.8	8.8	10.7	11.3	12.5	12.3
62	44	42	33	19		11	32	53	65

92.8	92.1	93.2	97.6					86.5
5.9	5.6	5.5	1.1					12.2
83	85	89	100					75

98.5	92.7	92.9	92.5
0.2	6.0	5.8	6.2
93	80	75	74

Sta + x - Elev.

898.69

20+41

✓

+72

✓

MH ± Pinetree Ch 6.80 891.89

✓

March 5, 1964

LT

£

RT

6

92.3	92.0	92.1	91.7	89.3	87.8	86.3	85.3	83.4	79.7
6.4	6.7	6.6	20	9.4	10.9	12.4	13.4	15.3	19.0
39	21	20	13	7		19	21	33	61

92.1	92.4	94.1	95.4
6.6	6.3	4.6	3.3
60	62	71	80

✓

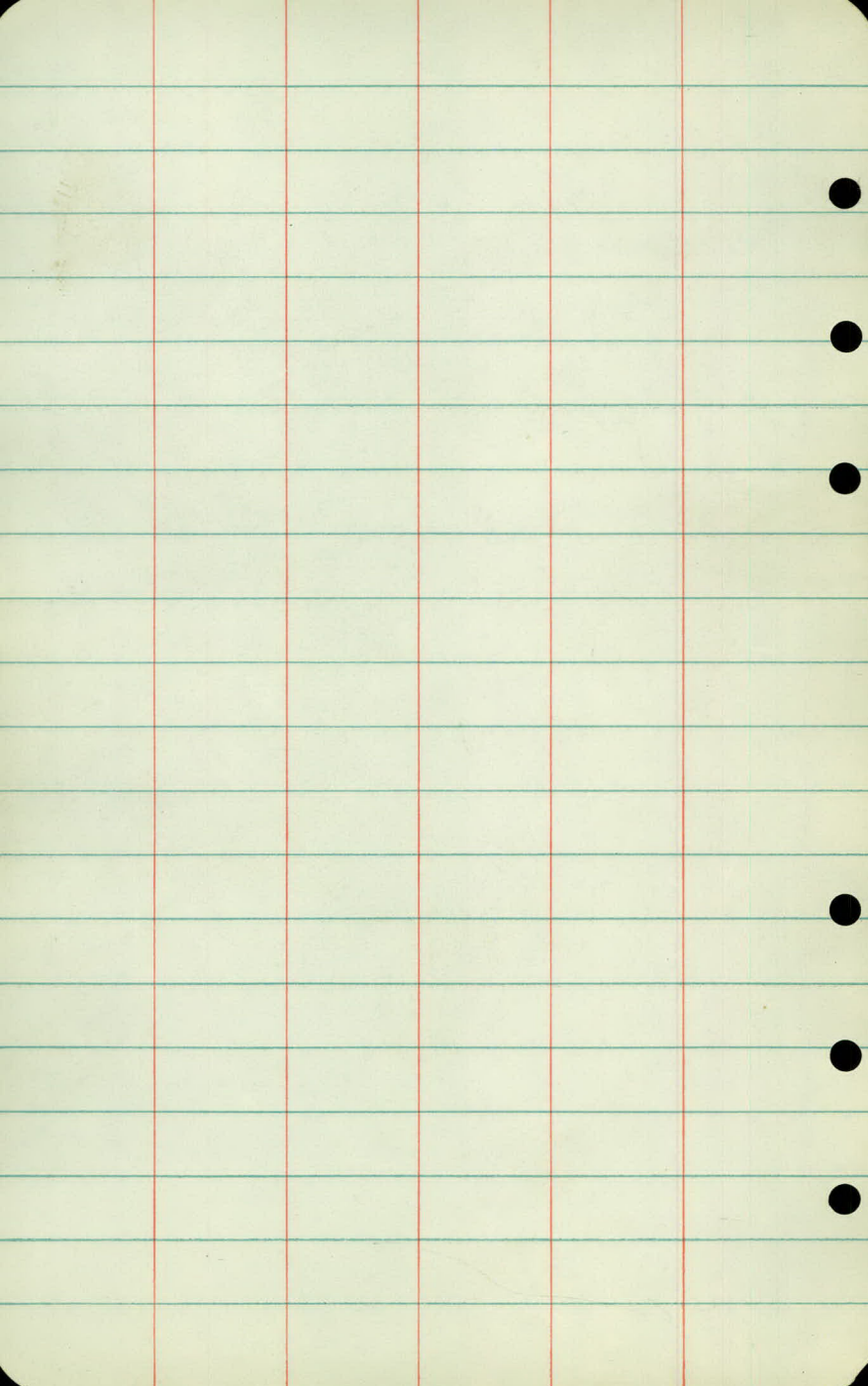
78.2
20.5
75

91.8	92.1	91.8	92.1	91.1	90.1	88.3	86.7	85.0	82.6
6.9	6.6	6.9	6.6	7.7	8.6	10.4	12.0	13.7	16.1
50	30	12	11	5		7	16	32	48

✓

92.0	92.4
6.7	6.3
62	78

78.1	81.3
20.6	17.4
75	56



Dale St

sect \$

$90^{\circ}21'40''$
 10230
 $91^{\circ}24'$

$0^{\circ}29\frac{1}{2}'$

$1^{\circ}31\frac{1}{2}$
 $29\frac{1}{2}$

$1002\frac{1}{2}$

$1032'$

π at Sta 20+00

26+00 = Az $0^{\circ}00'$

$\angle$ Dale st 270° 52'

Curb Pineview Ct S. Side $310^{\circ}05'$ 83'

Curb Pineview Ct N. Side $327^{\circ}28'$ 97.5'

NE Cor Ho $268^{\circ}50'$ 125'

SE Cor Ho $253^{\circ}20'$ 140'

BM 4.65 897.71 893.06

0+00 2.5 95.2

+50 2.9 94.8

1 3.2 94.5

+35 Conc Ent. Lt 2.02 95.69

+50 3.5 94.2

+72 Conc Ent. Lt 2.38 95.43

FK
WM
TL

March 12, 1964
Clear Cool 25°

2

= Sta 3+00

Top NE Cor Lower Step No #1822 (Back Eht)

Sta	+	π	-	Elev
-----	---	-------	---	------

897.71

2+00			3.9	93.8
------	--	--	-----	------

+50			4.2	93.5
-----	--	--	-----	------

3			5.0	92.7
---	--	--	-----	------

+48.5 R. Tie Curb			5.6	92.1
-------------------	--	--	-----	------

+48.5			5.7	92.0
-------	--	--	-----	------

+79.5 R. Tie Curb			5.7	92.0
-------------------	--	--	-----	------

BM			5.83	891.88	891.95
----	--	--	------	--------	--------

BM	9.00	909.50		900.50
----	------	--------	--	--------

60+75 Profile Lt in Ent.

60	£		6.01	903.50
----	---	--	------	--------

March 12, 1964

3

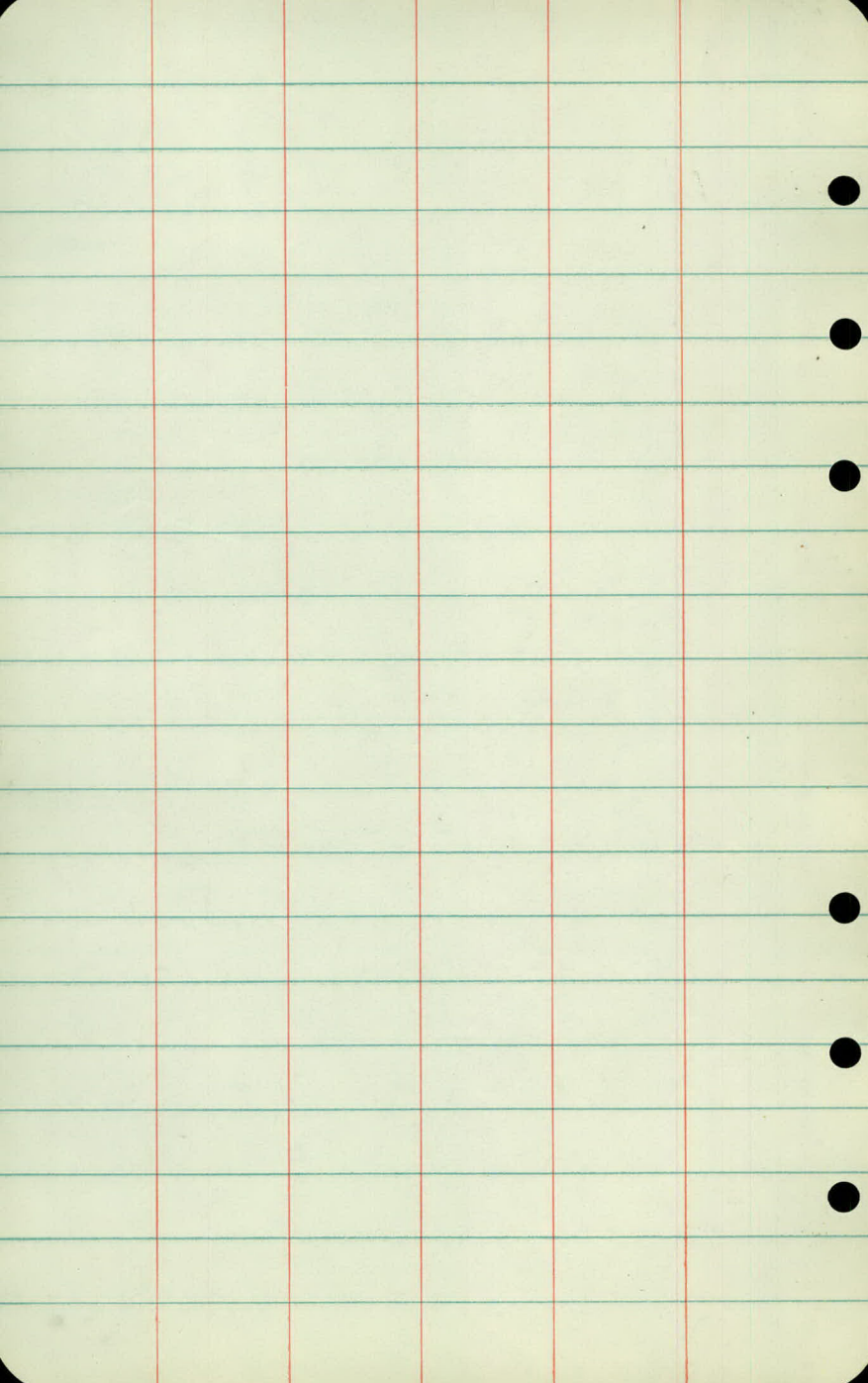
95.3	94.16	92.9	92.3
2.38	3.54	4.84	5.39
Curb	Curb	Curb	Curb
A+67	A+50	A+25	A

97.4	95.7	94.7	93.6	92.8	92.0
0.27	2.05	3.03	4.10	4.88	5.65
Curb	Curb	Curb	Curb	Curb	Curb
B+100	B+75	B+59	B+41	B+25	B

Top MH & Pinewood Ct.

Top Hyd Lt sta 59+15±

03.7	04.2	04.7	05.4	06.2	07.1	07.3
58	5.3	4.8	4.1	3.3	2.4	2.2
75	50	43	33	24.5	17	£
		Lt				



FK
JS
WM
TL

March 23, 1964

1

Dale St.

Co. Rd. "A²"

Dale to 200' East

X-sections

Rec. 3-23-64

Sta + π - Elev.

BM 9.74 916.99

907.25

0+42

+62

✓

/

✓

+15.5 30' Lt W.S.O.

+32

+41 E Wall Lt.

March 23, 1964

Flozy Windy 33° 2

1+

Roseville BM S.E. Cor. Dale & Co Rd "A2"

16.0	14.5	11.6	10.8	10.0	09.1	09.2	08.8	08.5	07.2	07.7	06.1
1.0	2.5	5.4	6.2	7.0	7.9	7.8	8.2	8.5	9.8	9.3	10.9
50	40	34	25	19	8		13	19	33	36	50

11.8	12.6	08.8	08.0	08.1	08.2	07.9	06.8	06.5	05.6
52	44	8.2	9.0	8.9	8.8	9.1	10.2	10.5	11.4
30	25	16	14	9		11	23	33	50

12.1	14.5	15.7	15.9
4.9	2.5	1.3	1.1
37	41	47	50

✓

10.2	06.2	05.5	06.0	06.2	05.9	05.5	05.0	04.0
6.8	10.8	11.5	11.0	10.6	11.1	11.5	12.0	13.0
23	16	13	8		10	14	19	32

13.1	13.8	13.4	13.7	14.6	14.8+
3.9	3.2	3.6	3.3	2.9	2.15
30	33	36	42	46	Walk 46

✓

04.7	03.9	03.9	04.4	04.5	04.3	03.63	03.3	02.4
12.3	13.1	13.1	12.6	12.5	12.7	13.36	13.7	14.
16	14	12	10		9	15	32	34

08.8	13.7	13.5	04.4
42	33	43	50

✓

14.8	50
------	----

Sta + π - E/cv

9/6.99

1+50

v

2+00

BM

3.30 913.69

4+41.5 30" CM X Drain

March 23, 1964

Lt

Lt

Rt 3

O.K.

07.0	03.6	02.9	02.9	03.5	03.6	02.8	01.8	01.2	03.2	00.5
10.0	13.4	14.1	14.1	13.5	13.4	14.2	15.2	13.8	16.5	
25	16	14	13	10		12	28	32	38	

10.0	11.5	13.2
2.0	5.5	3.8
33	35	50

15.8

00.3
16.7
50

✓

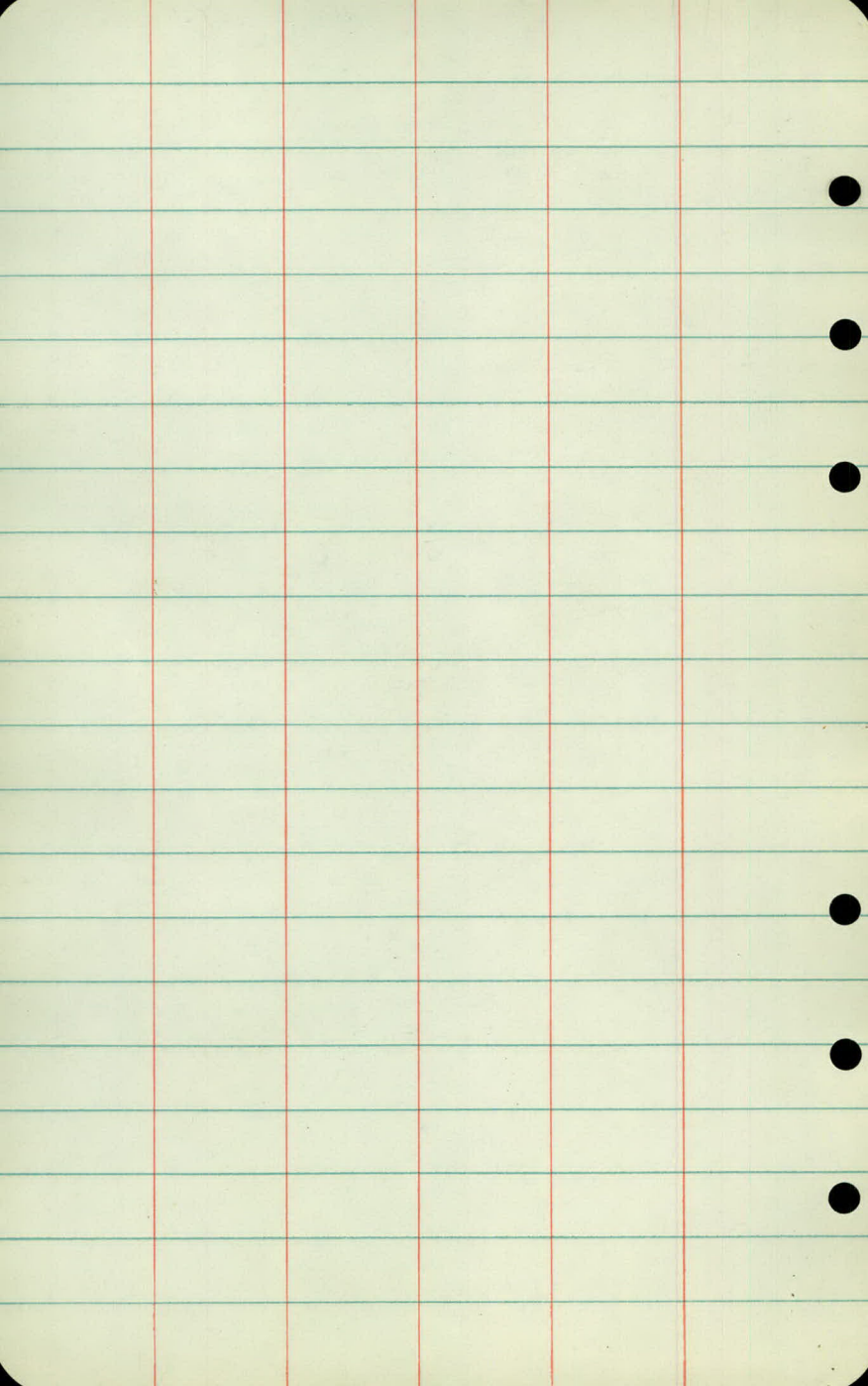
11.5	04.2	01.0	00.1	00.9	01.0	00.1	99.6	92.0	91.8
55	12.8	16.0	16.9	16.1	16.0	16.9	17.4	25.0	25.2
42	27	17	13-15	11		12	21	36	50

Bldg

✓

Top Hyd N.E. Cor A² + Date

✓



KP
US
FS
DS
WM
+L

8 APRIL 1964
COOL : SUNNY
40°

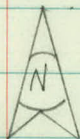
1.

DALE STREET

STA # 36 TO LARPEUR AVE

X-SECTIONS ON CO. RD A²

(7 PAGES)



ROSELAWN AVE

2+00

4+00

DALE ST.

STA	+	π	-	ELEV.
BM	5.45	912.70		907.25
1+00				
✓				
2+00				
✓				
✓				

8 APRIL 1964

2.

LT

±

RT

ROSEVILLE BM#16 SE. COR DALE & ROSE LAWN

06.2

6.5

01.0

8.6	11.5	12.5	11.9	11.7	12.4	13.3	17.4
25	18	14-16	12		10	21	29
		DITCH					FE

→	3.6	1.09	1.09
	35	41	44
		conc.	Blkg.

21.3	21.4	20.4	20.1
53	41	40	36

→	24.4	26.1	28.8
	70	87	100

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		912.70		
--	--	--------	--	--

2+12				
------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

8 APRIL 1963

3.

LT

4

RT

00.3

99.6

00.4

00.4

00.3

99.5

98.7

92.9

90.1

12.4 13.1 12.3 12.3 12.4 13.2 14.0 19.8 22.6

17 14-16 12 8 11 22 31 36

DITCH

FE

93.4

97.1

99.0

85.2

86.7

88.4

88.8

9.3 5.6 3.7

27.5 26.0 24.2 23.9

27 36 44

73 60 54 49

Cor Bldg.

83.0

81.8

29.7 30.9

90 100

97.9

96.8

98.2

98.4

98.3

97.6

96.9

90.7

85.3

14.8 15.9 14.5 14.3 14.4 15.1 15.8 22.0 27.4

20 16-18 13 8 11 20 31 46

DITCH

FE

99.9

92.7

96.7

97.7

10.1

80.1

81.7

83.8

12.8 10.0 6.0 5.0 2.6

32.6 31.0 28.9

24 35 45 49 50

100 83 63

WALL TOO WASH

10.7

2.0

60

STA	+	π	-	ELEV
-----	---	-------	---	------

		912.70		
--	--	--------	--	--

2456				
------	--	--	--	--

		17.29	895.41	
--	--	-------	--------	--

2467 = $\neq$ DRIVE				
---------------------	--	--	--	--

2476				
------	--	--	--	--

		18.17	894.53	
--	--	-------	--------	--

3400				
------	--	--	--	--

✓				
---	--	--	--	--

LT

E

RT

4.

FL W. END 18" CM 18.0 LT

97.5
 15.2
 9
 97.6
 15.1
 41
 99.8
 12.9
 64
 03.2
 9.5
 Left

FL E. END 18" CM 18.0 LT

96.8	94.2	95.9	96.1	96.0	95.3	94.9	88.3
15.9	18.5	16.8	16.6	16.7	17.4	17.8	24.4
24	17-19	13	8		12	21	32
	DITCH						FE
00.2	01.8	03.5	78.9	80.1	81.5	82.1	
12.5	10.9	9.2	33.8	32.6	31.2	30.6	
42	50	56	100	71	59	49	

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		912.70		
--	--	--------	--	--

3+31				
------	--	--	--	--

		19.70	893.00	
--	--	-------	--------	--

+37				
-----	--	--	--	--

		20.09	892.61	
--	--	-------	--------	--

+50				
-----	--	--	--	--

✓				
---	--	--	--	--

+90				
-----	--	--	--	--

✓				
---	--	--	--	--

8 APRIL 1964

5.

LT

±

RT

FL W. END 18" CM 19.0 LT

FL E. END 18" CM 19.0 LT

95.6	93.8	92.3	94.2	94.4	93.6	92.0	87.4	82.0
17.1	18.9	20.4	18.5	18.3	19.1	19.7	25.3	30.7
26	22	18-20	14		12	22	32	51
		DITCH					FE	
96.9	98.9	102.4				74.6	80.7	
15.8	13.8	10.3				34.1	32.0	
27	35	50				100	71	
TOP OF WALL								

94.2	98.5	97.0	94.0
18.5	14.2	15.7	18.7
38	38	28	27
TOP WALL	TOP WALL		
97.2	99.4	99.7	97.7
15.5	13.3	13.0	15.0
47	47	50	50
TOP WALL	TOP WALL		

STA	+	π	-	ELEV.
-----	---	-------	---	-------

		912.70		
--	--	--------	--	--

4+00				
------	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

✓				
---	--	--	--	--

+37				
-----	--	--	--	--

		25.7	887.0	
--	--	------	-------	--

+47				
-----	--	--	--	--

		24.1	888.6	
--	--	------	-------	--

8 APRIL 1964 6.

Δ
 92.9 92.2 90.2 86.4
 19.8 20.5 22.5 26.3
 12 26 32
 Fc
 84.3 83.7 83.9
 28.4 29.0 28.8
 50 44 36
 85.2 DITCH 85.2 85.3
 27.5 27.5 27.4
 69 83 100
 81.3 84.3
 31.4 28.4
 116 111

FL SEND 30" CM 30.0 RT

FL N. END 30" CM 19.0 LT

STA	+	Δ	-	ELEV.
		912.70		
4+73			23.7	889.0
5+14			23.2	889.5
5+00				
✓				
6+00				
✓				
7+00				
BM			5.45	907.25 (907.25)

8 APRIL 1964

7.

LT

~~E~~

RT

FL W. END 18" CM 19.0 LT

FL END 18" CM 19.0 LT

91.6

21.1

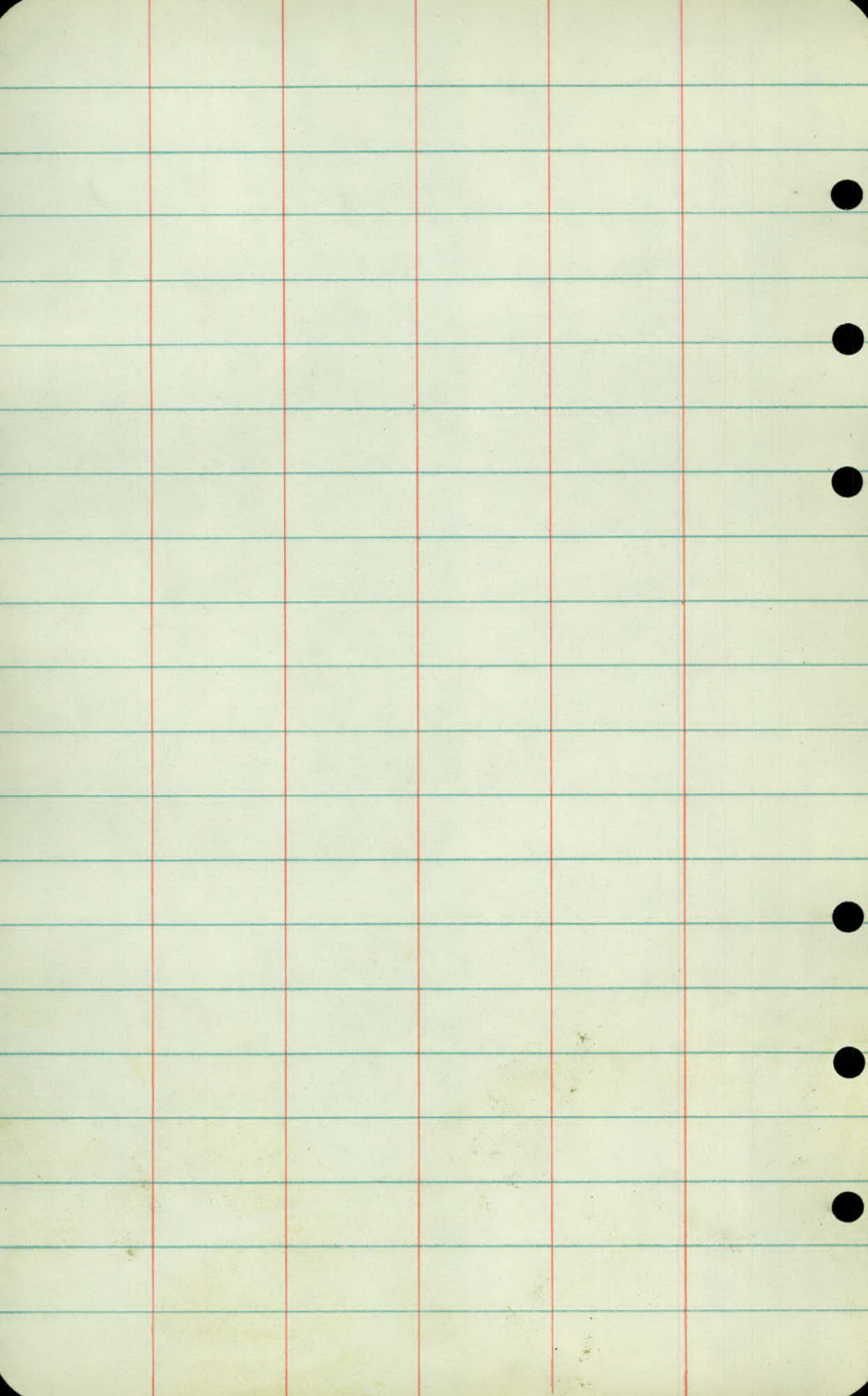
93.3

19.4

95.6

17.1

ROSEVILLE BM #16



KP
DS
JS
FS

9 APRIL 1964

WM
TH

ROSELAWN AVE
DALE ST TO RICE ST
X-SECTION THRU
LOWEST AREA ON
RIGHT.

STA + K -

BM 0.77 896.84

896.07

2+79

✓

12.62 908.69 0.77 896.07

BM

1.45 907.24 907.25

9 APRIL 1964

Rt.

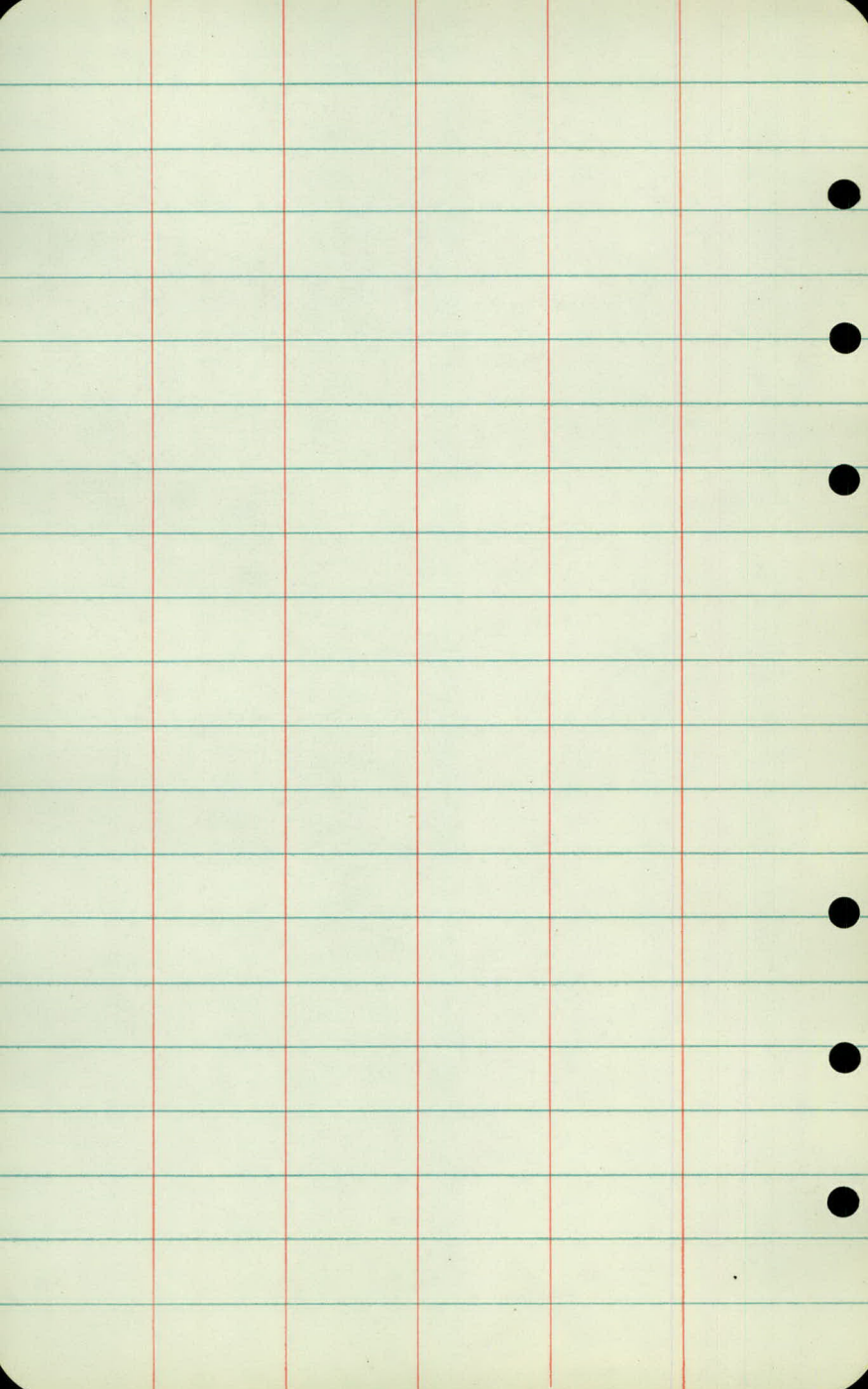
Top PK ± STA 3+00

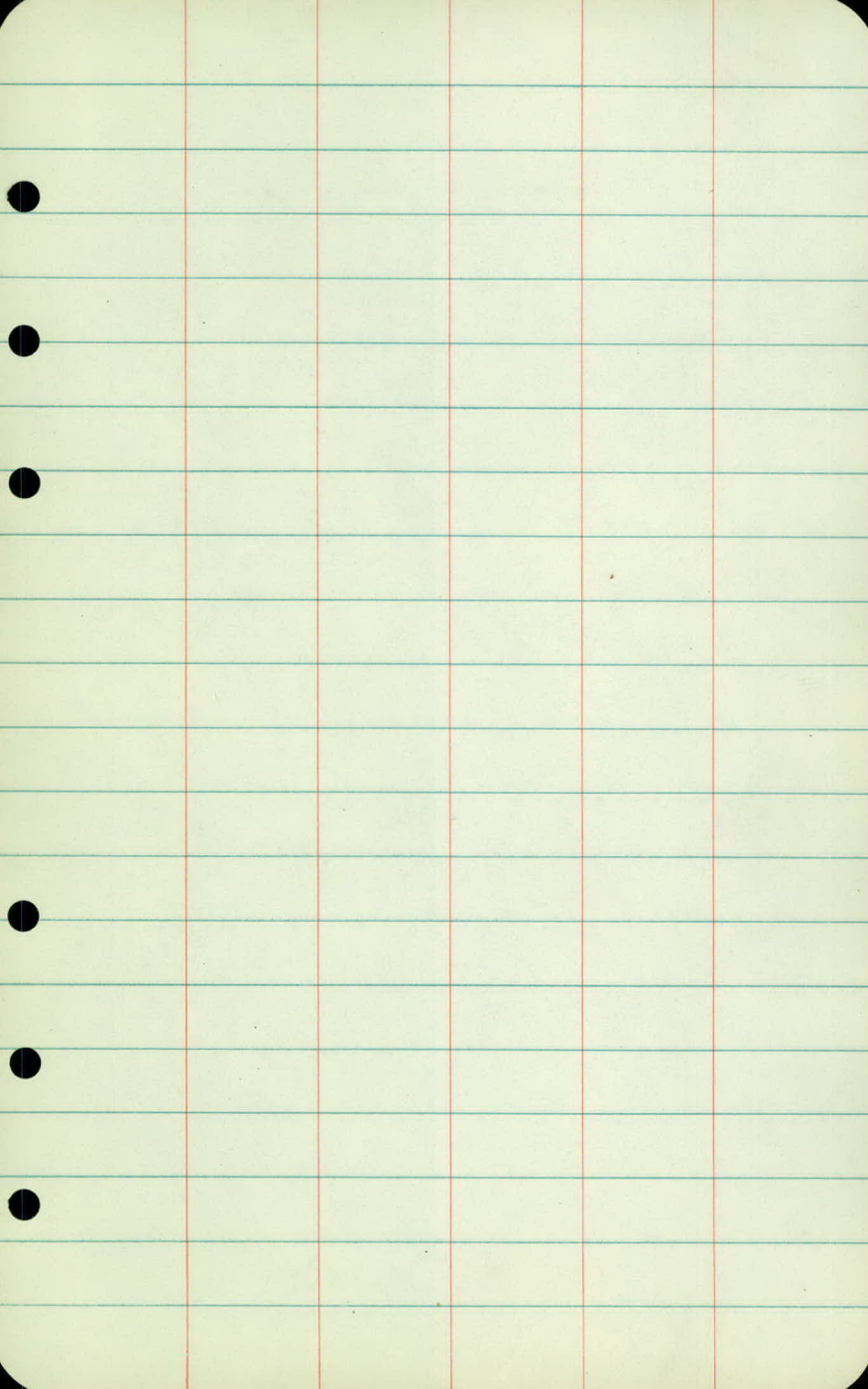
96.7	96.2	95.6	89.7	83.2	80.6	77.6
+0.1	0.6	1.2	7.1	13.6	16.2	19.2
	12	22	32	47	69	100
			FE			

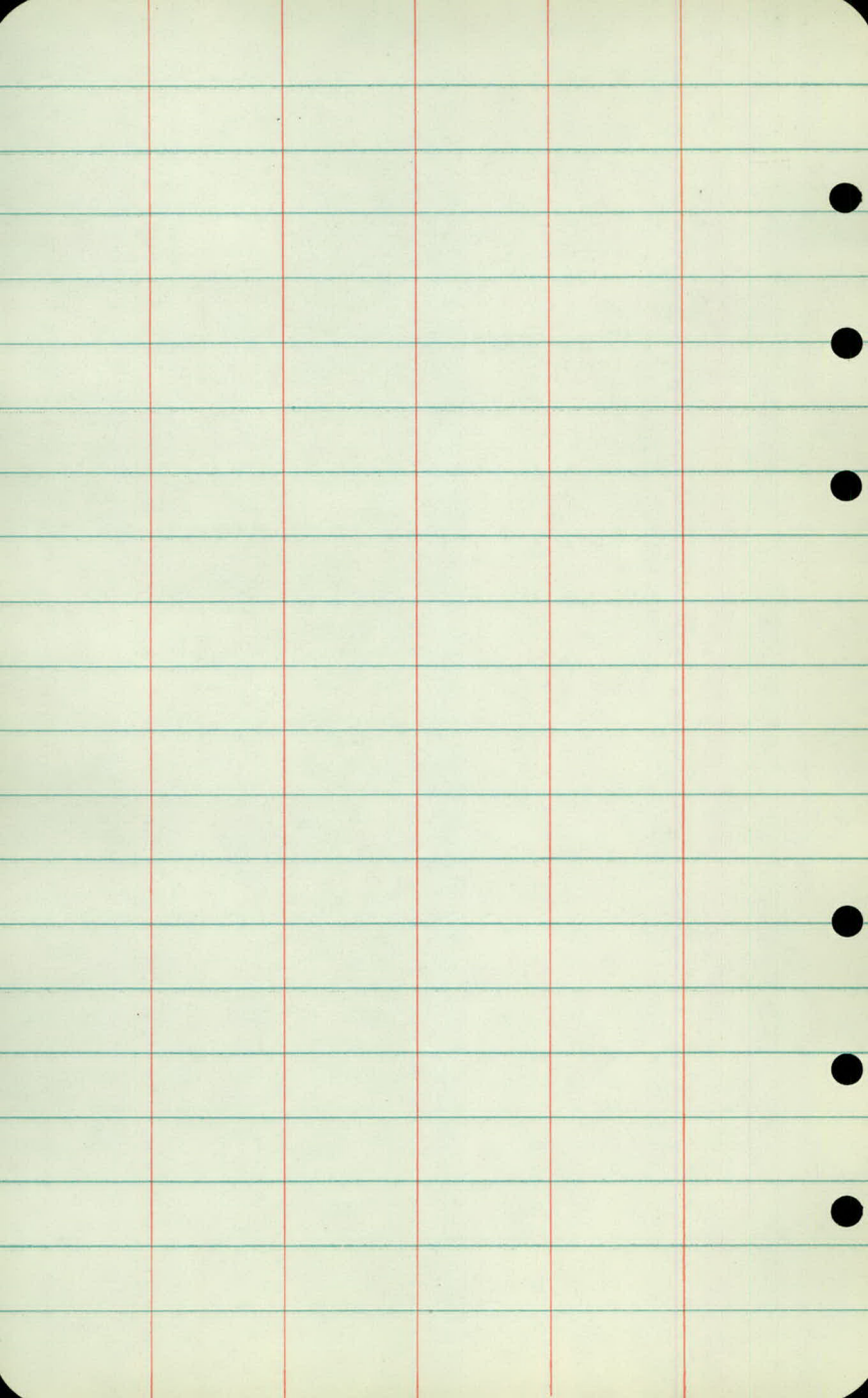
71.4	74.5	76.5
25.4	22.3	20.3
200	158	125

Top PK ± STA 3+00

ROSEVILLE BM #16







KP
JS
FS
DS
WM
TH

10 APRIL 1964

DALE ST.

STH # 36 TO CO. RD. B

SOUNDINGS

STA	+	π	-	ELEV.
BM	0.32	894.54		(894.22)
54+00			6.3	888.24
55+25			6.0	888.54
57+00			2.2	891.34
55+35			10.19	84.35
55+00			10.2	84.5
54+50			12.1	82.4

10 APRIL 1964

Lt

£

Rt

TOP HYDRANT N.E. COR DALE & CO. RD B

ELEVATION TEST HOLE #1 24' LT

ELEVATION TEST HOLE #2 24' LT

ELEVATION TEST HOLE #3 24' LT

FL 18" CM Lt 33.0

£ DITCH 73.0 LT.

£ DITCH 139.0 LT

STA	+	π	-	ELEV.
		894.54		

54+00

12.8

53+75

13.4

BM

3.42

891.12

891.13

10 APRIL 1964

Lt

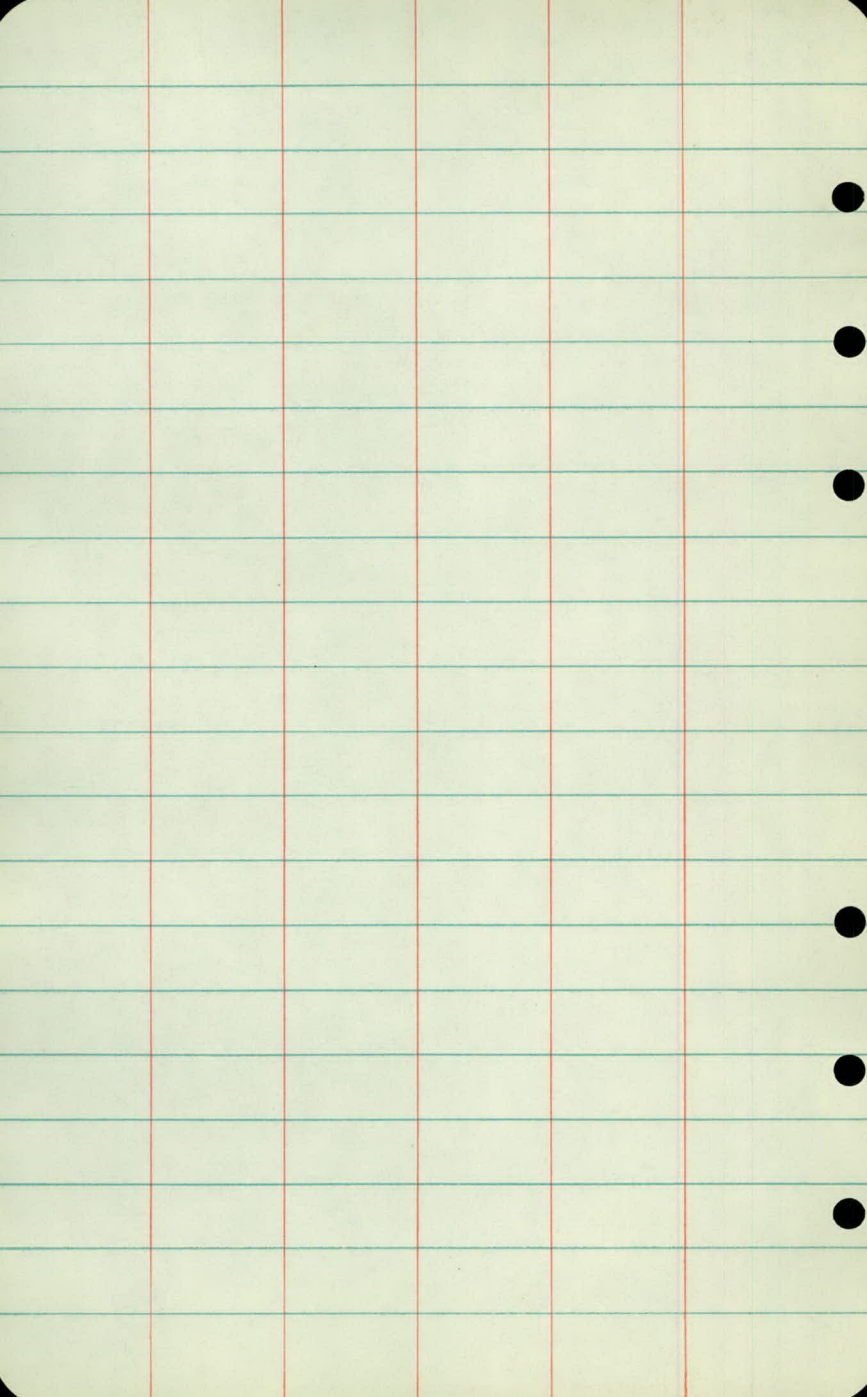
±

Rt

± DITCH 181.0 LT

END OF DITCH ± 202' LT

TOP HYDRANT 28' ± LT STA 56+05

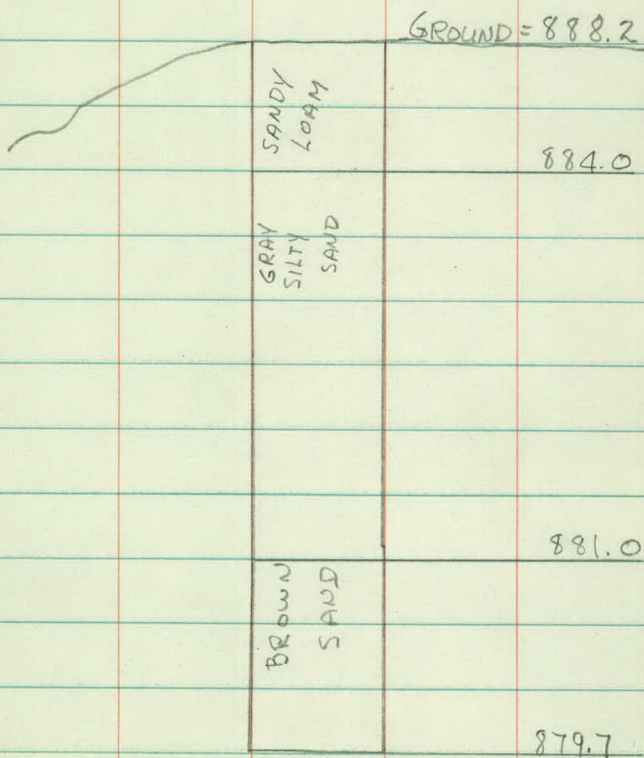


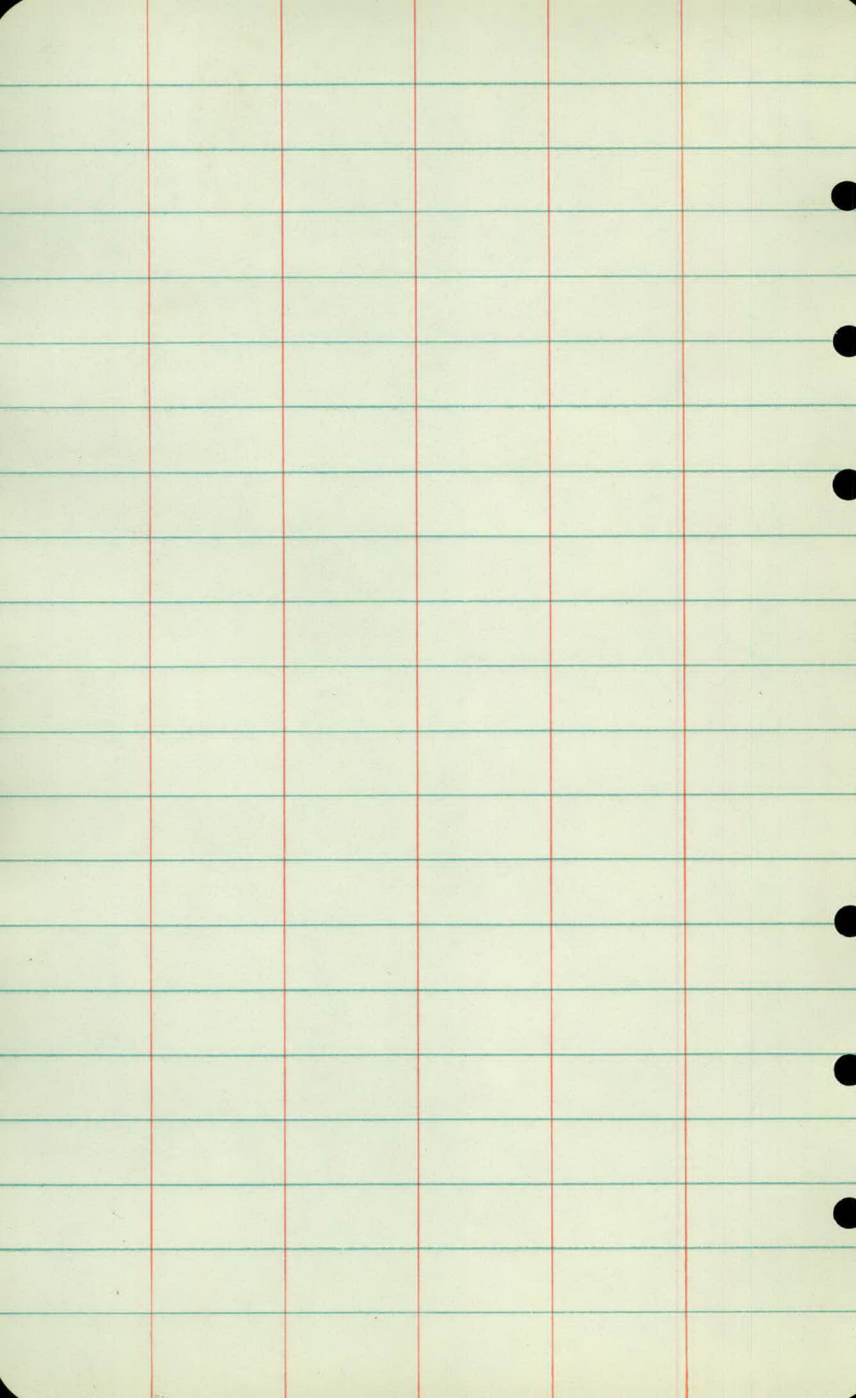
10 APRIL 1964

TEST HOLE #1

24' LT STA 54+00

ELEVATION 888.24



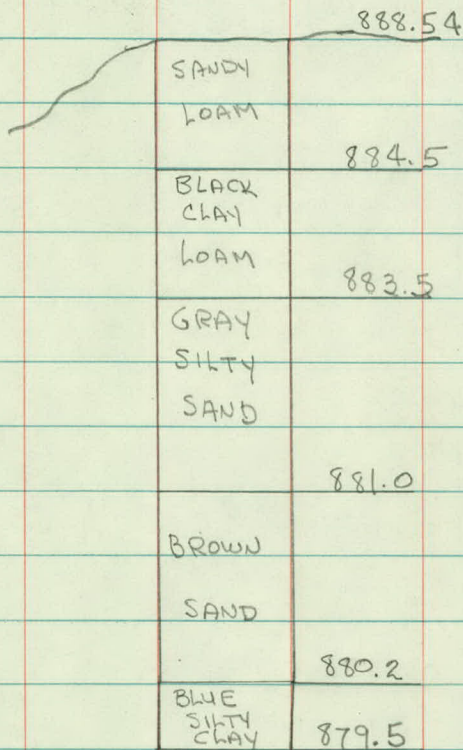


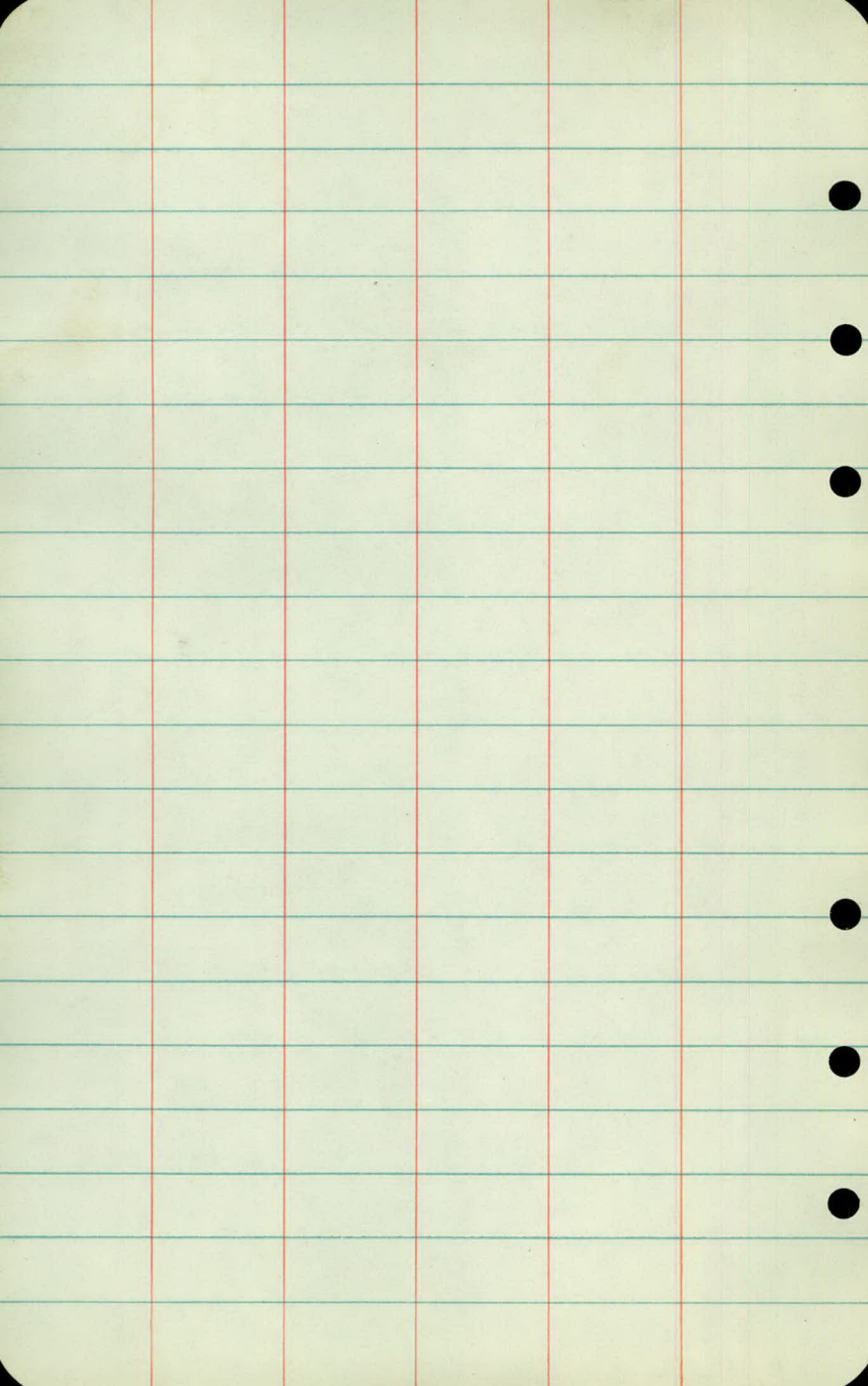
10 APRIL 1964

TEST HOLE #2

24' LT STA 55+25

ELEVATION 888.54





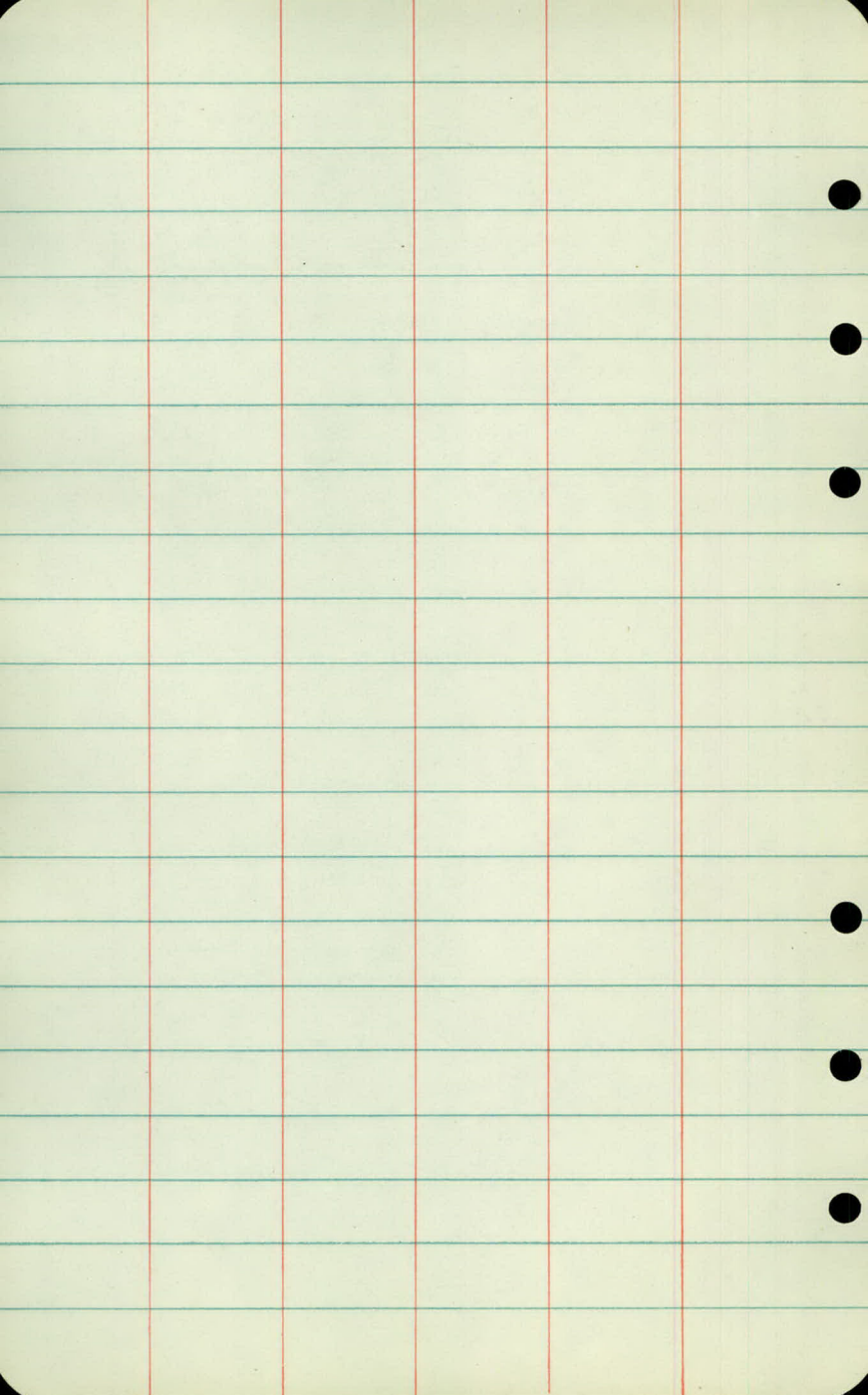
10 APRIL 1964

TEST HOLE # 3

24' LT STA 57+00

ELEVATION 891.34

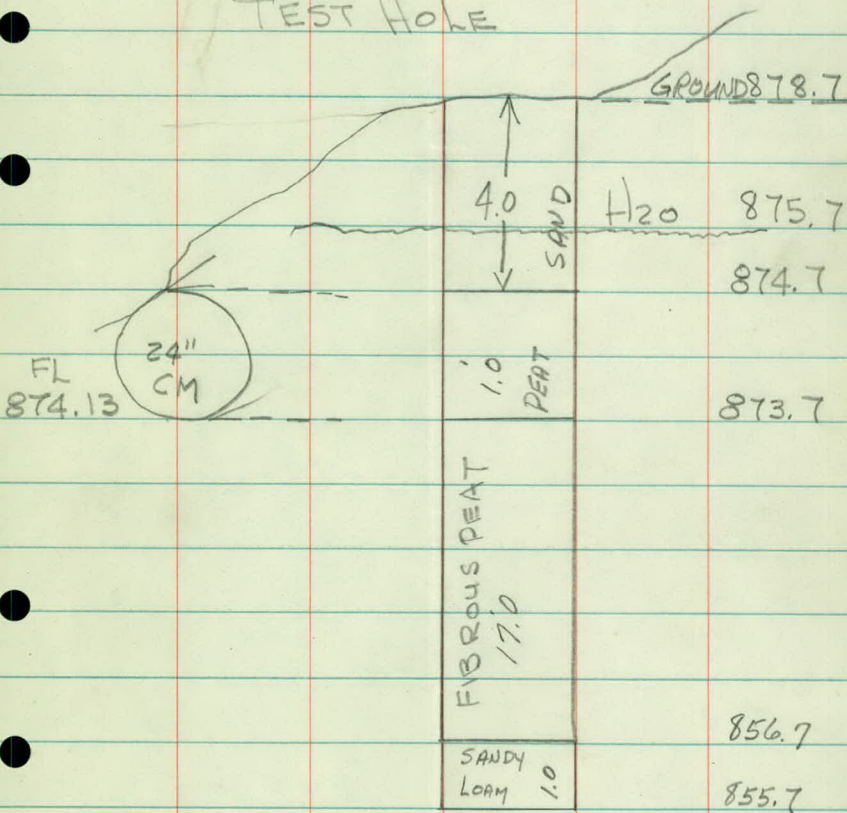
	891.34
SANDY LOAM	
	886.4
BLACK SILTY CLAY	885.1
GRAY CLAY (SANDY)	
	883.3

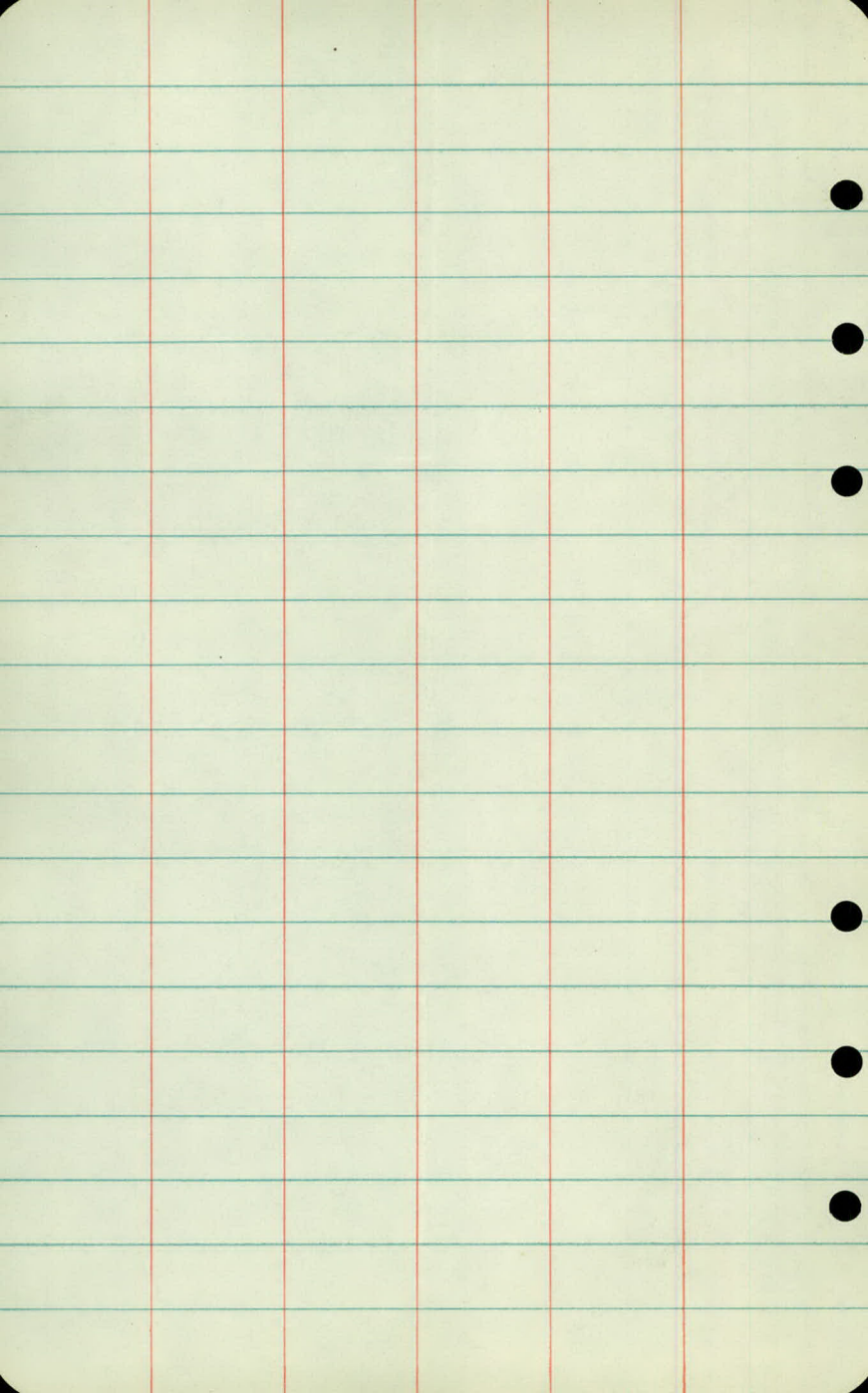


DALE ST.

50+93 LT 62.0

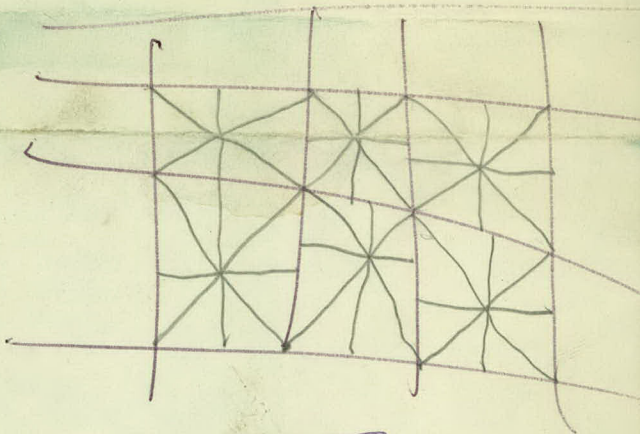
TEST HOLE





Alexander Const Co.
729-2304 ✓

Barton Const. Co.
425-2188



Aug
GEO. MATTSON
about

10 APRIL 1964

SPILLWAYS

STA

18+75

Center 3.0 Spillway (DIRT)
65-74 LT

19+05

Center 4.0 Spillway (BT)
54-67 LT

19+18

Center 3.0 Spillway (BT)
48-59 LT

22+33

Center 2.0 Spillway (BT)
11-26 RT

23+02

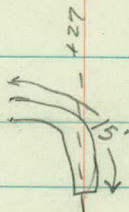
Center 30.0 Spillway (BT)
20-32 LT

10 APRIL 1964

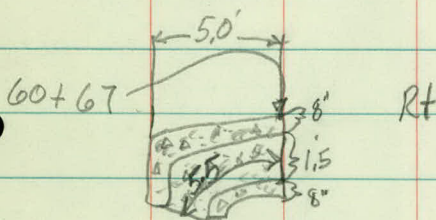
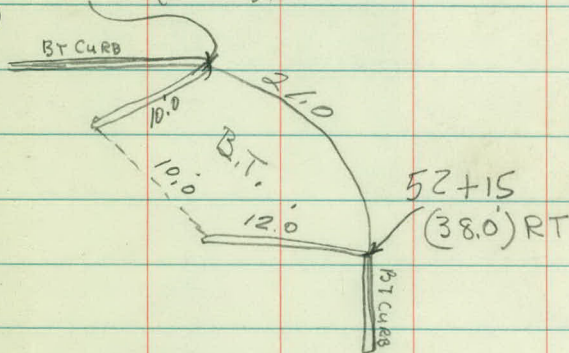
STA

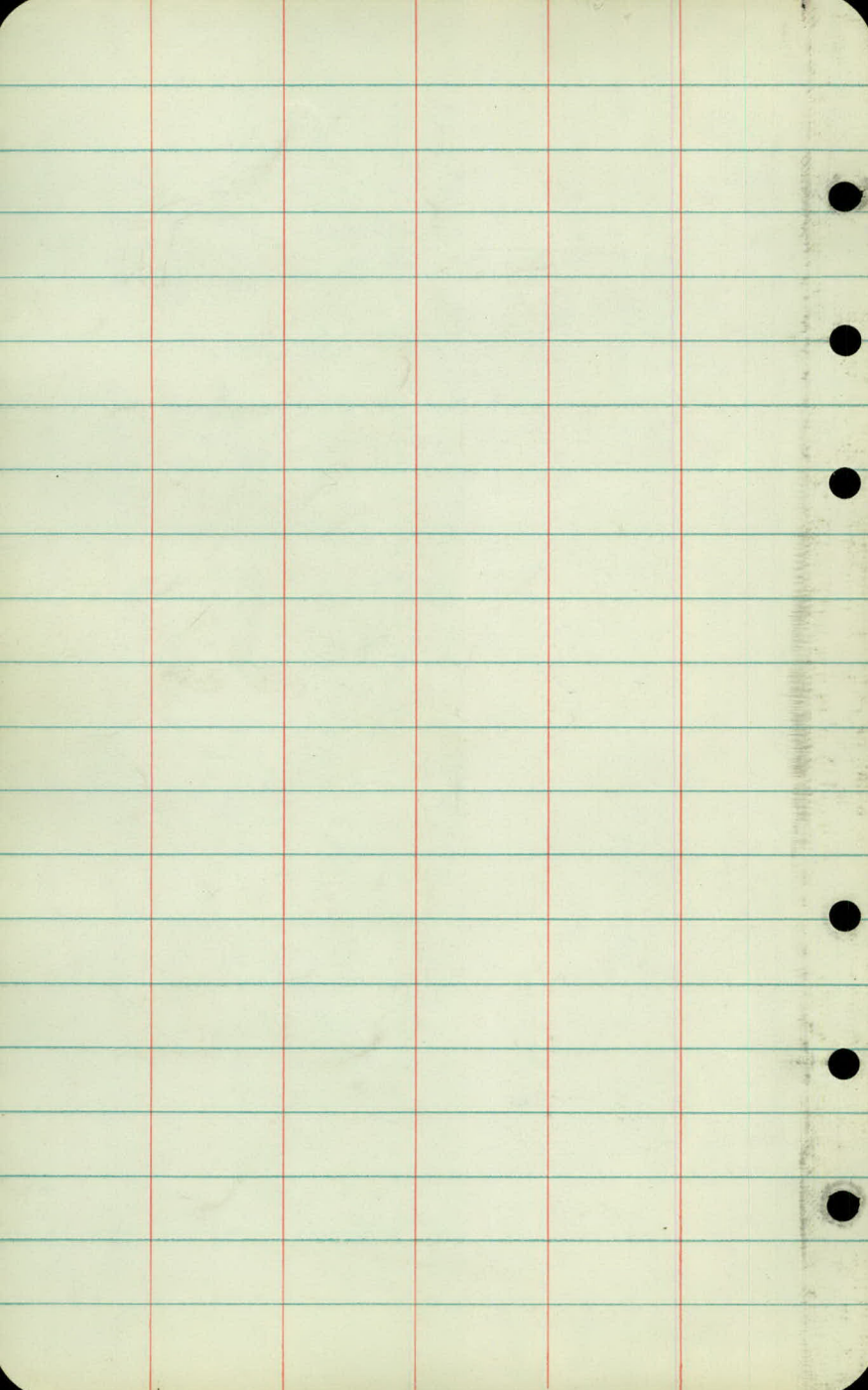
42+20

SPILLWAY
20-24
RT



52+00 (25.0') RT





Dale St.

Sta	+	Δ	-	Elev
BM	4.19	925.74		(921.55)
TP	0.04	916.84	8.94	916.80
6+54	Lt 87'		5.2	11.6
+86	Lt 102'		8.7	08.1
7	Lt 110'		8.9	07.9
+20	Lt 142'		5.2	11.6
9+00 [?]			3.75	913.1
TP			4.18	912.66 (912.73)

FK
WM
TL

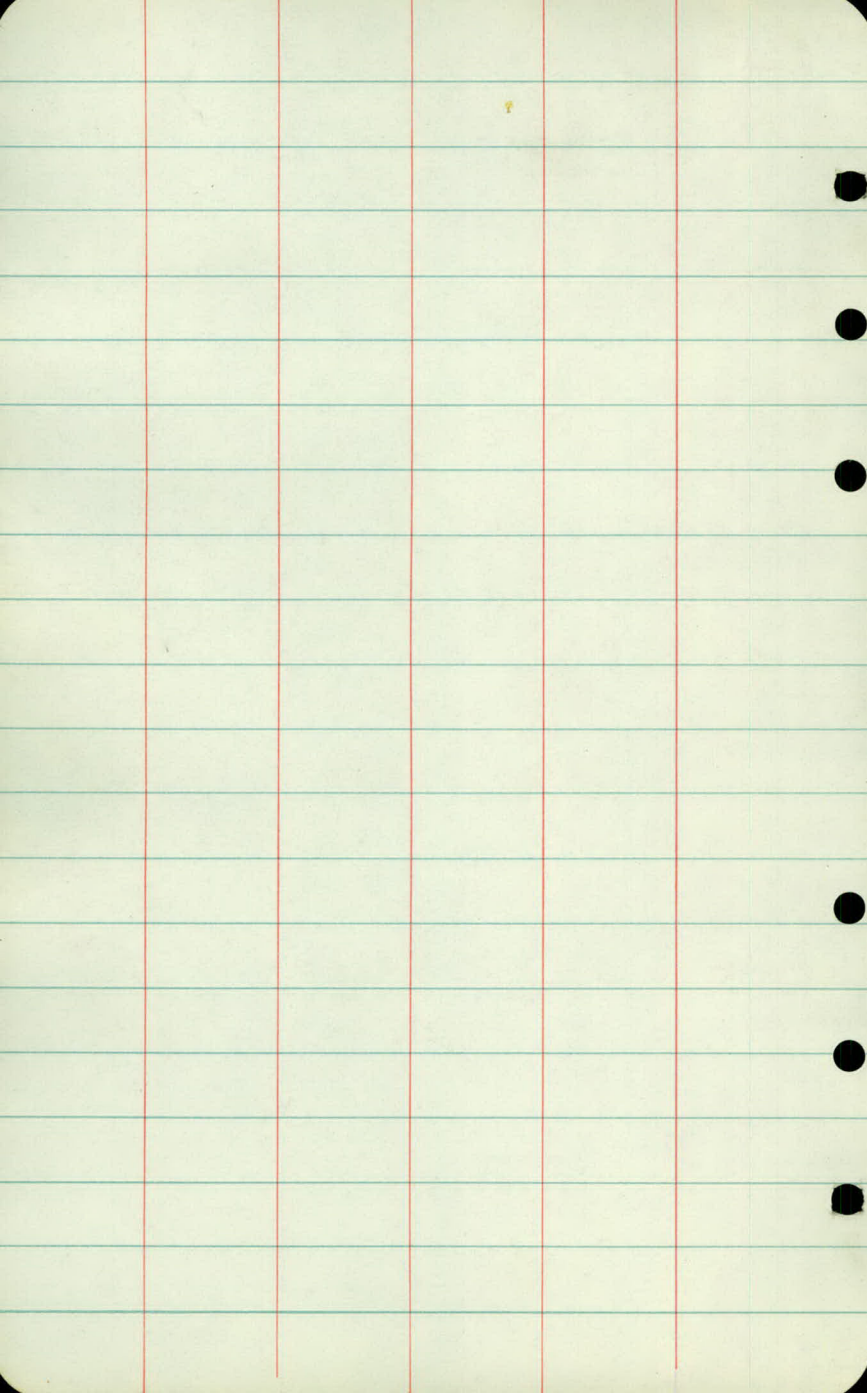
May 3, 1964

2

BM top Hyd S.W. Cor Larpenteur & Dale

75

stone



1
Dale Street

x-section Extensions

Sta	+	π	-	Elev.
BM	1.06	918.19		917.13

TP	0.55	905.17	13.57	904.62
----	------	--------	-------	--------

TP	4.72	898.57	11.32	893.85
----	------	--------	-------	--------

7+24

TP	12.80	910.54	0.83	897.74
----	-------	--------	------	--------

+24

+50

+71

TP	12.37	921.01	1.90	908.64
----	-------	--------	------	--------

7+24

+50

FK
DS
TL

Lt

May 20, 1964

Clear 54°

£ 2

Iron pin at Fe Post

98.0	93.5	91.8	91.4	90.0	90.1	89.3
0.6	5.1	6.8	7.2	8.6	8.5	9.3
105	96	74	60	39	19	

10.1	03.5
0.4	7.0
123	114

10.5	01.7	98.5
0.0	8.8	12.0
131	117	100

08.4	05.4
2.1	5.1
133	125
	100

13.9	12.4
7.1	8.6
161	133

14.0	13.0	12.8
7.0	8.0	8.2
161	149	135

Sta + π - Elev.

921.01

7+71

+98

8

+20

TP 7.33 924.46 3.88 912.13

+45

+60

May 20, 1964

Lt

3

15.8	14.9	12.9	12.0
5.2	6.1	8.1	9.0
158	151	137	133

19.2	18.0	18.5	17.2	16.5
1.8	3.0	2.5	3.8	4.5
150	133	115	105	100

21.0	20.9	20.1	19.4	17.7
0.0	0.1	0.9	1.6	3.1
150	133	115	105	100

20.5	19.8	18.1
0.5	1.2	2.9
110	100	90

21.5	20.4	20.1
3.0	4.1	4.4
117	100	91

22.0	21.8	21.6
2.5	2.7	2.9
117	100	91

Sta + π - Elev

924.46

9+00

+32

8+60 $\neq$

~~11.4~~ ~~13.0~~ 13.3

9 $\neq$

13.16 11.3 ✓ 11.3

May 20, 1964

LH

4

14.4	16.8	14.8
8.1	7.7	7.7
118	100	96

10.7	10.3
13.8	14.2
105	80

$$\begin{array}{r}
 893.06 \\
 \underline{29} \\
 893.35 \\
 \underline{11.60} \\
 881.75 \\
 \underline{80} \\
 882.55 \\
 \underline{866.70} \\
 15.85 \\
 \underline{13} \\
 2
 \end{array}$$

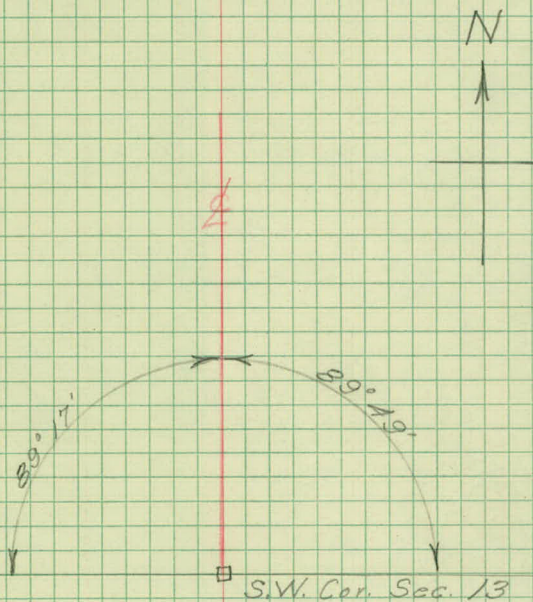
$$\begin{array}{r}
 882.50 \\
 \underline{3.9} \\
 878.65
 \end{array}$$

$$\begin{array}{r}
 93.92 \\
 \underline{11.44} \\
 82.48
 \end{array}$$

FK
LC
JM
RG

May 25, 1956
Fair 50°

1



Date 5/25

Horse Locations

5

+05 End Fe
32.8

4

+57.2 S.E. Cor. Ho.
56.2

3

+64.2 S.E. Cor Ho
36.0+64.2 Fe
33

2

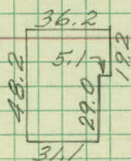
1

+75 Fe Cor Pillar
33.1

0+00 £ Larpenteur

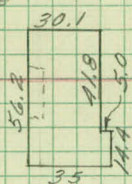
May 25, 1956

2



Note:

Houses Square
With Section
Lines



Dale Street

Profile

Larpentour to Roselawn

26 13.2

8 pages

1-7 Void

7h

Sta	+	x	-	Elev.
BM	1.85	923.27		921.42
0+00	± Lamp		4.60	18.67
0+045	Sec. Cor.		4.64	18.63
+50			4.7	18.6
1			5.7	17.6
+50			6.3	17.0
2			5.9	17.4
+50			4.9	18.4
3			4.0	19.3
+50			3.0	20.3

FA
LB
BZ
FK

August 6, 1963

2

Top Hyd SW Cor Larp & Dale

Sta + π - 902.56
Elev.

923.27

4 2.9 20.4

+50 2.9 20.4

+80 3.4 19.9

T.P. 1.52 921.65 3.14 920.13

5 3.5 18.2

+10 3.8 17.9

+26 4.4 17.3

+32 5.2 16.5

+49 10.9 10.8

T.P. 2.83 923.31 1.17 920.48

B.M. 3.08 912.78 13.61 909.70

T.P. 1.08 900.99 12.87 899.91

B.M. 8.08 892.91

August 6, 1963

3

Top S.W. Cor. C.B. by 1766 Dale St.

N.W. Cor Walk Ho #1822 Dale St

Sta	+	π	-	Elev.
		900.99		
TP	4.69	898.22	7.46	893.53
TP	13.61	910.63	1.20	897.02
BM	3.48	910.63	3.48	907.15

26+13.2 +0.13 10.76

26+13 +0.4 11.0

26 0.4 10.2

+50 3.4 07.2

25 6.5 04.1

+50 9.4 01.2

24 12.1 98.5

TP 0.02 899.38 11.27 899.36

+50 3.6 95.8

August 6, 1963 4

Bench Elev. Marker S.E. Cor Dale & Roseb.

Top Monument $\pm$ Dale & A² or Rosebawn

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		899.38		
--	--	--------	--	--

23			5.7	93.7
----	--	--	-----	------

+50			6.9	92.5
-----	--	--	-----	------

22			7.3	92.1
----	--	--	-----	------

+50			7.7	91.7
-----	--	--	-----	------

21			7.8	91.6
----	--	--	-----	------

+50			10.7	88.7
-----	--	--	------	------

2428			12.6	86.8
------	--	--	------	------

20			10.4	89.0
----	--	--	------	------

+71			9.5	89.9
-----	--	--	-----	------

+50			10.7	88.7
-----	--	--	------	------

August 6, 1963

5

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		899.38		
--	--	--------	--	--

+12			13.3	86.1
-----	--	--	------	------

19			13.6	85.8
----	--	--	------	------

T.P.	7.15	896.82	9.71	889.67
------	------	--------	------	--------

+70			9.8	87.0
-----	--	--	-----	------

+50			10.4	86.4
-----	--	--	------	------

+25			12.4	84.4
-----	--	--	------	------

18			14.1	82.7
----	--	--	------	------

+83			14.7	82.1
-----	--	--	------	------

+61			11.1	85.7
-----	--	--	------	------

+35			7.4	89.4
-----	--	--	-----	------

+13			6.8	90.0
-----	--	--	-----	------

17			6.8	90.0
----	--	--	-----	------

BM	1.66	894.57	3.89	892.93	(892.91)
----	------	--------	------	--------	----------

FK
LB
BZ
FK

August 6, 1963 6

N.W. Cor Walk Ho # 1822 Dale St.

Sta	+	π	-	Elev.
		894.57		

16+54			4.0	90.6
-------	--	--	-----	------

+19			6.7	87.9
-----	--	--	-----	------

16			7.6	87.0
----	--	--	-----	------

+72			9.2	85.4
-----	--	--	-----	------

+50			10.3	84.3
-----	--	--	------	------

+23			12.8	81.8
-----	--	--	------	------

T.P.	0.38	882.58	12.37	882.20
------	------	--------	-------	--------

15			3.3	79.3
----	--	--	-----	------

+80			6.0	76.6
-----	--	--	-----	------

+62			8.7	73.9
-----	--	--	-----	------

+37			11.5	71.1
-----	--	--	------	------

+12			13.0	69.6
-----	--	--	------	------

14			13.7	68.9
----	--	--	------	------

T.P.	3.83	876.39	10.02	872.56
------	------	--------	-------	--------

+70			8.6	67.8
-----	--	--	-----	------

+54			9.0	67.4
-----	--	--	-----	------

+31			9.9	66.5
-----	--	--	-----	------

+06	Corr.		9.5	66.9
-----	-------	--	-----	------

T.P.	12.88	888.60	0.67	875.72
------	-------	--------	------	--------

FK
LB
BZ
FK

August 7, 1963

7

Sta	+	π	-	Elev.
-----	---	-------	---	-------

		888.60		
--	--	--------	--	--

T.P.	12.04	898.87	1.77	886.83
------	-------	--------	------	--------

T.P.	13.55	912.00	0.42	898.45
------	-------	--------	------	--------

BM	13.50	923.30	2.20	909.80
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BM	2.63	924.54	1.39	921.91
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BM			3.07	921.47 (921.42)
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August 7, 1963 8

Tap Hyd S.W. Cor Dale & Larpenteur

St. 27.47
27.87
276.88

Dale

95' 85' 71.64 75 60
95 84.36 70.55 71.64
95

59.90

Judicial Peroration = 291.64
County Distance = 291.64

8+59.77

Used 5+69.15
5+69.15
5+68.02

dyeline Fe A

end Fence

Extended Fence line

old location of iron
0.75'
0.20' IRON

59°26'
89°0'1/2'

E DALE ST E

13400

14100

13459.80
Ext. Iron sight
13459.75
Ext. Fe line
13459.40

N

